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## Computer Program for Three Body Break Up Reaction

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A FORTRAN program is developed to calculate the energy spectrum for three body break up reaction at intermediate energy. Energy spectra are calculated on the basis of AGS (Alt, Grassberger and Sandhas) formalism assuming quasi free scattering with final state interaction. The calculated curves reproduced well energy spectra of  $^3\text{He}$  in coincidence with protons for  $^3\text{He}(\tau, \tau p)$  reaction and deuterons for  $^3\text{He}(\tau, \tau d)$  reaction at 120 MeV.

KEY WORDS Nuclear Reaction  $^3\text{He}(\tau, \tau p)$  at 120 MeV /  
Program for QF Scattering with FSI/

### I INTRODUCTION

Three body problems could be treated exactly on the basis of Faddeev's equations with given two body interaction potentials and the energy spectrum of nucleons from break up reaction of deuterons by nucleons could be successfully explained using a separable potential for nucleon-nucleon interaction<sup>1)</sup>. For the case where components of high angular momentum contribute to the two body interaction in the break up reaction, the problem is not so easy because that realistic separable potential has not yet been obtained and a long computer time needs to solve the integral equations. Furthermore if composite particles are concerned in the final state complicated reaction mechanism is presumed. At intermediate energies, however, continuous energy spectra of emitted particles show rather simple shape with large peaks due to quasi free scattering and some times with peaks for final state interaction appearing at low relative energies of the interacting two particles<sup>2)</sup>. Then it is reasonable to assume some simplifications in calculation for the break up reaction. Alt *et al.*<sup>3)</sup> have derived one dimensional integral equations for the three body scattering problem and derived a scattering amplitude at the special case where, in the first place, a quasi free process produces three particles and in the final state any two particles interact. We have obtained a computer program to calculate this amplitude and using it evaluated energy spectra for the break up reaction of  $^3\text{He}$  nucleus by  $^3\text{He}$  beam at 120 MeV.

### II EQUATIONS

Break up amplitude for three body break up reaction can be calculated using Eq. (5. 2) in Ref. 3 as follows,

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Program for Three Body Break Up Reaction

$$X_{p_1, 1m}(z) = - \sum_{r \neq 1} \langle \mathbf{p}_1 | T'_r(z) G_0(z) | 1, m; z \rangle + \sum_{r \neq 1} \langle \mathbf{p}_1 | T_1(z) G_0(z) T_r(z) G_0(z) | 1, m; z \rangle, \quad (1)$$

where  $T'_r$  are non separable "amplitude" and small compared with the two body amplitude  $T_1$ . In the calculation the following conditions are assumed. 1) two body amplitude  $T_1$  and  $T'_r$  have not any singularity on the energy shell, 2) the Green's function  $G_0$  at the last position in the second term does not given any singularity because the cancellation of amplitudes at two integration angles  $\mathbf{p}_1''$  and  $-\mathbf{p}_1''$ , and 3) a pole approximation is applied to integrate the other Green's function in the second term. Then the cross section is given as follows,

$$\frac{d^3\sigma}{d\Omega_1 d\Omega_2 dE_1} = \frac{2\pi}{\hbar^2} \cdot \frac{\mu_{in}}{k_{in}} \rho |M_+ + M_-|^2, \quad (2)$$

$$\begin{aligned} M_{\pm} &= \langle \mathbf{q}_1 | X_{\pm} | \mathbf{q}_0 \rangle \\ &= - \sum_{r \neq 1} \left( \frac{1}{S_{r1}} \right)^3 \langle \mathbf{p}'_r | T'_r(z - q_1^2) | \mathbf{p}_r \rangle \frac{1}{\left\{ \mathbf{p}'_1 - \frac{C_{r1}}{S_{r1}} (\mathbf{q}_1 \mp \mathbf{q}_0) \right\}^2 - Q} \\ &\quad \times \langle \mathbf{p}'_1 - \frac{C_{r1}}{S_{r1}} (\mathbf{q}_1 - \mathbf{q}_0) | 1, m; z \rangle \\ &\quad + \sum_{r \neq 1} \left( \frac{1}{S_{r1}} \right)^3 \int d\Omega'' \langle \mathbf{p}_1 | T_1(z - q_1^2) | \mathbf{p}_1'' \rangle \frac{\pi}{2} i \mathbf{p}_1'' \langle \mathbf{p}'_r | T'_r(z - q_1^2) | \mathbf{p}_r \rangle \\ &\quad \times \frac{1}{\left\{ \mathbf{p}'_1 - \frac{C_{r1}}{S_{r1}} (\mathbf{q}_1 - \mathbf{q}_0) \right\}^2 - Q} \langle \mathbf{p}'_1 - \frac{C_{r1}}{S_{r1}} (\mathbf{q}_1 \mp \mathbf{q}_0) | 1, m; z \rangle, \end{aligned} \quad (3)$$

$$p_1''^2 = z - q_1^2,$$

where  $\rho$  is the phase space for factor three body system in the final state.  $M_+$  and  $M_-$  are matrix elements for the target break up process and projectile break up process, respectively. The variable  $p_1^2$  and  $q_1^2$  have a dimension of energy and relate to the usual wave vector  $\mathbf{k}$  and mass  $m$ ,

$$\left. \begin{aligned} \mathbf{p}_1 &= [2m_2 m_3 (m_2 + m_3)]^{-1/2} (m_3 \mathbf{k}_2 - m_2 \mathbf{k}_3), \\ \mathbf{q}_1 &= [2m_1 (m_2 + m_3) (m_1 + m_2 + m_3)]^{-1/2} [m_1 (\mathbf{k}_2 + \mathbf{k}_3) - (m_2 + m_3) \mathbf{k}_1], \end{aligned} \right\} \quad (4)$$

and the variables in the  $i$ - $jk$  system are related to the variables in the  $j$ - $ki$  system through the following relations,

$$\left. \begin{aligned} \mathbf{p}_2 &= C_{21} \mathbf{p}_1 + S_{21} \mathbf{q}_1, \\ \mathbf{q}_2 &= -S_{21} \mathbf{p}_1 + C_{21} \mathbf{q}_1. \end{aligned} \right\} \quad (5)$$

where

$$\left. \begin{aligned} C_{21} &= - \left[ \frac{m_1 m_2}{(m_1 + m_3) (m_2 + m_3)} \right]^{1/2} = C_{12}, \\ S_{21} &= \sqrt{1 - C_{21}^2}, \end{aligned} \right\} \quad (6)$$

Four types of potential are assumed in the calculation of the initial interaction, that is Gaussian type, Yukawa type, Woods Saxson type and Woods Saxson for real potential with the first derivative of Woods Saxson for imaginary potential,

$$\langle \mathbf{p}_r | T_r(z - q_0^2) | \mathbf{p}'_r \rangle = T_r(\mathbf{p}'_r - \mathbf{p}_r), \quad (7)$$

$$= -\pi^{3/2} \frac{V}{\alpha^3} \exp\left[-\frac{(\mathbf{p}'_r - \mathbf{p}_r)^2}{4\alpha^2}\right], \quad \text{for Gaussian} \quad (8)$$

$$= -4\pi V \left[ \frac{1}{\alpha_1^2 + (\mathbf{p}'_r - \mathbf{p}_r)^2} + \frac{\eta}{\alpha_2^2 + (\mathbf{p}'_r - \mathbf{p}_r)^2} \right], \quad \text{for Yukawa} \quad (9)$$

$$= \int d\mathbf{r}^3 V(\mathbf{r}) e^{i(\mathbf{p}'_r - \mathbf{p}_r) \cdot \mathbf{r}}, \quad \text{for Woods Saxon } V(\mathbf{r}). \quad (10)$$

The form factor of the target nucleus is assumed as,

$$\begin{aligned} \langle \mathbf{p}_1 | 1, m; z \rangle &= (z - q_0^2) \phi_{1m}(\mathbf{p}_1), \\ \phi_{1m}(\mathbf{p}_1) &= \frac{\sqrt{\alpha}}{\pi} \frac{1}{\alpha^2 + \mathbf{p}_1^2}. \end{aligned} \quad (11)$$

S wave final state interaction between particle 2 and particle 3 relates to the effective range parameters at zero energy limit in the two body scattering,

$$|\langle \mathbf{p}_1 | T_1(z - q_1^2) | \mathbf{p}'_1 \rangle|^2 = \frac{C^2(\eta)}{4\pi^2} \cdot \frac{1}{C^2(\eta)q^2 + \left(-\frac{1}{a} + \frac{1}{2}r q^2\right)}, \quad (12)$$

$$\begin{aligned} q^2 &= (\mathbf{p}'_1 - \mathbf{p}_1)^2, \\ C^2(\eta) &= 2\pi\eta / [\exp(2\pi\eta) - 1], \\ \eta &= z_2 z_3 e^2 / \hbar v, \end{aligned}$$

where  $C(\eta)$  is the Coulomb penetration factor. For the  $l$ -th partial wave interaction in the final state Brait-Wigner type resonance form is assumed as follows,

$$|\langle \mathbf{p}_1 | T_1(z - q_1^2) | \mathbf{p}'_1 \rangle|^2 = A \frac{\Gamma_1^2}{(z - q_1^2 - E_1)^2 + \frac{1}{4}\Gamma_1^2} P_l(\cos\omega). \quad (13)$$

The angular integral of Eq. (3) is done analytically where the angular momentum of  $l$  is less than or equal to 2. The values of parameters in Eq. (8), (9), and (11) are transformed from the radial parameters in fm using following relation,

$$\alpha^2_{\text{MeV}} = \frac{\gamma}{\mu a_{\text{fm}}}, \quad \gamma = \frac{41.6}{2},$$

$\mu$ : reduced mass

### III COMPUTER PROGRAM

The computer program "AGSIA" calculates the three body break up cross section on the basis of AGS formalism. Seven types of card have to read in the format of free field as the input data. Three body kinematics is calculated using a subprogram "KINEMA" which is the same as the program developed by Ohlsen<sup>4</sup>), and the numerical integration of Eq. (10) is made using a sub-program "SIMPSON" which is a usual program of Simpson Integral. The matrix element in Eq. (3) is calculated using a sub-program "XMAT". Four types of initial interaction can be selected by **KCODE4** and five print out format can be selected by **KCODE3**. All calculated energy spectra are print out in units of  $10^{-26} \text{cm}^2/\text{sr}^2 \cdot \text{MeV}$ . as a function of the laboratory energy of particle 1. The FORTRAN programs are given in an Appendix.

The energy spectrum of  ${}^3\text{He}$  in coincidence with protons for  ${}^3\text{He}(\tau, \tau p)d$  reaction

## Program for Three Body Break Up Reaction

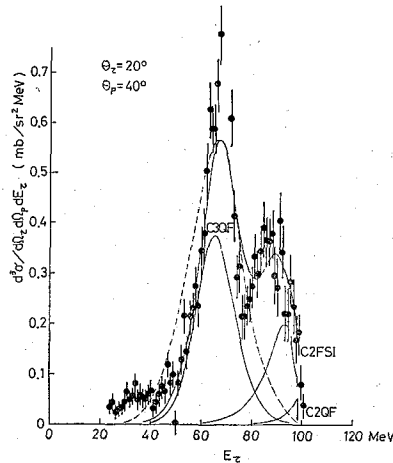


Fig. 1. Energy spectrum projected for the  ${}^3\text{He}(\tau, \tau p)d$  reactions at  $\theta_\tau=20^\circ$  and  $\theta_p=40^\circ$ . All solid curves are calculated on the basis of the AGS formalism. The dashed curve shows the calculated one of the simple spectator model.

at 120 MeV was calculated using the program of "AGSIA". Figure 1 shows the calculated curves at the angular set  $\theta_\tau=20^\circ$ ,  $\theta_p=40^\circ$  and  $\varphi_p=0^\circ$  (opposite side of, and in coplanar with, the beam) and shows the experimental energy spectrum which was obtained from the data in Ref. 2. The curves denoted as **C2QF** and **C2FSI** are calculated using only the first term at  $\gamma=2$  and the second term at  $\gamma=2$  in Eq. (1). The former corresponds to the cross section assuming the quasi free scattering of particle 1 ( ${}^3\text{He}$ ) and particle 3 (unobserved particle) and the latter corresponds to that for quasi scattering with the final state interaction of particle 2 and particle 3. The dashed curve is calculated using a simple impulsive spectator model. Nevertheless a normalization constant was needed to reproduce the experimental energy spectrum, the calculated energy spectrum is reproduced well using a reasonable parameter set.

### ACKNOWLEDGMENT

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Appendix

Instructions for use of "AGSIA"

Card 1 (general conditions in the calculation)

:KCODE1, KCODE2, KCODE3, KCODE4, IK, NO, FACT  
 KCODE1 = 1 print subtitle "XM3 IS NOT A COMPOSITE PARTICLE"  
 2 print subtitle "XM3=XM4+XM5 AND BREAKS TO SINGLET DEUTERON"  
 3 print subtitle "XM3=XM4+XM5 AND BREAKS TO TRIPLET p+n"  
 SYSTEM"

if any number is chosen, the program does not change to calculate the reaction

KCODE2 = 0 calculate the target breakup reaction ;  $M=M_+$   
 1 calculate the projectile breakup reaction ;  $M=M_-$   
 2 calculate the target breakup plus the projectile breakup reaction ;  $M=M_+ + M_-$   
 KCODE3 = 0 print out the kinematics of three body breakup reaction  
 1 print out all reaction amplitudes and phase space factor  
 2 print out the final cross sections  
 3 print out the cross sections for (1-2) quasi free, the cross sections for (1-3) quasi free and the final cross sections  
 4 print out all cross sections of components in Eq. (3) and the final cross sections  
 KCODE4 = 0 initial interaction of Gaussian type  
 1 initial interaction of double Yukawa type  
 2 initial interaction of Woods-Saxson type  
 3 initial interaction of Woods-Saxson (real) with the first derivative of the Woods-Saxson (imaginary)  
 LK number of resonance in the final state interaction  
 NO number of angular set  
 FACT factor of the second term by the first term in Eq. (3), and set 1 in the usual calculation.

Card 2 (kinematical parameters)

:XMP, XMT, XM1, XM2, XM3, Q, EPL, DE1L, ZZ  
 XMP mass of the projectile in atomic mass unit  
 XMT Mass of the target in atomic mass unit  
 XM1 Mass of the particle 1 in atomic mass unit  
 XM2 mass of the particle 2 in atomic mass unit  
 XM3 mass of the particle 3 in atomic mass unit  
 Q reaction Q value in MeV  
 EPL incident energy in MeV  
 DE1L energy increment in MeV  
 ZZ product of electric charges  $Z_2$  and  $Z_3$

Card 3 (form factor and effective range parameters)

:ALPHTO, ALPHAO, ERANGT  
 ALPHTO width of the form factor in fm  
 ALPHAO scattering length in fm  
 ERANGT effective range in fm

Card 4 (potential parameters for the first step interaction between particle 1 and particle 2.)

:VTPO1, RHTPO1, DHTPO1, YETAP1, VTPO2, RHTPO2, DHTPO2, YETAP2  
 VTPO1 real well depth in MeV  
 RHTPO1 real well width in fm  
 DHTPO1 real well diffuseness (for Gaussian or Woods-Saxson) or second well width in fm (for double Yukawa)  
 YETAP1 ratio of second Yukawa potential to the first Yukawa potential  
 VTPO2 imaginary well depth in MeV  
 RHTPO2 imaginary well width in fm  
 DHTPO2 imaginary well diffuseness (for Gaussian or Woods-Saxson) or the second well

Program for Three Body Break Up Reaction

width in fm (for double Yukawa)

YETAP2 ratio of the imaginary depth of second Yukawa to that of first Yukawa

Card 5 (potential parameters for the first step interaction between particle 1 and particle 3)  
:VTDO1, RHTDO1, DHTDO1, YETAD1, VTDO2, RHXDO2, DHTDO2, YETAD2  
similar to the Card 4

Card 6 (resonance parameters for the S wave final state interaction)

:COEF(1), ER(1) WIDTH(1)

COEF(1) coefficient of the Brait-Wigner resonance

ER(1) resonance energy in MeV

WIDTH(1) resonance width in MeV

If the resonances for the P wave and the D wave final state interactions are calculated, the Card 7 and Card 8 are used for the resonance parameters. If any resonance is not calculate, the COEF(1) in the Card 6 must be equal to zero. And the Card of angular set follows to the resonance Card.  
Card 7 (angular set)

:TH1R, TH2R, PHI2

TH1R polar angle of particle 1 in degrees in the laboratory

TH2R polar angle of particle 2 in degrees

PHI2 azimuthal angle of particle 2 in degrees. Set zero when the detectors for particle 1 and particle 2 are set opposite side of, in coplaner, with, the incident beam.

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SOURCE LIST
C PROGRAM AGS1A AGS00000
C CROSS SECTION IN UNITS OF 10**(-24) CM**2/MEV AGS00010
C AMPLITUDE IN UNITS OF 10**(-13) CM/(MEV**0.5) AGS00020
C ALPHA IN FERMI AGS00030
C V IN MEV/RH IN FERMI, NH IN FERMI AGS00040
C KCOD2 0 TARGET BREAK AGS00050
C 1 PROJECTILE BREAK AGS00060
C 2 TARGET BREAK AND PROJECTILE BREAK AGS00070
C AGS00080
0001 COMMON /DATA/AL1(300)+EPL(300)+E23(300)+E3(300)+E12(300)+2
1 TH1C(300)+TH2C(300)+TH3C(300)+THPC(300)+2
1 THCP2(300)+THP3(300)+2 HPOL(300)+2 HMO2(300)+2
1 TH3L(300)+2 PH1L(300)+2
COMMON /ALPH/ALPHA=ALPH+ERANGA*VTPD(2)+RHPTD(2)+DHPTD(2)+VETAP(2) AGS00090
1 VTD(2)+VH2D(2)+VH3D(2)+VETAD(2) AGS00100
0002 COMMON /RHSO/RCOE(4)+EM(4)+WIDTH(4) AGS00110
0003 COMMON /OUT/OUTFA2(2)+300)+H3(2)+300)+AL2(2)+2+300)+AL3(2)+2+300)
COMMON /KCODE/KCODE1+KCODE2+KCODE3+KCODE4 AGS00190
C HEAD INPUT DATA AGS00200
0008 READ(5*) KCODE1,KCODE2,KCODE3,KCODE4,LK,NH,FACTA AGS00220
0009 IF(KCODE1.EQ.0) GOTO 1 AGS00230
0010 WRITE(6,1000) GOTO 1 AGS00240
0011 PA(3)=1415027 AGS00250
0012 WRITE(6,1001) KCODE1,KCODE2,KCODE3,KCODE4,LK,NH,FACTA AGS00260
0013 GAHM=1.0/(4)+79 AGS00280
0014 FACT=SORT(1.0/(2)+0.6GAHM**3) AGS00290
0015 FACT=FACT1 AGS00300
0016 1 READ(6*) AMP,XT,XM1,XM2,XM3+0.0EPL,DELE1L,ZZ AGS00310
0017 WRITE(6,1001) AMP,XM1,XM2,XM3+0.0EPL,ZZ AGS00320
0018 IF(KCODE3.EQ.0) GOTO 4 AGS00330
C HEAD THE DATA OF FORM FACTOR FOR THE TARGET AGS00340
0019 READ(5*) ALPHAD,ALPHAD*ERANGT AGS00350
0020 WRITE(6,1002) ALPHAD,ALPHAD*ERANGT AGS00360
C HEAD THE DATA FOR INTERACTION WITH H2 AGS00370
0021 READ(5*) VPD1,RHPTD1,DHPTD1,VETAP1,VTD2,RHPTD2,DHPTD2,VETAP2
0022 WRITE(6,1003) VPD1,RHPTD1,DHPTD1,VETAP1,VTD2,RHPTD2,DHPTD2,VETAP2
0023 VPH(2)=VTD2 AGS00380
0024 VPH(3)=SORT((XM1+XM2)/(XM1+XM3)) AGS00390
0025 SXM1=SORT(XM1+XM3)/(XM2+XM3) AGS00400
0026 SXM3=SORT(XM2+XM3)/(XM2+XM3) AGS00410
0027 SXM2=SORT(XM2+XM3)/(XM2+XM3) AGS00420
0028 DHPTD(1)=FACT*(SXM1+RHPTD(1)) AGS00430
0029 RHPTD(2)=FACT*(SXM2+RHPTD(2)) AGS00440
0030 VETAP(1)=VETAP2 AGS00450
0031 VETAP(2)=VETAP2 AGS00460
0032 DHPTD(1)=1.0 AGS00470
0033 DHPTD(2)=1.0 AGS00480
0034 IF(VETAP3.EQ.0.0) GOTO 3 AGS00490
0035 DHPTD(1)=FACT*(SXM1+DHPTD(1)) AGS00500
0036 3 IF(VETAP2.EQ.0.0) GOTO 5 AGS00510
0037 DHPTD(2)=FACT*(SXM2+DHPTD(2)) AGS00520
0038 5 CONTINUE AGS00530
0039 ALPH=FACT1*(SX2+3*ALPH(1)) AGS00570
0040 ALPH=FACT1*(SX2+3*ALPH(1)) AGS00580
0041 ERANGA=FACT1/(SX2+3*ERANGT) AGS00590
0042 DD 10 1=14 AGS00600
0043 CMT(1)=0 AGS00610
0044 10 CONTINUE AGS00620
C HEAD THE DATA FOR INTERACTION WITH H3 AGS00640
0045 READ(5*) VTD1,RHPTD1,DHPTD1,VETAD1,VTD2,RHPTD2,DHPTD2,VETAD2
0046 WRITE(6,1003) VTD1,RHPTD1,DHPTD1,VETAD1,VTD2,RHPTD2,DHPTD2,VETAD2
0047 VTD(1)=VTD1 AGS00670
0048 VTD(2)=VTD2 AGS00680
0049 RHPTD(1)=AC1*(SXM1+RHPTD(1)) AGS00690
0050 RHPTD(2)=AC1*(SXM2+RHPTD(2)) AGS00700
0051 VTD(1)=VETAD1 AGS00710
0052 VTD(2)=VETAD2 AGS00720
0053 DHPTD(1)=1.0 AGS00730
0054 DHPTD(2)=1.0 AGS00740
0055 1 (VETAD1.EQ.0.0) GOTO 23 AGS00750
0056 DHPTD(1)=FACT*(SXM1+DHPTD(1)) AGS00760
0057 23 IF(VETAD2.EQ.0.0) GOTO 25 AGS00770
0058 DHPTD(2)=FACT*(SXM2+DHPTD(2)) AGS00780
0059 25 CONTINUE AGS00790
0060 DD 30 1=14 AGS00800
0061 1 (VETAD1.EQ.0) GOTO 38 AGS00810
0062 L=1 AGS00820
0063 WRITE(6,1004) L,COE(4,L),ER(4,L),WIDTH(4,L) AGS00830
0064 38 CONTINUE AGS00840
0065 40 CONTINUE AGS00850
0066 DD 300 11=14 AGS00860
0067 READ(5*) TH1L+TH2L+PH1ZL AGS00870
0068 WRITE(6,1007) TH1L+TH2L+PH1ZL AGS00880
C COMPUTE THE NEUTRONS AGS00900
0689 CALL LINEFM(EM,ALPH,ALPH*ERANGT,EM2,EM3,EM4,EM5,EM6,EM7,EM8,EM9,EM10)
1 ZPD,ZMT,XM1,ZM2,ZM3+0.0EPL,DELE1L,TH1L,TH2L,PH1ZL,LMAX,LMIN,
1 ICODE AGS00910
IF(KCODE3.EQ.0) GOTO 110 AGS00940
ERELTV=AMT+EPL*(AMP+XMT) AGS00950
TTO=AMT+ELTV AGS00960
XMT=AMP+XMT*(EXP+XMT) AGS00970
XMT2=AMP+XMT*(EXP+XMT) AGS00980
XMT3=XMT*(EXP+XMT)*(EXP+XMT) AGS00990
FACT3=PAI**2/ZPD**2 AGS01000
FACT2=FACT3*SORT(SORT(SORT(EM1)/ERELTV))*(GAHM+XM1**2+3*XM2**2+1.5)
AGS01010
0077 63D=SORT(EM1/TV) AGS01020
0078 DD 700 1=1+LK AGS01030
0079 L=1+LK AGS01040
0080 DD 100 1=LMIN,LMAX AGS01050
0081 K1=SORT(1.0/(2)+3*1) AGS01060
0082 P1=SORT(2+2*1) AGS01070
0083 1=1+L(1) AGS01080
0084 E2=E2L(1+1) AGS01090

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0085 E3=EPL+0.0L(1)+E2L(1+1) AGS01100
0086 DD 90 1=1+KCODE2 AGS01110
IF(KCODE2.EQ.1) AND(NH.EQ.1) GO TO 50 AGS01120
IF(KCODE2.EQ.2) AND(NH.EQ.2) GO TO 50 AGS01130
C TARGET BREAK AGS01140
0090 N1=1 AGS01150
THE TA1=TH1C(1) AGS01160
GOTO 40 AGS01170
0091 AGS01180
0092 AGS01190
C PROJECTILE BREAK AGS01200
0093 30 THE TA1=1.0-NH*TH1C(1) AGS01210
N1=2 AGS01220
40 CONTINUE AGS01230
THE TA2=1.0-NH*THC(1+1) AGS01240
PH1Z=PH1ZL AGS01250
0097 AGS01260
C COMPUTE A.G.S. AMPLITUDES AGS01270
CALL CMT(EM1,EM2,EM3,EM4,EM5,EM6,EM7,EM8,EM9,EM10,TH1L,THE TA1,THE TA2,PH1Z,ZZ,L)
AGS01280
DD TO J=1+2 AGS01290
R2(1)=J+1+AL2(2)+FACT2 AGS01300
A3(1)=J+1+AL3(2)+FACT2 AGS01310
AL2(1)=J+1+AL12(2)+FACT2+FACT4 AGS01320
AL3(1)=J+1+AL13(2)+FACT2+FACT4 AGS01330
IF(ABS(A2(1)+J+1))-L1.1.0E-37) A2(1)=J+1+0.0 AGS01340
IF(ABS(A3(1)+J+1))-L1.1.0E-37) A3(1)=J+1+0.0 AGS01350
IF(ABS(AL2(1)+J+1))-L1.1.0E-37) AL2(1)=J+1+0.0 AGS01360
IF(ABS(AL3(1)+J+1))-L1.1.0E-37) AL3(1)=J+1+0.0 AGS01370
70 CONTINUE AGS01380
90 CONTINUE AGS01390
100 CONTINUE AGS01400
110 CONTINUE AGS01410
112 CALL PH1ZL(1)=LMAX+KCODE1+KCODE2+KCODE3) AGS01420
IF(KCODE3.EQ.0) GOTO 300 AGS01430
200 CONTINUE AGS01440
300 CONTINUE AGS01450
STOP AGS01460
1000 FORMAT(1H1,ENERGY SPECTRUM OF THREE BODY BREAK UP REACTION*)
11 ZZ**10.4) AGS01470
1001 FORMAT(1H1,EM,ALPH,ALPH*ERANGT*3F10.4) AGS01480
11 ZZ**10.4) AGS01490
1002 FORMAT(1H1,ALPH,ALPH*ERANGT*3F10.4) AGS01500
103 FORMAT(1H1,PD1,PARAM, WITH XMT**3F10.4) AGS01510
1003 FORMAT(1H1,PD1,PARAM, WITH XMT**3F10.4) AGS01520
11 10TH) AGS01530
104 FORMAT(1H1,PD1,PARAM, WITH XMT**3F10.4) AGS01540
1004 FORMAT(1H1,PD1,PARAM, WITH XMT**3F10.4) PH1ZL+FD1.4) AGS01550
1010 FORMAT(1H1, KCODE1,2,3,4,LMAX,ANGLE SET AND FACT**4,615,FD1.4) AGS01560
END AGS01570
0001 SUBROUTINE XMAT(EM1,EM2,EM3,EM4,EM5,EM6,EM7,EM8,EM9,EM10,TH1L,THE TA1,THE TA2,PH1Z,ZZ,L)
0002 COMMON /HSLT/H12(2)+A13(2)+AL12(2)+AL13(2)
0003 COMMON /RHSO/RCOE(4)+EM(4)+WIDTH(4)
1 VTD(2)+VH2D(2)+VH3D(2)+VETAD(2)
COMMON /ALPH/ALPHA=ALPH+ERANGA*VTPD(2)+RHPTD(2)+DHPTD(2)+VETAP(2)
COMMON /RHSO/RCOE(4)+EM(4)+WIDTH(4)
COMMON /KCODE/KCODE1,KCODE2,KCODE3,KCODE4
DI=EM10*FL(2)+TI(2)+TI(2)+TI(2)
K=KCODE1
0009 PA(3)=1415027
0010 C01=COS(TH1+PA1/180.0)
0011 C02=COS(TH2+PA1/180.0)
0012 S1=SIN(TH1+PA1/180.0)
0013 S12=SIN(TH2+PA1/180.0)
0014 CP=2*C01*EPL+PA1/180.0)
0015 RHPTD(1)=XMT+XMT**3
0016 C12=SORT(XM1+XMT**3)/(XM2+XM3)
0017 C13=SORT(XM2+XMT**3)/(XM2+XM3)
0018 S12=SORT(1.0-C12**2)
0019 S13=SORT(1.0-C13**2)
0020 GAHM=(C12/S13)
0021 GAHM1=C13/S13
0022 AP2=1+C02*2.0L(C01+C02)-5*(1+S12)*CPH2)
0023 AP3=AP2
0024 Z2(1)=1+10*10-2.0*AP1+0.0C01
0025 T1=SORT(1.0)
0026 P125TH=SHH(F2*(X2**3)+X33)
0027 P135TH=SHH(F3*(X2**3)+X33)
0028 DD 45 1=1+2
0029 DD 51 1=1+3
0030 4=CGDFA
0031 IF(KCODE1.EQ.3) GOTO 42
4=CGDFA*(1+1)
0032 CONTINUE
0033 CALL F12E(1)=G02-VTD(1)+RHPTD(1)+DHPTD(1)+VETAP(1)+44)
TI(1)=1+1
0034 CALL F13E(1)=G02-VTD(1)+RHPTD(1)+DHPTD(1)+VETAP(1)+44)
TI(1)=1+1
0035 45 CONTINUE
0036 50 C02=AP2
C COMPUTE 3 BODY FACTORS AGS01980
0041 GFM1=3*EM1*(EM1+135TR)/(135TR**2+0) AGS01990
0042 GFM2=3*EM2*(EM2+135TR)/(135TR**2+0) AGS02000
0043 GFM3=3*EM3*(EM3+135TR)/(135TR**2+0) AGS02010
C COMPUTE AMPLITUDES AGS02020
0044 FACT=AMT AGS02030
0045 FACT2=2*(AMT(52)+3) AGS02040
0046 FACT3=3*(AMT(51)+3) AGS02050
DD 45 1=1+2 AGS02060
A1(1)=AMT+AL12(1)+F12(1)+GFM1 AGS02070
A1(1)=AMT+AL13(1)+F13(1)+GFM1 AGS02080
0050 CONTINUE AGS02100

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K. FUKUNAGA and S. KARIKI



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0051 30L#80*ALPH#(1+T1-GAMA12-1)/5*(GAM12-1)  AGS02130
0052 30L#80*ALPH#(1+T1-GAMA12-1)/5*(GAM12-1)  AGS02130
0053 (L3)=36*ET(CALPH*PA1)+36*(C3)+SUNT(CABS(C3)+P1+T1-GAMA12-1)-  AGS02130
30L#80*ALPH#(1+T1-GAMA12-1)/5*(GAM12-1)  AGS02130
0054 AL1(1)=(L3)+PA1*(FACT1)+FACT*(FLM(1)+T2(1)+FLM(2)+T2(1))+G12  AGS02170
AL1(2)=(L3)+PA1*(FACT2)+FACT*(FLM(1)+T2(1)+FLM(2)+T2(1))+G12  AGS02180
0055 AL1(3)=(L3)+PA1*(FACT3)+FACT*(FLM(1)+T2(1)+FLM(2)+T2(1))+G12  AGS02190
0056 AL1(2)=(L3)+PA1*(FACT13)+FACT*(FLM(1)+T2(1)+FLM(2)+T2(1))+G13  AGS02200
0057 RETURN  AGS02210
0058 END  AGS02220

0001 SUBROUTINE FLCP(LM,PI-LEZ2)  AGS02230
C  SUMROUTINE FOR F.S.I.  AGS02240
C  Z2=1+Z2 ELEC CHARGES  AGS02250
C  L ANGULAR MOMENTUM OF THE FSI STATE  AGS02260
C  L-TM RESONANCE CRITICAL ENERGY TYPE  AGS02270
COMMON/AM01M/ALPH4,ALPHA,ENANGA,VTM0(2),RHTP0(2),DHTP0(2),YETAP(2)  AGS02290
1,VTD(2),H1T0(2),H1TD(2),VETAD(2)  AGS02300
COMMON /RES/COFF(A),FR(C),WIDH(A)  AGS02310
DIMENSION FLM(3)  AGS02320
PA1=3.1415927  AGS02340
FACT=0.5/(PA1**2)  AGS02350
FLM(1)=0  AGS02360
FLM(2)=0  AGS02370
FLM(3)=0  AGS02380
IF(L=3) I=0.5  AGS02390
9 FLM(2)=0.5  AGS02400
0013 FLM(3)=0.5  AGS02410
RETURN  AGS02420
10 I=1+L  AGS02430
IF(Z2) Z=1+Z0  AGS02440
15 C=1.0  AGS02450
GO TO Z  AGS02460
20 YETA0=2*Z*PA1+Z*SQRT(ENANGA-ENANGA*(Z2)+Z*Z)/PI  AGS02470
YETA2=Z*(YETA0+YETA1)  AGS02480
C=YETA2*(I)*YETA2*PI-1.0  AGS02490
23 CONTINUE  AGS02500
IF(L=3) GOTD 25  AGS02510
ALPHALPHA=(1.5+YETA2)/ENANGA  AGS02520
9*ALPHALPHA*(ENANGA**2)+YETA2  AGS02530
FLM=C*ALPHALPHA/PA1  AGS02540
0027 FLM=C*CF*PI/PA1  AGS02550
25 CONTINUE  AGS02560
IF(COEF(L3)) I=1.5+3.0  AGS02570
30 DENOM=(PI**2*(H1TD(13)+H1TD(23)+WIDH(L3)+Z2/PA1)  AGS02580
FLM(C)=H1TD(L3)+Z2/PA1+COEF(L3)/DENOM  AGS02590
0032 FL=(C+PI**2)*(L3)+H1TD(L3)+COEF(L3)/DENOM  AGS02600
GO TO M0  AGS02610
35 FL=0.0  AGS02620
FL=0.0  AGS02630
40 FLM(1)=FACT*(FL+L*FR/PI)  AGS02640
FLM(2)=FACT*(FL+L*FL/PI)  AGS02650
RETURN  AGS02660
END  AGS02670

0001 SUBROUTINE F1STPR(TF,QA,VM,DM,YETAR,EA)  AGS02680
C FIRST SET TRANSITION AMPLITUDES  AGS02690
K=0 GAUSS TYPE POTENTIAL  AGS02700
1 YUKAWA TYPE  AGS02710
2 WOODS SAXON TYPE  AGS02720
3 REAL PART WOODS SAXON AND IMAG=1-ST DERIV  AGS02730
DIMENSION F(10)  AGS02740
PA1=3.1415927  AGS02760
IF(L=1) I=0.5 GOTD 10  AGS02770
IF(L=2) I=1.5 GOTD 20  AGS02780
GO TO 30  AGS02790
10 AK=0(OR1)/PA1  AGS02800
B=0/(2.0+PA1)  AGS02810
92=PA1*B  AGS02820
TIME=-V*EXP(B*Z)*A**3  AGS02830
RETURN  AGS02840
20 A=PA1*(C+PA1)+Y  AGS02850
R1=(H+H**2+D+Z**2)*DB  AGS02860
R2=(D+D**2+H**2)*DB  AGS02870
TIME=A*(1.0/81+Y*Z**2)/R2  AGS02880
RETURN  AGS02890
30 B=1.0+0.8H  AGS02900
DE=1.0+0.1  AGS02910
I=0.2+2.0  AGS02920
C(1)=B  AGS02930
C(2)=V  AGS02940
C(3)=DM  AGS02950
B(A)=DM  AGS02960
P(S)=4  AGS02970
CALL SMPDN(P(A),H=DEL I*MAX(S11,S12),IER)  AGS02980
IER=IER+1  AGS02990
GOTD(A=50,50,50+40+I,IER)  AGS03000
27 TIME=-DM*PA1*Y*EXP(DH+DM)  AGS03010
RETURN  AGS03020
0031 TIME=0.0  AGS03030
0032 RETURN  AGS03040
0033 END  AGS03050

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0001 FUNCTION GL(CALPHA,PA,T,GAMMA,L)  AGS03070
C ANGULAR INTEGRAL  AGS03080
PA1=3.1415927  AGS03100
RE IZ-ALPHALPHA+PA+PA*GAMMA+GAMMA*AT  AGS03110
F=AT**2+RE IZ-1+I**2+PA*PA+0.5*(GAMMA+GAMMA*PA)  AGS03120
F=L-0.8*RE IZ+GAMMA*PA  AGS03130
G=ALPHA*(GAMMA+AT)**2  AGS03140
S1=ABS(E+FA)  AGS03150
S2=ABS(F+FA)  AGS03160
SP=SQRT(S1)  AGS03170
SN=SQRT(S2)  AGS03180
SG=SQRT(S3)  AGS03190
GA=-2.0*PA1/56  AGS03200
IF(GE=0) GOTD 10  AGS03210
10 GAMMALOG(1)-SP*2.585/(BETAD-SG)  AGS03220
GO TO 15  AGS03230
10 GAMMA=0*PA1/BETA2  AGS03240
15 CONTINUE  AGS03250
IF(L=3) GO TO 40  AGS03260
IF(L=2) GO TO 30  AGS03270
IF(L=1) GO TO 20  AGS03280
GL=0  AGS03290
GO TO 999  AGS03300
20 GA1=2.0*PA1*(COP+SG)/  AGS03310
GO TO 999  AGS03320
GL=GA1-981  AGS03330
30 GA2=0.75*PA1/(C+G)  AGS03340
(G2-C-0.090-3.0*PA1*SG)/(2.0*G+3.0*PA1)*G  AGS03350
(C2-C-0.090)*I-2.0*G*(C1+0.090)  AGS03360
GL=GA2*(G2+D)+*(C2-1.0)*G  AGS03370
GO TO 999  AGS03380
40 GA3=3.0*PA1*(SP-2N)/G  AGS03390
GB=3.0*PA1/(2+0.090*3)  AGS03400
GC=C*(1-0.04*PI)-D*(G+PI)+2*(D*G+PI)  AGS03410
GL=GC+2U*(D+G)  AGS03420
GB*(GC+D)*D  AGS03430
GF=0.75*PA1/G  AGS03440
GH=(C5-DM)*F-0.8*G*F/(15.0*G**3)  AGS03450
GL=GH+DM*(3+D)-C*(3+DM)*G  AGS03460
999 CONTINUE  AGS03480
RETURN  AGS03490
END  AGS03500

0001 FUNCTION F3H(CALPHA,PA)  AGS03510
C FORM FACTOR OF HELIUM-3  AGS03520
PA1=3.1415927  AGS03530
FORM=SQRT(CALPHA)/(PA1*(ALPHA+ALPHA*PA))  AGS03540
RETURN  AGS03550
END  AGS03570

0001 SUBROUTINE SMPDN(P(A),H=DEL I*MAX(S11,S12),IER)  AGS03580
C DIMENSION F(10)  AGS03590
S11=0.0  AGS03600
S=0.0  AGS03610
H=0  AGS03620
H=H-A  AGS03630
IF(BA) Z=1+Z0  AGS03640
RETURN  AGS03650
20 IF(DLE) Z=Z*Z+Z  AGS03660
22 I=Z**2  AGS03670
RETURN  AGS03680
23 IF(HA=1) Z=2+Z0  AGS03690
24 I=Z**3  AGS03700
RETURN  AGS03710
0016 COMPUTE SIGMA(1)  AGS03720
25 H=H+Z*DM  AGS03730
NHALF=1  AGS03740
SUMH=CALPH*H+Z*0.73-D  AGS03750
S=SUMH*(FA-PA)/(R-PA)*H/A/6.0  AGS03760
DIVIDE (A-R) INTO 2,...,2+M-1 INTERVALS  AGS03780
COMPUTE SIGMA (2), SIGMA(3),... SIGMA(I)  AGS03790
DO 28 I=2,IMAX  AGS03800
S11=5  AGS03810
S=C+S*SUM(Z/D)^2/D  AGS03820
NHALF=NHALF+2  AGS03830
H=H+NHALF  AGS03840
FRST=A*(H+NHALF)/Z-D  AGS03850
SUMH=(F*H*Z)+P  AGS03860
S=SUMH*H  AGS03870
ELAST=NHALF-1  AGS03880
F=H-C*H+NHALF  AGS03890
DO 26 K=1,LAST  AGS03900
S11=S*F+K  AGS03910
26 SUMH=SUMH+(F**K)/P  AGS03920
SUMH=SUMH*2.0/PA/(3.0*H+NHALF)  AGS03930
S=S+SUMH  AGS03940
END  AGS03950

0035 COMPARE THE I-TH AND (I-1)ST RESULTS  AGS03960
27 IF(ABS(S-S11)-ABS(DEL(S)) 29=28-28  AGS04010
28 CONTINUE  AGS04020
IER=4  AGS04030
GO TO 30  AGS04040
30 I=0  AGS04050
29 I=0  AGS04060
28 I=0  AGS04070
RETURN  AGS04080
END  AGS04090

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0001      FUNCTION F (Y-D)                                A6504100
C          FUNCTION FOR SYMSON INTEGRAL                A6504110
0002      DIMENSION P(10)                                A6504120
0003      P(1)=1.0/3.1415927                            A6504130
0004      Q=PI(1)                                        A6504140
0005      W=PI(2)                                        A6504150
0006      P=PI(3)                                       A6504160
0007      D=PI(4)                                       A6504170
0008      E=PI(5)                                       A6504180
0009      IF (E+.E0.13) GO TO 20                        A6504200
0010      W=PI(10)/(PI*W)                              A6504210
0011      B=1/1.5*(E+PI*W)                              A6504220
0012      P=PI(4)                                       A6504230
0013      B=PI(10)                                     A6504240
0014      20 P=PI(8)-PI(10)                             A6504250
0015      B=PI(10)/(PI*W)                              A6504260
0016      F=PI(11)*B                                   A6504270
0017      RETURN                                         A6504280
0018      END                                           A6504290

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0001      SUBROUTINE I 318 MAX(ELMAX,ELI(1),PI,PLMAX,ELI(1),THLMAX,THDMAX
1 XHM=XH*AM1-XM2,AM3=0+PL-DFLELL,THL1,THL2,PHI1,PLMAX,LMIN
1 I (CODE)
A6504300
A6504310
A6504320
A6504330
A6504340
A6504350
A6504360
A6504370
A6504380
A6504390
A6504400
A6504410
A6504420
A6504430
A6504440
A6504450
A6504460
A6504470
A6504480
A6504490
A6504500
A6504510
A6504520
A6504530
A6504540
A6504550
A6504560
A6504570
A6504580
A6504590
A6504600
A6504610
A6504620
A6504630
A6504640
A6504650
A6504660
A6504670
A6504680
A6504690
A6504700
A6504710
A6504720
A6504730
A6504740
A6504750
A6504760
A6504770
A6504780
A6504790
A6504800
A6504810
A6504820
A6504830
A6504840

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C          COMPUTE MAXIMUM POSSIBLE ANGLES AND ENERGIES
A6504740
A6504750
A6504760
A6504770
A6504780
A6504790
A6504800
A6504810
A6504820
A6504830
A6504840

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0040      213 IF (TH1)HAB=THL1 214.214-.215
0041      215 IF (TH1)HAB=THL2 214.214-.216
0042      216 WRITE(6,3) TH1MAX,TH2MAX
0043      ICH=2
0044      01 TURN
0045      02 TURN
0046      03 TURN
0047      04 TURN
0048      05 TURN
0049      06 TURN
0050      07 TURN
0051      08 TURN
0052      09 TURN
0053      10 TURN
0054      11 TURN
0055      12 TURN
0056      13 TURN
0057      14 TURN
0058      15 TURN
0059      16 TURN
0060      17 TURN
0061      18 TURN
0062      19 TURN
0063      20 TURN
0064      21 TURN
0065      22 TURN
0066      23 TURN
0067      24 TURN
0068      25 TURN
0069      26 TURN
0070      27 TURN
0071      28 TURN
0072      29 TURN
0073      30 TURN
0074      31 TURN
0075      32 TURN
0076      33 TURN
0077      34 TURN
0078      35 TURN
0079      36 TURN
0080      37 TURN
0081      38 TURN
0082      39 TURN
0083      40 TURN
0084      41 TURN
0085      42 TURN
0086      43 TURN
0087      44 TURN
0088      45 TURN
0089      46 TURN
0090      47 TURN
0091      48 TURN
0092      49 TURN
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0098      55 TURN
0099      56 TURN
0100      57 TURN
0101      58 TURN
0102      59 TURN
0103      60 TURN
0104      61 TURN
0105      62 TURN
0106      63 TURN
0107      64 TURN
0108      65 TURN
0109      66 TURN
0110      67 TURN
0111      68 TURN
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0113      70 TURN
0114      71 TURN
0115      72 TURN
0116      73 TURN
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0123      80 TURN
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0125      82 TURN
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0198      155 TURN
0199      156 TURN
0200      157 TURN
0201      158 TURN
0202      159 TURN
0203      160 TURN
0204      161 TURN
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0223      180 TURN
0224      181 TURN
0225      182 TURN
0226      183 TURN
0227      184 TURN
0228      185 TURN
0229      186 TURN
0230      187 TURN
0231      188 TURN
0232      189 TURN
0233      190 TURN
0234      191 TURN
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0237      194 TURN
0238      195 TURN
0239      196 TURN
0240      197 TURN
0241      198 TURN
0242      199 TURN
0243      200 TURN
0244      201 TURN
0245      202 TURN
0246      203 TURN
0247      204 TURN
0248      205 TURN
0249      206 TURN
0250      207 TURN
0251      208 TURN
0252      209 TURN
0253      210 TURN
0254      211 TURN
0255      212 TURN
0256      213 TURN
0257      214 TURN
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0259      216 TURN
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0261      218 TURN
0262      219 TURN
0263      220 TURN
0264      221 TURN
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0269      226 TURN
0270      227 TURN
0271      228 TURN
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0273      230 TURN
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0285      242 TURN
0286      243 TURN
0287      244 TURN
0288      245 TURN
0289      246 TURN
0290      247 TURN
0291      248 TURN
0292      249 TURN
0293      250 TURN
0294      251 TURN
0295      252 TURN
0296      253 TURN
0297      254 TURN
0298      255 TURN
0299      256 TURN
0300      257 TURN
0301      258 TURN
0302      259 TURN
0303      260 TURN
0304      261 TURN
0305      262 TURN
0306      263 TURN
0307      264 TURN
0308      265 TURN
0309      266 TURN
0310      267 TURN
0311      268 TURN
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0313      270 TURN
0314      271 TURN
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0317      274 TURN
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0319      276 TURN
0320      277 TURN
0321      278 TURN
0322      279 TURN
0323      280 TURN
0324      281 TURN
0325      282 TURN
0326      283 TURN
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0329      286 TURN
0330      287 TURN
0331      288 TURN
0332      289 TURN
0333      290 TURN
0334      291 TURN
0335      292 TURN
0336      293 TURN
0337      294 TURN
0338      295 TURN
0339      296 TURN
0340      297 TURN
0341      298 TURN
0342      299 TURN
0343      300 TURN
0344      301 TURN
0345      302 TURN
0346      303 TURN
0347      304 TURN
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