

Subwavelength-grating metamaterial integrated devices for the near- and mid-infrared wavelengths

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ABSTRACT

The subwavelength patterning of planar structures is now widely used in silicon photonics, enabling the synthesis of metamaterials with engineered optical properties, including refractive index, dispersion, and anisotropy. A wide range of integrated devices based on subwavelength grating (SWG) metamaterials have been demonstrated at telecom wavelengths, some with unprecedented performance. The benefits of SWG metamaterials can be leveraged not only in the typical telecom near-infrared bands, but also at the longer mid-infrared wavelengths. In this invited presentation, we will review our latest developments in SWG-based silicon and germanium photonic devices for the near- and the mid-infrared.

Keywords: Silicon photonics, Integrated optics, Subwavelength gratings, Metamaterials, Near-infrared, Mid-infrared, Waveguides, Off-chip couplers

1. INTRODUCTION

Since their early demonstration at NRC Canada¹⁻⁷, subwavelength grating (SWG) metamaterials in silicon waveguides have been advantageously used to control the flow of light in integrated photonic devices⁸. The refractive index, wavelength dispersion, birefringence, and anisotropy of nanophotonic waveguides can be controlled by judiciously choosing the geometrical parameters of the lithographically defined patterns. This enables the synthesis of metamaterials on-chip, with engineered optical properties. At the near-infrared wavelengths of the 1.55- μm telecom band, integrated optical components based on SWG metamaterials — including waveguides, beam splitters, multimode interference couplers, polarization splitters, Bragg filters, and fiber-chip couplers — have been demonstrated with unprecedented performance⁹.

The benefits of SWG metamaterial engineering can also be harnessed at longer wavelengths. The mid-infrared band, comprising the wavelength range of 2–15 μm , holds promise for important emerging applications, particularly in sensing and free-space optical communications¹⁰. While silicon-on-insulator (SOI) is becoming established as a leading platform for photonic integration, conventional silicon waveguides have prohibitive loss beyond $\lambda \sim 4 \mu\text{m}$, due to the strong absorption of the silicon dioxide cladding at these longer wavelengths¹¹. Various alternatives have been proposed using materials with a wider transparency range (e.g., sapphire, germanium on silicon, etc.)¹²⁻¹⁴. We have developed all-silicon and all-germanium SWG metamaterial waveguide platforms with the operational range extending into the mid-infrared¹⁵⁻¹⁸.

Efficient and broadband fiber-chip coupling of light is one of the most significant challenges in silicon photonics¹⁹. This issue is due to the mode size mismatch between optical fibers (with a typical diameter of $\sim 10 \mu\text{m}$) and integrated photonic wires (cross-section of $\sim 500 \text{ nm} \times 220 \text{ nm}$ at 1550-nm wavelength). To cope with the fiber-chip coupling

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problem, edge couplers and surface grating couplers are the most used devices, with the latter offering important advantages such as wafer-scale testing and robust misalignment tolerance²⁰. A surface grating coupler is a waveguide with a (quasi) periodic perturbation that converts the guided mode into a free-propagating plane wave²¹. The radiated field can be collected by an optical fiber that is positioned above the chip. The coupling efficiency (the fraction of input power that is coupled into the optical fiber) and the 1-dB bandwidth (the range of wavelengths for which the coupling efficiency is ~80% of its peak value) are the two important parameters in surface grating couplers²². State-of-the-art surface grating couplers have a coupling efficiency–bandwidth product of ~60 nm and incorporate sophisticated techniques such as multilayering^{24,25} and plasmonics²⁶, or use non-conventional optical fibers with reduced mode field diameters^{25,26}.

In this work, we will show some of our latest advances in silicon photonic components using SWG metamaterials for both the near- and mid-infrared wavelengths, with the emphasis on off-chip couplers. Specifically, we will present a broadband and highly efficient grating coupler using subwavelength grating metamaterials for the near-infrared and a micro-antenna for a novel mid-infrared suspended germanium platform with subwavelength-grating lateral cladding.

2. ZERO-ORDER GRATING COUPLER FOR THE NEAR-INFRARED BAND

A zero-order grating coupler is illustrated in Fig. 1. It comprises a periodic waveguide of length L , with a subwavelength period Λ and a duty cycle $DC = a/\Lambda$, and a silicon prism with an angle ϕ_{prism} between the input and output surfaces. The prism is tilted at ϕ_{clad} degrees and has an antireflective coating on its output surface. A linear taper of length L_{taper} is used to adiabatically increase the mode size of the interconnecting waveguide. Then, a fork-shaped transition of length L_{fork} adapts this mode to the Floquet mode of the grating.

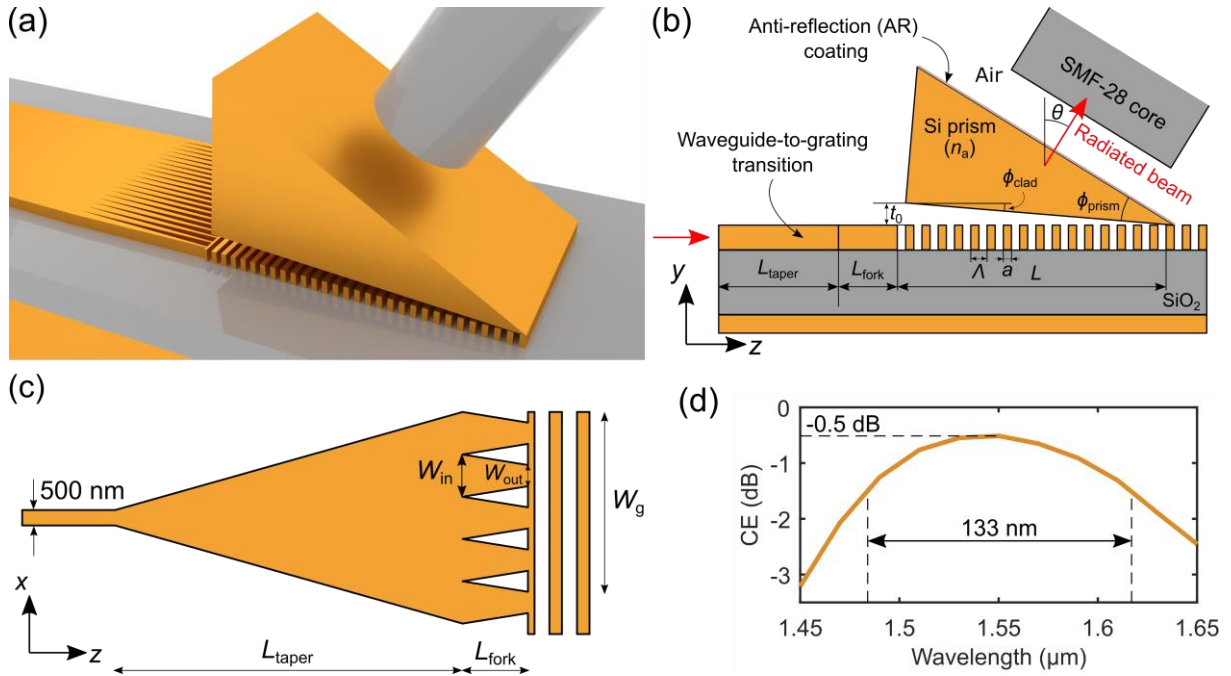


Figure 1. (a) Schematic of a zero-order grating coupler, including the homogeneous-to-SWG injection stage and the core of the single-mode optical fiber. (b) Schematic of a zero-order grating coupler (side view). (c) Schematic of the homogeneous-to-SWG injection stage (top view). (d) 3D-FDTD simulated coupling efficiency as a function of the wavelength.

The radiation angle θ in surface grating couplers is determined by²¹

$$\theta = \sin^{-1} \left(\frac{n_{\text{eff}}}{n_a} + m \frac{\lambda}{n_a \Lambda} \right), \quad (1)$$

where n_{eff} is the effective index of the Floquet mode supported by the grating waveguide, n_a is the refractive index of the superstrate, m is the diffraction order, λ is the operating wavelength, and A is the grating period. In conventional grating couplers, Eq. (1) is satisfied for $m = -1$ order²¹. The explicit dependence of the radiation angle on the wavelength is the primary cause of narrow bandwidth in surface grating couplers. This bandwidth limitation can be overcome by imposing $m = 0$, such that Eq. (1) becomes the zero-order grating coupler equation:

$$\theta = \sin^{-1} \left(\frac{n_{\text{eff}}}{n_a} \right). \quad (2)$$

To enable radiation in the zeroth order, i.e., via evanescent coupling, the period A is reduced to operate in the subwavelength regime ($A < 0.5\lambda/n_{\text{eff}}$) and a high-refractive-index material is used as a superstrate ($n_a > n_{\text{eff}}$). Under these conditions, the bandwidth fundamentally depends on the SWG and material dispersions of n_{eff} and n_a , respectively. To maximize the bandwidth, we choose the geometry that minimizes the SWG dispersion by operating as far as possible from the Bragg regime, i.e., DC = 50% and $A = 2 \times \text{MFS}$, where MFS is the minimum feature size of the fabrication process. In our case, $A = 200$ nm. The coupling efficiency is optimized by tilting the silicon prism ($L = 20 \mu\text{m}$, $\phi_{\text{prism}} = 35.7^\circ$, $\phi_{\text{clad}} = 1^\circ$). According to our 3D-FDTD simulations, a peak coupling efficiency of -0.5 dB and a 1-dB bandwidth of 133 nm are achieved [see Fig. 1(d)]. The grating width $W_g = 15 \mu\text{m}$ maximizes the overlap with the optical fiber mode in the x direction. A detailed description of our design flow can be found in our theoretical paper²³. The structural parameters of the input injection stage are $L_{\text{taper}} = 200 \mu\text{m}$, $L_{\text{fork}} = 3 \mu\text{m}$, $W_{\text{in}} = 0.5 \mu\text{m}$, and $W_{\text{out}} = 0.3 \mu\text{m}$.

The surface grating couplers were fabricated by electron beam lithography and inductively coupled (ICP) high-density plasma etching on an SOI wafer with 220-nm Si and 3- μm SiO₂ layers. A silicon prism with a base of 2 mm \times 2 mm was suspended on top of the subwavelength grating using a holder and a micro-positioning stage with tilting capabilities. An SEM image of the fabricated coupler is shown in Fig. 2(a).

The coupling efficiency and the bandwidth were measured using two complementary experiments. First, light was coupled in the chip via diffractive surface grating couplers and out of the chip via the zero-order grating coupler under test. The bandwidth of the measured spectral response, ~ 30 nm, coincides with that of the input conventional grating couplers, confirming the broad bandwidth of the zero-order grating coupler. By subtracting out the loss of the characterization setup and the propagation losses of the waveguides, this experiment provided an upper bound for the coupling efficiency of -1.0 dB. Subsequently, the bandwidth was measured by injecting light into the chip through the chip facet, which does not limit the spectral response. We obtained a 1-dB bandwidth of 94 nm. A photograph of the facet-to-prism-coupling experimental setup is shown in Fig. 2(b).

Our zero-order grating coupler can be lithographically patterned using standard fabrication processes in microelectronics and has a demonstrated coupling efficiency–bandwidth product of ~ 75 nm, the highest value yet reported in the literature for surface coupling to an SMF-28 optical fiber. We believe these results open new venues for the development of high-performance surface grating couplers.

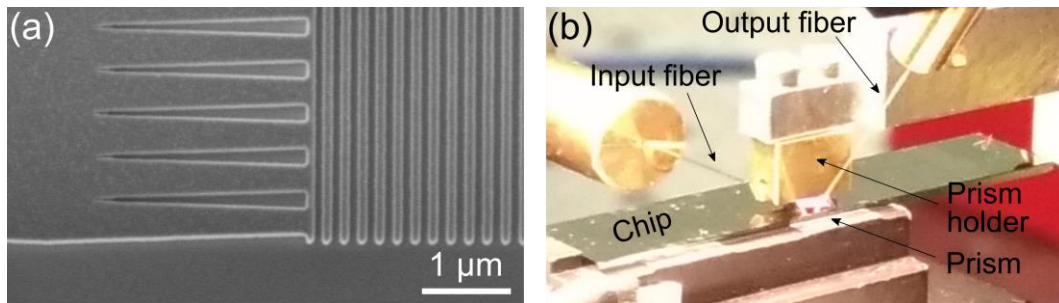


Figure 2. (a) SEM image of the beginning of a zero-order grating couplers, showing the input waveguide-to-grating stage and the first microns of the subwavelength grating. (b) Photograph of the characterization setup that was used to measure the 1-dB bandwidth of the zero-order grating coupler.

3. SUSPENDED GERMANIUM MICRO-ANTENNA FOR THE MID-INFRARED BAND

Here we present a broadband surface coupler for the suspended germanium platform with subwavelength grating lateral cladding for the mid-infrared wavelength range at a central wavelength of $7.67 \mu\text{m}$ (see Fig. 3)²⁷. This germanium platform is based on Ge-on-SOI wafers with thinned Si layer. Suspended waveguides comprise a germanium core that is anchored to lateral germanium slabs by a periodic cladding operating in the subwavelength regime (width W_{clad} , period Λ_{SWG} , duty cycle $\text{DC} = a_{\text{SWG}}/\Lambda_{\text{SWG}}$). The lateral cladding has a three-fold function: (i) to allow the flow of an HF etching solution that removes the SiO_2 bottom layer of the original Ge-on-SOI wafer, (ii) to hold the suspended structures, and (iii) to provide the lateral mode confinement that is required for light guiding. As illustrated in Fig. 3, the proposed suspended germanium fiber-chip surface coupler is formed by three suspended grating periods of pitch Λ and duty cycle $\text{DC} = a/\Lambda$ and an adaptation section with a hole and a germanium strip of lengths b_{ad} and a_{ad} , respectively.

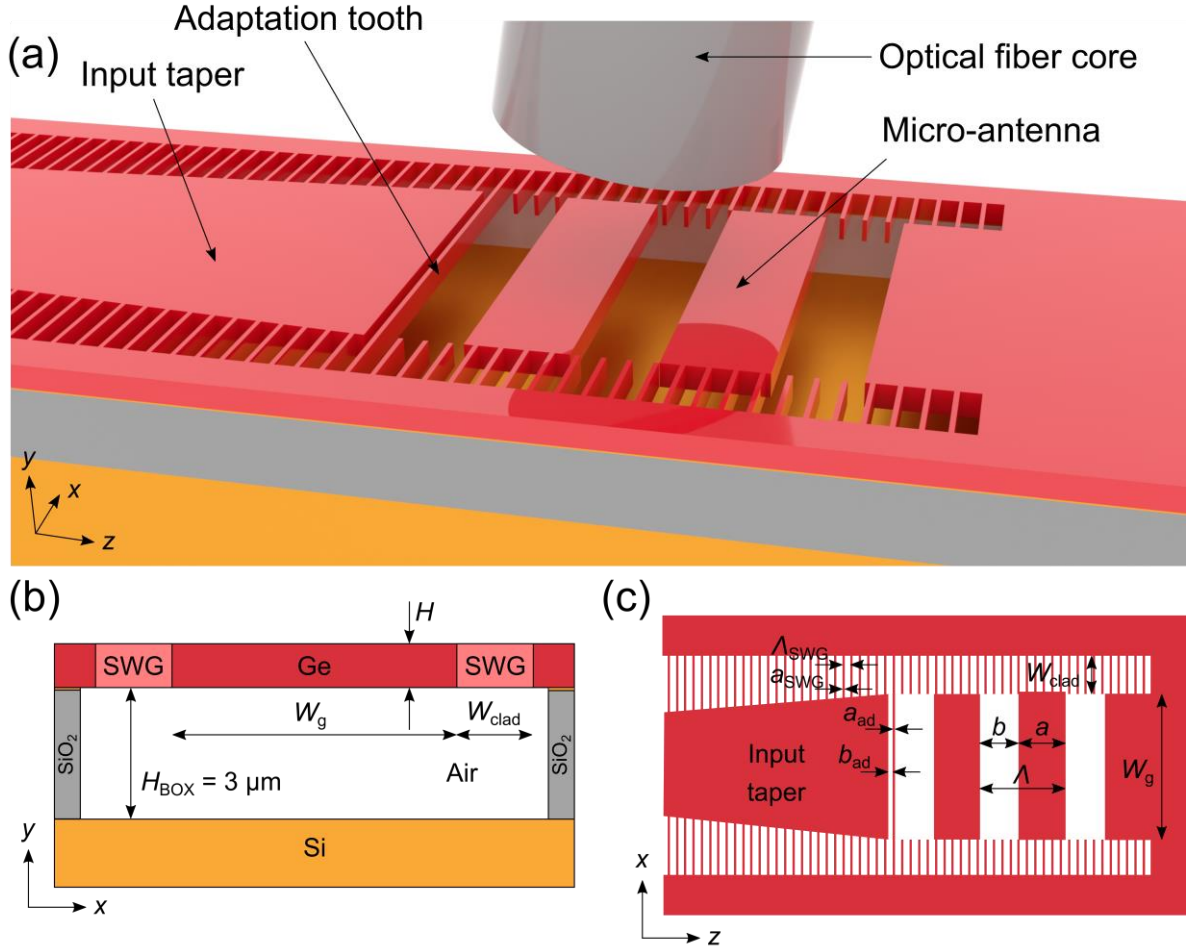


Figure 3. Schematics of the micro-antenna-type fiber-chip coupler for the SWG-cladding suspended germanium platform. (a) 3D view, including the optical fiber core and the input suspended taper. (b) Front view. (c) Top view, including the input taper. The micro-antenna comprises only three radiative elements, with a total length that is comparable to the operating wavelength.

Since the Ge-air index contrast is higher than that in silicon waveguides ($n_{\text{Ge}} \sim 4 > n_{\text{Si}} \sim 3.5$), the photonic bandgaps of a germanium grating are wider and the range of periods that enable radiation but operate far away from the Bragg regime is smaller²⁸. As a result, the design space of broadband and tolerant surface grating couplers is reduced compared to conventional designs in the near-infrared band. Thus, instead of using $m = -1$ in Eq. (1), we relax the typical single-beam design constraint and allow radiation in no more than two diffraction orders simultaneously, provided that only one order carries most of the power. The two-beam condition is satisfied if²⁷

$$A < \frac{\lambda}{n_a}, \quad (3)$$

where n_a is the refractive index of the upper medium (air).

At long-wave infrared wavelengths ($\lambda = 7 - 15 \mu\text{m}$), commercial chalcogenide optical fibers have high numerical aperture, which leads to mode field diameters (MFDs) that are small relative to the wavelength. For example, an SMF-28 optical fiber at $1.55 \mu\text{m}$ ²⁹ has $\text{MFD}/\lambda = 10.4/1.55 = 6.7$, while an IRFlex's IRF-Se-12 at $7.7 \mu\text{m}$ ³⁰ has $\text{MFD}/\lambda = 13.6/7.7 = 1.8$. Consequently, surface grating couplers in the long-wave infrared should operate as optical micro-antennas with much stronger radiation than conventional grating couplers in the near-infrared band.

Using our in-house eigenmode expansion simulator (FEXEN³¹), we choose the best design with high coupling efficiency to an IRF-Se-12 optical fiber, radiation angle $< 20^\circ$ and high tolerance to fabrication imperfections ($A = 7.6 \mu\text{m}$, DC = 55%). Then, we reduce back-reflections by adapting the fundamental mode of input waveguide to that of the micro-antenna waveguide ($a_{\text{ad}} = 200 \text{ nm}$, $b_{\text{ad}} = 400 \text{ nm}$). Further details on our design methodology can be found in our previous theoretical work²⁷. Using only three radiative elements, we achieve 3D-FDTD simulated coupling efficiency of -4 dB and 1-dB bandwidth of 436 nm [see Fig. 4(a)]. The latter is a fractional bandwidth (BW/λ) of $\sim 6\%$, around twice the fractional bandwidth of surface grating couplers in the near-infrared band. Furthermore, a high tolerance to fiber tilt misalignments, or angular bandwidth, of $\pm 10^\circ$ is reported [see Fig. 4(c)], which is almost a three-fold improvement over conventional silicon grating couplers at 1550-nm telecom wavelengths. In addition, 2D FDTD simulations reveal that the design is tolerant to fabrication errors of $\pm 150 \text{ nm}$. Figure 4(b) shows an electric field propagation for the TE polarization and $\lambda = 7.67 \mu\text{m}$. An SEM image of a suspended germanium micro-antenna, including the input subwavelength-grating waveguide and taper, is shown in Fig. 4(d). To provide mechanical robustness, the lateral cladding of the micro-antenna was not etched, which does not affect the field propagation due to the short length of the structure. While the coupling efficiency has not yet been experimentally corroborated, we measured an angular bandwidth of, at least, 15° . These results constitute a new route for the development of high-performance fiber-chip surface couplers at long-wave infrared wavelengths.

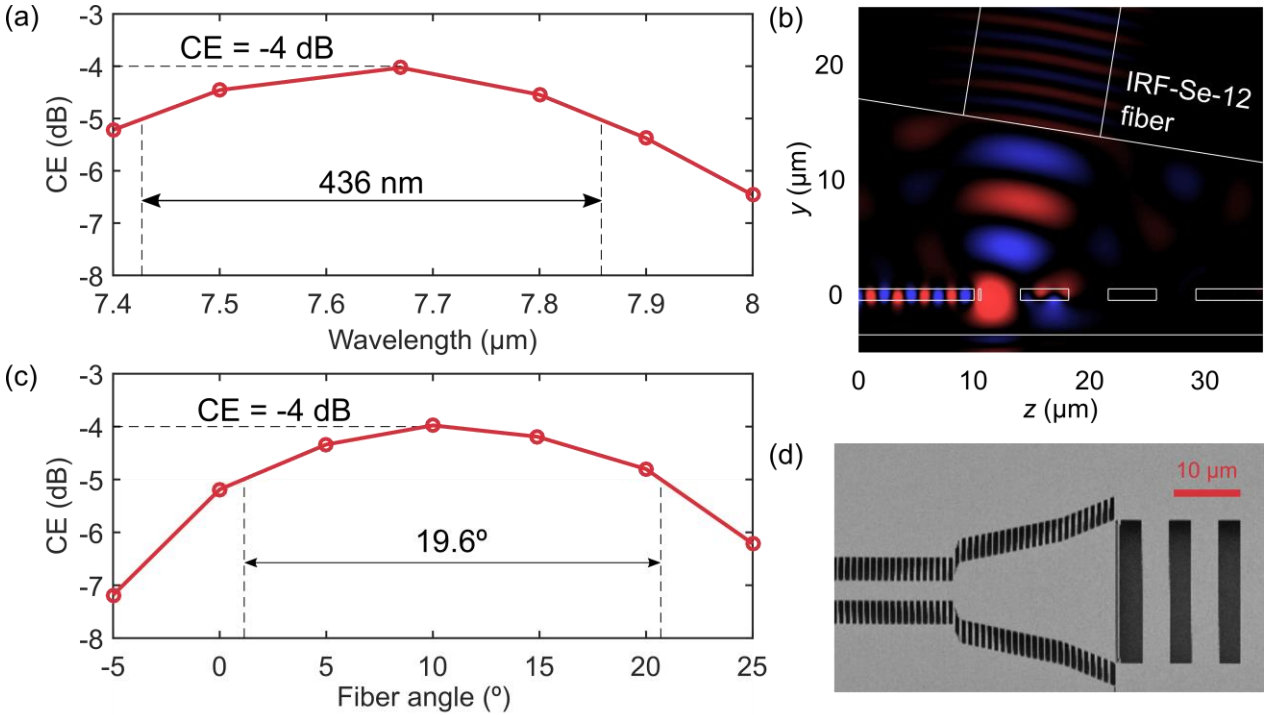


Figure 4. 3D-FDTD simulated coupling efficiency of the suspended germanium micro-antenna as a function of (a) the wavelength and (c) the optical fiber angle. (b) 2D-FDTD electric field propagation for TE polarization at 7.67- μm wavelength. (d) SEM image of a fabricated suspended germanium micro-antenna, including the input waveguide and taper.

ACKNOWLEDGMENTS

The authors acknowledge funding from Universidad de Málaga; Ministerio de Ciencia, Innovación y Universidades (MCIU) (PID2019-106747RB-I00); Consejería de Economía, Conocimiento, Empresas y Universidad (CECEU) (UMA18-FEDERJA-219, PY18-1453, PY18-793); and National Research Council of Canada (NRC) Collaborative Science, Technology and Innovation Program (CSTIP) (HTSN 209).

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