

New results from the low-frequency counterpart of the XMM large scale structure survey*

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ABSTRACT

The XMM Large Scale Structure survey (XMM-LSS) is an X-ray survey aimed at studying the large scale structure of the Universe. The XMM-LSS field is currently being followed up using observations across a wide range of wavelengths, and in this paper we present the observational results of a low frequency radio survey of the XMM-LSS field using the Very Large Array at 74 and 325 MHz. This survey will map out the locations of the extragalactic radio sources relative to the large scale structure as traced by the X-ray emission. This is of particular interest because radio galaxies and radio loud AGN show strong and complex interactions with their small and larger scale environment, and different classes of radio galaxies are suggested to lie at different places with respect to the large scale structure.

For the phase calibration of the radio data, we used standard self-calibration at 325 MHz and field-base calibration at 74 MHz. Polyhedron-based imaging as well as mosaicing methods were used at both frequencies. At 74 MHz we have a resolution of 30", a median 5σ sensitivity of ~ 162 mJy/beam and we detect 666 sources over an area of 132 square degrees. At 325 MHz, we have a resolution of 6.7", a median 5σ sensitivity of 4 mJy/beam, and we detect 847 sources over an area of 15.3 square degrees. At 325 MHz we have detected a region of diffuse radio emission which is a cluster halo or relic candidate.

Key words. techniques: interferometric – surveys – cosmology: observations – large-scale structure of Universe – methods: data analysis – radio continuum: general

1. Introduction

Extragalactic radio sources such as radio loud quasars and radio galaxies, have been extensively studied to understand the physical processes relating active galactic nuclei (AGN), host galaxies, and environments. For powerful radio sources emission line and radio luminosities seem to be well correlated (McCarthy 1993), while at lower radio luminosities ($L_{1.4 \text{ GHz}} \leq$ 10^{25} W Hz⁻¹) radio loudness becomes decoupled from the AGN activity as probed by emission line luminosity (Zirbel & Baum 1995; Best et al. 2005). It has been suggested that environment plays a major role in making a galaxy radio loud or radio quiet. In the local universe, FRI-type (Fanaroff & Riley 1974) radio galaxies inhabit moderately rich cluster environments, while FRII-type radio sources tend to lie in either small groups or isolated fields (Yates et al. 1989; Hill & Lilly 1991; Ledlow & Owen 1996). Furthermore a number of recent X-ray observations have shown a strong, FRI/FRII morphology-dependent coupling between steep spectrum radio emission and their surrounding intergalactic medium (IGM) (Fabian et al. 2003; Blanton et al. 2004; Fabian et al. 2005; Croston et al. 2005). The question therefore arises as to what extent both AGN activity and environment properties are coupled with radio activity.

One way to statistically study the connections between various radio source populations and their environment is to compare X-rays emitted by the hot IGM plasma tracing Large Scale Structures (LSS), to low-frequency radio observations (v < 1 GHz). The XMM-Large Scale Structure Survey (XMM-LSS) is an X-ray survey designed to investigate the nature, properties and content of the LSS in the Universe up to redshift $z \sim 1$ (Pierre et al. 2004). The XMM-LSS field is being observed by the XMM-Newton satellite and will cover 10 degree². It is predicted to detect 1500 X-ray quasars, and 100–200 galaxy clusters up to z = 1, and ~50 within 1 < z < 2 (Refregier et al. 2002). At present, ~5 degree² of the XMM-LSS field has been observed.

The XMM-LSS field will be mapped in five bands using the 1 deg² CCD camera MEGACAM as part of the Canada France Hawaï Telescope Legacy Survey (CFHTLS¹). The XMM-LSS field is also observed as part of the SWIRE (Lonsdale et al. 2003) survey in 9 bands between 3.6 and 24 μ m. Spectroscopic follow-up (NTT, Magellan, VLT) of the ~ 70 galaxy cluster candidates found in the first 5 degree² of the survey is completed

¹ For more information on the CFHT Legacy Survey, see http://www.cfht.hawaii.edu/Science/CFHLS/

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^{*} Appendix A is only available in electronic form at http://www.edpsciences.org

Array configuration	А	В
	31 Jul. 03,	15, 16,
Obs. dates	5 Aug. 03,	17, 20 Jun. 02,
	3 Sept. 03	16 Jul. 02
Number of pointings	4	4
Int. time per pointing	~6 h	~8 h
Observing frequency	73.8/325 MHz	73.8/325 MHz
Frequency	73.8 MHz	325 MHz
Band width	1.56 MHz	6.25 MHz
$N_{\rm channel}$	128	2×16
Channel width	12.20 kHz	195.31 kHz
Band Pass calibrator	3C 405	3C 48
Flux calibrator	3C 405	3C 48
Resolution	30″	6.7″
Area (degree ²)	132	15.3
Sensitivity (at 5σ)	162 mJy/Beam	4.0 mJy/Beam

 Table 1. Observational parameters for the VLA radio survey of the XMM-LSS field.

(Pierre et al. 2006; Pacaud et al. 2006, in preparation). Standard spectroscopic follow-up of the SWIRE and XMM sources is underway at the 2-degree field spectrograph (2dF). Combining these data will provide an unprecedented view of the LSS of the universe (see Pierre et al. 2004, for a general lay-out of the associated surveys).

Using the Very Large Array (VLA) radio telescope, we have begun a low frequency radio survey at 325 and 74 MHz of the XMM-LSS field in order to address the following questions: (1) where are different classes of radio sources located with respect to the distribution of mass on cosmological scales as traced by the X-ray emission? (2) Can the radio loud/quiet aspect of optical and X-ray quasars be understood in terms of environmental effects? (3) How does the hot IGM influence the physical properties of the radio sources such as linear size and radio power?

In this paper we describe the observations we have conducted using the VLA in July 2003 in the A-configuration (most extended) and in June 2002 in the B-configuration. This combination provides resolutions of 6.7" and 30" at 325 and 74 MHz, respectively. Following the observational strategy described in Cohen et al. (2003), but using a mosaic of four pointings, at 325 MHz we cover a ~15 degree² area with a resolution of 6.7" and a mean flux density limit per beam (5σ) of ~4 mJy/Beam. At 74 MHz, we cover a 132 degree² area with a resolution of 30" and a flux density limit per beam of ~160 mJy/Beam. A summary of these results appear in Table 1.

Figure 1 shows the sensitivity and resolution of the XMM-LSS low-frequency counterpart, at 74 and 325 MHz, compared with others radio surveys. At 325 MHz, the lowfrequency survey of the XMM-LSS field is deeper than the WENSS survey (Rengelink et al. 1997) by a factor of ~3, and in resolution by a factor of ~10. At 74 MHz, we exceed the VLSS (Cohen et al. 2006) by a factor of ~3 in both sensitivity and resolution. The NVSS survey (Condon et al. 1998) covers the whole XMM-LSS field, and most of our 74 MHz sources will have a counterpart at 1.4 GHz, whereas our 325 MHz data is deep enough so that many sources will not have detected counterparts in the NVSS. Compared with the VLA-VIRMOS deep field at 1.4 GHz (Bondi et al. 2003), reaching a brightness temperature limit at 5σ of ~90 μ Jy/Beam, probing nearby starbursts over \sim 1 degree² area, we are probing powerful AGN over a larger area.



Fig. 1. Sensitivity and resolution of our XMM-LSS radio surveys, in comparison with that of other surveys. The dashed lines represent fiducial sources with a spectral index $\alpha = -0.8$.

This paper is organized as follows. In Sect. 2 we describe the observations, and the data reduction. In Sect. 3 we describe the sources extraction and we study the reliability/completeness aspects of the source lists. Section 4 presents the final results and we conclude in Sect. 5 by discussing the survey, and future plans.

2. Observations

The XMM-LSS field² is centered at α (J2000) = 2^h24^m00.27^s, δ (J2000) = -4°09′47.6″ (Pierre et al. 2004). This location was chosen because of its high Galactic latitude and low extinction. The declination near the equator also gives the advantage of being visible from many astronomical observatories.

2.1. Observational strategy

The first radio observations at 74 and 325 MHz of the XMM-LSS field were carried out with the VLA (Cohen et al. 2003) in an 8 h run. It covered 5.6 degree² at 325 MHz with a resolution of 6.3", and reached a flux density limit per beam of 4 mJy beam⁻¹ (5 σ), leading to the detection of 256 sources. At 74 MHz the primary beam covered a 110 degree² area with a resolution of 30", and a flux density limit per beam of 275 mJy beam⁻¹ (5 σ), leading to the detection of 211 sources.

² for more information on the present status of the XMM-LSS survey see http://vela.astro.ulg.ac.be/themes/spatial/xmm/LSS/ index_e.html.

We carried out a 24 h observation of the XMM-LSS field simultaneously at 74 and 325 MHz in the A-configuration. This observation was spread over July, August and September 2003. At 325 MHz, we have added data from a \sim 35 h observing run in the B-configuration, observed in June and July 2002. The observational parameters are listed in Table 1. The A-configuration gives us the needed high resolution to determine morphologies of the radio sources, and the B configuration is used for the determination of reliable flux densities and provides sensitivity to large angular scale emission needed, for example, to detect giant radio halos. At 74 MHz the primary beam is large enough to cover the whole XMM-LSS field in a single pointing, and at 325 MHz the pointing grid has been set so that we cover \sim 90% of the XMM-LSS field with four pointings.

2.2. Data reduction

For the data reduction, we used the Astronomical Image Processing System (AIPS).

2.2.1. The 325 MHz data

After a first round of flagging data affected by Radio Frequency Interference (RFI), we calibrated the relative response within each channel (i.e. *bandpass*), and performed gain and amplitude calibration. On the calibrated data, RFI was removed manually using the AIPS's routines TVFLG and SPFLG. In each of the four pointings ~ 15% of the data have been flagged. We combined the A and B configuration data in the u-v plane using the AIPS routine DBCON.

The phase calibrator we used (3C48) being far from the field, the initial phase calibration is very poor. Assuming a median spectral index $\alpha_{325}^{1400} = -0.8$, we generate a model of the sky at 325 MHz from the NVSS database at 1.4 GHz (Condon et al. 1998). This model consists of a list of clean components located at the position of the sources from the NVSS survey. Fourier transforming the modeled image allows for a phase-only calibration of each antenna using a solution interval of one minute, providing better results than the traditional calibrator-based phase calibration.

Because of the very large primary beam and the noncoplanar geometry of the VLA array, imaging would normally require the use of a 3D Fourier transform. However, this is currently too computationally expensive to be practical. The commonly used solution is to compute a pseudo-three-dimensional Fourier transform (Perley 1999), in which the field of view is divided into much smaller fields (facets). The 3D Fourier transform can then be approximated by using a two dimensional one. For the 325 MHz data, we used 286 facets, each 512 × 512 pixels, sampled at 1.5'' pixel⁻¹, with an overlap of two pixels between the facets. After the u-v data have been imaged into individual facet and deconvolved, the facets are combined into a single image. After a few iterations of phase-only self-calibration, we combined the four pointings (each 2.5 degree in diameter) as described by Condon et al. (1998) in a 15.3 deg² single map.

The resulting noise is quite inhomogeneous across the field, ranging between ~0.5 and ~2.5 mJy beam⁻¹. The noise is higher close to the bright sources, where sensitivity is dynamic-range limited. In each of the four pointings, the size of the synthesized beam was ~ $6.7'' \times 6.3''$ and we have set the restoring beam to be a circular Gaussian with a 6.7'' FWHM.

2.2.2. The 74 MHz data

For the 74 MHz data, we used Cygnus-A (3C 405) as bandpass and flux density calibrator. Due to its large angular size, the calibrator is resolved by our observation. To calibrate the data, we used a standard model available from previous observations.

The problems of RFI and the non-coplanar geometry are solved in a similar way as with the 325 MHz data. However, at 74 MHz the ionosphere poses an additional challenge. Electrons in the ionosphere produce distortion of the wavefront and the resulting phase shifts $\Delta \phi$ increases linearly with the wavelength (Kassim et al. 1993). Moreover at higher frequencies the primary beam is relatively smaller in size so that angle-variant phase shifts across the field-of-view can be ignored and standard self-calibration can be utilized to derive one time variable phase correction per antenna. Below 150 MHz positional-dependent phase variations become significant, and simple angle-invariant self-calibration breaks down. Therefore at 74 MHz we have used the technique of "field-based calibration" first developed for the VLSS survey in which the phase calibration is position-dependent across the field-of-view (Cotton et al. 2004). This technique was also used and discussed into much details in Cohen et al. (2003).

Combining the A and B-configuration data in the UV-plane didn't lead to much improvement, probably because of complications of the ionospheric calibration routine. We therefore only considered the higher resolution A-configuration data. For each pointing, after the uv plane has been imaged in the 184 facets, we used a circular Gaussian restoring beam of 30'' FWHM. The four pointings have then been combined into a single map. As with the 325 MHz data, the noise is inhomogeneous across the field and as low as ~20 mJy/Beam and as high as ~55 mJy/Beam near bright sources.

3. Source list

3.1. Detection

As a first step in our source finding algorithm, we have normalized the image by a noise map, produced using AIPS's task RMSD. The noise is calculated within windows, fitting a Gaussian to the histogram of the pixel values. The data above and below the 3σ domain are rejected, and after 30 iterations, a reliable estimation of the noise is obtained. The size of the window is critical since if it is too small, the noise evaluation will be overestimated by the presence of a strong signal, while if it is too big, it will not take into account the smaller scale variation in the noise pattern.

We set the window to be 80×80 pixels, corresponding to $10' \times 10'$ and $2' \times 2'$, at 74 and 325 MHz, respectively, and in order to save computing time, the rms is evaluated every 3×3 pixel, which is of the order of the correlation length. This introduces pixel-to-pixel uncorrelated noise, and in order to avoid for discontinuous variation in the noise level, we convolve this noise map with a circular Gaussian with diameters of 100'' and 20''at 74 and 325 MHz respectively which slightly smooths the noise image. Figure 2 shows the area mapped as a function of sensitivity for each frequency.

Dividing the original map by the noise map we get an image containing uniform noise, where we can apply the AIPS's source extraction algorithm "Search And Destroy" (SAD). SAD is given an input cut of 5 in the noise-normalized map ($\leq 5\sigma$ in the original map) applied on both peak and integrated flux density, above which each pixel group is considered as a



Fig. 2. Area as a function of limiting flux density per beam at 5σ . The full line corresponds to the 74 MHz survey whereas the dashed one corresponds to the 325 MHz survey.

potential source (island). SAD fits one or more Gaussian components to these islands, thereby producing an initial source list. Assuming the noise distribution to be Gaussian, the input cut of 5σ leads to a total number of false detection over the surveyed areas of $\leq 5 \times 10^{-2}$ at 325 and 74 MHz. A visual inspection of the residual map does reveal some false detections, due to the non-Gaussian, correlated nature of the noise in the proximity of bright sources. We have deleted these false detections from the list while comparing the source list positions with NVSS as described below.

3.2. Noise dependent errors

Finally, the absolute flux densities are obtained by multiplying the measured noise-normalized flux density by the local noise. Following Condon (1997) we calculate the true uncertainties, from the signal-to-noise ratio of the Gaussian fit ρ , as expressed by:

$$\rho^{2} = \frac{\theta_{\rm M}\theta_{\rm m}}{4\theta_{\rm N}^{2}} \left[1 + \left(\frac{\theta_{\rm N}}{\theta_{\rm M}}\right)^{2} \right]^{\alpha_{\rm M}} \left[1 + \left(\frac{\theta_{\rm N}}{\theta_{\rm m}}\right)^{2} \right]^{\alpha_{\rm m}} \frac{S_{\rm P}^{2}}{\sigma_{\rm map}^{2}} \tag{1}$$

where $\theta_{\rm M}$ and $\theta_{\rm m}$ are fitted *FWHM*s of the major and minor axes, $\theta_{\rm N}$ is the *FWHM* of the Gaussian correlation length of the image noise, corresponding to the *FWHM* of the synthesized beam, $S_{\rm P}$ is the peak flux density, and $\sigma_{\rm map}^2$ is the local noise variance. $\{\alpha_{\rm M}, \alpha_{\rm m}\}$ have values determined empirically using Monte-Carlo simulations (Condon 1997, see Table 2). We have then calculated the errors of the fitted parameters as follows:

$$\frac{\sigma^2(S_{\rm P})}{S_{\rm P}^2} = 8 \ln 2 \frac{\sigma^2(x_0)}{\theta_{\rm M}^2} = 8 \ln 2 \frac{\sigma^2(y_0)}{\theta_{\rm m}^2} = \frac{\sigma^2(\theta_{\rm M})}{\theta_{\rm M}^2}$$
$$= \frac{\sigma^2(\theta_{\rm m})}{\theta_{\rm m}^2} = \frac{\sigma^2(\phi)}{2} \left(\frac{\theta_{\rm M}^2 - \theta_{\rm m}^2}{\theta_{\rm M}\theta_{\rm m}}\right)^2 \approx \frac{2}{\rho^2}$$
(2)

$$\frac{\sigma^2(S_{\rm T})}{S_{\rm T}^2} \approx \frac{\sigma^2(S_{\rm P})}{S_{\rm P}^2} + \left(\frac{\theta_{\rm N}^2}{\theta_{\rm M}\theta_{\rm m}}\right) \left(\frac{\sigma^2(\theta_{\rm M})}{\theta_{\rm M}^2} + \frac{\sigma^2(\theta_{\rm m})}{\theta_{\rm m}^2}\right).$$
(3)

Here S_T is the total flux density, ϕ is the position angle of the major axis. $\sigma(x_0)$ and $\sigma(y_0)$ are related to the uncertainties in

Table 2. Values of $\{\alpha_M, \alpha_m\}$ used for the calculation of error bars on individual parameters (Condon 1997).

Parameter	$\alpha_{\rm M}$	$\alpha_{\rm m}$
$S_{\rm p}$	3/2	3/2
$\theta_{\rm M}, x_0$	5/2	1/2
$\theta_{\mathrm{m}}, y_0, \phi$	1/2	5/2

right ascension and declination (respectively $\sigma_{\alpha,\text{fit}}$ and $\sigma_{\delta,\text{fit}}$) by the relations given by Condon et al. (1998):

$$\sigma_{\alpha,\text{fit}}^2 = \sigma^2(x_0)\sin^2(\phi) + \sigma^2(y_0)\cos^2(\phi) \tag{4}$$

$$\sigma_{\delta,\text{fit}}^2 = \sigma^2(x_0)\cos^2(\phi) + \sigma^2(y_0)\sin^2(\phi).$$
(5)

3.3. Calibration errors

– *Position errors:* the imperfect phase calibration adds positional uncertainties. We can quantify these by comparing our astrometry measurements to a much more accurate source positioning catalog. Figure 3 shows all the position differences between the NVSS survey and our source samples at both 74 and 325 MHz on both right ascension and declination. At 325 MHz, the mean value of the position differences do not show any significant offset, while at 74 MHz we measure an average offset of 2.25" and -0.4" on respectively right ascension and declination. We have removed these offsets in the final source list. The scatter around the NVSS positions is given by:

$$\sigma_{\alpha}^{2} = \epsilon_{\alpha,\text{calib}}^{2} + \epsilon_{\alpha,\text{NVSS}}^{2} + \sigma_{\alpha,\text{fit}}^{2} \tag{6}$$

$$\sigma_{\delta}^2 = \epsilon_{\delta,\text{calib}}^2 + \epsilon_{\delta,\text{NVSS}}^2 + \sigma_{\delta,\text{fit}}^2 \tag{7}$$

where $\epsilon_{\alpha,\text{calib}}$ and $\epsilon_{\delta,\text{calib}}$ are the calibration errors due to the ionosphere, $\epsilon_{\alpha,\text{NVSS}}$ and $\epsilon_{\delta,\text{NVSS}}$ are the calibration errors of the NVSS sources, and $\sigma_{\alpha,\text{fit}}$ and $\sigma_{\delta,\text{fit}}$ are the Gaussian fitting errors (Eqs. (1)–(5)).

At 325 MHz, the scatter in the distribution of the positional differences between the 325 MHz single source population and their associated NVSS counterpart contains the fitting errors of both ours and NVSS databases, as well as calibration errors. Therefore, selecting only the sources with higher signal-to-noise ratio lower the noise-dependent error contributions. Selecting the 325 MHz sources with associated NVSS counterparts having error bar lower than 0.6" gives a subsample of 41 sources with associated Gaussian fitting error contributions on the level of 0.05". For this high signal-to-noise ratio subsample, we find scatters of $\sigma_{\alpha} = 1.15''$ and $\sigma_{\delta} = 1.83''$. Compared with the NVSS noise-independent uncertainties of $\epsilon_{\alpha,\text{NVSS}} = 0.45^{\prime\prime}$ and $\epsilon_{\delta,\text{NVSS}} = 0.56''$, our values are much higher. We can explain this difference by the fact that we have used an NVSS-based model to phase calibrate the data which included low signal-to-noise NVSS sources, where noise-dependent uncertainties dominate noise-independent ones. Therefore, we consider the quadratic differences between our measurement of the position uncertainties of respectively 1.15" and 1.83" and the NVSS calibration errors to be a good estimate of our calibration errors. This leads to $\epsilon_{\alpha,\text{calib}} = 1.06^{\prime\prime}$ and $\epsilon_{\delta,\text{calib}} = 1.75^{\prime\prime}$

At 74 MHz, we get scatter values of $\sigma_{\alpha} = 6.8''$ and $\sigma_{\delta} = 3.7''$ for the whole population, which contains uncertainties coming from both Gaussian fitting errors and calibration errors, as for the 325 MHz data. Although the NVSS resolution is lower than ours, we assume the position errors from NVSS to be negligible, as the signal-to-noise ratio of NVSS is on



Fig. 3. Positional differences in right ascension and declination between our source sample and NVSS at 325 (*on the left*) and 74 MHz (*on the right*). The 74 MHz source sample corresponds to a much brighter source population in NVSS than the 325 MHz source sample counterpart, so that the scatter in positional differences on the right reflects the 74 MHz dataset calibration errors. At 325 MHz, the scatter is dominated by the NVSS uncertainties.

average ~10 times greater (see Fig. 1). In order to quantify the calibration errors, we select sources with $\sigma_{\alpha,\text{fit}}$ and $\sigma_{\delta,\text{fit}}$ lower than 0.5", which makes a subsample of 43 sources detected at high signal-to-noise ratio. We find standard deviations in right ascension and declination of respectively $\sigma_{\alpha} = 3.43''$ and $\sigma_{\delta} = 2.14''$, which, subtracting the NVSS calibration error contribution, leads to $\epsilon_{\alpha,\text{calib}} = 3.37''$ and $\epsilon_{\delta,\text{calib}} = 2.00''$. We have quadratically added these errors to the Gaussian fitted ones.

- *Flux density errors:* for the flux density calibration, we have used 3C48, and 0137+331, at 74 and 325 MHz respectively. We have assumed the flux density of these sources to be reliable at the level of 5% (see Cohen et al. 2003). We therefore have an uncertainty at the level of 5% on the overall flux density scale. We have quadratically added that uncertainty value to the noise-based Gaussian fitting error, given for the peak and integrated flux densities.

- Source size errors: as discussed in detail by Cohen et al. (2003), at 74 MHz incompletely corrected ionospheric effects, which are similar to "seeing" effects in the optical domain, are hard to quantify, as we would need to know the actual source sizes. In order to evaluate the effects of the seeing we define the fitted size of resolved source of diameter θ_{source}^2 to be:

$$\theta_{\rm fit}^2 = \theta_{\rm source}^2 + \theta_{\rm beam}^2 + \theta_{\rm seeing}^2.$$
(8)

Here θ_{beam} is the beam size, and θ_{seeing} corresponds to the size of a point source, deconvolved from the beam and imaged with that level of seeing. Figure 4 shows the scatter of the extendedness of the whole source population at 74 MHz as estimated by S_t/S_p .

Although we do not have any information on the actual source sizes of the individual sources, assuming the bulk of the source population is unresolved, we can directly get an upper limit on the actual value of the seeing. The median value $med(S_t/S_p) = 1.48$ gives an upper limit on the seeing of 20.7", and in order to be conservative, we have considered its lower limit to be 0".



Fig. 4. At 74 MHz: the ratio of the integrated to the peak flux density of each source vs. the peak flux density. Even if we cannot disentangle the discrepancy between the effects of seeing and physical size, for the seeing effect estimation we take the median value as a good upper limit (dashed line), assuming that the sources with that size are actually unresolved.

3.4. Completeness

In order to quantify the source detection efficiency, we have computed a Monte-Carlo simulation, generating 1000 sources with peak flux densities between 4 and 12σ in a 2800 × 3100 pixel image, cut from the residual map. Figure 5 shows the number of undetected sources as a function of the signal-tonoise ratio. A function of the following form, gives a fit to the Monte-Carlo outputs:

$$f_{\rm m}(S_{\rm p}/\sigma_l) = 1.13 \left(\frac{S_{\rm p}}{\sigma_l} - 3.67\right)^{-2.68}$$
(9)

where S_p is the peak flux density and σ_1 is the local noise value. We can see that ~95% of the sources are detected above 7σ , and this value could be a reasonable estimation of the completeness level. Though assuming the missed fraction to be known, we can correct the source counts estimation by compensating down to the 5σ level the SAD detection inefficiency. We define



Fig. 5. The fraction of the missed sources as a function of SNR, from Monte-Carlo simulation, and fitted curve (dashed line).

an effective area element as the integration of a surface element weighted by the detection efficiency $(1 - f_m(S_p/\sigma_1))$. The total effective area at each flux density level *S* is the integration of that quantity over the domain where the local noise σ_1 is as $\sigma_1 < S/5$:

$$A_{\rm eff}(S) = \int_{\sigma_l < S/5} [1 - f_{\rm m}(S_{\rm p}/\sigma_l)] \mathrm{d}A. \tag{10}$$

The source count estimator $N(>S_0)$ is then corrected as follows:

$$N_{\rm c}(>S_0) = \int_{S_0}^{+\infty} \frac{n(S)\mathrm{d}S}{A_{\rm eff}(S)}.$$
(11)

We have computed the uncertainties from the source counts, assuming Poisson statistics:

$$\sigma^2(N > S_0) = \sum_i \frac{1}{A_i^2} N_i.$$

Here N_i is the number of sources per bin, and A_i is the area used in the source count calculation.

3.5. Extended flux density estimation

The source extraction method using Gaussian fitting algorithm can lead to an underestimation of the integrated flux densities, when significant part of the emission are extended. In order to quantify this effect, we derive another estimation of the integrated flux density inside a 60" diameter aperture, centered at the position of each Gaussian component. Then we have $S_{\text{int}} = \Sigma \times 4 \ln 2 / (\pi . FWHM)$, where S_{int} is the integrated flux density, Σ is the sum of the pixels inside the aperture, and FWHM is the Full Width at Half Maximum in pixels. Figure 6 shows the cumulative probability distribution of the noise-normalized difference between the two flux density estimates for subsamples of unresolved point-like sources, and resolved, or multiple sources. Using a Kolmogorov-Smirnoff test, we compare both distributions with a purely Gaussian distribution. We derive probability values for the distributions to be Gaussian of $P_{\rm KS} \sim 0.7$ for point like sources and $P_{\rm KS} \ll 10^{-4}$ for extended sources, indicating that the flux density estimates by the two methods are in agreement for point-like sources and obviously disagree for resolved sources. The median value of the ratio between the flux densities derived from the two methods for extended sources gives the average bias to be \sim 7%. Therefore, at 325 MHz, since the



Fig. 6. The cumulative probability distribution of the noise-normalized difference between the two flux density estimates derived by the Gaussian fitting method (*"int_Gauss"* label) and the pixel-based method (*"int_pix"* label). The solid line represents a subsample of single, unresolved sources, whereas the dash-dotted line represents the extended sources. The purely Gaussian distribution is over-plotted the dotted line.

error bars generated by the pixel based method are much higher, when the significance of the difference between the two estimates is above 2σ , we derive the integrated flux density following the pixel-based method, rather than summing over the Gaussian component individual flux densities. At 74 MHz, the resolution being much larger, most sources are unresolved and the Gaussian fitting based integrated flux density estimation is reliable.

4. Results

4.1. 325 MHz results

At 325 MHz using the extraction method described above, we extract 877 sources from the 15.3 degree² combined map. This sample contains a significant number of obviously false detections and by visual inspection, we rejected 30 that were close to the brightest sources where the noise is non-Gaussian.

We have defined as multiple sources those separated by less that 60", and assuming Poissonian statistics this makes the probability of two independent sources to be classified as multiple lower than 1%. We finally arrive at a list of 847 sources in which 621 are single ("S"), and 226 are multiple³ ("M"). We have defined as unresolved sources the ones distinguishable from the beam size at the 2σ level, and on the 621 single component sources, 484 where unresolved. The final source list appears in Table A.1. Images of the multiple component sources larger than twice the beam size are shown in Fig. A.1.

Since the Cohen et al. (2003) radio sources are all detected in our deeper and wider survey, at the same frequency, we can directly compare their flux densities. We found that Cohen et al. (2003) flux densities are on average higher than our flux densities by $\sim 20\%$. In order to address this issue, we built radio spectra of ~ 200 radio sources using the 74 MHz flux densities (that are in agreement with Cohen et al. (2003), see Sect. 4.3), and 1.4 GHz flux densities retrieved from the NVSS database. Also, we considered two more measurements obtained in August 2004 by the Giant Meterwave Radio Telescope

³ The largest multiple sources J0217.0-0449*, J0227.2-0325*, J0216.3-0245*, do not satisfy the <60'' criteria, but regarding at the morphology it is obvious that are actually multiple, see Fig. A.1.



Fig. 7. The left panel shows the Euclidean normalized differential source count at 325 MHz. The values with doted error bar are uncorrected, whereas the error bar in full line show the differential source count corrected from the noise variations within the map and from the source finding algorithm efficiency falling steeply bellow 10σ . The differential source count from deep 325 MHz survey (Wieringa 1991) is over plotted in dashed line. The right panel shows the Euclidean normalized differential source count at 74 MHz. The dashed lines shows the Wieringa (1991) differential source count extrapolated from 325 to 74 MHz using different spectral index in the 0 to -1 range. Dots are showing the differential source count extrapolation derived from Monte-Carlo simulation, taking in account spectral index dispersion $\sigma(\alpha_{325}^{74}) = 0.24$ of a typical radio source population (De Breuck et al. 2000).

(GMRT) at 230 and 610 MHz, covering the same field at comparable depth (Tasse et al. in prep.). Selecting a sample of single, unresolved sources at 325 MHz, most often, when the general trend of the radio spectra doesn't indicate any spectral aging or self absorption break, the flux density estimate by Cohen et al. (2003) is a poorer match to the physical synchrotron power low spectra, whereas the new flux density estimates and their associated error bars are well compatible with a power law spectra. We therefore conclude the flux densities published in Cohen et al. (2003) to be overestimated by ~20%, and the flux densities presented here to be more reliable. Although not understood, the overestimation on the fluxes of Cohen et al. (2003) might be due to instrumental or algorithm errors.

Figure 7 shows the Euclidean normalized differential source count. We have calculated the source density in each flux density bin as described in the previous section, compensating for noise inhomogeneities across the image. As the error bars have been computed considering the decreasing effective area, we claim that the derived source counts are correct down to the 5σ level, where σ is the minimum noise value in the noise map, so that $5\sigma \sim 2.5$ mJy/beam. Comparing the Euclidean normalized differential source count estimation from a deep Westerbork survey (Wieringa 1991), we find good agreement at low flux densities, where we have applied the efficiency corrections, but at flux densities higher than 30 mJy, they appear to differ by a factor of $\sim 2-3$, which we attribute to either cosmic variance or resolution difference.

We have compared our source list to the NVSS database, looking for 1.4 GHz counterparts within 45" of each source. The total integrated flux density used to derive the spectral index is calculated as described in Sect. 3.5. The resolution difference between our data (6.7") and NVSS (45"), makes the estimation of accurate spectral index less robust, as we can miss some of the extended emission seen in NVSS. This probably leads to a small over estimate of the spectral index for the extended sources, and we would need to match resolution to correct for this effect.

Out of the 847 detected sources at 325 MHz, we have found 566 sources to have NVSS counterparts, and for the 281 remaining sources we give an upper limit on their spectral index based on the NVSS detection limit. Figure 8 shows the spectral index distribution, and the corresponding flux density and

completeness limit of NVSS. We have derived the median spectral index $\alpha_{325}^{1400} \sim -0.66$, for the whole radio source sample, excluding the unidentified sources in NVSS, and $\alpha_{325}^{1400}(S_{325} > 0.05 \text{ Jy}) \sim -0.72$, on the brightest sources subsample. Figure 9 shows we find close agreement between the spectral index distributions of a S > 0.05 Jy subsample, and the De Breuck et al. (2000) Gaussian fit to the spectral index distributions derived from the WENSS/NVSS surveys flux densities ($S_{325} > 0.05$ Jy subsample).

4.2. A Radio halo candidate at 325 MHz

Giant radio halo and relic radio sources are generally diffuse low surface brightness sources with steep spectra and typical physical sizes of $\sim 0.1-1$ Mpc. They are found in rich environment, showing signs of cluster merger activity (for extended reviews on the subject see Feretti 1999; Sarazin 2005).

An extended, low surface brightness object of ~1.9' along the right ascension axis, and $\sim 0.9'$ along the declination axis is detected at 325 MHz at α (J2000) = 2^h19^m42^s, δ (J2000) = $-4^{\circ}00'30''$. Since that source is extended on the scale of the box being used for the local noise calculation, the peak flux density was below the 5σ level after the local noise normalization. We have therefore extracted the Gaussian components of that source on the original map, which appear together with the other sources in Table A.1. Using AIPS's task TVSTAT, we find its integrated flux density to be 150.7 ± 12.5 mJy. We detect the diffuse emission counterparts at 74 MHz and 1.4 GHz (NVSS, Condon et al. 1998) at flux density levels of 1.34 ± 0.2 Jy, and 27.7 ± 1.8 mJy respectively. This makes the spectral indexes to be $\alpha_{74}^{325} \sim -1.48 \pm 0.15$ and $\alpha_{325}^{1400} \sim -1.16 \pm 0.1$. We have looked for counterparts using the NED databases (NED Team 1992), and Fig. 10 shows the overlay between an image retrieved in the Digital Sky Survey (DSS) and the radio halo contours. We have found four objects classified as galaxies in Maddox et al. (1990).

Based on the morphology and the fairly steep spectral index, we suggest that this object is a good candidate for either a radio halo, a radio relic or both. The difference between the spectral indexes α_{74}^{325} and α_{325}^{1400} suggests the presence of more than one electron population. The contour lines on the east side of the object shows a steep fall-off of the surface brightness, which



Fig. 8. Spectral index distribution at 325 MHz (*left panel*) and 74 MHz (*right panel*), derived from comparison with flux density of each radio source counterpart at 1.4 GHz in the NVSS. The flat dashed lines on both plots represents the median value being respectively $\alpha_{325}^{1400} = -0.72$ and $\alpha_{74}^{1400} = -0.72$. In the 325 MHz spectral index distribution plot, the dashed lines on the left correspond to the spectral index reachable as a function of the 325 MHz flux density, with respect to the completeness, and flux density limit levels of NVSS.



Fig.9. Spectral index distribution (S > 0.05 Jy) comparison with De Breuck et al. (2000) Gaussian fits, based on the WENSS/NVSS surveys. Dashed line and dashed-dotted line show the spectral index distribution of the steep-spectrum and the flat-spectrum radio source population respectively (De Breuck et al. 2000).

indicates the presence of a shock. A polarization observation of the halo could confirm the relic origin of its diffuse emission. Visually, it looks like a galaxy overdensity and this diffuse emission likely belongs to a galaxy group or cluster as discovered in recent, similarly observed objects at low frequencies (Kassim et al. 2001). The detection of diffuse X-ray emission would confirm the cluster identification, but unfortunately, the ~5 degree² X-ray field does not overlap the source.

4.3. 74 MHz results

At 74 MHz, on the criteria outlined above, we detect 686 sources. Matching the source list with NVSS 1.4 GHz objects, we find 20 sources to be false detections due to the correlated sidelobe noise close to bright sources. As for the 325 MHz data, any sources closer than 60" have been classified as multiple. Of the 666 remaining sources, 615 have been classified as single (S) and 51 as multiple (M) (see Fig. A.2). Of the 615 simple sources, 465 were unresolved. Yet, as discussed in Sect. 3, the size measurement at 74 MHz have very high uncertainties, as the seeing effect is poorly defined.



Fig. 10. Radio contours of the giant radio halo candidate detected at 325 MHz overlaid with an image retrieved from Digitized Sky Survey. The contours corresponds to levels of $1.5 \text{ mJy/Beam} \times \{1, 1.4, 2, 2.8...\}$.

As for the 325 MHz dataset, we have checked for the consistency between our and Cohen et al. (2003) observed flux densities at 74 MHz. Results do not show any significant overall offsets in between the two measurement, as opposed to the 325 MHz observations. In addition, we compare our flux density estimates to the VLSS radio survey at 74 MHz (Cohen et al. 2006). Again, flux differences are compatible with the error bar estimates.

At 74 MHz, assuming $\alpha = -0.8$ the corresponding flux density limit at 1.4 GHz is about an order of magnitude higher than the NVSS flux density limit. Consequently, all the 74 MHz sources have a counterpart in the NVSS database within a 60" radius. Moreover our 30" resolution 74 MHz map roughly matching the NVSS resolution of 45", we expect the spectral index estimation to be highly reliable. The spectral index distribution is shown in Fig. 8, and we find a spectral index median value of $\alpha_{74}^{1400} = -0.72$.

Figure 7 shows the Euclidean normalized differential source count with and without applied corrections. In order to compare that result, we can analytically extrapolate the relation given

Table 3. Objects identified in NED database with known redshifts.

Name	RA radio source	Dec radio rource	Type	RA	Dec	Dist from	Redshift	Reference
	(J2000)	(J2000)		NED object	NED object	object (")		
J0201.7-0211	02 01 43.10	-02 11 51.93	G	02 01 43.11	-02 11 47.6	4.33	0.19590	2
J0201.7-0211	02 01 47.18	-02 11 59.60	G	02 01 47.03	-02 11 55.7	4.50	0.19600 ± 0.00100	3
J0213.7-0256	02 13 46.93	-02 56 41.32	G	02 13 47.00	-02 56 37.5	3.96	0.35680 ± 0.00020	4
J0215.6-0222*	02 15 41.85	-02 22 54.27	QSO	02 15 42.02	-02 22 56.8	3.59	1.17800	5
J0216.2+0008	02 16 16.51	+00 08 59.32	GClstr	02 16 17.30	+00 11 37.0	158.12	0.21998	1
J0216.6-0444*	02 16 40.90	-04 44 05.12	QSO	02 16 40.65	-04 44 04.7	3.77	0.87000	6
J0217.4-0015	02 17 25.01	-00 15 47.02	GClstr	02 17 32.80	-00 15 52.0	116.95	0.31075	1
J0218.5-0923	02 18 34.50	-09 23 39.64	QSO	02 18 34.38	-09 23 38.5	2.13	0.47000	6
J0218.6-0015	02 18 39.78	-00 15 07.11	GClstr	02 18 39.40	-00 12 20.0	167.20	0.31075	1
J0220.0-0143	02 20 01.98	-01 43 49.67	QSO	02 20 02.31	-01 43 52.7	5.80	0.47000	6
J0220.5+0027	02 20 32.50	+00 27 59.65	GClstr	02 20 34.30	+00 27 56.0	27.24	0.26537	1
J0220.9-0156*	02 20 54.11	-01 56 53.07	G	02 20 54.25	-01 56 51.8	2.45	0.17500	7
J0223.0-0826	02 23 01.84	-08 26 09.02	QSO	02 23 01.55	-08 26 09.9	4.43	1.52070	8
J0224.3-0752	02 24 22.41	-07 52 58.85	QSO	02 24 22.39	-07 52 58.7	0.33	2.44920	8
J0225.1-0035	02 25 07.73	-00 35 32.50	QSO	02 25 08.09	-00 35 31.4	5.51	0.68700	9
J0227.6-0052	02 27 36.20	-00 52 58.03	GClstr	02 27 35.40	-00 54 05.0	68.03	0.34479	1
			GClstr	02 27 35.50	-00 51 32.0	86.66	0.33344	1
J0228.4+0032	02 28 25.01	+00 32 12.08	GClstr	02 28 26.50	+00 32 20.0	23.71	0.50000	10
J0228.6-0042	02 28 40.90	-00 42 55.03	GClstr	02 28 42.90	-00 43 20.0	39.03	0.42421	1
J0228.1-0115	02 28 07.50	-01 15 43.10	AbLS	02 28 07.79	-01 15 40.5	5.06	1.99760	11
			QSO	02 28 07.80	-01 15 40.6	5.14	2.03700	1
J0230.4+0108	02 30 26.25	+01 08 49.10	GClstr	02 30 27.40	+01 09 04.0	22.79	0.40000	10
J0231.0-0049	02 31 00.82	-00 49 44.42	GClstr	02 31 11.20	-00 49 21.0	157.45	0.39017	1
J0233.4+0015	02 33 25.37	+00 15 48.75	GClstr	02 33 28.10	+00 17 22.0	101.84	0.35613	1
			GClstr	02 33 27.90	+00 18 37.0	172.47	0.34479	1
J0233.5-0203	02 33 30.17	-02 03 22.19	G	02 33 30.34	-02 03 22.4	2.55	0.79400	9
J0234.3-0139	02 34 21.64	-01 39 00.25	G	02 34 21.83	-01 39 00.6	2.87	0.64500 ± 0.00200	12
J0234.9-0736	02 34 58.71	-07 36 17.98	QSO	02 34 58.44	-07 36 19.8	4.44	2.17260	8
J0235.5-0705	02 35 30.73	-07 05 01.43	QSO	02 35 30.71	-07 05 04.6	3.18	2.05980	8
J0235.5-0219	02 35 32.43	-02 19 31.19	QSO	02 35 32.51	-02 19 32.0	1.44	1.32100	9
J0237.9-0145	02 37 57.00	-01 45 10.77	G	02 37 57.09	-01 45 11.4	1.48	0.84000	9
J0239.2-0118	02 39 13.42	-01 18 15.01	QSO	02 39 13.68	-01 18 16.4	4.14	1.79400	9
J0239.7-0234	02 39 45.71	-02 34 39.93	QSO	02 39 45.47	-02 34 40.9	3.72	1.11600	9
J0242.6-0000	02 42 40.40	-00 00 45.21	G	02 42 40.71	-00 00 47.8	5.32	$(1137 \pm 3) \text{ km s}^{-1}$	13
			GClstr	02 42 32.10	+00 00 14.0	137.86	0.21998	1
J0242.7-0157	02 42 47.57	-01 57 46.54	QSO	02 42 47.65	-01 57 49.6	3.28	0.61700	9

An asterisk (*) after the source-name indicates the source has been detected at both frequencies.

References: (1) Goto et al. (2002), (2) Crawford et al. (1999), (3) Crawford et al. (1995), (4) Owen et al. (1995), (5) Drinkwater et al. (1997), (6) Becker et al. (2001), (7) Hewitt & Burbidge (1991), (8) Schneider et al. (2003), (9) Dunlop et al. (1989), (10) Postman et al. (1996), (11) Junkkarinen et al. (1991), (12) Stanford et al. (2000), (13) Huchra et al. (1999).

by Wieringa (1991) from 325 MHz to 74 MHz, assuming various mean spectral indices ($\langle \alpha_{74}^{225} \rangle = \{-1.00, -0.75, -0.50, -0.25, 0.00\}$). Also, to take in account the spectral index dispersion of the radio source population at 325 MHz, we have conducted an extensive Monte-Carlo simulation, by generating a radio source population following the Wieringa (1991) source counts at 325 MHz, and then giving each source a random spectral index following a Gaussian distribution with mean values of $\langle \alpha_{74}^{325} \rangle$, and a dispersion of $\sigma(\alpha_{74}^{325}) = 0.24$ (De Breuck et al. 2000). Extrapolating the flux density of each source to 74 MHz, we can build the differential source count at 74 MHz. Figure 7 shows that the analytical and Monte-Carlo extrapolated differential source counts are in close agreement.

The Euclidean normalized differential source count of our sample roughly corresponds to the extrapolation done with $\alpha_{74}^{325} \sim -0.5$ which contrasts with the median value $\alpha_{74}^{1400} = -0.72$ found between our 74 MHz sources and their NVSS counterparts at 1.4 GHz. This suggests a flattening of the spectrum at $\nu < 325$ MHz, likely due to the sources being synchrotron self absorbed.

4.4. Source identification from literature:

We have searched for published data on all objects we have detected at both frequencies, using the NASA/IPAC Extragalactic database (NED / NED Team 1992). We set the searching radius at 6" for the individual object search, and at 3' for the galaxy cluster search. On the 1460 detected objects at 74 and 325 MHz, 34 with known redshift have been identified optically as QSO, Galaxy, or are expected to belong to a galaxy cluster, and we have only selected the ones with their redshift determined (see Table 3). All of them have been identified at 74 MHz and only four have also been identified at 325 MHz. This appears to be a selection effect as the survey at 74 MHz probes a much brighter source population and an area which is ~7 times larger than at 325 MHz. Figure 11 shows the redshift distribution of our identified source sub-sample.

5. Conclusion and future work

We have mapped the XMM-LSS field over \sim 130 and \sim 15 squares degrees at 74 and 325 MHz respectively,



Fig. 11. Redshift distribution of our whole radio source sample identified with NED, and with measured redshift for the QSOs, galaxies, and galaxy cluster.

detecting ~1500 sources in total. We detect one source of diffuse, steep-spectrum emission, which is a candidate for a radio halo or relic. The Euclidean normalized differential source counts at 74 MHz are consistent with previous studies assuming $\alpha_{325}^{74} \sim -0.5$, suggesting a flattening of the spectrum of radio source population for $\nu < 325$ MHz.

In the near future we will combine the VLA data at 74 and 325 MHz with observations from the GMRT (Giant Meterwave Radio Telescope) at 230 and 610 MHz of the XMM-LSS field, adding two additional frequencies. Cross-correlating this data with upcoming X-ray and optical observations will allow us to probe in detail the low frequency spectrum of a large radio galaxy sample, and to determine the influence of the small and large scale environment on the radio source properties, such as linear size, and radio power.

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Appendix A: Radio images and source lists



Fig. A.1. The multiple component sources in the 325 MHz source list larger than 13", sorted in decreasing angular size order. Contours corresponds to levels of $3\sigma \times (-1.4, -1, 1, 1.4, 2, 2.8, 4, 5.6, 8, 11, ...)$ and greyscale is scaled from -3σ to the maximum value in the image. On the top-left corner of each images appears the name of the corresponding source in the source list, as well as its mean coordinate. The local noise level is shown on the bottom of each image.



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Fig. A.1. continued.



Fig. A.1. continued.

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Fig. A.2. The multiple component sources in the 74 MHz source list larger than 60", sorted in decreasing angular size order. Contours corresponds to levels of $3\sigma \times (-1.4, -1, 1, 1.4, 2, 2.8, 4, 5.6, 8, 11, ...)$ and greyscale is scaled from -3σ to the maximum value in the image. On the top-left corner of each images appears the name of the corresponding source in the source list, as well as its mean coordinate. The local noise level is shown on the bottom of each image.

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Table A.1. The 325 MHz source list.

Name	RA 12000	σ_{α}	Dec 12000	σ_{δ}	Туре	S _{int}	S _{comp}	Major axis	Minor axis	Position	Spectral index α^{1400}
10214 5-0314	02 14 31 89	2 47	-03 14 27 12	1 77	М	$\frac{1115y}{778 + 77}$	$\frac{1115y}{498 + 71}$	1000000000000000000000000000000000000		$\frac{\text{Aligic}}{852 \pm 0.9}$	-1.40
30214.5 0514	02 14 31.90	1.07	-03 14 23.56	1.75	C	//.0 ± /./	27.9 ± 3.1	<2.9	<2.7	156.3 ± 41.2	1.40
J0214.6-0333	02 14 34.07	1.37	-03 33 42.48	1.90	Š	7.0 ± 1.6	7.0 ± 1.6	<9.7	<5.1	51.2 ± 10.3	-0.47
J0214.7-0314	02 14 42.70	1.07	-03 14 20.43	1.75	М	55.8 ± 4.9	37.2 ± 4.0	<3.0	<2.5	144.3 ± 8.6	-0.50
	02 14 42.48	1.16	-03 14 23.31	1.81	С		18.6 ± 2.9	6.5 ± 4.5	<4.0	45.5 ± 7.1	
J0214.9-0411	02 14 52.88	1.08	-04 11 21.00	1.76	М	22.6 ± 2.3	13.0 ± 1.8	<4.1	<3.3	125.8 ± 20.1	-0.37
	02 14 52.70	1.15	-04 11 21.04	1.85	С		9.6 ± 1.6	<7.6	<3.2	37.1 ± 4.3	
J0214.9-0324	02 14 53.43	1.08	-03 24 57.64	1.75	M	19.4 ± 2.1	11.1 ± 1.5	<3.9	<2.8	99.9 ± 10.3	-0.97
10214.0 0451	02 14 53.48	1.32	-03 25 00.67	1.76	C	(1.12	8.3 ± 1.4	<8.0	<3.2	81.6 ± 4.2	0.52
J0214.9-0451	02 14 55.07	1.12	-04 51 27.92	1.99	5 5	0.4 ± 1.3	0.4 ± 1.3	< 9.0	<4.5	103.3 ± 8.3 164.0 ± 18.5	<-0.52
J0214.9-0249 J0214.0-0425	02 14 55.40	1.07	-02 49 19.30	1.70	s r	31.3 ± 3.3 75 ± 1.4	31.3 ± 3.3 75 ± 1.4	< 3.1	< 2.8	104.0 ± 18.3 55.5 ± 14.4	-0.30
10215 0-0256	02 14 50.03	1.21	-042343.28 -02560219	1.01	S	7.3 ± 1.4 143 + 20	7.5 ± 1.4 143 + 20	<4.9	<4.8	55.5 ± 14.4 65.0 ± 42.7	-0.43
10215.0-0458*	02 14 58 92	1.06	-045812.87	1.76	M	121.6 + 8.6	62.4 ± 6.5	6.5 + 1.1	<1.8	33.1 ± 1.5	-0.49
021010 0100	02 14 59.11	1.06	-04 58 13.16	1.75	C	12110 2 010	51.4 ± 5.4	3.2 ± 1.2	<2.0	140.5 ± 3.6	0.1.2
	02 14 58.92	1.18	-04 57 41.24	1.89	С		7.8 ± 1.6	<8.1	<4.7	33.0 ± 11.2	
J0215.0-0453*	02 15 00.37	1.06	-04 53 59.65	1.75	М	392.5 ± 25.8	224.0 ± 22.7	11.6 ± 0.6	5.3 ± 0.4	133.8 ± 1.3	-0.74
	02 14 59.63	1.08	-04 53 30.22	1.78	С		83.5 ± 9.0	14.3 ± 1.8	<2.5	148.6 ± 1.4	
	02 14 59.32	1.10	-04 53 30.90	1.86	С		55.9 ± 7.2	14.4 ± 3.3	5.1 ± 2.0	163.0 ± 4.2	
	02 14 59.78	1.15	-04 54 01.06	1.86	С		19.6 ± 3.2	8.0 ± 4.3	<5.0	152.7 ± 11.3	
10215 0 0504	02 15 00.06	1.30	-04 53 41.64	1.81	C	1166 0.0	9.6 ± 1.8	<7.8	<5.9	92.2 ± 23.3	0.00
J0215.0-0506	02 15 02.03	1.13	-05 06 01.65	1.79	M	116.6 ± 9.2	74.6 ± 8.2	17.0 ± 2.6	<2.2	46.9 ± 0.9	-0.80
	02 15 01.94	1.08	-05 06 05.55	1.70	C		33.4 ± 3.9	5.4 ± 1.8	< 3.3	105.0 ± 10.7	
10215 1-0521	02 15 02.30	1.14	$-05\ 00\ 00.90$	1.70	M	47.2 ± 4.4	3.0 ± 1.4 27.3 + 3.0	<3.0	< 3.3	72.3 ± 11.1 50 9 \pm 7 3	-0.66
J0215.1-0521	02 15 04.00	2.05	$-05\ 21\ 39.18$ $-05\ 21\ 43\ 20$	1.75	C	47.2 ± 4.4	199 ± 32	146 ± 97	<2.5	30.9 ± 7.3 76.0 + 1.1	-0.00
10215 1-0304	02 15 05 12	1.20	$-03\ 04\ 21\ 83$	1.79	S	10.0 ± 1.8	10.0 ± 0.2 10.0 ± 1.8	<6.6	<5.1	74.5 ± 21.3	-1.08
J0215.1-0322	02 15 06.41	1.14	$-03\ 22\ 33.66$	2.39	ŝ	16.5 ± 3.4	16.5 ± 3.4	13.0 ± 9.2	<4.8	9.8 ± 4.7	<-1.17
J0215.1-0422	02 15 07.20	1.08	-04 22 12.72	1.76	S	16.1 ± 1.9	16.1 ± 1.9	<3.8	<3.2	63.6 ± 14.4	-0.40
J0215.1-0315	02 15 07.30	1.09	-03 15 16.52	1.78	S	15.2 ± 2.0	15.2 ± 2.0	<4.8	<4.0	8.1 ± 19.2	-0.74
J0215.2-0449	02 15 11.17	1.10	-04 49 36.50	1.81	S	9.2 ± 1.4	9.2 ± 1.4	<5.8	<4.4	9.2 ± 16.4	-0.25
J0215.2-0343*	02 15 11.57	1.06	-03 43 11.70	1.75	М	397.5 ± 37.1	367.1 ± 37.0	8.4 ± 0.4	3.4 ± 0.3	30.6 ± 1.1	-0.50
	02 15 11.10	1.09	-03 43 18.96	1.83	С		18.2 ± 2.5	<6.7	<2.5	23.6 ± 2.5	
10215 4 0242	02 15 11.33	1.12	-03 43 24.66	1.77	C	0.5.00	12.2 ± 2.0	<5.4	<3.2	57.7 ± 9.4	0.70
J0215.4-0343	02 15 21.44	1.40	-03 43 22.07	1.98	S	9.5 ± 2.2	9.5 ± 2.2	<10.1	< 6.9	43.7 ± 19.8	<-0.79
J0215.4-0305	02 15 22.01	1.09	-03 05 30.01	1.70	5 5	12.0 ± 1.7	12.0 ± 1.7	< 5.1	< 3.8	158.0 ± 14.0 21.2 + 24.7	-0.47
J0215.4 - 0.000000000000000000000000000000000	02 15 22.08	1.10	-03 44 42.80 -04 16 18 26	1.79	S S	10.0 ± 2.4 9.6 ± 1.4	10.0 ± 2.4 9.6 ± 1.4	< 3.2 57+38	<4.5	21.2 ± 54.7 114.4 ± 14.2	-0.79
10215.4 - 0435	02 15 24.72	1.10	$-04\ 35\ 58\ 40$	1.76	S	257 + 30	257 + 30	7.0 ± 2.0	<2.8	47.7 + 3.9	-0.70
J0215.5-0320	02 15 28.81	1.25	$-03\ 20\ 15.25$	1.92	Š	7.6 ± 1.7	7.6 ± 1.7	<8.0	<7.1	-1.0 ± 71.4	<-0.64
J0215.5-0532	02 15 29.51	1.26	-05 32 58.68	1.77	\tilde{M}	39.0 ± 4.2	23.1 ± 3.5	9.2 ± 4.1	<4.2	84.0 ± 6.3	-0.22
	02 15 30.00	1.15	-05 32 56.39	1.83	С		8.0 ± 1.6	<6.3	< 5.8	-1.0 ± 88.6	
	02 15 29.10	1.19	-05 33 00.18	1.95	С		7.9 ± 1.7	<8.9	<5.2	25.7 ± 12.1	
J0215.5-0418	02 15 30.36	1.08	-04 18 11.16	1.78	М	16.2 ± 1.8	8.5 ± 1.3	<4.9	<3.7	171.0 ± 15.8	-1.00
	02 15 30.17	1.14	-04 18 14.41	1.80	С		7.7 ± 1.3	<6.3	<4.4	43.1 ± 13.7	
J0215.5-0319	02 15 30.40	1.28	-03 19 02.22	1.91	S	8.9 ± 1.9	8.9 ± 1.9	<7.9			0.02
J0215.5-0302	02 15 31.44	1.10	-03 02 17.21	1.78	S	14.3 ± 2.0	14.3 ± 2.0	<4./			-1.00
J0215.5-0440	02 15 31.57	1.23	-04 41 00.05	1.89	M	12.0 ± 1.7	6.1 ± 1.2	.5</td <td>< 6.9</td> <td>-1.0 ± 84.1</td> <td>0.15</td>	< 6.9	-1.0 ± 84.1	0.15
10215 6-0321*	02 15 28.31	1.56	$-04\ 40\ 45.14$ $-03\ 21\ 46\ 00$	1.60	M	$31/3 \pm 10.0$	0.0 ± 1.2 133 7 \pm 13 8	8.3 ± 0.1	< 0.3	03.3 ± 19.1	-0.73
J0215.0-0521*	02 15 35.20	1.07	$-03\ 21\ 40.00$ $-03\ 21\ 57\ 57$	1.75	C	514.5 ± 19.9	133.7 ± 13.0 83.7 ± 9.8	10.3 ± 0.9 11.3 ± 2.0	5.2 ± 0.8 74 + 16	42.7 ± 1.8 41.8 ± 8.4	-0.75
	02 15 34.36	1.31	-0322157.57	2.01	C		51.9 ± 9.0	14.7 ± 5.4	10.4 ± 4.1	21.0 ± 20.6	
	02 15 33.57	1.09	$-03\ 22\ 26.61$	1.78	Č		45.5 ± 5.4	8.8 ± 2.0	3.7 ± 1.9	34.8 ± 6.4	
J0215.6-0344	02 15 36.14	1.18	-03 44 27.26	1.93	М	45.0 ± 4.5	22.8 ± 3.6	9.9 ± 5.6	<3.3	32.4 ± 2.9	-0.90
	02 15 36.37	1.08	-03 44 26.12	1.77	С		22.2 ± 2.8	3.6 ± 3.1	<3.3	157.9 ± 9.1	
J0215.6-0531	02 15 36.34	1.19	-05 31 47.15	1.76	М	31.3 ± 3.2	20.4 ± 2.8	7.7 ± 3.5	<3.5	86.7 ± 4.9	-0.87
	02 15 36.35	1.08	-05 31 43.76	1.77	С		10.9 ± 1.5	<4.3	<3.6	33.8 ± 22.3	
J0215.7-0222*	02 15 42.03	1.06	-02 23 00.91	1.75	M	1206.6 ± 76.0	679.3 ± 68.1	6.2 ± 0.2	4.8 ± 0.2	179.1 ± 2.7	-0.62
	02 15 41.95	1.06	-02 22 43.52	1.75	C		245.7 ± 25.0	6.0 ± 0.5	3.8 ± 0.5	131.0 ± 4.4	
	02 15 41.94	1.07	-02 22 50.73	1.75	C		212.4 ± 21.9	11.4 ± 1.0	<1.9	78.4 ± 1.0	
	02 15 42.02	1.06	-02 22 38.39	1.62	C		39.5 ± 3.1	0.1 ± 3.7	<2.0	102.0 ± 2.7 164.2 ± 6.1	
10215 7-0401	02 15 41.70	1.00	$-02\ 23\ 00.02$ $-04\ 01\ 14\ 87$	2.00	c s	52 ± 11	29.9 ± 3.4 5 2 + 1 1	<10.1	< 6.0	104.2 ± 0.1 9.3 ± 13.0	<-0.38
10215 8-0340	02 15 45 11	1.10	$-03\ 40\ 10\ 31$	1.77	M	3.2 ± 1.1 28 9 + 3 1	3.2 ± 1.1 174 ± 23	<4 5	<3.4	1322 + 141	-0.82
30213.0 0340	02 15 44.91	1.13	-03 40 12.81	1.80	C	20.7 ± 3.1	11.5 ± 2.1	<5.6			0.02
J0215.8-0433	02 15 45.60	1.10	-04 33 35.32	1.83	S	4.5 ± 0.9	4.5 ± 0.9	<6.4	<4.4	4.0 ± 18.7	<-0.28
J0215.8-0335	02 15 46.12	1.06	-03 35 54.78	1.75	М	120.1 ± 9.2	74.3 ± 7.7	5.2 ± 0.9	<2.0	150.4 ± 3.0	-0.36
	02 15 45.93	1.07	-03 35 56.16	1.77	С		45.7 ± 5.1	7.1 ± 1.8	<2.4	30.0 ± 2.4	
J0215.9-0442	02 15 51.18	1.07	-04 42 26.56	1.77	М	13.3 ± 1.5	8.1 ± 1.1	<4.5	<3.3	14.1 ± 11.2	-0.37
	02 15 51.14	1.17	-04 42 31.22	1.82	\overline{C}	100 -	5.2 ± 1.0	<6.1			
J0215.9-0359*	02 15 52.24	1.06	-03 59 53.04	1.75	S	109.3 ± 11.1	109.3 ± 11.1	6.5 ± 0.5	3.0 ± 0.6	104.8 ± 2.6	-0.54
J0216.0-0350*	02 15 57.95	1.07	-03 50 27.32	1.76	M	96.2 ± 7.4	36.4 ± 4.0	3.6 ± 1.7	<2.9	22.8 ± 12.0	-0.67
	02 15 57.85	1.47	-03 50 31.94	1.78	C		33.4 ± 4.9	13.9 ± 5.3	<4.5 5 1 + 2 0	19.8 ± 3.3	
	02 13 37.33	1.19	-03 30 42.00	1.60	L		20.4 ± 3.8	9.3 ± 3.4	3.1 ± 2.9	02.7 ± 12.0	

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	1 2	1	0	2,		

Table A.1. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	$S_{\rm int}$	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec	• •	mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
J0216.0-0430	02 15 58.73	1.10	-04 30 54.77	1.76	S	9.7 ± 1.3	9.7 ± 1.3	<4.4	<3.7	74.3 ± 20.7	-0.74
J0216.0-0344*	02 16 00.01	1.06	-03 44 22.84	1.75	М	384.5 ± 25.2	205.5 ± 20.7	5.0 ± 0.4	<1.4	152.2 ± 1.8	-0.82
	02 15 59.83	1.07	-03 44 24.44	1.76	С		126.6 ± 13.2	10.1 ± 1.2	<1.9	30.9 ± 1.2	
	02 15 59.11	1.18	-03 44 16.10	1.76	С		33.0 ± 4.5	6.9 ± 3.6	<3.1	101.0 ± 3.8	
	02 15 59.11	1.16	-03 44 19.94	1.78	С		19.3 ± 2.9	<5.8	<4.6	92.9 ± 17.8	
J0216.0-0432	02 16 00.90	1.11	-04 32 45.62	1.78	S	8.4 ± 1.2	8.4 ± 1.2	<5.6	<3.8	44.3 ± 9.6	-0.53
J0216.0-0244	02 16 00.98	1.44	-02 44 51.50	1.80	S	6.5 ± 1.4	6.5 ± 1.4	<9.1	<5.5	83.6 ± 13.3	-0.39
J0216.1-0510	02 16 03.26	1.08	-05 10 10.02	1.79	M	14.2 ± 1.7	9.0 ± 1.3	<5.1	<3.6	172.4 ± 11.0	-0.80
1001 (1 0505	02 16 03.01	1.50	-05 10 13.73	1.84	C	45.7 0.6	5.2 ± 1.1	<9.6	<6.6	82.9 ± 18.8	0.(1
J0216.1-050/	02 16 03.66	1.06	-05 07 59.27	1.75	M	45.7 ± 3.6	25.9 ± 2.7	<2.4	<2.2	163.6 ± 12.1	-0.61
10016 1 0056	02 16 03.43	1.09	-05 08 00.76	1.78	C	0.0 . 1.5	19.8 ± 2.3	1.1 ± 2.1	<2.3	38.5 ± 1.8	0.74
J0216.1-0256	02 16 03.79	1.18	-02 56 49.49	1.79	5	8.8 ± 1.5	8.8 ± 1.5	< 6.2	< 5.2	96.6 ± 28.0	<-0.74
J0210.1-0244	02 16 03.83	1.50	-02 43 51.71	1.85	M	48.0 ± 5.1	21.4 ± 3.4	12.8 ± 4.8	4.2 ± 3.7	54.5 ± 1.1	-0.45
	02 16 04.32	1.09	-02 43 54.89	2.08	C		14.9 ± 2.7 12.2 ± 2.6	10.4 ± 0.0	<4.2	1.9 ± 4.5	
10216 1-0503	02 16 03.80	1.56	-024403.30 -05031350	1.90	s	63 ± 12	12.2 ± 2.0 63 + 12	9.5 ± 0.8	<5.7	41.0 ± 22.2 $1/1/3 \pm 1/7/2$	-0.67
J0216.1-0303	02 16 07 32	1.17	-02343300	1.05	S	0.3 ± 1.2 7.4 ± 1.6	0.3 ± 1.2 7 4 ± 1.6	<0.0	< 5.7	144.3 ± 47.2 185 ± 401	-0.67
J0216.1-0234	02 16 07.32	1.23	-02.34.33.90 -02.26.01.83	1.92	M	7.4 ± 1.0 56.2 + 5.0	7.4 ± 1.0 38 3 + 1 1	< 0.2	<3.0	10.5 ± 40.1 50.0 ± 6.1	<-0.02 -0.57
30210.1 0220	02 16 07 89	1.00	$-02\ 25\ 59\ 52$	1.70	C	50.2 ± 5.0	17.8 ± 2.3	<46	<3.6	143.6 ± 12.9	0.57
10216 1-0448	02 16 07 80	1.10	-04 48 45 32	2.06	Š	5.3 ± 1.0	5.3 ± 1.0	< 9.8	<4.3	176.8 ± 5.6	<-0.38
J0216.1-0446	02 16 08.36	1.07	-04 46 46.33	1.75	ŝ	28.8 ± 3.1	28.8 ± 3.1	5.0 ± 1.3	<2.3	59.4 ± 3.7	-0.41
J0216.2-0426	02 16 10.91	1.06	-04 26 08.85	1.75	М	23.4 ± 2.2	18.6 ± 2.0	<2.8	<2.5	145.8 ± 15.4	-0.01
	02 16 10.62	1.20	-04 26 11.94	1.83	С		4.8 ± 0.9	<7.7	<4.4	46.6 ± 10.3	
J0216.2-0321	02 16 13.61	1.11	-03 21 38.48	1.85	S	17.2 ± 2.6	17.2 ± 2.6	8.6 ± 3.7	<4.7	0.9 ± 10.5	-0.32
J0216.3-0512	02 16 16.68	1.19	-05 12 57.31	1.85	S	5.4 ± 1.0	5.4 ± 1.0	<7.7	<4.5	42.2 ± 10.1	0.15
J0216.3-0507	02 16 17.93	1.14	-05 07 21.89	1.86	S	4.1 ± 0.8	4.1 ± 0.8	<7.2	<4.9	26.6 ± 19.2	<-0.21
J0216.3-0245*	02 16 20.00	1.13	-02 45 31.98	1.96	М	314.8 ± 32.4	278.8 ± 32.0	34.8 ± 4.4	12.2 ± 1.6	164.5 ± 1.9	0.01
	02 16 20.96	1.21	-02 45 42.01	1.88	С		27.4 ± 4.7	9.5 ± 4.7	<5.6	144.6 ± 13.2	
	02 16 19.80	1.18	-02 44 27.73	2.23	S		8.7 ± 2.2	<11.4	<6.1	174.0 ± 12.7	0.01
J0216.3-0459	02 16 20.25	1.10	-04 59 25.00	1.79	S	5.2 ± 0.9	5.2 ± 0.9	<5.2	<4.4	33.3 ± 33.4	<-0.37
J0216.3-0532	02 16 21.12	1.06	-05 32 58.43	1.79	M	12.3 ± 1.5	6.4 ± 0.7	<5.3	<0.7	0.9 ± 0.3	<-0.97
	02 16 20.79	1.53	-05 32 58.95	1.92	С		5.9 ± 1.4	<10.3	<7.2	64.0 ± 20.6	
J0216.5-0345	02 16 27.15	1.06	-03 45 19.30	1.75	S	43.4 ± 4.5	43.4 ± 4.5	4.1 ± 0.9	<2.1	57.3 ± 5.2	-0.90
J0216.5-0242	02 16 29.01	1.09	-02 42 35.58	1.77	S	16.8 ± 2.1	16.8 ± 2.1	<4.2	<4.0	58.0 ± 57.4	-1.10
J0216.5-0454	02 16 30.87	1.14	-04 54 50.06	1.79	S	4.4 ± 0.9	4.4 ± 0.9	<5.7	<4.9	54.8 ± 49.4	-0.21
J0216.5-044/	02 16 32.25	1.22	-04 4 / 42.40	1.86	C	4.9 ± 1.0	4.9 ± 1.0	<1.4	<6.2	41.1 ± 42.9	0.02
J0216.6-0311	02 16 34.78	1.08	-03 11 11.64	1.78	S	12.0 ± 1.6	12.0 ± 1.6	<4.6	< 3.8	21.1 ± 19.0	0.82
J0216.6-0454	02 16 34.96	1.38	-04 54 29.56	1.99	5	4.4 ± 1.0	4.4 ± 1.0	<10.6	< 5.4	42.2 ± 9.4	-0.21
J0210.0-0447	02 16 35.50	1.08	-04 47 00.93	1.70	M C	49.5 ± 5.9	20.0 ± 3.0 17.2 ± 2.2	0.1 ± 1.0 75 + 2.0	< 3.0	30.0 ± 0.3 71.6 + 4.4	-0.58
	02 10 34.75	1.15	-04 47 02.37	1.70	C		17.5 ± 2.5 5.4 ± 1.0	7.5 ± 3.0	< 3.5	71.0 ± 4.4 117.0 ± 16.8	
10216 6-0409	02 16 37 07	1.10	-04 10 00 53	1.78	s	49 ± 10	3.4 ± 1.0 4.9 ± 1.0	<0.2	<4.5	77 ± 38.6	< -0.34
J0216.6-0407	02 16 37.07	1.20	$-04\ 47\ 36\ 55$	1.70	C	4.9 ± 1.0 8 4 + 1 3	$\frac{4.9 \pm 1.0}{8.4 \pm 1.3}$	<5.6	<3.9	73.0 ± 12.5	<-0.54
J0216.7-0438	02 16 38 98	1.08	-04 38 05 76	1.86	S	48 ± 0.9	4.8 ± 0.9	<7.1	<3.8	174.6 ± 9.1	<-0.32
J0216.7-0444*	02 16 40.74	1.06	-04 44 07.80	1.75	S	153.0 ± 15.3	153.0 ± 15.3	2.0 ± 0.3	<1.1	58.8 ± 6.5	-0.37
J0216.7-0436	02 16 42.26	1.22	-04 36 03.08	1.89	ŝ	4.5 ± 1.0	4.5 ± 1.0	<7.8	<6.5	154.4 ± 49.0	<-0.28
J0216.7-0224	02 16 42.43	1.31	-02 24 47.89	1.81	М	65.1 ± 6.9	42.0 ± 6.3	13.2 ± 4.2	6.8 ± 2.8	73.8 ± 9.4	-0.75
	02 16 42.44	1.07	-02 24 42.76	1.76	С		23.1 ± 2.7	<3.7	<3.3	170.7 ± 25.7	
J0216.7-0341	02 16 42.62	1.07	-03 41 19.68	1.77	S	22.6 ± 2.6	22.6 ± 2.6	6.4 ± 1.9	<3.1	15.7 ± 5.5	-0.73
J0216.7-0358	02 16 43.59	1.20	-03 58 17.82	1.86	S	5.9 ± 1.2	5.9 ± 1.2	<7.0	<6.5	-1.0 ± 87.3	0.27
J0216.7-0306	02 16 44.78	1.16	-03 06 17.06	1.80	S	6.3 ± 1.1	6.3 ± 1.1	<6.7	<4.0	50.1 ± 10.4	-0.17
J0216.8-0337*	02 16 45.78	1.08	-03 37 19.13	1.77	М	150.7 ± 11.2	85.5 ± 9.0	14.9 ± 1.6	<2.1	35.7 ± 0.9	-0.74
	02 16 45.78	1.06	-03 37 20.83	1.75	С		65.2 ± 6.7	4.7 ± 0.8	<1.9	148.9 ± 3.3	
J0216.8-0237*	02 16 47.21	1.06	-02 37 21.60	1.75	S	82.1 ± 8.3	82.1 ± 8.3	2.0 ± 0.8	<1.7	1.2 ± 21.7	-0.76
J0216.8-0401	02 16 49.10	1.18	-04 01 44.50	1.92	М	10.3 ± 1.4	5.3 ± 1.0	<8.1	<6.1	166.6 ± 21.8	-0.56
	02 16 49.32	1.15	-04 01 33.91	1.88	С		5.0 ± 1.0	<7.4	<5.7	176.2 ± 24.7	
J0216.8-0427	02 16 49.51	1.23	-04 27 39.88	1.88	S	4.4 ± 1.0	4.4 ± 1.0	<7.3			-0.51
J0216.9-0315	02 16 50.90	1.27	-03 15 28.94	1.85	S	5.9 ± 1.2	5.9 ± 1.2	<8.0	< 5.8	52.7 ± 21.8	0.23
J0216.9-0215	02 16 51.00	1.13	-02 15 27.01	1.82	S	9.7 ± 1.8	9.7 ± 1.8	<6.2	< 5.2	158.0 ± 38.2	0.10
J0216.9-0333	02 16 51.55	1.34	-03 33 51.85	1.8/	5	7.0 ± 1.4	7.0 ± 1.4	< 9.2	< 5.0	53.1 ± 9.2	-0.22
J0210.9-0314	02 16 55.27	1.10	-03 14 10.44	1.//	M	83.3 ± 0.7	37.0 ± 4.4	7.2 ± 1.9	5.5 ± 1.8	93.1 ± 21.4	-0.80
	02 16 55.15	2.22	-03 13 55.20	1.//	C		27.3 ± 4.3	24.3 ± 9.0	<4.1	94.7 ± 2.0	
10216.0-0520	02 10 34.94	1.07	-03 13 49.23	1.70	c c	268 ± 20	21.0 ± 2.4 26.8 ± 2.0	< 3.3 1 1 ± 1 7	<2.9 ~2 1	131.3 ± 19.1 128 ± 12	_0.82
I0217 0_0401	02 16 55.50	1.07	-03 39 39.33	1.70	5	20.0 ± 3.0 4.0 ± 0.7	20.0 ± 3.0 4.0 ± 0.7	+.1 ± 1./ <5 5	<2.4 <5.0	$+2.0 \pm 4.3$ -10 + 761	<-0.02 <-0.20
J0217.0-0401	02 16 57 26	1.12	-03 21 11 78	1.00	S	60 + 13	60 ± 13	< 8.6	<5.8	40.6 ± 18.6	<-0.48
J0217.0-0548	02 16 57 64	1.20	-05 48 11 81	1.80	ŝ	5.8 ± 1.2	5.8 ± 1.2	<93	<5.2	80.5 ± 11.0	<-0.45
J0217.0-0220	02 16 58 13	1.11	$-02\ 20\ 56\ 04$	1.76	ŝ	24.3 ± 3.0	24.3 ± 3.0	6.0 ± 2.5	<3.3	108.9 ± 6.0	-0.74
J0217.0-0308	02 16 58.81	1.26	-03 08 39.91	1.80	M	19.8 ± 2.6	13.4 ± 2.3	7.8 ± 4.5	<5.2	102.7 ± 13.7	-0.93
	02 16 58.23	1.16	-03 08 37.73	1.91	С		6.4 ± 1.3	<8.0	<5.6	16.4 ± 17.6	
J0217.0-0449*	02 16 58.86	1.11	-04 50 06.23	2.58	S	96.4 ± 9.5	71.0 ± 9.0	48.2 ± 9.0	7.6 ± 1.8	4.8 ± 1.2	-1.66
	02 16 58.98	1.13	-04 48 49.89	2.24	М		16.7 ± 2.8	19.2 ± 7.1	<5.1	5.2 ± 4.0	-1.66
	02 16 59.06	1.24	-04 48 30.64	2.00	С		8.8 ± 1.8	9.7 ± 5.9	<7.1	5.5 ± 23.9	
J0217.0-0516	02 17 02.60	1.10	-05 16 20.50	1.82	S	4.6 ± 0.8	4.6 ± 0.8	<6.4	<3.5	28.5 ± 8.5	<-0.29

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Table A.1. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{int}	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
J0217.1-0210*	02 17 02.80	1.06	-02 10 45.51	1.75	M	266.7 ± 20.1	180.8 ± 18.3	6.7 ± 0.5	4.7 ± 0.5	44.0 ± 4.4	-0.67
	02 17 04.30	1.07	$-02\ 10\ 50.74$ $-02\ 10\ 46\ 94$	1.70	C		75.7 ± 8.0 10.2 ± 1.0	6.1 ± 1.0	3.3 ± 1.1	9.2 ± 7.0 12.8 ± 22.7	
I0217 1-0430	02 17 03.33	1.12	$-02\ 10\ 40.94$ $-04\ 30\ 33\ 01$	2 17	S	48 + 10	10.2 ± 1.9 4 8 + 1 0	<10.9	<4.9	12.8 ± 22.7 178.0 ± 6.0	<-0.32
J0217.0-0421	02 17 03.10	1.09	$-04\ 21\ 50.47$	1.83	M	11.2 ± 1.4	4.0 ± 1.0 6.0 ± 1.0	<6.6	<3.2	158.5 ± 5.8	<-0.90
	02 17 02.41	1.22	-04 21 32.95	1.98	С		5.2 ± 1.0	<9.6	<4.0	148.2 ± 5.7	
J0217.1-0422*	02 17 05.51	1.06	-04 22 56.85	1.75	S	153.1 ± 15.4	153.1 ± 15.4	2.9 ± 0.3	1.0 ± 0.7	43.7 ± 4.4	-0.53
J0217.1-0305	02 17 06.36	1.08	-03 05 51.28	1.77	S	15.5 ± 1.9	15.5 ± 1.9	<4.0			-0.30
J0217.1-0315	02 17 06.76	1.74	-03 15 12.00	1.92	S	11.1 ± 2.5	11.1 ± 2.5	12.1 ± 8.2	<7.4	72.3 ± 14.9	-0.63
J0217.1-0337	02 17 07.68	1.23	-03 37 25.14	1.81	5	4.1 ± 0.9	4.1 ± 0.9	< 6.9	<5.7	82.9 ± 42.7	-0.41
J0217.2-0244 J0217.2-0310	02 17 09.42	1.12	-024458.21 -03102524	1.60	S	6.9 ± 1.4 165 + 10	6.9 ± 1.4 165 + 19	<3.7	<4.5	30.0 ± 19.2 0.2 + 11.6	-0.50
J0217.2-0310	02 17 12.97	1.10	$-03\ 53\ 43\ 73$	1.70	S	46 ± 0.8	46 ± 0.8	<6.6	<4.2	13.6 + 13.0	-0.48
J0217.3-0248	02 17 16.07	1.15	-02 48 04.53	1.76	\widetilde{M}	44.5 ± 4.1	32.2 ± 3.8	11.8 ± 2.5	<2.9	69.5 ± 2.2	-0.92
	02 17 16.27	1.08	$-02\ 48\ 00.07$	1.76	С		12.3 ± 1.5	<3.8	<3.6	158.3 ± 50.0	
J0217.3-0407	02 17 16.82	1.11	-04 07 51.57	1.77	S	4.6 ± 0.8	4.6 ± 0.8	<4.8	<4.0	81.1 ± 30.5	-0.54
J0217.3-0333	02 17 18.13	1.15	-03 33 39.31	1.86	S	5.6 ± 1.2	5.6 ± 1.2	<7.2	<5.5	22.8 ± 27.3	<-0.43
J0217.3-0214	02 17 18.41	1.18	-02 14 50.34	1.82	S	9.7 ± 1.7	9.7 ± 1.7	< 6.6	< 5.6	127.0 ± 36.2	-0.95
I0217.3-0339	02 17 18.73	1.10	-03 26 04 87	1.76	S M	124.1 ± 10.7	103.8 ± 10.6	<4.9	37 ± 0.6	-1.0 ± 60.3 88.6 + 3.1	-0.02
30217.5 0320	02 17 19.04	1.06	-03 26 06.03	1.94	C	124.1 ± 10.7	7.8 ± 1.1	<8.2	<1.9	2.6 ± 1.2	0.97
	02 17 19.31	1.08	-03 26 11.18	1.80	Ĉ		6.7 ± 1.1	<5.4	<3.8	5.6 ± 15.3	
	02 17 20.41	1.11	-03 26 04.73	1.77	С		5.8 ± 1.0	<5.0	<4.0	61.2 ± 29.0	
J0217.3-0318	02 17 20.10	1.14	-03 18 55.96	2.25	S	5.7 ± 1.2	5.7 ± 1.2	<11.7	<4.5	167.6 ± 5.3	<-0.44
J0217.4-0339*	02 17 21.54	1.06	-03 39 48.54	1.75	M	119.0 ± 11.4	113.2 ± 11.4	5.0 ± 0.3	3.2 ± 0.4	103.0 ± 3.5	-0.53
10217 4 0427	02 17 21.18	1.15	-03 39 54.38	1.81	C	17.6 ± 1.0	5.8 ± 1.0	< 6.8	<3.6	137.4 ± 6.9	0.56
J0217.4-0427 J0217.4-0452	02 17 22.23	1.07	$-04\ 27\ 03.93$ $-04\ 52\ 50\ 46$	1.75	S	$1/.0 \pm 1.9$ 3.0 ± 0.7	$1/.0 \pm 1.9$ 3.0 ± 0.7	2.5 ± 2.1	<2.4	41.3 ± 5.3 74.2 ± 33.5	-0.56
J0217.4-0432 J0217.5-0213	02 17 24.78	1.15	-021301.75	1.78	S	19.5 ± 0.7	19.5 ± 0.7	13.8 + 7.9	<6.0	74.2 ± 33.3 839 + 7.7	-1.33
J0217.5-0221	02 17 30.25	1.09	$-02\ 21\ 27.20$	1.76	S	31.9 ± 3.8	31.9 ± 3.8	6.2 ± 2.0	<3.5	118.6 ± 9.8	-0.91
J0217.5-0224	02 17 30.92	1.06	-02 24 42.57	1.75	М	108.9 ± 10.3	100.8 ± 10.2	1.9 ± 0.7	<1.5	175.1 ± 8.2	-0.11
	02 17 30.48	1.12	-02 24 47.67	1.77	С		8.1 ± 1.4	<5.1	<4.4	86.0 ± 44.2	
J0217.5-0507	02 17 31.04	1.13	-05 07 12.12	1.84	S	3.7 ± 0.7	3.7 ± 0.7	<7.0	<4.4	29.8 ± 13.2	<-0.15
J0217.6-0313*	02 17 34.19	1.06	-03 13 10.48	1.75	M	103.1 ± 7.8	64.7 ± 6.6	4.5 ± 0.6	<1.6	142.8 ± 2.2	-0.76
10217 6-0408	02 17 34.12	1.07	-03 13 13.05 -04 08 06 85	1.75	C S	3.1 ± 0.7	38.4 ± 4.1 3.4 ± 0.7	5.7 ± 1.2	<2.3	37.1 ± 3.3 193 + 140	<-0.08
J0217.6-0513	02 17 35.01	1.17	-051331.45	1.92	S	3.9 ± 0.7	3.4 ± 0.7 3.9 ± 0.9	<10.0	<6.2	125.2 ± 15.4	-0.37
J0217.7-0401	02 17 40.08	1.08	$-04\ 02\ 00.75$	1.76	Š	10.7 ± 1.3	10.7 ± 1.3	<3.8	<3.4	26.5 ± 25.0	<-0.87
J0217.7-0541*	02 17 41.61	1.12	-05 41 55.71	1.77	Μ	171.2 ± 12.3	100.8 ± 11.0	18.1 ± 2.0	7.0 ± 1.0	57.5 ± 2.1	-0.67
	02 17 40.43	1.10	-05 41 50.63	1.77	С		39.5 ± 4.5	10.8 ± 2.0	<3.0	49.1 ± 2.9	
	02 17 39.78	1.14	-05 41 53.22	1.80	C		16.4 ± 2.4	7.2 ± 3.4	<4.6	42.9 ± 12.1	
102177 0252	02 17 40.77	1.22	-05 41 52.57	2.00	C	22.1 + 2.5	14.6 ± 2.5	11.0 ± 6.4	<4.1	149.4 ± 4.2	0.90
J0217.7-0352 J0217.7-0354	02 17 42.20	1.07	-035207.53 -03545355	1.70	3 5	23.1 ± 2.3 20.6 ± 3.1	23.1 ± 2.3 20.6 ± 3.1	4.9 ± 1.4 2.0 ± 1.1	<2.0	30.0 ± 3.3 113.8 ± 10.8	-0.89
J0217.7=0334 J0217.7=0417	02 17 42.82	1.00	$-03\ 54\ 53.55$ $-04\ 17\ 32\ 47$	1.75	M	29.0 ± 3.1 80 + 09	47 ± 0.7	2.9±1.1	<2.5	113.8 ± 10.8 60.0 ± 3.9	-0.97
30217.7 0117	02 17 43.56	1.15	-04 17 29.79	1.78	C	0.0 ± 0.9	3.3 ± 0.5	<6.3	<2.4	56.6 ± 3.7	0.76
J0217.8-0500	02 17 45.85	1.11	-05 00 58.87	1.78	S	4.2 ± 0.7	4.2 ± 0.7	<5.2	<4.0	47.1 ± 25.6	<-0.23
J0217.8-0239	02 17 46.56	1.13	-02 39 09.96	1.79	S	7.5 ± 1.3	7.5 ± 1.3	<6.0	<4.4	45.3 ± 17.7	-0.64
J0217.8-0541	02 17 46.87	1.13	-05 41 40.07	1.80	M	32.8 ± 3.2	19.6 ± 2.5	9.5 ± 3.2	<3.1	42.3 ± 3.0	-0.70
	02 17 46.93	1.15	-05 41 39.10	1.82	C	100 10	13.2 ± 2.0	7.7 ± 4.2	<3.9	138.6 ± 5.8	0.54
J0217.9-0448	02 17 52.54	1.08	-04 48 26.17	1.76	5	10.2 ± 1.2	10.2 ± 1.2	<3.6	<3.3	68.4 ± 33.7	-0.54
J0217.9-0512 J0217.9-0526	02 17 54.13	1.07	-051251.80 -052654.89	1.70	S	13.2 ± 1.7 95 ± 13	13.2 ± 1.7 95 + 13	< 3.3 4 5 + 3 3	<2.9 ~3.0	04.2 ± 10.3 40.2 ± 11.3	-0.95
J0217.9-0320	02 17 55.07	1.10	$-03\ 46\ 03.75$	1.80	M	11.0 ± 1.7	11.0 ± 1.7	4.5 ± 3.5 8.4 ± 3.6	5.6 ± 3.3	76.3 ± 23.7	-0.18
J0218.0-0346	02 17 57.45	1.10	-03 46 48.80	1.79	C	13.5 ± 1.4	7.1 ± 1.0	<5.8	<2.9	36.3 ± 4.4	
	02 17 57.61	1.10	-03 46 49.20	1.77	С		6.5 ± 0.9	<5.2	<3.4	135.1 ± 9.6	
J0218.0-0347	02 17 58.03	1.15	-03 47 59.76	1.85	S	3.8 ± 0.8	3.8 ± 0.8	<7.3	<4.6	31.2 ± 13.6	<-0.17
J0218.0-0432	02 17 58.90	1.10	-04 32 57.88	1.81	S	4.9 ± 0.8	4.9 ± 0.8	<5.8	<4.3	9.5 ± 18.2	<-0.34
J0218.0-0450	02 18 00.65	1.15	-04 50 05.99	1.77	S	3.9 ± 0.7	3.9 ± 0.7	< 5.8	<4.0	110.2 ± 16.2	0.10
JU218.0-0344	02 18 01.32	1.11	$-03\ 44\ 02.13$ $-02\ 01\ 17\ 74$	1.70	s r	11.4 ± 1.3 12.3 ± 2.1	11.4 ± 1.3 12.3 ± 2.1	3.8 ± 2.8	<4.2	123.9 ± 17.0 110.0 ± 35.7	-0.80
10218 0-0341	02 18 01.33	1.14	-02 01 17.74 -03 41 31 65	1.79	S	12.3 ± 2.1 21.5 + 2.3	12.5 ± 2.1 21.5 + 2.3	2.6 ± 1.5	< <u>+</u> .9 <23	21.6 ± 7.1	-0.82
J0218.1-0306	02 18 03.26	1.12	-03 06 25.38	1.79	S	7.8 ± 1.2	7.8 ± 1.2	<5.3	<4.7	49.3 ± 42.5	-0.64
J0218.1-0538	02 18 03.28	1.11	-05 38 27.71	1.78	M	27.0 ± 2.6	19.3 ± 2.4	7.8 ± 2.8	<2.8	47.9 ± 2.8	-0.66
	02 18 03.40	1.14	-05 38 28.14	1.77	С		7.7 ± 1.2	<5.7	<3.5	117.3 ± 7.9	
J0218.1-0456	02 18 05.14	1.16	-04 56 25.71	1.78	S	5.2 ± 0.9	5.2 ± 0.9	<6.1	<4.3	118.8 ± 14.4	<-0.38
J0218.1-0501	02 18 07.47	1.10	-05 01 49.38	1.94	S	4.3 ± 0.9	4.3 ± 0.9	<8.3	<4.4	2.1 ± 9.4	<-0.25
JU218.1-0324	02 18 07.64	1.09	-03 24 38.95	1.77	S	8.4 ± 1.1	8.4 ± 1.1	<4.4	<3.8	50.7 ± 24.6	-0.61
JU218.1-U546	02 18 07.90	1.09		1.//	5	14.0 ± 1.8 8 2 + 1 2	14.0 ± 1.8	4.1 ± 2.5	3.8 ± 2.7	$-1.0 \pm /1.2$	-0.21
10218.1-0504	02 18 08 81	1.17	-05 48 26 98	1.79	S	0.2 ± 1.3 55 + 10	0.2 ± 1.3 55 + 10	5.0 ± 4.4	< 1.0	40.2 ± 21.7	-0.09 -0.69
J0218.2-0459	02 18 09.37	1.10	-04 59 48.25	1.80	S	6.2 ± 1.0	6.2 ± 1.0	<5.4	<4.5	4.2 ± 29.7	<-0.50
J0218.2-0319	02 18 11.26	1.08	-03 19 37.65	1.78	м М	38.6 ± 3.0	17.4 ± 2.2	5.5 ± 2.3	<3.7	15.0 ± 12.0	-0.77
	02 18 12.37	1.10	-03 20 23.86	1.78	С		10.7 ± 1.5	<4.6			

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Table A.1. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Type	Sint	Scomp	Major axis	Minor axis	Position	Spectral
1 (dillo	J2000	arcsec	J2000	arcsec	Type	mJy	mJy	arcsec	arcsec	Angle	index α_{225}^{1400}
	02 18 10.97	1.29	-03 19 47.94	1.92	С	,	5.5 ± 1.1	<8.9	<6.3	139.4 ± 18.5	323
	02 18 12.61	1.18	-03 20 25.34	1.86	С		5.0 ± 1.0	<7.8	<4.6	36.8 ± 12.1	
J0218.2-0301*	02 18 12.33	1.06	-03 01 32.18	1.75	М	131.7 ± 9.5	77.9 ± 7.9	4.6 ± 0.6	3.5 ± 0.6	90.8 ± 11.2	-0.98
	02 18 11.25	1.07	-03 01 22.45	1.76	C		47.9 ± 5.1	6.2 ± 1.1	4.6 ± 1.1	130.9 ± 12.9	
10218 2 0427	02 18 11.90	1.22	-03 01 38.16	1.86	C	46+08	5.9 ± 1.1	<8.3	< 3.9	137.6 ± 6.6	< 0.20
J0218.2-0427 J0218 3-0453	02 18 15.51	1.20	$-04\ 27\ 04.38$ $-04\ 53\ 48\ 92$	1.70	s s	4.0 ± 0.8 4.6 ± 0.9	4.0 ± 0.8 4.6 ± 0.9	< 0.7	<4.7	75.0 ± 14.9 175.8 ± 12.3	<-0.30
J0218.3-0435	02 18 15.82	1.10	-03 16 03 47	2.08	S	4.3 ± 1.0	4.0 ± 0.9 4.3 ± 1.0	<10.1	<5.9	175.0 ± 12.5 15.3 ± 12.4	<-0.25
J0218.3-0446*	02 18 18.05	1.06	-04 46 09.15	1.75	м М	191.9 ± 18.1	180.6 ± 18.1	4.0 ± 0.2	1.4 ± 0.4	1.4 ± 1.8	-0.76
	02 18 17.67	1.17	-04 46 14.61	1.89	С		5.9 ± 0.9	<8.4	<2.2	144.7 ± 1.6	
	02 18 17.70	1.08	-04 46 11.65	1.80	С		5.4 ± 0.7	<5.9	<1.5	153.2 ± 1.3	
J0218.3-0515	02 18 18.33	1.21	-05 15 47.76	1.82	S	5.1 ± 1.0	5.1 ± 1.0	<7.0	<5.4	122.6 ± 28.6	<-0.36
J0218.3-0547	02 18 18.72	1.12	-05 47 12.23	1.86	S	4.9 ± 1.0	4.9 ± 1.0	<7.0	<4.9	12.7 ± 20.3	-0.55
J0218.3-0403	02 18 18.85	1.13	-04 03 29.05	1.77	M	25.5 ± 2.6	13.3 ± 1.7	7.4 ± 2.8	<3.8	67.4 ± 7.2	-0.55
	02 18 17.75	1.02	-04 03 32.82	1.97	C		8.2 ± 1.8	12.2 ± 7.9	< 0.0	37.3 ± 10.8	
10218 3-0441	02 18 20.00	1.42	$-04\ 03\ 30.37$	1.00	c c	50 ± 10	4.1 ± 0.9 5 0 ± 1 0	< 9.0	< 0.8	70.9 ± 24.0 6.2 ± 3.8	<-0.47
J0218.3-0441 J0218 3-0438	02 18 20.34	1.03	-04 41 38.81 -04 38 34 97	1.99	S	5.9 ± 1.0 5.2 ± 0.9	5.9 ± 1.0 5.2 ± 0.9	< 8.8	<3.3	0.2 ± 5.8 1764 + 41	<-0.38
J0218.4-0516	02 18 22.44	1.11	-05 16 51.13	1.78	S	5.2 ± 0.9 5.4 ± 0.9	5.2 ± 0.9 5.4 ± 0.9	<5.1	<4.1	51.0 ± 26.8	-0.58
J0218.4-0214	02 18 22.58	1.10	-02 14 37.72	1.78	Ŝ	12.4 ± 1.8	12.4 ± 1.8	<5.4	<3.5	144.5 ± 8.0	<-0.97
J0218.4-0542	02 18 22.70	1.28	-05 42 17.07	1.77	Μ	32.8 ± 3.2	20.4 ± 2.8	12.2 ± 4.0	<3.7	98.6 ± 3.5	-0.32
	02 18 22.45	1.07	-05 42 13.45	1.76	С		12.4 ± 1.5	<3.9	<2.7	14.0 ± 6.8	
J0218.4-0229	02 18 22.71	1.08	-02 29 37.65	1.76	S	14.7 ± 1.8	14.7 ± 1.8	<3.9	<3.4	118.4 ± 18.9	-0.51
J0218.4-0525	02 18 23.46	1.15	-05 25 02.50	1.89	S	5.7 ± 1.0	5.7 ± 1.0	<8.1	<3.9	29.7 ± 6.4	0.49
J0218.4-0419	02 18 23.51	1.07	-04 19 02.22	1.75	S	17.0 ± 1.8	17.0 ± 1.8	<2.9	<2.5	47.7 ± 13.1	-0.67
J0218.4-0406	02 18 23.59	1.20	-04 06 15.35	1.76	S	5.1 ± 0.7	5.1 ± 0.7	<6.6	<2.7	100.9 ± 3.3	<-0.36
J0218.4-0453	02 18 24.00	1.07	-04 53 06.51	1.70	S	$1/.5 \pm 2.0$	17.5 ± 2.0	<3.3	<2.8	29.0 ± 11.7	-0.52
J0218.4-0343	02 18 25.30	1.10	-034339.30 -04595024	1.70	S	16.0 ± 2.2	0.1 ± 1.0 16.0 ± 2.2	< 3.0	<4.2	41.3 ± 34.0 54.6 ± 9.3	-0.48
J0218.5-0412	02 18 23.30	1.12	$-04\ 12\ 21\ 90$	1.86	S	3.9 ± 0.8	39 ± 0.8	<7.5	<6.2	36.2 + 37.8	0.12
J0218.5-0454*	02 18 27.29	1.06	-04 54 39.68	1.75	\tilde{M}	296.4 ± 19.5	183.5 ± 18.4	7.6 ± 0.3	2.5 ± 0.4	28.7 ± 1.0	-0.87
	02 18 27.01	1.06	-04 54 49.32	1.75	С		40.5 ± 4.2	<2.3	<2.0	138.6 ± 6.7	
	02 18 26.86	1.07	-04 54 54.67	1.75	С		28.1 ± 3.0	2.4 ± 1.7			
	02 18 27.63	1.08	-04 54 28.49	1.75	С		25.3 ± 2.8	4.1 ± 1.9	<2.1	60.8 ± 2.6	
	02 18 27.56	1.08	-04 54 32.04	1.75	С		19.0 ± 2.1	3.3 ± 2.5	<1.9	86.4 ± 2.0	
J0218.5-0534	02 18 27.54	1.08	-05 34 55.78	1.76	S	13.5 ± 1.6	13.5 ± 1.6	3.3 ± 2.8	<3.4	45.9 ± 12.8	-0.81
J0218.5-0418	02 18 32.62	1.13	-04 18 28.48	1.78	M	9.4 ± 1.0	5.3 ± 0.8	<6.0	<3.2	52.5 ± 5.8	-1.02
10219 5 0216	02 18 32.56	1.07	-04 18 25.68	1.//	C	72 . 15	4.0 ± 0.6	<4.3	<3.0	29.7 ± 13.3	0.17
J0218.3-0210 J0218 6-0259	02 18 32.79	1.24	$-02\ 10\ 24.13$ $-02\ 59\ 13\ 98$	1.92	S	7.3 ± 1.3 185 + 21	7.5 ± 1.5 185 + 21	< 3.6	< 3.3	143.8 ± 14.0 12.8 ± 31.4	-0.17
J0218.5-0313	02 18 33 24	1.09	-03 13 33 34	1.77	M	10.5 ± 2.1 33.8 ± 2.5	10.5 ± 2.1 11.6 ± 1.5	<4.6	<3.1	133.2 + 7.0	-0.99
0021010 0010	02 18 32.99	1.11	$-03\ 13\ 35.30$	1.77	C	0010 = 210	8.9 ± 1.3	<5.2	<3.8	54.2 ± 11.9	0.77
	02 18 31.18	1.16	-03 13 43.58	1.82	С		7.0 ± 1.2	<6.8	<4.7	41.6 ± 13.0	
	02 18 32.48	1.16	-03 13 36.01	1.79	С		6.2 ± 1.1	<5.9	<5.2	95.0 ± 53.4	
J0218.6-0248	02 18 33.67	1.07	-02 48 08.93	1.76	S	14.4 ± 1.7	14.4 ± 1.7	<3.7	<3.4	161.7 ± 30.5	-0.44
J0218.6-0346	02 18 34.90	1.26	-03 46 17.10	1.82	S	4.7 ± 0.9	4.7 ± 0.9	<7.6	<5.9	66.4 ± 25.4	<-0.31
J0218.6-0246	02 18 35.39	1.13	-02 46 27.52	1.80	S	9.4 ± 1.5	9.4 ± 1.5	<6.0	<4.6	41.1 ± 16.7	-0.49
J0218.6-0357	02 18 36.88	1.21	-03 57 12.27	1.80	M	16.5 ± 1.7	9.0 ± 1.4	8.3 ± 5.4	<3.3	42.8 ± 3.2	-1.22
10218 6-0334	02 18 37.00	1.12	-03 37 12.31 -03 34 12 79	1.70	c s	93 ± 12	7.3 ± 1.0 9.3 ± 1.2	< 3.1 37 + 31	< 3.4	113.0 ± 0.0 34.1 ± 33.0	-0.66
J0218.0-0554	02 18 37 77	1.05	-05 42 00 99	1.77	S	5.3 ± 1.2 61+06	9.3 ± 1.2 61 ± 0.6	<53	<0.2	1737 ± 0.0	<-0.00
J0218.6-0545	02 18 37.80	1.06	-05 45 48.03	1.77	Š	5.4 ± 0.7	5.4 ± 0.7	<4.4	<1.5	179.8 ± 1.9	<-0.40
J0218.6-0245	02 18 37.96	1.11	-02 45 17.67	1.88	S	8.6 ± 1.4	8.6 ± 1.4	6.5 ± 5.2	<4.2	19.8 ± 7.0	-0.38
J0218.6-0347	02 18 38.71	1.08	-03 47 06.77	1.77	S	6.4 ± 0.9	6.4 ± 0.9	<4.2			<-0.52
J0218.7-0441*	02 18 39.37	1.06	-04 41 50.62	1.75	М	282.4 ± 24.0	236.7 ± 23.7	9.5 ± 0.3	<1.1	112.7 ± 0.4	-1.15
	02 18 39.88	1.06	-04 41 53.49	1.75	C		30.4 ± 3.1	<2.7	<1.2	20.1 ± 0.9	
10210 7 0222	02 18 40.17	1.06	-04 41 56.22	1.75	C	20.1 . 2.4	15.3 ± 1.5	<2.6	<0.0	129.1 ± 0.0	0.00
J0218.7-0322	02 18 40.24	1.09	-03 23 09.63	2.15	M	30.1 ± 3.4	18.5 ± 3.0	16.0 ± 0.5	<4.3	$1//.4 \pm 3.4$	-0.09
	02 18 40.15	1.23	$-03\ 23\ 01.41$ $-03\ 23\ 13\ 77$	1.60	C		0.4 ± 1.2 5 2 \pm 1 1	< 7.5	< 3.5	102.8 ± 20.9 70.6 ± 0.3	
10218 8-0423	02 18 46 65	1.42	$-03\ 23\ 13.77$ $-04\ 23\ 41\ 87$	1.01	S	34 ± 08	3.2 ± 1.1 3.4 ± 0.8	< 9.2	<57	15.5 ± 15.4	<-0.10
J0218.8-0209	02 18 46.76	1.31	$-02\ 09\ 49.92$	1.84	Š	9.9 ± 1.9	9.9 ± 1.9	<8.7	<4.3	55.1 ± 7.2	-0.12
J0218.8-0414	02 18 46.95	1.09	-04 14 19.12	1.82	\tilde{M}	11.1 ± 1.3	6.3 ± 1.0	<6.2	<4.0	13.3 ± 9.2	-0.11
	02 18 47.51	1.30	-04 14 10.88	1.85	С		4.8 ± 0.9	7.4 ± 5.7	<6.1	119.3 ± 19.5	
J0218.8-0241	02 18 47.23	1.38	-02 41 29.23	1.88	S	6.2 ± 1.4	6.2 ± 1.4	<8.6	<7.2	99.1 ± 45.6	0.28
J0218.8-0458	02 18 50.48	1.06	-04 58 33.74	1.75	S	23.0 ± 2.4	23.0 ± 2.4	<2.4	<2.2	10.5 ± 10.7	-0.77
J0218.8-0211*	02 18 51.04	1.06	-02 11 13.10	1.75	M	696.9 ± 49.5	364.9 ± 36.6	3.5 ± 0.2	2.5 ± 0.3	0.1 ± 4.4	-0.72
10010 0 0500	02 18 50.73	1.06	-02 11 22.03	1.75	C	52.0 5.4	332.0 ± 33.3	5.4 ± 0.2	1.7 ± 0.4	177.8 ± 1.3	0.75
J0218.9-0509	02 18 51.29	1.06	-05 09 04.05	1.75	5	53.9 ± 5.4	53.9 ± 5.4	<1.6	<1.6	25.6 ± 12.0	-0.75
JU218.9-U310 J0218.0-0447	02 18 52.07	1.17	$-03\ 10\ 48.42$ $-01\ 47\ 29\ 14$	1.85	5 5	3.3 ± 1.1 21.5 ± 2.2	3.3 ± 1.1 21.5 ± 2.2	< 0.8	< 0.1	-1.0 ± 68.1 30.8 \pm 12.1	-0.33
10218.9-0447 10218 9-0257	02 18 55 30	1.00	-07 47 50.14 -02 57 40 20	1.75	S	21.5 ± 2.5 44.6 ± 4.8	21.5 ± 2.5 44.6 ± 4.8	46 ± 13	<2.2	30.6 ± 12.1 39.6 + 10.3	-0.20
J0218.9-0401	02 18 56 04	1.47	-04 01 28 28	1.83	S	10.5 ± 1.9	10.5 ± 1.9	11.4 ± 6.1	<5.1	68.3 ± 6.8	-0.77
J0219.0-0409	02 18 58.14	1.06	-04 09 24.85	1.75	ŝ	40.2 ± 4.1	40.2 ± 4.1	2.7 ± 0.9	<1.7	33.5 ± 3.8	-0.57

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Table A.1. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{int}	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
J0219.0-0225	02 18 58.82	1.06	-02 25 46.96	1.75	S	116.9 ± 11.8	116.9 ± 11.8	<1.5	<1.4	100.1 ± 31.0	-0.09
J0219.0-0402	02 18 59.79	1.19	-04 02 38.98	1.85	S	4.5 ± 0.9	4.5 ± 0.9	<7.6	<5.0	41.7 ± 15.8	<-0.28
J0219.0-0355 J0219.1-0305	02 19 00.60	1.06	-03 55 59.09	1.75	5	32.9 ± 3.4 67 ± 1.4	32.9 ± 3.4 67 ± 1.4	3.2 ± 0.9	<2.1	73.5 ± 8.2 72 ± 11.0	-0.58
J0219.1-0305	02 19 04.89	1.08	-04 35 32.15	1.76	S	9.6 ± 1.2	9.6 ± 1.2	<3.9	<3.0	42.6 ± 11.9	-0.72
J0219.1-0414	02 19 05.79	1.15	-04 14 18.76	1.89	Ŝ	4.1 ± 0.8	4.1 ± 0.8	<7.6	<5.6	179.1 ± 22.5	-0.34
J0219.1-0459	02 19 06.64	1.11	-04 59 04.13	1.81	S	4.0 ± 0.7	4.0 ± 0.7	<5.8	<4.9	4.3 ± 41.7	-0.07
J0219.1-0252*	02 19 07.45	1.06	-02 52 53.00	1.75	М	638.1 ± 59.5	592.6 ± 59.3	2.9 ± 0.2	1.1 ± 0.4	177.2 ± 2.5	-0.63
	02 19 07.06	1.07	-02 53 01.64	1.78	С		25.6 ± 3.3	<4.9	<3.1	164.5 ± 6.6	
10210 1 0516	02 19 07.16	1.08	-02 52 58.58	1.76	C	52.00	19.9 ± 2.6	<4.4	<2.4	133.8 ± 4.8	. 0.20
J0219.1-0310 J0219.1-0455	02 19 08.30	1.09	$-03\ 10\ 37.20$ $-04\ 55\ 38\ 56$	1.65	S	3.5 ± 0.9 3.5 ± 0.8	3.5 ± 0.9 3.5 ± 0.8	<0.3	< 5.8	12.0 ± 0.0 23.5 + 24.0	<-0.39
J0219.1-0455	02 19 08.45	1.15	-035803.30	1.75	M	118.2 + 8.7	78.9 ± 8.0	61+0.5	3.5 ± 0.5	130.6 + 3.6	-0.63
0021911 0007	02 19 06.75	1.08	-035743.36	1.76	C	11012 - 017	27.1 ± 3.1	5.2 ± 1.5	4.5 ± 1.5	91.2 ± 46.1	0100
	02 19 08.18	1.16	-03 57 55.63	1.78	С		6.6 ± 1.1	<6.0	<4.8	73.4 ± 24.4	
	02 19 08.24	1.24	-03 57 59.87	1.86	С		5.5 ± 0.9	<8.6	<3.3	45.8 ± 3.7	
J0219.1-0423	02 19 09.01	1.07	-04 23 22.31	1.76	M	10.0 ± 1.1	6.1 ± 0.8	<3.7	<3.2	153.5 ± 24.5	-0.40
10210 2 0552	02 19 08.85	1.17	-04 23 23.98	1.79	C	50 . 12	4.0 ± 0.7	<6.1	<4.9	103.5 ± 31.4	. 0.46
J0219.2-0552 J0219.2-0220	02 19 09.26	1.22	$-05\ 52\ 43.51$ $-02\ 20\ 12\ 94$	1.89	S	5.9 ± 1.3 14.8 ± 2.0	3.9 ± 1.3 14.8 ± 2.0	<8.0	< 0.1	31.9 ± 31.3 11.0 ± 21.8	<-0.46
J0219.2-0220 J0219.2-0344*	02 19 10.29	1.08	$-02\ 20\ 12.94$ $-03\ 44\ 31.99$	1.76	M	14.3 ± 2.0 89.7 + 9.0	14.8 ± 2.0 85.1 + 9.0	13.0 + 1.2	< 3.8 7 8 + 0 8	11.0 ± 21.8 113.3 + 3.4	-0.63
0021712 0011	02 19 10.72	1.18	-03 44 40.92	1.86	C	0,11, 2,110	4.6 ± 1.0	<7.0	<6.2	-1.0 ± 67.2	0100
J0219.2-0248	02 19 12.64	1.24	-02 48 34.13	1.78	S	14.2 ± 2.5	14.2 ± 2.5	<7.1	<4.6	91.9 ± 12.3	-1.20
J0219.3-0438	02 19 16.42	1.08	-04 38 35.86	1.76	S	5.4 ± 0.7	5.4 ± 0.7	<3.7	<3.3	40.0 ± 35.1	-0.67
J0219.3-0552*	02 19 18.24	1.24	-05 52 40.08	1.87	Μ	118.9 ± 10.6	67.1 ± 9.4	16.7 ± 4.2	8.9 ± 2.5	44.4 ± 7.4	-0.69
	02 19 17.83	1.21	-05 52 52.05	1.77	C		27.3 ± 3.9	9.3 ± 3.4	<4.3	77.0 ± 7.4	
10210 2 0244*	02 19 18.79	1.10	-05 52 36.99	1.//	C M	205.2 ± 11.0	24.6 ± 3.2 71.2 + 7.0	5.1 ± 2.7	<4.1 5.2 ± 1.2	44.3 ± 20.7	0.82
J0219.3-0244	02 19 20.12	1.06	-024422.73 -02435300	1.70	C M	203.3 ± 11.9	71.2 ± 7.9 46.2 ± 4.9	0.2 ± 1.3	5.2 ± 1.3	30.0 ± 0.4 167.0 + 22.9	-0.82
	02 19 19.19	1.00	-024903.00 -024402.05	1.75	C		44.4 ± 4.9	4.2 ± 1.5	<2.8	107.0 ± 22.9 115.8 ± 10.6	
	02 19 21.22	1.22	-02 44 05.93	1.77	C		43.7 ± 5.6	13.2 ± 3.3	3.9 ± 2.3	101.8 ± 4.2	
J0219.4-0238	02 19 21.15	1.14	-02 38 55.37	2.12	S	6.3 ± 1.4	6.3 ± 1.4	<10.4	<5.3	6.8 ± 9.3	<-0.51
J0219.4-0307	02 19 23.37	1.09	-03 07 21.40	1.77	S	14.5 ± 1.9	14.5 ± 1.9	3.7 ± 3.1	<3.9	142.8 ± 19.8	-0.56
J0219.4-0340	02 19 23.39	1.22	-03 40 41.78	1.81	S	4.7 ± 0.9	4.7 ± 0.9	<7.2	<5.1	60.4 ± 16.8	<-0.31
J0219.4-0300	02 19 23.70	1.51	-03 00 10.98	2.22	S	14.0 ± 3.1	14.0 ± 3.1	14.0 ± 9.1	< 5.9	143.4 ± 7.1	<-1.06
J0219.4-0348	02 19 25.05	1.12	-03 48 00.72	1.82	M	11.3 ± 2.0 11.7 ± 1.8	11.3 ± 2.0 11.7 ± 1.8	< 0.0 11 4 + 4 7	<4.1	147.3 ± 11.3 140.0 ± 5.3	-0.41
J0219.4-0404	02 19 26.54	1.18	$-03\ 13\ 50.25$	1.94	S	4.8 ± 1.0	4.8 ± 1.0	<8.4	<6.1	166.5 ± 23.8	<-0.32
J0219.4-0302	02 19 26.82	1.22	-03 02 03.68	1.90	ŝ	5.2 ± 1.1	5.2 ± 1.1	<8.5	<5.0	142.9 ± 13.0	<-0.38
J0219.5-0229	02 19 27.51	1.07	-02 29 57.99	1.76	S	21.6 ± 2.5	21.6 ± 2.5	<3.4	<3.2	0.4 ± 61.9	-0.75
J0219.5-0403	02 19 27.53	1.12	-04 03 44.31	1.77	С	7.4 ± 1.0	3.9 ± 0.7	<5.2	<4.0	80.1 ± 23.7	
10010 5 0520*	02 19 27.55	1.32	-04 03 47.56	1.81	C	1410.0 + 101.4	3.5 ± 0.8	<8.2	<5.3	68.2 ± 16.4	0.04
J0219.5-0539*	02 19 28.29	1.06	-05 39 49.45	1.75	M	1412.8 ± 131.4	1310.4 ± 131.1	2.9 ± 0.1	1.8 ± 0.1	125.1 ± 2.0	-0.84
	02 19 23.33	1.00	-053913.98 -05395716	1.75	C		70.7 ± 8.1 25.7 ± 3.4	2.3 ± 1.0	<2.4	20.1 ± 10.3 178.7 ± 3.6	
J0219.5-0251*	02 19 29.55	1.06	-025111.62	1.75	M	459.8 ± 30.9	245.4 ± 24.7	7.0 ± 0.3	3.3 ± 0.3	102.6 ± 1.6	-0.96
0021710 0201	02 19 30.86	1.06	-02 51 15.18	1.75	C	10010 2 0010	180.9 ± 18.3	6.4 ± 0.4	3.2 ± 0.5	90.8 ± 2.3	0170
	02 19 30.26	1.11	-02 51 14.09	1.81	С		21.1 ± 3.0	5.8 ± 3.9	<3.8	32.5 ± 7.0	
	02 19 30.12	1.06	-02 51 10.88	1.77	С		12.4 ± 1.6	<4.1	<2.5	7.8 ± 6.9	
J0219.5-0342	02 19 32.73	1.09	-03 42 57.39	1.78	S	7.4 ± 1.0	7.4 ± 1.0	<4.8	<3.8	29.7 ± 16.3	<-0.61
J0219.6-0305	02 19 34.47	1.33	-03 05 41.55	1.99	S	4.9 ± 1.1	4.9 ± 1.1	<10.3	<5.0	141.1 ± 8.0	<-0.34
J0219.0-0414 J0219.6-0418	02 19 34.89	1.50	-04 14 30.70 -04 18 42 92	2.00	S	3.4 ± 0.7 28.8 + 3.0	3.4 ± 0.7 28.8 + 3.0	<10.7	<4.1	41.0 ± 4.0 167.8 ± 51.2	<-0.08
J0219.6-0306	02 19 36.96	1.10	$-03\ 06\ 50.28$	1.80	s	7.7 ± 1.2	7.7 ± 1.2	<5.7	<4.5	18.4 ± 20.6	-0.75
J0219.6-0301	02 19 37.74	1.07	-03 01 48.55	1.76	M	71.9 ± 5.3	33.1 ± 3.7	6.8 ± 1.5	<2.9	150.7 ± 5.5	-0.90
	02 19 38.84	1.08	-03 02 06.45	1.76	С		32.8 ± 3.7	7.1 ± 1.5	<3.0	136.1 ± 6.0	
	02 19 38.36	1.22	-03 01 59.90	1.84	С		6.1 ± 1.2	<7.3	<5.8	52.4 ± 32.4	
J0219.6-0349	02 19 37.94	1.12	-03 49 18.18	1.79	S	6.6 ± 1.0	6.6 ± 1.0	<5.8	<4.0	41.5 ± 9.9	<-0.54
J0219.7-0511	02 19 39.07	1.11	-05 11 36.23	1.86	S	4.2 ± 0.8	4.2 ± 0.8	.3</td <td><4.1</td> <td>21.3 ± 10.4</td> <td><-0.23</td>	<4.1	21.3 ± 10.4	<-0.23
J0219.7-0341 J0219.7-0400	02 19 41.88	1.24	-034135.77 -04003710	1.95	5 M	4.1 ± 0.9 150 7 ± 12 5*	4.1 ± 0.9	< 8.8	< 3.8	145.5 ± 10.4 170.0 ± 4.3	0.07
J0219.7-0400	02 19 42.78	2 15	$-04\ 00\ 37.10$ $-04\ 00\ 25\ 66$	2 27	C	150.7 ± 12.5	44.0 ± 0.0 35.1 + 6.1	29.0 ± 9.93	< 11.8	170.9 ± 4.3 60 7 + 11 3	-1.10
	02 19 42.02	1.70	$-04\ 00\ 46.00$	2.13	Č		20.7 ± 4.0	17.8 ± 7.09	< 13.7	122.6 ± 32.4	
	02 19 39.16	2.16	-04 00 19.82	2.39	С		10.3 ± 3.2	16.4 ± 10.92	<5.3	123.7 ± 26.6	
	02 19 41.21	1.89	-04 00 4.73	2.25	С		7.8 ± 2.5	< 20.4	< 14.0	71.6 ± 84.1	
	02 19 40.36	2.04	-04 00 13.37	3.35	C		7.5 ± 3.0	< 34.1	< 12.4	19.8 ± 18.6	
	02 19 39.37	1.42	-03 59 48.97	2.07	C		6.4 ± 1.9	< 15.6	<3.2	3.9 ± 53.7	
	02 19 39.57	2.03	$-04\ 00\ 2.66$	2.18	C		0.1 ± 2.2	< 21.2	.5</td <td>100.2 ± 38.4</td> <td></td>	100.2 ± 38.4	
	02 19 30.11	1.30 5.69	-04 00 13.90 -03 59 51 74	5.58 5.47	C		4.0 ± 2.0 4.5 ± 2.8	< 53.0 < 68.6	 < 10.2	13.9 ± 9.9 473 + 77	
J0219.7-0604	02 19 42 77	1.08	-06 04 25 85	1.81	м	18.3 ± 1.6	7.7 ± 1.3	< 6.0	<3.9	47.3 ± 7.7 6.3 ± 11.7	<-1.24
	02 19 41.83	1.07	-06 04 35.84	1.79	С		5.4 ± 0.7	<5.4	<2.6	13.7 ± 3.9	•
	02 19 42.16	1.08	-06 04 23.61	1.79	С		5.1 ± 0.7	<5.1	<3.3	164.6 ± 8.9	
J0219.7-0326	02 19 43.03	1.08	-03 26 27.36	1.76	S	17.0 ± 1.9	17.0 ± 1.9	3.8 ± 1.8	<3.1	69.6 ± 13.3	-0.61

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Table A.1. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	$S_{\rm int}$	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec	•••	mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
J0219.7-0516	02 19 43.54	1.07	-05 16 24.39	1.76	М	27.7 ± 2.4	17.4 ± 2.0	4.1 ± 2.0	<3.0	157.1 ± 7.8	-0.85
	02 19 43.37	1.08	-05 16 20.35	1.76	С		10.4 ± 1.3	<4.3	<2.7	40.8 ± 5.3	
J0219.7-0332	02 19 44.43	1.09	-03 32 16.19	1.76	S	9.6 ± 1.2	9.6 ± 1.2	<4.3	<3.5	47.9 ± 14.7	-0.49
J0219.7-0448	02 19 44.65	1.28	-04 48 46.62	1.77	M	16.4 ± 2.0	12.4 ± 1.8	10.6 ± 4.1	<4.3	96.1 ± 5.6	-0.72
	02 19 44.93	1.15	-04 48 44.54	1.80	С		4.0 ± 0.7	<6.3	<4.6	47.6 ± 19.8	
J0219.8-0453	02 19 45.33	1.09	-04 53 34.57	1.77	М	25.4 ± 2.7	14.1 ± 1.7	5.3 ± 2.2	<3.8	52.7 ± 16.3	-0.51
	02 19 45.82	1.23	-04 53 42.49	2.17	C		11.3 ± 2.1	14.8 ± 7.2	<5.5	20.9 ± 6.0	0.11
J0219.8-0456	02 19 45.73	1.26	-04 56 20.34	1.82	S	3.5 ± 0.7	3.5 ± 0.7	<7.8	<5.2	59.6 ± 17.0	<-0.11
J0219.8-0549	02 19 48.80	1.13	-05 49 23.99	2.04	S	8.2 ± 1.5	8.2 ± 1.5	<9.9	<3.2	160.4 ± 3.2	<-0.69
J0219.8-0437	02 19 50.66	1.12	-04 37 20.27	1.78	S	3.3 ± 0.6	3.3 ± 0.6	<5.4	<4.2	124.6 ± 25.9	-0.30
J0219.9-0158	02 19 51.57	1.10	-01 58 54.70	1.79	S	11.3 ± 1.9	11.3 ± 1.9	<5.4	<4.2	156.1 ± 23.6	-0.46
J0219.9-0444	02 19 51.73	1.12	-04 44 35.89	1.77	S	6.2 ± 0.9	6.2 ± 0.9	<5.4	<4.1	61.9 ± 15.1	<-0.50
J0219.9-0604	02 19 52.27	1.07	-06 04 25.41	1.81	M	12.0 ± 1.1	5.2 ± 0.7	<5.8	<2.4	171.9 ± 3.0	<-0.95
	02 19 52.62	1.20	-06 04 31.33	1.81	C		3.4 ± 0.6	.3</td <td><4.1</td> <td>128.0 ± 10.0</td> <td></td>	<4.1	128.0 ± 10.0	
10210 0 0522	02 19 53.92	1.11	-06 04 31.40	2.10	C	(1.10	3.4 ± 0.6	<10.4	<3.0	165.9 ± 2.6	. 0.40
J0219.9-0532	02 19 52.74	1.13	-05 32 50.37	1.89	5	6.1 ± 1.2	6.1 ± 1.2	./</td <td><4.9</td> <td>14.7 ± 13.6</td> <td><-0.49</td>	<4.9	14.7 ± 13.6	<-0.49
J0219.9-0518*	02 19 53.47	1.06	-05 18 37.08	1.75	M	74.2 ± 5.9	53.5 ± 5.4	1.8 ± 0.9	<1.6	33.4 ± 6.8	-0.89
10210 0 0211	02 19 52.73	1.07	-05 18 07.83	1.75	C	10.1 . 2.0	20.7 ± 2.2	< 3.0	<2.6	23.1 ± 10.7	. 1.02
J0219.9-0211	02 19 53.92	1.22	-02 11 29.32	1.79	S	18.1 ± 2.9	18.1 ± 2.9	1.2 ± 4.3	<4.9	70.7 ± 12.7	<-1.23
J0219.9-0549	02 19 54.55	1.10	-05 49 24.41	1.79	S M	11.5 ± 1.8	11.5 ± 1.8	< 3.3	<4.4	28.9 ± 27.0	-0.84
J0219.9-0527	02 19 55.55	1.08	-05 27 48.54	1.70	M	40.0 ± 5.5	15.9 ± 1.9	< 3.8	< 3.5	41.0 ± 29.7	0.08
	02 19 56.76	1.14	-05 28 25.12	1.84	C		14.4 ± 2.2	8.0 ± 3.0	4.5 ± 3.0	17.9 ± 20.8	
10220 0 0222	02 19 55.71	1.12	-05 27 51.08	1.79	C M	10.2 + 1.2	10.4 ± 1.5	< 5.1			0.91
J0220.0-0322	02 19 57.16	1.09	-03 22 09.99	1.//	M	10.2 ± 1.2	5.5 ± 0.9	<4.7	< 3.8	32.7 ± 29.4	-0.81
10000 0447*	02 19 56.96	1.08	-03 22 10.00	1.94	C M	10(0,100	4.9 ± 0.8	<8.3	<3.1	9.7 ± 3.9	0.70
J0220.0-044/*	02 19 57.25	1.06	-04 47 53.48	1.75	M	126.2 ± 12.2	122.0 ± 12.2	4.0 ± 0.2	<1.0	32.7 ± 1.2	-0.79
10220 0 0522	02 19 50.72	1.07	-04 47 43.52	1.85	C M	0.9 . 1.2	4.2 ± 0.7	<0.7	<2.8	8.2 ± 4.5	0.69
J0220.0-0525	02 19 57.29	1.20	-05 23 50.48	1.85	M	9.8 ± 1.2	5.4 ± 0.9	< /.8	< 3.2	40.3 ± 4.4	-0.68
10220 0 0240	02 19 57.20	1.10	-05 25 48.12	1./8	C	28.08	4.4 ± 0.8	<4.8	<4.4	$-1.0 \pm 8/.5$	< 0.17
J0220.0-0549	02 19 39.75	1.20	-05 49 40.55	1.04	S M	5.0 ± 0.0	5.0 ± 0.0	< 0.5	< 3.1	33.2 ± 13.4	<-0.17
J0220.0-0322	02 20 01.00	1.08	-05 22 18.38	1.70	C NI	19.2 ± 1.0	12.4 ± 1.4	< 3.0	<2.7	37.2 ± 7.1	-0.13
10220 1-0340	02 20 03.23	1.08	$-03\ 22\ 23.98$ $-03\ 48\ 55\ 14$	1.01	M	17.0 ± 1.8	0.0 ± 1.0 13.5 ± 1.7	< 0.1	<3.5	10.1 ± 3.0	0.08
J0220.1-0349	02 20 08.31	1.11	-03 48 33.14	1.70	C NI	17.0 ± 1.0	13.3 ± 1.7	7.7 ± 2.7	< 3.1	40.3 ± 3.0	0.08
10220 1-0545	02 20 07.90	1.55	-05 45 58 88	1.00	M	121 + 38	3.4 ± 0.7 23.4 ± 3.1	(9.4)	< 3.4	34.1 ± 4.3	-0.76
J0220.1-0343	02 20 08.73	1.14	-054553.88	1.60	C M	42.4 ± 3.0	23.4 ± 3.1 10.0 ± 2.2	9.3 ± 3.4	<3.0	40.3 ± 2.9	-0.70
10220 2-0404	02 20 09.01	1.07	-03 + 3 + 3 + 3 + 3 + 3 + 3 + 3 + 3 + 3 +	1.70	s	5.0 ± 0.8	19.0 ± 2.2 5.0 ± 0.8	< 6.8	~5.0	35.7 ± 15.6	< -0.34
10220.2-0404	02 20 10.37	1.15	-04 04 22.51 -03 05 34 51	1.05	M	15.0 ± 0.0	10.0 ± 0.0	< 3.0	<2.0	102.6 ± 9.6	<-0.54
J 0220.2-0505	02 20 11.49	1.00	$-03\ 05\ 31\ 60$	1.75	C	15.0 ± 1.4	50 ± 0.7	<1.8	<2.5	102.0 ± 5.0 103.0 ± 5.3	<-1.10
10220 2-0421	02 20 11.44	1.11	$-03\ 03\ 31.00$ $-04\ 21\ 49\ 16$	1.75	S	11.9 ± 1.3	11.9 ± 1.3	<3.2	<2.4	42.4 ± 7.5	-0.50
10220.2 0421	02 20 13.10	1.07	$-04\ 41\ 15\ 57$	1.70	S	36 ± 0.7	36 ± 0.7	<7.3	<4.6	49 ± 125	< -0.12
10220.2 0441	02 20 15.00	1.10	-03 46 06 17	1.80	S	5.0 ± 0.7 54 + 08	5.0 ± 0.7 5.4 ± 0.8	<56	<4.0	177.6 + 13.6	-0.61
I0220.3 0540	02 20 10.92	1.09	-05 18 51 82	1.00	S	68 ± 0.0	68 ± 0.0	<43	<32	40.1 ± 11.8	<-0.56
10220.3-0324	02 20 18 33	1.00	-03242361	1 79	S	72 ± 11	72 ± 11	<61	<43	135.1 ± 13.1	<-0.60
10220.3-0557	02 20 18 80	1 19	-05 57 31 70	1.88	S	7.2 ± 1.1 7.5 ± 1.3	7.2 ± 1.1 7.5 ± 1.3	< 8.3	<3.6	143.1 ± 5.1	-0.52
10220.3-0336	02 20 18 96	1.30	-03 36 32 30	1.00	S	35 ± 0.7	35 ± 0.7	<97	<37	43.1 ± 4.8	<-0.11
10220.3-0237	02 20 19 67	1.10	-02 37 57 24	1.72	S	112 ± 16	11.2 ± 1.6	<46	<3.8	54.6 ± 20.6	-0.16
10220.4-0448	02 20 24 84	1.10	-04 48 16 32	1.84	S	32 ± 0.7	32 ± 0.7	<6.5	10.0	51.0 ± 20.0	<-0.04
10220.5-0348	02 20 27 18	1.22	-03484312	2.01	Š	3.6 ± 0.8	3.2 ± 0.7 3.6 ± 0.8	< 9.8	< 5.0	152.2 + 9.1	<-0.12
J0220.5-0330	02 20 27.41	1.12	-03 30 49.06	1.78	ŝ	6.4 ± 0.9	6.4 ± 0.9	<5.4	<3.9	54.8 ± 12.6	0.28
J0220.5-0442	02 20 27.83	1.08	-04 42 19.12	1.76	ŝ	6.9 ± 0.9	6.9 ± 0.9	<3.9	<3.5	23.9 ± 26.8	<-0.57
J0220.5-0422	02 20 27.84	1.12	-04 22 51.92	1.78	ŝ	5.2 ± 0.8	5.2 ± 0.8	<5.2	<4.7	53.1 ± 50.4	<-0.37
J0220.5-0547	02 20 28.85	1.13	-05 47 36.74	1.78	S	6.3 ± 1.1	6.3 ± 1.1	<5.5	<4.8	117.0 ± 45.6	-0.40
J0220.5-0603	02 20 29.66	1.08	-06 03 10.15	1.78	М	18.5 ± 1.9	9.9 ± 1.4	< 5.0	<3.3	17.8 ± 9.7	-0.87
	02 20 29.64	1.15	-06 03 13.46	1.78	С		8.6 ± 1.3	< 6.3	<3.0	54.0 ± 4.8	
J0220.5-0251	02 20 30.81	1.08	-02 51 05.83	1.77	S	16.8 ± 2.0	16.8 ± 2.0	4.0 ± 2.5	<3.4	157.3 ± 12.0	-0.49
J0220.5-0450	02 20 31.97	1.09	-04 50 03.56	1.78	S	5.5 ± 0.8	5.5 ± 0.8	<5.3	<3.1	140.7 ± 6.1	<-0.42
J0220.6-0414	02 20 33.06	1.12	-04 14 16.58	1.80	S	3.5 ± 0.6	3.5 ± 0.6	<6.1	<3.5	40.5 ± 9.6	<-0.11
J0220.6-0257	02 20 33.26	1.18	-02 57 43.33	1.86	S	5.1 ± 1.1	5.1 ± 1.1	<7.5	<5.1	35.4 ± 18.2	<-0.37
J0220.6-0517	02 20 34.47	1.38	-05 17 47.43	1.87	S	4.6 ± 0.8	4.6 ± 0.8	<9.7	<3.7	54.5 ± 4.2	<-0.29
J0220.6-0410	02 20 34.71	1.21	-04 10 59.57	1.87	S	4.1 ± 0.8	4.1 ± 0.8	<7.1			<-0.21
J0220.6-0409	02 20 34.81	1.15	-04 09 54.54	1.82	S	3.9 ± 0.7	3.9 ± 0.7	<6.7	<4.7	142.0 ± 17.9	<-0.17
J0220.6-0513	02 20 35.34	1.06	-05 14 00.39	1.75	S	38.1 ± 3.9	38.1 ± 3.9	<1.9	<1.6	30.6 ± 4.4	-0.92
J0220.6-0342	02 20 35.35	1.27	-03 42 45.56	1.81	S	4.6 ± 0.9	4.6 ± 0.9	<7.6	<5.4	68.6 ± 18.3	<-0.29
J0220.6-0240	02 20 35.86	1.06	-02 40 25.41	1.75	S	48.5 ± 5.0	48.5 ± 5.0	<2.3	<2.3	48.4 ± 30.6	-0.64
J0220.6-0408	02 20 36.13	1.21	-04 08 09.39	1.81	Μ	6.9 ± 0.9	3.7 ± 0.7	<7.5	<4.0	54.9 ± 8.2	<-0.57
	02 20 36.03	1.12	-04 08 06.05	1.83	С		3.2 ± 0.6	<6.7	<4.3	27.7 ± 14.6	
J0220.6-0543	02 20 36.26	1.06	-05 43 29.86	1.75	Μ	39.8 ± 3.0	20.6 ± 2.2	<2.8	<2.5	6.5 ± 15.3	-0.82
	02 20 37.22	1.08	-05 43 30.61	1.76	С		13.7 ± 1.7	<3.8	<3.4	39.2 ± 22.5	
	02 20 36.52	1.11	-05 43 28.08	1.87	С		5.5 ± 1.1	<7.2	<4.6	11.8 ± 13.9	
J0220.6-0312	02 20 36.70	1.07	-03 12 40.97	1.75	S	20.3 ± 2.2	20.3 ± 2.2	<3.0	<2.6	30.3 ± 10.7	-0.75
J0220.6-0437	02 20 38.95	1.08	-04 37 27.20	1.76	M	24.4 ± 2.2	15.2 ± 1.7	5.3 ± 1.7	<3.3	144.2 ± 13.3	-0.63
	02 20 38.62	1.12	-04 37 19.01	1.78	С		9.3 ± 1.3	5.3 ± 3.1	<4.4	53.9 ± 19.2	
J0220.7-0222	02 20 42.46	1.17	-02 22 02.71	1.78	S	13.8 ± 2.0	13.8 ± 2.0	5.5 ± 4.2	<3.9	65.2 ± 7.8	-0.48

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Table A.1. continued.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Name	RA	σ_{α}	Dec	σ_{δ}	Туре	S _{int}	S _{comp}	Major axis	Minor axis	Position	Spectral
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		J2000	arcsec	J2000	arcsec		mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
$ \begin{array}{c} 2020 - 0.518 \\ 2020 - 0.518 \\ 2020 - 0.518 \\ 2020 - 0.518 \\ 2020 - 0.518 \\ 2020 - 0.518 \\ 2020 - 0.518 \\ 2020 - 0.518 \\ 1020 - 0.518 $	J0220.7-0339	02 20 44.17	1.10	-03 39 48.03	1.83	S	11.2 ± 1.7	11.2 ± 1.7	6.2 ± 4.0	<4.2	165.7 ± 9.1	-0.63
$ \begin{array}{llllllllllllllllllllllllllllllllllll$	J0220.7-0518	02 20 44.18	1.07	-05 18 06.61	1.80	S	6.7 ± 0.9	6.7 ± 0.9	<5.7	<2.9	11.5 ± 4.3	<-0.55
$ \begin{array}{c} \mu_{2230} \ \mu_{3230} \ \mu_{2230} \ \mu_{3230} \ \mu_{3330} \ \mu_{3300} \ \mu_{$	J0220.8-0321	02 20 45.64	1.13	-03 21 30.90	1.77	S	9.5 ± 1.4	9.5 ± 1.4	<5.3	<4.4	94.6 ± 23.0	-0.42
$\begin{array}{c} 100000-0.031, 0.25 + 0.25 + 0.06 & -0.03 + 0.01 & 0.05 & s & 214.5 \pm 0.2 & 214.5 \pm 0.2 & -0.12 & -0.13 & -0.02 & -0.03 & -0.05 $	J0220.8-0335	02 20 45.67	1.21	-03 35 51.86	1.85	S	4.9 ± 1.0	4.9 ± 1.0	.6</td <td>< 5.5</td> <td>43.8 ± 21.9</td> <td><-0.33</td>	< 5.5	43.8 ± 21.9	<-0.33
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JU220.8-0237 I0220.8-0333*	02 20 48.18	1.09	-023720.42 -03331700	1.80	3 5	12.2 ± 1.9 224.5 \pm 22.5	12.2 ± 1.9 224.5 \pm 22.5	< 3.0 75 ± 0.2	<4.0	$1/8.1 \pm 13.7$ 73.7 ± 0.0	-0.97
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10220.8-0553	02 20 49.32	1.00	-05 53 17.90	1.75	S	224.3 ± 22.3 19.0 + 2.2	224.3 ± 22.3 19.0 + 2.2	7.5 ± 0.2	5.2 ± 0.2	73.7 ± 0.9 22.7 ± 12.2	-0.55
$\begin{array}{c} 102208-0510 & 02.2 \\ 0.$	10220.8-0535 10220 8-0537	02 20 49.02	1.07	$-05\ 37\ 15\ 14$	1.76	S	19.0 ± 2.2 147 + 16	19.0 ± 2.2 14.7 ± 1.6	<3.7	<2.5	22.7 ± 12.2 31.5 ± 7.5	-1.03
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0220.8-0510	02 20 50.50	1.15	$-05\ 10\ 19\ 70$	1.88	M	12.0 ± 1.0	8.7 ± 1.0	88+41	< 5.7	178.5 ± 18.3	-0.37
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0022010 0010	02 20 50.98	1.13	-05 09 59.93	1.91	C	12:0 2 1:0	3.3 ± 0.7	<8.0	<4.8	14.7 ± 13.1	0107
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	J0220.8-0340	02 20 51.12	1.50	-03 40 55.53	1.80	М	65.6 ± 5.8	37.7 ± 4.9	22.4 ± 5.5	<3.3	70.5 ± 1.5	-1.14
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 20 50.22	1.08	-03 40 59.87	1.76	С		27.8 ± 3.1	5.1 ± 1.6	<2.9	61.8 ± 7.3	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0220.9-0512	02 20 51.69	1.07	-05 12 37.11	1.77	S	8.6 ± 1.1	8.6 ± 1.1	<4.5	<3.2	3.6 ± 8.0	0.01
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	J0220.9-0413	02 20 51.77	1.07	-04 13 45.79	1.79	М	8.9 ± 1.0	5.7 ± 0.7	<5.2	<2.2	166.0 ± 2.8	<-0.75
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 20 51.84	1.42	-04 13 58.13	1.79	С		3.2 ± 0.7	<9.0	<4.9	97.3 ± 10.9	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0220.9-0601*	02 20 51.96	1.07	-06 01 18.92	1.76	M	79.7 ± 7.7	70.4 ± 7.5	9.5 ± 1.2	3.6 ± 1.1	135.1 ± 3.1	-0.72
$ \begin{array}{c} 102209-9033 \\ 02209-9033 \\ 02209-9033 \\ 022095551 \\ 02209-9033 \\ 022095551 \\ 02209-9034 \\ 022095551 \\ 02209-9034 \\ 022095571 \\ 022095571 \\ 006 \\ 02305557 \\ 006 \\ 0230557 \\ 006 \\ 0230557 \\ 006 \\ 006 \\ 006 \\ 000 \\ 0230557 \\ 000 \\ 0230557 \\ 000 \\ 0230557 \\ 000 \\ 000 \\ 000 \\ 0230557 \\ 000 \\ 000 \\ 000 \\ 0230557 \\ 000 \\ 000 \\ 000 \\ 0230557 \\ 000 \\ 00$	10220 0 0252	02 20 51.42	1.15	-06 01 13.45	1.86	C	127.29	9.3 ± 1.5	./</td <td>< 3.6</td> <td>33.2 ± 5.0</td> <td>0.00</td>	< 3.6	33.2 ± 5.0	0.00
$ \begin{array}{c} 10220 - 0210 \\ 0220 - 0230 \\ 0220 - 0230 \\ 0220 - 0230 \\ 0220 - 0340 \\ 0221 - 0350 \\ 0221 - $	J0220.9-0252	02 20 52.04	1.48	-02 53 01.68	1.97	5	12.7 ± 2.8	12.7 ± 2.8	10.0 ± 7.8	< 0.3	129.9 ± 11.7	-0.96
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0220.9-0329 J0220.9-0329	02 20 53.20	1.09	$-03\ 29\ 08.03$ $-02\ 19\ 17\ 50$	1.70	S	0.3 ± 0.9 $1/3 \pm 2.9$	0.3 ± 0.9 $1/13 \pm 2.0$	<4.0	<4.0	23.4 ± 20.0 88.0 + 21.4	<-0.31
$ \begin{array}{c} 0.22 0 53.67 \\ 0.22 055.0 \\ 0.22 055.0 \\ 0.22 055.0 \\ 0.22 055.0 \\ 0.22 055.0 \\ 0.22 055.0 \\ 0.22 055.0 \\ 0.22 055.0 \\ 0.23 055.0 \\ 0.22 055.0 \\ 0.21 00.33 \\ 0.21 00.33 \\ 0.21 00.30 \\ 0.21 00.$	10220.9-0333	02 20 54.25	1.26	-03 33 31 72	1.00	M	438 ± 42	14.3 ± 2.9 387+40	<7.0	<5.5	00.7 ± 21.4	-0.38
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	30220.7 05555	02 20 55.67	1.24	$-03\ 33\ 50.24$	1.90	C	15.0 ± 1.2	5.1 ± 1.1	<8.3	<6.1	36.9 ± 24.9	0.50
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0220.9-0348*	02 20 55.77	1.06	-03 48 34.89	1.75	M	402.2 ± 35.1	348.6 ± 34.9	6.4 ± 0.1	2.9 ± 0.2	76.4 ± 0.7	-1.11
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 20 55.29	1.06	-03 48 36.97	1.76	С		27.6 ± 2.9	5.2 ± 1.8	<1.1	168.9 ± 0.5	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 20 55.10	1.06	-03 48 37.04	1.76	С		19.9 ± 2.2	<3.6	<2.1	1.0 ± 2.8	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 20 55.60	1.53	-03 48 47.00	1.76	С		6.1 ± 1.1	<9.8	<3.4	84.2 ± 3.4	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.0-0358	02 20 57.53	1.10	-03 58 48.60	1.77	М	24.5 ± 2.5	17.6 ± 2.2	6.6 ± 2.6	<3.2	47.4 ± 5.2	-1.10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		02 20 57.07	1.08	-03 58 53.47	1.78	С		6.9 ± 1.0	<4.9	<3.6	156.4 ± 15.2	
$ \begin{array}{c} 102210-053 & 02.21 00.54 & 1.16 & -0.05 030.7 & 1.82 & S & 5.4 \pm 1.0 & 5.4 \pm 1.0 & -0.64 & -0.65 & 10.2 \pm 1.70 & -0.18 \\ \hline 102210-020 & 0221 02.21 & 01.8 & -0.24 02.19 & 1.75 & C & -4.1 \pm 0.6 & -5.5 & -2.7 & 81.1 \pm 5.0 & -0.70 \\ \hline 102211-0204 & 0221 02.27 & 10.8 & -0.24 02.19 & 1.77 & S & 22.4 \pm 2.9 & 23.4 \pm 2.9 & 3.4 \pm 2.6 & & & -0.57 \\ \hline 102211-0235 & 0221 02.95 & 1.09 & -02 55 13.83 & 1.77 & S & 12.7 \pm 1.7 & 12.7 \pm 1.7 & -4.5 & -3.8 & 12.8.5 \pm 2.01 & -0.97 \\ \hline 102211-0246 & 0221 02.91 & 10.8 & -02 46 00.3 & 1.77 & M & 127 04.8.9 & 60.6 6.7 & 11.1 \pm 1.7 & 4.5 & +1.2 & 15.9 \pm 3.5 \\ \hline 102211-0216 & 10.7 & -0.24 61 96.3 & 1.81 & C & -3.18 \pm 3.9 & 10.4 \pm 2.6 & -3.4 & 115.7 \pm 2.3 \\ \hline 102211-0216 & 10.7 & -0.24 61 96.3 & 1.81 & C & -10.17 & 13.4 \pm 6.5 & -4.2 & 115.8 \pm 3.9 \\ \hline 102211-0216 & 10.6 & -0.25 53.70 & 1.75 & C & -8.8.5 \pm 9.0 & 4.3 \pm 0.5 & -4.2 & 11.85 \pm 3.5 \\ \hline 102213-0255 & 0221 16.40 & 1.06 & -02 55 37.0 & 1.75 & C & -8.8.5 \pm 9.0 & 4.3 \pm 0.5 & -2.4 & 18.5 \pm 3.5 & -0.61 \\ \hline 102213-0257 & 0221 17.51 & 1.07 & -05 56 01.42 & 1.76 & S & 24.1 \pm 2.6 & -3.2 & -2.5 & 2.9.7 \pm 7.6 & -0.80 \\ \hline 102213-0257 & 0221 17.81 & 1.6 & -0.48 0.77 & 1.78 & S & 5.7 \pm 1.7 & -5 & -2.4 & 38.6 \pm 1.73 & -0.51 \\ \hline 102213-0257 & 0221 17.81 & 1.6 & -0.48 0.77 & 1.78 & 5.57 \pm 4.7 & 15.7 \pm 4.7 & 12.2 3.1 & -0.6 & -0.25 \\ \hline 102213-0246 & 0221 17.81 & 1.07 & -0.65 53.44 & 2.0 & -6.5 & -3.2 & -2.5 & 2.9.7 \pm 7.6 & -0.80 \\ \hline 102213-0247 & 0221 17.85 & 1.20 & -0.0221 73.18 & 1.77 & S & 5.7 \pm 4.7 & 15.7 \pm 4.7 & 12.2 3.1 & -0.93 \\ \hline 102213-0246 & 0221 19.28 & 1.07 & -0.65 53.44 & 2.0 & -6.5 & -3.52 & -3.1 & 89.3 \pm 9.9 & -0.61 \\ \hline 102213-036 & 0221 19.28 & 1.07 & -0.55 10.24 & 1.76 & S & 15.8 \pm 1.8 & -5.4 & -0.76 \\ \hline 102214-0424 & 0221 19.28 & 1.07 & -0.55 10.24 & 1.76 & S & 15.8 \pm 1.8 & -5.1 & -0.23 \\ \hline 102214-0424 & 0221 19.38 & 1.77 & -0.55 10.6 & -1.5 10.5 5.2 & -2.0 & -0.61 \\ \hline 102213-036 & 021 19.38 & 1.07 & -0.5 5.42 & 1.6 & -0.5 & -0.24 & -0.55 \\ \hline 102214-0424 & 0221 23.59 $	J0221.0-0413	02 20 58.71	1.37	-04 13 22.71	1.86	S	4.3 ± 0.8	4.3 ± 0.8	<9.4	<4.4	56.3 ± 6.2	<-0.25
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.0-0535	02 21 00.34	1.16	-05 35 30.77	1.82	S	5.4 ± 1.0	5.4 ± 1.0	< 6.4	< 5.6	150.2 ± 47.0	-0.18
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.0-0500	02 21 01.95	1.11	-05 00 48.10	1.75	M C	12.1 ± 1.2	8.1 ± 1.0	<4.8	<2.7	95.5 ± 4.1	-0.70
$ \begin{array}{c} 102211 - 0223 & 0221 & 0225 & 109 & -023 & 1383 & 1.77 & S & 12.7 \pm 1.7 & 12.7 \pm 1.7 & 14.25 & -3.8 & 12.8 \pm 2.01 & -0.97 \\ 102211 - 0246 & 002 & 103.97 & 108 & -02 & 46 & 40.03 & 1.77 & M & 12.7 & \pm .8 & 60.6 \pm 6.7 & 11.1 \pm 1.7 & 4.5 \pm 1.2 & 156.9 \pm 3.5 & -0.74 \\ 0.2 & 21 & 03.61 & 110 & -02 & 46 & 40.03 & 1.83 & C & 34.6 \pm 4.3 & 13.1 \pm 2.5 & <3.1 & 152.7 \pm 2.3 \\ 0.2 & 21 & 03.30 & 1.07 & -02 & 46 & 19.63 & 18.1 & C & 34.8 \pm 2.9 & <3.0 & 43.2 \pm 3.1 & -0.54 \\ 0.2 & 21 & 01.2 & 111 & 112 & -0.5 & 112 & 12.0 & 1.77 & M & 23.5 \pm 2.4 & 13.5 \pm 1.7 & 88 \pm 2.9 & <3.0 & 43.3 \pm 3.1 & -0.54 \\ 0.2 & 21 & 01.01 & 10.6 & -02 & 55 & 49.2 & 1.75 & M & 23.5 \pm 1.7 & 18.4 \pm 5.5 & <4.2 & 115.8 \pm 3.9 \\ 0.2 & 1.0 & -0.55 & 02 & 21 & 16.07 & 10.6 & -02 & 55 & 50.1 & 17.5 & K & 23.5 \pm 1.7 & 14.73 \pm 14.8 & 4.2 \pm 0.5 & 3.2 \pm 0.0 & 50.9 \pm 9.1 \\ 0.2 & 1.0 & -0.55 & 02 & 21 & 17.6 & 116 & -0.3 & 48 & 30.77 & 17.8 & S & 6.2 \pm 1.0 & 6.2 \pm 1.0 & 6.2 & 2.0 & 5.5 & -0.61 \\ 0.2 & 1.0 & -0.55 & 02 & 21 & 17.81 & 11.6 & -0.3 & 48 & 30.77 & 17.8 & S & 6.2 \pm 1.0 & 6.2 \pm 1.0 & 6.2 & 2.0 & 5.5 & 1.2 & -0.05 \\ 0.2 & 1.0 & -0.57 & 02 & 21 & 17.81 & 11.6 & -0.3 & 48 & 30.77 & 17.8 & S & 6.2 \pm 1.0 & 6.2 \pm 1.0 & 6.2 & 2.0 & 5.8 & 5.1 & -0.93 \\ 0.2 & 1.0 & -0.4 & 0.2 & 11.38 & 1.77 & S & 35.7 \pm 4.7 & 13.5 & 1.75 & 5 & 16.3 \pm 1.7 & 2.7 & 2.4 & 58.6 \pm 1.73 & -0.15 \\ 1022 & 1.3 & -0.4 & 0.2 & 11.93 & 11.0 & -0.4 & 40.80 & 1.76 & S & 15.8 \pm 1.8 & 15.8 \pm 1.8 & 3.5 \pm 1.9 & -2.9 & 51.2 \pm 10.5 & -0.21 \\ 1022 & 1.3 & -0.3 & 10.8 & -0.3 & 53.44 & 2.02 & M & 16.2 \pm 1.5 & 7.8 \pm 1.4 & 1.75 & 4.2 & 5.1 & 9.3 \pm 5.9 & -0.65 \\ 0.2 & 11 & 9.1 & 1.16 & -0.3 & 05.5 & 1.77 & C & 2.4 & 58.8 \pm 1.8 & 1.58 \pm 1.8 & 1.58 & 1.48 & 3.5 \pm 1.9 & -2.9 & 51.2 \pm 10.5 & -0.21 \\ 102 & 2.1 & -0.305 & 50.24 & 1.76 & K & 1.76 & K & 1.4 & 4.8 & 4.1 & 1.7 \pm 1.7 & 3.8 \pm 2.1 & -3.0 & 6.6 & 2.28 & 10.23 \pm 1.38 & 1.2 & -0.65 \\ 102 & 2.1 & -0.44 & 10.6 & 53.52 & 2.00 & K & 4.1 & 1.7 \pm 1.7 & 1.7 & 3.8 \pm 2.1 & -3.0 & 6.6 & -2.8 & 0$	10221 0-0240	$02\ 21\ 01.91$ $02\ 21\ 02\ 27$	1.14	$-03\ 00\ 43.20$ $-02\ 40\ 27\ 90$	1.75	c s	23.4 ± 2.0	4.1 ± 0.0 23.4 ± 2.0	< 3.3	<2.7	61.1 ± 3.0	-0.57
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	I0221.0-0240	02 21 02.27	1.00	-02 + 027.90 -02 53 13 83	1.77	S	12.7 ± 1.7	12.7 ± 1.7	5.4 ± 2.0 <4 5	< 3.8		-0.97
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.1-0246*	02 21 02.93	1.08	-024640.03	1.77	M	127.0 ± 8.9	60.6 ± 6.7	11.1 ± 1.7	4.5 ± 1.2	156.9 ± 3.5	-0.74
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 21 03.61	1.10	-02 46 20.73	1.83	С		34.6 ± 4.3	13.1 ± 3.2	<3.1	152.7 ± 2.3	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 21 03.30	1.07	-02 46 19.63	1.81	С		31.8 ± 3.9	10.4 ± 2.6	<3.4	177.7 ± 3.9	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.2-0511	02 21 10.94	1.11	-05 11 20.79	1.79	М	23.5 ± 2.4	13.5 ± 1.7	8.8 ± 2.9	<3.0	43.3 ± 3.1	-0.54
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 21 11.17	1.52	-05 11 21.26	1.84	С		10.0 ± 1.7	13.4 ± 6.5	<4.2	115.8 ± 3.9	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	J0221.3-0255*	02 21 16.40	1.06	-02 55 49.21	1.75	M	235.8 ± 17.3	147.3 ± 14.8	4.2 ± 0.3	2.5 ± 0.3	118.5 ± 3.5	-0.61
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10221 2 0555	02 21 16.07	1.06	-02 55 53.70	1.75	C	24.1 2.6	88.5 ± 9.0	4.3 ± 0.5	3.2 ± 0.5	65.9 ± 9.1	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.3-0555	02 21 17.51	1.07	-05 56 01.42	1.70	S	24.1 ± 2.6	24.1 ± 2.6	<3.2	<2.5	29.7 ± 7.6	-0.80
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.3-0348	02 21 17.81	1.10	-03 48 30.77	1.78	3 5	0.2 ± 1.0	0.2 ± 1.0	<0.2	< 3.8	01.0 ± 8.9 07.2 ± 5.1	-0.01
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	I0221.3-0227	02 21 17.85	1.20	$-02\ 27\ 13.18$ $-04\ 57\ 23\ 15$	1.77	S	163 ± 17	163 ± 17	22 ± 3.1	<2.4	58.6 ± 17.3	-0.95
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.3-0344	02 21 10.44	1.07	-03444080	1.76	S	15.8 ± 1.7	15.8 ± 1.7	35 ± 19	<2.9	51.2 ± 10.5	-0.21
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.3-0329	02 21 19.90	1.12	-032908.21	1.76	M	16.2 ± 1.5	8.8 ± 1.2	<5.1	<3.1	98.3 ± 5.9	-0.65
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 21 19.93	1.08	-03 29 05.13	1.75	С		7.4 ± 0.9	<3.6	<2.8	102.3 ± 13.8	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	J0221.3-0305*	02 21 21.16	1.16	-03 05 53.44	2.02	М	64.9 ± 6.5	35.2 ± 5.1	19.3 ± 5.2	6.9 ± 2.5	163.5 ± 4.5	-0.99
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 21 19.76	1.21	-03 05 50.65	1.79	С		29.8 ± 4.1	11.7 ± 3.2	7.1 ± 2.4	91.2 ± 10.6	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.4-0405	02 21 21.28	1.34	-04 05 35.32	2.00	S	4.9 ± 0.9	4.9 ± 0.9	<10.8	<2.9	139.9 ± 2.4	<-0.33
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.4-0424	02 21 23.94	1.13	-04 24 14.63	1.79	S	6.8 ± 1.1	6.8 ± 1.1	<5.4			<-0.56
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.4-0352	02 21 24.31	1.08	-03 52 40.04	1.76	S	14.7 ± 1.7	14.7 ± 1.7	3.8 ± 2.1	<3.0	60.8 ± 9.1	-0.55
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.4-0347	02 21 25.57	1.06	-03 47 20.93	1.75	S	47.2 ± 4.8	47.2 ± 4.8	2.7 ± 0.8	<1.8	43.2 ± 6.4	-0.70
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.4-0202	02 21 20.32	1.22	$-02\ 02\ 35.13$	1.81	M C	58.1 ± 4.8	10.8 ± 2.7 15.6 ± 2.2	0.5 ± 5.5	< 3.9	120.8 ± 3.0	-0.80
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		02 21 27.03	1.13	$-02\ 02\ 34.13$ $-02\ 02\ 35\ 02$	1.70	C		13.0 ± 2.3 13.7 ± 2.5	< 3.2	< 3.2	64.0 ± 0.4 57 1 ± 6 0	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		02 21 20.38	1.33	$-02\ 02\ 35.02$ $-02\ 02\ 37\ 00$	1.04	Ċ		12.0 ± 2.0	<67	<31	888 + 57	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.5-0516	02 21 27.26	1.08	-05 16 11.37	1.76	S	12.8 ± 1.5	12.8 ± 1.5	<3.7	<3.1	58.4 ± 15.8	-0.15
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	J0221.5-0504	02 21 27.43	1.09	-05 04 02.04	1.78	Ŝ	6.9 ± 1.0	6.9 ± 1.0	<4.7	<3.9	18.9 ± 19.7	<-0.57
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.5-0434	02 21 27.91	1.88	-04 34 11.41	1.78	S	17.3 ± 2.8	17.3 ± 2.8	21.6 ± 7.7	<4.6	86.1 ± 2.8	-0.55
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	J0221.5-0509	02 21 30.90	1.37	-05 09 29.44	1.88	S	4.1 ± 0.9	4.1 ± 0.9	<8.6	<7.0	113.0 ± 38.7	<-0.22
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.5-0556	02 21 31.33	1.06	-05 56 26.03	1.75	М	84.6 ± 6.3	49.3 ± 5.1	<2.2	<1.8	41.4 ± 5.6	-0.56
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		02 21 29.61	1.07	-05 56 23.83	1.75	С		35.3 ± 3.8	<2.8	<2.4	47.9 ± 10.4	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	J0221.5-0423	02 21 31.50	1.07	-04 23 47.52	1.75	S	22.8 ± 2.5	22.8 ± 2.5	<2.8	<2.6	62.6 ± 22.8	-0.59
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	J0221.5-0344	02 21 32.68	1.09	-03 44 02.40	1.77	S	7.5 ± 1.0	7.5 ± 1.0	<4.7	<3.5	47.9 ± 13.8	0.94
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	J0221.6-0409	02 21 33.27	1.11	-04 09 04.02	1.76	M	23.2 ± 2.3	15.8 ± 2.0	<4.9	<3.0	64.1 ± 5.4	-0.55
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10221 6 0226	02 21 33.34	1.10	-040900.42	1.//	C c	60+00	1.4 ± 1.2	<5.0	<2.9	34.7 ± 8.3	< 0.49
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.0-0230 I0221.6_0519	02 21 34.41	1.08	-02 30 10.00 -05 18 22 56	1.//	5 M	0.0 ± 0.9 24.7 ± 2.4	0.0 ± 0.9 16.8 ± 2.2	<4.4 10 3 ± 3 2	<4.U 23.2	-1.0 ± 33.9 30.8 \pm 3.2	<-0.48 _0.50
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	30221.0-0318	02 21 33.01	1.11	-05 16 22.30	1.02	м С	24.1 ± 2.4	10.0 ± 2.2 7 8 + 1 1	10.3 ± 3.2	< 3.2 < 1	30.0 ± 3.2 1 5 + 22 8	-0.59
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0221.7-0509	02 21 30.02	1.09	-05 09 43 50	1.77	S	9.2 ± 1.1	9.2 + 1.1	<4.0	< 3.5	12.8 + 19.3	-0.31
$J0221.7 - 0413 * 02 21 43.06 1.06 - 04 13 45.57 1.75 S 1269.7 \pm 127.0 1269.7 \pm 127.0 1.75 \pm 0.1 2.2 \pm 0.1 135.0 \pm 0.2 - 0.59$	J0221.7-0451*	02 21 42.06	1.06	-04 51 12.38	1.75	ŝ	198.3 ± 19.9	198.3 ± 19.9	10.6 ± 0.3	2.0 ± 0.3	166.3 ± 0.4	-0.88
	J0221.7-0413*	02 21 43.06	1.06	-04 13 45.57	1.75	S	1269.7 ± 127.0	1269.7 ± 127.0	7.5 ± 0.1	2.2 ± 0.1	135.0 ± 0.2	-0.59

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Table A.1. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Туре	$S_{\rm int}$	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec	• •	mJy	mJy	arcsec	arcsec	Angle	index α_{225}^{1400}
J0221.7-0249	02 21 43.30	1.06	-02 49 29.82	1.75	S	26.9 ± 2.8	26.9 ± 2.8	<2.6	<2.2	53.6 ± 7.5	-0.52
J0221.7-0404	02 21 43.73	1.17	-04 04 27.45	1.99	S	7.0 ± 1.5	7.0 ± 1.5	<9.0	<6.0	174.8 ± 17.7	<-0.58
J0221.7-0357	02 21 44.28	1.09	-03 57 50.62	1.76	M	28.3 ± 2.6	15.9 ± 2.0	3.8 ± 2.7	<3.7	59.1 ± 17.7	-0.80
	02 21 45.44	1.09	-03 57 41.75	1.77	С		12.4 ± 1.7	<4.6	<3.6	51.7 ± 13.1	
J0221.8-0329	02 21 45.60	1.07	-03 29 29.03	1.76	M	17.1 ± 1.5	9.1 ± 1.1	<3.4	<2.7	44.0 ± 12.9	-1.25
	02 21 45.63	1.12	-03 29 32.19	1.76	С		8.0 ± 1.1	<5.1	<3.0	72.4 ± 5.6	
J0221.8-0308	02 21 46.33	1.24	-03 08 35.06	1.88	S	3.6 ± 0.8	3.6 ± 0.8	<7.4			<-0.13
J0221.8-0456	02 21 46.85	1.09	-04 56 46.34	1.78	S	7.9 ± 1.1	7.9 ± 1.1	<4.6	<4.3	18.9 ± 55.5	-0.64
J0221.8-0326	02 21 47.76	1.08	-03 26 39.03	1.76	S	11.1 ± 1.4	11.1 ± 1.4	<3.9	<3.6	87.5 ± 47.5	-0.68
J0221.8-0257	02 21 48.00	1.18	-02 57 16.13	1.78	S	4.4 ± 0.8	4.4 ± 0.8	<6.4	<4.5	75.2 ± 17.5	<-0.26
J0221.9-0505	02 21 51.43	1.11	-05 05 38.19	1.77	S	7.9 ± 1.0	7.9 ± 1.0	4.5 ± 3.4	<3.3	59.4 ± 6.6	-0.40
J0221.9-0427	02 21 51.92	1.08	-04 27 28.81	1.86	S	6.0 ± 1.0	6.0 ± 1.0	<6.9	<4.0	0.5 ± 8.6	-0.54
J0221.9-0205	02 21 52.78	1.11	-02 05 04.11	1.77	M	72.6 ± 6.5	37.9 ± 4.8	7.0 ± 2.4	<3.6	54.5 ± 7.3	-0.68
	02 21 53.17	1.12	-02 05 09.38	1.76	С		34.7 ± 4.5	6.6 ± 2.5	<3.9	96.5 ± 10.4	
J0221.9-0318	02 21 56.49	1.21	-03 18 14.84	1.79	S	4.8 ± 0.9	4.8 ± 0.9	<6.7	<5.0	103.9 ± 20.9	-0.39
J0221.9-0407	02 21 56.49	1.10	-04 07 58.48	1.77	S	10.1 ± 1.4	10.1 ± 1.4	<4.8	<3.9	44.4 ± 16.0	-0.83
J0222.0-0443	02 21 59.78	1.12	-04 43 27.62	1.78	S	5.7 ± 0.9	5.7 ± 0.9	<5.1	<4.6	59.9 ± 49.1	<-0.44
J0222.0-0339	02 22 00.39	1.06	-03 39 35.94	1.75	S	50.0 ± 5.1	50.0 ± 5.1	4.4 ± 0.6	<1.9	66.0 ± 5.2	-0.62
J0222.0-0550	02 22 00.83	1.08	-05 51 00.19	1.79	S	8.7 ± 1.3	8.7 ± 1.3	<5.2	<3.7	1.4 ± 12.3	-0.42
J0222.0-0240*	02 22 01.29	1.06	-02 40 14.93	1.75	M	473.7 ± 27.5	240.8 ± 24.1	5.1 ± 0.2	2.1 ± 0.3	140.3 ± 1.3	-0.76
	02 21 59.98	1.06	-02 40 00.46	1.75	C		108.8 ± 11.0	7.0 ± 0.5	2.9 ± 0.6	118.3 ± 2.2	
	02 21 59.55	1.06	-02 39 55.42	1.75	C		54.2 ± 5.5	<2.0	<1.9	50.6 ± 51.2	
	02 22 00.87	1.19	-02 40 10.19	1.79	C		27.1 ± 3.2	11.5 ± 3.7	<1.8	54.4 ± 0.8	
	02 22 00.74	1.08	-02 40 07.82	1.76	C		17.8 ± 2.1	<4.0	<2.7	66.0 ± 5.7	
	02 22 00.97	1.07	-02 40 20.30	1.75	C		11.5 ± 1.4	<2.8	<2.4	41.7 ± 20.7	
	02 22 00.72	1.09	-02 40 19.33	1.89	C		7.9 ± 1.2	<7.6	<3.2	163.4 ± 3.9	
	02 21 59.17	1.27	-02 40 01.11	2.07	C		5.6 ± 1.3	<10.4	<6.1	153.0 ± 13.0	0.47
J0222.0-0337	02 22 02.88	1.11	-03 37 16.13	1.84	S	3.8 ± 0.7	3.8 ± 0.7	<6.9	<3.6	25.3 ± 8.3	<-0.16
J0222.1-0448	02 22 03.93	1.08	-04 48 35.93	1.77	S	5.7 ± 0.8	5.7 ± 0.8	<4.1	<3.5	14.5 ± 30.3	<-0.44
J0222.1-0338	02 22 04.80	1.06	-03 38 16.22	1.75	M	96.4 ± 9.2	91.1 ± 9.1	2.5 ± 0.4	1.1 ± 0.8	16.9 ± 7.4	-0.49
10222 1 0220	02 22 04.40	1.08	-03 38 20.99	1.70	C	10.0 . 0.0	5.3 ± 0.8	<4.5	<3.2	47.9 ± 15.2	0.20
J0222.1-0320	02 22 06.21	1.23	-03 20 39.87	1.84	3	19.0 ± 2.9	19.0 ± 2.9	10.5 ± 3.6	9.2 ± 3.3	77.9 ± 48.9	-0.30
J0222.1-0334	02 22 06.29	1.06	-03 34 20.23	1.75	3	23.8 ± 2.5	23.8 ± 2.5	<2.6	<2.4	34.9 ± 16.4	-0.36
J0222.1-0504	02 22 06.73	1.12	-05 04 18.36	1.90	3	3.3 ± 0.7	3.3 ± 0.7	.6</td <td><5.1</td> <td>$1/3.3 \pm 1/.3$</td> <td><-0.07</td>	<5.1	$1/3.3 \pm 1/.3$	<-0.07
J0222.1-0232	02 22 07.70	1.06	-02 33 01.09	1.//	3	7.6 ± 0.8	7.6 ± 0.8	<4.3	<1.0	$1/9.4 \pm 0.7$	-0.04
J0222.1-0428	02 22 07.91	1.29	-04 28 09.48	1.84	S	4.7 ± 0.9	4.7 ± 0.9	<8.5	<4.8	124.9 ± 9.2	0.04
J0222.2-0452	02 22 11.59	1.10	-04 52 21.91	1.84	S	3.8 ± 0.7	3.8 ± 0.7	<0./	<5.7	150.9 ± 42.7	<-0.17
J0222.2-0549	02 22 11.82	1.00	-05 49 05.85	1.75	S	83.8 ± 8.3	83.8 ± 8.3	<1.0	<1.5	38.3 ± 8.0	-0.97
J0222.2-0222 J0222.2 0428	02 22 11.91	1.12	-02 22 17.50	1.//	5	8.3 ± 1.3 7.0 + 1.1	8.3 ± 1.3	< 3.2	<4.1	122.2 ± 25.6	-0.70
10222.2-0428	02 22 13.03	1.10	-04 28 33.80	1.77	S C	7.9 ± 1.1	7.9 ± 1.1	<4.0	<4.1	132.3 ± 33.0 11.7 + 10.0	-0.00
10222.2-0300	02 22 14.08	1.09	-03 00 31.00	1.04	S C	4.2 ± 0.7	4.2 ± 0.7	< 0.7	< 3.9	11.7 ± 10.0 106.7 ± 12.6	<-0.23
10222.3-0249	02 22 18.30	1.10	-02 49 33.83	1.70	S C	0.3 ± 1.2 7 2 + 1 2	0.3 ± 1.2	<4.5	< 5.5	100.7 ± 13.0 128.2 ± 26.8	-0.42
10222.3-0240	02 22 18.03	1.10	-02 40 31.81	1.00	M	7.2 ± 1.2	7.2 ± 1.2	<0.5	< 3.1	120.3 ± 20.0	-0.17
J0222.3-0242	02 22 20.70	1.00	-02 42 10.47	1.75	C M	201.4 ± 14.9	127.0 ± 12.9 72.6 ± 7.5	4.7 ± 0.3	3.2 ± 0.4	41.7 ± 4.7 74.2 ± 12.6	-1.15
10222 4-0217	02 22 20.81	1.00	-024231.02 -021740.06	1.75	c c	18.0 ± 2.7	13.0 ± 7.3	4.0 ± 0.0 113 ± 1.6	5.0 ± 0.0	14.2 ± 12.0 133.1 ± 5.2	-0.67
J0222.4-0217 J0222.4-0231	02 22 20.90	1.23	$-02\ 17\ 40.90$ $-02\ 31\ 32\ 30$	1.05	S	16.0 ± 2.7 5.6 ± 1.3	16.0 ± 2.7 5.6 ± 1.3	11.3 ± 4.0	<4.3	153.1 ± 5.2 152.2 ± 14.5	-0.07
10222.4-0251	02 22 21.15	1.24	$-02\ 51\ 52.30$ $-04\ 53\ 26\ 48$	1.55	M	3.0 ± 1.3 0.8 ± 1.0	5.0 ± 1.3	< 1.5	< 3.2	132.2 ± 14.3 78.2 ± 0.4	-0.42
J0222.4-04JJ	02 22 22.85	1.10	$-04\ 53\ 20.48$ $-04\ 53\ 23\ 63$	1.70	C	9.0 ± 1.0	0.0 ± 0.9 3.2 ± 0.5	< 5.0	<3.2	70.2 ± 9.4 58.4 ± 8.0	-0.70
10222 4-0349	02 22 22.80	1.14	-04 33 23.03	1.77	M	97 ± 10	5.2 ± 0.3 5.7 ± 0.8	<5.0	<3.2	98.0 ± 8.3	-0.60
J0222.4-0J47	02 22 24.90	1.11	-03 49 51 64	1.76	C	0.7 ± 1.0	3.7 ± 0.0 4.0 ± 0.6	< 1.5	<3.1	98.8 ± 11.8	-0.00
10222 5-0407	02 22 24.07 02 22 27 74	1.10	-04 07 18 80	1.70	M	78 ± 10	4.0 ± 0.0	<7.9	< 1.1	120 ± 73	<-0.66
30222.5 0407	02 22 27.14	1.20	-04 07 18 46	1 79	C	7.0 ± 1.0	35 ± 0.6	<66	<3.5	51.6 ± 8.3	< 0.00
10222 5-0431	02 22 27.40	1.10	-04 31 23 48	1.75	M	154 + 15	10.4 ± 1.2	<3.7	<3.3	97.4 ± 19.0	-0.58
30222.5 0451	02 22 28.89	1.12	-04 31 39 73	1.79	C	10.4 ± 1.0	5.0 ± 0.8	<5.3	<4.7	138.1 + 42.6	0.50
10222.5-0307*	02 22 28 73	1.06	-030744.72	1.75	Š	66.6 + 6.7	66.6 ± 6.7	2.0 ± 0.6	<1.5	46.1 + 13.2	-0.74
10222.5-0333	02 22 29 57	1.14	-03 33 16 46	1.77	Š	40 + 0.7	40 ± 0.7	< 5.7	<4.1	111.7 + 17.4	<-0.20
10222.5-0352	02 22 29 87	1.12	-03 52 38 60	1.82	Š	4.2 ± 0.7	4.2 ± 0.7	<61	< 5.0	3.7 + 30.5	-0.31
10222.5-0447	02 22 30 17	1.07	$-04\ 47\ 05\ 45$	1.75	M	53.8 ± 4.0	28.7 + 3.0	45 + 09	<2.3	71.3 + 6.9	-0.89
0022210 0117	02 22 30.96	1.07	-04 47 07 56	1.75	C	0010 = 110	25.1 ± 2.6	4.3 ± 1.1	<2.5	73.9 ± 10.1	010)
J0222.6-0414	02 22 36.71	1.09	-04 14 58.01	1.81	Š	3.8 ± 0.6	3.8 ± 0.6	<5.9	<3.6	159.0 ± 10.4	<-0.17
J0222.7-0334	02 22 42.29	1.14	-03 34 18.23	1.83	ŝ	4.8 ± 0.9	4.8 ± 0.9	<6.5	<5.1	152.1 ± 25.6	0.23
J0222.7-0402	02 22 44.35	1.20	$-04\ 02\ 35.29$	1.84	ŝ	3.4 ± 0.7	3.4 ± 0.7	<7.1	< 5.8	45.2 ± 34.3	-0.28
J0222.8-0222	02 22 45 56	1.06	-02 22 22.74	1.75	S	31.9 ± 3.4	31.9 ± 3.4	<2.5	<2.2	81.0 ± 10.3	-0.96
J0222.8-0512	02 22 45.82	1.09	-05 12 17.18	1.92	S	4.4 ± 0.9	4.4 ± 0.9	<7.9	<4.3	178.7 ± 10.3	<-0.26
J0222.8-0303	02 22 46.16	1.06	-03 03 54.43	1.75	S	41.1 ± 4.2	41.1 ± 4.2	<2.0	<1.8	58.7 ± 9.3	-0.50
J0222.8-0348	02 22 47.61	1.06	-03 48 17.05	1.75	S	32.6 ± 3.3	32.6 ± 3.3	<2.0	<1.8	37.1 ± 9.2	-0.63
J0222.8-0344	02 22 48.31	1.68	-03 44 35.72	1.97	S	6.8 ± 1.4	6.8 ± 1.4	10.5 ± 9.9	<4.2	56.0 ± 4.0	<-0.56
J0222.8-0412	02 22 48.76	1.08	-04 12 15.77	1.76	S	8.8 ± 1.0	8.8 ± 1.0	<3.7	<3.1	49.3 ± 14.5	-0.87
J0222.8-0311	02 22 50.04	1.10	-03 11 51.61	1.80	S	12.3 ± 1.7	12.3 ± 1.7	6.6 ± 2.9	<4.2	19.9 ± 11.4	-0.78
J0222.9-0432	02 22 51.15	1.10	-04 32 14.25	1.79	S	5.6 ± 0.9	5.6 ± 0.9	<5.4	<4.2	28.8 ± 19.9	-0.19
J0222.9-0416	02 22 52.06	1.12	-04 16 46.38	1.77	М	9.7 ± 1.0	6.0 ± 0.8	<5.3	<3.6	57.1 ± 9.1	-0.69
	02 22 52.13	1.08	-04 16 48.97	1.78	С		3.7 ± 0.6	<4.8	<3.4	18.5 ± 13.9	
J0222.9-0525	02 22 54.08	1.26	-05 25 31.75	1.85	S	7.0 ± 1.5	7.0 ± 1.5	<8.3	<5.1	49.8 ± 14.0	<-0.58

C. Tusse et al.: The for frequency counterpart of the Think function survey, Onthic france that p 1	С.	Tasse et al.: Th	ne low-frec	quency cour	terpart of the	XMM large scale	structure survey,	Online	Material	p 14	4
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Table A.1. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{int}	S _{comp}	Major axis	Minor axis	Position	Spectral
10000 0 0011*	J2000	arcsec	J2000	arcsec		mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
J0222.9-0311*	02 22 54.60	1.07	-03 11 29.87	1.75	M	50.3 ± 4.9	46.5 ± 4.8	6.4 ± 0.8	4.0 ± 0.8	112.6 ± 6.0	-1.35
10222 9-0414	02 22 33.82	1.57	$-03\ 11\ 28.37$ $-04\ 14\ 04\ 77$	1.95	c s	175 ± 22	5.8 ± 0.9 17.5 ± 2.2	< 9.1 70 + 22	< 1.3	31.8 ± 30.3 30.7 ± 16.7	-0.26
10222.9-0309	02 22 54.62	1.10	-03 09 43 21	1.70	S	6.5 ± 1.0	6.5 ± 1.0	<6.5	<4.2	40.8 ± 9.8	<-0.53
J0222.9-0518*	02 22 55.76	1.06	-05 18 17.15	1.75	\tilde{M}	577.3 ± 54.4	543.2 ± 54.4	3.5 ± 0.1	2.9 ± 0.1	49.6 ± 3.7	-0.53
	02 22 56.15	1.09	-05 18 24.05	1.83	С		12.9 ± 1.8	<6.6	<2.7	22.1 ± 2.9	
	02 22 56.01	1.06	-05 18 22.35	1.76	С		11.6 ± 1.4	<3.5	<1.6	8.4 ± 2.6	
	02 22 56.13	1.22	-05 18 10.01	1.79	С		9.6 ± 1.6	<7.3	<3.6	62.1 ± 6.1	
J0223.0-0242*	02 22 56.07	1.06	-02 43 04.02	1.75	M	1489.9 ± 94.2	776.3 ± 77.7	6.4 ± 0.1	3.0 ± 0.1	93.1 ± 0.6	-0.84
	02 22 58.65	1.06	-02 42 53.31	1.75	C		515.7 ± 51.6	5.4 ± 0.1	2.6 ± 0.2	80.0 ± 1.0	
	02 22 30.03	1.07	-024305.89 -02425614	1.62	C		63.0 ± 9.1 63.3 ± 7.2	10.1 ± 2.7 73 + 16	< 1.0	10.9 ± 0.0 48.4 ± 11.0	
	02 22 57.78	1.03	-024250.14 -02425244	2.04	C		50.9 ± 6.4	18.0 ± 5.3		175.0 ± 1.0	
J0222.9-0424*	02 22 56.37	1.06	-04 24 49.55	1.75	M	70.0 ± 5.0	41.4 ± 4.2	3.0 ± 0.7	<1.8	24.7 ± 5.0	-0.98
	02 22 56.66	1.16	-04 24 52.40	1.76	С		19.7 ± 2.4	11.1 ± 2.8	<2.8	111.5 ± 2.1	
	02 22 57.23	1.10	-04 24 52.44	1.77	С		8.9 ± 1.2	4.1 ± 2.9	<4.0	131.1 ± 21.7	
J0223.0-0235	02 22 57.91	1.24	-02 35 37.05	1.97	S	8.6 ± 1.8	8.6 ± 1.8	<9.4	<5.4	32.6 ± 11.1	<-0.72
J0223.0-0407	02 22 58.05	1.19	-04 07 02.54	1.86	S	4.2 ± 0.8	4.2 ± 0.8	<6.9			-0.24
J0223.0-0504	02 22 58.22	1.07	-05 04 19.64	1.//	M	25.3 ± 2.5	19.1 ± 2.3	5.6 ± 2.0	< 3.3	$1/8.8 \pm 9.0$	-0.80
10223 0-0232	02 22 58.07	1.29	$-03\ 04\ 28.94$ $-02\ 33\ 01\ 34$	1.60	S	169 ± 21	0.2 ± 1.1 169 + 21	< 3.8	<4.5	15.3 ± 16.5	-0.68
J0223.0-0354	02 22 59.79	1.10	-03540555	1.77	M	37.9 ± 3.7	24.5 ± 2.9	84+18	7.9 ± 1.8	94.7 + 70.8	-0.78
022010 0001	02 23 00.16	1.25	-035339.84	1.86	C	0110 2011	13.4 ± 2.2	9.6 ± 4.1	8.3 ± 3.8	56.4 ± 58.7	0110
J0223.0-0409	02 23 01.29	1.10	-04 09 36.13	1.77	S	6.6 ± 0.9	6.6 ± 0.9	<4.7	<4.1	69.5 ± 27.5	-0.20
J0223.0-0428	02 23 02.43	1.13	-04 28 48.96	1.80	S	4.6 ± 0.8	4.6 ± 0.8	<5.5			<-0.30
J0223.1-0444	02 23 06.66	1.07	-04 44 44.74	1.76	S	8.9 ± 1.1	8.9 ± 1.1	<3.9	<3.3	169.5 ± 17.8	-0.07
J0223.2-0423	02 23 10.14	1.06	-04 23 06.92	1.75	S	44.5 ± 4.5	44.5 ± 4.5	2.2 ± 0.7	1.3 ± 1.1	13.2 ± 24.5	-0.13
J0223.2-0205*	02 23 12.99	1.06	-02 05 10.41	1.75	S	156.5 ± 15.7	156.5 ± 15.7	1.5 ± 0.6	<1.3	121.8 ± 13.1	-0.09
J0223.3-0207 J0223 3-0458	02 23 15.50	1.12	$-02\ 07\ 14.72$ $-04\ 58\ 44\ 72$	1.82	S	9.4 ± 1.7 57 ± 0.8	9.4 ± 1.7 57 ± 0.8	<0.2	< 3.0	21.2 ± 28.1 166.8 ± 24.0	-0.00
J0223.3-0444	02 23 10.01	1.37	-04 44 50.89	1.90	S	3.5 ± 0.8	3.5 ± 0.8	<8.8	<7.2	121.8 ± 39.8	<-0.10
J0223.3-0445	02 23 19.15	1.28	-04 45 49.22	1.87	Ŝ	3.9 ± 0.8	3.9 ± 0.8	<8.4	<5.8	131.0 ± 15.5	<-0.17
J0223.3-0318	02 23 20.72	1.06	-03 18 25.44	1.75	M	26.2 ± 2.4	21.2 ± 2.2	<2.4	<2.0	46.3 ± 6.3	-0.15
	02 23 18.40	1.12	-03 18 50.82	1.80	С		5.0 ± 0.8	<5.6	<4.7	33.0 ± 27.8	
J0223.4-0528	02 23 21.63	1.06	-05 28 04.66	1.83	Μ	42.7 ± 3.8	28.9 ± 2.9	12.3 ± 2.8	< 0.3	179.6 ± 0.0	<-1.82
10222 4 0222	02 23 21.85	1.08	-05 28 07.58	2.48	C	70.10	13.8 ± 2.4	17.8 ± 9.0	<3.7	2.7 ± 2.1	. 0.59
J0223.4-0222	02 23 22.67	1.09	-02 22 20.33	1.//	S	7.0 ± 1.0 5.1 ± 0.0	7.0 ± 1.0 5.1 ± 0.0	<4.2	<4.0	-1.0 ± 82.5	<-0.58
10223.4-0341 10223.4-0427	02 23 22.75	1.10	-03 41 43.00 -04 27 37 76	1.60	S M	3.1 ± 0.9 46.0 ± 3.4	3.1 ± 0.9 198 + 22	< 3.0	< 3.8	20.0 ± 12.0 32.8 ± 6.8	-0.43
30223.1 0127	02 23 25.52	1.08	$-04\ 27\ 09.23$	1.77	C	10.0 ± 5.1	15.9 ± 1.9	6.9 ± 1.8	3.0 ± 2.1	26.2 ± 9.4	0.57
	02 23 25.37	1.37	-04 27 22.41	2.10	С		10.2 ± 1.7	15.1 ± 7.6	<3.9	36.3 ± 2.9	
J0223.5-0540	02 23 27.42	1.07	-05 40 44.72	1.76	S	15.2 ± 1.7	15.2 ± 1.7	<3.3	<2.7	39.3 ± 9.9	-0.70
J0223.5-0303	02 23 29.38	1.18	-03 03 57.49	1.84	S	4.0 ± 0.8	4.0 ± 0.8	<7.7	<3.6	42.0 ± 6.6	<-0.20
J0223.5-0401	02 23 32.34	1.16	-04 01 45.68	1.79	S	3.5 ± 0.6	3.5 ± 0.6	<6.1	<4.7	114.6 ± 24.0	-0.21
J0223.5-0514	02 23 32.41	1.10	-05 14 37.41	1.75	5 M	11.3 ± 1.4	11.3 ± 1.4 1926 + 194	4.7 ± 2.8	< 3.0	52.5 ± 5.2	-0.86
J0223.0-0301*	02 23 33.13	1.00	$-03\ 01\ 23.93$ $-03\ 01\ 28\ 07$	1.75	C NA	200.0 ± 10.4	103.0 ± 10.4 10.4 ± 1.2	1.8 ± 0.3	1.2 ± 0.4	147.2 ± 10.0 176.2 ± 5.2	-1.09
	02 23 33.57	1.07	$-03\ 01\ 27.37$	1.76	C		6.9 ± 0.9	<4.0	<2.4	146.6 ± 5.7	
J0223.6-0458	02 23 34.06	1.32	-04 58 36.72	1.80	Š	$66.4 \pm 12.9^*$	32.6 ± 4.4	17.5 ± 4.1	8.2 ± 2.3	103.3 ± 5.5	-0.38
J0223.6-0232*	02 23 34.68	1.06	-02 32 24.03	1.76	M	172.8 ± 12.4	89.6 ± 9.2	11.4 ± 0.8	2.1 ± 0.8	14.7 ± 1.1	-0.91
	02 23 34.80	1.06	-02 32 19.22	1.75	С		83.2 ± 8.4	1.6 ± 0.7	<1.4	129.9 ± 4.1	
J0223.6-0348	02 23 35.75	1.20	-03 48 47.68	1.87	S	3.1 ± 0.7	3.1 ± 0.7	<7.4	<6.3	29.3 ± 49.9	<-0.02
J0223.6-0409	02 23 36.84	1.10	-04 09 33.15	1.76	M	9.7 ± 1.0	5.2 ± 0.7	<4.5	<3.7	67.9 ± 21.7	-0.71
10223 6-0213*	02 23 37.57	1.09	-04 09 33.06	1.78 1.75	S	831+86	4.3 ± 0.7 83 1 + 8 6	<3.1 10 8 + 1 2	< 3.0 <17	33.7 ± 11.3 54.3 ± 0.8	-1.07
J0223.6-0213	02 23 37.95	1.14	$-02\ 24\ 48\ 47$	1.94	S	12.8 ± 2.2	12.8 ± 2.2	9.1 ± 5.4	<4.6	19.3 ± 7.0	<-1.00
J0223.6-0506	02 23 38.18	1.17	-05 06 28.51	1.75	Š	26.4 ± 3.0	26.4 ± 3.0	14.0 ± 2.6	<2.9	85.7 ± 1.9	-0.74
J0223.7-0310	02 23 40.10	1.07	-03 10 26.22	1.78	М	8.2 ± 1.0	4.7 ± 0.7	<4.7	<2.9	167.8 ± 8.3	<-0.69
	02 23 39.91	1.10	-03 10 25.00	1.95	С		3.5 ± 0.7	<8.5	<4.4	175.4 ± 9.4	
J0223.7-0239*	02 23 41.65	1.06	-02 39 45.77	1.75	M	205.2 ± 19.8	197.9 ± 19.8	4.0 ± 0.2	1.7 ± 0.3	35.0 ± 1.9	-0.97
	02 23 41.23	1.07	-02 39 51.77	1.77	C		7.4 ± 1.0	<4.4	<2.7	9.2 ± 7.1	0.50
J0223.7-0411	02 23 42.80	1.07	-04 11 59.94	1.76	S	14.2 ± 1.6	14.2 ± 1.6	3.7 ± 1.7	<2.8	30.8 ± 10.0	-0.73
JU225.7-U551 I0223.7-0224	02 23 44.17	1.07	-03 31 32.97 -02 24 52 00	1.81	М	4.1 ± 0.7 10.1 ± 1.1	4.1 ± 0.7 5.4 ± 0.0	< 3.9	< 3.0 ~ 2 7	0.6 ± 0.8 26.0 ± 3.4	<-0.21
30223.7-0224	02 23 44 71	1.07	$-02\ 24\ 52.09$ $-02\ 24\ 52.39$	1.85	C	10.1 ± 1.1	3.7 ± 0.9 4.7 + 0.7	<6.1	<2.1	20.9 ± 3.4 18.1 + 3.7	-0.04
J0223.7-0232	02 23 44.65	1.19	-02 32 45.70	1.91	Š	4.9 ± 1.1	4.9 ± 1.1	<8.1	<6.1	159.2 ± 30.3	<-0.34
J0223.8-0340*	02 23 45.44	1.06	-03 40 42.18	1.75	S	106.5 ± 10.7	106.5 ± 10.7	5.8 ± 0.3	2.6 ± 0.4	103.7 ± 1.8	-0.72
J0223.8-0332*	02 23 46.58	1.06	-03 32 36.03	1.75	М	111.5 ± 10.6	106.0 ± 10.6	1.6 ± 0.4	1.1 ± 0.6	65.8 ± 28.3	-0.52
	02 23 47.01	1.07	-03 32 39.80	1.76	С		5.5 ± 0.7	<3.9	<2.6	142.3 ± 8.3	
J0223.8-0551	02 23 48.08	1.06	-05 51 14.65	1.75	S	129.9 ± 13.1	129.9 ± 13.1	2.2 ± 0.5	<1.4	19.1 ± 7.2	-0.22
J0223.8-0412*	02 23 49.08	1.06	-04 12 11.53	1.75	M	85.6 ± 6.3	43.1 ± 4.5	6.8 ± 0.8	4.0 ± 0.8	151.9 ± 5.2	-0.77
10223 8-0521	02 23 49.83	1.00	-04 12 30.83 -05 31 05 56	1.75	c c	81 + 11	42.3 ± 4.4 8 1 \pm 1 1	3.3 ± 0.7	4.2 ± 0.7	113.3 ± 12.4 39.6 \pm 12.1	_0.85
J0223.9-0522	02 23 52.63	1.06	-05 22 25.48	1.75	S	26.6 ± 2.7	26.6 ± 2.7	<2.3	<2.1	37.9 ± 9.6	-0.65

C.	Tasse et al.:	The	low-frequenc	v counterr	part of the	XMM la	ge scale	structure	survev	. Online	Material	p 15
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Table A.1. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Type	$S_{\rm int}$	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec	21	mJy	mJy	arcsec	arcsec	Angle	index α_{225}^{1400}
J0223.9-0445	02 23 55.02	1.12	-04 45 45.70	2.01	S	4.6 ± 0.9	4.6 ± 0.9	< 9.4	<3.6	17.4 ± 4.4	<-0.30
J0223.9-0254	02 23 56.45	1.14	-02 54 31.36	1.76	м М	7.8 ± 1.0	4.1 ± 0.7	<5.5	<3.8	100.5 ± 14.2	-0.88
0022010 0201	02 23 56 45	1.23	-02543448	1.77	C	/10 = 110	3.7 ± 0.7	<7.1	<3.9	71.8 ± 9.1	0100
I0224 0-0441*	02 23 57 03	1.06	-04 41 12.64	1.75	M	219.3 + 21.0	209.4 + 21.0	3.7 ± 0.2	1.9 ± 0.3	19.1 + 2.2	-0.99
0022110 0111	02 23 57.49	1.27	-04 41 15.68	2.03	C	21/10 2 2110	9.9 ± 1.8	9.3 ± 7.8	<3.8	33.4 ± 3.9	0.77
J0224.0-0353	02 23 59.37	1.07	-03 53 58.38	1.75	Š	14.5 ± 1.6	14.5 ± 1.6	<2.9	<2.5	43.0 ± 11.0	-0.96
10224.0-0325	02 24 00 43	1.11	-03 25 36 51	1.78	м М	9.1 + 1.1	5.9 ± 0.8	< 5.6	<3.4	44.3 ± 6.6	<-0.76
0022110 0020	02 24 00 66	1 54	-03253575	1 91	C	<i>y</i> <u>_</u>	32 ± 0.7	<10.9	<5.0	1222 + 70	
10224 0-0238	02 24 01 16	1.21	-02384918	1.78	S	46 ± 0.8	46 ± 0.8	<69	<4.6	712 ± 137	< -0.29
J0224.0 0230	02 24 01.10	1.21	-03 20 29 71	1.70	S	4.0 ± 0.0 4.9 ± 0.8	4.0 ± 0.0 4.9 ± 0.8	<7.1	<4.8	68.5 ± 12.4	-0.53
J0224.0 0520	02 24 01.20	1.22	-04 33 04 96	1.82	S	9.1 ± 1.5	9.1 ± 1.5	85+44	<5.3	61.6 ± 12.4	-0.59
J0224.1-0433	02 24 05.74	1.25	-02 02 22 82	1.02	S	30.1 ± 3.2	30.1 ± 3.2	2.3 ± 4.4	<5.5	01.0 ± 12.0	-1.02
J0224.1-0202 J0224.1_0512	02 24 03.43	1.00	-02 02 22.82	1.75	S S	30.1 ± 3.2	30.1 ± 3.2	<2.3	-2.0		-1.02
J0224.1-0312 J0224.1_0227	02 24 05.31	1.07	-03 12 26.29	1.70	5	11.0 ± 1.3	11.0 ± 1.3	< 3.2	< 3.0	41.0 ± 32.3	-0.39
J0224.1-0227	02 24 03.77	1.10	-02 27 31.99	1.60	5	3.7 ± 1.0	3.7 ± 1.0	< 3.0	<4.5	$1/3.0 \pm 2/.0$	-0.48
J0224.1-0319	02 24 00.71	1.10	-05 19 00.01	1.69	<u></u> с	5.3 ± 0.7	5.5 ± 0.7	<7.5	<0.2	10.2 ± 42.1	<-0.00
J0224.1-0259	02 24 07.84	1.11	-02 59 51.15	1.//	3	6.3 ± 0.9	0.3 ± 0.9	< 5.0	<4.1	74.0 ± 21.9	-0.43
J0224.2-0450	02 24 10.21	1.09	-04 50 32.89	1.76	S	6.0 ± 0.8	6.0 ± 0.8	<4.1	<3.5	101.4 ± 26.6	-0.15
J0224.2-0446*	02 24 10.29	1.06	-04 46 07.72	1.75	M	66.5 ± 5.3	46.9 ± 4.8	4.8 ± 0.6	<1.8	99.0 ± 3.7	-0.88
	02 24 09.51	1.08	-04 46 05.45	1.76	С		19.6 ± 2.2	5.2 ± 1.6	3.9 ± 1.7	102.0 ± 27.7	
J0224.2-0433	02 24 10.42	1.37	-04 33 18.83	1.88	S	3.3 ± 0.7	3.3 ± 0.7	<8.8	<6.8	117.7 ± 30.7	<-0.07
J0224.2-0350	02 24 10.81	1.06	-03 50 17.09	1.75	S	18.7 ± 2.0	18.7 ± 2.0	<2.4	<2.2	62.9 ± 14.7	-0.76
J0224.2-0307	02 24 11.85	1.07	-03 07 44.44	1.76	S	18.1 ± 2.0	18.1 ± 2.0	3.8 ± 1.6	<2.5	34.4 ± 5.5	-0.55
J0224.2-0355	02 24 12.14	1.14	-03 55 57.60	1.80	S	4.5 ± 0.7	4.5 ± 0.7	<5.9	<4.9	41.8 ± 30.0	-0.01
J0224.2-0222	02 24 13.92	1.07	-02 22 19.90	1.75	М	36.3 ± 2.7	17.2 ± 1.9	<3.1	<2.7	61.9 ± 13.7	-0.79
	02 24 11.07	1.07	-02 22 34.07	1.75	С		13.7 ± 1.6	<3.2	<2.5	61.8 ± 10.2	
	02 24 11.08	1.23	-02 22 36.95	1.75	Ċ		5.4 ± 0.9	<7.0	<2.9	90.1 ± 4.5	
10224.2-0528*	02 24 15 02	1.06	-05 28 45 79	1.75	M	494.5 + 24.9	158.0 ± 16.0	7.9 ± 0.4	4.5 ± 0.4	143.3 + 2.1	-0.72
0022.112 0020	02 24 14 52	1.09	-05 28 33 00	1 77	C	19 110 2 2 119	131.1 ± 14.0	162 + 15	94 ± 10	1349 + 33	0172
	02 24 13 46	1.10	-05 28 08 37	1.78	C		87.0 ± 9.7	15.2 ± 1.0 15.3 ± 2.0	77 ± 1.0	147.4 + 3.4	
	02 24 13.40	1.10	$-05\ 20\ 00.37$ $-05\ 27\ 55\ 23$	1.75	C		66.2 ± 6.7	3.1 ± 0.7	/./ ± 1.2	$3/5 \pm 7.3$	
	02 24 12.00	1.00	-05 27 53.25	1.75	C		52.2 ± 5.7	10.0 ± 1.6	<2.5	160.3 ± 2.1	
10224 2 0242	02 24 12.03	1.07	-03 27 37.70	1.//	c	26106	32.2 ± 3.1	10.9 ± 1.0	<2.5	100.3 ± 2.1	< 0.12
J0224.5-0542	02 24 15.05	1.10	-05 42 25.92	1.01	<u></u> с	5.0 ± 0.0	5.0 ± 0.0	< 3.8	<4.5	19.4 ± 21.2	<-0.15
J0224.3-0431	02 24 15.96	1.22	-04 31 42.58	1.80	3	5.0 ± 0.0	3.0 ± 0.0	<7.9	<5.5	43.9 ± 17.0	< 0.01
J0224.3-0200	02 24 16.66	1.23	-02 00 35.49	1.97	S	5.7 ± 1.3	5.7 ± 1.3	<8.6	<6.9	4.7 ± 36.6	<-0.44
J0224.3-0243*	02 24 18.40	1.07	-02 43 29.05	1.76	М	142.4 ± 8.5	41.4 ± 4.4	8.1 ± 1.1	<2.2	141.7 ± 2.3	-0.12
	02 24 17.74	1.13	-02 43 13.41	1.81	С		34.4 ± 4.4	11.7 ± 2.7	8.1 ± 2.1	148.0 ± 12.4	
	02 24 18.87	1.21	-02 43 42.55	1.79	С		30.9 ± 4.0	14.1 ± 3.4	5.7 ± 2.1	118.1 ± 5.0	
	02 24 17.23	1.21	-02 43 04.72	1.82	С		26.5 ± 3.8	11.9 ± 3.5	7.5 ± 2.6	55.1 ± 12.8	
	02 24 18.05	1.24	-02 43 40.97	2.09	С		9.2 ± 1.9	10.6 ± 6.8	<6.9	168.3 ± 16.1	
J0224.3-0300*	02 24 18.84	1.06	-03 00 22.15	1.75	М	79.1 ± 5.9	55.4 ± 5.6	4.6 ± 0.5	1.6 ± 1.0	26.5 ± 4.2	-0.86
	02 24 19.10	1.07	-03 00 12.85	1.75	С		14.4 ± 1.6	<3.1	<2.2	74.0 ± 5.1	
	02 24 19.14	1.10	-03 00 15.62	1.75	С		9.4 ± 1.1	<4.4	<2.0	97.7 ± 2.3	
J0224.3-0502	02 24 19.06	1.22	-05 02 36.42	1.77	S	13.0 ± 1.8	13.0 ± 1.8	9.9 ± 3.6	<3.6	74.5 ± 4.0	-0.82
J0224.4-0311	02 24 21.54	1.12	-03 11 25.32	1.78	S	6.1 ± 0.9	6.1 ± 0.9	<5.4	<4.1	54.5 ± 16.8	<-0.49
10224 4-0425*	02 24 21 59	1.06	-04 25 49 99	1 75	м	837 + 59	48.6 ± 4.9	29 ± 0.6	21 ± 07	67.5 ± 15.7	-0.96
30221.1 0123	02 24 20 22	1.00	-04 25 42 57	1.75	C	05.7 ± 5.9	31.4 ± 3.2	36 ± 0.8	19 ± 12	57.5 ± 13.7 52.7 ± 11.5	0.90
	02 24 20.22	1.00	-04 25 44 85	1.75	C		38 ± 0.7	-6 5	-5.4	35.7 ± 11.5 35.5 ± 38.6	
10224 4 0402	02 24 20.78	1.10	-04 23 44.83	2.06	c	26+05	3.8 ± 0.7	<10.5	<3.0	33.3 ± 38.0	< 0.00
J0224.4-0403	02 24 23.83	1.23	-04 03 27.12	2.00	S M	2.0 ± 0.3	2.0 ± 0.3	12.1 ± 7.0	< 3.9	26.7 ± 4.3	< 0.09
J0224.3-0320	02 24 27.33	1.05	$-05\ 20\ 50.40$	1.62	M C	11.0 ± 1.7	7.0 ± 1.3	12.1 ± 7.0	< 0.1	94.0 ± 9.8	-0.50
10004 5 0040*	02 24 27.09	1.15	-05 20 30.05	1.79	C M	1151 . 100	4.0 ± 0.7	< 3.8	<4.4	30.1 ± 20.8	0.50
J0224.5-0245*	02 24 27.50	1.00	-02 43 05.73	1.75	M	115.1 ± 10.9	108.1 ± 10.8	<1.1	<1.1	81.5 ± 29.5	-0.59
10001 5 0110	02 24 27.11	1.07	-02 43 10.00	1.78	C	24.2 2.4	7.0 ± 0.9	<4.8	<2.7	150.1 ± 5.3	0.40
J0224.5-0449	02 24 28.76	1.09	-04 49 52.30	1.76	M	24.2 ± 2.4	15.2 ± 1.8	6.1 ± 1.9	4.3 ± 2.0	75.1 ± 21.5	-0.49
	02 24 27.49	1.55	-04 49 52.95	1.81	C		9.0 ± 1.6	13.8 ± 6.0	<5.7	91.2 ± 7.7	0.05
J0224.5-0307	02 24 28.99	1.07	-03 07 20.22	1.76	S	9.0 ± 1.1	9.0 ± 1.1	<3.6	<3.0	43.0 ± 13.8	-0.85
J0224.5-0504	02 24 29.20	1.07	-05 04 23.21	1.76	Μ	20.9 ± 1.9	15.2 ± 1.7	4.6 ± 1.8	<2.4	129.7 ± 3.7	-1.13
	02 24 29.31	1.10	-05 04 21.43	1.77	С		5.7 ± 0.8	<5.3	<3.0	43.7 ± 5.9	
J0224.5-0335	02 24 29.68	1.09	-03 35 30.45	1.77	S	5.0 ± 0.7	5.0 ± 0.7	<4.7	<3.7	50.7 ± 19.1	-0.59
J0224.5-0314	02 24 30.23	1.13	-03 14 54.15	1.83	S	4.3 ± 0.7	4.3 ± 0.7	<6.5	<5.0	25.0 ± 20.8	<-0.24
J0224.5-0219*	02 24 30.33	1.09	-02 19 33.15	1.75	М	112.7 ± 9.2	84.2 ± 8.8	14.6 ± 1.3	3.1 ± 0.8	104.7 ± 1.1	-0.50
	02 24 30.77	1.06	-02 19 34.38	1.76	С		23.7 ± 2.6	3.6 ± 1.8	<2.2	15.5 ± 3.2	
	02 24 30.68	1.31	-02 19 25.13	1.91	С		4.8 ± 1.0	<9.6	<4.0	134.6 ± 5.9	
J0224.5-0534	02 24 32.15	1.08	-05 34 30.35	1.77	S	13.7 ± 1.7	13.7 ± 1.7	<4.2	<3.3	34.5 ± 12.5	0.12
J0224.6-0354	02 24 32 92	1.11	-03 54 38 69	1.79	S	38.3 ± 11.8*	6.0 ± 0.9	< 5.5	<4.2	38.6 ± 15.8	-0.09
J0224.6-0334	02 24 32.95	1.09	-03 34 12 55	1.76	ŝ	$67.2 \pm 10.6^*$	39.1 + 4.3	12.1 ± 1.6	5.2 + 1.0	54.9 + 3.0	-0.73
10224 6-0408	02 24 33 84	1.07	-04 08 52 93	1.76	ŝ	10.4 + 1.2	10.4 ± 1.2	<35	<32	41.4 + 74.8	-0.90
I0224.0 -0408	02 24 33.04	1.07	_03 10 50 74	1.70	ç	46 ± 0.8	46 ± 0.8	<7.6	<1.0	110.8 ± 120	<_0.20
I0224.6-0310	02 24 34.00	1.25	_0/ 1/ 22 50	1 70	S	-1.0 ± 0.0 28 ± 0.5	7.0 ± 0.0 28 ± 0.5	<53	~7.7	117.0 ± 12.0 21.4 ± 27.7	_0.12
I0224.0-0414	02 24 34.20	1.09	_0/ 13 02 19	1.19	ç	2.0 ± 0.3 3.0 ± 0.6	2.0 ± 0.5 3.0 ± 0.6	~5.5	~7.1	21.7 ± 21.7 -1.0 ± 72.2	-0.12 <-0.01
10224.0-0413	02 24 30.33	1.14	-04 13 02.18	1.02	ა ი	3.0 ± 0.0	3.0 ± 0.0	< 0.1	< 3.5	$-1.0 \pm /3.2$	<-0.01
JUZZ4.7-U357	02 24 39.07	1.19	-03 3/ 41.38	1.//	5	3.2 ± 0.0	5.2 ± 0.0	< 0.4	<4.5	01.0 ± 14.3	<-0.05
JU224.7-0347	02 24 39.83	1.11	-03 4/ 10.64	1.88	M	13.4 ± 1.5	1.8 ± 1.2	$\delta.\delta \pm 4.4$	<4.1	18.2 ± 6.0	-0.52
10004 7 0000	02 24 39.61	1.07	-03 47 12.64	1.76	C	47 7 2 2 2	1.0 ± 0.9	<3.5	<3.1	1.7 ± 21.2	0.07
J0224.7-0209*	02 24 41.08	1.09	-02 09 53.06	1.76	M	41.1 ± 3.8	23.5 ± 2.8	4.5 ± 2.2	<3.3	$11/.1 \pm 10.3$	-0.37
	02 24 41.12	1.07	-02 09 49.32	1.75	C		17.9 ± 2.0	<2.9	<2.7	91.1 ± 27.9	

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Table A.1. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{int}	Scomp	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
	02 24 41.52	1.54	-02 10 20.01	1.89	С		6.3 ± 1.4	<10.2	<7.1	108.9 ± 20.7	.12.1
J0224.7-0311	02 24 42.40	1.09	-03 11 36.99	1.78	S	5.2 ± 0.8	5.2 ± 0.8	<5.0	<4.1	164.1 ± 27.8	<-0.38
J0224.7-0330	02 24 44.28	1.07	-03 30 16.70	1.75	S	14.8 ± 1.6	14.8 ± 1.6	<2.8	<2.5	53.0 ± 15.3	-0.99
J0224.7-0351	02 24 44.74	1.14	-03 51 40.72	1.77	S	8.3 ± 1.2	8.3 ± 1.2	6.0 ± 3.3	<4.0	65.4 ± 10.0	-0.63
J0224.8-0302*	02 24 46.04	1.06	-03 01 56.81	1.75	M	397.7 ± 21.9	183.7 ± 18.4	2.4 ± 0.2	2.0 ± 0.2	169.8 ± 11.9	-0.66
	02 24 45.47	1.06	-03 02 33.74	1.75	С		93.2 ± 9.4	4.1 ± 0.3	<1.3	34.0 ± 2.2	
	02 24 45.61	1.06	-03 02 25.75	1.75	C		57.6 ± 5.8	3.7 ± 0.5	<1.6	26.7 ± 3.5	
	02 24 45.47	1.30	-03 02 05.61	1.77	C		25.7 ± 3.3	17.3 ± 3.9	4.2 ± 2.0	102.2 ± 2.8	
	02 24 44.90	1.20	-03 02 51.87	1.90	C		16.4 ± 2.5	14.1 ± 4.5	5.3 ± 2.9	33.9 ± 6.4	
	02 24 45.58	1.09	-03 02 01.18	1.76	C		11.1 ± 1.3	<4.0	<3.1	96.8 ± 9.8	
	02 24 45.76	1.25	-03 02 19.54	1.80	C		5.3 ± 0.9	.8</td <td>< 3.4</td> <td>59.8 ± 4.5</td> <td></td>	< 3.4	59.8 ± 4.5	
10224 9 0409	02 24 44.88	1.30	-03 02 39.00	1.95	C M	62.06	4.7 ± 0.9	8.7 ± 0.4	< 5.9	139.3 ± 12.7	< 0.50
J0224.8-0408	02 24 47.04	1.10	$-04\ 08\ 31.88$	1.//	M C	0.2 ± 0.0	3.3 ± 0.3 3.0 ± 0.3	< 5.0	< 5.7	31.8 ± 19.0 164.1 ± 0.0	<-0.50
10224 8-0545*	02 24 40.91	1.07	$-04\ 08\ 49.03$ $-05\ 45\ 20\ 83$	1.04	M	1255 + 94	5.0 ± 0.3 64 1 + 6 8	(5+10)	47 ± 10	104.1 ± 0.0 156.2 + 10.1	-0.71
30224.0 0343	02 24 49 65	1.07	-05 45 47 96	1.76	C	125.5 ± 7.4	55.0 ± 6.4	11.7 ± 2.1	54 ± 1.0	108.3 ± 4.6	0.71
	02 24 49.05	1 39	-05 45 29 75	1.70	C		64 ± 14	< 8.8	-62 -62	106.5 ± 4.0 106.7 ± 21.4	
10224 8-0326	02 24 48 38	1.10	-03 26 11 39	1.04	S	64 + 09	64 ± 0.9	<47	<4.2	51.6 + 39.2	<-0.51
10224 8-0221*	02 24 48.75	1.06	-02.2119.08	1.76	S	83.0 + 8.6	83.0 + 8.6	12.0 ± 1.0	<1.8	26.2 ± 0.9	-0.49
J0224.8-0353	02 24 50.68	1.07	-03 53 58.85	1.78	Š	5.2 ± 0.7	5.2 ± 0.7	<4.8	<2.6	9.8 ± 4.3	<-0.38
J0224.8-0431	02 24 50.83	1.08	-04 31 40.73	1.76	Š	5.0 ± 0.7	5.0 ± 0.7	<4.4	<3.2	45.8 ± 10.4	<-0.35
J0224.9-0428	02 24 51.07	1.08	-04 29 01.43	1.78	ŝ	4.8 ± 0.7	4.8 ± 0.7	<5.0	<3.6	16.4 ± 12.0	<-0.32
J0224.9-0452	02 24 52.00	1.12	-04 52 52.40	2.10	S	2.8 ± 0.6	2.8 ± 0.6	<10.2	<4.9	6.7 ± 8.6	< 0.04
J0224.9-0434	02 24 53.87	1.06	-04 34 14.30	1.75	S	25.3 ± 2.6	25.3 ± 2.6	2.9 ± 0.9	<2.1	76.0 ± 18.5	-0.61
J0224.9-0332	02 24 54.82	1.06	-03 32 04.40	1.75	S	23.6 ± 2.4	23.6 ± 2.4	<2.1	<2.0	62.8 ± 13.8	-0.43
J0224.9-0251	02 24 54.85	1.17	-02 51 10.88	1.79	М	9.2 ± 1.1	5.0 ± 0.8	<6.6	<3.6	56.2 ± 6.9	-0.68
	02 24 54.72	1.12	-02 51 09.17	1.79	С		4.2 ± 0.7	<5.4	<4.7	135.9 ± 51.6	
J0224.9-0329	02 24 54.90	1.08	-03 29 05.63	1.76	S	9.3 ± 1.1	9.3 ± 1.1	<3.7	<3.4	38.8 ± 42.6	<-0.78
J0224.9-0256	02 24 55.20	1.19	-02 56 55.74	1.77	S	9.9 ± 1.5	9.9 ± 1.5	6.5 ± 4.0	<4.0	75.8 ± 7.5	-0.64
J0224.9-0310	02 24 55.66	1.06	-03 10 40.48	1.76	S	16.8 ± 1.8	16.8 ± 1.8	2.4 ± 2.0	<2.5	1.0 ± 8.8	-0.51
J0224.9-0408	02 24 56.47	1.08	-04 08 53.98	1.77	S	4.9 ± 0.6	4.9 ± 0.6	<4.1	<3.6	4.1 ± 28.1	<-0.33
J0225.0-0516*	02 24 57.72	1.06	-05 16 48.34	1.75	M	111.7 ± 8.0	56.9 ± 5.8	4.0 ± 0.6	<1.7	22.8 ± 3.9	-0.76
	02 24 57.21	1.06	-05 17 03.00	1.75	С		54.8 ± 5.6	4.9 ± 0.6	<1.8	45.4 ± 3.3	
J0225.0-0435	02 24 59.49	1.10	-04 35 36.54	1.76	S	5.0 ± 0.7	5.0 ± 0.7	<4.6	<3.6	89.5 ± 15.5	-0.51
J0225.0-0321*	02 25 00.59	1.13	-03 21 08.18	1.79	M	35.6 ± 3.6	25.5 ± 3.2	10.5 ± 2.5	7.5 ± 2.1	131.4 ± 14.2	-0.83
	02 24 59.90	1.13	-03 20 52.61	1.82	С		10.2 ± 1.5	7.6 ± 3.3	5.1 ± 3.2	11.3 ± 26.2	
J0225.1-0536*	02 25 05.13	1.06	-05 36 48.02	1.75	M	596.3 ± 56.7	566.1 ± 56.7	4.4 ± 0.1	2.5 ± 0.2	5.6 ± 1.4	-0.62
	02 25 05.39	1.15	-05 36 41.26	1.75	С		17.9 ± 2.1	<5.7	<1.5	91.2 ± 1.0	
	02 25 05.47	1.21	-05 36 38.66	1.75	С		12.4 ± 1.5	<6.6	<1.2	87.5 ± 0.6	
J0225.1-0321	02 25 05.40	1.10	-03 21 18.32	1.76	S	5.4 ± 0.8	5.4 ± 0.8	<4.5	<3.6	84.3 ± 17.4	<-0.40
J0225.1-0519	02 25 05.90	1.10	-05 19 59.76	1.77	S	9.0 ± 1.2	9.0 ± 1.2	<4.6	<4.0	48.3 ± 23.8	-0.50
J0225.1-0300	02 25 06.20	1.27	-03 00 23.81	1.81	S	3.6 ± 0.7	3.6 ± 0.7	<7.7	<5.0	65.3 ± 15.1	<-0.12
J0225.1-0533	02 25 06.25	1.29	-05 33 11.31	1.88	Μ	40.3 ± 4.5	25.0 ± 3.8	10.1 ± 5.9	<2.9	47.6 ± 2.2	-1.03
	02 25 06.42	1.10	-05 33 13.50	1.79	С		15.3 ± 2.3	<5.3	<4.4	17.7 ± 24.8	
J0225.1-0516	02 25 07.12	1.16	-05 16 31.10	1.85	S	4.1 ± 0.9	4.1 ± 0.9	<6.8	<6.0	-1.0 ± 62.9	<-0.22
J0225.1-0316	02 25 08.14	1.12	-03 16 38.30	1.90	S	15.7 ± 2.2	15.7 ± 2.2	13.9 ± 4.0	<4.2	160.6 ± 4.1	-0.07
J0225.1-0406	02 25 08.32	1.11	-04 06 53.60	1.79	S	2.9 ± 0.5	2.9 ± 0.5	<5.3	<4.6	$14/.8 \pm 49.6$	< 0.02
J0225.2-0401	02 25 09.14	1.06	-04 01 02.24	1.75	S	24.0 ± 2.5	24.0 ± 2.5	<2.0	<1.8	31.3 ± 12.7	-0.86
J0225.2-0509	02 25 09.72	1.18	-05 09 49.05	1.81	5	3.6 ± 0.7	3.6 ± 0.7	< 6.9	<4.9	50.4 ± 20.0	-0.30
J0225.2-0403	02 25 10.21	1.09	-04 04 01.46	1.70	5	5.7 ± 0.8	5.7 ± 0.8	<4.3	<3.7	64.8 ± 23.4	-0.56
J0225.2-0205	02 25 10.50	1.12	-02 03 25.25	1.79	S M	7.1 ± 1.3	7.1 ± 1.3	< 3.3	52.22		<-0.59
J0225.2-0454	02 23 11.13	1.51	-04 54 52.45	1.70	M C	33.0 ± 3.3	20.2 ± 2.8	13.1 ± 4.0	3.3 ± 2.3	01.0 ± 4.0 114.8 ± 12.4	-0.47
	02 25 10.17	1.35	-04 54 50.10	1.05	C		0.7 ± 1.3	0.3 ± 3.0	< 5.0	114.0 ± 12.4 76 4 ± 29 1	
10225 2-0240	02 25 11.95	1.35	-04 34 23.83 -02 40 03 85	1.05	c c	40 ± 0.8	0.0 ± 1.3	0.3 ± 3.4	<0.7	-1.0 ± 78.2	0.03
10225.2-0249	02 25 11.34	1.23	-024903.83 -05241212	1.90	S	4.0 ± 0.0	4.0 ± 0.0 5 7 \pm 1 1	< 8.1	< 5.1	-1.0 ± 70.2 151 3 ± 12.7	0.03
10225.2-0324	02 25 12.08	1.10	-03 /3 09 77	1.90	S	3.7 ± 1.1 7.2 ± 0.9	5.7 ± 1.1 7.2 ± 0.9	<3.7	<3.2	131.3 ± 12.7 14.0 ± 18.3	<-0.42
10225 2-0229	02 25 12.07	1.07	-02291606	1.70	M	10.7 ± 0.9	67 ± 10	<5.4	<3.5	14.7 ± 10.5 137.3 ± 9.4	0.50
J 0225.2-0227	02 25 13.92	1.10	-02291622	1.70	C	10.7 ± 1.5	40 ± 0.8	<9.9	<43	137.3 ± 9.4 53.6 + 6.6	0.50
10225 2-0301	02 25 15.82	1.40	$-02\ 27\ 10.22$ $-03\ 01\ 06\ 72$	1.00	S	124 + 15	12.4 ± 1.5	42 + 23	<31	100.2 ± 8.6	-0.30
10225.2 0501	02 25 14.55	1.05	-04 36 15 60	1.76	M	96 ± 10	65 ± 0.8	-1.2 ± 2.3	<3.1	819 ± 80	-0.64
30223.2 0430	02 25 14.00	1.10	-04 36 12 48	1.70	C	9.0 ± 1.0	3.0 ± 0.5	<9.4	<29	724 ± 20	0.04
10225 3-0233	02 25 14 98	1.10	-02334724	1.80	Š	63 ± 07	63 ± 0.5	<5.5	<0.9	30 ± 0.3	<-0.51
J0225.3-0424	02 25 16 52	1.07	-04 24 26 54	1.77	Š	3.9 ± 0.7	3.9 ± 0.7	<4.0	<3.3	16.4 ± 22.9	<-0.18
J0225.3-0546	02 25 16.67	1.12	-05 46 02.61	1.94	Š	6.1 ± 1.3	6.1 ± 1.3	<8.3	<4.8	167.6 ± 12.3	<-0.48
J0225.3-0417	02 25 17.96	1.33	-04 17 54.64	1.81	Š	2.5 ± 0.5	2.5 ± 0.5	<8.4	<4.9	65.6 ± 12.0	< 0.13
J0225.3-0240	02 25 18.29	1.08	-02 40 47 82	1.75	M	21.3 ± 1.7	9.5 ± 1.1	<3.5	<2.3	85.4 ± 5.5	-0.56
	02 25 18.29	1.10	-02 40 50.82	1.75	Ċ		8.1 ± 1.0	<4.7	<2.5	77.5 ± 4.0	
	02 25 18.99	1.18	-02 40 49.11	1.92	С		3.8 ± 0.8	<8.5	< 5.0	151.8 ± 13.1	
J0225.3-0354	02 25 19.85	1.06	-03 54 40.17	1.75	S	22.3 ± 2.3	22.3 ± 2.3	<2.0	<1.8	49.9 ± 11.2	-1.06
J0225.4-0327	02 25 21.76	1.14	-03 27 54.00	1.83	S	2.7 ± 0.6	2.7 ± 0.6	<6.5	<5.3	157.7 ± 39.6	< 0.08
J0225.4-0349	02 25 25.19	1.29	-03 49 26.68	1.84	S	2.7 ± 0.6	2.7 ± 0.6	<7.6	<6.6	100.7 ± 55.2	< 0.07
J0225.4-0248*	02 25 25.71	1.06	-02 48 14.60	1.75	М	60.0 ± 4.3	35.0 ± 3.6	<1.9	<1.8	57.7 ± 13.9	-0.82
	02 25 26.57	1.07	-02 48 16.52	1.76	С		12.8 ± 1.5	<3.3	<2.7	177.5 ± 13.2	

C.	Tasse et al.:	The l	low-freauencv	counterpart	t of the XMN	A large scale	structure survey	1. Online	Material	p 17	7
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Table A.1. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Type	S_{int}	$S_{\rm comp}$	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec	21	mJv	mJv	arcsec	arcsec	Angle	index α_{225}^{1400}
	02 25 26.33	1.09	-02 48 16.74	1.89	С	- 5	12.2 ± 1.8	9.1 ± 4.3	<3.7	12.3 ± 4.3	325
J0225.5-0524	02 25 26.97	1.18	-05 24 56.60	1.82	Š	3.8 ± 0.8	3.8 ± 0.8	<7.1	<4.7	45.7 ± 17.3	<-0.16
10225 5-0538	02 25 27 69	1.10	-05 38 56 21	2.07	S	48 ± 10	48 ± 10	<10.5	<5.2	151.9 ± 8.1	<-0.32
10225 5-0513	02 25 27.05	1.12	$-05\ 13\ 43\ 94$	1 79	S	54 ± 0.8	54 ± 0.8	< 5.6	<4.5	368 + 216	<-0.40
J0225.5-0536	02 25 28.52	1.11	-05 36 56.64	1.77	ŝ	6.4 ± 1.0	6.4 ± 1.0	<5.2	<3.2	55.5 ± 8.9	-0.58
10225 5-0439	02 25 30 22	1.18	-04 39 35 37	1.89	Š	3.1 ± 0.6	3.1 ± 0.6	<7.5	<6.2	3.8 + 38.9	<-0.03
10225 6-0210*	02 25 34 16	1.06	-02 10 18 59	1.75	Š	790.6 + 79.1	790.6 + 79.1	1.0 ± 0.3	< 0.7	20.8 ± 10.4	-0.39
10225 6-0306	02 25 34 98	1.09	-03.06.27.17	1.80	м	26.6 ± 2.1	13.0 ± 1.7	8.6 ± 2.8	<3.6	1544 + 51	-0.84
0022010 0000	02 25 34 41	1.08	-03.06.16.92	1.78	C	2010 2 211	7.0 ± 0.9	<4.6	< 3.8	173.1 + 18.4	0.01
	02 25 35 45	1.00	-03 06 35 82	1.82	Č		34 ± 0.7	<62	<5.4	354 + 552	
	02 25 35 37	1.37	-03.06.33.05	1.95	Ĉ		3.1 ± 0.6	<10.4	< 3.5	45.4 + 3.9	
10225 6-0502	02 25 35.03	1.15	-05 02 09 51	1.99	M	21.0 ± 2.7	174 ± 26	123 + 39	70 + 28	165 ± 112	-0.57
30223.0 0302	02 25 35.05	1.15	-05 02 16 70	1.84	C	21.0 ± 2.7	36 ± 0.6	<72	<40	144.3 ± 9.1	0.57
10225 6-0421	02 25 34.00	1.15	$-04\ 21\ 43\ 10$	1.86	S	24 ± 05	2.0 ± 0.0 2 4 + 0 5	<7.0	<5.2	163.0 ± 25.3	< 0.14
10225.6-0512	02 25 36 46	1 11	-05 12 59 31	1.00	S	7.4 ± 0.5 7.8 ± 1.0	78 ± 10	<49	<2.9	83.0 ± 5.2	<-0.65
10225.6-0500	02 25 36 48	1.07	$-05\ 00\ 11\ 27$	1.76	S	243 ± 27	243 + 27	57 + 13	36 ± 14	48.7 ± 12.2	-0.51
10225.6-0406	02 25 30.40	1.07	-04 06 50 25	1.75	M	24.5 ± 2.7 30.5 ± 2.2	15.7 ± 1.7	-26	2.0 ± 1.4	555 ± 51	_0.82
J0225.0-0400	02 25 37.38	1.00	-04 06 20 40	1.75	C	50.5 ± 2.2	15.7 ± 1.7 7.6 ± 0.0	<2.0	<2.1	33.3 ± 3.1	-0.82
	02 25 39.17	1.00	-04 06 29.49	1.70	C		7.0 ± 0.9 7.1 ± 1.0	82 ± 52	<2.8	47.0 ± 13.7 73.1 \pm 2.3	
10225 7-0604	02 25 37.77	1.32	-04 00 40.33	2.00	s	88+18	7.1 ± 1.0 8.8 ± 1.8	13.0 ± 6.0	<4.5	$1/0 / \pm 1/1$	< -0.74
J0225.7-0004	02 25 39.35	1.23	-00.04 57.04 -04.17 56.17	1.78	S	6.0 ± 0.8	6.0 ± 0.8	13.0 ± 0.0 ∠5.0	<3.0	363 ± 13.6	_0.39
10225.7-0417	02 25 40.00	1.10	-04 17 30.17	1.70	S	0.0 ± 0.0	0.0 ± 0.0	<7.6	<3.4	30.3 ± 15.0 151 2 \pm 5 0	-0.39
10225.7-0555	02 25 40.25	1.15	-03 33 31.78	1.07	S	3.4 ± 1.0 8.4 ± 1.4	3.4 ± 1.0	<7.0	<1.0	101.2 ± 0.9	< 0.70
J0225.7-0210	02 23 42.00	1.12	-02 10 00.75	1.//	S	0.4 ± 1.4	0.4 ± 1.4	< 3.2	<4.0	105.0 ± 25.0	<-0.70
J0225.7-0402	02 23 42.70	1.12	-04 02 38.37	1.00	5	5.2 ± 0.0	3.2 ± 0.0	< 3.4	< 5.0	-1.0 ± 70.5	<-0.04
J0225.7-0230	02 25 43.24	1.10	-02 30 05.92	1.82	S	4.6 ± 0.9	4.0 ± 0.9	< 0.2	<4.5	$1/9.3 \pm 19.7$	-0.34
J0225.7-0319	02 25 43.86	1.07	-03 19 35.00	1.70	5	9.5 ± 1.1	9.5 ± 1.1	<3.2	<2.7	25.0 ± 15.5	-0.77
J0225.7-0311	02 25 43.93	1.28	-03 11 03.86	1.82	M	9.3 ± 1.1	4.7 ± 0.8	1.2 ± 5.6	<4.8	60.8 ± 9.4	-0.50
10005 5 0(04	02 25 45.14	1.17	-03 11 01.62	1.79	C	70 00	4.6 ± 0.8	<6.5	<4.4	56.3 ± 13.6	0.50
J0225.7-0604	02 25 44.18	1.08	-06 04 25.64	1.85	M	7.0 ± 0.8	4.1 ± 0.6	<6.7	<3.6	2.9 ± 6.2	<-0.58
10005 7 0016	02 25 45.65	1.15	-06 04 31.18	1.88	C	11 7 1 2	2.9 ± 0.5	<8.2	<2.8	$14/.3 \pm 3.3$	0.46
J0225.7-0316	02 25 44.19	1.07	-03 16 32.46	1.76	3	11.7 ± 1.3	11.7 ± 1.3	<3.5	<2.8	19.2 ± 8.9	-0.46
J0225.8-0505	02 25 45.38	1.11	-05 05 47.68	1.80	S	4.0 ± 0.7	4.0 ± 0.7	<5.6	<4.8	$1/0.4 \pm 40.0$	<-0.20
J0225.8-0415	02 25 45.76	1.12	-04 15 27.80	1.77	S	5.5 ± 0.8	5.5 ± 0.8	4.0 ± 3.6	<4.2	75.8 ± 19.1	-0.56
J0225.8-0226	02 25 47.59	1.09	-02 26 28.69	1.77	M	14.1 ± 1.5	8.8 ± 1.2	<4.3	<3.8	49.5 ± 29.3	-0.82
	02 25 48.36	1.17	-02 25 54.39	1.79	С		5.3 ± 0.9	<6.3	<4.5	63.5 ± 17.7	
J0225.8-0258	02 25 47.76	1.24	-02 58 18.49	1.91	М	$78.2 \pm 16.1^*$	14.4 ± 2.5	9.9 ± 4.5	7.8 ± 4.0	163.9 ± 40.9	0.10
	02 25 45.82	1.10	-02 58 04.49	1.77	С		6.4 ± 0.9	<4.8	<3.5	130.9 ± 12.4	
	02 25 48.67	1.18	-02 58 20.54	1.81	С		5.5 ± 0.9	5.5 ± 4.4	<5.6	55.4 ± 34.5	
J0225.8-0341	02 25 48.41	1.12	-03 41 29.08	1.77	S	3.2 ± 0.5	3.2 ± 0.5	<5.2	<4.1	91.4 ± 26.4	<-0.05
J0225.8-0600	02 25 49.63	1.08	-06 00 51.69	1.76	S	17.2 ± 2.1	17.2 ± 2.1	<3.8	<3.6	16.9 ± 46.0	-0.14
J0225.8-0400	02 25 49.77	1.10	-04 00 23.98	1.77	S	4.4 ± 0.7	4.4 ± 0.7	<4.7	<4.1	128.2 ± 38.4	<-0.26
J0225.8-0251	02 25 50.08	1.07	-02 51 46.67	1.76	S	8.2 ± 1.0	8.2 ± 1.0	<3.7	<3.0	46.4 ± 15.1	-0.78
J0225.8-0422	02 25 50.19	1.07	-04 22 19.94	1.75	S	11.8 ± 1.3	11.8 ± 1.3	<2.9	<2.4	40.2 ± 8.4	-0.69
J0225.9-0336	02 25 50.96	1.10	-03 36 32.72	1.76	S	5.1 ± 0.7	5.1 ± 0.7	<4.7	<3.4	58.2 ± 10.6	<-0.36
J0225.9-0500	02 25 52.94	1.13	-05 00 16.72	1.77	M	14.0 ± 1.5	9.4 ± 1.3	6.3 ± 3.1	<3.6	119.2 ± 6.6	-0.53
	02 25 53.52	1.11	-05 00 20.79	1.80	С		4.6 ± 0.8	<5.8	<4.7	24.4 ± 23.5	
J0225.9-0157	02 25 53.19	1.07	-01 57 59.92	1.77	S	10.9 ± 1.5	10.9 ± 1.5	<4.5	<3.3	18.4 ± 11.1	-0.98
J0225.9-0553	02 25 53.76	1.17	-05 53 04.05	1.92	S	14.1 ± 2.4	14.1 ± 2.4	9.7 ± 4.7	<5.9	11.5 ± 16.1	-0.09
J0225.9-0428	02 25 54.78	1.08	-04 28 54.64	1.76	М	23.5 ± 2.0	12.7 ± 1.4	5.1 ± 1.7	<3.1	42.5 ± 9.1	-0.73
	02 25 56.08	1.18	-04 28 48.40	1.78	С		8.1 ± 1.2	7.5 ± 3.4	<4.6	78.0 ± 11.7	
	02 25 55.31	1.14	-04 28 48.48	1.85	С		2.7 ± 0.6	<6.8	<5.5	9.4 ± 38.1	
J0225.9-0545*	02 25 55.35	1.06	-05 45 40.25	1.75	S	117.0 ± 11.8	117.0 ± 11.8	7.6 ± 0.4	1.4 ± 0.8	39.3 ± 1.1	-0.46
J0225.9-0247	02 25 55.90	1.11	-02 47 27.29	1.99	S	3.9 ± 0.7	3.9 ± 0.7	<8.9	<4.9	178.9 ± 8.8	<-0.18
J0225.9-0447	02 25 56.04	1.10	-04 47 22.91	1.76	S	3.6 ± 0.6	3.6 ± 0.6	<4.6	<3.8	73.4 ± 28.7	-0.29
J0225.9-0534	02 25 56.42	1.08	-05 34 49.82	1.78	S	6.0 ± 0.9	6.0 ± 0.9	<5.0	<3.6	3.6 ± 13.2	0.34
J0226.0-0500	02 25 58.79	1.07	-05 00 52.94	1.75	S	10.9 ± 1.2	10.9 ± 1.2	<3.0	<2.6	16.5 ± 15.4	-0.86
J0226.0-0542	02 25 59.43	1.13	-05 42 52.11	1.86	ŝ	4.8 ± 1.0	4.8 ± 1.0	<7.0	<5.2	177.1 ± 24.9	<-0.31
10226.0-0444	02 25 59 56	1.37	-04 44 05 44	1.77	Š	154 ± 2.1	154 + 2.1	164 + 4.5	< 3.9	99.6 ± 2.8	-0.17
10226.0-0222	02 26 00 12	1 10	-02 22 30 03	1 78	ŝ	61 ± 0.9	61 ± 0.9	< 5.5	<36	142.6 ± 11.1	<-0.49
10226.0-0512	02 26 01 30	1.10	$-05\ 12\ 07\ 14$	1.83	S	35 ± 0.8	35 ± 0.8	< 8.4	< 5.5	63.1 ± 16.6	-0.25
10226.1-0429	02 26 03 07	1.02	-04 29 30 33	1.05	S	5.9 ± 0.0	5.9 ± 0.8	<41	<3.1	43.7 ± 13.0	<-0.46
J0226.1-0429	02 26 03 59	1.00	$-04\ 20\ 50.55$	1.70	M	11.0 ± 1.0	3.9 ± 0.0 8.0 ± 1.2	58 ± 31	<3.8	1605 ± 84	0.16
30220.1-0430	02 26 03.37	1.07	-04 31 15 65	1.75	C	11.7 ± 1.4	3.0 ± 0.7	-85	<6.0	100.5 ± 0.4 12.0 ± 41.2	0.10
10226 1 0258	02 26 03.77	1.24	-04 51 15.05	1.95	M	50.08	3.0 ± 0.7	< 6.2	<0.9	12.0 ± 41.2	0.67
JU220.1-0238	02 20 04.07	1.17	-02 50 11.55	2.00	C NI	5.7 ± 0.8	3.0 ± 0.0 28 ± 0.6	<0.5	<4.4 ~5 1	176.0 ± 10.3	-0.07
10226 1 0251	02 20 04.44	1.12	-02 50 12.50	2.09	c c	85110	2.0 ± 0.0 85 1 10	~10.1	>J.1	$1/0.0 \pm 9.3$	< -0.71
10226 1 0201	02 20 03.13	1.00	-02 51 51.08	1.70	с с	0.3 ± 1.0 3 4 ± 0.7	0.3 ± 1.0 3.4 ± 0.7	< 3.9 ~7 0	< 3.1	30.0 ± 11.0 102.2 ± 26.0	<-0./1
JU220.1-U3U1	02 20 03.88	1.30	-03 01 06./1	1.82	3	3.4 ± 0.7	3.4 ± 0.7	< 1.8	< 3.9	102.3 ± 20.8	<-0.09
JU220.1-U233	02 20 00.04	1.07	-02 33 48.33	1.70	ა ი	10.0 ± 1.8	10.0 ± 1.8	< 3.1	<2.8	2.4 ± 18.0	-0.55
JU220.1-0416	02 20 00.50	1.28	-04 10 32.05	1.82	3	2.8 ± 0.0	2.8 ± 0.0	<1.1	<3./	10.4 ± 25.7	< 0.04
J0226.1-0532	02 26 06.91	1.06	-05 32 16.75	1.75	3	40.9 ± 4.8	40.9 ± 4.8	2.4 ± 0.8	<1./	30.0 ± 6.0	-0.07
JU226.1-0235	02 26 08.12	1.06	-02 35 15.97	1.75	S	21.6 ± 2.3	21.6 ± 2.3	<2.3	<2.1	35.1 ± 11.3	-0.48
J0226.2-0433	02 26 09.09	1.06	-04 33 35.92	1.75	S	26.4 ± 2.7	26.4 ± 2.7	<2.0	<1.9	167.2 ± 9.4	-0.90
J0226.2-0212	02 26 09.90	1.15	-02 12 23.68	1.91	S	4.8 ± 1.0	4.8 ± 1.0	< 7.8	<5.7	$1/9.3 \pm 24.0$	<-0.33
J0226.2-0204	02 26 11.25	1.09	-02 04 07.44	1.80	S	7.2 ± 1.2	7.2 ± 1.2	<5.7	<4.0	5.6 ± 14.1	<-0.60

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Table A.1. continued.

Name	RA	σ_{α}	Dec	σ_s	Type	Sint	Scomp	Major axis	Minor axis	Position	Spectral
Tunie	J2000	arcsec	J2000	arcsec	Type	mJy	mJy	arcsec	arcsec	Angle	index α_{225}^{1400}
J0226.2-0505	02 26 11.35	1.16	-05 05 03.85	1.77	М	10.4 ± 1.1	5.2 ± 0.8	<6.1	<3.3	65.4 ± 6.2	<-0.85
	02 26 11.31	1.08	-05 05 06.99	1.76	С		5.2 ± 0.7	<4.0	<3.6	118.0 ± 42.9	
J0226.2-0403	02 26 12.67	1.07	-04 03 19.84	1.76	S	8.4 ± 1.0	8.4 ± 1.0	<3.4	<3.0	53.3 ± 23.1	-0.74
J0226.2-0307	02 26 14.39	1.07	-03 07 55.42	1.75	S	13.3 ± 1.4	13.3 ± 1.4	<2.7	<2.3	59.5 ± 10.5	-0.44
J0226.3-0422	02 26 15.20	1.06	-04 22 34.64	1.75	M	34.5 ± 2.8	21.1 ± 2.2 12.4 + 1.7	<2.3	<2.2	112.1 ± 20.4	-0.84
10226 3-0219	02 26 15.55	1.15	$-04\ 22\ 50.75$ $-02\ 19\ 49\ 54$	1.79	S	50 ± 10	13.4 ± 1.7 50 + 10	9.3 ± 3.1	< 5.0	46.5 ± 2.9 39 3 + 28 0	-0.15
J0226.3-0504	02 26 17.39	1.06	$-05\ 04\ 41.90$	1.75	S	17.1 ± 1.8	17.1 ± 1.8	<2.6	<2.4	17.5 ± 16.7	-0.52
J0226.3-0400*	02 26 19.09	1.12	-04 00 15.04	1.78	\tilde{M}	132.7 ± 10.9	91.5 ± 9.9	22.1 ± 2.2	9.5 ± 1.1	127.8 ± 2.0	-0.28
	02 26 18.48	1.39	-03 59 26.41	2.09	С		19.3 ± 3.7	15.4 ± 6.5	9.1 ± 4.5	30.2 ± 15.7	
	02 26 18.58	1.18	-04 00 07.09	1.84	С		14.4 ± 2.0	11.3 ± 4.2	<3.2	138.1 ± 2.7	
T0004 0 0000	02 26 17.23	1.23	-03 59 33.04	2.03	С		7.6 ± 1.6	9.2 ± 6.5	<6.9	173.5 ± 20.6	0.67
J0226.3-0203	02 26 19.53	1.06	-02 03 50.36	1.75	S	23.2 ± 2.5	23.2 ± 2.5	<2.5	<2.2	60.5 ± 14.4	-0.65
J0220.3-0423*	02 26 19.75	1.00	$-04\ 25\ 31.89$ $-04\ 25\ 39\ 46$	1.75	M C	115.1 ± 8.2	60.1 ± 0.1	4.2 ± 0.5 3.4 ± 0.5	3.2 ± 0.0 1.4 ± 1.0	54.5 ± 11.0 163.8 ± 6.8	-0.75
J0226.4-0554	02 26 21.03	1.14	$-05\ 55\ 01.50$	1.75	S	5.1 ± 0.9	5.1 ± 0.9	<5.5	<3.9	99.5 ± 18.9	<-0.36
J0226.4-0557	02 26 25.89	1.14	-05 57 10.90	1.82	ŝ	5.0 ± 1.0	5.0 ± 1.0	<6.3	<5.0	30.9 ± 34.1	<-0.35
J0226.5-0332	02 26 27.08	1.10	-03 33 00.82	1.76	S	7.4 ± 0.9	7.4 ± 0.9	<4.5	<3.1	84.8 ± 7.3	<-0.62
J0226.5-0601	02 26 29.20	1.13	-06 01 38.77	1.83	S	6.4 ± 1.2	6.4 ± 1.2	<6.4	<5.2	17.9 ± 33.9	<-0.52
J0226.5-0454	02 26 30.19	1.18	-04 54 34.23	1.81	S	3.6 ± 0.7	3.6 ± 0.7	<6.7	<4.9	52.9 ± 20.7	<-0.12
J0226.5-0513	02 26 32.53	1.06	-05 13 28.26	1.75	S	168.3 ± 16.9	168.3 ± 16.9	2.0 ± 0.3	<1.0	23.5 ± 4.0	-0.48
J0226.6-0253	02 26 32.93	1.10	-02 53 58.68	1.//	5	4.3 ± 0.7	4.3 ± 0.7	< 5.8	<4.4	93.4 ± 19.3	-0.22
10226.6-0422	02 26 33.02	1.08	$-03\ 13\ 34.03$ $-04\ 22\ 19\ 12$	1.77	S	4.3 ± 0.7 25 ± 0.6	4.3 ± 0.7 25 ± 0.6	<4.0	 < 5.5	 10.7 + 16.5	0.45
J0226.6-0414	02 26 34.09	1.07	-04 14 35.94	1.75	S	9.4 ± 1.1	9.4 ± 1.1	<3.2	<2.6	47.2 ± 11.5	-0.44
J0226.6-0411	02 26 35.02	1.12	-04 11 26.25	1.80	Ŝ	3.7 ± 0.6	3.7 ± 0.6	<5.4	<5.0	-1.0 ± 82.6	<-0.14
J0226.6-0512	02 26 35.21	1.19	-05 12 14.60	1.86	S	4.5 ± 0.9	4.5 ± 0.9	<7.9	<4.7	140.7 ± 12.0	<-0.27
J0226.6-0432	02 26 35.87	1.12	-04 32 27.58	1.82	S	3.7 ± 0.6	3.7 ± 0.6	<6.0	<5.0	172.1 ± 30.3	-0.41
J0226.6-0602	02 26 37.35	1.08	-06 02 13.87	1.77	S	18.1 ± 2.2	18.1 ± 2.2	<4.2	<3.1	31.2 ± 7.7	-0.41
J0226.6-0407	02 26 37.43	1.06	-04 07 59.43	1.75	S	12.4 ± 1.3	12.4 ± 1.3	<2.7	<2.3	12.4 ± 11.0	-0.37
J0220.0-0545	02 26 37.44	1.29	-05 45 15.90 -04 12 46 32	2.21	S S	10.0 ± 1.9 3.4 ± 0.6	10.0 ± 1.9 3.4 ± 0.6	<12.2	< 3.5	152.1 ± 2.9 31.7 \pm 10.7	<-0.82
10226.6-0412	02 20 37.84	1.12	$-04\ 12\ 40.32$ $-05\ 00\ 36\ 12$	2 10	S	3.4 ± 0.0 7.6 + 1.6	3.4 ± 0.0 7.6 + 1.6	(0.5)	<4.0 <6.6	31.7 ± 10.7 12.8 ± 13.3	-0.24
J0226.7-0501	02 26 38.92	1.25	$-05\ 01\ 55.26$	2.39	Š	12.6 ± 2.3	12.6 ± 2.3	20.7 ± 8.4	<5.9	12.0 ± 19.9 17.0 ± 4.9	-0.48
J0226.7-0552*	02 26 40.02	1.06	-05 52 36.80	1.75	S	132.0 ± 13.3	132.0 ± 13.3	4.6 ± 0.4	1.9 ± 0.6	41.8 ± 3.3	-0.11
J0226.7-0320	02 26 40.94	1.09	-03 20 06.81	1.77	S	6.1 ± 0.8	6.1 ± 0.8	<4.6	<4.0	46.8 ± 25.4	-0.59
J0226.7-0334	02 26 41.68	1.24	-03 34 24.09	1.79	S	2.7 ± 0.6	2.7 ± 0.6	<7.3	<4.8	108.9 ± 16.7	< 0.07
J0226.7-0446	02 26 42.23	1.09	-04 46 25.98	1.78	М	9.6 ± 1.1	6.8 ± 0.9	4.6 ± 2.9	<4.1	0.2 ± 18.1	-0.47
10226 7 0157	02 26 40.46	1.18	-04 46 07.12	1.89	C	710 + 75	2.8 ± 0.6	.9</td <td>< 5.3</td> <td>29.7 ± 19.1</td> <td>0.19</td>	< 5.3	29.7 ± 19.1	0.19
J0220.7-0137	02 26 42.03	1.08	-01 57 52.30 -01 57 40 31	2.15	M C	71.0 ± 7.3	31.2 ± 5.0 30.9 ± 6.3	0.4 ± 1.9 13.0 ± 6.6	< 3.1 101 + 53	54.5 ± 0.2 11 ± 20.4	-0.18
	02 26 42.14	1.21	-015740.27	1.82	C		9.0 ± 1.6	<6.8	<6.1	107.3 ± 61.8	
J0226.7-0323	02 26 43.98	1.12	-03 23 55.08	1.79	Š	5.0 ± 0.8	5.0 ± 0.8	<5.2			-0.13
J0226.7-0206	02 26 44.72	1.10	-02 06 15.78	1.91	S	6.1 ± 1.1	6.1 ± 1.1	<7.9	<4.6	7.5 ± 9.6	-0.23
J0226.8-0230	02 26 45.81	1.08	-02 30 28.27	1.77	S	4.0 ± 0.6	4.0 ± 0.6	<4.4	<3.7	0.7 ± 36.0	<-0.20
J0226.8-0249	02 26 45.91	1.07	-02 49 51.75	1.76	S	10.0 ± 1.1	10.0 ± 1.1	<3.4	<3.1	80.4 ± 24.4	-0.79
J0226.8-0223	02 26 47.27	1.20	-02 23 35.55	1.85	S	4.0 ± 0.8	4.0 ± 0.8	<7.5	<5.3	43.7 ± 20.8	<-0.20
J0220.8-0411	02 26 49.11	1.19	$-04\ 11\ 13.13$ $-04\ 11\ 10\ 62$	1.80	M C	0.3 ± 0.7	3.4 ± 0.0 2.0 ± 0.5	<7.2	<2.9	52.1 ± 4.0 57.2 ± 0.0	-0.00
10226 8-0232	02 26 50 13	1.15	-02322452	1.77	S	285 ± 29	2.9 ± 0.3 28 5 + 2 9	<23	<1.8	37.2 ± 9.0 48 5 + 3 4	-1.03
J0226.8-0252	02 26 50.13	1.14	-025752.08	1.78	Š	3.5 ± 0.6	3.5 ± 0.6	<5.7	<4.6	107.1 ± 32.2	<-0.10
J0226.8-0351	02 26 50.37	1.62	-03 51 29.93	1.82	S	5.8 ± 1.2	5.8 ± 1.2	<10.9	<4.8	71.7 ± 6.4	<-0.45
J0226.8-0255	02 26 50.37	1.15	-02 55 26.52	1.83	S	3.0 ± 0.6	3.0 ± 0.6	<6.4	<5.6	-1.0 ± 66.9	<-0.00
J0226.9-0359	02 26 52.20	1.08	-03 59 21.65	1.77	S	7.1 ± 0.9	7.1 ± 0.9	<4.3	<3.6	39.5 ± 17.5	-0.57
J0226.9-0431	02 26 52.42	1.10	-04 31 46.22	1.78	S M	4.8 ± 0.7	4.8 ± 0.7	<5.3	<4.1	141.8 ± 15.7	-0.47
JU220.9-0301	02 20 33.41	1.08	-03 01 43.09 -03 01 47 60	1.//	M C	0.0 ± 0.8	4.3 ± 0.0 38 ± 0.6	<4.3 <1 /	< 3.3	23.1 ± 14.0 47.1 ± 19.1	-0.85
10226 9-0418	02 20 55.55	1.08	-03 01 47.09	1.70	S	2.5 ± 0.6	3.0 ± 0.0 2.5 + 0.6	< 4.4 <7.2	< 5.5 < 6.1	$+7.1 \pm 10.1$ 78.2 + 50.7	< 0.12
J0226.9-0305	02 26 55.75	1.14	$-03\ 05\ 34.68$	1.81	S	3.3 ± 0.6	3.3 ± 0.6	<6.4	<4.6	39.8 ± 20.5	<-0.06
J0226.9-0542	02 26 55.84	1.27	-05 42 41.94	1.81	S	8.4 ± 1.5	8.4 ± 1.5	7.1 ± 5.0	<5.6	70.3 ± 18.2	-0.97
J0226.9-0403	02 26 56.32	1.13	-04 03 26.40	1.85	S	3.1 ± 0.6	3.1 ± 0.6	<7.1	<4.9	156.6 ± 16.9	<-0.01
J0227.0-0223*	02 26 57.37	1.06	-02 24 01.78	1.75	M	42.1 ± 3.5	27.0 ± 2.8	2.4 ± 1.4	<2.2	101.2 ± 8.7	-0.60
	02 26 56.29	1.18	-02 23 40.35	2.03	C		9.7 ± 1.9	10.0 ± 6.4	<5.4	161.0 ± 8.7	
10007 0 0007	02 26 56.79	1.09	-02 23 50.19	1.79	C	64.00	5.3 ± 0.9	<5.2	<4.0	4.4 ± 20.3	0.60
JU227.0-0337	02 20 38.90	1.09	-055/40.24 -05005242	1.//	5 5	0.4 ± 0.9	0.4 ± 0.9 4.7 ± 0.7	<4.4	<4.2 ~3 7	-1.0 ± 82.1 0.0 + 26.2	-0.69
I0227.0-0500	02 26 59 33	1.06	-05 55 48 43	1.75	M	4.7 ± 0.7 1017.2 + 67.7	4.7 ± 0.7 506 4 + 51 0	19.1 ± 0.7	<13	0.9 ± 20.2 150.1 + 0.3	-0.93
30221.0 0333	02 26 59.15	1.06	$-05\ 55\ 40.42$	1.75	C	1017.2 ± 07.7	442.1 ± 44.3	3.2 ± 0.2	<1.0	42.2 ± 1.9	0.75
	02 26 59.32	1.06	-05 55 34.50	1.76	Ċ		18.5 ± 2.2	<3.2	<1.9	171.1 ± 4.8	
	02 26 59.51	1.09	-05 55 34.48	1.86	С		16.9 ± 2.6	<7.2	<3.0	159.4 ± 3.7	
	02 26 59.68	1.07	-05 55 45.18	1.77	С		16.8 ± 2.3	<4.3	<2.8	6.1 ± 9.3	
10000 0 0000	02 26 59.79	1.09	-05 55 48.51	1.75	C		16.5 ± 2.3	<4.3	<2.9	98.0 ± 9.5	0.05
J0227.0-0228	02 26 59.60	1.15	-02 28 15.75	1.83	S	5.2 ± 1.0	5.2 ± 1.0	< 6.3	<5.6	14.7 ± 50.9	-0.06
JU227.0-0328	02 20 39.67	1.06	-03 28 20.66	1.75	M	33.8 ± 3.8	21.1 ± 2.9	4.1 ± 0.9	<1.9	44.8 ± 3.2	-0.73

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Table A.1. continued.

Name	RA	σ_{c}	Dec	σ_s	Type	Sint	Scome	Maior axis	Minor axis	Position	Spectral
1 vanie	J2000	arcsec	J2000	arcsec	1,100	mJy	mJy	arcsec	arcsec	Angle	index α_{225}^{1400}
	02 26 58.77	1.06	-03 28 48.46	1.75	С	,	22.6 ± 2.4	4.5 ± 1.1	<2.1	32.4 ± 3.1	343
	02 26 59.33	1.08	-03 28 27.12	1.77	С		5.5 ± 0.7	<4.7	<2.9	151.3 ± 6.9	
J0227.0-0539	02 27 00.29	1.52	-05 39 53.21	1.89	S	5.4 ± 1.2	5.4 ± 1.2	<10.3	<6.4	63.9 ± 15.2	0.29
J0227.0-0541	02 27 00.93	1.06	-05 41 49.95	1.75	S	36.8 ± 3.9	36.8 ± 3.9	3.3 ± 1.2	<2.5	13.2 ± 12.7	-0.79
J0227.1-0423 J0227.1-0543	02 27 04.18	1.17	$-04\ 25\ 38.20$ $-05\ 43\ 41\ 29$	1.80	S	2.8 ± 0.3 60 + 13	2.8 ± 0.3 60 + 13	<10.7	<4.2	37.3 ± 8.7 78.0 + 11.0	< 0.04
J0227.1-0221	02 27 08.21	1.43	$-02\ 21\ 21.40$	1.88	S	4.5 ± 1.0	4.5 ± 1.0	<9.6	<6.0	120.6 ± 14.8	<-0.28
J0227.1-0320	02 27 08.81	1.38	-03 20 49.56	2.00	S	7.2 ± 1.6	7.2 ± 1.6	9.5 ± 7.1	<7.0	40.7 ± 18.5	-0.07
J0227.2-0259	02 27 10.94	1.14	-02 59 10.95	1.87	S	4.7 ± 0.8	4.7 ± 0.8	6.6 ± 5.4	<4.2	152.1 ± 7.1	<-0.31
J0227.2-0418	02 27 12.61	1.13	-04 18 17.15	1.76	М	6.8 ± 0.7	3.6 ± 0.5	<5.4	<2.9	81.0 ± 6.1	<-0.56
	02 27 12.63	1.10	-04 18 19.96	1.76	С		3.2 ± 0.5	<4.6	<2.7	68.2 ± 7.0	
J0227.2-0446	02 27 12.94	1.07	-04 46 35.37	1.75	S	12.4 ± 1.4	12.4 ± 1.4	<3.1	<2.7	46.4 ± 13.6	-0.20
J0227.2-0312	02 27 13.30	1.13	-03 12 45.99	1.78	S	5.4 ± 0.9	5.4 ± 0.9	< 5.4	<4.9	$108.4 \pm 5/.1$	<-0.40
J0227.2-0411 J0227 3-0549	02 27 14.10	1.13	$-04\ 11\ 28.40$ $-05\ 49\ 58\ 20$	1.95	S	2.0 ± 0.0 6 3 + 1 4	2.0 ± 0.0 63 + 14	< 7.5	<5.9	171.0 ± 10.3 80.8 + 34.3	< 0.09 -0.48
J0227.3-0257	02 27 16.12	1.14	-025734.73	1.76	M	9.2 ± 1.0	5.6 ± 0.8	<5.6	<2.6	76.5 ± 4.0	<-0.76
	02 27 16.11	1.26	-02 57 32.00	1.75	С	,	3.6 ± 0.6	<7.3	<2.6	83.7 ± 3.4	
J0227.2-0325*	02 27 16.28	1.17	-03 25 36.66	1.77	М	$195.8 \pm 24.1^{*}$	24.3 ± 3.1	10.6 ± 2.9	<3.9	68.5 ± 5.1	-0.20
	02 27 15.51	1.24	-03 25 37.70	2.69	С		8.4 ± 2.3	<15.2	<5.8	12.7 ± 7.2	
	02 27 15.86	1.66	-03 25 43.30	2.41	С		4.0 ± 1.0	<14.9	<5.7	143.0 ± 7.0	
	02 27 08.89	1.42	-03 25 58.35	2.16	M		32.7 ± 6.2	16.6 ± 6.6	11.9 ± 5.0	14.6 ± 23.6	-0.20
	02 27 08.02	1.10	$-03\ 26\ 00.32$	1.//	C		22.3 ± 2.7	0.7 ± 2.1	<3./	53.3 ± 9.8	
10227 3-0341	02 27 08.40	1.98	$-03\ 23\ 43.81$ $-03\ 41\ 07\ 77$	1.75	S	38.1 ± 4.0	9.7 ± 2.0 38.1 ± 4.0	13.2 ± 10.4 83 + 10	< 9.5	916 ± 17	-0.65
J0227.3-0341	02 27 17.00	1.16	-03 11 28.34	1.78	S	4.7 ± 0.8	4.7 ± 0.8	<6.0	<4.3	69.4 ± 15.4	<-0.30
J0227.3-0330	02 27 20.51	1.06	-03 30 36.65	1.75	S	14.4 ± 1.5	14.4 ± 1.5	<2.7	<2.3	44.9 ± 12.2	-1.29
J0227.3-0445	02 27 20.67	1.11	-04 45 35.40	1.79	S	5.3 ± 0.8	5.3 ± 0.8	<5.3	<4.8	28.7 ± 45.8	<-0.39
J0227.4-0341	02 27 22.42	1.12	-03 41 22.27	1.77	S	5.3 ± 0.8	5.3 ± 0.8	<5.4	<3.9	59.7 ± 14.0	-0.51
J0227.4-0433	02 27 22.73	1.10	-04 33 50.03	1.78	S	6.4 ± 0.9	6.4 ± 0.9	<5.0	<4.3	35.6 ± 25.9	<-0.52
J0227.4-0240*	02 27 22.89	1.08	-02 39 53.10	1.76	M	119.7 ± 7.2	43.1 ± 4.6	9.8 ± 1.3	<2.5	116.3 ± 2.4	-0.76
	02 27 26.52	1.00	$-02\ 40\ 19.50$ $-02\ 40\ 18\ 91$	1.75	C		35.4 ± 3.0 22.4 ± 3.3	< 2.3 25.3 \pm 10.4	<2.1	78.4 ± 12.0	
	02 27 25.94	1.04	-024018.91 -02401822	2.30	C		22.4 ± 3.3 187 + 26	23.3 ± 10.4 113 + 35	< 2.0 45+27	43.1 ± 0.8 105.6 ± 7.4	
J0227.4-0512	02 27 23.02	1.41	$-05\ 12\ 38.29$	2.00	S	3.6 ± 0.8	3.6 ± 0.8	<9.9	<7.6	41.9 ± 29.4	-0.10
J0227.4-0254	02 27 23.36	1.07	-02 54 24.53	1.75	\tilde{M}	21.6 ± 1.7	11.8 ± 1.3	<3.0	<1.8	80.0 ± 3.2	-1.05
	02 27 23.37	1.07	-02 54 27.49	1.75	С		9.9 ± 1.1	<3.5	<1.7	71.7 ± 2.2	
J0227.4-0241	02 27 23.37	1.10	-02 41 39.35	1.75	S	7.0 ± 0.8	7.0 ± 0.8	<4.4	<1.6	92.1 ± 1.7	<-0.58
J0227.4-0223	02 27 25.41	1.07	-02 23 49.50	1.75	M	22.9 ± 2.1	16.2 ± 1.8	<3.1	<2.8	44.6 ± 23.1	-0.64
10227 4 0528	02 27 24.85	1.10	$-02\ 23\ 33.07$	1.78	C	44 + 10	6.6 ± 1.0	<5.0	<3.9	41.5 ± 21.1	< 0.25
J0227.4-0538 I0227.5-0437*	02 27 20.87	1.22	$-05\ 38\ 43.83$ $-04\ 37\ 33\ 65$	1.92	S M	4.4 ± 1.0 673 + 65	4.4 ± 1.0 64.1 ± 6.4	< 8.4 28 + 0.4	< 0.2	151.1 ± 20.7 176.6 ± 6.6	<-0.25
J0227.5-0457*	02 27 27.83	1.14	-043735.03 -043726.76	1.94	C	07.5 ± 0.5	3.3 ± 0.7	2.8 ± 0.4 <8.3	<5.1	170.0 ± 0.0 165.6 ± 13.5	-0.80
J0227.5-0403	02 27 28.01	1.06	-04 03 38.84	1.75	M	23.6 ± 1.8	13.3 ± 1.4	<3.0	<2.5	159.2 ± 8.8	-1.20
	02 27 28.50	1.08	-04 03 46.45	1.76	С		7.2 ± 0.9	<3.7	<3.1	47.5 ± 16.0	
	02 27 28.54	1.13	-04 03 49.39	1.77	С		3.0 ± 0.5	<5.6	<3.3	64.7 ± 9.5	
J0227.5-0402	02 27 30.38	1.10	-04 02 17.54	1.79	S	5.1 ± 0.8	5.1 ± 0.8	<5.3	<4.3	10.7 ± 21.1	-0.63
J0227.5-0519	02 27 31.17	1.11	-05 19 15.00	1.78	S	7.1 ± 1.0	7.1 ± 1.0	<5.5	<3.8	45.4 ± 9.4	-0.26
J0227.5-0524	02 27 31.86	1.29	-05 24 11.32	1.83	S	3.8 ± 0.8	3.8 ± 0.8	<8.0	<5.8	115.9 ± 22.8	<-0.17
J0227.5-0201 J0227 5-0327	02 27 31.93	1.40	$-02\ 01\ 48.13$ $-03\ 27\ 35\ 30$	1.92	S	11.2 ± 2.2 4.4 ± 0.8	11.2 ± 2.2 4.4 ± 0.8	9.0 ± 7.0	< 3.0	53.4 ± 0.7 57.6 + 29.0	0.90
J0227.5-0557*	02 27 32.95	1.07	$-05\ 57\ 47.96$	1.76	M	114.4 ± 7.9	36.7 ± 4.0	3.6 ± 1.7	<2.8	21.1 ± 9.6	-0.39
	02 27 31.75	1.23	-05 57 48.65	1.79	С		30.7 ± 4.3	11.5 ± 3.6	4.9 ± 2.6	107.1 ± 7.6	
	02 27 30.78	1.46	-05 57 49.00	1.81	С		25.9 ± 4.3	14.0 ± 5.3	5.4 ± 3.5	97.2 ± 8.1	
	02 27 32.65	1.08	-05 57 45.42	1.82	С		21.1 ± 3.0	6.3 ± 3.5	<3.8	0.7 ± 7.5	
J0227.6-0433	02 27 33.93	1.14	-04 33 12.90	1.78	S	4.2 ± 0.7	4.2 ± 0.7	<5.9	<4.2	55.7 ± 16.6	-0.09
J0227.6-0456	02 27 34.37	1.06	-04 56 49.31	2.04	M	11.5 ± 1.1	8.4 ± 0.9	9.5 ± 6.4	<0.4	179.7 ± 0.0	<-0.92
10227 6 0425	02 27 34.04	1.31	-04 56 52.42	1.99	C	48 + 07	3.1 ± 0.7	<10.3	<4.3	38.7 ± 5.9	< 0.22
10227.6-0433	02 27 35.47	1.11	$-04\ 35\ 35.13$ $-03\ 14\ 37\ 39$	1.77	S M	4.0 ± 0.7 837+66	4.0 ± 0.7 62.5 ± 6.3	42 ± 05	<4.2	71.0 ± 39.0 32.4 ± 1.3	<-0.35 -1.14
30227.0 0314	02 27 35.67	1.06	$-03\ 14\ 37.98$	1.75	C	05.7 ± 0.0	17.5 ± 1.8	<2.1	<0.4	87.8 ± 0.1	1.14
	02 27 32.84	1.55	-03 14 55.51	1.86	Ĉ		3.7 ± 0.8	<10.2	<6.2	109.0 ± 13.7	
J0227.5-0411	02 27 37.23	1.07	-04 11 06.70	1.76	М	46.3 ± 2.8	10.8 ± 1.2	<3.5	<3.1	150.7 ± 18.3	-0.93
	02 27 36.86	1.09	-04 11 07.33	1.87	С		10.8 ± 1.6	10.2 ± 3.8	<4.3	176.3 ± 6.2	
	02 27 34.18	1.12	-04 11 40.36	1.80	С		9.3 ± 1.3	7.3 ± 3.3	<4.3	39.2 ± 9.9	
	02 27 30.48	1.07	-04 11 17.13	1.76	C		8.8 ± 1.0	<3.5	<3.2	16.0 ± 27.2	
	02 27 33.87	1.25	-04 11 43.36	1.89	C		3.3 ± 0.7	<8.7	<4.6	137.7 ± 8.9	
10227 7- 0254	02 27 30.43	1.15	-04 11 08.76 -02 54 02 71	1.88	C c	47 ± 0.0	3.3 ± 0.7	<1.3	<3.8 <5.2	4.4 ± 31.1 72 0 ± 12 0	_0.44
J0227.7-0254 J0227.7-0502	02 27 43.00	1.55	-02 34 02.71	1.01	5	$+.7 \pm 0.9$ 24.0 + 2.5	4.7 ± 0.9 24.0 + 2.5	< 0.3 36 + 11	< 3.2	12.7 ± 12.0 138 1 + 10 5	-0.44
J0227.7-0250*	02 27 44 16	1.06	-0250250.90	1.75	M	137.7 ± 11.5	112.0 ± 11.2	3.4 ± 0.3	1.7 ± 0.5	123.3 ± 4.4	-0.76
20227.7 0220	02 27 44.93	1.07	-02 51 00.49	1.75	C	10,., 11.0	17.6 ± 1.9	<3.2	<2.5	98.1 ± 6.9	0.70
	02 27 44.91	1.10	-02 51 03.48	1.75	С		8.1 ± 1.0	<4.5	<2.5	97.3 ± 4.6	
J0227.8-0315	02 27 45.22	1.07	-03 15 46.99	1.75	S	17.5 ± 1.9	17.5 ± 1.9	<2.8	<2.6	50.2 ± 24.8	-0.73
J0227.8-0202	02 27 45.82	1.30	-02 03 00.14	1.91	S	21.2 ± 3.3	21.2 ± 3.3	13.0 ± 5.6	<4.0	135.5 ± 3.7	-0.31

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Table A.1. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{int}	S _{comp}	Major axis	Minor axis	Position	Spectral
10007.0 0550	J2000	arcsec	J2000	arcsec	C	mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1100}
J0227.8-0552	02 27 46.97	1.20	-05 52 58.10	1.84	S	5.9 ± 1.2	5.9 ± 1.2	.5</td <td><5.1</td> <td>43.4 ± 19.0</td> <td><-0.46</td>	<5.1	43.4 ± 19.0	<-0.46
J0227.8-0232	02 27 48.26	1.06	-02 32 07.08	1.75	S	30.6 ± 3.2	30.6 ± 3.2	2.5 ± 1.3	<2.1	62.2 ± 5.2	-0.46
J0227.9-0518	02 27 50.91	1.15	-05 18 50.04	1.94	5	4.2 ± 0.8	4.2 ± 0.8	<8.3	< 3.0	$1/1.9 \pm 15.0$	<-0.23
J0227.9-0429	02 27 52.60	1.07	-04 29 40.09	1.70	3 M	8.0 ± 1.0	6.0 ± 1.0	< 3.0	< 3.5	35.1 ± 25.0	<-0.07
J0227.9-0343	02 27 53.35	1.09	-03 43 32.70	1.//	M C	19.5 ± 1.9	15.5 ± 1.0	5.4 ± 2.0	< 3.1	37.3 ± 3.1	-0.82
10227 0-0444	02 27 53.31	1.10	-03 43 54.23 -04 44 50 48	1.70	M	358 + 35	0.0 ± 0.9	< 3.4 8 4 ± 1 5	< 3.0	141.0 ± 12.0 160.2 ± 6.5	-0.78
J0227.9-0444	02 27 53.91	1.07	-04 44 50.48	1.77	C	33.0 ± 3.3	50.2 ± 0.4	0.4 ± 1.3	4.7 ± 1.5	100.2 ± 0.3	-0.78
10227 0_0233	02 27 54 14	1.00	-02 33 48 43	1.05	s	113 ± 15	113 ± 15	<4.6	<3.8	4.5 ± 0.5	-0.40
10227.9-0255 10227.9-0457	02 27 54 79	1.05	-025340.43 -04570322	1.77	S	11.3 ± 1.3 61.1 ± 6.2	11.3 ± 1.3 61.1 ± 6.2	10 ± 07	<1.5	43.3 ± 10.7	-0.40
10228 0-0400	02 27 59 93	1.00	-04 00 15 18	1.88	S	85 ± 14	85 ± 14	98 ± 45	<4.8	32.6 ± 8.1	-0.50
10228.0-0325	02 27 59.95	1 11	$-03\ 25\ 47\ 13$	1.00	M	113 ± 11	66 ± 0.9	<52	<3.0	52.0 ± 0.1 58.6 + 5.8	<-0.91
30220.0 0323	02 28 00.00	1 11	-03 25 49 76	1.76	C	11.5 ± 1.1	47 ± 0.7	<5.0	<2.5	69.2 ± 5.0	< 0.91
10228 0-0312	02 28 01 94	1.09	-03 12 13 31	1.76	Š	62 ± 09	62 ± 0.9	<47	<3.2	51.5 ± 10.1	<-0.50
J0228.1-0505	02 28 05.42	1.08	$-05\ 05\ 47.19$	1.78	Ň	9.5 ± 1.1	6.1 ± 0.9	<4.9	<3.3	162.7 ± 9.6	<-0.79
	02 28 05.60	1.26	-05 05 46.15	2.01	С		3.4 ± 0.6	<10.3	<3.1	34.4 ± 3.2	
J0228.1-0242	02 28 07.53	1.35	-024204.79	1.90	Š	11.7 ± 2.3	11.7 ± 2.3	9.1 ± 5.1	7.7 ± 4.8	74.5 ± 73.2	<-0.93
J0228.1-0231*	02 28 07.58	1.06	-02 31 06.85	1.75	ŝ	531.1 ± 53.2	531.1 ± 53.2	8.1 ± 0.1	1.2 ± 0.3	114.0 ± 0.3	-0.99
J0228.1-0408	02 28 08.46	1.07	-04 08 51.21	1.75	\tilde{M}	15.5 ± 1.4	11.9 ± 1.3	<2.9	<2.8	41.5 ± 32.0	-0.82
	02 28 11.29	1.11	-04 08 42.76	1.77	С		3.6 ± 0.6	<5.2	<3.6	63.4 ± 15.4	
J0228.2-0232	02 28 09.89	1.12	-02 32 08.30	1.76	S	8.6 ± 1.2	8.6 ± 1.2	<5.4	<2.6	120.7 ± 4.8	<-0.72
J0228.2-0229	02 28 10.26	1.43	-02 29 49.25	1.80	S	6.9 ± 1.3	6.9 ± 1.3	<9.4	<3.8	110.3 ± 5.3	<-0.57
J0228.2-0433	02 28 14.13	1.17	-04 33 32.14	1.81	S	5.3 ± 0.8	5.3 ± 0.8	<7.0	<3.7	131.0 ± 5.8	<-0.39
J0228.2-0503	02 28 14.39	1.18	-05 02 40.64	2.06	M	50.0 ± 5.0	30.9 ± 4.5	20.8 ± 5.6	7.2 ± 2.6	19.1 ± 4.3	-0.45
	02 28 13.58	1.21	-05 03 18.43	1.94	С		10.8 ± 1.9	11.0 ± 5.3	<5.3	29.6 ± 8.7	
	02 28 14.35	1.08	-05 02 36.60	1.77	С		8.3 ± 1.1	<4.3	<3.6	15.9 ± 19.1	
J0228.3-0414	02 28 16.16	1.21	-04 13 55.37	1.80	М	11.9 ± 1.5	8.1 ± 1.3	6.8 ± 4.6	<4.3	60.3 ± 8.2	-1.00
	02 28 15.34	1.13	-04 14 05.07	1.81	С		3.8 ± 0.7	<5.8	<5.2	-1.0 ± 74.1	
J0228.3-0422	02 28 16.64	1.10	-04 22 10.75	1.77	S	5.1 ± 0.8	5.1 ± 0.8	<5.0	<3.8	48.6 ± 15.8	-0.19
J0228.3-0423	02 28 18.88	1.21	-04 23 12.75	1.85	S	3.6 ± 0.8	3.6 ± 0.8	<7.3	<6.1	42.8 ± 44.2	<-0.12
J0228.3-0404	02 28 19.08	1.09	-04 05 00.68	1.77	S	7.3 ± 1.0	7.3 ± 1.0	<4.6	<3.7	46.4 ± 16.0	<-0.61
J0228.3-0432	02 28 20.65	1.08	-04 32 27.58	1.79	S	5.5 ± 0.9	5.5 ± 0.9	<5.2	<3.6	179.4 ± 12.6	<-0.42
J0228.4-0323	02 28 21.59	1.11	-03 23 42.58	1.78	S	7.2 ± 1.1	7.2 ± 1.1	<5.0	<4.4	60.1 ± 42.5	<-0.60
J0228.4-0259	02 28 21.84	1.11	-02 59 26.03	1.78	M	11.9 ± 1.4	7.6 ± 1.1	<4.9	<4.5	62.0 ± 52.3	-0.77
	02 28 22.03	1.36	-02 59 25.52	1.93	С		4.3 ± 0.8	<10.2	<3.7	46.6 ± 4.3	
J0228.4-0453	02 28 22.30	1.22	-04 53 42.86	1.93	S	3.8 ± 0.8	3.8 ± 0.8	<9.1	<4.2	35.6 ± 7.0	<-0.17
J0228.4-0430	02 28 23.28	1.09	-04 30 25.09	1.77	М	39.6 ± 3.8	32.2 ± 3.6	10.8 ± 2.0	<2.8	133.4 ± 2.5	-0.74
	02 28 23.04	1.18	-04 30 09.04	1.79	С		7.4 ± 1.2	<6.4	<4.7	113.5 ± 14.8	
J0228.4-0427	02 28 24.05	1.26	-04 27 07.86	1.81	M	16.6 ± 2.1	11.8 ± 1.9	9.5 ± 4.1	5.0 ± 3.7	107.8 ± 15.8	-0.45
	02 28 24.58	1.14	-04 27 10.77	1.92	C		4.9 ± 0.9	<8.4	<3.8	25.6 ± 5.4	0.40
J0228.4-0349	02 28 24.51	1.08	-03 49 08.53	1.77	S	5.5 ± 0.8	5.5 ± 0.8	<4.2	<3.7	41.3 ± 42.6	<-0.42
J0228.4-0435	02 28 25.29	1.07	-04 34 40.25	1.76	M	16.4 ± 1.6	12.5 ± 1.4	<3.2	<2.9	40.7 ± 22.0	-0.70
10220 4 0226	02 28 22.18	1.07	-04 35 04.12	2.01	C	50 11	4.0 ± 0.7	<9.2	<3.0	$1/3.6 \pm 3.4$	0.05
J0228.4-0326	02 28 25.31	1.22	-03 26 38.71	1.81	S	5.0 ± 1.1	5.0 ± 1.1	<6.8	< 5.8	76.5 ± 46.9	<-0.35
J0228.4-0417	02 28 26.78	1.11	-04 1/ 51.//	1.78	3	6.9 ± 1.0	6.9 ± 1.0	<5.0	<4.5	55.8 ± 38.0	<-0.57
J0228.5-0540	02 28 27.54	1.00	-05 41 00.89	1.75	S	81.0 ± 8.3	81.0 ± 8.3	5.0 ± 0.0	2.7 ± 0.7	142.2 ± 4.0 100.4 ± 2.2	-0.32
J0228.5-0225*	02 28 29.19	1.00	-02 23 10.42	1.75	S	$1/2.2 \pm 1/.3$	$1/2.2 \pm 1/.5$	4.1 ± 0.3	1.0 ± 0.7	100.4 ± 2.2	-0.81
J0228.3-0410	02 28 31.40	1.21	-04 10 24.30	1.69	S M	4.0 ± 0.9	4.0 ± 0.9	.4</td <td>< 0.0</td> <td>-1.0 ± 09.0</td> <td><-0.20</td>	< 0.0	-1.0 ± 09.0	<-0.20
J0228.3-0440	02 28 31.02	1.08	-04 40 03.30	1.//	M C	21.2 ± 2.1	10.2 ± 2.0	3.0 ± 2.2	< 3.1	131.2 ± 0.1	-0.75
10228 6 0417	02 28 31.09	1.22	-04 40 03.03	2.00	c c	28 107	3.0 ± 0.9	<0.2	<3.7	43.7 ± 3.3	< 0.16
I0220.0-0417	02 20 34.32	1.09	-07 17 56.25	2.00	5	3.0 ± 0.7 21 3 \pm 2 4	5.0 ± 0.7 21.3 ± 2.4	<33	<3.0	9.5 ± 3.4 85.9 \pm 23.0	_0.10
I0228.0-0339	02 28 34.04	1.07	-04 28 52 41	1.70	S	21.5 ± 2.4 38 + 00	21.5 ± 2.4 38 + 00	<7.7	<5.0	1645 + 305	<-0.40
I0228 6_0428	02 28 35.80	1 23	-04 49 29 85	2 11	S	3.0 ± 0.9 3.7 ± 0.9	3.5 ± 0.9 3.7 ± 0.9	<10.3	<69	15 + 187	<-0.15
10228.6-0505	02 28 38 46	1.23	$-05\ 05\ 12\ 37$	1.81	S	5.7 ± 0.9 58 + 09	5.7 ± 0.9 58 + 09	<62	<42	1.5 ± 10.7 33 8 + 11 8	0.15
10228.6-0406	02 28 38 49	1.06	-04 06 47 77	1.01	ŝ	30.0 ± 3.1	30.0 ± 3.1	<2.4	<2.2	65 ± 145	-0.23
J0228.7-0435	02 28 39 30	1.07	-04 35 52.77	1.76	M	36.9 ± 2.5	16.3 ± 1.8	<3.2	<2.8	176.9 ± 13.9	-0.86
0022017 0100	02 28 39 66	1.07	-043542.01	1.76	C	0000 = 200	10.5 ± 1.2	<3.5	<2.5	20.5 + 8.3	0.00
	02 28 39.79	1.08	-04 35 44.08	1.77	Ĉ		10.2 ± 1.2	<4.8	<2.0	32.0 ± 2.1	
J0228.8-0502	02 28 45.58	1.08	$-05\ 02\ 32.17$	1.76	M	10.1 ± 1.1	6.5 ± 0.9	<4.3	<3.2	46.8 ± 12.3	-0.85
	02 28 45.65	1.54	$-05\ 02\ 28.92$	1.80	С		3.6 ± 0.7	<10.2	<3.2	71.1 ± 3.2	
J0228.8-0213	02 28 45.96	1.21	-02 13 27.99	1.79	S	9.4 ± 1.6	9.4 ± 1.6	<7.1	<3.9	62.8 ± 7.3	-0.67
J0228.8-0253	02 28 47.52	1.08	-02 53 48.02	2.65	S	34.7 ± 5.3	34.7 ± 5.3	25.7 ± 9.7	<3.5	178.3 ± 1.4	<-1.68
J0228.8-0357	02 28 47.74	1.09	-03 57 32.98	2.11	S	19.0 ± 3.1	19.0 ± 3.1	11.7 ± 6.7	<3.2	10.2 ± 2.3	<-1.27
J0228.8-0238	02 28 49.27	1.40	-02 38 47.37	1.82	S	6.0 ± 1.2	6.0 ± 1.2	<9.1	<5.1	110.3 ± 10.9	-0.41
J0228.9-0337*	02 28 53.22	1.06	-03 37 36.60	1.75	M	2144.5 ± 200.4	2000.5 ± 200.1	4.5 ± 0.1	2.6 ± 0.1	129.0 ± 0.8	-0.54
	02 28 53.69	1.06	-03 37 41.21	1.75	С		98.9 ± 10.3	<2.6	<1.7	36.8 ± 2.4	
	02 28 53.59	1.07	-03 37 31.11	1.76	С		45.0 ± 5.2	<4.0	<2.2	142.6 ± 3.4	
J0228.9-0350	02 28 53.47	1.07	-03 50 54.75	1.77	M	28.7 ± 3.1	17.1 ± 2.3	<4.5	<3.1	166.3 ± 10.0	-0.66
	02 28 53.65	1.12	-03 50 55.02	1.81	С		11.5 ± 2.0	<6.5	<3.4	38.0 ± 7.4	
J0228.9-0224	02 28 55.32	1.09	-02 24 56.08	1.76	S	11.9 ± 1.6	11.9 ± 1.6	<4.2	<3.7	55.6 ± 27.6	-0.44
J0229.1-0436	02 29 04.27	1.14	-04 36 46.66	1.86	S	6.8 ± 1.2	6.8 ± 1.2	<7.6	<3.4	147.2 ± 5.2	<-0.56
J0229.1-0421	02 29 04.99	1.07	-04 21 21.15	1.76	S	21.4 ± 2.5	21.4 ± 2.5	<3.1			-0.61
J0229.1-0541*	02 29 05.81	1.07	-05 41 06.50	1.75	М	759.5 ± 69.0	681.7 ± 68.5	29.1 ± 0.8	6.9 ± 0.2	51.3 ± 0.3	-0.86

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Table A.1. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Туре	S_{int}	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec	• •	mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
	02 29 05.19	1.07	-05 41 11.02	1.75	С	•	77.8 ± 8.1	6.7 ± 0.8	<2.0	79.7 ± 2.3	
J0229.1-0402	02 29 05.90	1.07	-04 02 41.40	1.75	M	58.6 ± 5.2	47.4 ± 5.0	4.5 ± 1.1	<2.2	54.9 ± 4.4	-0.36
	02 29 06.38	1.07	-04 02 37.20	1.77	С		11.3 ± 1.6	<4.5	<3.4	176.7 ± 14.7	
J0229.1-0443	02 29 06.03	1.09	-04 43 47.21	1.77	S	15.7 ± 2.0	15.7 ± 2.0	<4.6	<3.9	34.7 ± 21.0	-0.56
J0229.1-0510	02 29 07.77	1.11	-05 10 12.57	1.78	S	8.4 ± 1.3	8.4 ± 1.3	<5.2	<4.4	45.2 ± 35.1	<-0.71
J0229.1-0508	02 29 08.49	1.11	-05 08 31.07	1.80	S	9.3 ± 1.5	9.3 ± 1.5	<5.6	<4.5	30.9 ± 22.2	-0.66
J0229.1-0507	02 29 08.69	1.07	-05 07 24.31	1.76	М	32.8 ± 3.2	26.3 ± 2.9	3.3 ± 1.7	<2.9	57.4 ± 15.4	-1.03
	02 29 05.78	1.18	-05 07 40.81	1.92	С		6.5 ± 1.4	<8.1	<6.2	175.0 ± 28.8	
J0229.1-0223*	02 29 08.73	1.06	-02 23 11.17	1.75	S	98.0 ± 9.9	98.0 ± 9.9	2.6 ± 0.6	<1.6	25.7 ± 11.4	-0.83
J0229.2-0406	02 29 10.80	1.09	-04 06 09.58	1.77	M	16.9 ± 1.8	9.0 ± 1.3	<4.8	<3.6	139.8 ± 13.4	-0.92
	02 29 10.80	1.18	-04 06 05.26	1.79	C		7.9 ± 1.3	<6.5	<4.7	120.6 ± 14.6	0.50
J0229.2-0243	02 29 11.05	1.18	-02 43 43.88	1.85	S	7.1 ± 1.4	7.1 ± 1.4	<6.8	<6.2	-1.0 ± 72.2	<-0.59
J0229.2-0329	02 29 11.45	1.37	-03 29 27.11	2.18	S	14.3 ± 3.2	14.3 ± 3.2	11.9 ± 8.3	<6.5	29.5 ± 10.6	<-1.07
J0229.2-0311*	02 29 11.93	1.06	-03 11 38.03	1.75	M	63.8 ± 5.0	41.5 ± 4.3	<2.1	<1.9	51.2 ± 12.9	-0.68
10220 2 0511	02 29 10.38	1.07	-03 11 22.13	1.76	C	75.10	22.2 ± 2.5	<3.3	<2.9	18.3 ± 15.6	0.45
J0229.2-0511	02 29 13.01	1.10	-05 11 19.46	1.79	5	7.5 ± 1.3	7.5 ± 1.3	< 6.2	<4.7	124.4 ± 20.8	-0.45
J0229.2-0502	02 29 14.38	1.08	-05 02 10.49	2.28	S	11.5 ± 2.2	11.5 ± 2.2	<11.9	<3.5	2.3 ± 3.0	<-0.92
J0229.2-0308	02 29 14.87	1.25	-03 08 10.28	1.80	S	7.1 ± 1.3	7.1 ± 1.3	.3</td <td>< 5.3</td> <td>102.2 ± 18.7</td> <td>0.09</td>	< 5.3	102.2 ± 18.7	0.09
J0229.3-0442*	02 29 15.70	1.06	-04 42 16.30	1.75	M	$1058.0 \pm / 1.1$	623.2 ± 62.4	3.6 ± 0.1	2.3 ± 0.2	145.7 ± 2.0	-0.73
	02 29 16.10	1.00	-04 42 11.20	1.75	C		334.4 ± 33.0	0.8 ± 0.3	5.2 ± 0.3	39.3 ± 1.4	
	02 29 15.37	1.00	-04 42 14.06	1.75	C		26.9 ± 2.9	<2.9	<1.0	$1/.0 \pm 2.4$	
	02 29 15.28	1.00	-04 42 11.05	1.75	C		20.9 ± 2.9	<2.9	<1.0	20.7 ± 2.4	
	02 29 15.87	1.09	-04 42 05.15	1.70	C		19.0 ± 2.5	<4.0	<2.8	130.4 ± 0.2	
	02 29 16.44	1.07	-04 42 09.23	1.79	C		15.2 ± 2.1	< 5.2	<2.0	$1/3.5 \pm 4.5$	
10000 2 0001	02 29 16.70	1.15	-04 42 08.45	1.95	C	96.12	11.9 ± 2.2	<8.9	<4.1	155.0 ± 0.0	0.72
J0229.3-0231	02 29 10.34	1.10	-02 31 25.14	1.//	S	8.0 ± 1.3	8.0 ± 1.3	<4./	<4.1	49.7 ± 42.7	-0.73
J0229.5-0405	02 29 17.22	1.07	-04 03 27.83	1.70	S	24.3 ± 2.7	24.3 ± 2.7	4.0 ± 1.0	< 3.0	90.8 ± 14.3	-0.62
J0229.3-0515	02 29 17.38	1.00	-05 15 29.49	1.77	5	13.1 ± 1.7	13.1 ± 1.7	<4.5	< 5.0	32.2 ± 19.3	-0.30
J0229.3-0303	02 29 18.04	1.21	-03 03 12.19	1.79	5	1.4 ± 1.5	1.4 ± 1.5	<0.0	< 3.5	90.2 ± 24.2	-0.45
J0229.3-0427	02 29 19.08	1.11	-04 27 30.33	2.10	5	14.0 ± 2.0	14.0 ± 2.0	10.3 ± 7.0	< 3.5	11.0 ± 3.0	<-1.08
10229.3-0431	02 29 19.97	1.10	-04 51 55.54	1.90	S	0.4 ± 1.3 127 ± 1.5	12.7 ± 1.5	< 3.7	<4.4	172.0 ± 0.0 43.0 ± 11.3	-0.20
10229.4-0313	02 29 21.38	1.07	$-03\ 13\ 13.01$ $-04\ 54\ 24\ 03$	1.70	M	12.7 ± 1.3 35.0 ± 3.4	12.7 ± 1.3 20.7 ± 2.8	<3.7 76+35	< 3.0	43.0 ± 11.3 27.1 ± 4.3	-0.20
J0229.4-0454	02 29 21.97	1.10	-04 54 24.03	1.02	C M	33.0 ± 3.4	20.7 ± 2.0	7.0 ± 3.3	<3.5	27.1 ± 4.3 12.2 ± 8.4	-0.87
10220 4-0407	02 29 22.04	1.07	$-04 \ 34 \ 28.34$ $-04 \ 07 \ 28 \ 84$	1.77	c c	16.2 ± 1.0	14.3 ± 1.0 16.2 ± 1.0	<4.2	<2.9	12.3 ± 0.4	-1.02
10229.4-0407	02 29 22.34	1.07	-04 07 28.84 -02 40 25 90	1.70	S S	10.2 ± 1.9 61 ± 1.2	10.2 ± 1.9 61 ± 1.2	< 5.2	-5.5	175 0 ± 38 6	-1.02
10229.4-0240	02 29 22.92	1.14	-02 40 23.90 -03 50 37 58	1.87	S	0.1 ± 1.2 65 ± 13	0.1 ± 1.2 65 ± 13	<6.2	<5.5	175.0 ± 58.0	-0.00
10229.4-0235	02 29 25.00	1.15	-03 30 37.38 -02 35 23 28	1.02	S	286 ± 30	286 ± 30	< 2.8	~2.2	${587 \pm 50}$	-0.89
10229 5-0303	02 29 25.11	1.07	-02 03 25.20 -03 03 24 05	1.75	S	45 ± 10	20.0 ± 5.0	<7.6	<5.1	121.8 ± 17.7	-0.32
10229 5-0248	02 29 21.21	1.24	$-03\ 03\ 24.03$ $-02\ 48\ 46\ 48$	1.02	S	$\frac{1.5}{275} \pm 2.9$	$\frac{4.5 \pm 1.0}{27.5 \pm 2.9}$	<7.0	<2.2	467 ± 11.5	-1.00
10229.6-0433	02 29 34 78	1.00	-04 33 12 50	1.75	S	65 ± 11	65 ± 11	<7.7	<4.4	40.7 ± 11.5 507 + 104	0.45
10229.6-0241	02 29 34 90	1.19	-02411792	1.01	S	58 ± 1.1	58 ± 1.1	< 8.8	<36	128 + 52	<-0.45
10229.6-0440	02 29 35 62	1.10	-04 40 08 89	1.97	S	5.0 ± 1.1 53 + 11	5.0 ± 1.1 5.3 ± 1.1	<7.3	<5.7	94.0 ± 31.6	<-0.39
10229 6-0336	02 29 36 50	1.20	-03 36 20 55	1.01	ŝ	237 + 39	237 + 39	183 + 73	<46	839 + 34	-0.99
10229 6-0435	02 29 36 54	1.12	-04 35 15 61	1.78	ŝ	91 + 13	91 + 13	<54	<4.6	497 + 262	-0.88
10229.6-0509	02 29 37 82	1.09	-05 09 24 68	1.76	ŝ	10.2 ± 1.3	10.2 ± 1.3	<43	< 3.9	83.6 ± 41.2	0.07
10229 6-0442	02 29 37.02	1.09	-04 42 40 62	1.70	ŝ	11.2 ± 1.1 11.4 ± 1.5	11.2 ± 1.1 11.4 ± 1.5	<4.4	<3.5	32.0 ± 11.2 32.2 + 14.4	-0.53
10229 7-0330	02 29 38 93	1.00	-03 30 20 23	1.83	ŝ	72 + 14	72 + 14	<63	<5.4	159.9 ± 45.6	-0.54
10229.7-0238*	02 29 39.06	1.06	-02.3836.70	1.75	M	121.9 ± 11.7	115.5 ± 11.6	3.2 ± 0.4	1.9 ± 0.6	70.9 ± 7.5	-0.53
022011 0200	02 29 38.54	1.18	-023834.31	1.89	C	1211/ 2 111/	6.4 ± 1.2	<8.3	<4.0	33.9 ± 7.1	0.000
J0229.7-0531	02 29 39.85	1.08	$-05\ 31\ 52.55$	2.03	Š	5.7 ± 1.2	5.7 ± 1.2	< 9.4	<3.9	1.8 ± 5.9	-0.34
J0229.7-0247	02 29 40.02	1.19	-02 47 04.64	1.84	ŝ	5.8 ± 1.2	5.8 ± 1.2	<7.0	<5.9	42.2 ± 47.8	<-0.45
J0229.7-0341	02 29 44.71	1.31	-03 41 08.17	1.84	S	5.7 ± 1.3	5.7 ± 1.3	<7.9	<6.4	107.7 ± 39.5	<-0.44
J0229.7-0524	02 29 44.84	1.07	-05 24 30.99	1.75	S	26.2 ± 2.8	26.2 ± 2.8	<2.7	<2.6	16.3 ± 42.8	-0.55
J0229.8-0337	02 29 47.59	1.08	-03 37 52.79	1.86	S	5.7 ± 1.0	5.7 ± 1.0	<7.1	<3.7	4.8 ± 7.8	-0.31
J0229.9-0330	02 29 51.05	1.12	-03 30 50.18	1.88	S	6.3 ± 1.2	6.3 ± 1.2	<7.4	<5.1	5.8 ± 17.1	<-0.50
J0229.9-0447	02 29 51.22	1.15	-04 47 40.02	1.80	S	20.3 ± 2.7	20.3 ± 2.7	10.3 ± 3.3	<3.8	45.2 ± 4.8	-0.52
J0229.9-0225	02 29 51.55	1.17	-02 25 59.28	2.63	S	24.2 ± 3.7	24.2 ± 3.7	22.5 ± 10.0	<3.0	166.3 ± 1.1	<-1.43
J0229.9-0413	02 29 52.59	1.42	-04 13 05.55	1.91	S	5.2 ± 1.2	5.2 ± 1.2	<9.5	<6.8	58.3 ± 21.8	-0.35
J0229.9-0228	02 29 54.73	1.11	-02 28 41.95	1.76	M	18.1 ± 1.8	10.5 ± 1.4	<4.9	<2.7	71.9 ± 5.1	-1.00
	02 29 54.77	1.09	-02 28 44.62	1.75	С		7.5 ± 1.0	<4.5	<2.5	71.0 ± 6.1	
J0230.0-0249	02 29 58.09	1.17	-02 49 31.02	1.76	M	14.1 ± 1.6	7.5 ± 1.2	<6.1	<3.5	83.3 ± 7.4	-0.71
	02 29 58.06	1.11	-02 49 27.93	1.76	С		6.6 ± 1.0	<5.0	<3.4	73.3 ± 12.8	
J0230.0-0500	02 29 59.88	1.09	-05 01 01.41	1.76	S	8.2 ± 1.2	8.2 ± 1.2	<4.2	<3.9	67.9 ± 53.1	<-0.69
J0230.0-0331*	02 30 00.92	1.06	-03 31 49.65	1.75	M	82.4 ± 5.8	42.7 ± 4.5	3.3 ± 1.1	<2.2	61.8 ± 6.0	-0.77
	02 30 01.41	1.06	-03 31 50.93	1.75	С		33.9 ± 3.6	<2.6	<2.3	33.6 ± 10.6	
	02 30 01.80	1.15	-03 31 46.97	1.90	С		5.8 ± 1.1	<8.3	<3.9	28.7 ± 7.1	
J0230.0-0440	02 30 01.12	1.20	-04 40 59.61	1.82	S	4.9 ± 1.0	4.9 ± 1.0	<7.0	<5.4	51.5 ± 30.3	<-0.33
J0230.0-0324	02 30 01.20	1.52	-03 24 31.20	1.93	S	12.3 ± 2.7	12.3 ± 2.7	9.7 ± 7.5	<6.8	59.2 ± 15.8	-1.06
J0230.0-0402	02 30 02.22	1.11	-04 02 59.72	1.78	S	11.6 ± 1.6	11.6 ± 1.6	<5.7	<3.5	45.3 ± 6.6	-0.50
J0230.0-0359	02 30 02.75	1.40	-03 59 32.51	1.83	S	5.5 ± 1.1	5.5 ± 1.1	<9.3	<4.8	116.6 ± 8.5	<-0.42
J0230.1-0512	02 30 04.37	1.07	-05 12 08.32	1.76	M	24.7 ± 2.3	17.5 ± 2.0	<3.4	<2.7	133.4 ± 9.6	-0.89
	02 30 04.53	1.14	-05 12 06.44	1.83	С		7.2 ± 1.1	<7.2	<3.1	38.3 ± 4.0	
J0230.1-0305	02 30 05.78	1.10	-03 05 28.18	1.77	S	11.1 ± 1.5	11.1 ± 1.5	<4.7	<4.0	53.3 ± 23.2	0.32

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Table A.1. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Туре	S _{int}	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		mJy	mJy	arcsec	arcsec	Angle	index α_{325}^{1400}
J0230.1-0341	02 30 05.89	1.07	-03 41 52.24	1.75	М	39.7 ± 3.7	23.5 ± 2.6	<2.9	<2.6	33.1 ± 18.0	-1.23
	02 30 05.87	1.34	-03 41 48.52	1.77	С		16.3 ± 2.6	9.4 ± 4.9	<4.3	93.2 ± 5.9	
J0230.1-0457	02 30 07.11	1.20	-04 57 15.15	1.80	S	25.2 ± 3.6	25.2 ± 3.6	10.0 ± 3.3	6.6 ± 2.7	108.5 ± 16.2	-0.28
J0230.2-0457	02 30 11.56	1.09	-04 57 40.50	1.83	S	13.1 ± 1.9	13.1 ± 1.9	6.4 ± 3.8	<3.8	12.4 ± 6.9	-0.64
J0230.2-0320	02 30 13.43	1.23	-03 20 09.40	1.95	S	6.3 ± 1.2	6.3 ± 1.2	<9.5	<3.8	34.8 ± 4.9	<-0.51
J0230.3-0512	02 30 15.16	1.08	-05 12 38.71	1.98	S	4.9 ± 1.0	4.9 ± 1.0	<8.8	<3.6	2.0 ± 5.5	<-0.34
J0230.3-0405	02 30 16.48	1.18	-04 05 16.25	1.85	S	5.3 ± 1.1	5.3 ± 1.1	<7.4	<5.0	141.0 ± 18.6	<-0.38
J0230.3-0257	02 30 17.85	1.18	-02 57 47.02	2.10	S	13.5 ± 2.7	13.5 ± 2.7	<10.6	<4.6	20.0 ± 6.0	<-1.03
J0230.3-0432	02 30 18.91	1.11	-04 32 47.71	1.79	M	22.5 ± 2.2	13.0 ± 1.8	5.3 ± 3.7	<3.3	41.0 ± 5.3	-0.94
	02 30 18.72	1.09	-04 32 47.68	1.76	С		9.5 ± 1.4	<4.1	<3.5	106.9 ± 27.9	
J0230.4-0255*	02 30 21.98	1.06	-02 55 03.86	1.75	M	430.5 ± 41.9	417.7 ± 41.9	10.0 ± 0.2	2.7 ± 0.2	156.8 ± 0.4	-1.07
	02 30 22.44	1.10	-02 55 00.67	1.80	С		12.7 ± 1.9	<6.1	<3.5	149.4 ± 6.5	
J0230.4-0412*	02 30 23.42	1.06	-04 12 26.54	1.75	M	493.4 ± 43.3	429.0 ± 43.0	4.0 ± 0.2	2.5 ± 0.3	46.2 ± 2.8	-0.55
	02 30 23.83	1.06	-04 12 21.76	1.75	С		37.3 ± 4.1	<2.7	<2.3	177.7 ± 10.8	
	02 30 23.09	1.06	-04 12 23.30	1.75	С		27.2 ± 2.9	<2.1	<1.6	21.2 ± 6.1	
J0230.4-0305	02 30 23.93	1.07	-03 05 25.57	2.45	S	24.5 ± 4.0	24.5 ± 4.0	17.3 ± 8.8	<3.3	177.8 ± 1.7	<-1.44
J0230.4-0432	02 30 24.17	1.07	-04 32 13.57	1.75	S	26.7 ± 2.9	26.7 ± 2.9	<3.0	<2.7	43.5 ± 18.9	-0.84
J0230.5-0442	02 30 27.32	1.30	-04 42 42.05	1.83	S	6.6 ± 1.3	6.6 ± 1.3	<7.8	<6.3	97.5 ± 32.3	-0.44
J0230.5-0410	02 30 27.66	1.36	-04 10 36.53	2.08	M	13.9 ± 1.6	7.1 ± 1.1	<11.5	<2.1	142.8 ± 1.1	-1.08
	02 30 27.51	1.38	-04 10 34.40	2.09	С		6.8 ± 1.1	<11.7	<2.1	37.4 ± 1.2	
J0230.5-0346	02 30 32.78	1.08	-03 46 43.58	1.94	S	5.0 ± 1.0	5.0 ± 1.0	<8.3	<3.7	172.9 ± 6.6	-0.49
J0230.6-0309*	02 30 33.39	1.06	-03 09 06.78	1.75	S	115.0 ± 11.6	115.0 ± 11.6	2.5 ± 0.5	<1.5	80.2 ± 10.2	-0.55
J0230.6-0421*	02 30 33.50	1.06	-04 21 07.66	1.75	M	175.0 ± 12.7	92.6 ± 9.5	4.7 ± 0.7	<1.6	142.3 ± 1.8	-0.59
	02 30 33.71	1.06	-04 21 07.13	1.75	С		82.4 ± 8.5	5.4 ± 0.9	<1.7	35.4 ± 1.6	
J0230.6-0328	02 30 35.86	1.14	-03 28 02.94	1.87	S	7.4 ± 1.4	7.4 ± 1.4	<7.7	<4.2	28.8 ± 8.6	-0.04
J0230.7-0328*	02 30 40.92	1.06	-03 28 37.58	1.75	M	228.5 ± 15.3	102.4 ± 10.3	<1.6	<1.5	148.8 ± 6.0	-0.90
	02 30 40.63	1.28	-03 28 33.64	1.75	С		101.6 ± 10.9	26.1 ± 3.5	<1.9	95.6 ± 0.4	
	02 30 41.14	1.08	-03 28 48.53	1.77	С		15.1 ± 2.0	<4.7	<3.3	145.3 ± 8.4	
	02 30 41.31	1.09	-03 28 45.53	1.88	С		9.4 ± 1.6	<7.4	<3.9	11.1 ± 7.1	
J0230.7-0256*	02 30 43.37	1.49	-02 56 10.68	2.24	M	31.4 ± 4.9	16.1 ± 3.6	14.2 ± 8.9	<6.6	34.4 ± 8.9	0.56
	02 30 42.98	1.38	-02 56 00.30	2.11	С		15.4 ± 3.3	12.2 ± 7.3	<7.2	30.8 ± 14.6	
J0230.8-0424	02 30 48.35	1.09	-04 24 20.71	2.08	S	5.1 ± 1.0	5.1 ± 1.0	<10.0	<4.0	4.7 ± 5.3	<-0.37
J0230.9-0459	02 30 54.17	1.24	-04 59 19.10	2.08	S	4.8 ± 1.0	4.8 ± 1.0	<10.6	<5.2	26.5 ± 8.4	<-0.32
J0231.0-0451*	02 30 57.54	1.06	-04 51 36.75	1.75	M	103.4 ± 10.0	97.0 ± 9.9	8.8 ± 0.7	4.5 ± 0.6	36.8 ± 2.4	-0.56
	02 30 57.04	1.10	-04 51 32.92	1.86	С		6.5 ± 1.1	<7.2	<4.2	15.5 ± 9.0	
J0231.0-0447	02 30 57.75	1.20	-04 47 54.34	1.95	S	5.4 ± 1.1	5.4 ± 1.1	<9.1	<4.8	28.8 ± 9.1	<-0.41

An asterisk (*) after the sourcename indicates this source was also detected at 74 MHz. Description of columns:

1. Source Name.

2. Right Ascension (J2000).

3. Right Ascension uncertainty in arcseconds.

Right Ascension uncertainty in arcseconds.
 Declination (J2000).
 Declination uncertainty in arcseconds.
 Source type: Single (S), Multiple (M) or Component (C) of multiple source.
 Integrated flux density in mJy. An asterisk (*) indicates the flux density has been calculated using pixel based method.
 Flux density of individual componant in mJy as derived through the Gaussian fitting method.
 Size of Major Axis in arcseconds, or the 2*σ* upper limit if the source is unresolved.
 Size of Minor Axis in arcseconds, or the 2*σ* upper limit if the source is unresolved.

10. Size of Minor Axis in arcseconds, or the 2σ upper limit if the source is unresolved.

PA of Major axis in degrees.
 Spectral index with respect to NVSS flux density (1.4 GHz).

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Table A.2. The 74 MHz source list.

Name	RA	σ_{α}	Dec	σ_{δ}	Туре	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		Jy	arcsec	arcsec	Angle	index α_{74}^{1400}
J0157.7-0500	01 57 43.28	3.7	-05 00 06.50	2.5	S	1.69 ± 0.15	40.0 ± 13.3	<33.2	35.2 ± 9.8	-0.97
J0158.1-0311	01 58 07.51	4.3	-03 11 53.89	3.5	S	0.48 ± 0.09	<46.9	<31.1	32.3 ± 28.1	-0.47
J0159.2-0400	01 59 12.69	4.2	-04 00 07.77	4.4	S	0.65 ± 0.11	42.1 ± 28.6	<33.2	13.5 ± 11.9	-0.93
J0159.2-0605	01 59 13.15	5.7	-06 05 30.76	4.3	S	0.63 ± 0.14	<66.4	<51.7	92.7 ± 43.1	-0.71
J0159.4-0408	01 59 25.02	4.1	-04 08 44.72	3.4	S	0.68 ± 0.10	<55.5	<35.5	27.5 ± 18.3	-0.67
J0159.7-0408	01 59 44.11	4.3	-04 08 08.00	4.8	M	0.33 ± 0.08	<62.7	<24.1	163.1 ± 14.3	-0.71
	01 59 45.32	4.4	-04 07 57.42	3.2	С	0.32 ± 0.06	<41.0	<24.4	53.6 ± 28.1	
J0159.9-0150	01 59 51.21	4.3	-01 50 04.25	4.2	S	0.92 ± 0.15	41.8 ± 26.3	<45.4	178.4 ± 19.7	-0.89
J0200.4-0257	02 00 21.95	4.5	-02 57 31.60	3.4	S	0.30 ± 0.07	<37.2			-0.66
J0200.5-0346	02 00 31.33	3.6	-03 46 23.36	2.4	S	1.19 ± 0.11	31.0 ± 14.4	<30.3	48.9 ± 12.9	-0.85
J0201.0-0217	02 00 59.97	6.7	-02 17 39.82	5.7	S	0.77 ± 0.18	<82.2			-0.75
J0201.0-0324	02 01 01.21	5.5	-03 24 48.56	3.0	S	1.38 ± 0.18	77.9 ± 23.9	<45.1	80.6 ± 6.7	-0.82
J0201.3-0421	02 01 20.83	4.6	-04 21 04.69	3.6	S	0.42 ± 0.08	<58.3	<26.5	46.5 ± 14.2	-0.75
J0201.6-0024	02 01 36.89	5.2	-00 24 07.21	4.4	M	0.32 ± 0.09	<49.5	<36.4	46.0 ± 52.8	-0.43
10201 7 0211	02 01 38.28	4.7	-00 23 55.14	4.4	C	0.23 ± 0.06	<48.1	<21.6	149.3 ± 25.4	0.77
J0201.7-0211	02 01 43.17	4.2	-02 11 50.45	4.3	S	1.20 ± 0.16	62.3 ± 22.8	<46.9	13.9 ± 10.3	-0.77
J0201.8-0355	02 01 45.42	3.7	-03 55 11.66	2.7	S	0.55 ± 0.07	<3/.1	<25.7	$1/3.1 \pm 24.1$	-0.75
J0201.8-0419	02 01 45.69	3.6	-04 19 26.52	2.4	S	1.14 ± 0.10	25.9 ± 15.1	<34.7	54.5 ± 29.3	-0.71
J0201.8-0609	02 01 46.10	4.9	-06 09 39.83	3.6	S	0.98 ± 0.15	52.9 ± 24.6	<41.0	54.3 ± 11.4	-0.81
J0201.8-0211	02 01 47.12	6.0	-02 12 00.37	3.9	S	0.44 ± 0.10	<69.8	<39.5	102.0 ± 20.7	-0.45
J0202.1-0558	02 02 07.30	4.3	-05 58 59.54	3.5	S	0.50 ± 0.09	<53.3	<29.2	39.0 ± 18.0	-0.28
J0202.1-0/28	02 02 07.46	6.2	-07 28 40.06	4.1	S	1.29 ± 0.22	75.4 ± 31.1	<46.4	62.9 ± 8.6	-1.08
J0202.6-0310	02 02 36.86	6.0	-03 10 07.64	5.1	S	$0.5/\pm 0.13$	8.6</td <td><58.4</td> <td>49.7 ± 34.9</td> <td>-0.63</td>	<58.4	49.7 ± 34.9	-0.63
J0202.9-0048	02 02 51.81	3.6	-00 48 58.67	2.3	5	1.83 ± 0.15	28.8 ± 12.3	<35.1	122.2 ± 25.7	-0.52
J0202.9-0412	02 02 55.86	4.1	-04 12 58.94	2.8	S	0.86 ± 0.10	36.1 ± 18.6	< 38.8	63.5 ± 18.3	-0.68
J0202.9-0605	02 02 50.01	3.4	-06 05 23.97	2.1	5	3.09 ± 0.19	33.3 ± 7.3	18.4 ± 11.3	41.3 ± 0.4	-0.76
J0203.3+0000	02 03 19.02	4.5	$+00\ 00\ 53.42$	3.8	5	0.55 ± 0.11	<44.1			-0.49
J0203.4-0257	02 03 20.39	4.0	-02 57 08.40	4.5	5	0.21 ± 0.06	<47.5	< 30.3	3.4 ± 38.4	-0.50
J0205.3-0554	02 03 29.70	3.9	-05 54 59.01	3.5	5 5	0.41 ± 0.10	1.9</td <td><32.0</td> <td>130.0 ± 37.3</td> <td>-0.82</td>	<32.0	130.0 ± 37.3	-0.82
J0203.7-0038	02 03 41.33	4.0	-00 38 22.38	4.0	5 5	0.23 ± 0.00	<40.8			-0.01
J0203.8-0034	02 03 40.33	2.5	-00 34 30.75	3.7	S S	0.37 ± 0.10 2.63 ± 0.10	< 00.3	<41.0	12.0 ± 27.9	-0.70
J0203.8-0811	02 03 40.79	5.5	-08 11 10.70	2.2 5.4	S S	2.03 ± 0.19	23.4 ± 11.0	20.0 ± 14.0	43.7 ± 41.3 26.1 + 16.2	-0.03
J0204.0+0023	02 04 02.08	12	+002330.32	2.4	S S	0.36 ± 0.14	< 38.0	< 39.1	50.1 ± 10.2	-0.03
J0204.1-0408	02 04 05.00	4.2	-04 08 32.02	3.4 4.0	S S	0.32 ± 0.00	< 30.9	-527		-0.04
J0204.1-0528 J0204.5-0535	02 04 00.09	4.5	$-05\ 26\ 40.92$	4.0	S	0.77 ± 0.12 0.37 ± 0.07	55.1 ± 27.5	<32.7	4.3 ± 40.1 35.5 ± 24.5	-0.70
J0204.5-0555	02 04 31.11	4.4	-025012.91	5.8 4.6	S	0.37 ± 0.07 0.25 ± 0.06	<53.1	<37.4	33.3 ± 24.3 43 ± 30.2	-0.55
J0204.0-0230	02 04 35.07	37	-06 19 38 16	12.6	S	6.49 ± 0.00	$\sqrt{33.1}$	30.7 ± 12.0	$\frac{1}{27} \pm \frac{3}{20}$	-0.50
J0204.0-0017	02 04 30.40	17	-001930.10 -01283210	3.0	S	0.49 ± 0.00	420.2 ± 37.0	/30.1 ± 12.7	2.7 ± 0.0	-0.76
J0204.0 0420	02 04 37.10	5.0	-07 25 39 29	54	S	0.75 ± 0.11 0.55 ± 0.13	<68.9	<44.4	$\frac{43.1 \pm 0.5}{8.6 \pm 27.6}$	-0.63
10204.9-0655	02 04 55 00	3.6	-06 55 08 33	2.5	S	2.54 ± 0.13	46.0 ± 11.3	251 ± 135	17.0 ± 9.1	-0.52
J0204.9 0035	02 04 55 18	3.6	-07 15 55 51	2.5	S	2.07 ± 0.21 2.07 ± 0.18	40.0 ± 11.5 34.6 ± 12.6	23.1 ± 15.3 21.7 ± 16.2	17.0 ± 9.1 141.8 ± 19.3	-0.70
10205 0-0429	02 05 00 33	3.9	-04 29 46 91	2.1	S	0.68 ± 0.08	30.9 ± 12.0 30.9 ± 19.7	<29.8	58.0 ± 13.2	-0.83
10205 4-0225	02 05 21 27	37	-02 25 33 60	23	S	0.00 ± 0.00 0.95 ± 0.09	<39.4	<29.0	70.8 ± 18.9	-0.57
10205 4-0301	02 05 23 30	3.9	-03 01 00 78	3.0	S	0.53 ± 0.09 0.54 + 0.08	<40.9	<34.2	153.1 + 49.2	-0.84
10205 4-0304	02.05.23.70	4.7	-03.0445.08	5.2	Š	0.32 ± 0.08	<64.3	< 37.8	0.0 + 24.5	-0.59
10205 4-0642	02.05.24.20	4.3	-06 42 05 24	3.9	Š	0.51 ± 0.10	<53.0	<36.6	14.6 + 28.9	-1.05
10205.7-0134	02.05.39.81	4.6	-01 34 29 56	4.1	Š	0.32 ± 0.07	<47.6	< 38.3	3.7 + 60.8	-0.70
J0205.7-0819	02 05 41.45	4.1	$-08\ 19\ 42.25$	3.1	Š	1.06 ± 0.15	<50.2	<43.0	37.4 ± 47.3	-0.72
J0206.1-0432	02 06 03.54	3.9	-04 32 59.50	3.0	Š	0.48 ± 0.07	<40.6	<30.9	176.6 ± 35.1	-0.66
J0206.1-0503	02 06 03.86	3.6	$-05\ 03\ 29.91$	2.3	м	1.46 ± 0.12	37.2 ± 12.1	<29.1	136.8 ± 8.3	-0.63
	02 06 05.42	3.6	-05 03 37.25	2.4	С	1.26 ± 0.11	38.0 ± 12.6	<23.5	28.3 ± 6.5	
J0206.1-0511	02 06 04.15	3.8	-05 11 31.50	2.1	S	6.20 ± 0.36	131.9 ± 9.3	24.3 ± 8.5	108.8 ± 0.8	-0.94
J0206.2-0604	02 06 11.46	3.9	-06 04 03.15	2.8	S	0.52 ± 0.07	<41.9	<23.3	41.4 ± 17.5	-0.46
J0206.3-0553	02 06 17.02	3.7	-05 53 23.49	2.4	S	1.41 ± 0.13	42.4 ± 12.7	<26.4	49.5 ± 6.4	-0.41
J0206.5-0344	02 06 27.36	3.7	-03 44 21.41	4.1	S	1.57 ± 0.15	104.6 ± 19.6	<31.3	17.0 ± 2.5	-0.64
J0207.1-0854	02 07 04.10	3.7	-08 54 43.41	2.5	S	1.95 ± 0.19	32.9 ± 14.5	<36.7	29.6 ± 19.4	-0.76
J0207.1-0149	02 07 07.15	4.3	-01 49 55.54	3.6	S	0.17 ± 0.04	<37.5	<23.1	32.8 ± 37.9	-0.59
J0207.2-0704	02 07 14.06	4.2	-07 04 16.63	3.8	S	0.59 ± 0.09	35.2 ± 26.8	<36.6	21.5 ± 15.8	-0.84
J0207.3-0812	02 07 18.74	5.4	-08 12 50.63	4.3	S	0.62 ± 0.13	<68.0	<44.7	55.2 ± 25.3	-0.88
J0207.6-0158	02 07 32.93	4.9	-01 58 39.03	4.1	S	0.27 ± 0.06	<56.9	<31.5	45.3 ± 22.7	-0.77
J0207.6+0006	02 07 35.39	3.9	+00 06 00.92	2.6	S	1.04 ± 0.12	<45.2	<33.9	110.3 ± 24.0	-1.00
J0207.8-0304	02 07 50.19	5.2	-03 04 54.57	4.9	S	0.30 ± 0.07	<64.6	<43.9	32.5 ± 31.5	-0.96
J0207.9-0053	02 07 51.83	4.2	-00 53 58.80	3.7	S	0.77 ± 0.12	<58.3	<43.4	169.3 ± 27.1	-0.80
J0207.9-0052	02 07 52.15	4.5	-00 52 52.93	4.0	S	0.42 ± 0.09	<53.0	<34.4	154.3 ± 27.8	-0.64
J0207.9-0115	02 07 54.04	3.6	-01 15 30.04	2.3	S	0.76 ± 0.08	<32.2	<24.0	99.2 ± 26.9	-0.83
J0208.0-0527	02 07 57.53	3.4	-05 27 19.58	2.0	S	2.50 ± 0.14	29.3 ± 7.2	<23.4	46.6 ± 5.1	-0.63
J0208.2+0022	02 08 10.69	3.4	+00 23 01.98	2.1	М	3.10 ± 0.19	23.0 ± 9.9	20.2 ± 10.9	106.8 ± 51.5	-0.71
	02 08 09.84	4.5	+00 22 18.33	4.0	С	0.24 ± 0.06	<44.8	<17.7	147.1 ± 22.5	
J0208.3-0708	02 08 19.93	4.4	-07 08 16.68	3.7	S	1.28 ± 0.16	65.3 ± 21.3	<45.7	39.5 ± 8.8	-0.78
J0208.4-0047	02 08 25.99	3.4	-00 47 49.13	2.0	S	2.45 ± 0.15	<26.9	<24.7	94.5 ± 35.5	-0.49
J0208.5-0637	02 08 29.10	4.6	-06 37 11.07	4.1	S	0.26 ± 0.06	<51.3	<30.0	32.6 ± 26.7	-0.62
J0208.5-0226	02 08 32.44	3.9	-02 26 44.87	2.9	S	0.52 ± 0.07	<49.5	<23.8	39.0 ± 11.7	-0.81
J0208.8-0516	02 08 48.18	4.8	-05 16 22.13	3.4	S	0.25 ± 0.05	<57.6	<23.0	57.3 ± 13.8	-0.69

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Table A.2. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Type	Scomp	Major axis	Minor axis	Position	Spectral
	12000	arceac	12000	arceac	-71-	~ comp	0100000	arcsac	Angle	index α^{1400}
10208.0 - 0100	J2000	4.5	J2000	2 4	14	$\frac{Jy}{0.65 \pm 0.12}$	150.4	120.7	Aligie	0.79
J0208.9+0109	02 08 53.88	4.5	+01 09 59.53	3.4	М	0.65 ± 0.12	<50.4	<30.7	$12/.1 \pm 22.5$	-0.78
	02 08 54.26	4.3	+01 09 43.18	3.9	С	0.45 ± 0.10	<53.0	<20.6	32.3 ± 15.3	
J0209.0-0307	02 09 01.99	4.0	-03 07 20.39	2.8	S	0.66 ± 0.08	25.6 ± 23.2	<38.7	108.7 ± 29.0	-0.66
J0209.1-0622	02 09 06.85	5.3	-06 22 55.25	4.3	S	0.37 ± 0.08	<69.3	<33.8	47.9 ± 16.1	-0.78
10209 1-0308	02.09.07.12	3.5	-03 08 08 51	2.2	S	1.27 ± 0.09	17.6 ± 15.4	<31.5	18.5 + 84.8	-0.59
10200 5-0807	02 09 07.12	4.6	-08 07 47 21	17	ç	0.00 ± 0.16	17.0 ± 19.1	<11.5	10.5 ± 01.0 21.1 ± 15.2	-1.02
10209.5-0429	02 09 20.03	4.0	-08 07 47.21	4.7	5	0.90 ± 0.10	40.7 ± 20.9	-24.7	21.1 ± 13.2	-1.02
J0209.5-0438	02 09 30.97	4.3	-04 38 29.77	3.6	3	0.49 ± 0.08	37.4 ± 26.0	<34.7	36.6 ± 13.9	-0.27
J0209.5-0736	02 09 31.89	3.4	-07 36 44.66	2.1	Μ	3.63 ± 0.22	34.1 ± 7.9	30.3 ± 8.3	175.0 ± 27.4	-0.82
	02 09 34.92	5.0	-07 36 08.60	3.8	С	0.50 ± 0.11	<53.2	<43.8	78.6 ± 58.6	
J0209.6+0028	02 09 38.03	3.8	+00 28 36.81	3.2	S	0.41 ± 0.07	<40.7	<13.5	12.8 ± 14.3	-1.05
10209 6-0059	02 09 38 05	3.6	-00 59 57 52	24	S	0.74 ± 0.08	< 30.1	<26.9	1032 + 696	-0.48
10200 7-0330	02 09 30 30	3.0	-03 30 33 21	3.4	ŝ	0.71 ± 0.00	53.7 ± 18.6	<20.9	27.0 ± 6.0	-0.84
10209.7-0339	02 09 39.30	3.9	-03 39 33.21	3.4	5	0.60 ± 0.10	JJ.7 ± 10.0	< 30.8	27.0 ± 0.9	-0.64
J0209.7+0020	02 09 39.96	3.7	+00 20 47.11	2.7	3	0.04 ± 0.08	<35.1	<22.3	109.1 ± 22.3	-0.63
J0209.7-0338	02 09 41.48	4.3	-03 38 41.55	4.4	S	0.40 ± 0.08	<62.3	<35.1	11.5 ± 18.2	-0.72
J0209.8-0137	02 09 45.05	3.4	-01 37 37.51	2.0	S	4.57 ± 0.24	19.7 ± 7.7	<23.1	77.7 ± 9.6	-0.57
J0209.8-0512	02 09 45.62	3.7	-05 12 11.58	2.6	S	0.54 ± 0.06	27.7 ± 18.4	<16.3	38.2 ± 7.9	-0.58
10209 8-0200	02 09 45 90	49	-02 00 56 08	43	S	0.29 ± 0.07	< 52 5	<351	361 + 349	-0.66
10200 8-0237	02 00 46 21	3.0	-02 37 10 35	3.4	M	0.25 ± 0.01	<16.5	<12.3	25.0 ± 12.2	-0.52
J0209.8-0237	02 09 40.21	5.5	-02 37 10.33	2.4	C	0.20 ± 0.04	<40.J	<12.5	23.9 ± 12.2	-0.52
70200 0 0511	02 09 47.15	4.4	-02 37 09.39	3.3	C	0.09 ± 0.03	<31.4	< 0.0	55.5 ± 50.0	0.70
J0209.9-0511	02 09 52.26	4.8	-05 11 35.21	4.4	S	0.17 ± 0.04	<53.5	<25.6	36.4 ± 22.7	-0.69
J0210.2-0505	02 10 12.34	4.0	-05 05 32.35	2.9	S	0.29 ± 0.05	<35.1	<24.8	44.4 ± 36.6	-0.30
J0210.3-0007	02 10 16.09	4.7	-00 07 09.56	4.2	S	0.27 ± 0.06	<52.9	<25.7	145.6 ± 21.5	-0.55
10210 3-0344	02 10 16 19	3.5	-03 44 11 35	2.0	М	3.99 ± 0.23	83.4 + 7.1	24.9 + 8.4	97.8 ± 1.5	-0.83
0021010 0011	02 10 13 00	3.5	-03 44 07 77	2.1	C	1.00 ± 0.07	<30.1	<23.0	51.2 ± 21.7	0102
10210 2 0417	02 10 15.00	5.5	04 17 02 02	2.1	c c	1.00 ± 0.07	627 1 25 9	<20.9	51.2 ± 21.7 52.7 ± 6.9	0.96
J0210.3-0417	02 10 17.20	5.1	-04 17 02.92	3.7	S	0.01 ± 0.09	62.7 ± 25.8	< 30.8	33.7 ± 0.8	-0.80
J0210.3+0105	02 10 18.17	3.8	+01 05 19.86	2.8	S	0.86 ± 0.11	<43.2	<28.2	36.0 ± 19.6	-0.83
J0210.5-0055	02 10 29.73	3.9	-00 55 15.07	3.1	S	0.46 ± 0.07	<46.4	<23.1	29.1 ± 14.4	-0.79
J0210.6-0822	02 10 33.84	5.0	-08 22 18.97	4.9	S	0.77 ± 0.15	<69.4	<54.6	7.3 ± 40.2	-0.67
J0210.7-0014	02 10 40.26	3.6	-00 14 40.35	2.2	S	1.07 ± 0.09	<32.3	<26.9	83.6 ± 32.5	-0.70
10210.9_0633	02 10 53 70	12	-06 33 36 84	2.5	S	2.14 ± 0.20	67.8 ± 15.0	32.7 ± 14.3	84.2 ± 6.8	-0.41
10211.0 0220	02 10 55.70	2.0	02 20 26 17	2.0	S C	2.14 ± 0.20	07.0 ± 15.0	-02 7	150.5 ± 28.0	0.41
J0211.0-0529	02 10 39.99	5.9	-05 29 20.17	5.0	3	0.20 ± 0.04	< 34.1	<23.7	139.3 ± 38.0	-0.00
J0211.1-0644	02 11 05.68	3.4	-06 44 42.29	2.0	S	4.63 ± 0.25	41.7 ± 5.4	17.4 ± 9.5	46.8 ± 2.7	-0.66
J0211.1-0312	02 11 08.55	5.1	-03 12 45.95	4.8	S	0.21 ± 0.06	<53.0	<42.4	166.2 ± 65.2	-0.89
J0211.2-0735	02 11 09.87	5.3	-07 35 04.72	4.5	S	0.49 ± 0.11	<59.0	<49.8	42.0 ± 69.3	-0.48
J0211.3-0117	02 11 16.71	4.9	-01 17 55.45	5.3	S	0.35 ± 0.08	<77.1	<33.8	26.4 ± 13.6	-1.30
10211 3-0250	02 11 19 94	5.0	-02 50 19 19	43	ŝ	0.18 ± 0.05	< 47.2	<36.9	140.5 ± 65.1	-0.22
10211 4-0212	02 11 21 17	3.0	$-02\ 12\ 23\ 37$	28	ŝ	0.10 ± 0.03 0.20 ± 0.04	<35.5	<10.1	37.8 ± 21.0	-0.20
J0211.4 0112	02 11 21.17	4.1	-02 12 25.57	2.0	S C	0.29 ± 0.04	<27.0	<10.9	10.0 ± 21.7	0.70
J0211.4-0118	02 11 20.32	4.1	-01 18 01.90	3.5	3	0.19 ± 0.04	<37.9	<19.8	18.8 ± 27.5	-0.79
J0211.6-0025	02 11 33.88	4.3	-00 25 54.81	3.2	S	0.42 ± 0.07	<40.6	<35.8	118.8 ± 86.3	-0.65
J0211.6-0008	02 11 37.86	3.6	-00 08 17.29	2.3	S	0.71 ± 0.07	<31.5	<24.8	60.9 ± 33.0	-0.67
J0211.8-0920	02 11 46.78	5.3	-09 20 50.48	7.2	M	0.93 ± 0.21	65.0 ± 40.9	< 50.4	163.4 ± 13.1	-0.70
	02 11 48 03	5.3	-09 20 34 34	4.1	С	0.50 ± 0.11	<64.3	<31.6	53.0 ± 18.0	
10212 0-0027	02 12 01 31	57	-00 27 54 24	3.3	ç	0.20 ± 0.011	<63.5	~20.3	106.3 ± 13.4	-0.31
J0212.0-0027	02 12 01.51	J.7 1 E	-00 27 34.24	2.5	5	0.24 ± 0.00	<03.5	~20.3	100.3 ± 13.4	-0.51
J0212.0-0340	02 12 01.00	4.5	-03 40 49.55	3.5	3	0.20 ± 0.04	<40.0	<32.4	130.8 ± 08.0	-0.47
J0212.1-0307	02 12 05.72	3.4	-03 07 24.03	2.0	S	2.30 ± 0.13	20.4 ± 8.6	<21.0	37.5 ± 7.4	-0.82
J0212.1-0516	02 12 06.28	3.8	-05 16 39.01	2.8	S	0.39 ± 0.05	<38.7	<23.5	29.0 ± 20.1	-0.59
J0212.2+0130	02 12 10.84	3.4	+01 30 44.02	2.1	S	2.53 ± 0.16	16.8 ± 13.2	<16.2	149.6 ± 7.2	-0.87
10212.2-0550	02 12 13 77	3.9	-05 50 01 79	3.1	S	0.24 ± 0.04	< 38.9	<16.2	30.3 + 18.1	-0.62
10212.2 0000	02 12 16 82	3.8	-04 50 13 30	3 3	M	1.01 ± 0.11	57.2 ± 16.0	<10.1	113 ± 81	-0.72
J0212.J-0 4 J0	02 12 10.02	5.0	-04 50 15.50	1.1	C	1.01 ± 0.11	57.2 ± 10.7	<47.2	11.5 ± 0.1	-0.72
10010 4 0100	02 12 16.93	5.7	-04 51 11.22	4.4	C	0.29 ± 0.07	<01.8	<47.3	107.5 ± 47.0	0.61
J0212.4+0100	02 12 25.16	4.1	+01 00 55.98	4.3	2	0.46 ± 0.09	<57.2	<25.3	$1/3.1 \pm 15.0$	-0.61
J0212.5-0136	02 12 27.78	3.9	-01 36 13.89	2.6	S	0.49 ± 0.06	<40.3	<27.6	74.3 ± 22.8	-0.77
J0212.5+0118	02 12 28.78	3.5	+01 18 53.08	2.4	S	1.52 ± 0.14	23.5 ± 16.4	<22.7	154.1 ± 10.8	-0.78
J0212.5+0057	02 12 30.12	4.9	+005750.34	4.1	S	0.23 ± 0.06	<47.8	<24.4	136.0 ± 28.3	-0.77
10212 6-0759	02 12 33 38	53	-07 59 27 14	5.0	S	0.46 ± 0.10	< 78.2	<36.5	383 + 143	-0.63
10212.6 0921	02 12 35.30	27	08 21 25 74	2.5	M	1.82 ± 0.16	40.0 + 12.8	25.0 + 15.0	30.5 ± 14.5 24.0 ± 15.2	0.64
J0212.0-0821	02 12 33.27	5.7	-08 21 23.74	2.5	M	1.82 ± 0.10	40.9 ± 12.8	23.9 ± 13.0	24.0 ± 13.3	-0.04
	02 12 35.55	3.7	-08 20 33.95	2.5	C	1.69 ± 0.16	34.6 ± 13.9	31.0 ± 14.4	42.4 ± 69.0	
J0212.6-0104	02 12 36.86	4.3	-01 04 46.01	3.0	S	0.31 ± 0.05	<42.6	<28.0	76.2 ± 28.3	-0.73
J0212.7-0155	02 12 41.87	4.0	-01 55 51.68	3.1	S	0.20 ± 0.04	<30.0	<24.1	33.4 ± 75.6	-0.52
J0212.8-0335	02 12 45.83	3.7	-03 35 12.10	2.6	S	0.42 ± 0.05	<35.5	<23.9	10.3 ± 22.9	-0.75
10212 8-0336	02 12 46 14	42	-03 36 43 21	34	S	0.37 ± 0.06	< 50.6	< 35 3	1532 + 260	-0.96
10213.0 ± 0052	02 12 10.11	4.1	$\pm 00.5219.78$	2.0	ŝ	0.37 ± 0.00 0.73 ± 0.10	<51.6	<29.0	133.2 ± 20.0 128.3 ± 14.5	-0.74
IO212.1 0210	02 12 57.00	4 C	00 32 17.70	2.7	5	0.73 ± 0.10	<10.2	~27.0	120.3 ± 14.3 207 + 120	0.74
JU213.1-U219	02 13 03.43	4.2	-02 19 28.04	J.4	5	0.23 ± 0.04	<49.2 	<10.7	30.7 ± 13.0	-0.08
J0213.2-0141	02 13 11.91	3.5	-01 41 13.74	2.1	М	0.90 ± 0.07	<26.5	<23.9	57.0 ± 58.6	-0.80
	02 13 10.20	3.5	-01 40 57.27	2.2	С	0.80 ± 0.07	<28.1			
J0213.2-0457	02 13 12.38	3.4	-04 57 19.71	2.0	S	2.09 ± 0.12	26.5 ± 8.2	<21.7	41.9 ± 5.9	-0.60
J0213.2-0312	02 13 14.32	4.3	-03 12 09.43	2.9	S	0.61 ± 0.08	39.9 ± 21.0	<32.4	62.0 ± 11.4	-0.59
J0213 3-0719	02 13 17 08	3.7	-07 19 30 68	2.5	S	0.91 ± 0.09	30.4 + 16.1	<26.9	35.2 + 11.0	-0.32
I0213 3±0005	02 13 17 25	3.8	$\pm 00.05.23.72$	2.0	ç	0.13 ± 0.05	/38.8	~10.0	$1/8.6 \pm 17.0$	_0.94
10212.2 0420	02 13 17.23	J.0 / 1	04 20 14 67	2.7	5	0.73 ± 0.00	~50.0	~17.0	170.0 ± 17.0	-0.94
JU213.3-0420	02 13 19.82	4.1	-04 20 14.67	4.0	2	0.31 ± 0.06	<51.8	<24.6	$1/1.3 \pm 1/1.3$	-0.46
J0213.4-0434	02 13 23.79	3.5	-04 34 59.26	2.2	S	0.82 ± 0.07	<32.3	<24.1	48.5 ± 20.5	-0.85
J0213.4-0758	02 13 24.40	4.2	-07 58 24.13	3.4	S	0.62 ± 0.10	<53.5	<34.7	37.1 ± 20.4	-0.80
J0213.4-0419	02 13 24.77	3.5	-04 20 00.37	2.1	S	2.66 ± 0.17	52.1 ± 7.8	<28.5	91.6 ± 3.2	-0.99
J0213.4-0938	02 13 24.88	4.2	-09 38 00.98	3.9	S	0.95 ± 0.15	34.0 ± 27.9	<42.1	4.9 ± 21.4	-0.88

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Table A.2. continued.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{comp}	Major axis	Minor axis	Position	Spectral
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		J2000	arcsec	J2000	arcsec		Jy	arcsec	arcsec	Angle	index α_{74}^{1400}
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0213.7-0143	02 13 39.71	4.0	-01 43 02.85	3.3	S	0.13 ± 0.03	<27.6	<15.1	18.6 ± 45.5	-0.55
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0213.7-0345	02 13 43.47	4.7	-03 45 14.89	4.2	S	0.19 ± 0.05	<54.9	<19.0	38.4 ± 16.1	-0.65
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0213.8+0139	02 13 45.91	5.3	+01 39 48.81	3.9	S	0.37 ± 0.10	<47.6	<36.1	78.6 ± 57.5	-0.86
	J0213.8-0256	02 13 46.96	3.4	-02 56 43.04	2.1	S	3.21 ± 0.18	51.9 ± 5.8	<26.2	5.2 ± 2.1	-0.76
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0213.8-0342	02 13 47.40	4.1	-03 42 52.85	3.4	S	0.18 ± 0.04	<38.9	<12.2	32.6 ± 18.9	-0.57
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0213.9-0210	02 13 51.94	4.3	-02 10 53.43	4.2	S	0.14 ± 0.04	<43.5	<21.8	9.2 ± 28.1	-0.76
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0213.9-0253	02 13 56.37	4.7	-02 53 26.61	4.0	S	0.25 ± 0.06	<46.0			-0.68
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.3-0437	02 14 16.25	5.0	-04 37 10.06	3.6	S	0.39 ± 0.07	<63.1	<39.6	114.1 ± 20.7	-0.81
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.3-0153	02 14 16.55	3.5	-01 53 21.41	2.2	М	0.80 ± 0.07	<32.2	<24.7	127.8 ± 22.6	-0.60
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		02 14 14.49	4.0	-01 52 58.77	3.0	С	0.13 ± 0.03	<21.8			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.3-0422	02 14 20.36	3.7	-04 22 20.04	2.7	S	0.28 ± 0.04	<33.8	<16.2	22.9 ± 18.0	-0.77
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.4+0143	02 14 22.60	5.2	+01 43 26.52	4.9	S	0.59 ± 0.14	<60.8	<46.5	158.3 ± 47.0	-0.85
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.4-0555	02 14 25.45	3.9	-05 55 44.39	3.0	S	0.38 ± 0.05	<44.5	<22.5	30.5 ± 15.0	-0.58
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.5-0720	02 14 27.24	3.6	-07 20 09.43	2.4	S	1.13 ± 0.10	40.0 ± 12.1	<24.9	37.9 ± 6.2	-0.80
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.6-0603	02 14 36.38	3.5	-06 03 44.79	2.2	S	0.90 ± 0.07	26.1 ± 12.6	<16.4	46.7 ± 6.6	-0.71
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.6+0042	02 14 37.02	4.0	+00 42 30.60	3.9	S	0.74 ± 0.12	35.6 ± 26.8	<31.9	9.3 ± 12.9	-0.58
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.7-0004	02 14 44.58	6.1	-00 04 27.89	6.0	S	0.67 ± 0.13	75.7 ± 38.6	<36.8	41.1 ± 7.6	-0.89
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0214.8-0541	02 14 49.96	4.6	-05 41 57.19	4.1	S	0.42 ± 0.08	<56.7	<46.0	8.4 ± 46.5	-0.57
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.0-0458*	02 14 59.25	4.1	-04 58 07.65	3.6	S	0.17 ± 0.04	<40.1	<19.8	21.0 ± 24.6	-0.39
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.0-0453*	02 15 00.17	3.5	-04 53 50.48	2.6	S	1.19 ± 0.10	52.0 ± 11.6	<28.8	170.5 ± 4.8	-0.74
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.0+0114	02 15 01.51	3.4	+01 14 48.28	2.0	S	3.28 ± 0.20	22.5 ± 9.7	<24.5	136.2 ± 11.1	-0.93
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.1-0600	02 15 05.78	3.5	-06 00 50.90	2.2	S	0.97 ± 0.08	20.8 ± 14.9	<21.5	40.5 ± 10.5	-0.76
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.1-0702	02 15 08.03	3.4	-07 02 04.40	2.1	S	2.11 ± 0.13	39.5 ± 7.5	<24.0	45.6 ± 3.9	-0.67
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.2-0135	02 15 10.00	3.4	-01 35 27.27	2.0	S	1.71 ± 0.10	25.2 ± 9.0	<17.9	60.7 ± 5.3	-1.04
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.2-0343*	02 15 11.52	3.5	-03 43 12.08	2.2	S	0.68 ± 0.05	<32.0	<14.2	42.5 ± 9.1	-0.43
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.3+0030	02 15 15.79	3.8	+00 30 32.18	3.0	M	0.52 ± 0.08	<39.5	<20.7	178.8 ± 18.1	-0.67
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		02 15 16.80	4.0	+00 30 34.04	3.6	С	0.32 ± 0.06	<49.1	<3.1	154.2 ± 10.8	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.3-0153	02 15 17.14	3.5	-01 53 32.72	2.1	S	0.75 ± 0.06	<20.7	<17.0	63.3 ± 46.0	-0.81
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.3+0050	02 15 17.38	4.6	+00 50 21.82	4.4	S	0.33 ± 0.08	<52.8	<28.2	155.8 ± 24.2	-0.66
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.3+0040	02 15 19.03	3.5	+00 40 44.88	2.3	S	1.19 ± 0.11	<33.2	<22.5	144.5 ± 17.7	-0.58
$ \begin{array}{llllllllllllllllllllllllllllllllllll$	J0215.6-0756	02 15 34.22	4.3	-07 56 08.22	4.0	S	0.35 ± 0.07	<51.8	<36.7	7.7 ± 32.0	-0.59
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.6-0321*	02 15 34.47	3.8	-03 22 00.00	2.9	S	0.67 ± 0.08	41.0 ± 17.1	<26.8	31.0 ± 8.2	-0.61
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.6-0711	02 15 34.98	4.4	-07 11 00.46	3.2	S	0.63 ± 0.09	38.2 ± 23.2	<39.4	57.0 ± 16.9	-0.54
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.6-0206	02 15 37.39	3.5	-02 06 05.80	2.2	S	0.62 ± 0.06	<25.2	<18.1	53.6 ± 28.9	-0.93
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.7-0056	02 15 39.61	3.7	-00 56 59.28	2.4	S	0.62 ± 0.07	<36.1	<23.1	100.3 ± 18.7	-0.97
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.7-0222*	02 15 41.89	3.4	-02 22 55.03	2.0	S	5.29 ± 0.27	19.0 ± 7.3	<21.1	19.3 ± 6.1	-0.81
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.7-0057	02 15 44.17	4.1	-00 57 11.24	2.6	S	0.45 ± 0.06	<41.8	<23.5	83.2 ± 18.0	-0.95
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.7+0133	02 15 44.46	5.0	+01 33 18.38	4.4	S	0.50 ± 0.12	<58.6	<34.0	139.7 ± 25.1	-0.56
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.8-0142	02 15 44.99	3.5	-01 42 50.53	2.1	S	0.78 ± 0.06	<20.5	<10.2	76.1 ± 17.6	-0.60
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.9-0359*	02 15 52.26	4.3	-03 59 51.32	3.5	S	0.11 ± 0.03	<28.7			-0.25
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0215.9+0025	02 15 56.51	5.2	+00 25 23.27	4.0	S	0.33 ± 0.08	<57.4	<31.1	53.6 ± 23.0	-0.70
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0216.0-0825	02 15 57.56	5.2	-08 25 15.24	5.7	S	0.43 ± 0.10	5.2</td <td><49.4</td> <td>166.9 ± 27.2</td> <td>-0.58</td>	<49.4	166.9 ± 27.2	-0.58
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0216.0-0350*	02 15 58.66	7.7	-03 50 27.56	3.8	M	0.30 ± 0.07	51.3 ± 46.3	<35.1	84.4 ± 10.9	-0.82
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	102160 0244*	02 15 57.81	4.3	-03 50 44.79	3.8	C	0.11 ± 0.03	<38.1	<16.9	153.6 ± 28.5	0.70
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0216.0-0344*	02 15 59.79	3.5	-03 44 21.49	2.2	S	0.92 ± 0.07	<31.3	<25.0	59.9 ± 23.2	-0.70
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0216.2-0011	02 16 13.94	3.9	-00 11 39.46	3.0	S	0.42 ± 0.06	<36.9	<29.9	21.0 ± 51.2	-0.82
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0216.3+0008	02 16 16.54	3.4	+00 08 58.67	2.1	5	1.12 ± 0.09	<24.6	<15.9	100.7 ± 17.0	-0.60
$ \begin{array}{c} J0216.5-0243^\circ 0216\ 20.11 4.0 -0245\ 30.82 2.9 S 0.52\pm 0.07 <44.1 <33.4 155.4\pm 30.0 -0.37 \\ 021624.64 -0917 0216\ 23.69 4.9 -0917\ 24.86 3.8 S 0.36\pm 0.08 <51.8 <35.2 55.8\pm 33.1 -0.82 \\ J0216.5-0623 0216\ 29.22 4.4 -06\ 23\ 51.55 4.3 S 0.18\pm 0.04 <49.4 <25.9 15.9\pm 24.6 -0.54 \\ J0216.6-0024 0216\ 36.81 4.8 -00\ 24\ 54.03 4.1 S 0.33\pm 0.07 <50.6 <37.6 34.2\pm 44.7 -0.67 \\ J0216.7-0933 0216\ 40.20 4.4 -09\ 53\ 43.33 3.6 S 0.66\pm 0.12 <51.2 <39.2 29.9\pm 37.3 -0.56 \\ J0216.7-0444^\circ 0216\ 42.23 3.8 -06\ 13\ 45.08 2.7 S 0.43\pm 0.06 <40.6 <28.1 40.8\pm 23.0 -0.76 \\ J0216.8-0337^\circ 0216\ 42.23 3.8 -06\ 13\ 45.08 2.7 S 0.43\pm 0.06 <40.6 <28.1 40.8\pm 23.0 -0.76 \\ J0216.8-0337^\circ 0216\ 45.73 4.0 -0.3\ 71\ 8.54 4.5 S 0.24\pm 0.07 <50.7 \dots \dots -0.72 \\ J0216.8-0337^\circ 0216\ 45.73 4.0 -0.3\ 71\ 8.54 4.5 S 0.24\pm 0.07 <50.7 \dots \dots -0.72 \\ J0216.8-0337^\circ 0216\ 45.79 5.5 -02\ 37\ 18.64 4.5 S 0.24\pm 0.07 <50.7 \dots \dots -0.72 \\ J0217.0-0449^\circ 0216\ 59.937 4.3 -01\ 55\ 12.14 3.0 S 0.27\pm 0.05 <41.8 <23.2 61.9\pm 2.3.7 -0.67 \\ J0217.0-0459^\circ 021\ 65\ 9.37 4.3 -00\ 55\ 7.02 2.8 S 1.29\pm 0.14 38.5\pm 16.7 <30.8 37.4\pm 10.3 -0.82 \\ J0217.0-063 02\ 17\ 02.58 3.5 -06\ 03\ 27.39 2.2 S 0.69\pm 0.06 <35.8 <20.5 47.1\pm 10.8 -1.44 \\ J0217.1-0219^\circ 02\ 17\ 03.16 3.8 -09\ 54\ 50.12 2.8 S 1.29\pm 0.14 38.5\pm 16.7 <30.8 37.4\pm 10.3 -0.82 \\ J0217.0-063 02\ 17\ 02.58 3.5 -06\ 03\ 27.39 2.2 S 0.69\pm 0.06 <35.8 <20.5 47.1\pm 10.8 -1.44 \\ J0217.1-0219^\circ 02\ 17\ 03.16 3.8 -08\ 20\ 46.04 2.8 S 0.99\pm 0.01 35.2\pm 17.2 <33.2 8.5\pm 12.1 -0.82 \\ J0217.1-0422^\circ 02\ 17\ 03.16 3.8 -08\ 20\ 46.04 2.8 S 0.99\pm 0.01 35.2\pm 17.2 <33.2 8.5\pm 12.1 -0.82 \\ J0217.3-0326^\circ 02\ 17\ 18.19 4.1 -08\ 20\ 40.04 2.8 S 0.99\pm 0.01 35.2\pm 17.2 <33.2 8.5\pm 12.1 -0.82 \\ J0$	J0216.3-0010	02 16 19.84	3.7	-00 10 59.43	2.5	5	0.39 ± 0.05	<23.6			-0.58
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0216.3-0245*	02 16 20.11	4.0	-02 45 30.82	2.9	5	0.52 ± 0.07	<44.1	<33.4	135.4 ± 30.0	-0.37
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10216 4 0017	02 16 24.64	5.4	-02 45 18.69	3.9	5	0.43 ± 0.09	<64.6	<47.6	83.0 ± 33.4	-0.37
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0216.4-0917	02 16 23.09	4.9	-09 17 24.80	3.8	5	0.30 ± 0.08	<31.8	<35.2	35.8 ± 35.1	-0.82
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0210.3-0023	02 10 29.22	4.4	-00 25 51.55	4.5	3 5	0.18 ± 0.04	<49.4	<23.9	13.9 ± 24.0	-0.54
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0210.0-0024	02 10 30.81	4.0	-00 24 34.03	4.1	3 5	0.55 ± 0.07	< 30.0	< 37.0	34.2 ± 44.7	-0.07
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0210.7-0935	02 16 40.20	4.4	-09 33 43.33	2.0	3 5	0.00 ± 0.12	<31.2	< 39.2	29.9 ± 57.5	-0.50
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10216.7-0444	02 10 40.93	4.7	-04 44 05.30	2.9	5	0.19 ± 0.04	<49.0	<27.5	42.1 ± 24.4	-0.23
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10216.8 0227*	02 10 42.23	5.0 4.0	-00 13 43.08	2.7	5	0.43 ± 0.00	<40.0	<20.1	40.8 ± 23.0	-0.70
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0210.8-0337*	02 10 45.75	4.0	-03 37 18.34	5.0 4.5	5	0.27 ± 0.03	< 38.3	<23.3	44.9 ± 29.2	-0.37
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0210.8-0237*	02 10 40.79	1.9	-02 37 18.04	4.5	5	0.24 ± 0.07	<50.7	-50.2	24.4 + 20.5	-0.72
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0217.0-0449*	02 10 38.91	4.0	-04 30 00.78	4.2	5	0.40 ± 0.08	< 07.1	< 14.0	34.4 ± 30.3	-1.52
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10217.0 0155	02 10 39.09	4.0	-04 46 43.92	2.0	5	0.40 ± 0.09	03.1 ± 33.4	<44.0	10.1 ± 11.1	-1.52
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10217.0-0155	02 10 39.37	4.5	$-01\ 55\ 12.14$ $-09\ 54\ 50\ 12$	2.0	S	0.27 ± 0.03 1 20 ± 0.14	<41.0 385 ± 167	<23.2	01.9 ± 23.7 37.4 ± 10.3	-0.87
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10217.0-0554	02 17 02.24	3.5	-0003700.12	2.0	S	1.27 ± 0.14 0.69 ± 0.06	25 8	<20.5	47.1 ± 10.3	-1.44
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10217 1_0210*	02 17 02.56	<i>J</i> . <i>J</i>	-000527.55 -02105176	2.2	M	0.07 ± 0.00	<17.0	<10.1	$\frac{47.1 \pm 10.0}{87.0 \pm 8.3}$	-0.58
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	30217.1-0210	02 17 03.13	37	-02 10 37 61	2.7	C	0.19 ± 0.03	<14.6	×10.1	80.5 ± 43.4	0.50
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	I0217 1_0820	02 17 03 16	3.8	-08 20 46 04	2.7	S	0.19 ± 0.03 0.99 ± 0.11	352 + 172	 <37 5	285 ± 175	-0.28
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	I0217.1-0020	02 17 05 70	4.0	-04 22 54 75	2.0	S	0.40 ± 0.06	<49.4	<23.9	20.5 ± 17.5 48.9 ± 12.4	-0.59
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0217 3-0825	02 17 18 19	4.1	-08 25 17 10	4.2	S	0.56 ± 0.00	40.8 + 27.2	<33.2	8.5 ± 12.4	-0.82
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0217.3-0326*	02 17 19 73	4.2	-03 26 03 67	3.0	ŝ	0.32 ± 0.05	<41.2	<34.0	90.8 ± 52.3	-0.79
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J0217 3+0155	02 17 20 64	3.4	+01552345	2.1	ŝ	3.68 ± 0.25	31.8 ± 9.4	<23.9	152.6 + 6.4	-0.98
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10217 4-0339*	02 17 20.04	4.6	-03 39 48 20	3.3	Š	0.22 ± 0.05	<43.7	<29.2	62.0 + 33.9	-0.48
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	J0217 4-0618	02 17 22 81	3.7	-06 18 31 15	2.7	Š	0.19 ± 0.03	<31.3		29.2 + 12.4	-0.49
J0217.4-0015 02 17 25.10 4.7 -0015 47.82 4.2 S 0.27 + 0.07 <45.9 <34.6 156.7 + 54.7 -0.75	J0217.4-0200	02 17 24 50	3.7	-02 00 06 19	2.6	Š	0.16 ± 0.03	<16.7		1.6 ± 47.7	-0.64
	J0217.4-0015	02 17 25.10	4.7	-00 15 47.82	4.2	ŝ	0.27 ± 0.07	<45.9	<34.6	156.7 ± 54.7	-0.75

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Table A.2. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		Jy	arcsec	arcsec	Angle	index α_{74}^{1400}
J0217.5-0052	02 17 28.41	3.4	-00 52 29.80	2.0	S	1.23 ± 0.08	<19.3			-0.58
J0217.5-0725	02 17 28.80	5.0	-07 25 52.52	4.6	S	0.25 ± 0.06	<56.1	<42.9	30.6 ± 48.2	-0.76
J0217.5-0047	02 17 32.26	3.6	-00 47 01.31	2.3	S	0.71 ± 0.07	<37.3	<18.0	56.2 ± 11.2	-0.65
J0217.6-0313*	02 17 33.98	4.1	-03 13 10.13	3.3	S	0.24 ± 0.04	<49.2	<11.1	35.2 ± 11.0	-0.67
J0217.7-0917	02 17 40.92	6.1	-09 17 35.75	4.4	S	0.65 ± 0.14	43.9 ± 37.7	<48.8	65.3 ± 19.2	-0.80
J0217.7-0541*	02 17 41.17	4.0	-05 41 55.48	2.8	S	0.54 ± 0.07	<46.2	<39.5	89.7 ± 45.9	-0.72
J0217.8-0157	02 17 46.14	3.8	-01 57 19.29	2.6	S	0.34 ± 0.05	<27.7	<21.3	51.7 ± 51.2	-0.78
J0217.8-0030	02 17 46.35	3.4	-00 30 33.86	2.2	Μ	4.54 ± 0.26	76.2 ± 6.7	<21.2	155.1 ± 1.2	-0.93
10017 0 0000	02 17 44.51	3.6	-00 29 45.96	2.2	C	0.32 ± 0.04	<19.8		64.6 ± 10.4	1.07
J0217.8+0008	02 17 48.21	3.6	+00 08 58.74	2.4	S	1.00 ± 0.10	<36.0	<29.0	58.5 ± 29.0	-1.06
J0217.8+0144	02 17 48.45	3.4	+01 44 48.08	2.1	5	2.84 ± 0.19	22.5 ± 11.0	<22.8	153.0 ± 9.8	-0.44
J0217.9-0030	02 17 50.87	4.1	-00 30 00.01	3.3	5	0.26 ± 0.03	< 37.0	<19.3	30.4 ± 20.7	-1.13
J0218.0-0918	02 17 38.18	4.5	-09 18 18.91	4.2	S S	0.73 ± 0.12	42.7 ± 20.0	< 38.5	21.3 ± 14.0 127.6 ± 72.4	-0.78
J0218.2-0301 I0218 3_0121	02 18 11.79	4.2	-03 01 28.03 -01 21 38 20	3.2 4 7	S	0.33 ± 0.00	< 39.0	<33.9	127.0 ± 72.4 67 ± 35.0	-0.79
10218 3_0446*	02 18 15.01	4.0	$-01\ 21\ 38.20$ $-01\ 46\ 08\ 13$	2.0	S	0.19 ± 0.03 0.30 ± 0.04	<35.5	<20.8	0.7 ± 33.9 0.8 + 22.9	-0.53
J0218.5-0440	02 18 18.05	3.5	-04 54 38 95	2.9	S	0.30 ± 0.04 0.80 ± 0.06	<34.1	<16.3	41.8 ± 8.2	-0.55
10218 6-0923	02 18 34 74	4 5	-09 23 38 45	47	S	0.50 ± 0.00 0.50 ± 0.10	<72.5	<28.8	262 ± 113	-0.39
J0218.6-0725	02 18 38 06	3.6	$-07\ 25\ 29.04$	2.3	S	0.98 ± 0.08	35.1 + 12.6	<24.2	48.5 + 7.3	-0.64
J0218.7-0441*	02 18 39.62	3.5	-04 41 50.61	2.2	Š	0.65 ± 0.06	<29.9	<25.0	38.2 ± 36.0	-0.84
J0218.7-0015	02 18 39.85	4.7	-00 15 07.84	3.7	ŝ	0.25 ± 0.06	<41.3	<32.8	54.2 ± 69.0	-0.57
J0218.8-0836	02 18 45.56	4.2	-08 36 57.88	3.4	S	0.21 ± 0.05	<32.9			-0.20
J0218.8-0211*	02 18 50.73	3.4	-02 11 16.64	2.0	S	1.79 ± 0.11	<24.0	<16.8	46.5 ± 12.5	-0.68
J0218.9-0812	02 18 54.95	4.1	-08 12 54.21	3.5	S	0.71 ± 0.10	36.9 ± 22.3	<44.9	16.7 ± 25.4	-0.42
J0219.0-0149	02 18 57.06	3.5	-01 49 11.44	2.2	S	0.81 ± 0.07	<25.0	<18.5	71.8 ± 27.3	-0.52
J0219.0-0155	02 18 57.62	3.6	-01 55 33.98	2.3	S	0.43 ± 0.05	<25.9	<9.5	66.7 ± 18.4	-0.65
J0219.1+0120	02 19 06.59	3.5	+01 20 56.05	2.2	S	2.04 ± 0.16	26.9 ± 12.4	<24.3	167.3 ± 9.7	-0.49
J0219.1-0252*	02 19 07.28	3.4	-02 52 51.85	2.1	S	0.89 ± 0.06	<23.5	<16.4	60.0 ± 19.9	-0.43
J0219.1-0357*	02 19 08.39	4.8	-03 57 50.95	3.6	M	0.19 ± 0.04	<45.4	<32.2	58.0 ± 42.2	-0.59
	02 19 08.82	4.1	-03 58 06.53	3.3	С	0.08 ± 0.02	<27.0		36.3 ± 32.3	
J0219.2-0344*	02 19 11.19	4.8	-03 44 31.78	3.6	S	0.14 ± 0.04	<41.0	<28.0	69.8 ± 46.7	-0.46
J0219.3-0152	02 19 17.92	4.7	-01 52 49.56	3.7	S	0.32 ± 0.07	<48.8	<29.9	129.4 ± 28.3	-0.71
J0219.3-0552*	02 19 18.21	4.9	-05 52 43.70	4.3	S	0.29 ± 0.06	<67.5	<26.2	42.1 ± 12.8	-0.63
J0219.3-0244*	02 19 20.05	4.6	-02 44 11.83	3.5	S	0.38 ± 0.07	<55.4	<31.0	48.7 ± 18.8	-0.62
J0219.3-0051	02 19 20.20	4.8	-00 51 36.57	3.3	S	0.21 ± 0.05	<44.6	<15.7	118.3 ± 19.7	-0.33
J0219.5-0539*	02 19 28.28	5.4	-05 39 47.63	2.0	5	3.89 ± 0.20	20.6 ± 7.1	<19.5	49.6 ± 4.5	-0.76
J0219.3+0024 I0210.5_0251*	02 19 28.49	2.5	+00.24.57.24	5.4 2.1	S S	0.43 ± 0.09	<03.5	<18.0	36.0 ± 9.8	-0.09
10219.5-0251	02 19 29.94	3.5	-02 31 12.00	2.1	M	0.93 ± 0.07	<31.0	<13.2	93.0 ± 0.7 120.0 ± 10.3	-0.72
J0219.J=0058	02 19 31.30	3.5	-005820.03	3.8	C	0.31 ± 0.03	<58.4	<10.0	129.9 ± 19.3 172.8 ± 0.8	-0.85
10219 5-0747	02 19 32 26	5.0 4.7	-005052.02 -07473959	3.5	S	0.49 ± 0.08 0.54 + 0.09	42.8 ± 26.0	<37.9	54.6 ± 13.7	-0.47
10219 6-0944	02 19 32.20	4.7	-09440227	4 5	S	0.54 ± 0.09 0.59 ± 0.12	<62.0	<49.6	21.0 ± 15.7 21.9 ± 46.6	-1.01
10219.7-0400	02 19 41 51	6.3	-04 00 30 39	9.5	S	1.34 ± 0.12	172.2 ± 50.1	31.3 + 25.6	1534 + 35	-1.15
J0219.8+0001	02 19 44.99	3.7	+00.01.57.18	2.8	S	0.41 ± 0.06	<31.7	<16.5	4.8 ± 23.3	-0.50
J0219.9-0518*	02 19 52.98	3.9	-05 18 28.29	4.0	Š	0.20 ± 0.04	<53.0	<10.7	166.6 ± 11.1	-0.76
J0219.9-0732	02 19 55.34	4.3	-07 32 01.63	3.7	Ŝ	0.34 ± 0.06	<51.6	<35.1	24.9 ± 27.1	-0.62
J0220.0-0447*	02 19 57.58	3.9	-04 47 49.90	3.3	S	0.29 ± 0.05	<44.8	<25.9	11.7 ± 20.4	-0.65
J0220.0+0155	02 19 58.05	3.5	+01 55 32.44	2.3	М	2.21 ± 0.19	24.7 ± 14.6	<32.3	176.4 ± 24.3	-0.60
	02 19 58.61	3.6	+01 56 08.31	2.4	С	1.11 ± 0.12	<27.5			
J0220.0-0155	02 19 59.06	3.7	-01 55 37.06	2.5	S	0.70 ± 0.09	<32.4	<19.4	35.1 ± 21.2	-0.73
J0220.0-0143	02 20 02.01	4.0	-01 43 50.48	3.1	S	0.42 ± 0.07	<41.3	<15.6	143.8 ± 16.1	-0.70
J0220.0-0000	02 20 02.73	5.0	-00 00 22.08	4.3	S	0.28 ± 0.07	<48.4	<37.1	42.6 ± 58.0	-0.63
J0220.2-0723	02 20 08.95	4.0	-07 23 49.10	4.5	S	0.48 ± 0.08	51.7 ± 25.5	<31.6	176.6 ± 8.9	-0.78
J0220.5+0152	02 20 31.74	4.0	+01 52 38.03	3.1	S	0.54 ± 0.10	<32.8	<24.0	5.5 ± 48.8	-0.96
J0220.5+0027	02 20 32.50	3.8	+00 27 59.43	2.8	S	0.69 ± 0.09	<37.9	<26.0	154.5 ± 24.6	-0.60
J0220.6+0232	02 20 36.58	4.4	+02 32 12.69	3.8	S	0.74 ± 0.15	<52.3	<25.9	148.0 ± 18.4	-0.84
J0220.7-0149	02 20 43.51	3.7	-01 49 58.16	2.5	S	0.51 ± 0.07	<18.5			-0.40
J0220.8-0333*	02 20 49.38	3.6	-03 33 17.48	2.4	S	0.32 ± 0.04	<20.6			-0.37
J0220.9-0601*	02 20 52.46	5.3	-06 01 15.63	3.2	S	0.25 ± 0.05	<59.0	<28.0	89.7 ± 16.5	-0.72
J0220.9-0156*	02 20 54.15	3.4	-01 56 53.84	2.0	S	40.51 ± 2.03	<20.0	<15.0	43.3 ± 1.4	-0.83
J0220.9-0725	02 20 54.82	3.7	-07 25 44.85	2.8	5	0.42 ± 0.05	<46.8	<18.2	29.5 ± 9.9	-0.50
10220.9-0348* 10220.0-0210*	02 20 33.71	3.4	-03 40 34.07	2.0	с С	1.17 ± 0.07 0.33 ± 0.06	<24.3 <167	\14.0	37.4 ± 10.3 24.5 ± 8.4	-0.90
$J0220.9-0219^{\circ}$ $J0221.0\pm0231$	02 20 30.00	3.8 4.0	-021902.27	3.5	S	0.33 ± 0.00	<40.7		24.3 ± 0.4	-1.42
10221.0+0231	02 21 02.39	+.⊅ 3⊿	+00 59 38 05	2.0	S	3.30 ± 0.14 2 30 + 0 1/	<72.0 <25.1	 <14 0	 177 6 + 8 5	-0.70
I0221.1+0039	02 21 03.28	43	$-02\ 46\ 30\ 71$	2.0	S	2.37 ± 0.14 0.32 + 0.07	<47.0	<31.5	1667 + 326	-0.67
J0221 1-0240	02 21 05.50	3.8	-09 31 46 69	2.9	S	0.65 ± 0.07	<45.2	<23.8	31.8 + 14.5	-0.75
J0221.2-0146	02 21 13 38	3.6	-01 46 04 81	2.8	Š	1.56 ± 0.16	41.8 ± 14.9	<22.4	9.1 ± 6.3	-0.82
J0221.3-0015	02 21 15.60	3.9	-00 15 57.30	4.1	M	0.52 ± 0.07	59.9 ± 23.0		24.8 ± 3.4	-0.73
	02 21 14.21	3.8	-00 16 04.41	2.7	C	0.20 ± 0.04	<20.7		33.9 ± 34.2	
	02 21 16.98	3.7	-00 15 47.96	2.5	Ċ	0.16 ± 0.03	<14.3		33.8 ± 22.2	
J0221.3-0255*	02 21 16.22	3.6	-02 55 49.68	2.4	S	0.42 ± 0.05	<27.1	<12.3	50.9 ± 19.2	-0.49
J0221.3+0141	02 21 18.76	3.4	+01 41 08.81	2.0	S	5.09 ± 0.30	37.5 ± 6.7	<26.7	39.2 ± 4.2	-1.14
J0221.3-0305*	02 21 19.55	4.7	-03 05 47.27	4.0	S	0.28 ± 0.06	<49.0	<37.5	33.3 ± 48.4	-0.97

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Table A.2. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		Jy	arcsec	arcsec	Angle	index α_{74}^{1400}
J0221.7-0451*	02 21 42.11	3.6	-04 51 10.45	2.4	S	0.63 ± 0.06	<36.2	<28.8	58.8 ± 28.5	-0.83
J0221.7-0413*	02 21 43.07	3.4	-04 13 44.86	2.0	S	2.41 ± 0.13	<24.2	<17.7	41.4 ± 8.0	-0.51
J0221.8-0925	02 21 50.83	4.6	-09 25 05.03	4.7	S	0.29 ± 0.07	<66.2	<19.2	31.7 ± 11.7	-0.53
J0222.0-0240*	02 22 00.59	3.6	-02 40 08.69	2.2	S	1.30 ± 0.11	43.0 ± 11.5	<15.9	122.2 ± 4.1	-0.72
J0222.1-0620	02 22 03.21	4.5	-06 20 03.52	4.1	5	0.16 ± 0.04	<46.4	<27.1	152.2 ± 31.0 150.5 ± 12.0	-0.66
J0222.1+0101	02 22 03.43	5.9 2.4	+01 01 05.89	3.0 2.1	5	0.30 ± 0.07	<4/.0	<11.0	159.5 ± 12.0 165.6 ± 11.4	-0.01
J0222.1+0137	02 22 03.09	3.4	+013721.43 -00003437	2.1	S	2.14 ± 0.14	<29.0	<19.0	103.0 ± 11.4 55.0 ± 35.0	-0.71
10222.3-0009	02 22 17.04	3.5	-000934.37 -02422089	2.1	S	0.83 ± 0.07 0.90 + 0.07	<20.9	<18.4	175.0 ± 55.9	-1.07
10222.5 0242	02 22 20.04	3.6	+00592545	2.3	S	0.90 ± 0.07 0.83 ± 0.08	<26.5	<19.1	179.2 ± 00.2 150.6 ± 29.9	-0.72
J0222.5-0817	02 22 28.19	4.3	-08 17 08.81	4.0	M	0.26 ± 0.06	<46.6	<31.4	9.0 ± 34.7	-0.64
	02 22 29.57	3.8	-08 17 07.16	4.3	С	0.16 ± 0.04	<51.4		173.8 ± 10.7	
J0222.5-0307*	02 22 28.48	4.0	-03 07 42.30	3.7	S	0.18 ± 0.04	<40.7	<16.3	7.9 ± 20.8	-0.71
J0222.6-0614	02 22 33.14	4.5	-06 14 46.89	4.4	S	0.22 ± 0.05	<52.4	<33.8	7.9 ± 31.2	-0.80
J0222.7+0059	02 22 38.93	3.5	+00 59 20.03	2.3	S	1.04 ± 0.10	<27.7	<23.3	171.7 ± 45.3	-0.67
J0222.8+0028	02 22 45.61	4.3	+00 28 24.97	3.0	M	0.22 ± 0.05	<31.2	<18.5	73.5 ± 39.9	-0.59
	02 22 45.58	3.7	+00 28 08.49	2.8	С	0.21 ± 0.04	<26.4		26.2 ± 19.1	
J0222.9-0009	02 22 51.19	4.1	-00 09 57.09	2.8	S	0.45 ± 0.07	<42.1	<23.6	56.0 ± 19.3	-0.64
J0222.9-0942	02 22 53.18	4.7	-09 42 55.03	4.0	S	0.37 ± 0.08	<51.5	<33.8	40.0 ± 31.5	-0.82
J0222.9-0311*	02 22 53.94	4.1	-03 11 32.56	2.9	S	0.20 ± 0.04	<34.3	<17.5	55.9 ± 26.9	-1.10
J0222.9-0518*	02 22 55.86	3.4	-05 18 16.63	2.0	S M	1.56 ± 0.09	<26.2	<21.2	35.0 ± 14.5	-0.60
J0223.0-0242*	02 22 50.05	3.4 2.4	-02 43 04.05	2.0	M	2.37 ± 0.13	<17.9	<13.2	71.0 ± 22.0	-0.78
10222 0-0602	02 22 36.38	3.4 4.0	-024234.48 -06020670	2.0	c c	1.87 ± 0.11 0.15 ± 0.03	<24.2	<17.2	04.9 ± 10.0 10.6 \pm 57.1	-0.40
10222.9-0002 10222 9_0424*	02 22 56.58	4.0	-00.02.00.79 -04.24.50.37	3.1	S	0.15 ± 0.05 0.25 ± 0.05	<20.5	<30.5	10.0 ± 57.1 30.5 ± 41.8	-0.40
10223 0-0630	02 22 58.07	41	-06305220	3.0	M	0.25 ± 0.05 0.25 ± 0.04	<45.7	< 8.8	453 ± 112	-0.50
30223.0 0030	02 22 58.46	5.1	-06 31 04.47	4.0	C	0.22 ± 0.01 0.22 ± 0.05	<47.3	<38.9	71.9 ± 76.3	0.01
J0223.0-0606	02 23 01.41	3.9	-06 06 26.01	3.5	Š	0.11 ± 0.03	<31.8		6.0 ± 21.8	-0.67
J0223.0-0826	02 23 01.93	4.5	-08 26 09.49	3.6	S	0.68 ± 0.10	41.6 ± 24.5	<40.5	45.9 ± 15.8	-0.54
J0223.1-0107	02 23 03.01	3.5	-01 07 46.46	2.2	S	0.49 ± 0.05	<19.3	<15.6	107.0 ± 66.2	-0.98
J0223.2-0750	02 23 11.77	3.6	-07 50 31.67	2.3	S	1.26 ± 0.10	35.6 ± 11.5	<32.2	58.4 ± 10.6	-0.65
J0223.2-0205*	02 23 12.89	3.7	-02 05 10.06	2.3	S	0.29 ± 0.04	<22.6	<5.6	119.1 ± 22.6	-0.26
J0223.3-0142	02 23 18.67	4.5	-01 42 04.29	3.9	S	0.21 ± 0.05	<41.0	<32.3	174.2 ± 66.9	-0.70
J0223.3-1023	02 23 20.80	4.7	-10 23 20.46	5.0	S	0.66 ± 0.14	<67.6	<42.6	177.1 ± 23.5	-0.99
J0223.4+0134	02 23 26.37	4.7	+01 34 16.40	4.9	S	0.54 ± 0.12	<67.9	<34.1	154.8 ± 17.1	-0.81
J0223.5+0139	02 23 32.28	5.0	+01 39 58.88	3.3	S	0.25 ± 0.06	<43.1	<22.3	102.3 ± 29.4	-0.72
J0223.6-0857	02 23 32.99	5.6	-08 5 / 42.89	5.6	S	0.41 ± 0.10	<68.7	<53.9	162.2 ± 51.1	-0.53
J0223.0-0301*	02 23 33.10	3.5	-03 01 24.99	2.3	5	0.47 ± 0.05	<22.2	<19.2	10.1 ± 73.3	-0.82
10223.0-0713	02 23 33.22	4.0	-071330.92 -02321836	2.2	S	0.81 ± 0.10 0.56 ± 0.05	41.0 ± 10.3	<43.9	21.1 ± 22.0 55.8 + 1/1.0	-0.00
10223.0-0232	02 23 34.03	3.5	$-02\ 32\ 18.30$ $-06\ 37\ 22\ 32$	2.2	S	0.30 ± 0.05 0.73 ± 0.06	<30.0	<74.5	51.0 ± 44.9 51.2 ± 32.0	-0.83
10223 6-0213*	02 23 37.95	3.6	-02.13.55.29	2.5	S	0.75 ± 0.00 0.25 ± 0.03	<22.6	<4.6	37.4 + 23.7	-0.89
J0223.7-0239*	02 23 41.59	3.5	-023944.16	2.2	Š	0.61 ± 0.05	<23.2	<16.8	54.2 ± 28.1	-0.84
J0223.7-0158	02 23 43.28	4.1	-01 58 35.77	3.4	Ŝ	0.10 ± 0.03	<25.9	<16.4	176.0 ± 67.2	-0.71
J0223.7+0040	02 23 44.00	3.9	+00 40 48.97	2.7	S	0.44 ± 0.07	<32.9	<22.8	125.5 ± 34.1	-0.64
J0223.8-0340*	02 23 45.29	3.8	-03 40 42.32	2.9	S	0.24 ± 0.04	<31.2	<21.0	9.8 ± 35.9	-0.62
J0223.8-0332*	02 23 46.46	4.9	-03 32 37.04	3.7	S	0.13 ± 0.04	<38.5	<29.6	114.9 ± 73.6	-0.30
J0223.8-0412*	02 23 49.30	4.1	-04 12 19.81	3.4	S	0.26 ± 0.05	<47.3	<22.2	146.9 ± 16.7	-0.75
J0223.9+0233	02 23 51.03	4.6	+02 33 19.48	4.2	S	0.64 ± 0.14	<51.2	<38.2	166.8 ± 42.2	-0.85
J0223.9+0012	02 23 54.95	4.2	+00 12 35.18	3.6	S	0.31 ± 0.06	<41.2	<29.5	165.8 ± 40.9	-0.66
J0223.9-0619	02 23 56.23	4.7	-06 19 31.60	3.2	S	0.51 ± 0.08	<60.1	<40.9	75.0 ± 21.8	-0.78
J0224.0-0441*	02 23 57.16	3.5	-04 41 11.62	2.2	S	0.63 ± 0.05	<28.8	<19.8	19.1 ± 18.7	-0.83
J0224.0-0638	02 24 00.95	3.4	-06 38 44.07	2.0	5	1.65 ± 0.10	22.9 ± 9.3	<21.4	54.0 ± 7.5	-0.87
J0224.1-0105	02 24 04.55	5.5 4 7	-01 03 48.09	2.3	5	0.41 ± 0.04	<10.8	<13.0	18.7 ± 73.9	-0.57
10224.2-0440	02 24 09.91	4.7	$-04\ 40\ 07.77$ $-01\ 30\ 03\ 52$	4.3	S	0.13 ± 0.04 0.26 ± 0.05	<45.0	<32.7	137.2 ± 00.3 197 + 112	-0.07
10224.2-0139	02 24 12.01	3.5	-01.39.03.32 -00.03.14.67	22	S	0.20 ± 0.05	<22.4	<11.2	19.7 ± 44.2 28.2 + 19.9	-0.92
10224 2-0528*	02 24 12.05	3.6	-05 28 39 39	2.3	M	0.01 ± 0.00 0.73 ± 0.07	<35.6	<27.5	152.2 ± 19.9	-0.71
30221.2 0320	02 24 13.04	3.7	$-05\ 27\ 58.53$	2.6	C	0.69 ± 0.07	30.2 ± 16.8	<29.4	132.2 ± 22.0 147.8 ± 13.0	0.71
J0224.3-0243*	02 24 17.86	4.7	-024323.42	4.0	Š	0.37 ± 0.07	<64.3	<35.6	139.9 ± 16.8	-0.39
J0224.3-0300*	02 24 18.97	4.4	-03 00 21.05	3.1	Ŝ	0.19 ± 0.04	<40.3	<23.3	59.1 ± 27.4	-0.70
J0224.4-0425*	02 24 21.13	4.5	-04 25 46.89	3.3	S	0.29 ± 0.05	<47.3	<35.7	68.6 ± 39.4	-0.89
J0224.4-0752	02 24 22.46	4.2	-07 52 59.21	3.7	S	0.45 ± 0.07	43.5 ± 24.5	<24.4	33.8 ± 8.4	-0.68
J0224.4-0129	02 24 22.96	4.2	-01 29 32.86	3.5	S	0.12 ± 0.03	<31.0	<18.7	166.8 ± 48.5	-0.83
J0224.5-0243*	02 24 27.44	3.8	-02 43 08.68	3.1	S	0.20 ± 0.03	<36.1	<8.1	22.8 ± 15.9	-0.47
J0224.5-0219*	02 24 30.46	3.8	-02 19 37.14	2.6	M	0.17 ± 0.03	<20.2	<14.6	120.5 ± 80.5	-0.56
	02 24 30.53	5.0	-02 19 21.29	3.5	C	0.13 ± 0.03	<52.2	<4.3	56.8 ± 13.0	<i></i>
J0224.7-0209*	02 24 40.91	4.2	-02 09 59.04	3.8	S	0.11 ± 0.03	<35.5	<17.3	$1/5.7 \pm 34.1$	-0.46
J0224.7-0732	02 24 43.60	5.1	-0/3234.35	4.0	S	0.44 ± 0.09	<64.8	<44.3	56.1 ± 26.0	-0.79
JU224.8-0302*	02 24 45.74	3.5	-03 02 05.78	2.3	M	$1.0/\pm0.08$	35.0 ± 10.7	<24.0	20.3 ± 6.4	-0.76
	02 24 45.25	4.5	-03 02 32.69	2.8 2.5	C	0.20 ± 0.04	<40.9 <10.7	<17.2	01.3 ± 12.9 76.2 ± 24.7	
10224 8-0545*	02 24 43.09	5.9 5.2	-05 02 59.20	2.3 4 1	S	0.11 ± 0.02 0.43 + 0.08	<19.7 49 1 + 30 0	 <40 /	10.2 ± 24.7 128.6 ± 13.0	-0.77
J0224.8-0620	02 24 48.67	4.2	-06 20 51.03	3.5	Š	0.19 ± 0.03	<37.4	<26.0	162.4 ± 42.7	-0.63

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Table A.2. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Type	S _{comp}	Major axis	Minor axis	Position	Spectral
	12000	arcsec	12000	arcsec		Iv	arcsec	arcsec	Angle	index α^{1400}
10224 8-0221*	02 24 48 97	3.0	_02 21 15 58	3.2	S	$\frac{0.27 \pm 0.04}{0.27 \pm 0.04}$	<15.0	<21.6	$\frac{267 \pm 160}{267 \pm 160}$	-0.64
10224.0-0221	02 24 40.97	5.9	-02 21 15.58	5.2	5	0.27 ± 0.04	<43.0	<21.0	20.7 ± 10.0	-0.04
J0224.9-0712	02 24 30.78	5.1	-07 12 43.13	5.5	3	0.33 ± 0.08	<07.5	<40.1	105.4 ± 52.1	-0.90
J0225.0-0516*	02 24 57.36	4.2	-05 16 55.98	3.2	S	0.32 ± 0.05	<50.0	<28.1	44.2 ± 17.7	-0.74
J0225.0-0942	02 25 00.13	4.4	-09 42 36.14	3.7	S	0.86 ± 0.13	42.0 ± 24.7	<36.5	39.1 ± 13.2	-0.48
J0225.0-0321*	02 25 00.22	5.0	-03 21 06.56	5.0	S	0.20 ± 0.05	<57.7	<40.1	162.3 ± 39.9	-0.92
J0225.0+0131	02 25 01.39	3.7	+01 31 36.96	2.5	S	1.01 ± 0.11	<36.1	<26.9	140.7 ± 25.1	-0.88
J0225.1-0536*	02 25 05.18	3.4	-05 36 46.36	2.0	S	1.46 ± 0.09	<28.2	<24.2	27.7 ± 22.2	-0.61
10225 1-0828	02 25 05 93	49	-08 28 03 25	51	ŝ	0.27 ± 0.07	<67.0	<31.1	29.4 + 17.7	-0.67
10225.1+0017	02 25 05.75	3.4	$\pm 00.17.04.82$	2.0	S	1.08 ± 0.12	<07.0	<17.2	27.4 ± 17.7 23.4 ± 17.8	-0.66
J0225.1+0017	02 25 07.74	2.4	+001704.62	2.0	5	1.96 ± 0.12	12.1 + 10.1	<17.2	23.4 ± 17.0	-0.00
J0225.1-0035	02 25 07.77	3.4	-00 35 35.22	2.0	3	7.78 ± 0.39	12.1 ± 10.1	<13.0	62.9 ± 2.7	-0.64
J0225.1-0938	02 25 08.11	6.6	-09 38 30.09	4.2	S	0.68 ± 0.15	48.4 ± 38.5	<47.7	77.8 ± 16.8	-0.81
J0225.2-0738	02 25 08.79	3.7	-07 38 36.19	2.3	M	1.45 ± 0.12	42.8 ± 12.0	22.6 ± 15.4	75.4 ± 10.7	-0.69
	02 25 09.96	3.7	-07 39 12.86	2.3	С	1.01 ± 0.09	35.8 ± 13.8	<29.1	67.7 ± 9.6	
J0225.3-0930	02 25 15.86	4.0	-09 30 58.58	3.2	S	1.01 ± 0.13	37.2 ± 20.7	<38.4	31.4 ± 16.8	-0.76
10225 4-0056	02 25 25 27	41	-00 56 38 82	33	S	0.19 ± 0.04	< 29.8	<20.5	1536 + 568	-0.84
10225 4-0248*	02 25 25.27	4.6	-02 48 15 02	3.0	S	0.15 ± 0.01 0.16 ± 0.04	~38.5	120.0	100.0 ± 00.0	-0.70
J0225.4-0248*	02 25 25.90	4.0	-02 48 13.02	2.5	S	0.10 ± 0.04	< 30.5		55.0 16.0	-0.70
J0225.6-0210*	02 25 34.05	3.4	-02 10 18.07	2.1	3	0.03 ± 0.05	<23.1	<13.9	55.0 ± 10.9	-0.12
J0225.8-0637	02 25 45.10	5.1	-06 37 50.79	4.8	S	0.24 ± 0.06	<55.2	<45.3	4.8 ± 69.1	-0.76
J0225.9-0545*	02 25 54.74	4.2	-05 45 43.23	5.1	M	0.13 ± 0.03	<63.1	<5.5	162.9 ± 10.7	-0.46
	02 25 55.58	3.9	-05 45 40.32	3.2	С	0.10 ± 0.02	<29.1		18.6 ± 24.6	
J0225.9+0219	02 25 55.51	3.6	+02 19 14.30	2.8	S	0.57 ± 0.08	<34.2	<3.4	7.6 ± 12.6	-0.57
I0225 9+0151	02 25 55 56	47	+01 51 29 22	35	S	0.41 ± 0.09	<42.7	<34.1	100.9 + 62.8	-0.74
10226.2-0133	02 26 09 14	4.5	-01 33 53 20	17	S	0.11 ± 0.01	< 50.1	~22.2	24.5 ± 16.2	-0.53
J0220.2-0133	02 20 09.14	4.5	-01 33 33.20	4.7	S	0.10 ± 0.04	-29.4	17.2	24.3 ± 10.2	-0.55
J0226.2+0129	02 26 09.18	3.4	+01 29 26.14	2.1	3	1.80 ± 0.12	<28.4	<17.3	3.0 ± 10.8	-0.54
J0226.2-0646	02 26 14.12	5.6	-06 46 00.60	4.4	S	0.18 ± 0.05	<52.2	<40.0	68.7 ± 60.1	-0.74
J0226.2+0205	02 26 14.83	3.7	+02 05 11.31	2.4	S	1.49 ± 0.14	36.6 ± 13.9	<22.5	130.2 ± 6.9	-0.49
J0226.3-0400*	02 26 18.81	4.8	-04 00 10.04	4.4	S	0.30 ± 0.06	<57.2	<46.7	12.6 ± 54.2	-0.41
J0226.3-0425*	02 26 19.88	3.7	-04 25 36.25	2.6	S	0.34 ± 0.04	<29.3	<20.4	13.5 ± 31.9	-0.73
10226 4-0846	02 26 25 36	3.6	-08 46 30 78	2.2	S	2.01 ± 0.15	39.2 ± 10.3	24.0 + 12.6	53.8 ± 11.2	-0.63
10226 6-0806	02 26 34 57	3.6	-08 06 18 67	23	ŝ	1.23 ± 0.10	35.1 ± 12.2	<29.5	11.6 ± 9.1	-0.68
10226.6 0715	02 20 34.37	2.0	-08 00 18.07	2.5	S	1.23 ± 0.10	33.1 ± 12.2	~29.5	44.0 ± 9.4	-0.08
J0220.0-0/15	02 26 35.98	3.7	-07 15 00.55	2.5	3	0.60 ± 0.06	<41.8	<22.3	43.2 ± 11.9	-0.87
J0226.7-0121	02 26 39.33	3.6	-01 21 24.44	2.4	S	0.44 ± 0.05	<30.0	<18.7	44.6 ± 21.6	-0.86
J0226.7-0552*	02 26 40.23	4.1	-05 52 37.19	3.4	S	0.24 ± 0.04	<43.3	<24.3	23.3 ± 22.8	-0.26
J0226.8-0712	02 26 45.18	3.6	-07 12 12.89	2.3	S	0.92 ± 0.08	29.2 ± 13.7	<27.3	39.9 ± 11.3	-0.85
J0227.0-0223*	02 26 57.08	4.5	-02 23 54.07	3.8	S	0.24 ± 0.05	<56.0	<27.2	140.9 ± 17.0	-0.89
10227 0+0206	02 26 59 06	3.7	+02.06.11.95	2.8	S	0.87 ± 0.11	< 38.2	<24.9	1768 + 216	-0.68
10227 0-0555*	02 26 59 31	34	-05 55 44 34	2.0	Š	246 ± 0.13	135 ± 117	<22.5	37.2 ± 18.6	-0.76
10227.0+0224	02 27 00 30	4.5	$\pm 02.24.10.73$	1.0	S	0.37 ± 0.00	10.0 ± 11.7	<22.5	152.8 ± 22.4	-0.58
J0227.0+0224	02 27 00.39	4.5	+02 24 19.73	4.2	5	0.37 ± 0.09	<49.1	<23.1	132.0 ± 22.4	-0.58
J0227.2-0325*	02 27 08.52	4.6	-03 25 56.57	4.0	3	0.36 ± 0.07	<56.7	<44.3	31.6 ± 39.9	-0.52
J0227.2-0141	02 27 11.56	5.5	-01 41 51.25	3.6	S	0.23 ± 0.05	<61.0	<32.7	75.0 ± 20.9	-1.07
J0227.2-0053	02 27 12.29	3.4	-00 53 44.98	2.1	S	0.86 ± 0.06	<19.0	<12.0	49.6 ± 21.2	-1.06
J0227.4-0240*	02 27 22.85	4.8	-02 39 56.17	3.7	M	0.24 ± 0.05	<46.5	<39.3	93.2 ± 75.9	-0.79
	02 27 25.85	4.6	-02 40 17.96	3.2	С	0.18 ± 0.04	<39.9	<27.3	87.4 ± 41.6	
I0227 4+0137	02 27 26 57	3.5	+01 37 33 32	2.4	S	0.96 ± 0.09	< 34.7	<16.0	5.3 + 10.9	-0.74
10227 5-0437*	02 27 28.57	17	-04 37 31 87	4.1	S	0.90 ± 0.05	<50.2	<35.2	146.1 ± 37.7	-0.74
10227.5-0457*	02 27 20.11	4.7	-04 57 51.87	4.1	S	0.20 ± 0.03	54.2 + 22.6	-07.6	140.1 ± 37.7	-0.74
J0227.5-0557*	02 27 31.82	0.4	-03 37 43.09	5.1	3	0.33 ± 0.07	34.2 ± 35.0	<27.0	95.7 ± 6.4	-0.58
J0227.6-0314*	02 27 35.72	4.6	-03 14 45.55	4.2	S	0.12 ± 0.03	<47.8	<20.5	33.7 ± 23.6	-0.65
J0227.6-0052	02 27 36.25	3.7	-00 52 58.18	2.5	S	0.56 ± 0.06	<31.7			-0.70
J0227.6+0133	02 27 37.11	3.7	+01 33 12.08	2.9	S	0.55 ± 0.08	<36.1	<18.6	1.7 ± 18.6	-0.65
J0227.7-0922	02 27 40.09	5.7	-09 22 19.76	4.3	S	0.44 ± 0.11	<65.3	<39.9	60.1 ± 25.4	-0.51
J0227.7-0908	02 27 40.47	4.4	-09 08 48.91	3.2	S	1.27 ± 0.16	48.0 ± 19.8	<49.4	56.9 ± 19.0	-0.83
J0227.7-0043	02 27 41.27	4.1	-00 43 45.66	2.6	S	0.28 ± 0.05	<34.8	<16.8	80.9 ± 21.1	-0.63
10227 7-0250*	02 27 44 22	3 5	-02 50 48 77	23	ŝ	0.35 ± 0.04	<25.6		1485 + 125	-0.68
10227.7-0250	02 27 44 62	12	-02 30 40.77	2.5	S	0.33 ± 0.04	<41.0	-22.2	$1+0.5 \pm 12.5$	0.00
J0227.7-0021	02 27 44.03	4.2	-00 21 07.22	3.5	5	0.27 ± 0.03	<41.0	<32.5	34.0 ± 49.9	0.23
J0227.8+0221	02 27 45.17	3.7	+02 21 42.43	3.0	3	1.03 ± 0.13	<46.2	<21.2	$1/2.9 \pm 11.6$	-0.89
J0227.9-0035	02 27 53.72	3.7	-00 35 35.32	2.7	S	0.24 ± 0.04	<26.0	<14.6	12.4 ± 34.4	-0.38
J0228.0-0644	02 28 02.20	3.6	-06 44 40.12	2.5	M	0.22 ± 0.03	<23.4		174.8 ± 18.9	-0.58
	02 28 03.40	3.9	-06 44 25.34	5.6	С	0.18 ± 0.04	<74.2		5.9 ± 7.7	
J0228.1+0031	02 28 05.61	3.4	$+00\ 31\ 17.25$	2.0	S	1.59 ± 0.10	<22.0	<19.7	15.0 ± 45.4	-0.61
I0228 1-0231*	02 28 07 48	34	-02 31 07 26	2.0	S	1.81 ± 0.10	<18.6	<17.2	752 + 458	-0.91
I0228 1_0115	02 28 07 54	3 1	-01 15 /3 86	2.0	ŝ	4.88 ± 0.25	20.8 ± 6.7	<15.6	94.1 ± 2.7	_0.80
10228.1-0115	02 28 07.34	2.5	-01 15 45.80	2.0	5	4.88 ± 0.23	20.8 ± 0.7	<10.2	120.4 ± 25.9	-0.80
10228.2-0040	02 20 10.43	3.3	-00 40 01.11	2.2	່ ເ	0.73 ± 0.07	<20.2	<19.2	127.4 ± 23.8	-0.87
J0228.3-0157	02 28 19.99	3.7	-01 57 55.33	2.6	5	0.23 ± 0.03	<23.6	<13.6	$1/5.1 \pm 3/.4$	-0.54
J0228.4+0032	02 28 25.03	4.0	+00 32 10.99	3.8	S	0.39 ± 0.07	<52.1	<24.6	11.1 ± 15.8	-1.06
J0228.5-0223*	02 28 29.16	3.5	-02 23 17.89	2.3	S	0.55 ± 0.05	<23.1			-0.79
J0228.6+0150	02 28 33.64	4.6	+01 50 36.91	3.7	S	0.45 ± 0.10	<39.9			-0.69
J0228.7-0602	02 28 40.58	3.4	-06 02 42.61	2.1	S	1.07 ± 0.08	<27.6	<22.3	38.9 ± 23.1	-0.79
10228 7-0042	02 28 40 95	48	-00 42 55 24	39	S	0.21 ± 0.05	<43.9	<35 5	51.6 + 71.2	-0.70
10228 8-0617	02 28 48 10	3.1	-06 17 53 62	2.0	ç	1.80 ± 0.05	~78 1	<27.0	46.7 ± 58.7	_1.00
10220.0-0017	02 20 40.10	20	100 10 16 16 01	2.0	14	0.21 ± 0.07	~20.4	~7.0	41.5 + 10.0	-1.00
JU228.8+0049	02 28 49.04	3.8	+00 49 40.91	2.1	M	0.51 ± 0.05	< 30.5	<1.9	41.3 ± 18.0	-0.78
	02 28 48.92	4.3	+00 50 01.60	3.3	C	0.14 ± 0.03	<43.3		46.2 ± 10.4	
J0228.9-0337*	02 28 53.17	3.4	-03 37 37.75	2.0	S	6.07 ± 0.31	<18.5	<16.4	62.1 ± 12.0	-0.63
J0229.0+0052	02 28 58.53	4.6	+00 52 55.83	5.0	S	0.28 ± 0.07	<56.5	<30.6	177.7 ± 25.2	-0.60
J0229.1-0655	02 29 04.22	4.9	-06 55 22.27	3.6	S	0.39 ± 0.07	<64.3	<29.7	54.5 ± 13.4	-0.81

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Table A.2. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		Jy	arcsec	arcsec	Angle	index α_{74}^{1400}
J0229.1-0541*	02 29 05.73	3.4	-05 41 10.76	2.1	S	1.17 ± 0.08	19.1 ± 13.2	<24.5	31.4 ± 14.6	-0.57
J0229.1-0223*	02 29 08.76	3.7	-02 23 08.01	2.7	S	0.21 ± 0.03	<29.1	<10.1	26.4 ± 20.8	-0.66
J0229.2-0656	02 29 10.13	3.7	-06 56 04.58	2.4	S	0.79 ± 0.08	<40.2	<27.7	56.7 ± 16.6	-0.81
J0229.2-0311*	02 29 11.92	4.7	-03 11 35.17	4.1	S	0.17 ± 0.04	<52.2	<20.8	140.6 ± 19.1	-0.65
J0229.3-0442*	02 29 15.90	3.4	-04 42 14.91	2.0	S	2.97 ± 0.16	<23.9	<18.2	45.0 ± 7.9	-0.72
J0229.6-0027	02 29 32.48	4.5	-00 27 40.63	3.9	M	0.43 ± 0.08	<64.2	<28.7	37.7 ± 12.6	-0.76
	02 29 33.70	5.1	-00 26 44.68	3.8	С	0.33 ± 0.07	<51.5	<41.1	79.4 ± 55.8	
	02 29 33.87	4.0	-00 26 25.98	3.0	С	0.32 ± 0.05	<43.4	<15.3	44.6 ± 13.7	
J0229.6-0752	02 29 37.56	4.6	-07 52 30.20	3.8	S	0.34 ± 0.07	<55.8	<28.0	43.4 ± 17.9	-0.59
J0229.6+0025	02 29 38.67	3.5	+00 25 26.05	2.2	Μ	1.13 ± 0.09	22.8 ± 15.0	<15.2	47.8 ± 7.3	-0.79
70000 E 00000	02 29 36.88	3.4	+00 24 59.95	2.1	C	1.11 ± 0.08	<22.5	<16.3	148.8 ± 24.2	0.05
J0229.7-0238*	02 29 38.91	4.0	-02 38 37.57	3.1	S	0.16 ± 0.03	<37.5	<12.7	141.1 ± 18.9	-0.35
J0229.7-0705	02 29 43.13	3.4	-07 05 37.64	2.0	S	2.29 ± 0.14	25.6 ± 8.6	15.0 ± 13.2	90.0 ± 13.5	-0.90
J0229.7-0148	02 29 44.20	5.6	-01 48 24.63	4.5	S	0.22 ± 0.06	<52.4			-1.02
J0229.8-0206	02 29 47.29	3.5	-02 06 48.36	2.3	S	0.64 ± 0.05	<33.1	<21.0	176.4 ± 14.0	-0.84
J0230.0-0331*	02 30 01.18	3.7	-03 31 51.27	2.8	S	0.20 ± 0.03	<28.5	<10.4	15.1 ± 23.1	-0.6/
J0230.1-0209	02 30 03.64	4.0	-02 09 22.60	3.3	S	0.10 ± 0.02	<30.1	<9.6	27.7 ± 29.9	-0.41
J0230.1-0628	02 30 05.16	3.8	-06 28 03.68	2.8	S	0.47 ± 0.06	<38.7	<31.8	18.2 ± 44.0	-0.84
J0230.2-0642	02 30 10.88	3.5	-06 42 27.99	2.3	S	0.73 ± 0.07	<30.7	<23.4	32.2 ± 24.8	-1.11
J0230.2-0056	02 30 14.12	3.8	-00 56 58.04	2.7	S	0.23 ± 0.04	<27.2	<20.8	18.5 ± 58.0	-0.79
J0230.3-1007	02 30 17.48	4.8	-10 07 08.05	5.3	S	0.94 ± 0.19	43.0 ± 34.8	<49.9	7.2 ± 21.3	-0.68
J0230.3-0750	02 30 17.77	3.8	-07 50 35.26	2.6	5	0.91 ± 0.10	33.5 ± 10.0	<30.7	54.6 ± 12.2	-0.69
J0230.4-0255*	02 30 21.92	3.4	-02 55 05.60	2.0	5	2.08 ± 0.11	<18.6	<16.6	15.1 ± 30.3	-1.07
J0230.4-0412*	02 30 23.51	3.4	-04 12 27.64	2.1	S	0.65 ± 0.05	<17.9	<15.5	0.5 ± 73.0	-0.37
J0230.4-0830	02 30 26.11	3.6	-08 30 40.61	2.2	S	2.12 ± 0.16	42.0 ± 10.4	<32.2	58.6 ± 7.2	-0.74
J0230.4+0108	02 30 20.34	4.2	+01 08 48.17	3.8	5	0.77 ± 0.12	41.4 ± 24.4	< 34.9	155.2 ± 12.0	-0.60
J0230.6-0309*	02 30 33.20	3.7	-03 09 09.00	2.7	5	0.32 ± 0.04	<31.2	<20.9	10.9 ± 29.9	-0.62
J0230.0-0421*	02 30 33.41	5.9	-04 21 07.50	3.0	S	0.18 ± 0.03	<33.0	<10.5	28.8 ± 19.9	-0.29
J0230.0-0038	02 30 34.89	4.1	-00 38 40.51	3.0 4.6	S	0.29 ± 0.05	<48.0	<25.8	157.9 ± 19.7	-0.69
J0230.6-0414	02 30 36.04	4.5	-04 14 48.00	4.0	S	0.15 ± 0.04	<48.0	<20.9	$1/3.8 \pm 30.9$	-0.//
10230.0-0409	02 30 30.88	5.5	-04 09 33.10	2.2	5	0.37 ± 0.03	<25.1	<10.8	33.3 ± 29.4	-0.01
J0230.7+0020	02 30 39.73	4.0	+00 20 19.13	5.9 2.4	5	0.49 ± 0.09	<04.7	<29.0	140.0 ± 13.0	-0.94
J0230.7-0328*	02 30 40.92	5.5	-05 28 38.77	2.4	5	0.37 ± 0.04	<23.0	<13.7	0.1 ± 21.7	-0.00
J0230.7-0230*	02 30 43.30	5.4 2.6	-02 36 22.48	0.0	S	0.42 ± 0.09	47.8 ± 40.2	<51.0	25.4 ± 18.7	-0.00
J0230.7-0701	02 30 45.39	5.0	-0/ 01 19.47	2.5	5	0.79 ± 0.07	< 50.1	<23.3	44.9 ± 13.0	-0.82
10230.7-0840	02 30 44.11	J.1 4 4	-084044.03 -03361557	5.9 4 1	S	0.02 ± 0.12 0.12 ± 0.03	< 39.7	<47.2	03.4 ± 43.3 173 5 \pm 52 1	-0.82
J0230.8-0330	02 30 49.00	4.4	-07 21 00 52	3.5	S	0.12 ± 0.03	<37.3	<20.5	$1/3.5 \pm 52.1$ $1/2.5 \pm 66.2$	-0.74
10230.8 - 0721 10230.0 ± 0014	02 30 49.99	4.4	+00.14.16.50	3.5	S	0.24 ± 0.03	<15.1	<29.5	142.5 ± 00.2 22.1 \pm 25.7	-0.45
10230.9+0014	02 30 53 62	53	-03525098	12	S	0.34 ± 0.07 0.19 ± 0.05	<56.0	<20.4	53.4 ± 27.5	-0.71
10230.9-0909	02 30 55.02	3.8	-09 09 52 55	2.5	S	1.85 ± 0.17	397 ± 137	27.9 ± 15.3	63.6 ± 21.1	-0.73 -0.74
10231 0-0451*	02 30 57 55	4.2	-020732.33 -04513893	3.1	S	0.24 ± 0.04	<34.8	21.7 ± 15.5	05.0 ± 21.1	-0.74
10231.0-0431	02 30 57.55	37	-04 31 30.55 -06 24 47 55	2.6	S	0.24 ± 0.04 0.46 ± 0.06	<30.4	 <25.7	 168 7 + 57 8	-0.50
10231.0 - 0024 10231.0 + 0149	02 30 30.23	3.4	+01495815	2.0	S	2.93 ± 0.19	24.1 + 10.4	<24.1	165.9 ± 9.9	-1.08
10231.0-0049	02 31 00.50	35	-00 49 44 98	2.1	S	0.55 ± 0.05	<22.0	<16.5	61.4 + 37.3	-1.12
10231.0-0014	02 31 02 59	3.4	-00 14 03 68	2.2	S	2.16 ± 0.03	323 + 77	<19.4	1416 ± 40	-0.95
I0231 1-0822	02 31 05 39	69	-08 22 42 65	3.6	S	1.68 ± 0.13	105.0 ± 31.5	30.1 + 24.5	1035 ± 59	-1.18
I0231.3-0019	02 31 16 94	4.6	-00 19 56 01	3.5	S	0.19 ± 0.05	<39.0	<26.5	60.0 ± 45.6	-0.75
I0231 4-0315	02 31 26 53	4.0	$-03\ 15\ 01\ 18$	3.2	S	0.19 ± 0.05 0.29 ± 0.05	<36.6	<20.5	00.0 ± 45.0	-0.78
I0231.4-0421	02 31 26 69	3.4	-04 21 34 58	2.0	S	1.84 ± 0.05	<22.9	< 20.1	 47 7 + 25 2	-0.59
J0231.5-0212	02 31 30.25	3.7	$-02\ 12\ 44.10$	2.8	Š	0.21 ± 0.03	<27.2	<11.8	168.8 ± 27.1	-0.69
J0231.5-0228	02 31 31.88	3.5	$-02\ 28\ 03.96$	2.1	Š	0.62 ± 0.05	<20.6	<18.5	56.7 ± 80.7	-0.60
J0231.5-0041	02 31 32.37	4.2	-00 41 48.12	3.6	ŝ	0.25 ± 0.05	<41.5	<27.4	15.4 ± 34.3	-0.70
J0231.7-0453	02 31 40.39	3.5	-04 52 56.48	2.1	М	1.80 ± 0.12	32.7 ± 9.1	22.6 ± 11.2	81.1 ± 13.8	-0.76
	02 31 37.16	3.6	-04 53 16.92	2.4	С	0.73 ± 0.07	<34.1	<26.3	14.9 ± 24.9	
J0231.8-0326	02 31 45.81	6.0	-03 26 15.69	4.4	S	0.25 ± 0.06	<62.2	<45.2	83.4 ± 42.4	-1.20
J0231.8-0305	02 31 50.49	4.1	-03 05 59.15	3.9	S	0.18 ± 0.04	<44.7	<21.2	167.1 ± 21.6	-0.60
J0231.9-0226	02 31 52.25	3.5	-02 26 46.71	2.4	М	0.38 ± 0.04	<26.5	<9.0	173.5 ± 15.5	-0.82
	02 31 51.20	4.0	-02 26 53.37	3.0	С	0.30 ± 0.05	<39.2	<23.0	37.1 ± 22.7	
J0232.1-0627	02 32 08.66	5.4	-06 27 25.45	3.8	Š	0.45 ± 0.09	<66.9	<39.2	68.0 ± 20.0	-0.52
J0232.2+0022	02 32 09.46	4.0	+002235.46	3.3	S	0.32 ± 0.06	<38.3	<22.6	25.2 ± 28.0	-0.80
J0232.2-0441	02 32 14.14	3.4	-04 41 50.62	2.1	S	1.31 ± 0.08	<29.2	<18.2	21.6 ± 9.3	-0.75
J0232.3-0749	02 32 15.65	3.8	-07 49 48.89	2.6	S	0.85 ± 0.10	<39.7	<33.6	61.6 ± 40.7	-0.73
J0232.3-0033	02 32 15.81	4.2	-00 33 03.33	3.9	S	0.28 ± 0.06	<49.5	<24.1	162.5 ± 19.2	-0.48
J0232.3-0545	02 32 16.64	4.1	-05 45 19.63	3.6	S	0.19 ± 0.04	<42.2	<13.9	27.5 ± 17.8	-0.56
J0232.3-0401	02 32 17.64	5.5	-04 01 32.56	5.0	S	0.34 ± 0.07	48.6 ± 38.1	<28.7	42.6 ± 9.7	-0.65
J0232.4-0525	02 32 21.97	4.2	-05 25 47.17	3.8	S	0.17 ± 0.04	<40.7	<21.7	160.3 ± 28.5	-0.65
J0232.4-0003	02 32 26.74	5.1	-00 03 22.92	4.7	S	0.34 ± 0.08	<71.3	<27.4	39.8 ± 13.3	-0.74
J0232.5+0113	02 32 28.77	3.9	+01 13 54.28	3.3	S	0.31 ± 0.06	<34.8	<15.6	5.6 ± 23.8	-0.65
J0232.5-0418	02 32 32.87	3.8	-04 18 31.04	2.7	S	0.40 ± 0.06	<33.8	<26.6	39.3 ± 43.6	-0.51
J0232.6-0428	02 32 34.27	4.3	-04 28 34.17	3.2	S	0.29 ± 0.05	<45.2	<26.0	47.4 ± 21.9	-0.75
J0232.6-0104	02 32 37.09	5.5	-01 04 04.35	4.6	S	0.26 ± 0.07	<52.3			-0.44
J0232.6-0444	02 32 37.84	4.3	-04 44 42.51	3.8	S	0.25 ± 0.05	<47.7	<30.2	19.9 ± 27.6	-0.60
J0232.6-0105	02 32 38.83	4.3	-01 05 19.83	3.5	S	0.54 ± 0.09	<49.4	<43.8	22.0 ± 73.6	-0.59

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Table A.2. continued.

Name	RA	σ_{α}	Dec	σ_{δ}	Type	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec	J 1	Jv	arcsec	arcsec	Angle	index α_{24}^{1400}
10232 6+0056	02 32 38 86	3.7	+00.56.20.00	2.4	S	120 ± 0.12	<37.4	<33.3	1014 + 517	-1.04
10232.7-0233	02 32 30.00	3.5	-02330022	2.4	M	1.20 ± 0.12 2.28 ± 0.15	40.0 + 8.8	370 ± 80	51.8 ± 60.5	-0.72
J0232.7-0233	02 32 41.67	2.5	-02 33 09.22	2.2	M C	2.26 ± 0.13	40.0 ± 0.0	37.9 ± 0.9	51.6 ± 00.3	-0.72
	02 32 45.81	3.4	-02 34 29.22	2.2	C	2.03 ± 0.13	41.8 ± 8.4	<29.4	159.4 ± 5.2	
	02 32 43.24	4.8	-02 33 54.99	4.0	C	0.41 ± 0.07	43.1 ± 30.3	<26.9	45.4 ± 9.7	
	02 32 45.09	5.4	-02 33 53.18	4.7	С	0.23 ± 0.05	54.5 ± 35.6		44.3 ± 4.6	
J0232.7-0632	02 32 44.80	4.1	-06 32 09.47	3.0	S	0.32 ± 0.06	<31.9	<24.8	126.5 ± 59.5	-0.52
J0232.8-0829	02 32 44.97	5.1	-08 30 00.14	4.7	S	0.40 ± 0.10	<60.6	<40.2	35.0 ± 31.9	-0.75
J0232.8-0425	02 32 49.47	4.2	-04 25 31.20	3.1	М	0.24 ± 0.04	<47.6	<13.8	132.2 ± 12.5	-0.57
	02 32 49 96	44	-04 25 34 52	3.6	С	0.23 ± 0.04	< 58.0	< 9.4	41.0 + 9.5	
10232 8+0017	02 32 50 10	3 5	+00.17.20.30	2.0	S	0.78 ± 0.07	<25.1	<14.5	179.9 ± 18.7	-0.54
10232.0+0017	02 32 51 01	4.0	$\pm 00.0235.01$	1.2	S	0.76 ± 0.07	<50.0	<13.6	78 ± 858	-0.70
10222.9+0002	02 32 51.91	4.9	+00.02.33.01	2.0	S	0.30 ± 0.09	176 ± 71	142 86	7.0 ± 0.00	-0.70
J0232.9-0043	02 32 54.00	5.4	-00 45 52.57	2.0	3	10.36 ± 0.35	$1/.0 \pm /.1$	14.5 ± 8.0	08.7 ± 12.0	-0.07
J0232.9-0351	02 32 55.82	4.0	-03 51 41.05	3.0	3	0.21 ± 0.04	<30.6	<19.2	$3/.3 \pm 38.1$	-0.51
J0233.1-0843	02 33 03.92	4.5	-08 43 36.66	3.1	S	1.03 ± 0.14	44.6 ± 21.9	<36.5	57.8 ± 11.9	-0.98
J0233.2-0220	02 33 10.36	4.1	-02 20 01.01	3.3	S	0.20 ± 0.04	<33.8	<21.7	24.8 ± 39.7	-0.43
J0233.2-0012	02 33 13.39	3.8	-00 12 18.51	2.1	S	2.23 ± 0.16	72.9 ± 10.7	<21.7	78.7 ± 2.2	-1.00
J0233.3-0320	02 33 18.88	3.4	-03 20 55.05	2.0	М	5.33 ± 0.28	45.2 ± 4.5	<20.3	86.4 ± 1.3	-0.75
	02 33 15.79	3.5	-03 20 55.74	2.2	С	1.06 ± 0.08	<31.2	<25.3	177.6 ± 24.9	
10233 3-0455	02 33 20 24	39	-04 55 01 14	31	S	0.44 ± 0.07	<44.2	<31.1	21.6 + 26.2	-0.25
10233 4-0454	02 33 24 38	37	-04 55 00 22	24	S	0.62 ± 0.07	<34.6	<27.1	68.4 ± 20.2	-0.37
10233 4+0015	02 33 24.30	4.5	$\pm 00.15.47.02$	2.4	S	0.52 ± 0.07	<40.0	<36.5	03.4 ± 29.9	-0.83
10222 4 0425	02 33 23.43	4.5	+00 15 47.92	3.2	5	0.30 ± 0.10	<49.9	< 30.5	93.0 ± 31.0	-0.83
J0233.4-0435	02 33 26.02	3.9	-04 35 55.87	3.0	3	0.38 ± 0.06	< 39.2	<23.0	22.4 ± 25.1	-1.06
J0233.5-0/13	02 33 28.69	4.1	-0/13 24.63	2.9	Μ	0.83 ± 0.11	40.4 ± 19.9	<27.5	128.7 ± 9.2	-1.03
	02 33 29.90	4.4	-07 13 19.86	4.0	С	0.39 ± 0.08	<58.6	<23.6	34.6 ± 13.6	
	02 33 27.30	4.5	-07 12 42.42	3.7	С	0.29 ± 0.06	<47.6	<23.3	42.1 ± 21.4	
J0233.5-0203	02 33 30.22	3.4	-02 03 22.92	2.0	S	2.23 ± 0.13	<21.6	<17.0	45.6 ± 15.2	-0.66
J0233.6-0412	02 33 33.60	4.0	-04 12 38.78	3.1	S	0.18 ± 0.04	<31.6	<16.7	28.5 ± 32.4	-0.35
10233 6-0519	02 33 33 86	4.1	-05 19 53 28	33	S	0.33 ± 0.06	<40.7	< 30.8	25.5 ± 41.9	-0.77
10233 6-0306	02 33 36 28	4.0	-03 06 37 27	3.4	s	0.55 ± 0.00 0.16 ± 0.04	<30.5	<16.4	11.6 ± 38.8	-0.53
10222 6 0050	02 33 30.20	27	01 00 00 24	2.0	S	0.10 ± 0.04	< 27.1	<10.4	174.2 ± 21.2	0.62
10233.0-0039	02 33 37.30	5.7	-01 00 00.24	2.9	5	0.18 ± 0.03	<27.1		$1/4.2 \pm 21.3$	-0.02
J0233.7-0039	02 33 39.54	4.5	-06 39 35.25	5.0	3	0.20 ± 0.05	< 34.2			-0.55
J0233.7-0912	02 33 41.50	4.1	-09 12 45.55	5.3	Μ	0.65 ± 0.12	57.5 ± 30.9	<13.3	18.3 ± 5.7	-0.97
	02 33 40.25	4.5	-09 12 41.13	3.9	С	0.58 ± 0.12	<50.2	<37.6	24.0 ± 40.1	
J0233.7-0232	02 33 43.88	3.4	-02 32 11.08	2.0	S	2.06 ± 0.12	26.6 ± 8.1	<20.2	64.0 ± 5.2	-0.93
J0233.8-0052	02 33 46.62	4.4	-00 52 35.54	3.4	S	0.30 ± 0.06	<42.4	<32.2	137.6 ± 45.5	-0.62
J0234.0-0508	02 33 57.16	3.4	-05 07 59.93	2.4	М	2.08 ± 0.14	56.4 ± 9.1	<26.2	173.3 ± 3.1	-1.08
	02 33 58.07	3.7	-05 08 54.58	2.8	С	0.80 ± 0.09	34.0 ± 17.5	<30.7	157.7 ± 12.2	
$I0234.0\pm0150$	02 34 01 23	3.9	+01501129	3.0	S	0.98 ± 0.14	<46.2	<27.6	155.2 ± 17.3	-0.73
J0234.1+0055	02 34 03 05	3.7	$\pm 00.55.38.17$	2.0	S	0.34 ± 0.05	<74.3	<11.0	36 ± 330	-0.86
10224.1+0033	02 34 03.03	3.7	+00.33.36.17	2.7	5	0.34 ± 0.03	<24.5	<11.9	3.0 ± 33.9	-0.80
J0234.2-0308	02 34 10.89	4.1	-03 08 27.98	3.9	3	0.21 ± 0.04	<45.8	<18.0	10.9 ± 18.5	-0.76
J0234.2-0121	02 34 10.90	4.1	-01 21 44.68	2.8	S	0.37 ± 0.06	<37.4	<28.6	102.2 ± 40.8	-0.78
J0234.2-0025	02 34 11.71	4.0	-00 25 54.03	2.8	S	0.39 ± 0.06	<33.9	<26.5	86.1 ± 50.7	-0.79
J0234.2-0603	02 34 12.17	3.5	-06 03 58.85	2.2	S	0.82 ± 0.07	<28.2	<24.6	5.1 ± 49.5	-0.71
J0234.3+0123	02 34 15.61	3.7	+01 23 40.39	3.0	S	0.68 ± 0.09	<41.2	<20.5	172.7 ± 15.2	-0.96
J0234.3-0935	02 34 16.36	3.9	-09 35 22.11	3.2	S	2.09 ± 0.23	47.6 ± 16.9	<44.3	167.4 ± 14.1	-0.41
10234 3+0149	02 34 17 04	4.0	+01 /0 32 36	4.6	Š	0.29 ± 0.07	<52.0	< 8 3	177.8 ± 13.8	-0.74
10234 3-0415	02 34 20 70	4.0	-04 15 44 82	3.6	S	0.25 ± 0.07	<12.0	<23.0	73 ± 241	-0.70
10224.5-0415	02 34 20.70	4.0	-04 13 44.62	3.0	5	0.20 ± 0.03	<42.4	<23.0	7.5 ± 24.1	-0.70
J0234.4-0525	02 34 21.55	3.5	-05 25 55.04	2.5	3	0.01 ± 0.06	<27.4	<10.1	5.1 ± 17.2	-0.87
J0234.4-0139	02 34 21.68	3.5	-01 39 01.00	2.2	S	0.51 ± 0.05	<20.0	<13.7	166.4 ± 35.7	-0.65
J0234.4-0645	02 34 23.74	3.5	-06 45 37.20	2.3	М	2.15 ± 0.16	50.5 ± 10.1	<30.6	147.0 ± 4.8	-0.90
	02 34 22.64	4.0	-06 45 04.42	2.7	С	0.30 ± 0.05	<34.2	<14.6	60.9 ± 20.8	
J0234.4-0013	02 34 26.86	3.4	-00 13 42.68	2.1	S	1.32 ± 0.09	<21.7	<20.1	25.4 ± 79.7	-0.69
J0234.5-0150	02 34 27.40	4.4	-01 50 13.15	4.2	S	0.21 ± 0.05	<52.8	<21.2	150.3 ± 17.6	-0.92
J0234.5-0245	02 34 31.25	4.9	-02 45 19.60	5.1	S	0.25 ± 0.06	<62.6	<36.8	19.1 ± 25.9	-0.91
10234 6-0419	02 34 35 89	48	-04 19 33 17	52	S	0.39 ± 0.09	<76.5	<31.5	1543 + 128	-0.56
10234 8-0050	02 34 45 53	3.4	_00 50 24 09	2.1	s	1.25 ± 0.09	<25.1	<21.6	101.7 ± 34.8	-0.69
10225 0 0726	02 34 45.55	27	07 26 18 52	2.1	S	1.25 ± 0.07	<25.0	<28.7	101.7 ± 34.0 112.2 ± 24.2	0.75
J0235.0-0730	02 34 36.73	5.7	-07 30 18.32	2.4	5	0.09 ± 0.09	<35.0	<20.7	112.3 ± 34.3	-0.73
J0235.0-0115	02 35 01.03	4.7	-01 15 10.04	3.2	3	0.28 ± 0.06	<47.7	<26.8	11.0 ± 23.3	-0.70
J0235.0-0532	02 35 01.57	4.5	-05 32 35.25	4.6	S	0.17 ± 0.04	<54.2	<22.9	157.8 ± 19.6	-0.76
J0235.1-0402	02 35 07.02	3.4	-04 02 03.39	2.0	S	10.80 ± 0.54	17.3 ± 6.9	<16.3	74.1 ± 2.2	-0.66
J0235.2+0033	02 35 10.30	3.6	+00 33 38.17	2.6	S	0.52 ± 0.07	<29.1	<15.7	8.1 ± 22.3	-0.50
J0235.2-0159	02 35 12.77	3.8	-01 59 57.26	2.9	S	0.30 ± 0.05	<36.2	<14.6	31.4 ± 17.0	-0.53
J0235.3-0704	02 35 16.78	4.0	-07 04 19.57	3.2	S	0.33 ± 0.06	<37.4	<26.5	14.1 ± 38.1	-0.59
J0235 3-0012	02 35 18 29	44	-00 12 51 12	3.2	S	0.34 ± 0.06	<41.0	<28.8	112.1 + 37.3	-0.70
10235 4-0654	02 35 21 44	43	-06 54 54 48	53	Š	0.40 ± 0.08	<74.7	<31.1	171.0 ± 12.5	-0.55
I0235 4 + 0122	02 35 21.74 02 35 24 11	51	101 22 /0 00	5.5	c c	0.40 ± 0.00	~61.0	~16.0	111.0 ± 12.0	_1.02
10225 5 0027	02 33 24.11	J.1 4 1	-TUI JJ 49.98	2.1	ы С	0.57 ± 0.14	<01.0 -27.7	<40.9 <15 0	$+.1 \pm +/.9$	-1.02
JU233.5-0037	02 35 28.23	4.1	-00 37 09.09	3.8 2.7	3	0.15 ± 0.04	<31.1	<15.2	10.3 ± 20.1	-0.01
J0235.5-0705	02 35 30.79	4.3	-07 05 02.62	3.5	2	0.35 ± 0.07	<43.6	<32.9	150.1 ± 43.3	-0.87
J0235.5-0219	02 35 32.46	3.4	-02 19 32.00	2.0	S	5.80 ± 0.30	<21.9	<17.3	42.8 ± 6.5	-0.60
J0235.6-0515	02 35 35.03	4.3	-05 15 58.41	4.1	S	0.23 ± 0.05	<49.9	<23.6	158.1 ± 20.1	-0.54
J0235.6-0557	02 35 37.01	3.8	-05 57 02.19	2.9	S	0.38 ± 0.05	<38.9	<23.9	163.4 ± 22.2	-0.76
J0235.7-0759	02 35 42.21	4.1	-07 59 59.26	2.9	S	0.62 ± 0.09	<42.6	<31.9	57.9 ± 33.1	-0.52
J0235.8-0524	02 35 44.90	4.2	-05 24 36.88	3.5	S	0.20 ± 0.04	<37.4	<26.1	163.1 ± 44.0	-0.41
J0235 9-0803	02 35 54 50	4.2	-08 03 49 68	3.6	M	0.68 ± 0.10	42.8 + 24.3	<20.0	143.0 + 7.6	-0.63

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Table A.2. continued.

Name	RA	σ_{lpha}	Dec	σ_{δ}	Туре	S _{comp}	Major axis	Minor axis	Position	Spectral
	J2000	arcsec	J2000	arcsec		Jy	arcsec	arcsec	Angle	index α_{74}^{1400}
	02 35 55.67	4.2	-08 03 37.17	3.1	С	0.48 ± 0.08	<42.1	<28.0	46.9 ± 28.8	
J0236.1-0250	02 36 06.38	3.5	-02 50 10.74	2.2	S	0.84 ± 0.07	<28.0	<18.4	24.0 ± 17.0	-0.90
J0236.1-0628	02 36 08.59	4.6	-06 28 28.02	4.0	S	0.34 ± 0.07	<59.3	<30.9	140.8 ± 17.7	-0.61
J0236.3-0157	02 36 15.45	3.9	-01 57 32.86	2.8	S	0.31 ± 0.05	<31.1	<23.9	46.0 ± 50.7	-0.63
J0236.4-0437	02 36 21.62	3.7	-04 37 38.72	2.4	S	0.76 ± 0.08	<35.9	<30.2	91.8 ± 37.1	-0.87
J0236.4-0730	02 36 24.99	6.3	-07 30 29.42	4.8	S	0.42 ± 0.10	<81.2	<41.5	122.9 ± 17.7	-0.91
J0236.4-0334	02 36 26.30	4.5	-03 34 50.75	3.7	S	0.28 ± 0.06	<51.6	<25.9	139.7 ± 19.1	-0.47
J0236.6-0358	02 36 37.72	3.9	-03 58 24.54	3.0	S	0.13 ± 0.03	<22.5	<15.3	177.5 ± 75.4	-0.62
J0236.7+0131	02 36 39.65	5.0	+01 31 10.79	4.7	S	0.42 ± 0.11	<60.3	<32.3	145.2 ± 22.8	-0.90
J0236.8-0301	02 36 45.81	3.8	-03 01 53.48	3.1	5	0.22 ± 0.04	<39.4		28.7 ± 12.6	-0.61
J0236.9-0231	02 36 51.78	4.1	-02 31 11.72	4.2	5	0.26 ± 0.05	< 33.3	<25.2	$1/0.2 \pm 16.2$	-0.46
10230.9-0428	02 30 32.43	4.0	-04 28 35.92	3.5	5 5	0.10 ± 0.04	< 38.9	<10.4	60.3 ± 27.3	-0.47
J0237.2-0348	02 37 10.40	5.4	-05 48 24.25	2.0	5 5	2.00 ± 0.11	<24.2	<17.1	02.5 ± 9.0	-0.79
J0237.0-0243	02 37 30.05	4.0	-02 43 03.40	5.9 2.5	5	0.14 ± 0.04	< 38.7	<20.7	35.3 ± 35.0 151.2 ± 29.1	-0.38
10237.8-0033	02 37 46.30	4.2 5.4	-07 19 07 97	5.5	S	0.41 ± 0.07 0.30 ± 0.07	<82.8	<24.5	131.2 ± 20.1 141.2 ± 10.1	-1.02
J0238 0_0145	02 37 40.91	3.4	-01 45 11 66	2.0	S	4.05 ± 0.07	<24.0	<24.5	58.1 ± 11.3	-0.79
10238 2-0628	02 37 37.05	3.5	-06285158	2.0	S	1.03 ± 0.21 1.14 ± 0.09	<34.4	<20.2	104.7 ± 15.5	-0.59
I0238 3-0257	02 38 15 37	44	-02574471	3.8	S	0.21 ± 0.05	<40.4	<28.8	169 ± 472	-0.61
10238 3-0330	02 38 18 77	34	-03 30 18 42	2.0	S	2.98 ± 0.16	<72.4	<18.9	77.1 ± 13.4	-0.72
10238 4-0616	02 38 23 66	35	-06 16 18 26	2.0	S	1.13 ± 0.09	<27.9	<26.0	148.9 + 78.3	-0.59
10238 4-0348	02 38 24 15	4.3	-03 48 29 57	3.6	S	0.27 ± 0.05	<42.9	<32.8	5.0 + 47.4	-0.56
J0238.5-0616	02 38 28.24	3.5	-06 16 16.96	2.3	Š	0.96 ± 0.08	<32.5	<23.8	168.4 ± 19.1	-0.79
J0238.5-0425	02 38 28.39	4.1	-04 25 36.56	3.9	ŝ	0.38 ± 0.07	<62.5	<24.9	25.0 ± 10.8	-0.62
J0238.6-0607	02 38 32.97	4.5	-06 07 27.66	4.0	ŝ	0.19 ± 0.05	<41.0	<28.0	19.1 ± 46.6	-0.56
J0238.6-0432	02 38 35.24	3.5	-04 32 37.91	2.2	ŝ	0.73 ± 0.06	<30.1	<20.4	95.3 ± 17.2	-0.65
J0238.6-0103	02 38 37.56	3.9	-01 03 14.25	2.9	S	0.38 ± 0.06	<32.8	<27.6	164.0 ± 70.2	-0.77
J0238.9-0156	02 38 53.86	4.3	-01 56 07.70	3.3	S	0.35 ± 0.06	<44.1	<32.3	50.3 ± 37.2	-0.69
J0239.0-0255	02 38 57.05	3.5	-02 55 08.62	2.1	S	0.81 ± 0.06	<24.6	<20.7	66.6 ± 38.6	-0.61
J0239.0+0056	02 38 59.94	3.8	+00 56 12.33	3.0	S	0.60 ± 0.09	<38.0	<20.5	155.7 ± 20.3	-0.69
J0239.2-0851	02 39 09.75	4.9	-08 51 12.85	4.9	S	0.70 ± 0.15	<68.7	<46.5	161.5 ± 26.9	-0.99
J0239.2-0715	02 39 12.88	6.5	-07 15 46.40	5.4	S	0.65 ± 0.15	50.0 ± 41.2	<57.6	126.4 ± 22.3	-0.96
J0239.2-0118	02 39 13.47	3.4	-01 18 15.78	2.0	S	3.18 ± 0.18	21.1 ± 8.6	<19.0	51.1 ± 5.9	-0.87
J0239.4-0413	02 39 25.59	4.3	-04 13 01.46	3.3	S	0.15 ± 0.03	<32.0	<22.3	45.0 ± 54.4	-0.40
J0239.6-0506	02 39 33.01	4.2	-05 06 13.85	3.1	S	0.16 ± 0.03	<28.4	<17.9	128.5 ± 51.1	-0.51
J0239.6-0845	02 39 37.66	4.6	-08 45 31.77	4.0	S	1.17 ± 0.18	48.6 ± 25.2	<44.5	37.6 ± 14.9	-0.76
J0239.7-0218	02 39 39.79	3.8	-02 18 39.05	3.0	S	0.25 ± 0.04	<33.4	<18.1	2.1 ± 25.7	-0.49
J0239.7-0117	02 39 42.42	3.5	-01 17 17.38	2.1	S	1.19 ± 0.09	<26.4	<20.8	52.1 ± 25.2	-0.83
J0239.8-0234	02 39 45.73	5.1	-02 34 40.34	4.4	S	0.31 ± 0.07	<67.0	<32.0	136.5 ± 16.5	0.00
J0239.8-0057	02 39 48.88	5.1	-00 57 40.73	3.7	S	0.45 ± 0.09	<58.1	<37.6	63.1 ± 26.0	-0.74
J0239.9-0302	02 39 52.97	4.2	-03 02 06.54	3.2	S	0.14 ± 0.03	<26.5	<20.1	135.1 ± 86.3	-0.54
J0240.0-0057	02 39 57.07	4.1	-00 57 51.76	3.3	S	0.52 ± 0.09	<42.7	<35.3	3.4 ± 52.8	-0.67
J0240.1-0636	02 40 06.39	4.1	-06 36 42.22	4.2	S	0.37 ± 0.07	<60.6	<24.5	161.4 ± 12.6	-0.60
J0240.2-0331	02 40 11.38	4.9	-03 31 19.20	4.2	S	0.38 ± 0.08	<68.7	<32.9	139.1 ± 14.2	-0.70
J0240.3-0331	02 40 16.23	5.9	-03 31 39.64	3.9	S	0.40 ± 0.09	<71.9	<42.8	101.4 ± 20.8	-0.58
J0240.4-0130	02 40 25.80	3.6	-01 30 25.62	2.3	S	0.65 ± 0.07	<29.6	<18.4	57.5 ± 20.0	-0.78
J0240.5-0128	02 40 30.24	4.9	-01 28 14.53	3.4	S	0.27 ± 0.06	<50.8	<22.2	116.3 ± 18.7	-0.66
J0240.6-0408	02 40 35.30	4.1	-04 08 51.53	3.4	S	0.65 ± 0.09	49.5 ± 20.7	<26.9	144.5 ± 7.3	-0.88
J0240.6-0723	02 40 36.70	4.0	-0/231/.0/	2.9	M	0.69 ± 0.09	37.1 ± 20.3	<20.2	134.5 ± 7.9	-0.56
10240 7 0(20	02 40 37.81	2.5	-0/2307.96	3.5	C	0.37 ± 0.08	<03.1	<30.4	$/1.4 \pm 10.9$	0.50
J0240.7-0038	02 40 39.33	5.0 2.5	-00 38 23.09	2.7	5 5	0.88 ± 0.10	51.5 ± 10.4	<23.1	140.7 ± 9.4	-0.39
J0240.7-0440	02 40 41.10	5.5 2 7	-04 40 14.92	2.1	S M	1.00 ± 0.08	< 29.0	< 19.5	05.7 ± 15.8	-0.62
J0240.9-0138	02 40 53.58	2.0	-01 37 33.39	2.5	C NI	0.91 ± 0.11	53.9 ± 10.0	<22.0	$1/1.0 \pm 3.3$	-0.09
10240 0-0504	02 40 54.50	J.0 4.0	$-01\ 38\ 24.38$ $-05\ 04\ 41\ 35$	2.0	c c	0.40 ± 0.00	<54.5	<46.5	20.3 ± 29.7 178.6 \pm 75.3	-0.15
10241.0-0022	02 40 50.31	37	-00.2251.46	27	S	0.57 ± 0.00	<31.2	<70.5	83 ± 364	-0.13
J0241.0-0022 J0241.0-0020	02 40 58 66	4 1	-00 22 31.40	3.2	S	0.05 ± 0.09	<35.2	\22.0	0.5 ± 50.4	-0.58
I0241.1-0236	02 40 50.00	3.9	-02364605	2.6	S	0.30 ± 0.09 0.42 ± 0.06	<32.6		 78 6 + 50 9	-0.95
J0241.1-0815	02 41 05 48	4.2	-08 15 17 21	3.2	S	0.12 ± 0.00 0.91 ± 0.13	<48.7	\$20.5	70.0 ± 50.9	0.01
J0241.3-0533	02 41 15 98	4.6	-05 33 48 79	4.3	S	0.27 ± 0.06	<49.1	<35.2	1684 + 433	-0.51
I0241.5-0235	02 41 29 24	4.3	-02 35 12 31	4.2	Š	0.19 ± 0.05	<45.6	<23.1	166.7 ± 25.7	-0.62
J0241.5-0431	02 41 29.82	5.6	$-04\ 31\ 22.68$	4.2	Š	0.28 ± 0.07	<58.5	<42.1	71.4 ± 40.9	-0.78
J0241.6-0418	02 41 36.20	3.4	-04 18 20.45	2.1	S	1.42 ± 0.10	<27.7	<24.4	73.9 ± 37.1	-0.51
J0241.6-0647	02 41 38.22	3.4	-06 47 28.03	2.0	S	6.36 ± 0.33	25.2 ± 6.2	<21.8	125.5 ± 4.0	-0.71
J0241.6-0348	02 41 38.38	3.5	-03 48 41.40	2.3	S	0.63 ± 0.06	<26.6	<16.8	153.6 ± 21.0	-0.78
J0241.7-0357	02 41 40.41	5.0	-03 57 24.10	3.7	S	0.22 ± 0.05	<48.8	<30.0	58.8 ± 31.4	-0.67
J0241.7-0349	02 41 42.42	4.4	-03 49 40.37	3.0	Μ	0.41 ± 0.07	<55.7	<21.7	57.9 ± 11.3	-1.01
	02 41 42.15	5.4	-03 49 28.61	4.6	С	0.33 ± 0.07	<78.5	<24.9	134.4 ± 10.4	
J0241.7-0416	02 41 44.25	4.6	-04 16 45.42	3.2	S	0.51 ± 0.09	<56.1	<32.9	64.5 ± 18.1	-0.60
J0241.9-0241	02 41 52.10	4.0	-02 41 51.54	2.6	S	0.44 ± 0.06	<40.0	<24.0	90.4 ± 20.5	-0.47
J0241.9-0607	02 41 56.30	4.1	-06 07 12.05	3.4	S	0.28 ± 0.05	<38.1	<21.5	154.8 ± 27.9	-0.45
J0242.1-0128	02 42 08.16	3.5	-01 28 36.84	2.3	S	1.49 ± 0.12	20.9 ± 15.8	<29.1	150.9 ± 21.1	-0.71
J0242.3-0548	02 42 15.42	4.4	-05 48 28.55	3.6	S	0.57 ± 0.10	<52.8	<41.5	39.0 ± 38.6	-0.60
J0242.3-0240	02 42 18.52	3.5	-02 40 41.37	2.2	S	0.74 ± 0.07	<23.9	<20.7	23.5 ± 61.6	-0.67

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Table A.2. continued.

Name	RΔ	Œ	Dec	σc	Type	S	Major avis	Minor avis	Position	Spectral
INallie	12000	O_{α}	12000	08	Type	S comp			Angla	index al400
10242 2 0227	J2000	arcsec	J2000	arcsec	C	Jy	arcsec	arcsec		α_{74}
J0242.3-0337	02 42 18.79	5.0	-03 37 32.23	4.5	5	0.30 ± 0.08	<01.3	< 39.0	35.8 ± 27.7	-0.77
J0242.3+0009	02 42 19.75	4.0	+00 09 08.49	4./	5	0.59 ± 0.14	<05.8	<15.5	31.2 ± 10.9	-1.21
J0242.4-0012	02 42 22.66	4.3	-00 12 39.94	5.0	S	0.56 ± 0.14	4.0</td <td><15.5</td> <td>17.2 ± 9.9</td> <td>-1.66</td>	<15.5	17.2 ± 9.9	-1.66
J0242.4-0408	02 42 23.06	3.6	-04 08 58.40	2.3	S	0.69 ± 0.07	<29.0	<22.9	113.6 ± 36.6	-0.69
J0242.7-0000	02 42 40.45	3.4	-00 00 45.91	2.0	S	26.90 ± 1.36	23.1 ± 5.4	15.9 ± 7.7	46.5 ± 3.8	-0.58
J0242.7-0311	02 42 43.07	3.6	-03 11 45.87	2.2	S	1.34 ± 0.11	33.3 ± 12.1	<24.4	122.1 ± 7.6	-0.48
J0242.7-0332	02 42 43.44	3.8	-03 32 32.69	2.6	S	0.67 ± 0.08	<35.6	<31.5	26.5 ± 66.9	-0.71
J0242.8-0334	02 42 46.69	4.3	-03 34 30.61	3.4	S	0.74 ± 0.11	36.8 ± 24.0	<39.2	139.1 ± 17.5	-0.48
J0242.8-0157	02 42 47.61	3.4	-01 57 47.39	2.1	S	1.73 ± 0.12	<25.2	<23.0	6.3 ± 51.0	-0.70
J0243.2-0550	02 43 12.71	4.4	-05 50 54.67	3.4	S	0.39 ± 0.08	<42.5	<36.4	122.2 ± 76.1	0.13
J0243.3-0356	02 43 17.15	3.5	-03 56 58.22	2.2	S	0.95 ± 0.08	<31.2	<24.8	118.9 ± 26.7	-0.59
J0243.4-0433	02 43 23.20	3.8	-04 33 36.48	2.5	S	0.52 ± 0.07	<36.0	<23.6	76.5 ± 23.1	-0.68
J0243.5-0232	02 43 31.35	3.4	-02 32 55.83	2.1	S	1.58 ± 0.11	<27.4	<24.2	120.9 ± 38.8	-0.48
J0243.7-0718	02 43 42.03	4.2	-07 18 03.45	3.2	S	0.87 ± 0.13	35.5 ± 23.6	<34.0	134.1 ± 14.1	-0.80
J0243.8-0118	02 43 46.06	4.8	-01 18 06.51	4.7	S	0.53 ± 0.12	<56.7	<42.5	0.7 ± 43.4	-1.20
J0243.8-0102	02 43 48.96	3.9	-01 02 52.18	2.7	S	0.95 ± 0.12	<36.8			-0.56
J0243.9-0305	02 43 53.20	3.5	-03 05 06.67	2.2	S	0.97 ± 0.08	<26.1	<22.4	136.6 ± 46.9	-0.56
J0243.9-0027	02 43 56.55	3.8	-00 27 28.85	2.6	S	1.39 ± 0.16	23.5 ± 22.8	<29.5	50.9 ± 15.5	-0.86
J0244.0-0349	02 44 00.89	3.9	-03 49 55.45	3.1	S	0.45 ± 0.07	<47.0	<24.2	149.0 ± 15.4	-0.75
J0244.2-0443	02 44 11.35	4.7	-04 43 20.80	3.2	S	0.32 ± 0.06	<45.6	<28.6	83.3 ± 28.1	-0.59
J0244.3-0427	02 44 20.77	3.5	-04 27 45.32	2.1	S	1.25 ± 0.10	<33.2	<23.3	87.0 ± 14.4	-0.58
J0244.4-0653	02 44 23.17	3.5	-06 53 27.29	2.1	S	2.26 ± 0.15	30.7 ± 9.3	<20.7	118.5 ± 5.6	-0.87
J0244.4-0527	02 44 26.62	3.4	-05 27 15.94	2.0	S	2.44 ± 0.15	21.6 ± 9.7	<22.0	105.4 ± 8.8	-0.78
J0244.6-0310	02 44 33.79	5.2	-03 10 23.51	3.8	S	0.25 ± 0.06	<48.5	<30.7	112.6 ± 35.3	-0.77
J0244.6-0648	02 44 35.98	4.7	-06 48 49.21	3.9	S	0.35 ± 0.08	<52.2	<25.3	136.8 ± 20.1	-1.35
J0244.8-0547	02 44 50.06	7.9	-05 47 52.00	3.7	M	0.92 ± 0.18	82.9 ± 38.1	<44.9	91.6 ± 8.0	-0.71
	02 44 50.52	4.9	-05 47 25.72	3.4	С	0.47 ± 0.09	<60.4	<28.3	119.2 ± 14.8	
J0244.9-0548	02 44 54.01	4.7	-05 48 28.31	3.2	S	1.15 ± 0.16	54.5 ± 21.8	<43.7	115.4 ± 11.5	-0.64
J0244.9-0257	02 44 56.51	6.6	-02 57 46.80	3.9	S	0.47 ± 0.10	<85.3	<36.3	107.7 ± 12.6	-0.87
J0245.0-0447	02 44 57.66	3.7	-04 47 48.26	2.5	S	0.62 ± 0.07	<31.7	<28.6	136.8 ± 85.8	-0.94
J0245.1-0504	02 45 08.04	5.0	-05 04 43.14	4.3	S	0.44 ± 0.09	<65.1	<34.4	136.9 ± 18.0	-0.97
J0245.1-0452	02 45 08.38	3.7	-04 52 25.54	2.6	S	0.53 ± 0.07	<30.7	<26.1	135.0 ± 61.0	-0.82
J0245.2-0133	02 45 09.73	3.5	-01 33 50.27	2.2	S	1.59 ± 0.13	<34.7	<27.9	79.4 ± 23.7	-0.89
J0245.3-0256	02 45 19.65	4.4	-02 56 27.30	4.3	S	0.35 ± 0.08	<53.2	<30.8	160.5 ± 24.5	-0.52
J0245.6-0646	02 45 38.53	4.4	-06 46 16.39	3.1	S	0.55 ± 0.10	<51.1	<24.8	121.9 ± 15.9	-0.73
J0245.8-0300	02 45 46.12	4.0	-03 00 59.87	2.7	M	0.37 ± 0.06	<31.9	<22.4	100.8 ± 37.5	-0.65
	02 45 46.36	4.7	-03 00 44.97	3.0	С	0.26 ± 0.05	<46.3	<17.3	69.5 ± 16.8	
J0245.8-0518	02 45 50.48	3.8	-05 18 57.56	2.6	S	0.62 ± 0.08	<40.7	<21.0	126.0 ± 14.3	-0.70
J0246.1-0600	02 46 03.51	5.2	-06 00 25.01	3.6	S	0.38 ± 0.08	<57.8	<29.0	115.2 ± 18.9	-0.71
J0246.2-0335	02 46 11.84	3.9	-03 35 23.95	2.8	S	0.48 ± 0.07	<33.7	<29.6	102.0 ± 82.4	-0.68
J0246.2-0228	02 46 12.46	3.7	-02 28 35.71	2.7	S	0.69 ± 0.08	<36.9	<25.2	164.9 ± 23.2	-0.89
J0246.3-0131	02 46 18.64	3.8	-01 31 36.07	2.7	S	0.81 ± 0.10	<37.9	<29.5	129.7 ± 34.5	-0.59
J0246.4-0508	02 46 22.39	5.2	-05 08 57.41	4.3	S	0.58 ± 0.12	<66.2	<43.8	47.8 ± 25.6	-0.89
J0246.4-0449	02 46 22.93	3.4	-04 49 29.50	2.1	S	2.86 ± 0.18	41.2 ± 7.8	19.5 ± 11.6	23.7 ± 5.5	-0.79
J0246.8-0145	02 46 47.11	3.6	-01 45 33.12	2.3	S	1.36 ± 0.12	<35.2	<25.8	113.0 ± 19.7	-0.78
J0247.1-0529	02 47 07.04	4.0	-05 29 58.15	3.0	S	0.47 ± 0.08	<40.4	<20.0	143.4 ± 18.5	-0.69
J0247.1-0528	02 47 07.48	4.5	-05 28 12.31	3.6	S	0.35 ± 0.08	<46.8	<24.9	133.0 ± 23.4	-0.75
J0247.2-0354	02 47 09.65	3.9	-03 54 45.17	2.8	S	0.74 ± 0.10	<38.4			-0.76
J0247.3-0554	02 47 16.56	3.5	-05 54 41.18	2.2	S	2.05 ± 0.15	28.1 ± 11.0	<25.6	138.5 ± 9.5	-0.64
J0247.4-0338	02 47 25.04	4.4	-03 38 04.59	2.8	S	0.31 ± 0.06	<40.2	<20.0	93.7 ± 22.2	-0.43
J0247.5-0458	02 47 31.42	5.7	-04 58 14.87	4.3	S	0.62 ± 0.13	<66.4	<52.2	86.1 ± 44.3	-0.84
J0247.6-0538	02 47 35.07	4.8	-05 38 40.37	4.5	S	0.47 ± 0.10	<62.2	<34.2	148.2 ± 20.1	-0.85
J0248.1-0331	02 48 03.89	4.8	-03 31 41.64	3.4	S	0.68 ± 0.12	<55.6	<40.6	96.8 ± 30.3	-0.95
J0248.1-0432	02 48 05.34	6.0	-04 32 42.97	4.3	S	0.56 ± 0.13	<68.2	<50.3	85.1 ± 37.7	-0.65
J0248.2-0415	02 48 09.86	4.3	-04 15 02.18	3.2	S	0.79 ± 0.12	<48.7	<43.4	111.4 ± 73.9	-0.36
J0248.2-0415	02 48 12.41	4.2	-04 15 54.16	4.1	S	1.45 ± 0.19	61.5 ± 21.7	<46.9	159.1 ± 10.3	-0.60
J0248.2-0313	02 48 13.95	4.1	-03 13 16.64	3.0	М	0.48 ± 0.08	<46.1	<15.5	133.4 ± 12.3	-0.75
	02 48 14.89	4.6	-03 13 09.12	4.0	Ĉ	0.30 ± 0.07	<53.1	<17.5	38.9 ± 15.6	
J0248.5-0512	02 48 32.47	4.2	-05 12 59.20	3.2	S	0.38 ± 0.07	<37.7	<23.8	138.3 ± 32.7	-0.62

An asterisk (*) after the sourcename indicates this source was also detected at 325 MHz.

Description of columns:

Right Ascension (J2000).
 Right Ascension uncertainty in arcseconds.
 Declination (J2000).
 Declination uncertainty in arcseconds.

Declination uncertainty in arcseconds.
 Source type: Single (S), Multiple (M) or Component (C) of multiple source.
 Flux density of individual componant in Jy as derived through the Gaussian fitting method.
 Size of Major Axis in arcseconds, or the 2σ upper limit if the source is unresolved.
 Size of Major Axis in arcseconds, or the 2σ upper limit if the source is unresolved.
 PA of Major axis in degrees.
 Spectral index with respect to NVSS flux density (1.4 GHz).

^{1.} Source Name.