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- 1 Use of green solvents as pre-treatment of
- ² dissolving pulp to decrease CS₂ consumption

3 from viscose production

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8 Abstract

9 Choline chloride-based deep eutectic solvents are widely used in biomass processing. In this work, four 10 different green solvent mixtures were used as pre-treatment of acid sulphite dissolving pulp with the 11 hypothesis of increasing the possibilities to produce viscose fibres and decreasing the use of the harmful 12 and toxic carbon disulphide in the process. The experiments were performed at two different pulp to solvent 13 mass ratios. Pulp quality parameters were also measured to determine the suitability of the pre-treatment: 14 α -cellulose, viscosity, lignin and pentosan content. In addition, X-ray diffraction analysis of pulps at the 15 best solid to liquid ratio was performed to obtain the influence of the crystallinity index. Best results were 16 obtained with the use of lactic acid, with reactivity values close to 94 %, giving a reduction of CS₂ usage 17 of 15.83 %. Furthermore, a linear relationship between the crystallinity index calculated by the XRD and 18 reactivity with a regression factor of 0.87 was found.

19 Keywords: Deep eutectic solvents, Reactivity, Dissolving Pulp, Crystallinity

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21 Introduction

The growing concern about environmental issues has led researchers to find newer 22 technologies to solve conventional problems. In this sense, the search of greener solvents 23 to be used industrially has become of great importance (Zdanowicz et al. 2018). As a 24 result, Abbott et al. (2003) proposed deep eutectic solvents (DES) as an alternative to 25 traditional solvents. DES systems are a mixture of two or more components with a final 26 27 melting point much lower than the individual components (Kumar et al. 2016) which makes it liquid at room temperature (Procentese and Rehmann 2018). These solvents are 28 29 usually composed by a quaternary ammonium, phosphonium or sulfonium cation or a metal chloride (Smith et al. 2014), defined as Hydrogen Bond Acceptor (HBA) and a 30 Hydrogen Bond Donor (HBD). 31

32 Depending on the components employed to form the solvent, DES can be classified in four types (Zdanowicz et al. 2018): (1) Organic salts and metal chlorides; (2) Organic 33 salts and metal hydrates; (3) Organic salts and organic compounds (carboxylic acids, 34 alcohols, or amides); and (4) Metal chlorides and organic compounds (amides, alcohols). 35 These solvents have similar properties to Ionic Liquids (IL): low vapour pressure, 36 chemical and thermal stability, non-flammability and can be tailored (Wilpiszewska and 37 Spychaj 2011). However, DES mixtures exhibit some advantages when compared with 38 IL, i.e. easier to prepare, cheaper and have higher biodegradability (Ling et al. 2020). 39 These characteristics make DES to be used in a wide range of research areas: metal 40 41 processing (Zhang et al. 2012; Smith et al. 2014), biotechnology and bioengineering (Mbous et al. 2017), gas separation (García et al. 2015) or biomass processing 42 43 (Zdanowicz et al. 2018; Kalhor and Ghandi 2019) among others.

44 Regarding biomass processing, the use of DES has focused on lignocellulosic materials because of their ability to dissolve lignin with the almost negligible dissolution of 45 cellulose (Francisco et al. 2012), making biomass suitable for further processing. 46 However, lignin is not the only undesirable component in lignocellulosic materials. 47 Hemicelluloses, in the form of pentosan, can hinder the processability of this kind of 48 materials, in this sense, enzymatic treatment (Kaur et al. 2016) or alkali treatment (Kaur 49 et al. 2017) can be used effectively. The application of DES to lignocellulosic biomass 50 covers a wide range of steps during biomass processing: pre-treatment (Fang et al. 2017; 51

52 Tommasi et al. 2017; Shen et al. 2019), delignification, (Jablonský et al. 2015; Liu et al. 53 2017; Chen and Wan 2018), extraction (Huang et al. 2017; Cao et al. 2019; Deng et al. 2019) and reaction media (da Silva Lacerda et al. 2015; Sert et al. 2018; Lou et al. 2019). 54 Researches have tested several DES in biomass: Using different HBD's (Gunny et al. 55 2015; Ling et al. 2020); different HBA's (Francisco et al. 2012; Abdulmalek et al. 2017) 56 or even a different kind of DES (Biswas et al. 2006; Supeno et al. 2014). For the 57 components of the DES used in this field, Choline Chloride (ChCl) has been extensively 58 59 used as HBD, due to its availability and biodegradability (Gadilohar and Shankarling 2017). Carboxylic acids such as malic acid (MA), oxalic acid (OxA) and lactic acid (LA) 60 61 and amides such as urea (Ur) can be used as HBA for treatment of lignocellulosic biomass (Tan et al. 2019). 62

63 Cellulose is the most abundant natural polymer on earth, and dissolving pulp is the primary source of high purity cellulose (Li et al. 2018). Dissolving pulp can be used to 64 65 produce a wide variety of products such as cellulose acetates, cellulose nitrates, cellulose ethers, viscose fibres and lyocell fibres (Miao et al. 2014). Among the end-use products 66 67 mentioned above, viscose production is the main consumer of dissolving pulp; in fact, 70 % of viscose was produced from dissolving pulp (Kumar and Christopher 2017). Carbon 68 69 disulphide (CS₂) is used in the xanthation phase of the viscose process, to dissolve alkali 70 cellulose formed in the mercerisation phase. This compound is toxic and environmentally 71 harmful (Duan et al. 2015). Therefore, CS₂ consumption needs to be reduced as much as possible and as a result, mitigate the adverse effects that this reagent can produce on the 72 73 process, either economically or environmentally (Li et al. 2018). Cellulose reactivity is 74 the key parameter to improve for reducing the use of CS₂ within the viscose process. 75 Therefore, it is crucial to make the viscose process more sustainable with the 76 environment. Cellulose reactivity is defined as the ability of chemicals to dissolve cellulose, and it has a direct relationship with CS₂ consumption (the higher the reactivity, 77 the lower the CS₂ needed). Such parameter can be determined by several methods such 78 79 as Iodine sorption, NMR spectroscopy, viscose filterability and Fock's test (Arce et al. 2020). 80

Treatments of different nature can improve cellulose reactivity: (1) mechanically,
breaking or removing the primary cell wall and shortening cellulose chains (Tian et al.
2014); (2) chemically, eliminating undesired components or hydrolysing cellulose chain

(Arnoul-Jarriault et al. 2015; Wang et al. 2018); (3) enzymatic processes, removing 84 85 hemicelluloses (pentosan content) and adjusting viscosity (Ibarra et al. 2010; Gehmayr et al. 2011; Sango et al. 2018); (4) IL extraction, removing pentosan with nearly no effect 86 on cellulose (Li et al. 2012); (5) or using combinations of them (Yang et al. 2018). The 87 methods mentioned before, either use energy or reagents that increase the environmental 88 impacts of the pulping and the viscose process. For this reason, authors selected DES as 89 the best technique able to reduce the environmental impacts of the pulping and viscose 90 91 sectors. Due to the similarity between IL and DES, this work has the hypothesis that DES can be used as pre-treatment for dissolving pulp to increase its reactivity. DES green 92 93 solvents have been successfully used to increase the hydrolysis of cellulose (Xia et al. 2014) or to improve the production of hydroxymethylfurfural (HMF) and furfural (da 94 Silva Lacerda et al. 2015). DES have also been used in pulp to observe the effect that this 95 treatment would have on it (Jablonsky et al. 2018). However, DES have never been used 96 as pre-treatment to increase pulp reactivity, reducing the CS₂ used in the viscose process. 97 Therefore, this work aims to assess the enhancement of reactivity of dissolving pulp 98 towards viscose and quantify the theoretical reduction of CS₂ usage, employing ChCl-99 based DES mixtures. The properties α -cellulose content, pentosan content, lignin content 100 101 and intrinsic viscosity are also analysed to check that the resulting pulp meets the 102 requirements to be transformed into viscose. The reduction of the quantity of CS₂ used in 103 the viscose process, as a result of the reactivity increase, is also determined together with 104 the correlation between reactivity and cellulose crystallinity.

105 MATERIALS AND METHODS

106 **DES preparation and pulp treatment**

Dissolving pulp used in this work was provided by a pulp mill, Sniace S.A. located in
Northern Spain (Cantabria). This company produces dissolving pulp through the acid
sulphite cooking coupled with total chlorine-free (TCF) bleaching.

110 DES treatment of pulp was performed based on the methodology of Majová et al. (2017).

111 Initially, the pulp was soaked and stirred in water to obtain a consistency of 4 %. The

- mole ratio for each DES system was 1:9 ChCl:LA, 1:1 ChCl:MA, 1:3 ChCl:OxA and 1:2
- 113 ChCl:Ur as recommended in the bibliography (Jablonský et al. 2015; Pan et al. 2017).

These DES are widely used with lignocellulosic materials because of their ability to delignify (Zdanowicz et al. 2018). Reactants were weighed and mixed. The mixture was heated at 80 °C and magnetically stirred, until a clear liquid was formed. Finally, pulp and DES are put together in a flask and placed in a water bath at 60°C for one hour. When the treatment finishes, the pulp is washed with tap water, until the pH of washing wastewater is around 7.

120 Reactivity and intrinsic viscosity analyses were performed in triplicates; error bars were 121 calculated as standard deviation. Pentosan, α -cellulose and kappa number error bars were 122 calculated in duplicates, because of the scarce in pulp quantity and results were confirmed 123 with quality pulp parameters from the industry. These analyses are based on the 124 methodology used by a previous work of the authors (Llano et al. 2018). Table 1 shows 125 the characteristics of the untreated dissolving pulp.

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Table 1 Untreated pulp quality values

Sample	Pentosan (%)	Fock's reactivity (%)	α-cellulose (%)	Viscosity (mL/g)	Kappa
Raw pulp	2.89 ± 0.169	80.58 ± 2.437	91.05 ± 0.045	$465.90{\pm}14.46$	1.04 ± 0.179

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129 Fock reactivity

Reactivity of pulp samples was measured by the method described by Tian et al. (2013) 130 which is based on Fock (1959). First, 0.5 g of pulp calculated as oven-dried (o.d.) was 131 132 weighed and put into a 250 mL Erlenmeyer flask. Then, 50 mL of 9 % (w/w) NaOH was added and stirred for 10 min at 19 °C. 1.3 mL of CS₂ was added, sealed with plastic 133 134 parafilm and stirred at 250 rpm for 3 h at 19 °C; this is the xanthation phase in which cellulose-xanthate is formed. When reaction time finishes, water was added until a total 135 136 mass of 100 g, the solution was then agitated and centrifuged at 5000 rpm for 15 min. 137 Afterwards, 10 mL of the supernatant was poured in a 100 mL flask, and 3 mL of 138 sulphuric acid 20% (w/w) was added to regenerate the dissolved cellulose. The flasks were left in a fume hood for 15 h-20 h for the CS₂ excess to be removed. 139

140 Dissolved cellulose was measured by oxidation with $K_2Cr_2O_7$. Firstly, 20 mL of 68 %

141 (w/w) sulphuric acid was added and stirred at 250 rpm for 1 h. When the stirring time was

set, 10 mL of 1/6 M K₂Cr₂O₇ was added, and the mixture was reflux-boiled for 1 h.

Finally, the flasks were left to cool at room temperature and then diluted to a total volume
of 100 mL. 40 mL of the solution was pipetted into a 250 mL Erlenmeyer flask and 5 mL
of 10 % (w/w) KI was added and titrated with 0.1 N Na₂S₂O₃ using starch as an indicator.
The volume of Na₂S₂O₃ was used for the calculation of the dissolved cellulose (DC) using
equation 1:

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$$DC(\%) = \frac{\left[v_1 \cdot c_1 - \left(v_2 \cdot c_2 \cdot \frac{100}{40}\right) \cdot \frac{1}{6}\right] \cdot M \cdot \frac{1}{4} \cdot \frac{100}{10.4}}{m} \cdot 100 (1)$$

149 Where M is the molecular weight of a glucose unit, m is the o.d. weight of the pulp sample 150 (g), v_1 and c_1 are the volume and the concentration of K₂Cr₂O₇, respectively. v_2 and c_2 are 151 the volume and the concentration of Na₂S₂O₃, respectively.

152 **Pentosans**

The moisture content of the pulp was measured, and 1.6 g of pulp was weighed, and 100 mL of NaOH 5% (w/w) was added. Then, it was stirred for 3 min and left in a water bath for 1 hour, the suspension was filtered, and 15 mL of the filtrate was added to a 250 mL Erlenmeyer flask and mixed with 10 mL of $K_2Cr_2O_7$ 1/6 M and 35 mL of commercial H₂SO₄. It was left to cool for 15 min, and 50 mL of distilled was were added. The solution was titrated with 0.1 N (NH₄)₂Fe(SO₄)₂·6H₂O using ferroin as an indicator.

159 Intrinsic viscosity

160 Intrinsic viscosity was determined by the standard ISO 5351(2010). 0.25 g. oven-dried

161 pulp was dissolved in cupriethylendiamine solution for half an hour. After this, the sample

162 was left in a water bath at 25 °C for 15 minutes and passed through Cannon-Fenske 150

163 viscometer at 25 °C.

164 **α-cellulose**

165 α -cellulose was determined according to TAPPI T203 cm-99 (1999). Oven-dried pulp 166 samples were weighed to an equal of 1.6±0.1 g. Pulp was consecutively extracted with 167 17.5 % NaOH solutions at 25±0.2 °C for a total extraction time of 60±5 min. Then, pulp 168 samples were stirred and filtered. 25 mL of the filtrate were taken and mixed with 10 mL 169 of 0.5 N K₂Cr₂O₇ and 50 mL of 96 % H₂SO₄. After 15 minutes, samples were cooled by adding 50 mL of water and titrated with 0.1 N $(NH_4)_2Fe(SO_4)_2 \cdot 6H_2O$ using ferroin indicator.

172 **Kappa**

Kappa is an index that estimates the amount of residual lignin and hexenuronic acid by measuring the oxidant demand of the pulp. TAPPI UM 246 (1991) method was implemented to obtain the micro kappa number of high-purity pulp from the final stages of the bleaching process. Micro kappa is used in this work because lignin content at this stage of the production of dissolving pulp is too low, and using traditional kappa method may lead to unprecise values.

179 **CS₂ consumption calculation**

180 CS₂ consumption was calculated using Fock reactivity, α -cellulose content and the 181 stoichiometric value required for the xanthation phase which is 23.5 % (expressed in g 182 CS₂ per 100 g of cellulose) (Arce et al., 2020; Gondhalekar et al., 2019a). Considering 183 Fock's reactivity as a reaction yield of xanthation, and the α -cellulose content of the pulp, 184 the theoretical quantity of fibres (TF) is obtained using equation 2. CS₂ consumption is 185 calculated using the stoichiometric value of CS₂ and α -cellulose content (equation 3).

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$$TF(\%) = \frac{\alpha - cellulose(\%) \cdot Reactivity(\%)}{100} (2)$$

$$CS_2 usage(\%) = \frac{\alpha - cellulose(\%) \cdot 23.5}{100} (3)$$

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190 The CS_2 usage needs to be calculated not only to consider the reactivity of the sample but 191 also to assess the ratio of consumption per fibre (RCF), as shown in equation 4. The final 192 reduction of CS_2 usage was calculated using as reference the RCF from the inlet pulp.

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194
$$\operatorname{RCF} = \frac{\operatorname{CS}_2\operatorname{usage}(\%)}{\operatorname{TF}(\%)}$$
(4)

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196 X-ray diffraction and crystallinity index

197 Characterisation of the untreated pulp and DES-treated pulps at 1/20 S/L ratio was carried 198 out by powder-Ray diffraction (XRD); XRD studies were performed in air atmosphere 199 on a Bruker D8 Advance diffractometer, using Cu K α radiation and a LynxEye detector. 200 Diffraction patterns were collected with an angular 2 θ range between 10° and 70° with a 201 0.03° step size and measurement time of 3 s per step, and a graphite monochromator.

The XRD spectra were used to calculate de crystallinity index (CrI) using equation 5proposed by Segal (Segal et al. 1959).

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205
$$\operatorname{CrI}(\%) = \frac{(I_{002} - I_{am})}{I_{002}} \cdot 100 \ (5)$$

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207 Where I_{002} is the intensity of the crystalline plane (200) at around 22° and I_{am} is the 208 intensity of the amorphous cellulose at 18°.

209 **Results**

210 Effect of DES pre-treatment on pulp quality parameters

In this work, the pre-treatment of dissolving pulp with DES to increase reactivity has been assessed. Four DES were tested: ChCl:MA, ChCl:LA, ChCl:OxA and ChCl:Ur at two different S/L ratio, 1/5 and 1/20. Intrinsic viscosity, lignin content (micro-kappa), pentosan content and reactivity of the pulp were analysed to evaluate the effects of the pre-treatment α -cellulose content. The parameters α -cellulose and intrinsic viscosity are shown in figure 1, with both solid to liquid ratios.

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219 Figure 1 Evolution of a) α-cellulose content and b) intrinsic viscosity after DES treatment

At 1/20 solid to liquid ratio, cellulose content increases slightly when the system is formed by ChCl:LA (1.65 %), ChCl:MA (0.29 %) and ChCl:Ur (0.94 %), showing that the solubility of cellulose in the DES used in this work is almost negligible as stated by Kumar et al. (2016). It should be noted that the increase in cellulose does not mean that it is a product of a chemical reaction; it means that other compounds are eliminated; thus, cellulose content is concentrated.

Viscosity also increases when using the same DES systems, as long fibres of cellulose 226 227 are released. Higher viscosity values are obtained when the ChCl:LA and ChCL:Ur systems are used, reaching values of 509.25 and 507 mL/g respectively. The system 228 229 ChCL:MA nearly did not affect viscosity (479.61 mL/g concerning 465.9 mL/g in the raw pulp). However, using the ChCl:OxA DES mixture both α -cellulose content (86.86 230 231 %) and viscosity (338.70 mL/g) decrease. These results are in accordance with Škulcová 232 et al. (2016) and Zhang et al. (2020). The later studied the dissolution of cellulose when 233 using many DES systems. It was found that ChCl:OxA lead to the highest dissolution of 234 cellulose, up to 2.5 % of cellulose was dissolved in OxA. In this study the dissolution of cellulose was 4.57 %; however, the system in this study was formed by 1/3 ChCl:OxA 235 and Zhang et al. (2020) used 1/2 ChCl:OxA, therefore it is possible that increasing OxA 236 in the mixture, might lead to higher cellulose dissolution. 237

Regarding the S/L ratio, also affects the dissolution of OxA significantly, since increasing the quantity of DES results in the higher dissolution of cellulose. The decrease in cellulose, significantly affects viscose, since α -cellulose includes high molecular weight chains. This effect is probably due to the H-bonds formed when using this system. At 1/5 solid to liquid ratio, cellulose content remains almost constant for all the systems used with values ranging between 91.09 % for ChCl:LA and 89.46 % for ChCl:Ur. Therefore, using a lower S/L ratio softens the effect that DES has on the pulp, in terms of α -cellulose content.

Regarding viscosity changes, the trend is very similar to that shown for a 1/20 ratio. The highest viscosity increase was obtained with ChCl:Ur and the system ChCl:OxA gave the lowest viscosity as well; therefore this system harms pulp viscosity, making it unsuitable for pulp pre-treatment for viscose purposes. Figure 2 shows the influence of DES pretreatment on lignin content (kappa) and pentosan content.





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255 As can be seen from figure 2.b lignin content decreases for all the DES systems and ratios tested. When a 1/20 ratio is used, the higher lignin reduction is achieved with ChCl:LA, 256 257 reducing kappa number until 0.07 (91.83 % reduction). On the other hand, the lowest lignin reduction is obtained using ChCl:OxA with a final kappa value of 0.87 (3.71 % 258 259 reduction). Recent studies obtained the highest delignification with ChCl:OxA showing 260 a kappa reduction of 38.7 % (Majová et al. 2017). However, initial lignin content had a 261 strong influence on delignification, the lower the initial lignin, the lower the delignification. In fact, Majová et al. (2017) had a 0.8 % kappa reduction when initial 262 263 kappa was 11.8. This trend is also shown in this work, with an initial kappa value of 1.16, 264 the lignin reduction was 32.5 %. Nevertheless, initial kappa of 0.91 results in a 3.71 % 265 lignin reduction. This trend is the same when using ChCl:MA, achieving up to 90.9 %

266 lignin elimination when initial lignin content was higher. Taking into account the fact that 267 the raw material of this work is dissolving pulp, ChCl:OxA is not recommended because it gives low delignifying properties, a reduction of α -cellulose and a decrease of viscosity 268 269 in relation to the raw pulp. Zhang et al. (2016) used ChCl:LA, ChCl:OxA and ChCl:MA 270 to increase the saccharification rate of corncob, achieving 86.1 %, 98.5 % and 22.4 % of 271 lignin reduction, respectively. Procentese et al. (2015) employed ChCl:Ur in agricultural 272 biomass giving total lignin reduction of 7.1 %. In this work, the reduction of lignin when 273 using ChCl:Ur was in the range of 31.75 % and 43.17 % when the S/L ratio was 1/5 and 274 1/20, respectively.

Most of the studies focus on delignification of untreated biomass residues with higher lignin content than high-cellulose dissolving pulps such as rice residues (Kandanelli et al. 2018), corn stover (Xu et al. 2016) or potato peels (Procentese et al. 2018). Based on results obtained in this study, and comparing with the literature working with oxalicbased DES mixtures, it can be concluded that ChCl:OxA is more effective when used with high-lignin content samples than with dissolving pulps.

Pentosan content in the pulp, showed in figure 2.a, increases when a higher ratio is used. 281 282 The highest increase is produced when using ChCl:Ur at a 1/20 S/L ratio, up to 3.9 %. In 283 the bibliography studied, Zhao et al. (2018) achieved a 6 % xylan removal at a 1/5 S/L 284 ratio whereas Tan et al. (2019) obtained 20% xylan removal when using ChCl:Ur at 1/10 285 S/L ratio in the same study the authors reached a 100 % xylan removal with ChCl:LA at 286 1/10. As happened with lignin content, pentosan content seems to be affected by the initial content. The studies mentioned before use wheat straw (21.8 % xylan content) and oil 287 palm empty fruit bunch respectively, which have a higher amount of pentosan content 288 289 than dissolving pulp. Therefore, pentosan elimination reduces as the initial pentosan 290 content decreases. The evolution of pentosan content is not linear, since increasing the 291 quantity of DES in the system, does not always translate on higher pentosan elimination. 292 Morais et al. (2018) studied the effect solubilisation of xylans, similar to pentosan, using 293 DES, specifically ChCl:Ur, at different ratios and concentrations, and found out that 294 increasing DES quantity in the system does not lead to the same increase on xylan 295 dissolution, the maximum extraction was obtained at 50 % DES/water concentration whereas increasing DES content to a 75 %, xylan extraction did not improve. From table 296 297 2, reducing DES quantity leads to a reduction in pentosan. Morais et al. (2018), employed temperatures from 70 to 90 °C, thus reducing the viscosity of DES. In this work, the
temperature was kept at 60 °C; therefore, viscosity is higher. This fact might explain why
1/5 S/L ratio can extract more pentosan than 1/20 S/L ratio.

301 It should be noted that the raw material used in this work, has already been through several 302 processes (cooking and bleaching) which makes pulp more accessible to reactants than 303 the untreated material, by increasing the porosity and thus, the specific surface area (Li et 304 al. 2018).

305 The selectivity of the DES treatment towards delignification can be seen comparing Figures 1.a and 2.b. While α -cellulose content remained constant or even increased, lignin 306 content decreased for all the DES employed. Alvarez-Vasco et al. (2016) explained this 307 308 effect by the ability of DES to cleave ether bonds present in lignin. They also observed 309 no carbohydrates dissolved in the DES. Tang et al. (2017) showed that DES systems 310 exhibit strong interactions with lignin; in fact, some of the DES precipitated with the 311 lignin extracted. Therefore, the results showed in this work, regarding lignin and cellulose 312 content, agree with the bibliography studied.

Table 2 shows the yields obtained when compared with the raw pulp; negatives values imply the property decreased.

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	α-cel	lulose	Intrinsic	· Viscosity	Pent	tosan	Ka	ppa
S/L ratio	1/20	1/5	1/20	1/5	1/20	1/5	1/20	1/5
ChCl:LA	1.65	0.01	6.95	7.17	5.55	-6.08	-91.83	-75.47
ChCl:Ur	0.29	-1.78	6.47	11.63	38.99	-6.28	-43.17	-31.75
ChCl:MA	0.94	-0.08	0.72	7.81	7.42	-13.56	-31.78	-90.87
ChCl:OxA	-4.57	-1.25	-28.87	-3.14	21.66	-9.38	-3.71	-32.45

Table 2 Yields, in %, obtained referred to the raw pulp

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From table 2, some conclusions can be drawn. Regarding α -cellulose content, some DES lead to a low quantity (DES:Ur and DES:OxA), undesirable for viscose purposes. The reference values for pulp quality were obtained from the standard FZ/T 51001-2009. Regarding pentosan content, even though it increases for some systems, pentosan content never reaches 4 %, which is the maximum value that the standard considers. Kappa is always below 1 %, and viscosity barely changes, except for DES:OxA, which leads to a 28.87 % viscosity reduction and a 4.57 % α-cellulose reduction. These results make
DES:OxA unsuitable to be used as pre-treatment for viscose purposes.

Figure 3 represents the changes in reactivity with each DES and at each S/L ratio. Effects of DES mixtures over this parameter have never been studied before and is crucial for improving the viscose process and decrease the use of non-environmentally friendly reagents, i.e. CS₂ and NaOH. Error bars have been added in the figure. These errors are based on standard deviation and are lower than 10 for every analysis.



Reactivity (%)

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332 Figure 3 Evolution of reactivity after DES treatment

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Reactivity increases for all the DES employed. The best results were obtained using an 334 335 S/L ratio of 1/20, except for ChCl:MA. The highest increase of reactivity was produced using ChCl:OxA at a 1/20 ratio, however, as stated before, this DES will not be 336 337 considered as the best, because pulp after the treatment does not have enough quality to be considered suitable for viscose purposes. Tian et al. (2020), stated that the hydrogen 338 339 bonding abilities of DES could swell cellulose and as a result, increase reactivity, which agrees with this work. No literature has been found about the use of DES to increase 340 reactivity. This paper is the first research analysing the effect of DES over cellulose 341 reactivity. Previous works have used different lignocellulosic materials to increase their 342 accessibility to chemicals, i.e. several authors used DES for glucose release from cellulose 343 (Nor et al. 2016; Xu et al. 2016; Xing et al. 2018). This behaviour can be related to 344 345 reactivity.

346 Nevertheless, such behaviour had not been determined. Regarding reactivity towards 347 viscose, several authors have used different methods to upgrade cellulose pulp, recently. Duan et al. (2019) used mechanical and chemical treatments simultaneously to increase 348 349 reactivity up to 83.5 % while reducing viscosity to 411 mL/g. Zhou et al. (2019) 350 performed an ultrasonic pre-treatment to increase Fock's reactivity by breaking H-bonds 351 through cavitation. This treatment leads to a reactivity value of 73.2 % with nearly no changes on viscosity. Similar effects occurred in this study, since DES barely changed 352 353 viscosity, except for ChCl:OxA. Sango et al. (2018) used an enzymatic treatment and obtained a resulting pulp with a Fock's reactivity of 77.4 % with a small decrease in 354 355 viscosity. As an alternative, Arce et al. (2020) studied the possibility of increasing Fock's reactivity through bleaching, instead of using pre-treatments. As a result, bleaching 356 operating conditions were adjusted, and Fock's reactivity was improved to 95.3 % with a 357 viscosity of 448 mL/g. In this study, DES pre-treatment was proved to be an exciting 358 alternative, since Fock's reactivity was increased up to 93.7 % when using ChCl:LA with 359 360 minor changes on viscosity.

361 XRD spectra and effect on crystallinity index

362 Since the best results were obtained when using a 1/20 S/L ratio, XRD of the resulting

363 and untreated pulps were performed to explain this modification in cellulose reactivity.

Figure 4 shows the XRD for treated and untreated pulp using 1/20 pulp to DES ratio.





366 Figure 4 XRD spectra of pulp before and after DES treatment

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XRD spectra show the typical shape associated to cellulose I, with a broad peak at 2θ 368 369 between 12° and 18° and a maximum at around 22° (Li et al. 2012), which correspond to the planes $\overline{1}10$, 110 and 200 (Sirviö et al. 2015). After DES treatment, the structure of 370 cellulose remains intact, and the intensity of both peaks is reduced after the treatment. No 371 cellulose II is formed because there are no peaks at 20° and 22°, which are characteristic 372 of cellulose II (Hori and Wada 2006). To assess the influence of the intensity reduction, 373 a crystallinity index (CrI) for each pulp was calculated following the Segal method. This 374 375 method was chosen because it gave results easily comparable with other samples (Segal et al. 1959; Park et al. 2010). Table 3 shows the results obtained. 376

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 Table 3 Crystallinity indexes for untreated and DES-treated pulps

	Raw pulp	ChCl:MA	ChCl:LA	ChCl:OxA	ChCl:Ur
CrI (%)	79.09	71.63	70.23	65.8	70.63

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380 The CrI of the pulps were calculated using equation 5. As can be seen from table 3, CrI of pulp decreases after treatment with DES, making pulps more accessible for subsequent 381 reagent or enzymatic attacks and therefore more reactive. The highest decrease in 382 crystallinity is obtained with ChCl:Ox. Interestingly, the treatment with ChCl:Ox also 383 resulted in the lowest viscosity. This decrease was produced by the diminution of the 384 385 amorphous and crystalline regions, as proposed by Kumar et al. (2016), who found a decrease in the CrI of rice straw when treated by ChCl:LA system. Gondhalekar et al. 386 (2019a), proposed that the reduction of crystallinity is caused by the weakening of the 387 hydrogen bonding (Gondhalekar et al. 2019a). Procentese et al. (2015) found a slight 388 389 decrease, as well, in the crystallinity index of corncob when treated with ChCl:Urea system (Procentese et al. 2015). Additionally, a linear relationship between CrI and 390 reactivity was found as represented in figure 5. Looking at figure 5, for reactivity values 391 ranging between 75 and 100 %, the higher the crystallinity, the lower the reactivity. 392





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397 CS₂ consumption

Carbon disulphide is a critical compound in the manufacture of viscose fibre and environmental wise, one of the most concerning. CS_2 consumption was calculated, as stated by Arce et al. (2020). This calculation considers the α -cellulose content and Fock's reactivity, to measure the theoretical quantity of fibres, and the stoichiometric quantity of CS_2 , used in the xanthation phase to calculate the quantity used of this compound, 403 described by Gondhalekar et al. (2019b). Finally, a ratio between the CS_2 usage and the 404 theoretical fibres was obtained. The reduction was assessed using the untreated pulp (raw 405 pulp) as reference. Results are shown in table 4. DES treatment reduces the usage of CS_2 406 for every system.

- 407
- 408

Table 4 CS₂ consumption after DES treatment at a ratio of 1/20

Treatment	a-cellulose	Fock's reactivity (%)	$CS_2(\%)$	TF (%)	RCF	CS ₂ reduction (%)
Raw pulp	91.02	78.86	21.4	71.8	0.30	-
ChCl:LA	92.52	93.70	21.7	86.7	0.25	15.83
ChCl:Ur	91.28	94.81	21.5	86.5	0.25	16.82
ChCl:MA	91.88	85.18	21.6	78.3	0.28	7.416
ChCl:OxA	86.86	100.00	20.4	86.9	0.24	21.14

409

410 The DES that gave the highest reduction of CS_2 usage was ChCl:OxA, even though α -411 content was the lowest, meaning that reactivity has a more substantial influence on CS_2 412 than α -cellulose content.

Arce et al. (2020), obtained lower reductions, with a maximum reduction of 13.74 %, modifying the operating conditions of the bleaching stage of dissolving pulp. So, DES pre-treatment can be an excellent alternative to increase the reactivity of dissolving pulp and decrease the CS_2 in the process of viscose fibre manufacturing.

417 ChCl:LA at a 1/20 S/L ratio was considered as the best pre-treatment among the experiments performed. The authors would like to remark that the best DES treatment 418 depends significantly on the objective of the research, i.e. Zhang et al. (2016) found that 419 420 ChCl:OxA was the best for butanol fermentation and saccharification Kumar et al. (2016) 421 chose ChCl:Glycerol. Regarding lignin elimination and mechanical properties of pulp, 422 Škulcová et al. (2016) found ChCl:MA as the best, whereas Xu et al. (2016) selected 423 ChCl:Formic acid as the best for lignin elimination and Abdulmalek et al. (2017) 424 determined that Ethylamonium ethylene glycol as the best for both lignin and hemicellulose removal. Even though reactivity is not the highest obtained with ChCl:LA, 425 426 the results obtained using this configuration are following the pulp quality standards of FZ/T 51001-2009 for viscose purposes. It should be noted that the decrease in crystallinity 427

428 can affect not only to CS_2 consumption but also to NaOH consumption, since accessibility 429 increases when crystallinity decreases (Gondhalekar et al., 2019b).

430 **Conclusions**

The use of DES at two different solid/liquid ratios as a pre-treatment of dissolving pulp 431 to increase its reactivity together with other pulp parameters was assessed in this work. 432 As a result, it was concluded that DES used in this research, increase the reactivity of 433 pulp and reduce crystallisation index. Additionally, a relationship between reactivity and 434 this index was obtained. The highest increase of reactivity was obtained with ChCl:OxA, 435 however, other quality parameters of the pulp were not suitable for viscose purposes. 436 Lactic acid with choline chloride at a 1/20 ratio is recommended in this work. At these 437 conditions, reactivity increased up to 93.70 %, reducing the CS₂ usage by 15.83 %. 438 439 Treated pulp had the following characteristics: 92.50 % of α-cellulose, a kappa number of 0.07, an intrinsic viscosity in mL/g equal to 509.25, pentosan content of 2.93 %, with 440 441 a crystallinity index of 70.20 %.

As future work and with the knowledge acquired from this research, an optimisation of the pre-treatment will be performed to find the most suitable operating conditions to obtain the best quality for the pulp. Furthermore, the use of DES pre-treatment on different parts of the bleaching process will also be considered.

446 Acknowledgements

The authors acknowledge the pulp mill Sniace S.A. for providing the pulp needed for theexperiments and analyses, and the use of the laboratories when needed.

449 **Conflict of interest**

450 The authors declare no conflicts of interest.

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