



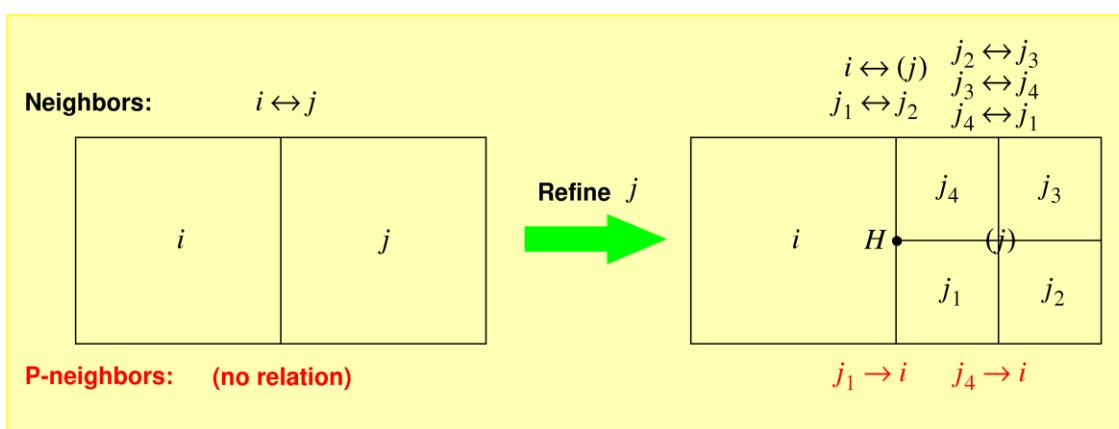
## J R C   T E C H N I C A L   R E P O R T S

# Adaptivity in CEA's Fluid Elements in EUROPLEXUS

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2014

Report EUR 26632 EN



**European Commission**  
Joint Research Centre  
Institute for the Protection and Security of the Citizen

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JRC89953  
EUR 26632 EN  
ISBN 978-92-79-37968-0  
ISSN 1831-9424  
doi:10.2788/72737

Luxembourg: Publications Office of the European Union, 2014

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Printed in Italy

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# 1. Introduction

This report is a sequel to reports and publications [1-13] on mesh adaptivity in fast transient dynamics and presents the implementation of mesh adaptivity for CEA's fluid elements (triangles and quadrilaterals in 2D, tetrahedra and hexahedra in 3D) in fast transient dynamics. The algorithms are implemented in the EUROPLEXUS code.

EUROPLEXUS [14] is a computer code for fast explicit transient dynamic analysis of fluid-structure systems jointly developed by the French Commissariat à l'Energie Atomique et aux Energies Alternatives (CEA Saclay) and by the Joint Research Centre of the European Commission (JRC Ispra).

Reference [1] presented the first implementation in EUROPLEXUS of an adaptive mesh refinement and un-refinement procedure, in two space dimensions (element shape QUA4) for solid mechanics. The procedure was extended to fluid mechanics (FE formulation) in 2D in reference [2]. Then, reference [3] applied a similar refinement and un-refinement procedure in three space dimensions to the CUB8 element shape, both in solids mechanics and in fluid mechanics (FE formulation).

All numerical examples presented in references [1-3] with a variable mesh used a so-called "manual" mesh adaptation directive, the WAVE directive (see the code manual in reference [14]), first introduced in reference [1]. This directive refines the mesh along "wavefronts" that are specified by the user, e.g. according to a known analytical solution to the problem considered. This technique was used with success to simulate a bar problem (in solid mechanics) and a shock tube problem (in fluid mechanics) both in 2D and in 3D [1-3].

However, those solutions cannot be qualified as "true" adaptive solutions, because in (true) adaptivity mesh refinement and un-refinement should be completely automatic, based upon suitable *error estimators* or *error indicators*. The formulation of error estimators in fast transient dynamics is challenging and is still a subject of research. The use of so-called error indicators, however, is much simpler. For this reason, subsequent work in EUROPLEXUS focused on error indicators. References [4] and [5] document a first prototype implementation of adaptivity based upon error indicators in EUROPLEXUS, limited to 2D problems in continuum and fluid mechanics. An extension of the indicator technique to 3D is under development but has not been completed and documented yet.

Publications [6-7] focus on the natural quantities of interest in goal-oriented error assessment and adaptivity, but limited to the case of linear elasto-dynamics.

The adaptive technique was then applied to Cell-Centred Finite Volumes (CCFV) for the description of the fluid domain, first in 2D (see [8]) and then also in 3D [9]. More recently, the technique has also been extended for use with the CDEM combustion model which makes use of the CCFV formulation [10]. A complete description of the element refinement and un-refinement techniques used in

mesh adaptation has been published in a paper [11]. Finally, reference [12] shows the combination of mesh adaptivity with Fluid-Structure Interaction, i.e. the automatic fluid mesh refinement and unrefinement near a moving and deforming structure.

Reference [13] extends mesh adaptivity to simplex element shapes, i.e. the 3-node triangle (TRI3) in 2D and the 4-node tetrahedron (TET4) in 3D. These elements are useful in fully general unstructured meshing of complex geometries. The extension covered solid continuum elements (CEA's TRIA and TETR elements *with solid material*), and for fluid Finite Elements (JRC's FL23 and FL34 elements) and Cell-Centered Finite Volumes (CEA's T3VF and TEVF elements).

The present work completes the implementation by extending adaptivity to CEA's fluid finite elements both in 2D (TRIA and CAR1) and in 3D (TETR and CUBE). The CAR1 is treated like other 2D quadrilaterals (Q41L, FL24) as far as geometrical issues are concerned. In addition to the solid case, the activation of adaptivity for fluids requires the suitable treatment of transport terms which arise in the Eulerian or ALE forms of the governing equations. For the CEA's fluid finite elements mentioned above (TRIA, CAR1, TETR and CUBE) this is done in routines `tr2me.ff` (for the 2D case) and `tr3me.ff` (for the 3D case), respectively. Therefore, most modifications for the current implementation are concentrated in those two routines. Actually, a special version of the routines is written, valid for the mesh adaptive case, but incompatible (for the moment) with the KAAPI library and with spatial partitioning, in order to limit the complexity of the resulting code.

This document is organized as follows:

- Section 2 presents the treatment of transport terms.
- Section 3 presents some numerical examples with 2D fluid elements (TRIA, CAR1).
- Section 4 presents some numerical examples with 3D fluid elements (TETR, CUBE).
- The references are listed in Section 5.

The Appendix contains a listing of all the input files mentioned in the present report.

## 2. Treatment of transport terms in adaptivity for CEA's fluid FEs

The CEA implementation of fluid Finite Elements differs somewhat from the one of JRC similar elements, that had been described e.g. in Section 2.2 of reference [2]. The conservation equations (Euler equations) are the same in both cases, of course, but CEA's approach is to use the same element routine for both solid and fluid, and to treat the transport terms in a separate routine (tr2me.ff for the 2D case and tr3me,ff for the 3D case). These routines compute the mass and energy transport terms across each face of the fluid elements. Faces are 2-node segments in 2D, and either 3-node triangles or 4-node quadrilaterals in 3D.

Although there are differences with respect to JRC's implementation, the key point is that in both cases the so-called “lowest-index rule” is used when computing transport between two neighboring elements, see Section 2.2.3 of reference [2]. Therefore, in CEA's fluid elements a similar extension to the adaptive case can be applied to the one adopted in JRC case and described in detail in Section 2.3 of reference [2].

This extension is based upon the generalization of “neighbor” definition and on the addition of a “pseudo-neighbor” definition, which applies to portions of the fluid-fluid interfaces which are non-conforming due to the presence of so-called hanging nodes in an adaptively refined mesh. These definitions are recalled below, see also the Figure 1 from reference [2].

### **Definition of (regular) neighbor element in adaptivity**

*The neighbor of an element across a given face is the same-level, active or inactive element on the other side of the face, or 0 if there is no such element.*

### **Definition of pseudo-neighbor element in adaptivity**

*The pseudo-neighbor of an (active) element across a given face is the larger (i.e. lower-level) active element on the other side of the face, or 0 if there is no such element. Inactive elements have no pseudo-neighbors.*

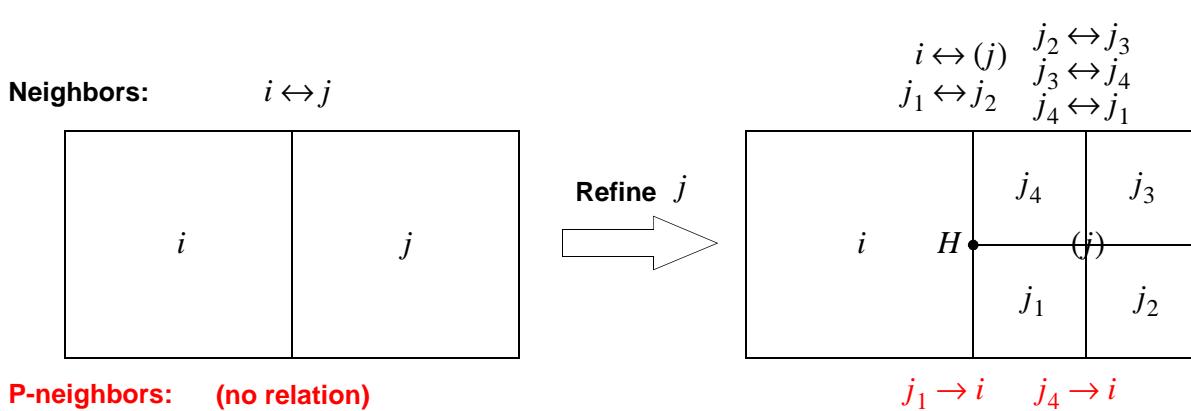


Figure 1 - Neighboring (in black) and pseudo-neighboring (in red) relations

The generalized transport algorithm, valid both in the normal (non-adaptive) and in the adaptive case, can therefore be reused as such from Section 2.3.5 of reference [2], also in the case of CEA's fluid elements. The algorithm is reported below for completeness.

#### ***General (non-adaptive or adaptive) transport algorithm***

1. Set total transport of mass and energy to zero for all elements.
2. Loop over the elements.
3. Loop over the faces of the current element  $i$ .
  4. Let  $j$  be the neighbor of  $i$  across the current face.
  5. If there is no adaptivity in the calculation, then (standard procedure):
    6. If  $j = 0$  (i.e., if there is no neighbor) skip transport for this face (GO TO 21).
    7. Else, if  $j < i$  skip transport for this face (GO TO 21).
    8. Else  $j > i$  : compute the transports of mass  $\Delta M$  and of internal energy  $\Delta I$  between  $i$  and  $j$ , add them (with the correct sign) to the total transport of mass and energy of element  $j$ , and subtract them from the total transport of mass and energy of element  $i$ . Go to next face (GO TO 21).
  9. Else there is adaptivity in the calculation.
    10. If  $j = 0$  (i.e. if there is no neighbor), let  $k$  be the pseudo-neighbor.
      11. If  $k = 0$  (i.e., if there is no pseudo-neighbor) or  $k < i$ , skip transport for this face (GO TO 21).
      12. Else  $k > i$  : compute the transports of mass  $\Delta M$  and of internal energy  $\Delta I$  between  $i$  and  $k$ , add them (with the correct sign) to the total transport of mass and energy of element  $k$ , and subtract them from the total transport of mass and energy of element  $i$ . Go to next face (GO TO 21).
    13. Else,  $j > 0$  ( $j$  is the neighbor of  $i$  across the current face).
      14. If element  $j$  is active then:
        15. If  $j < i$ , skip transport for this face (GO TO 21).
        16. Else  $j > i$  : compute the transports of mass  $\Delta M$  and of internal energy  $\Delta I$  between  $i$  and  $j$ , add them (with the correct sign) to the total transport of mass and energy of element  $j$ , and subtract them from the total transport of mass and energy of element  $i$ . Go to next face (GO TO 21).
      17. Else,  $j$  is inactive. Search and loop over all active descendants  $k$  of  $j$  which see  $i$  as pseudo-neighbor.
        18. If  $k < i$ , skip transport for this  $k$  (GO TO 20).
        19. Else  $k > i$  : compute the transports of mass  $\Delta M$  and of internal energy  $\Delta I$  between  $i$  and  $k$  by using the geometry of  $k$ , not of  $i$ , add them (with the correct sign) to the total transport of mass and energy of element  $k$ , and subtract them from the total transport of mass and energy of element  $i$ . Go to next  $k$  (GO TO 20).
      20. Next  $k$  (GO TO 15).
    21. Next face (GO TO 3).
    22. All faces have been considered for the current element and therefore its total transport of mass and energy has been computed. Update the element state to its final (end-of-step) value and compute internal forces.
    23. Next element (GO TO 2)

As anticipated in the Introduction, the (adaptive part of the) above algorithm is implemented in two new routines, `tr2me_adap.ff` for the 2D case and `tr3me_adap.ff` for the 3D case, respectively. These routines are called from the element routines whenever adaptivity is activated in a calculation, in place of the “normal” routines `tr2me.ff` and `tr3me.ff`. The separation of cases is useful to keep the algorithms readable. However, a drawback of this implementation is that adaptivity cannot be combined with the KAAPI library, nor with spatial partitioning (such cases are only treated in the normal non-adaptive version of the routines).

### 3. Numerical examples in 2D

We present some numerical examples in order to test the algorithms described in the previous Sections.

#### 3.1 Shock tube in 2D

The first example is a classical shock tube, similar to those considered in reference [2]. The adaptive mesh refinement is piloted by the WAVE directive.

First, reference solutions are obtained by means of a fine mesh of (non-adaptive) triangles (TRIA) or quadrilaterals (CAR1). Then, adaptive solutions with triangles or quadrilaterals are obtained. All performed calculations are summarized in Table 1.

Case	Base Mesh	Notes	Steps	CPU [s]	Els*step
FETR00	1,600 TRIA	Non-adaptive fine mesh CSTA 0.5	1,082	2.5	1,732,800
FETR01	200 TRIA	WAVE 4 PLAN MAXL 4 CSTA 0.25	2,279	7.9	2,865,237
FEQU00	800 CAR1	Non-adaptive fine mesh CSTA 0.5	838	1.6	671,200
FEQU01	100 CAR1	WAVE 4 PLAN MAXL 4 CSTA 0.25	1,681	4.9	1,056,875

**Table 1 - Calculations for the shock tube problem with 2D Finite Elements**

##### **FETR00**

This test uses a fine non-adaptive fluid mesh, of  $800 \times 2 = 1600$  triangular fluid elements TRIA. To obtain a solution with relatively few oscillations near the shock front, it is necessary to add some damping: OPTI AMOR QUAD 4 . 0 LINE 0 . 2. The solution is shown in Figures 2 (pressure), 3 (density) and 4 (velocity). This is taken as a reference for the subsequent adaptive solution.

##### **FETR01**

This solution is adaptive and uses a coarse base fluid mesh of 200 triangles, and four WAVE directives to track the wavefronts, with a maximum refinement level MAXL 4. A stability coefficient of 0.25 (instead of 0.5 like in the reference case) is needed to ensure stability. The solution is shown in Figures 5 (pressure), 6 (density) and 7 (velocity) and is in reasonable agreement with the reference.

##### **FEQU00**

This test uses a non-adaptive fine fluid mesh, of 800 quadrilateral fluid elements CAR1. To obtain a solution with relatively few oscillations near the shock front, it is necessary to add some damping:

OPTI AMOR QUAD 4 . 0 LINE 0 . 2. The solution is shown in Figures 8 (pressure), 9 (density) and 10 (velocity). This is taken as a reference for the subsequent adaptive solution.

### ***FEQU01***

This solution is adaptive and uses a coarse base fluid mesh of 100 CAR1, and four WAVE directives to track the wavefronts, with a maximum refinement level MAXL 4. A stability coefficient of 0.25 (instead of 0.5 like in the reference case) is needed to ensure stability. The solution is shown in Figures 11 (pressure), 12 (density) and 13 (velocity) and is in reasonable agreement with the reference.

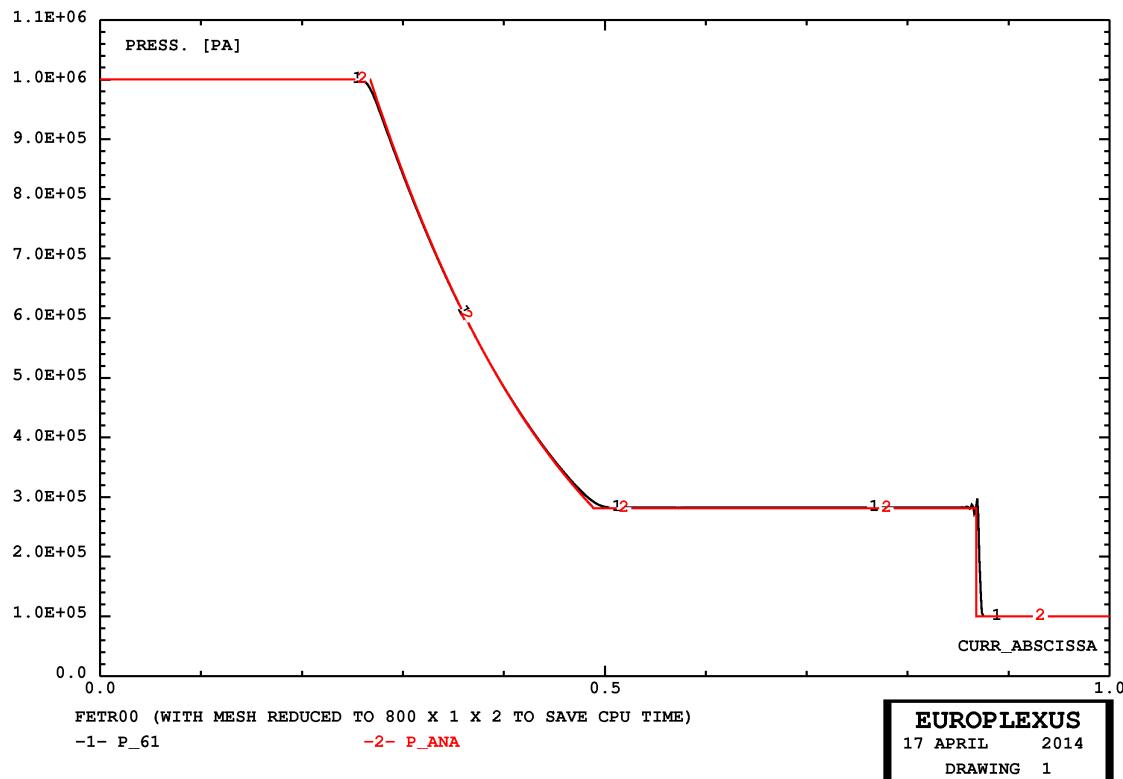


Figure 2 - Pressure in case FETR00

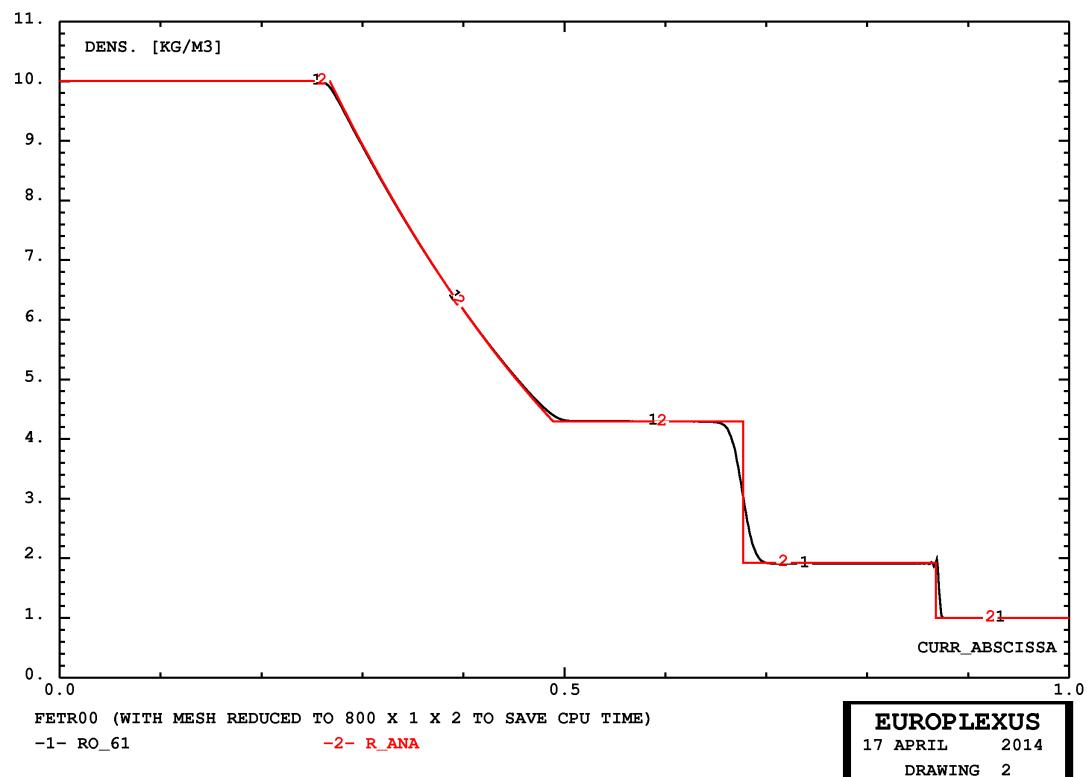


Figure 3 - Density in case FETR00

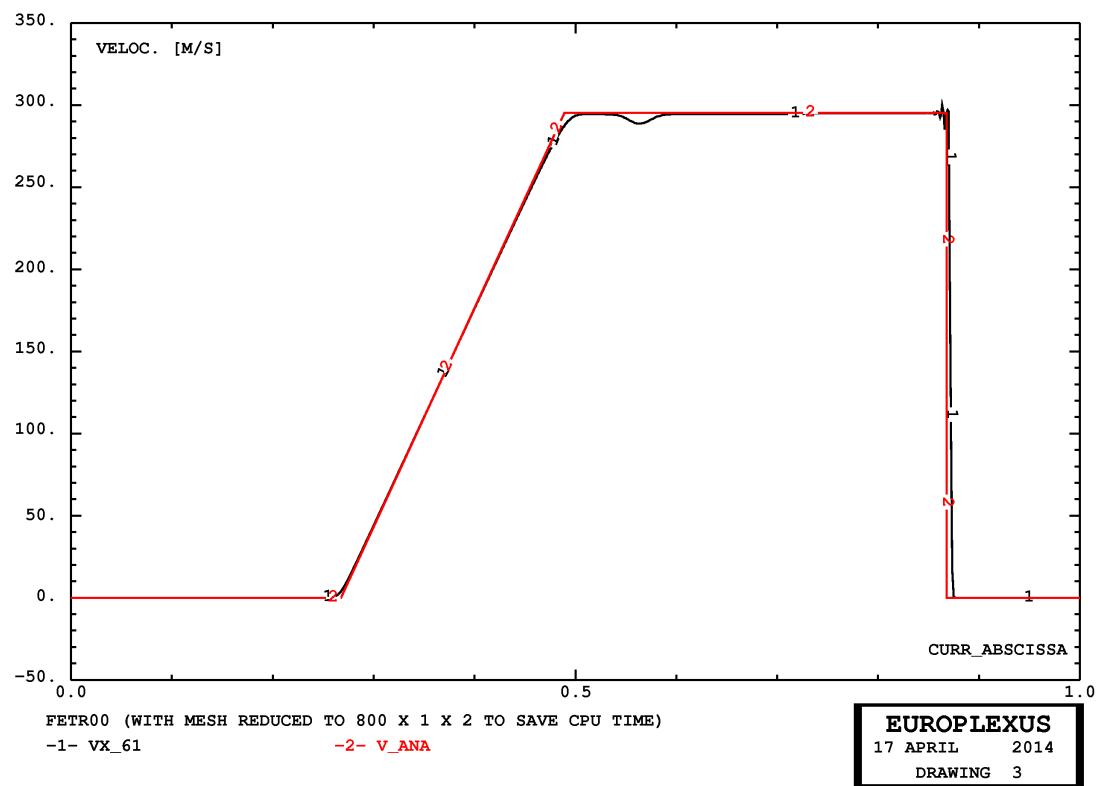


Figure 4 - Velocity in case FETR00

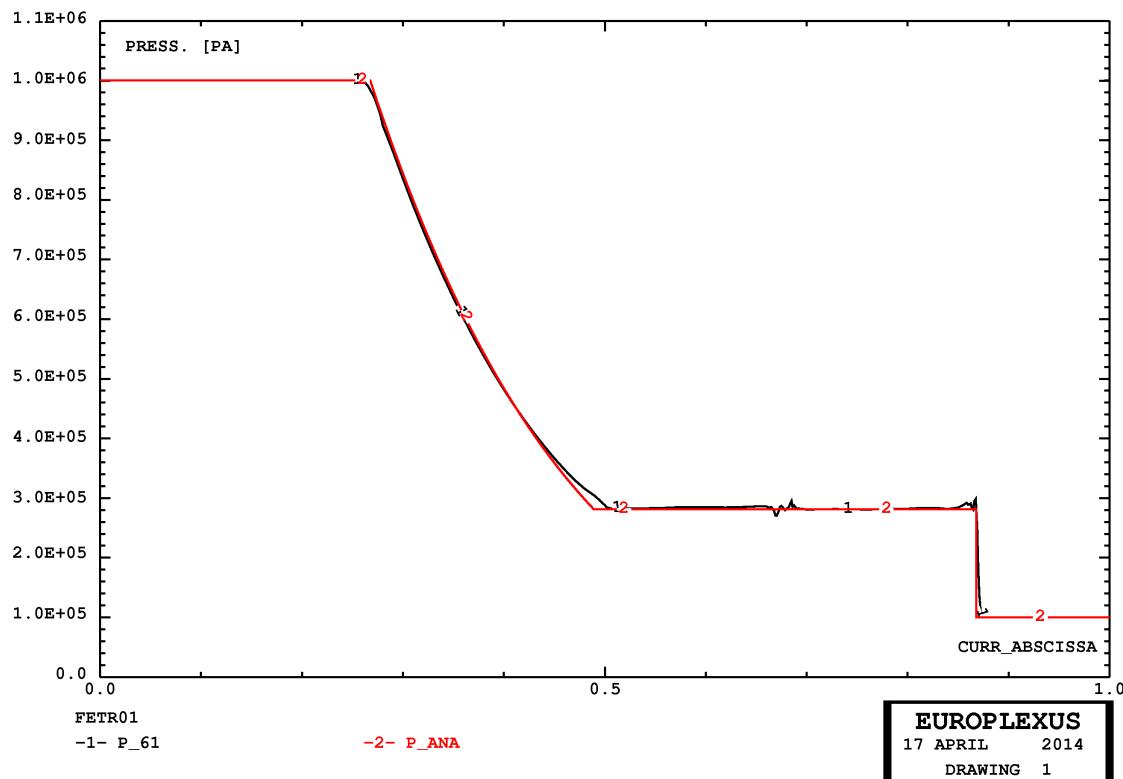


Figure 5 - Pressure in case FETR01

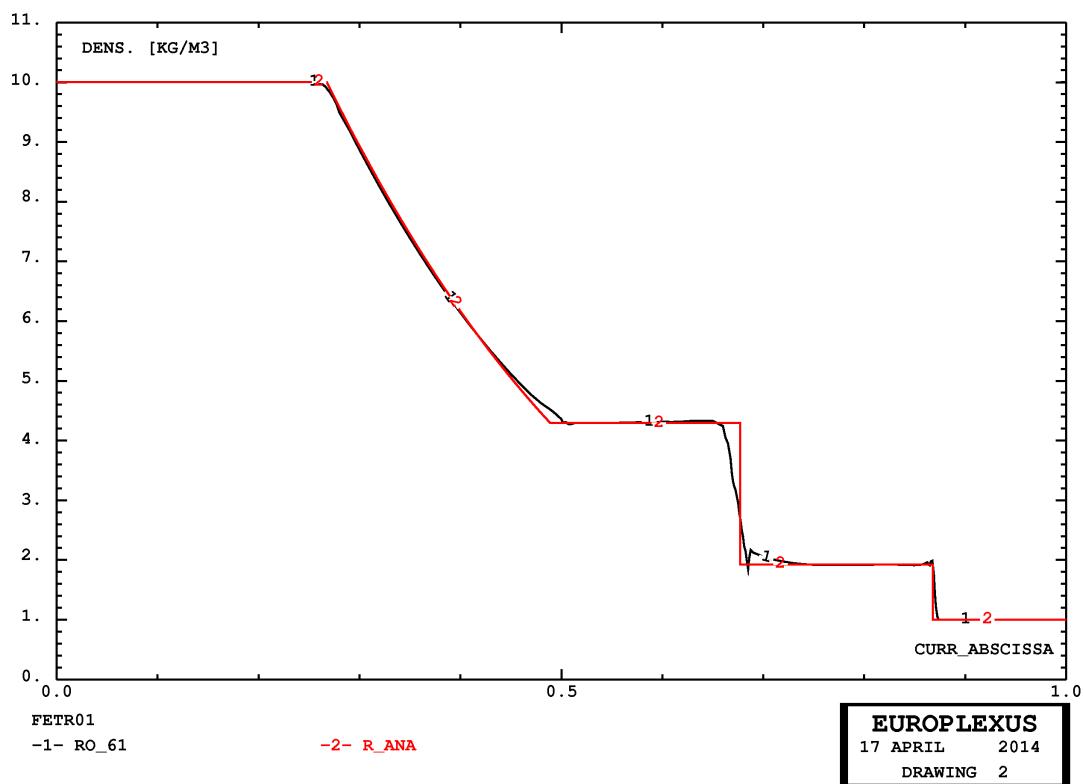


Figure 6 - Density in case FETR01

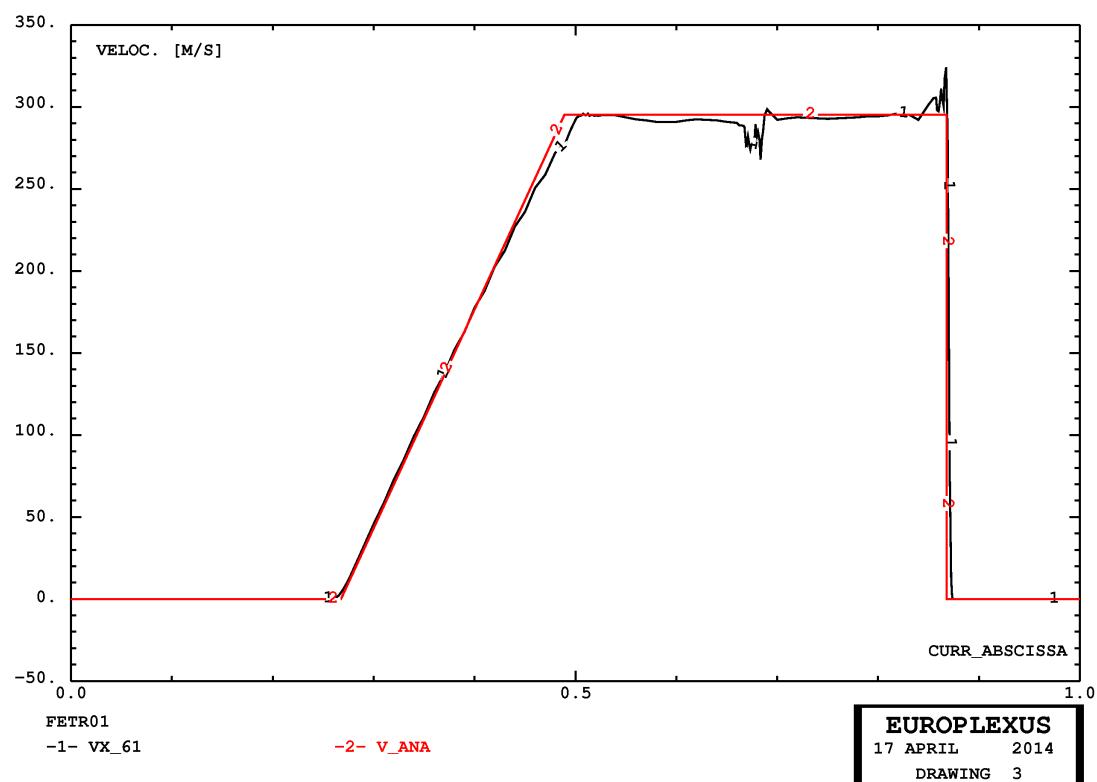


Figure 7 - Velocity in case FETR01

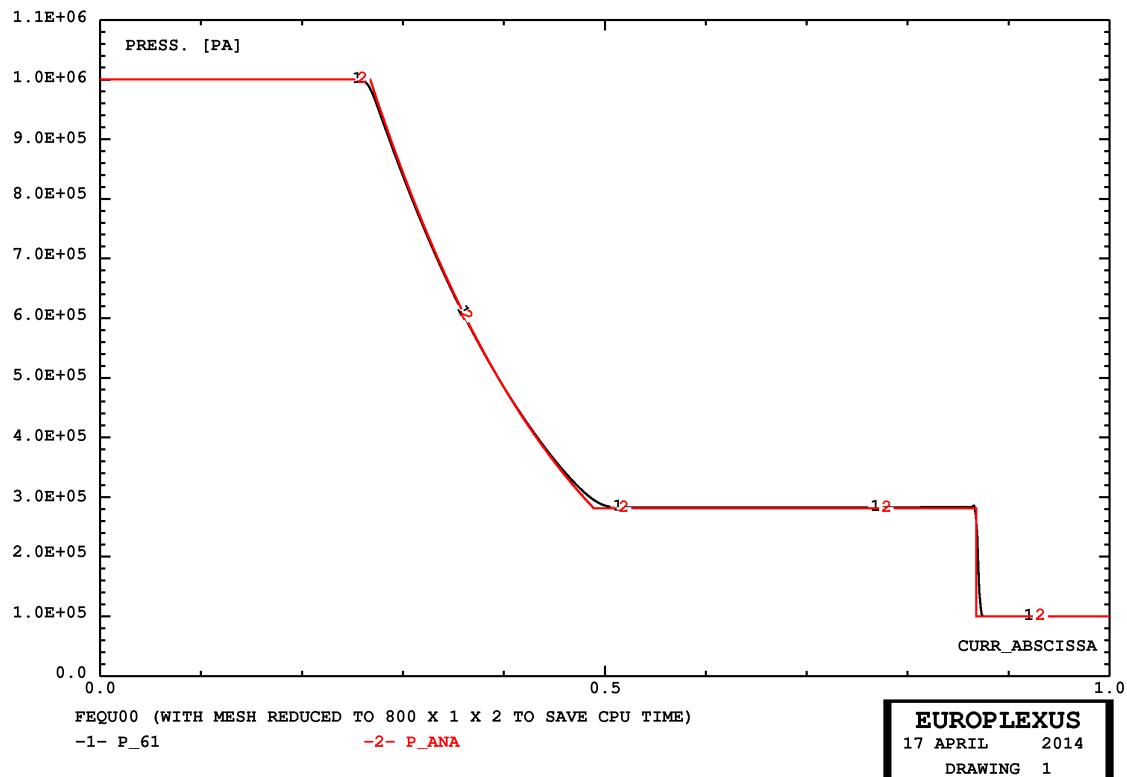


Figure 8 - Pressure in case FEQU00

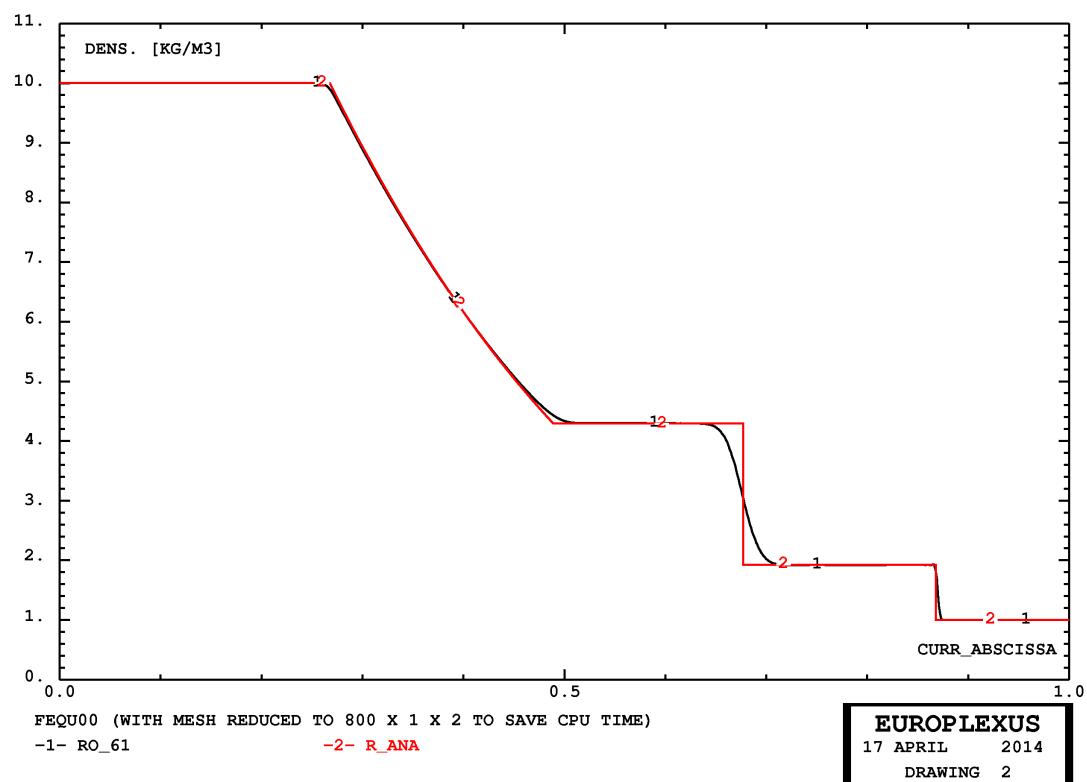


Figure 9 - Density in case FEQU00

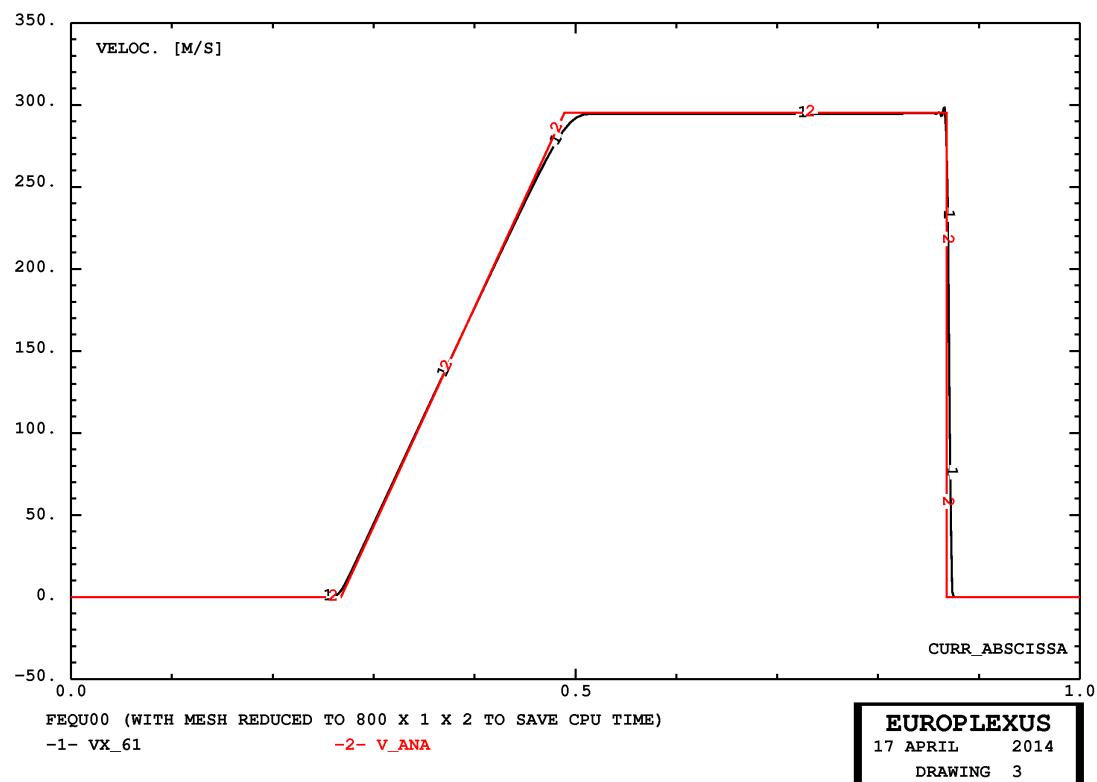


Figure 10 - Velocity in case FEQU00

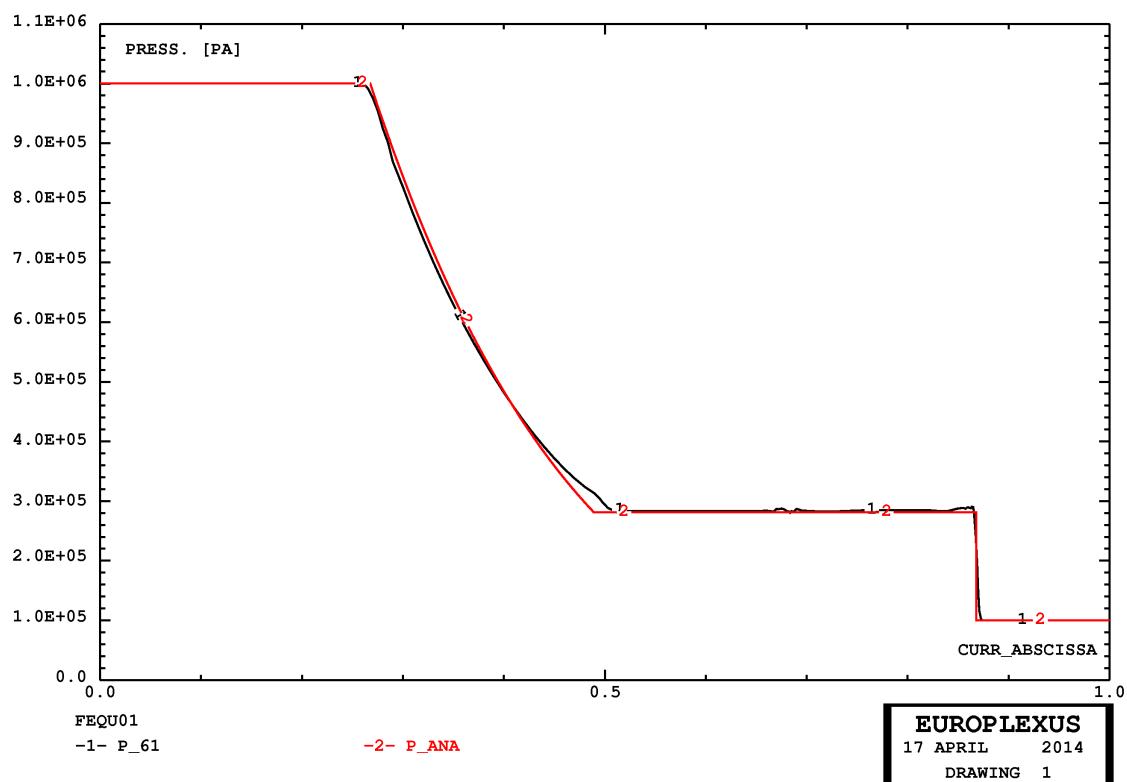


Figure 11 - Pressure in case FEQU01

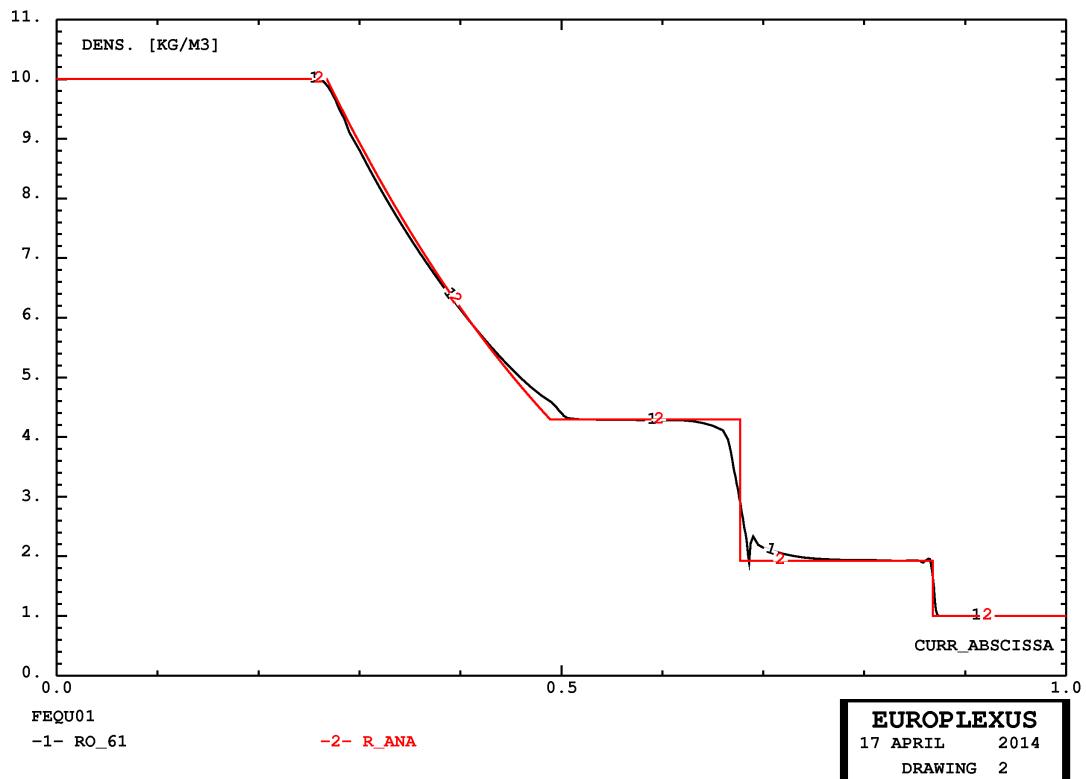


Figure 12 - Density in case FEQU01

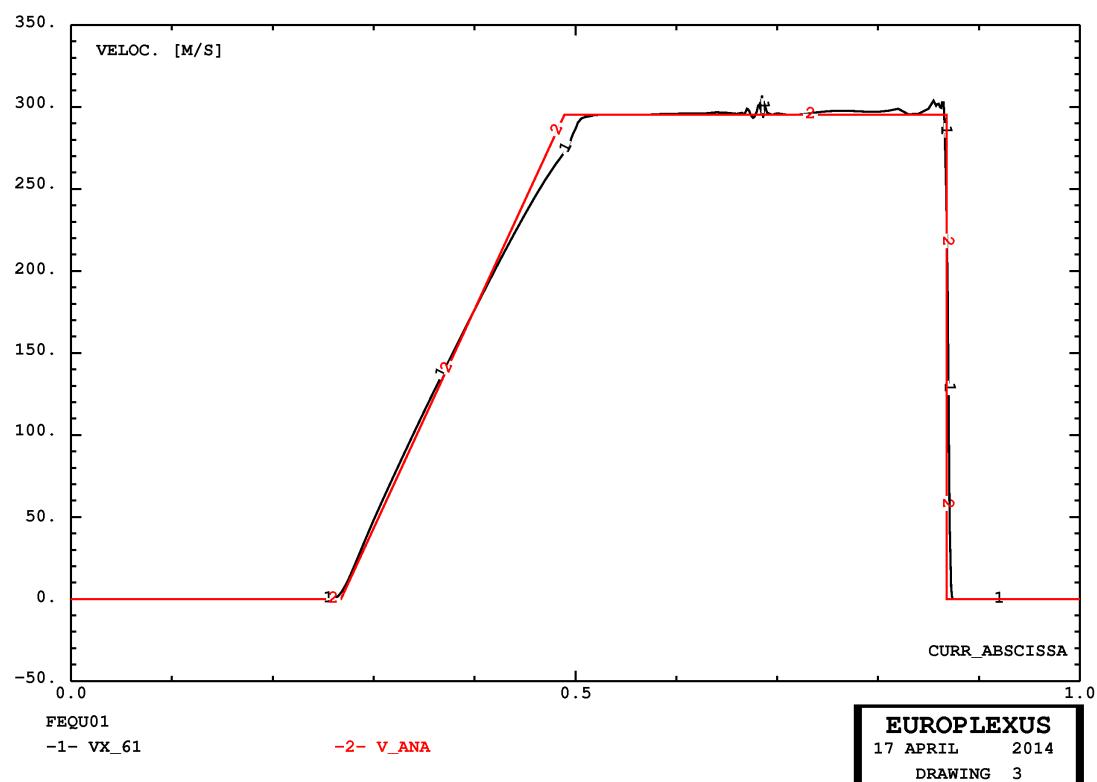


Figure 13 - Velocity in case FEQU01

## 4. Numerical examples in 3D

We present some numerical examples in order to test the algorithms described in the previous Sections.

### 4.1 Shock tube in 3D

The next example is a classical shock tube, similar to those considered in reference [2]. The adaptive mesh refinement is piloted by the WAVE directive.

First, reference solutions are obtained by means of a fine mesh of (non-adaptive) tetrahedra (TETR) or hexahedra (CUBE). Then, adaptive solutions with tetrahedra or hexahedra are obtained. All performed calculations are summarized in Table 2.

Case	Base Mesh	Notes	Steps	CPU [s]	Els*step
FET400	1,200 TETR	Non-adaptive fine mesh CSTA 0.5	237	0.7	285,600
FET401	1,200 TETR	WAVE 4 PLAN MAXL 3 CSTA 0.125	3,100	70.2	23,592,114
FEC800	100 CUBE	Non-adaptive fine mesh CSTA 0.5	119	0.2	12,000
FEC801	100 CUBE	WAVE 4 PLAN MAXL 3 CSTA 0.25	834	7.5	530,681

**Table 2 - Calculations for the shock tube problem with 2D Finite Elements**

#### **FET400**

This test uses a fine non-adaptive fluid mesh, of  $100 \times 12 = 1200$  tetrahedral fluid elements TETR. To obtain a solution with relatively few oscillations near the shock front, it is necessary to add some damping: OPTI AMOR QUAD 4 . 0 LINE 0 . 2. The solution is shown in Figures 14 (pressure), 15 (density) and 16 (velocity). This is taken as a reference for the subsequent adaptive solution.

#### **FET401**

This solution is adaptive and uses the same base fluid mesh as the previous case, and four WAVE directives to track the wavefronts, with a maximum refinement level MAXL 3. A stability coefficient of 0.125 (instead of 0.5 like in the reference case) is needed to ensure stability. The solution is shown in Figures 17 (pressure), 18 (density) and 19 (velocity) and is in reasonable agreement with the reference.

### **FEC800**

This test uses a non-adaptive fluid mesh, of 100 hexahedral fluid elements CUBE. To obtain a solution with relatively few oscillations near the shock front, it is necessary to add some damping: OPTI AMOR QUAD 4 . 0 LINE 0 . 2. The solution is shown in Figures 20 (pressure), 21 (density) and 22 (velocity). This is taken as a reference for the subsequent adaptive solution.

### **FEC801**

This solution is adaptive and uses the same base fluid mesh as the previous case, and four WAVE directives to track the wavefronts, with a maximum refinement level MAXL 3. A stability coefficient of 0.25 (instead of 0.5 like in the reference case) is needed to ensure stability. The solution is shown in Figures 23 (pressure), 24 (density) and 25 (velocity) and is in reasonable agreement with the reference.

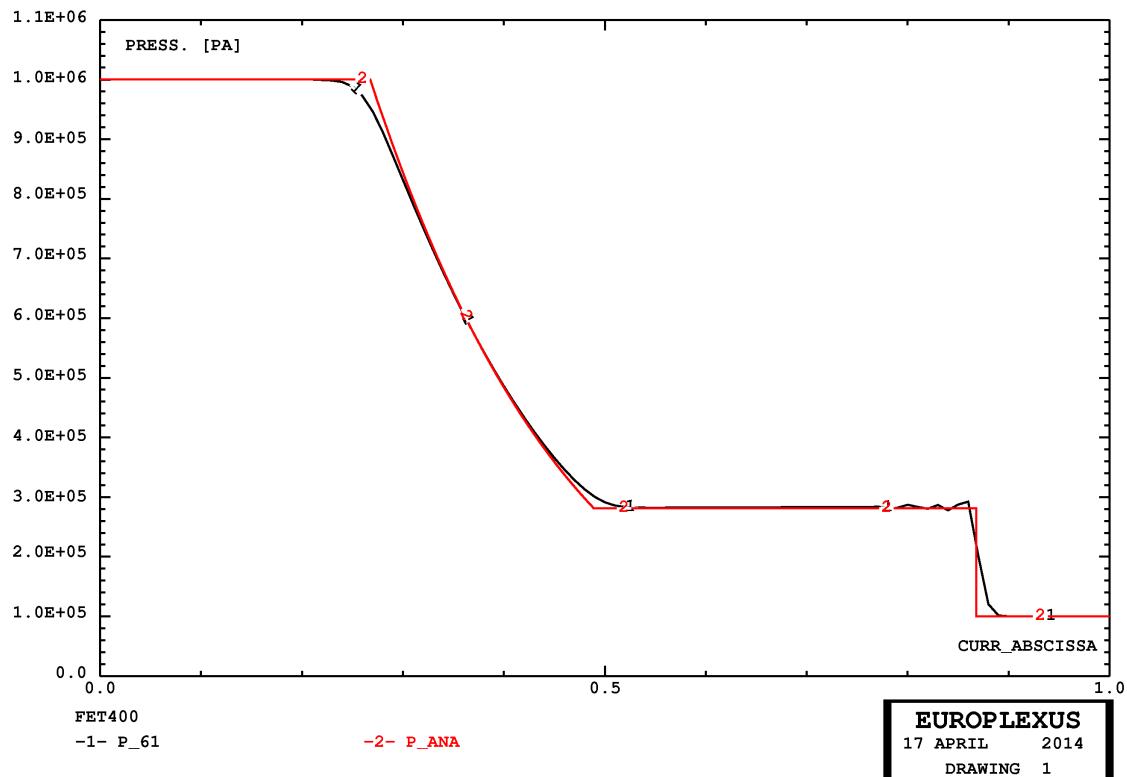


Figure 14 - Pressure in case FET400

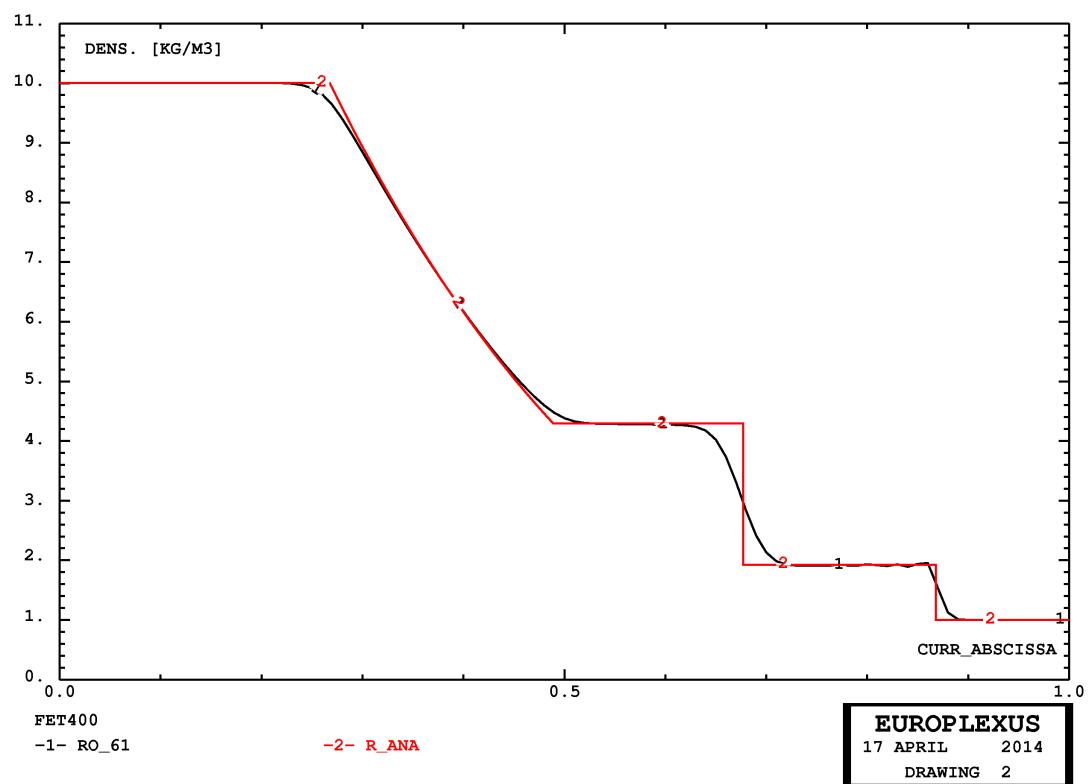


Figure 15 - Density in case FET400

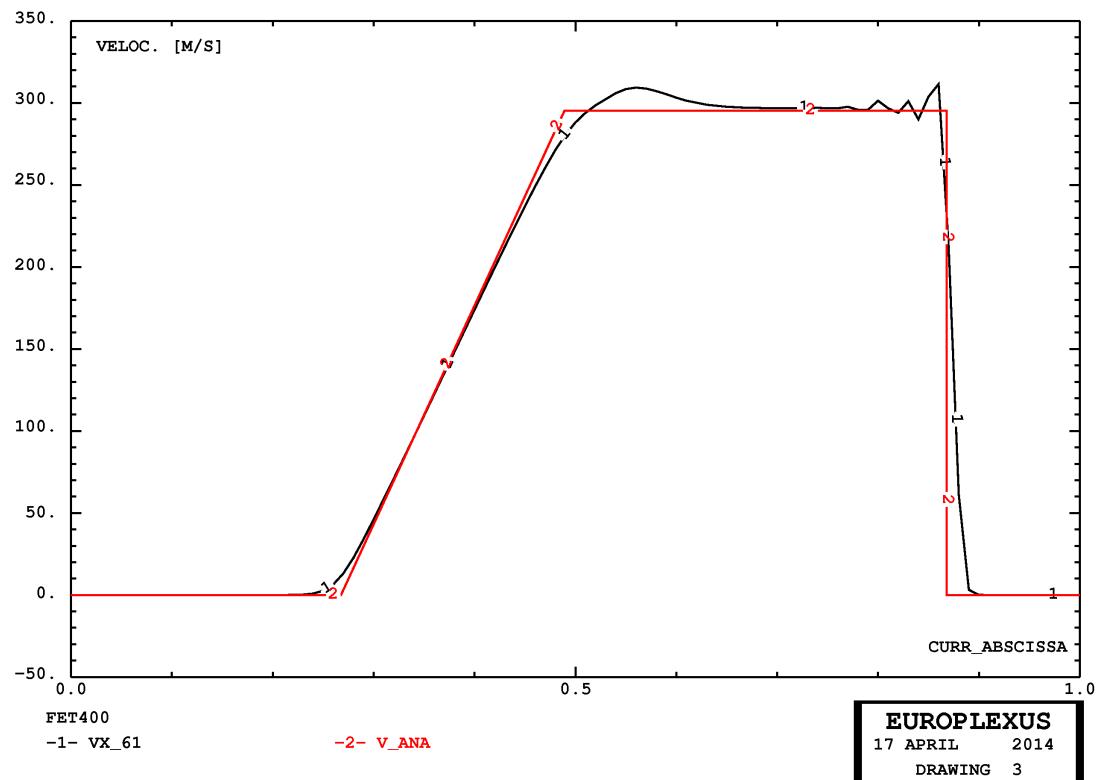


Figure 16 - Velocity in case FET400

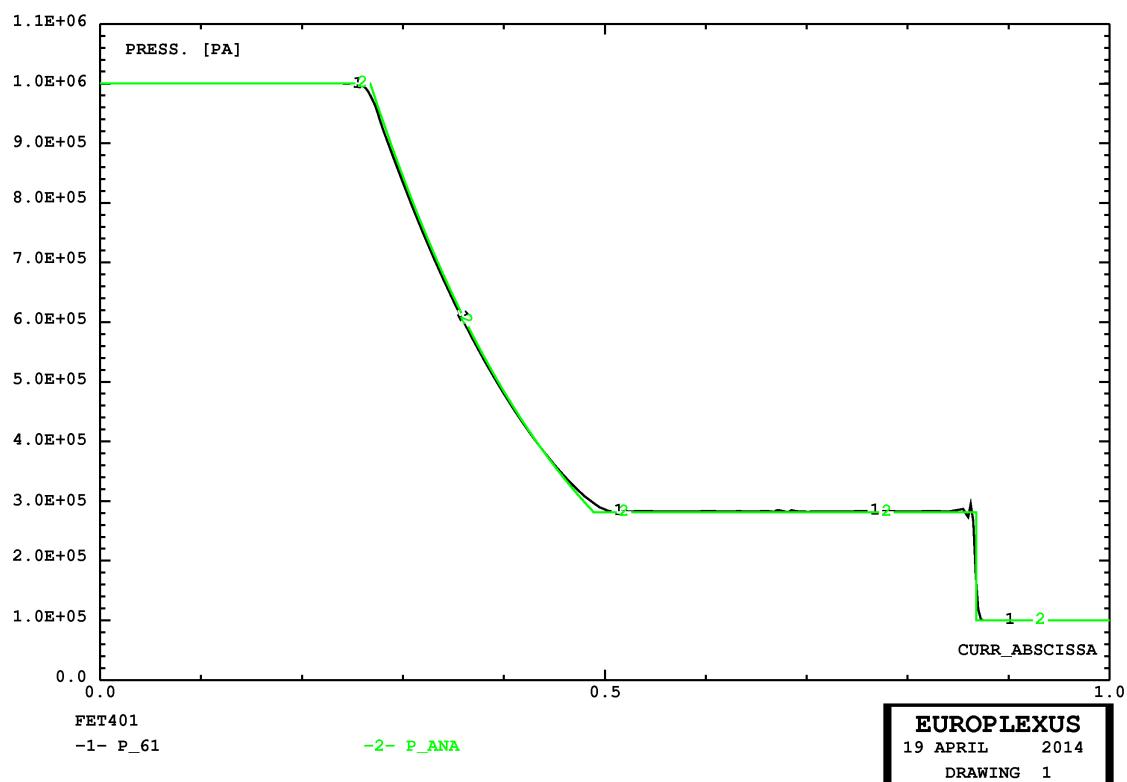


Figure 17 - Pressure in case FET401

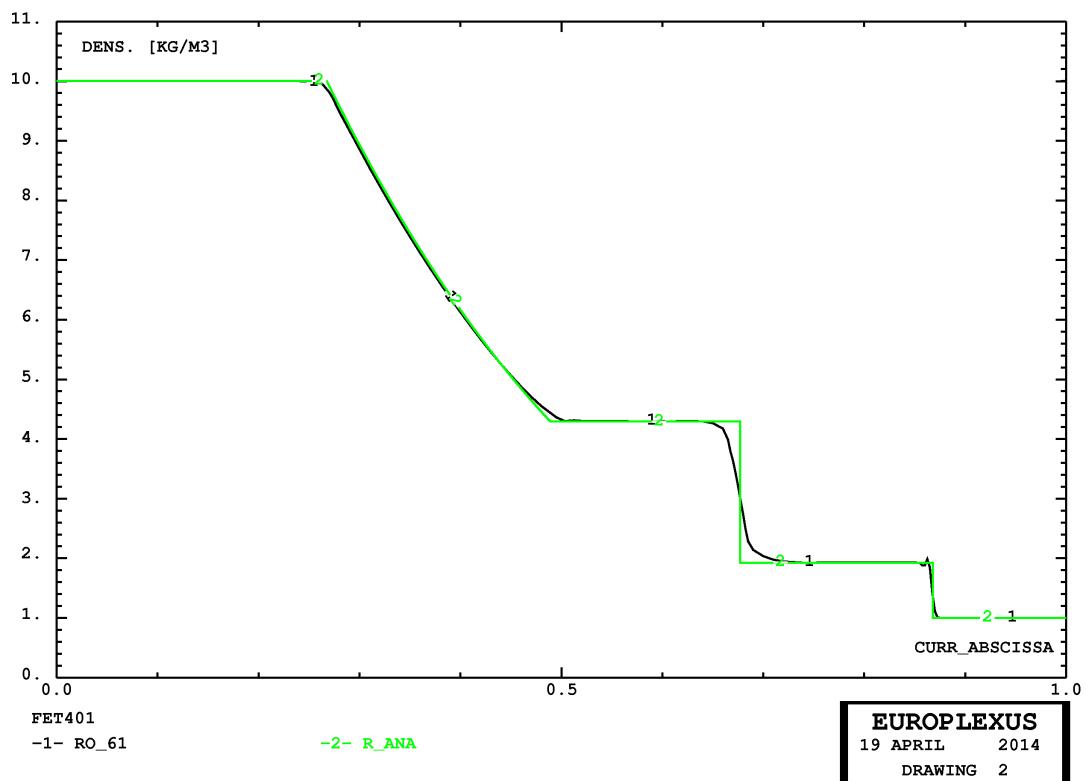


Figure 18 - Density in case FET401

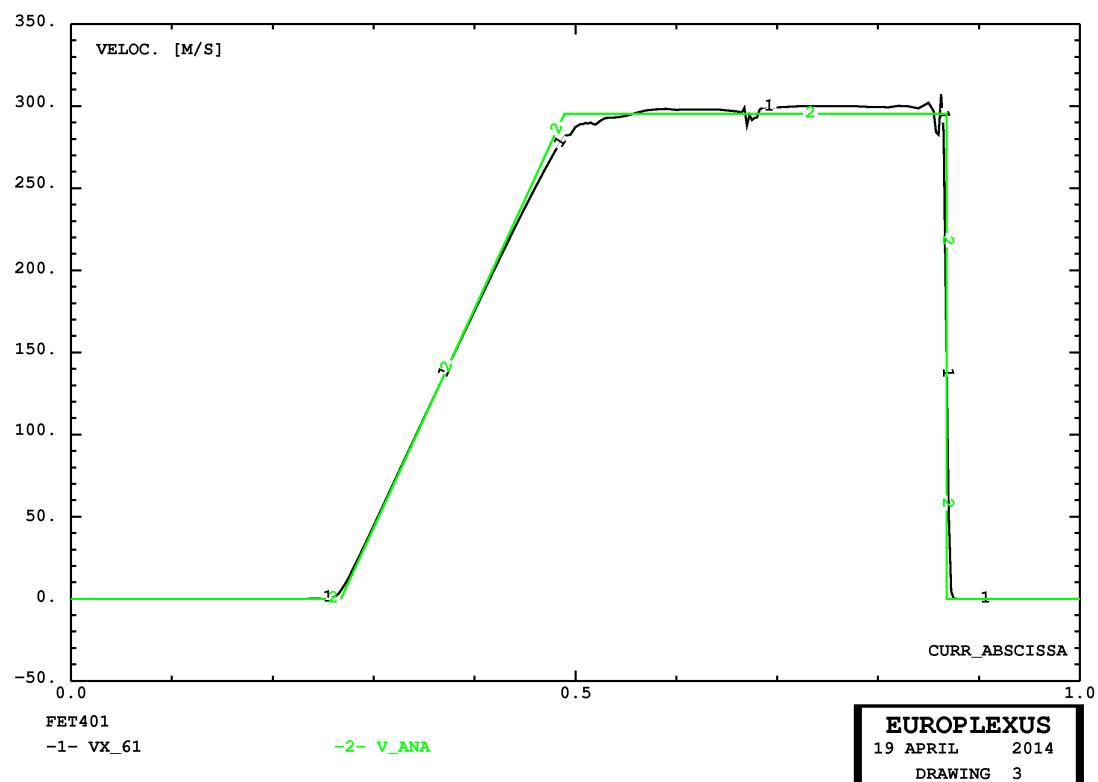


Figure 19 - Velocity in case FET401

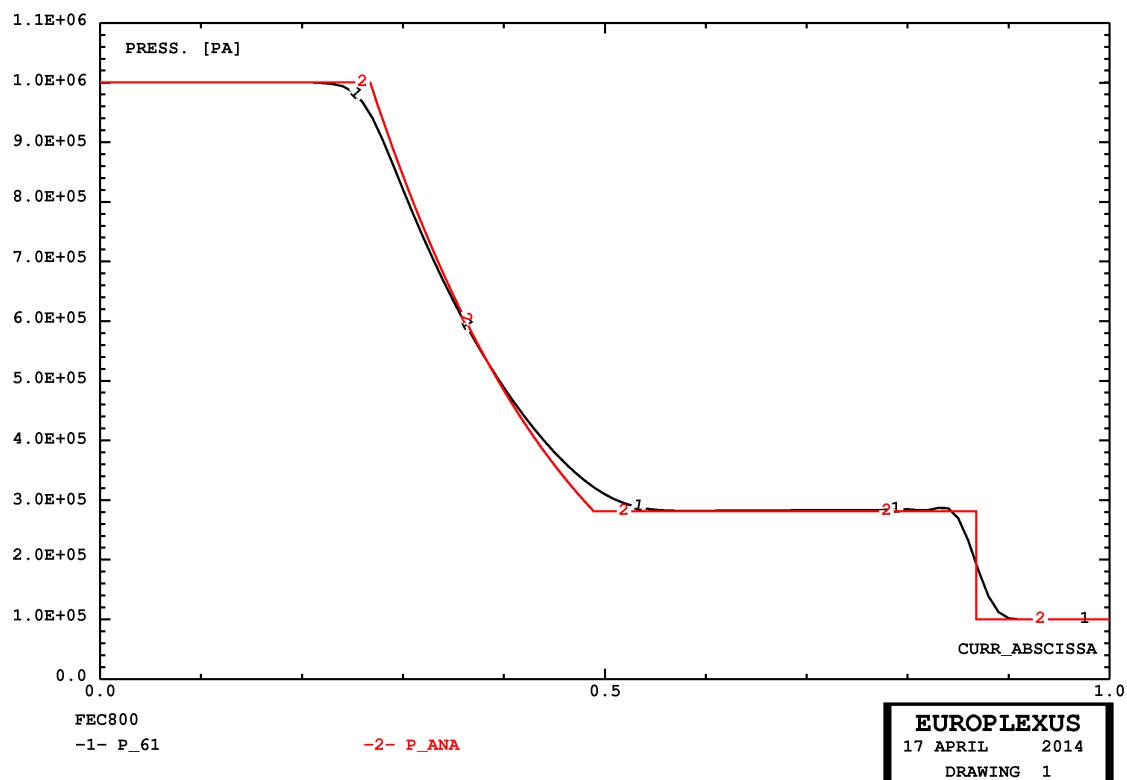


Figure 20 - Pressure in case FEC800

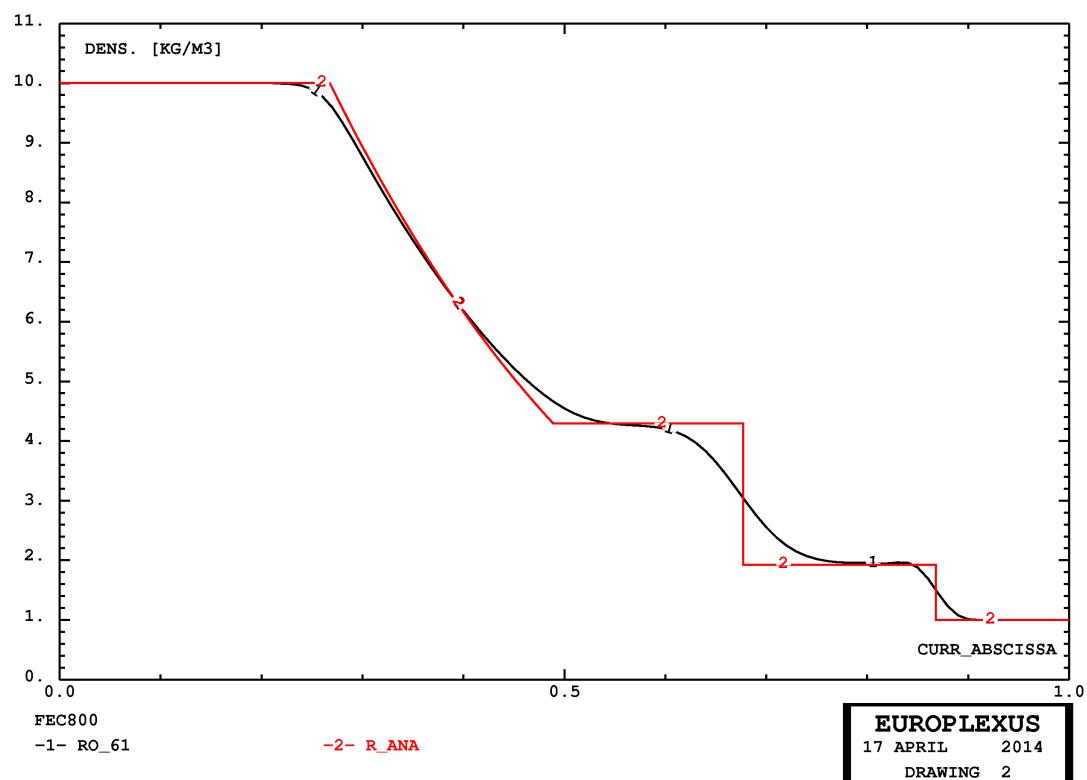


Figure 21 - Density in case FEC800

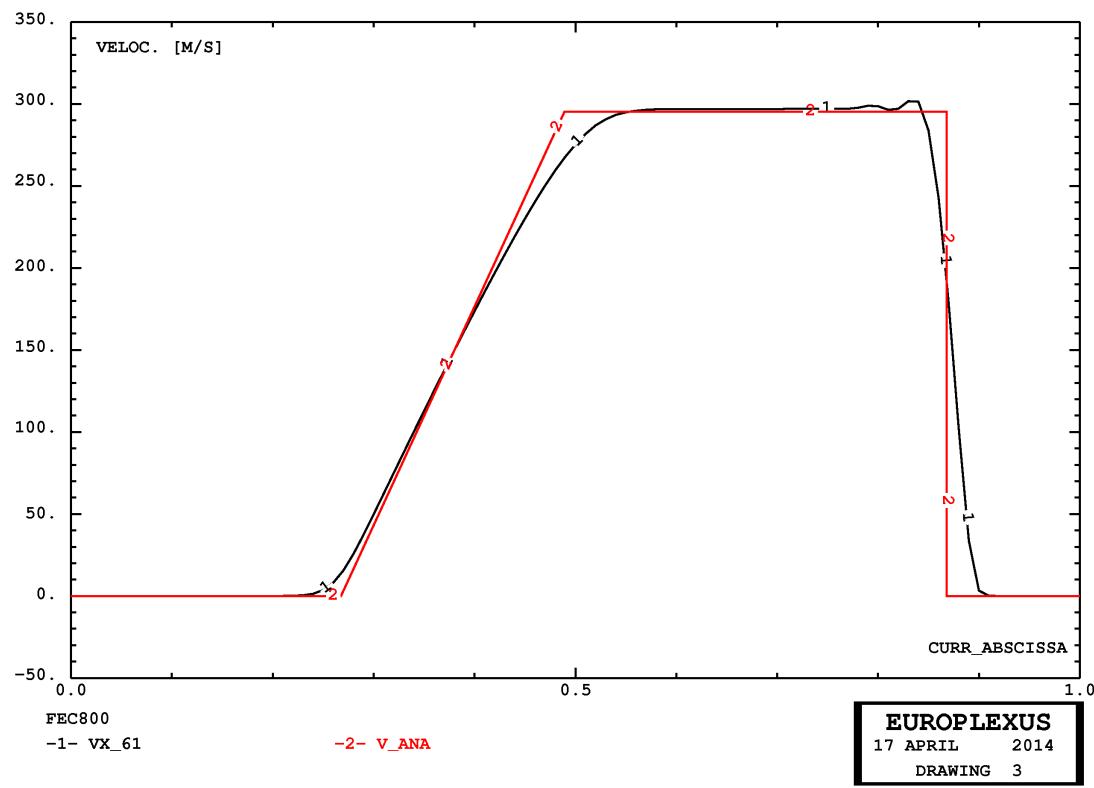


Figure 22 - Velocity in case FEC800

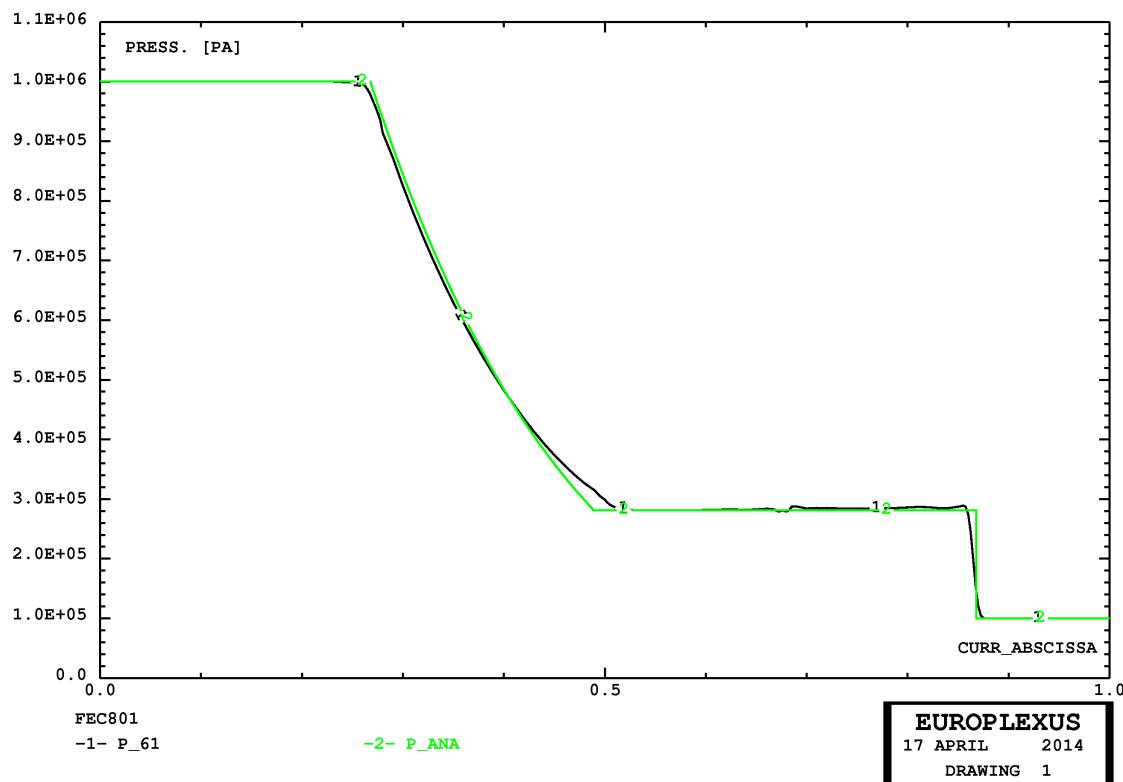


Figure 23 - Pressure in case FEC801

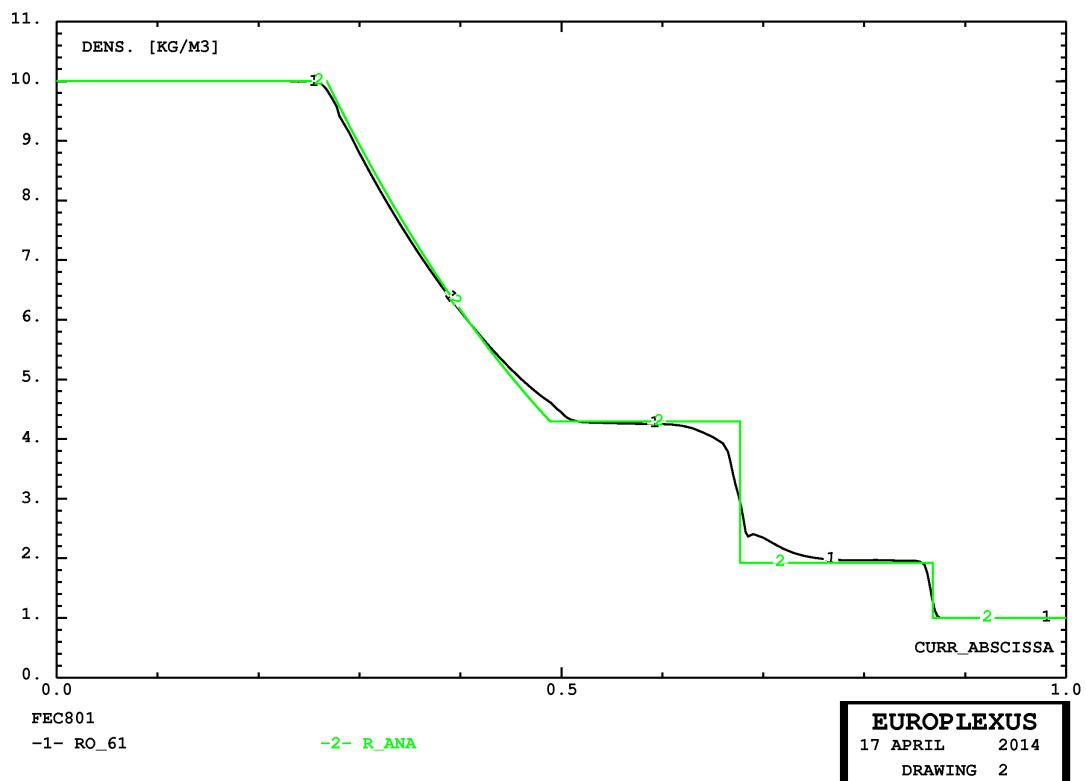


Figure 24 - Density in case FEC801

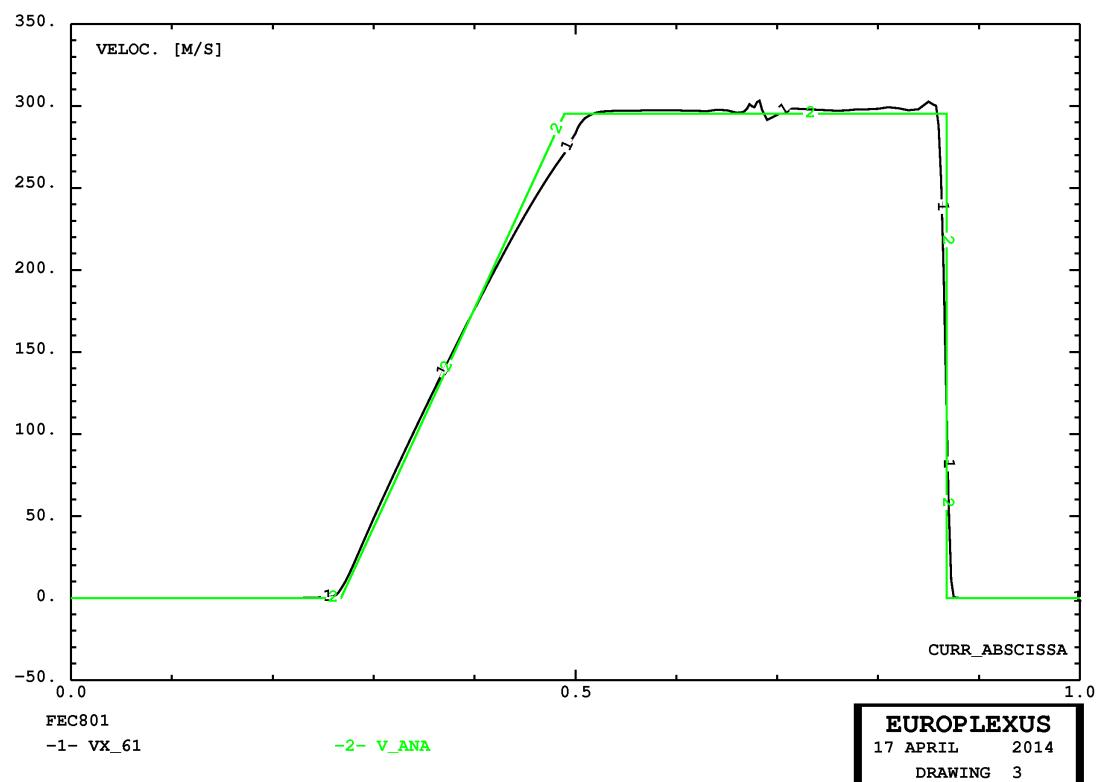


Figure 25 - Velocity in case FEC801

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Structure Interaction in EUROPLEXUS”, Technical Note, in publication, 2014.

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# Appendix

## Sample input files

This Section contains, in alphabetical file order, the listings of all input files related to the examples which were proposed in the previous Sections.

### fec800.dgibi

```
opti echo 1;
opti dime 3 elem cub8;
opti titr 'FEC800';
opti sauv form 'fec800.msh';
opti trac psc ftra 'fec800_mesh.ps';
p0 = 0 0 0;
dd = 0.01;
n = 100;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
bar = base volu n tran ((n*dd) 0 0);
mesh = bar;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;
```

### fec800.epx

```
FEC800
ECHO
!CONV win
CAST mesh
EULE TRID
GROM CUBE bar TERM
COMP GROU 4 'bar1' LECT 1 PAS 1 50 TERM
    'bar2' LECT 51 PAS 1 100 TERM
    'ea' LECT 26 TERM
    'eb' LECT 75 TERM
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
    X2 1 Y2 0 Z2 0 TOL 1.E-4
    'bas1' LECT bar TERM COND X LT 0.0001
    'bas2' LECT bar TERM COND X GT 0.9999
    'na' LECT bar TERM COND NEAR POIN 0.25 0 0
    'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
    VERT LECT bar2 TERM
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
    LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
    LECT bar2 TERM
LINE COUP BLOQ 1 LECT bas1 bas2 TERM
    BLOQ 23 LECT bar TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
    FICH ALIC TEMP FREQ 1
        POIN LECT na nb TERM
        ELEM LECT ea eb TERM
        FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.5
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR ROUG
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR ROUG
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR ROUG
LIST 65 AXES 1.0 'VELOC. [M/S]'
=====
QUAL ECRO COMP 1 LECT ea TERM REFE 9.78687E+5 TOLE 2.E-2
    ECRO COMP 1 LECT eb TERM REFE 2.83485E+5 TOLE 2.E-2
    ECRO COMP 2 LECT ea TERM REFE 9.85733E+0 TOLE 2.E-2
    ECRO COMP 2 LECT eb TERM REFE 2.04129E+0 TOLE 2.E-2
=====
SUIT
Post-treatment (time curves from alice temps file)
```

```
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fec800t.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_lea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'
COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'
COLO NOIR NOIR
LIST 1 4 AXES 1.0 'PRESS. [PA]'
LIST 2 5 AXES 1.0 'DENS. [KG/M3]'
LIST 3 6 AXES 1.0 'VELOC. [M/S]'
```

```
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00001E-01
    Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
    VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
    RIGH 1.00000E+00 0.00000E+00 0.00000E+00
    UP 0.00000E+00 1.00000E+00 0.00000E+00
    FOV 5.25000E+01
SCEN GEOM NAVI FREE
    ! LINE HEOU
        ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
        TEXT ISCA
        COLO PAPE
    SLER CAM1 1 NFRA 1
    TRAC OFFS SIZE 1400 400 FICH BMP REND
    SCEN GEOM NAVI FREE
    ! LINE HEOU
        ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
        TEXT ISCA
        COLO PAPE
    SLER CAM1 1 NFRA 1
    TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
FIN
```

### fec801.dgibi

```
opti echo 1;
opti dime 3 elem cub8;
opti titr 'FEC801';
opti sauv form 'fec801.msh';
opti trac psc ftra 'fec801_mesh.ps';
p0 = 0 0;
dd = 0.01;
n = 100;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
bar = base volu n tran ((n*dd) 0 0);
mesh = bar;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;
```

### fec801.epx

```
FEC801
ECHO
!CONV win
CAST mesh
EULE TRID
DIME
    ADAP NPOI 1045 CUBE 712 ENDA
TERM
GROM CUBE bar TERM
COMP GROU 4 'bar1' LECT 1 PAS 1 50 TERM
    'bar2' LECT 51 PAS 1 100 TERM
    'ea' LECT 26 TERM
    'eb' LECT 75 TERM
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
    X2 1 Y2 0 Z2 0 TOL 1.E-4
    'bas1' LECT bar TERM COND X LT 0.0001
    'bas2' LECT bar TERM COND X GT 0.9999
    'na' LECT bar TERM COND NEAR POIN 0.25 0 0
    'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
    VERT LECT bar2 TERM
WAVE 4 PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 613.568783589856 ! shock wave
    MAXL 3 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 295.278289836459 ! c.d. wave
    MAXL 3 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 Z 0 NX -1 NY 0 NZ 0 TO 0 C 18.2004723251679 ! r.wave (ri.)
    MAXL 3 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 Z 0 NX -1 NY 0 NZ 0 TO 0 C 387.298334620742 ! r. wav (le.)
    MAXL 3 H1 0.015 H2 0.05
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
    LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
    LECT bar2_cube TERM
LINK COUP BLOQ 1 LECT bas1 bas2 TERM
```

```

BLOQ 23 LECT bar TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
  FICH ALIC TEMP FREQ 1
    POIN LECT na nb TERM
    ELEM LECT ea eb TERM
    FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.25
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'

COLO NOIR VERT
LIST 61 AXES 1.0 'PRESS. [PA]'

TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'

COLO NOIR VERT
LIST 62 AXES 1.0 'DENS. [KG/M3]'

TRAC 65 75 AXES 1.0 'VELOC. [M/S]'

COLO NOIR VERT
LIST 65 AXES 1.0 'VELOC. [M/S]'

*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.97352E+5 TOLE 2.E-2
  ECRO COMP 1 LECT eb TERM REFE 2.83845E+5 TOLE 2.E-2
  ECRO COMP 2 LECT ea TERM REFE 9.98273E+0 TOLE 2.E-2
  ECRO COMP 2 LECT eb TERM REFE 2.02291E+0 TOLE 2.E-2
=====
SUIT
Post-treatment (time curves from alice temps file)
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fec80it.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_ea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'

COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'

COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'

COLO NOIR NOIR
LIST 1 4 AXES 1.0 'PRESS. [PA]'

LIST 2 5 AXES 1.0 'DENS. [KG/M3]'

LIST 3 6 AXES 1.0 'VELOC. [M/S]'

=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
!   Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 5.25000E+01
SCEN GEOM NAVI FREE
!   LINE HEOU
  ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
  TEXT ISCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
SCEN GEOM NAVI FREE
!   LINE HEOU
  ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
  TEXT ISCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
FIN

```

**fequ00.dgibi**

```

opti echo 0;
opti donn 'pxordpoi.proc';
opti echo 1;
opti dime 2 elem qua4;
opti sauw form 'fequ00.msh';
opti trac psc ftra 'fequ00_mesh.ps';
p0 = 0 ;
p0p = p0 plus (0 0.00125);
pmid = 0.5 ;
p1 = 1 ;
pip = p1 plus (0 0.00125);
pa = 0.25 0;
pb = 0.75 0;
tol = 1.E-5;
n = 800;

```

```

n2 = n / 2;
n4 = n2 / 2;
c11 = pa d n4 pa;
c12 = pa d n4 pmid;
c1 = c11 et c12;
c21 = pmid d n4 pb;
c22 = pb d n4 p1;
c2 = c21 et c22;
bar11 = c11 tran 1 (0 0.00125);
bar12 = c12 tran 1 (0 0.00125);
bar1 = bar11 et bar12;
bar21 = c21 tran 1 (0 0.00125);
bar22 = c22 tran 1 (0 0.00125);
bar2 = bar21 et bar22;
bar = bar1 et bar2;
elin tol (bar et p0p et plp et pa et pb);
ea = barl elem cont pa;
eb = bar2 elem cont pb;
xax = chan 'PO1' (cl et c2);
xaxo = pxordpoi xax p0;
mesh = bar et ea et eb et xaxo;
tass mesh;
sauv form mesh;
trac qual mesh;
trac ((cont mesh) et ea et eb);
fin;

```

**fequ00.epx**

```

FEQU00 (with mesh reduced to 800 x 1 x 2 to save CPU time)
ECHO
!CONV win
CAST mesh
EULU DPLA
GEON CAR1 bar TERM
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
  LECT bar1 TERM
  GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
  LECT bar2 TERM
LINK COUP BLOQ 1 LECT p0 p0p pl plp TERM
  BLOQ 2 LECT bar TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
  FICH ALIC TEMP FREQ 1
    POIN LECT pa pmid pb TERM
    ELEM LECT ea eb TERM
    FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.5
log 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
!PERF 'fequ00.pun'
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'

COLO NOIR ROUG
LIST 61 AXES 1.0 'PRESS. [PA]'

TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'

COLO NOIR ROUG
LIST 62 AXES 1.0 'DENS. [KG/M3]'

TRAC 65 75 AXES 1.0 'VELOC. [M/S]'

COLO NOIR ROUG
LIST 65 AXES 1.0 'VELOC. [M/S]'

*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.99996E+5 TOLE 2.E-2
  ECRO COMP 1 LECT eb TERM REFE 2.82943E+5 TOLE 2.E-2
  ECRO COMP 2 LECT ea TERM REFE 9.99997E+0 TOLE 2.E-2
  ECRO COMP 2 LECT eb TERM REFE 1.92000E+0 TOLE 2.E-2
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
!   Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 5.25000E+01
SCEN GEOM NAVI FREE
LINE HEOU
  ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
  TEXT ISCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
SCEN GEOM NAVI FREE
LINE HEOU
  ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
  TEXT ISCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
FIN

```

## fequ01.epx

```

FEQU01
ECHO
!CONV win
EULE DPLA
DIME
ADAP NPOI 1000 CAR1 2000 ENDA
TERM
GROM LIBR Poin 202 CAR1 100 TERM
0.00 0.00 0.01 0.00 0.02 0.00 0.03 0.00 0.04 0.00 0.05 0.00
0.06 0.00 0.07 0.00 0.08 0.00 0.09 0.00 0.10 0.00
0.11 0.00 0.12 0.00 0.13 0.00 0.14 0.00 0.15 0.00
0.16 0.00 0.17 0.00 0.18 0.00 0.19 0.00 0.20 0.00
0.21 0.00 0.22 0.00 0.23 0.00 0.24 0.00 0.25 0.00
0.26 0.00 0.27 0.00 0.28 0.00 0.29 0.00 0.30 0.00
0.31 0.00 0.32 0.00 0.33 0.00 0.34 0.00 0.35 0.00
0.36 0.00 0.37 0.00 0.38 0.00 0.39 0.00 0.40 0.00
0.41 0.00 0.42 0.00 0.43 0.00 0.44 0.00 0.45 0.00
0.46 0.00 0.47 0.00 0.48 0.00 0.49 0.00 0.50 0.00
0.51 0.00 0.52 0.00 0.53 0.00 0.54 0.00 0.55 0.00
0.56 0.00 0.57 0.00 0.58 0.00 0.59 0.00 0.60 0.00
0.61 0.00 0.62 0.00 0.63 0.00 0.64 0.00 0.65 0.00
0.66 0.00 0.67 0.00 0.68 0.00 0.69 0.00 0.70 0.00
0.71 0.00 0.72 0.00 0.73 0.00 0.74 0.00 0.75 0.00
0.76 0.00 0.77 0.00 0.78 0.00 0.79 0.00 0.80 0.00
0.81 0.00 0.82 0.00 0.83 0.00 0.84 0.00 0.85 0.00
0.86 0.00 0.87 0.00 0.88 0.00 0.89 0.00 0.90 0.00
0.91 0.00 0.92 0.00 0.93 0.00 0.94 0.00 0.95 0.00
0.96 0.00 0.97 0.00 0.98 0.00 0.99 0.00 1.00 0.00
0.00 0.01 0.01 0.01 0.02 0.01 0.03 0.01 0.04 0.01 0.05 0.01
0.06 0.01 0.07 0.01 0.08 0.01 0.09 0.01 0.10 0.01
0.11 0.00 0.12 0.01 0.13 0.01 0.14 0.01 0.15 0.01
0.16 0.01 0.17 0.01 0.18 0.01 0.19 0.01 0.20 0.01
0.21 0.01 0.22 0.01 0.23 0.01 0.24 0.01 0.25 0.01
0.26 0.01 0.27 0.01 0.28 0.01 0.29 0.01 0.30 0.01
0.31 0.01 0.32 0.01 0.33 0.01 0.34 0.01 0.35 0.01
0.36 0.01 0.37 0.01 0.38 0.01 0.39 0.01 0.40 0.01
0.41 0.01 0.42 0.01 0.43 0.01 0.44 0.01 0.45 0.01
0.46 0.01 0.47 0.01 0.48 0.01 0.49 0.01 0.50 0.01
0.51 0.01 0.52 0.01 0.53 0.01 0.54 0.01 0.55 0.01
0.56 0.01 0.57 0.01 0.58 0.01 0.59 0.01 0.60 0.01
0.61 0.01 0.62 0.01 0.63 0.01 0.64 0.01 0.65 0.01
0.66 0.01 0.67 0.01 0.68 0.01 0.69 0.01 0.70 0.01
0.71 0.01 0.72 0.01 0.73 0.01 0.74 0.01 0.75 0.01
0.76 0.01 0.77 0.01 0.78 0.01 0.79 0.01 0.80 0.01
0.81 0.01 0.82 0.01 0.83 0.01 0.84 0.01 0.85 0.01
0.86 0.01 0.87 0.01 0.88 0.01 0.89 0.01 0.90 0.01
0.91 0.01 0.92 0.01 0.93 0.01 0.94 0.01 0.95 0.01
0.96 0.01 0.97 0.01 0.98 0.01 0.99 0.01 1.00 0.01
1 2 103 102
2 3 104 103
3 4 105 104
4 5 106 105
5 6 107 106
6 7 108 107
7 8 109 108
8 9 110 109
9 10 111 110
10 11 112 111
11 12 113 112
12 13 114 113
13 14 115 114
14 15 116 115
15 16 117 116
16 17 118 117
17 18 119 118
18 19 120 119
19 20 121 120
20 21 122 121
21 22 123 122
22 23 124 123
23 24 125 124
24 25 126 125
25 26 127 126
26 27 128 127
27 28 129 128
28 29 130 129
29 30 131 130
30 31 132 131
31 32 133 132
32 33 134 133
33 34 135 134
34 35 136 135
35 36 137 136
36 37 138 137
37 38 139 138
38 39 140 139
39 40 141 140
40 41 142 141
41 42 143 142
42 43 144 143
43 44 145 144
44 45 146 145
45 46 147 146
46 47 148 147
47 48 149 148
48 49 150 149
49 50 151 150
50 51 152 151
51 52 153 152
52 53 154 153
53 54 155 154
54 55 156 155
55 56 157 156
56 57 158 157
57 58 159 158
58 59 160 159
59 60 161 160
60 61 162 161
61 62 163 162
62 63 164 163
63 64 165 164
64 65 166 165
65 66 167 166
66 67 168 167

67 68 169 168
68 69 170 169
69 70 171 170
70 71 172 171
71 72 173 172
72 73 174 173
73 74 175 174
74 75 176 175
75 76 177 176
76 77 178 177
77 78 179 178
78 79 180 179
79 80 181 180
80 81 182 181
81 82 183 182
82 83 184 183
83 84 185 184
84 85 186 185
85 86 187 186
86 87 188 187
87 88 189 188
88 89 190 189
89 90 191 190
90 91 192 191
91 92 193 192
92 93 194 193
93 94 195 194
94 95 196 195
95 96 197 196
96 97 198 197
97 98 199 198
98 99 200 199
99 100 201 200
100 101 202 201
COMP GROU 5 'bar1' LECT 1 PAS 1 50 TERM
          'bar2' LECT 51 PAS 1 100 TERM
          'bar' LECT bar1 bar2 TERM
          'ea' LECT 26 TERM
          'eb' LECT 76 TERM
NGRO 7 'p0' LECT 1 TERM
          'pop' LECT 102 TERM
          'p1' LECT 101 TERM
          'plp' LECT 202 TERM
          'pa' LECT 26 TERM
          'pmid' LECT 51 TERM
          'pb' LECT 76 TERM
WAVE 4 PLAN X 0.5 Y 0 NX 1 NY 0 TO 0 C 613.568783589856 ! shock wave
          MAXL 4 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 NX 1 NY 0 TO 0 C 295.278289836459 ! c.d. wave
          MAXL 4 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 NX 1 NY 0 TO 0 C 18.2004723251679 ! r.wave (right)
          MAXL 4 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 NX 1 NY 0 TO 0 C 387.298334620742 ! r. wave (left)
          MAXL 4 H1 0.015 H2 0.05
MATE GAZP RO 10 GAMM 1.5 PINI 1.E5 PREF 1.E5
          LECT bar1 TERM
GAZP 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
          LECT bar2_cax1 TERM
LINK COUP BLOQ 1 LECT p0 pop pl plp TERM
          BLOQ 2 LECT bar TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
          FICH ALIC TEMP FREQ 1
          POIN LECT pa pmid pb TERM
          ELEM LECT ea eb TERM
          FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
csta 0.25
log 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
COMP NGRO 1 'xaxo' LECT 1 PAS 1 101 TERM
SORT GRAP
!PERF 'fequ01.pun'
AXTE 1.0 'Time [s]'
*
* Attention: le SUPP /LECT/ est **mandatoire** dans les directives ci-dessous
* car sinon au risque de traiter les noeuds de l'element "bidon" comme
* faisant partie de l'abscisse curviligne (qui doit etre basee seulement
* sur les TRIA)
* En general, il est toujours une bonne idee de specifier le SUPPORT,
* s'il y a des doutes ...
*
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
          SUPP LECT bar TERM
          ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
          SUPP LECT bar TERM
          ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
          SUPP LECT bar TERM
          VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
          TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
          TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
          TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA] '
COLO NOIR ROUG
LIST 61 AXES 1.0 'PRESS. [PA] '
TRAC 62 72 AXES 1.0 'DENS. [KG/M3] '
COLO NOIR ROUG
LIST 62 AXES 1.0 'DENS. [KG/M3] '
TRAC 65 75 AXES 1.0 'VELOC. [M/S] '
COLO NOIR ROUG
LIST 65 AXES 1.0 'VELOC. [M/S] '
*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.99483E+5 TOLE 2.E-2
          ECRO COMP 1 LECT eb TERM REFE 2.84565E+5 TOLE 2.E-2
          ECRO COMP 2 LECT ea TERM REFE 9.99666E+0 TOLE 2.E-2
          ECRO COMP 2 LECT eb TERM REFE 1.95743E+0 TOLE 2.E-2
=====
SUIT

```

```

Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 5.25000E+01
SCEN GEOM NAVI FREE
LINE HEOU
ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
SUPP LECT bar TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP OBJE LECT bar TERM REND
SCEN GEOM NAVI FREE
LINE HEOU
ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
SUPP LECT bar TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP OBJE LECT bar TERM REND
ENDPLAY
=====
FIN

```

**fet400.dgibi**

```

opti echo 1;
opti donn 'pxhex2te.proc';
opti dime 3 elem cub8;
opti titr 'FET400';
opti sauv form 'fet400.msh';
opti trac psc ftra 'fet400_mesh.ps';
p0 = 0 0 0;
dd = 0.01;
n = 100;
tol = 0.0001;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
bar8 = base volu n tran ((n*dd) 0 0);
i = 0;
repe loop1 (nbrel bar8);
i = i + 1;
cubei = bar8 elem i;
tt = pxhex2te cubei;
si (ega i 1);
bar = tt;
sinon;
bar = bar et tt;
finsi;
fin loop1;
elim tol bar;
mesh = bar;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;

```

**fet400.epx**

```

FET400
ECHO
!CONV win
CAST mesh
EULE TRID
GEOM TETR bar TERM
COMP GROU 4 'bar1' LECT bar TERM COND XB LT 0.5
'bar2' LECT bar DIFF bar1 TERM
'ea' LECT bar TERM COND NEAR POIN 0.25 0 0
'eb' LECT bar TERM COND NEAR POIN 0.75 0 0
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
'bas1' LECT bar TERM COND X LT 0.0001
'bas2' LECT bar TERM COND X GT 0.9999
'na' LECT bar TERM COND NEAR POIN 0.25 0 0
'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
VERT LECT bar2 TERM
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
LECT bar2 TERM
LINE COUP BLOQ 1 LECT bas1 bas2 TERM
BLOQ 23 LECT bar TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO VFCC TFRE 0.3E-3
FICH ALIC TEMP FREQ 1
POIN LECT na nb TERM
ELEM LECT ea eb TERM
FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.5
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP

```

**fet401.dgibi**

```

opti echo 1;
opti donn 'pxhex2te.proc';
opti dime 3 elem cub8;
opti titr 'FET401';
opti sauv form 'fet401.msh';
opti trac psc ftra 'fet401_mesh.ps';
p0 = 0 0 0;
dd = 0.01;
n = 100;
tol = 0.0001;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
bar8 = base volu n tran ((n*dd) 0 0);
i = 0;
repe loop1 (nbrel bar8);
i = i + 1;
cubei = bar8 elem i;
tt = pxhex2te cubei;
si (ega i 1);
bar = tt;
sinon;
bar = bar et tt;
finsi;
fin loop1;
elim tol bar;
barsur = chan poi1 (enve bar);

```

```

mesh = bar et barsur;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;

```

## fet401.epx

```

FET401
ECHO
!CONV win
CAST mesh
EULE TRID
DIME
ADAP NPOI 1648 TETR 7872 ENDA
TERM
GROM TETR bar TERM
COMP GROU 4 'bar1' LECT bar TERM COND XB LT 0.5
  'bar2' LECT bar DIFF bar1 TERM
    'ea' LECT bar TERM COND NEAR POIN 0.25 0 0
    'eb' LECT bar TERM COND NEAR POIN 0.75 0 0
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
  X2 1 Y2 0 Z2 0 TOL 1.E-4
  'bas1' LECT bar TERM COND X LT 0.0001
  'bas2' LECT bar TERM COND X GT 0.9999
  'na' LECT bar TERM COND NEAR POIN 0.25 0 0
  'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
  VERT LECT bar2 TERM
WAVE 4 PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 613.568783589856 ! shock wave
  MAXL 3 H1 0.015 H2 0.05
  PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 295.278289836459 ! c.d. wave
  MAXL 3 H1 0.015 H2 0.05
  PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 18.2004723251679 ! r.wave (ri.)
  MAXL 3 H1 0.015 H2 0.05
  PLAN X 0.5 Y 0 Z 0 NX -1 NY 0 NZ 0 TO 0 C 387.298334620742 ! r. wav (le.)
  MAXL 3 H1 0.015 H2 0.05
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
  LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
  LECT bar2 _tetr TERM
LINK COUP BLOQ 1 LECT bas1 bas2 TERM
  BLOQ 23 LECT barsur TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
  FICH ALIC TEMP FREQ 1
    POIN LECT na nb TERM
    ELEM LECT ea eb TERM
    FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.125
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR VERT
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR VERT
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR VERT
LIST 65 AXES 1.0 'VELOC. [M/S]'
*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.99590E+5 TOLE 2.E-2
  ECRO COMP 1 LECT eb TERM REFE 2.82972E+5 TOLE 2.E-2
  ECRO COMP 2 LECT ea TERM REFE 9.99726E+0 TOLE 2.E-2
  ECRO COMP 2 LECT eb TERM REFE 1.92972E+0 TOLE 2.E-2
=====
SUIT
Post-treatment (time curves from alice temps file)
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fet401.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_ea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'
COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'
COLO NOIR NOIR
LIST 1 4 AXES 1.0 'PRESS. [PA]'
LIST 2 5 AXES 1.0 'DENS. [KG/M3]'
LIST 3 6 AXES 1.0 'VELOC. [M/S]'
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61

```

```

PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
  Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 5.25000E+01
SCEN GEOM NAVI FREE
!
```

```

LINE HEBOU
ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
TEXT ISCA
COLO PAPE

```

```

SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
SCEN GEOM NAVI FREE
!
```

```

LINE HEBOU
ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
TEXT ISCA
COLO PAPE

```

```

SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
```

```

FIN
```

## fet402.dgibi

```

opti echo 1;
opti donn 'pxhex2t2.proc';
opti dime 3 elem cub8;
opti titr 'FET402';
opti sauv form 'fet402.msh';
opti trac fscr ftra 'fet402_mesh.ps';
p0 = 0 0 0;
dd = 0.01;
n = 100;
tol = 0.0001;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
bar8 = base volu n tran ((n*dd) 0 0);
i = 0;
repe loop1 (nbel bar8),
  i = i + 1;
  cube1 = bar8 elem i;
  tt = pxhex2t2 cube1;
  si (egi 1);
    bar = tt;
  sinon;
    bar = bar et tt;
  finis;
fin loop1;
elin tol bar;
barsur = chan poil (enve bar);
mesh = bar et barsur;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;
```

## fet402.epx

```

FET402
ECHO
!CONV win
CAST mesh
EULE TRID
DIME
ADAP NPOI 3189 TETR 15712 ENDA
TERM
GROM TETR bar TERM
COMP GROU 4 'bar1' LECT bar TERM COND XB LT 0.5
  'bar2' LECT bar DIFF bar1 TERM
    'ea' LECT bar TERM COND NEAR POIN 0.25 0 0
    'eb' LECT bar TERM COND NEAR POIN 0.75 0 0
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
  X2 1 Y2 0 Z2 0 TOL 1.E-4
  'bas1' LECT bar TERM COND X LT 0.0001
  'bas2' LECT bar TERM COND X GT 0.9999
  'na' LECT bar TERM COND NEAR POIN 0.25 0 0
  'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
  VERT LECT bar2 TERM
WAVE 4 PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 613.568783589856 ! shock wave
  MAXL 3 H1 0.015 H2 0.05
  PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 295.278289836459 ! c.d. wave
  MAXL 3 H1 0.015 H2 0.05
  PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 18.2004723251679 ! r.wave (ri.)
  MAXL 3 H1 0.015 H2 0.05
  PLAN X 0.5 Y 0 Z 0 NX -1 NY 0 NZ 0 TO 0 C 387.298334620742 ! r. wav (le.)
  MAXL 3 H1 0.015 H2 0.05
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
  LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
  LECT bar2 _tetr TERM
LINK COUP BLOQ 1 LECT bas1 bas2 TERM
  BLOQ 23 LECT barsur TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
  FICH ALIC TEMP FREQ 1
    POIN LECT na nb TERM
    ELEM LECT ea eb TERM
    FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.125
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
```

```

SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR VERT
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR VERT
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR VERT
LIST 65 AXES 1.0 'VELOC. [M/S]'
*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.99014E+5 TOLE 2.E-2
    ECRO COMP 1 LECT eb TERM REFE 2.83201E+5 TOLE 2.E-2
    ECRO COMP 2 LECT ea TERM REFE 9.99359E+0 TOLE 2.E-2
    ECRO COMP 2 LECT eb TERM REFE 1.92907E+0 TOLE 2.E-2
=====
SUIT
Post-treatment (time curves from alice temps file)
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fet402.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_ea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'
COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'
COLO NOIR NOIR
LIST 1 4 AXES 1.0 'PRESS. [PA]'
LIST 2 5 AXES 1.0 'DENS. [KG/M3]'
LIST 3 6 AXES 1.0 'VELOC. [M/S]'
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
!     Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
    VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
    RIGH 1.00000E+00 0.00000E+00 0.00000E+00
    UP 0.00000E+00 1.00000E+00 0.00000E+00
    POV 5.25000E+01
SCEN GEON NAVI FREE
!     LINE HEOU
    ISO FILE FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
    TEXT ISCA
    COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
SCEN GEON NAVI FREE
!     LINE HEOU
    ISO FILE FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
    TEXT ISCA
    COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
FIN

```

**fet402a.epx**

```

FET402A
ECHO
RESU ALIC 'fet402.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
    X2 1 Y2 0 Z2 0 TOL 1.E-4
    'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
    X2 1 Y2 .01 Z2 0 TOL 1.E-4
    'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
    X2 1 Y2 .01 Z2 .01 TOL 1.E-4
    'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
    X2 1 Y2 0 Z2 .01 TOL 1.E-4
SORT VISU NSTO 61
FIN

```

**fet402b.epx**

```

FET402B
ECHO
OPTI PRIN
RESU ALIC 'fet402.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
    X2 1 Y2 0 Z2 0 TOL 1.E-4
    'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
    X2 1 Y2 .01 Z2 0 TOL 1.E-4
    'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
    X2 1 Y2 .01 Z2 .01 TOL 1.E-4
    'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
    X2 1 Y2 0 Z2 .01 TOL 1.E-4

```

```

    'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
    X2 1 Y2 .01 Z2 .01 TOL 1.E-4
    'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
    X2 1 Y2 0 Z2 .01 TOL 1.E-4
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 1
SCOU 62 'ro_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 2
SCOU 65 'vx_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    VITE COMP 1
SCOU 161 'p_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    ECRO COMP 1
SCOU 162 'ro_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    ECRO COMP 2
SCOU 165 'vx_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    VITE COMP 1
SCOU 261 'p_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    ECRO COMP 1
SCOU 262 'ro_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    ECRO COMP 2
SCOU 265 'vx_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    VITE COMP 1
SCOU 361 'p_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    ECRO COMP 1
SCOU 362 'ro_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    ECRO COMP 2
SCOU 365 'vx_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR BLEU TURQ VERT ROUG
LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR BLEU TURQ VERT ROUG
TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR BLEU TURQ VERT ROUG
FIN

```

**fet402c.epx**

```

FET402C
ECHO
OPTI PRIN
RESU ALIC 'fet402.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
    X2 1 Y2 0 Z2 0 TOL 1.E-4
    'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
    X2 1 Y2 .01 Z2 0 TOL 1.E-4
    'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
    X2 1 Y2 .01 Z2 .01 TOL 1.E-4
    'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
    X2 1 Y2 0 Z2 .01 TOL 1.E-4

```

```

SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 1
SCOU 62 'ro_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 2
SCOU 65 'vx_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    VITE COMP 1
SCOU 161 'p_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    ECRO COMP 1
SCOU 162 'ro_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    ECRO COMP 2
SCOU 165 'vx_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    VITE COMP 1
SCOU 261 'p_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    ECRO COMP 1
SCOU 262 'ro_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    ECRO COMP 2
SCOU 265 'vx_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    VITE COMP 1
SCOU 361 'p_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    ECRO COMP 1
SCOU 362 'ro_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    ECRO COMP 2
SCOU 365 'vx_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.0E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.0E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.0E-3 NRAR 30 VARI 5
TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR BLEU TURQ VERT ROUG
LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR BLEU TURQ VERT ROUG
TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR BLEU TURQ VERT ROUG
TRAC 161 71 AXES 1.0 'PRESS. [PA]'
COLO BLEU ROUG
TRAC 162 72 AXES 1.0 'DENS. [KG/M3]'
COLO BLEU
TRAC 165 75 AXES 1.0 'VELOC. [M/S]'
COLO BLEU
FIN

```

**fet403.dgibi**

```

opti echo 1;
opti domm 'pxhex2t2.proc';
opti dime 3 elem cub8;
opti titr 'FET403';
opti sauv form 'fet403.msh';
opti trac psc ftra 'fet403_mesh.ps';
p0 = 0 0 0;
dd = 0.01;
n = 100;
tol = 0.0001;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
bar8 = base volu n tran ((n*dd) 0 0);
i = 0;
repe loop1 (nbel bar8);
i = i + 1;
cubei = bar8 elem i;
tt = pxhex2t2 cubei;
si (egs i 1);
bar = tt;
sinon;
bar = bar et tt;
finsi;
fin loop1;
elin tol bar;
barsur = chan poil (enve bar);
mesh = bar et barsur;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;

```

**fet403.epx**

```

FET403
ECHO
!CONV win
CAST mesh
EULE TRID
DIME
ADAP NPOI 4208 TETR 19200 ENDA
TERM
GROM TETR bar TERM
COMP GROU 4 'bar1' LECT bar TERM COND XB LT 0.5
  'bar2' LECT bar DIFF bar1 TERM
  'ea' LECT bar TERM COND NEAR POIN 0.25 0 0
  'eb' LECT bar TERM COND NEAR POIN 0.75 0 0
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
  X2 1 Y2 0 Z2 0 TOL 1.E-4
  'bas1' LECT bar TERM COND X LT 0.0001
  'bas2' LECT bar TERM COND X GT 0.9999
  'na' LECT bar TERM COND NEAR POIN 0.25 0 0
  'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
  VERT LECT bar2 TERM
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
  LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
  LECT bar2 _tetra TERM
INIT ADAP SPLI LEVE 2 LECT bar TERM
LINK COUP BLOQ 1 LECT bas1 bas2 TERM
  BLOQ 23 LECT barsur TERM
ECRI COOR DEPL VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
  FICH ALIC TEMP FREQ 1
  POIN LECT na nb TERM
  ELEM LECT ea eb TERM
  FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.5
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
  COLO NOIR VERT
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
  COLO NOIR VERT
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
  COLO NOIR VERT
LIST 65 AXES 1.0 'VELOC. [M/S]'
  *
QUAL ECRO COMP 1 LECT ea TERM REFE 9.95808E+5 TOLE 2.E-2
  ECRO COMP 1 LECT eb TERM REFE 2.82388E+5 TOLE 2.E-2
  ECRO COMP 2 LECT ea TERM REFE 9.97203E+0 TOLE 2.E-2
  ECRO COMP 2 LECT eb TERM REFE 1.90880E+0 TOLE 2.E-2

```

**SUIT**

```

Post-treatment (time curves from alice temps file)
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fet403t.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_ea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'
  COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'
  COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'
  COLO NOIR NOIR
LIST 1 4 AXES 1.0 'PRESS. [PA]'
LIST 2 5 AXES 1.0 'DENS. [KG/M3]'
LIST 3 6 AXES 1.0 'VELOC. [M/S]'

=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
  ! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
    VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
    RIGH 1.00000E+00 0.00000E+00 0.00000E+00
    UP 0.00000E+00 1.00000E+00 0.00000E+00
    FOV 5.25000E+01
SCEN GEOM NAVI FREE
  ! LINE HEBOU
    ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
    TEXT ISCA
    COLO PAPE
  SLER CAM1 1 NFRA 1
  TRAC OFFS SIZE 1400 400 FICH BMP REND
  SCEN GEOM NAVI FREE
  ! LINE HEBOU
    ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
    TEXT ISCA
    COLO PAPE
  SLER CAM1 1 NFRA 1
  TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====

FIN

```

**fet403a.epx**

```

FET403A
ECHO
RESU ALIC 'fet403.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
  X2 1 Y2 0 Z2 0 TOL 1.E-4
  'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
  X2 1 Y2 .01 Z2 0 TOL 1.E-4
  'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
  X2 1 Y2 .01 Z2 .01 TOL 1.E-4
  'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
  X2 1 Y2 0 Z2 .01 TOL 1.E-4
SORT VISU NSTO 61
FIN

```

**fet403b.epx**

```

FET403B
ECHO
OPTI PRIN
RESU ALIC 'fet403.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
  X2 1 Y2 0 Z2 0 TOL 1.E-4
  'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
  X2 1 Y2 .01 Z2 0 TOL 1.E-4
  'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
  X2 1 Y2 .01 Z2 .01 TOL 1.E-4
  'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
  X2 1 Y2 0 Z2 .01 TOL 1.E-4
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  VITE COMP 1
SCOU 161 'p_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
  ECRO COMP 1
SCOU 162 'ro_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
  ECRO COMP 2
SCOU 165 'vx_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
  VITE COMP 1
SCOU 261 'p_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
  ECRO COMP 1
SCOU 262 'ro_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
  ECRO COMP 2
SCOU 265 'vx_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
  VITE COMP 1
SCOU 361 'p_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
  ECRO COMP 1
SCOU 362 'ro_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
  ECRO COMP 2
SCOU 365 'vx_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
  VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 5

```

```

TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_anal' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR BLEU TURQ VERT ROUG
LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR BLEU TURQ VERT ROUG
TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR BLEU TURQ VERT ROUG
FIN

```

**fet403c.epx**

```

FET403C
ECHO
OPTI PRIN
RESU ALIC 'fet403.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
    X2 1 Y2 0 Z2 0 TOL 1.E-4
'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
    X2 1 Y2 .01 Z2 0 TOL 1.E-4
'xaxg' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
    X2 1 Y2 .01 Z2 .01 TOL 1.E-4
'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
    X2 1 Y2 0 Z2 .01 TOL 1.E-4
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 1
SCOU 62 'ro_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 2
SCOU 65 'vx_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    VITE COMP 1
SCOU 161 'p_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    ECRO COMP 1
SCOU 162 'ro_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    ECRO COMP 2
SCOU 165 'vx_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
    VITE COMP 1
SCOU 261 'p_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    ECRO COMP 1
SCOU 262 'ro_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    ECRO COMP 2
SCOU 265 'vx_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
    VITE COMP 1
SCOU 361 'p_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    ECRO COMP 1
SCOU 362 'ro_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    ECRO COMP 2
SCOU 365 'vx_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
    VITE COMP 1
DCOU 71 'p_anal' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.0E-3 NRAR 30 VARI 1
DCOU 72 'r_anal' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.0E-3 NRAR 30 VARI 2
DCOU 75 'v_anal' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.0E-3 NRAR 30 VARI 5
TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR BLEU TURQ VERT ROUG
LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR TURQ VERT ROUG
TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR BLEU TURQ VERT ROUG
TRAC 161 71 AXES 1.0 'PRESS. [PA]'
COLO BLEU ROUG
TRAC 162 72 AXES 1.0 'DENS. [KG/M3]'
COLO BLEU ROUG
TRAC 165 75 AXES 1.0 'VELOC. [M/S]'
COLO BLEU
TRAC 161 AXES 1.0 'PRESS. [PA]'
COLO BLEU
TRAC 162 AXES 1.0 'DENS. [KG/M3]'
COLO BLEU
TRAC 165 AXES 1.0 'VELOC. [M/S]'
COLO BLEU
FIN

```

**fet404.dgibi**

```

opti echo 1;
opti domm 'pxhex2t2.proc';
opti dime 3 elem cub8;
opti titr 'FET404';
opti sauv form 'fet404.msh';
opti trac psc ftra 'fet404_mesh.ps';
p0 = 0 0 0;
dd = 0.01;
n = 100;
tol = 0.0001;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
base = base volu n tran ((n*dd) 0 0);
i = 0;
repeat loop1 (nbel bar8);
    i = i + 1;
    cubei = bar8 elem i;
    tt = pxhex2t2 cubei;
    si (egi i 1);
    bar = tt;
    sinon;
        bar = bar et tt;
    finisi;
    fin loop1;
    elim tol bar;
    barsur = chan poil (enve bar);

```

---

```

mesh = bar et barsur;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;

fet404.epx

```

---

```

FET404
ECHO
!CONV win
CAST mesh
EULE TRID
DIME
    ADAP NPOI 31836 TETR 172800 ENDA
TERM
GEOM TETR bar TERM
COMP GROU 4 'bar1' LECT bar TERM COND XB LT 0.5
    'bar2' LECT bar DIFF bar1 TERM
    'ea' LECT bar TERM COND NEAR POIN 0.25 0 0
    'eb' LECT bar TERM COND NEAR POIN 0.75 0 0
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
    X2 1 Y2 0 Z2 0 TOL 1.E-4
    'bas1' LECT bar TERM COND X LT 0.0001
    'bas2' LECT bar TERM COND X GT 0.9999
    'na' LECT bar TERM COND NEAR POIN 0.25 0 0
    'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
    VERT LECT bar2 TERM
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
    LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
    LECT bar2 _tet4 TERM
INIT ADAP SPLT LEVE 3 LECT bar TERM
LINK COUP BLOQ 1 LECT bas1 bas2 TERM
    BLOQ 23 LECT barsur TERM
ECRI COOR DPLT VITE ACCE FINT FEXT CONT ECRO TFRE 0.3E-3
    FICH ALIC TEMP FREQ 1
    POIN LECT na nb TERM
    ELEM LECT ea eb TERM
    FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.5
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    VITE COMP 1
DCOU 71 'p_anal' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_anal' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_anal' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR VERT
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR VERT
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR VERT
LIST 65 AXES 1.0 'VELOC. [M/S]'
*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.99349E+5 TOLE 2.E-2
    ECRO COMP 1 LECT eb TERM REFE 2.81990E+5 TOLE 2.E-2
    ECRO COMP 2 LECT ea TERM REFE 9.99566E+0 TOLE 2.E-2
    ECRO COMP 2 LECT eb TERM REFE 1.90769E+0 TOLE 2.E-2
=====
SUIT
Post-treatment (time curves from alice temps file)
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fet404t.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_ea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'
COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'
COLO NOIR NOIR
LIST 1 4 AXES 1.0 'PRESS. [PA]'
LIST 2 5 AXES 1.0 'DENS. [KG/M3]'
LIST 3 6 AXES 1.0 'VELOC. [M/S]'
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
    ! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
    VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
    RIGH 1.00000E+00 0.00000E+00 0.00000E+00
    UP 0.00000E+00 1.00000E+00 0.00000E+00
    FOV 5.25000E+01

```

```

SCEN GEOM NAVI FREE
!      LINE HEOU
ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
SCEN GEOM NAVI FREE
!      LINE HEOU
ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
FIN

```

**fet404a.epx**

```

FET404A
ECHO
RESU ALIC 'fet404.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
X2 1 Y2 .01 Z2 0 TOL 1.E-4
'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
X2 1 Y2 .01 Z2 .01 TOL 1.E-4
'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
X2 1 Y2 0 Z2 .01 TOL 1.E-4

```

SORT VISU NSTO 61

FIN

**fet404b.epx**

```

FET404B
ECHO
OPTI PRIN
RESU ALIC 'fet404.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
X2 1 Y2 .01 Z2 0 TOL 1.E-4
'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
X2 1 Y2 .01 Z2 .01 TOL 1.E-4
'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
X2 1 Y2 0 Z2 .01 TOL 1.E-4

```

SORT GRAP

AXTE 1.0 'Time [s]'

```

SCOU 61 'p_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 1
SCOU 62 'ro_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 2
SCOU 65 'vx_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
VITE COMP 1
SCOU 161 'p_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 1
SCOU 162 'ro_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 2
SCOU 165 'vx_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
VITE COMP 1
SCOU 261 'p_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 1
SCOU 262 'ro_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 2
SCOU 265 'vx_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
VITE COMP 1
SCOU 361 'p_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 1
SCOU 362 'ro_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 2
SCOU 365 'vx_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 5

```

TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'

COLO NOIR BLEU TURQ VERT ROUG

LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'

TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'

COLO NOIR BLEU TURQ VERT ROUG

TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'

COLO NOIR BLEU TURQ VERT ROUG

TRAC 161 71 AXES 1.0 'PRESS. [PA]'

COLO BLEU ROUG

TRAC 162 72 AXES 1.0 'DENS. [KG/M3]'

COLO BLEU ROUG

TRAC 165 75 AXES 1.0 'VELOC. [M/S]'

COLO BLEU ROUG

TRAC 161 AXES 1.0 'PRESS. [PA]'

COLO BLEU

TRAC 162 AXES 1.0 'DENS. [KG/M3]'

COLO BLEU

TRAC 165 AXES 1.0 'VELOC. [M/S]'

COLO BLEU

FIN

**fet404c.epx**

```

FET404C
ECHO
OPTI PRIN
RESU ALIC 'fet404.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
X2 1 Y2 .01 Z2 0 TOL 1.E-4
'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
X2 1 Y2 .01 Z2 .01 TOL 1.E-4
'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
X2 1 Y2 0 Z2 .01 TOL 1.E-4

```

SORT GRAP

AXTE 1.0 'Time [s]'

```

SCOU 61 'p_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 1
SCOU 62 'ro_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 2
SCOU 65 'vx_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
VITE COMP 1

```

```

SCOU 161 'p_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 1
SCOU 162 'ro_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 2
SCOU 165 'vx_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
VITE COMP 1
SCOU 261 'p_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 1
SCOU 262 'ro_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 2
SCOU 265 'vx_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
VITE COMP 1
SCOU 361 'p_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 1
SCOU 362 'ro_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 2
SCOU 365 'vx_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.0E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.0E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.0E-3 NRAR 30 VARI 5

```

TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'

COLO NOIR BLEU TURQ VERT ROUG

LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'

TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'

COLO NOIR BLEU TURQ VERT ROUG

TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'

COLO NOIR BLEU TURQ VERT ROUG

TRAC 161 71 AXES 1.0 'PRESS. [PA]'

COLO BLEU ROUG

TRAC 162 72 AXES 1.0 'DENS. [KG/M3]'

COLO BLEU ROUG

TRAC 165 75 AXES 1.0 'VELOC. [M/S]'

COLO BLEU ROUG

TRAC 161 AXES 1.0 'PRESS. [PA]'

COLO BLEU

TRAC 162 AXES 1.0 'DENS. [KG/M3]'

COLO BLEU

TRAC 165 AXES 1.0 'VELOC. [M/S]'

COLO BLEU

FIN

**fet405.dgibi**

```

opti echo 1;
opti donn 'pxhex2t2.proc';
opti dime 3 elem cub8;
opti titr 'PET405';
opti sauv form 'fet405.msh';
opti trac psc ftra 'fet405_mesh.ps';
p0 = 0 0 0;
dd = 0.01;
n = 100;
tol = 0.0001;
p1 = 0 dd 0;
p2 = 0 dd dd;
p3 = 0 0 dd;
c1 = p0 d 1 p1;
c2 = p1 d 1 p2;
c3 = p2 d 1 p3;
c4 = p3 d 1 p0;
base = dall c1 c2 c3 c4 plan;
bar8 = base volu n tran ((n*dd) 0 0);
i = 0;
repe loop1 (nbel bar8);
  i = i + 1;
  cube1 = bar8 elem i;
  tt = pxhex2t2 cube1;
  si (ega i 1);
    bar = tt;
    sinon;
      bar = bar et tt;
    finis;
fin loop1;
elim tol bar;
barsur = chan poi1 (enve bar);
mesh = bar et barsur;
tass mesh;
sauv form mesh;
trac qual cach mesh;
fin;

```

**fet405.epx**

```

FET405
ECHO
!CONV win
CAST mesh
EULE TRID
DIME
ADAP NPOI 8182 TETR 42688 ENDA
TERM
GEON TETR bar TERM
COMP GROU 4 'bar1' LECT bar TERM COND XB LT 0.5
  'bar2' LECT bar DIFF bar1 TERM
  'ea' LECT bar TERM COND NEAR POIN 0.25 0 0
  'eb' LECT bar TERM COND NEAR POIN 0.75 0 0
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
  'bas1' LECT bar TERM COND X LT 0.0001
  'bas2' LECT bar TERM COND X GT 0.9999
  'na' LECT bar TERM COND NEAR POIN 0.25 0 0
  'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
  VERT LECT bar2 TERM
WAVE 4 PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 613.568783589856 ! shock wave
  MAXL 3 H1 0.045 H2 0.15
  PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 295.278289836459 ! c.d. wave
  MAXL 3 H1 0.045 H2 0.15
  PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 18.2004723251679 ! r.wave (ri.)

```

```

MAXL 3 H1 0.045 H2 0.05
PLAN X 0.5 Y 0 Z 0 NX -1 NY 0 NZ 0 TO 0 C 387.298334620742 ! r. wav (le.)
MAXL 3 H1 0.045 H2 0.15
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
LECT barl TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
LECT bar2_tetr TERM
LINK COUP BLOQ 1 LECT bas1 bas2 TERM
BLOQ 23 LECT barsur TERM
ECRI COOR DEPL VITE ACCF FINT FEXT CONT ECRO TFRE 0.3E-3
FICH ALIC TEMP FREQ 1
POIN LECT na nb TERM
ELEM LECT ea eb TERM
FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.125
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR VERT
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR VERT
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR VERT
LIST 65 AXES 1.0 'VELOC. [M/S]'
*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.99360E+5 TOLE 2.E-2
ECRO COMP 1 LECT eb TERM REFE 2.83005E+5 TOLE 2.E-2
ECRO COMP 2 LECT ea TERM REFE 9.99574E+0 TOLE 2.E-2
ECRO COMP 2 LECT eb TERM REFE 1.93073E+0 TOLE 2.E-2
=====
SUIT
Post-treatment (time curves from alice temps file)
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fet405t.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_ea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'
COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'
COLO NOIR NOIR
LIST 1 4 AXES 1.0 'PRESS. [PA]'
LIST 2 5 AXES 1.0 'DENS. [KG/M3]'
LIST 3 6 AXES 1.0 'VELOC. [M/S]'
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 5.25000E+01
SCEN GEOM NAVI FREE
! LINE HEBOU
ISO FILT FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
SCEN GEOM NAVI FREE
! LINE HEBOU
ISO FILT FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
FIN

```

**fet405a.epx**

```

FET405A
ECHO
RESU ALIC 'fet405.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
X2 1 Y2 .01 Z2 0 TOL 1.E-4

```

```

'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
X2 1 Y2 .01 Z2 .01 TOL 1.E-4
'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
X2 1 Y2 0 Z2 .01 TOL 1.E-4
SORT VISU NSTO 61
FIN

```

**fet405b.epx**

```

FET405B
ECHO
OPTI PRIN
RESU ALIC 'fet405.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
X2 1 Y2 .01 Z2 0 TOL 1.E-4
'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
X2 1 Y2 .01 Z2 .01 TOL 1.E-4
'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
X2 1 Y2 0 Z2 .01 TOL 1.E-4

```

```

SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 1
SCOU 62 'ro_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 2
SCOU 65 'vx_61o' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
VITE COMP 1
SCOU 161 'p_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 1
SCOU 162 'ro_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 2
SCOU 165 'vx_61p' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
VITE COMP 1
SCOU 261 'p_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 1
SCOU 262 'ro_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 2
SCOU 265 'vx_61q' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
VITE COMP 1
SCOU 361 'p_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 1
SCOU 362 'ro_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 2
SCOU 365 'vx_61r' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR BLEU TURQ VERT ROUG
LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR BLEU TURQ VERT ROUG
TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR BLEU TURQ VERT ROUG
FIN

```

**fet405c.epx**

```

FET405C
ECHO
OPTI PRIN
RESU ALIC 'fet405.ali' GARD PSCR
COMP NGRO 4 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
X2 1 Y2 0 Z2 0 TOL 1.E-4
'xaxp' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 0
X2 1 Y2 .01 Z2 0 TOL 1.E-4
'xaxq' LECT bar TERM COND LINE X1 0 Y1 .01 Z1 .01
X2 1 Y2 .01 Z2 .01 TOL 1.E-4
'xaxr' LECT bar TERM COND LINE X1 0 Y1 0 Z1 .01
X2 1 Y2 0 Z2 .01 TOL 1.E-4

```

```

SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 1
SCOU 62 'ro_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
ECRO COMP 2
SCOU 65 'vx_61o' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
VITE COMP 1
SCOU 161 'p_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 1
SCOU 162 'ro_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
ECRO COMP 2
SCOU 165 'vx_61p' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxp TERM
VITE COMP 1
SCOU 261 'p_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 1
SCOU 262 'ro_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
ECRO COMP 2
SCOU 265 'vx_61q' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxq TERM
VITE COMP 1
SCOU 361 'p_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 1
SCOU 362 'ro_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
ECRO COMP 2
SCOU 365 'vx_61r' NSTO 1 SAXE 1.0 'curr_abscissa' LECT xaxr TERM
VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.0E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.0E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
TIME 0.0E-3 NRAR 30 VARI 5
TRAC 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR BLEU TURQ VERT ROUG
LIST 61 161 261 361 71 AXES 1.0 'PRESS. [PA]'
TRAC 62 162 262 362 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR BLEU TURQ VERT ROUG

```

```
TRAC 65 165 265 365 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR BLEU TURQ VERT ROUG
TRAC 161 71 AXES 1.0 'PRESS. [PA]'
COLO BLEU ROUG
TRAC 162 72 AXES 1.0 'DENS. [KG/M3]'
COLO BLEU ROUG
TRAC 165 75 AXES 1.0 'VELOC. [M/S]'
COLO BLEU ROUG
TRAC 161 AXES 1.0 'PRESS. [PA]'
COLO BLEU
TRAC 162 AXES 1.0 'DENS. [KG/M3]'
COLO BLEU
TRAC 165 AXES 1.0 'VELOC. [M/S]'
COLO BLEU
FIN
```

**fet406.epx**

```
FET406
ECHO
!CONV win
CAST mesh
EULE TRID
DIME
ADAP NPOI 259 TETR 1008 ENDA
TERM
GEOM TETR bar TERM
COMP GROU 4 'bar1' LECT bar TERM COND XB LT 0.5
  'bar2' LECT bar DIFF bar1 TERM
  'ea' LECT bar TERM COND NEAR POIN 0.25 0 0
  'eb' LECT bar TERM COND NEAR POIN 0.75 0 0
NGRO 5 'xaxo' LECT bar TERM COND LINE X1 0 Y1 0 Z1 0
  X2 1 Y2 0 Z2 0 TOL 1.E-4
  'bas1' LECT bar TERM COND X LT 0.0001
  'bas2' LECT bar TERM COND X GT 0.9999
  'na' LECT bar TERM COND NEAR POIN 0.25 0 0
  'nb' LECT bar TERM COND NEAR POIN 0.75 0 0
COUL ROUG LECT bar1 TERM
  VERT LECT bar2 TERM
WAVE 4 PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 613.568783589856 ! shock wave
  MAXL 2 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 Z 0 NX 1 NY 0 NZ 0 TO 0 C 295.278289836459 ! c.d. wave
  MAXL 2 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 Z 0 NX -1 NY 0 NZ 0 TO 0 C 18.2004723251679 ! r.wave (ri.)
  MAXL 2 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 Z 0 NX -1 NY 0 NZ 0 TO 0 C 387.298334620742 ! r. wav (le.)
  MAXL 2 H1 0.015 H2 0.05
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
  LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
  LECT bar2_tetr TERM
LINK COUP BLOQ 1 LECT bas1 bas2 TERM
  BLOQ 23 LECT barsur TERM
ECRI COOR DEPL VITE ACCR FINT FEXT CONT ECRO TFRE 0.3E-3
  FICH ALIC TEMP FREQ 1
    POIN LECT na nb TERM
    ELEM LECT ea eb TERM
    FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.125
LOG 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
  VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
  TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR VERT
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR VERT
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR VERT
LIST 65 AXES 1.0 'VELOC. [M/S]'
=====
QUAL ECRO COMP 1 LECT ea TERM REFE 9.97505E+5 TOLE 2.E-2
  ECRO COMP 1 LECT eb TERM REFE 2.84640E+5 TOLE 2.E-2
  ECRO COMP 2 LECT ea TERM REFE 9.98336E+0 TOLE 2.E-2
  ECRO COMP 2 LECT eb TERM REFE 1.93773E+0 TOLE 2.E-2
=====
SUIT
Post-treatment (time curves from alice temps file)
ECHO
RESU ALIC TEMP GARD PSCR
SORT GRAP
PERF 'fet406.pun'
AXTE 1.0 'Time [s]'
COUR 1 'p_ea' ECRO COMP 1 ELEM LECT ea TERM
COUR 2 'ro_ea' ECRO COMP 2 ELEM LECT ea TERM
COUR 3 'vx_ea' VITE COMP 1 NOEU LECT na TERM
COUR 4 'p_eb' ECRO COMP 1 ELEM LECT eb TERM
COUR 5 'ro_eb' ECRO COMP 2 ELEM LECT eb TERM
COUR 6 'vx_eb' VITE COMP 1 NOEU LECT nb TERM
TRAC 1 4 AXES 1.0 'PRESS. [PA]'
COLO NOIR NOIR
TRAC 2 5 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR NOIR
TRAC 3 6 AXES 1.0 'VELOC. [M/S]'
COLO NOIR NOIR
```

```
LIST 1 4 AXES 1.0 'PRESS. [PA]'
LIST 2 5 AXES 1.0 'DENS. [KG/M3]'
LIST 3 6 AXES 1.0 'VELOC. [M/S]'
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.0000E-01 5.0000E-03 3.00015E-01
  Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  POV 5.25000E+01
SCEN GEOM NAVI FREE
  LINE HEOU
  ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
  TEXT ISCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
SCEN GEOM NAVI FREE
  LINE HEOU
  ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
  TEXT ISCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP REND
ENDPLAY
=====
FIN
```

**fetr00.dgibi**

```
opti echo 0;
opti donn 'pxordpoi.proc';
opti echo 1;
opti dime 2 elem qua4;
opti sauv form 'fetr00.msh';
opti trac psc ftra 'fetr00_mesh.ps';
p0 = 0;
p0p = p0 plus (0 0.00125);
pmid = 0.5 0;
p1 = 1 0;
plp = p1 plus (0 0.00125);
pa = 0.25 0;
pb = 0.75 0;
tol = 1.E-5;
n = 800;
n2 = n / 2;
n4 = n2 / 2;
c11 = po d n4 pa;
c12 = pa d n4 pmid;
c1 = c11 et c12;
c21 = pmid d n4 pb;
c22 = pb d n4 pl;
c2 = c21 et c22;
bar11 = c11 tran 1 (0 0.00125);
bar12 = c12 tran 1 (0 0.00125);
bar1q = bar11 et bar12;
bar1 = chan tri3 bar1q;
bar21 = c21 tran 1 (0 0.00125);
bar22 = c22 tran 1 (0 0.00125);
bar2q = bar21 et bar22;
bar2 = chan tri3 bar2q;
bar = bar1 et bar2;
elim tol (bar et p0p et plp et pa et pb);
ea = bar1 elem cont pa;
eb = bar2 elem cont pb;
xax = chan 'POI1' (cl et c2);
xaxo = pxordpoi xax p0;
mesh = bar et ea et eb et xaxo;
tass mesh;
sauv form mesh;
trac qual mesh;
trac ((cont mesh) et ea et eb);
fin;
```

**fetr00.epx**

```
FETR00 (with mesh reduced to 800 x 1 x 2 to save CPU time)
ECHO
!CONV win
CAST mesh
EULE DPLA
GEOM TRIA bar TERM
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
  LECT bar1 TERM
GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
  LECT bar2 TERM
LINK COUP BLOQ 1 LECT p0 p0p pl pip TERM
  BLOQ 2 LECT bar TERM
ECRI COOR DEPL VITE ACCR FINT FEXT CONT ECRO TFRE 0.3E-3
  FICH ALIC TEMP FREQ 1
    POIN LECT pa pmid pb TERM
    ELEM LECT ea eb TERM
    FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
AMOR QUAD 4.0 LINE 0.2
CSTA 0.5
log 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
SORT GRAP
PERF 'fetr00.pun'
AXTE 1.0 'Time [s]'
```

```

SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 1                                         4   5 105
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    ECRO COMP 2                                         5   6 107
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    VITE COMP 1                                         107 106 5
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 1                         108 107 7
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 2                         109 108 7
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 5                         110 109 9
    9 10 111
    11 110 9
    10 11 111
    112 111 11
    11 12 113
    113 112 11
    12 13 113
    114 113 13
    13 14 115
    115 114 13
    14 15 115
    116 115 15
    15 16 117
    117 116 15
    16 17 117
    118 117 17
    17 18 119
    119 118 17
    18 19 119
    120 119 19
    19 20 121
    121 120 19
    20 21 121
    122 121 21
    21 22 123
    123 122 21
    22 23 123
    124 123 23
    23 24 125
    125 124 23
    24 25 125
    126 125 25
    25 26 127
    127 126 25
    26 27 127
    128 127 27
    27 28 129
    129 128 27
    28 29 129
    130 129 29
    29 30 131
    131 130 29
    30 31 131
    132 131 31
    31 32 133
    133 132 31
    32 33 133
    134 133 33
    33 34 135
    135 134 33
    34 35 135
    136 135 35
    35 36 137
    137 136 35
    36 37 137
    138 137 37
    37 38 139
    139 138 37
    38 39 139
    140 139 39
    39 40 141
    141 140 39
    40 41 141
    142 141 41
    41 42 143
    143 142 41
    42 43 143
    144 143 43
    43 44 145
    145 144 43
    44 45 145
    146 145 45
    45 46 147
    147 146 45
    46 47 147
    148 147 47
    47 48 149
    149 148 47
    48 49 149
    150 149 49
    49 50 151
    151 150 49
    50 51 151
    152 151 51
    51 52 153
    153 152 51
    52 53 153
    154 153 53
    53 54 155
    155 154 53
    54 55 155
    156 155 55
    55 56 157
    157 156 55
    56 57 157
    158 157 57
    57 58 159
    159 158 57
    58 59 159
    160 159 59
    59 60 161
    161 160 59
    60 61 161
    162 161 61
    61 62 163
    163 162 61
    62 63 163
    164 163 63
0 0 1 0 1 0 1 ! bidon nodes (203 a 206)
203 204 205 206 ! bidon element (1)
    1 2 103
103 102 1
    2 3 103
104 103 3
    3 4 105
105 104 3

```

```

63 64 165
165 164 63
64 65 165
166 165 65
65 66 167
167 166 65
66 67 167
168 167 67
67 68 169
169 168 67
68 69 169
170 169 69
69 70 171
171 170 69
70 71 171
172 171 71
71 72 173
173 172 71
72 73 173
174 173 73
73 74 175
175 174 73
74 75 175
176 175 75
75 76 177
177 176 75
76 77 177
178 177 77
77 78 179
179 178 77
78 79 179
180 179 79
79 80 181
181 180 79
80 81 181
182 181 81
81 82 183
183 182 81
82 83 183
184 183 83
83 84 185
185 184 83
84 85 185
186 185 85
85 86 187
187 186 85
86 87 187
188 187 87
87 88 189
189 188 87
88 89 189
190 189 89
89 90 191
191 190 89
90 91 191
192 191 91
91 92 193
193 192 91
92 93 193
194 193 93
93 94 195
195 194 93
94 95 195
196 195 95
95 96 197
197 196 95
96 97 197
198 197 97
97 98 199
199 198 97
98 99 199
200 199 99
99 100 201
201 200 99
100 101 201
202 201 101
COMP GROU 6 'bar1' LECT 2 PAS 1 101 TERM
    'bar2' LECT 102 PAS 1 201 TERM
    'bar' LECT bar1 bar2 TERM
    'ea' LECT 51 TERM
    'eb' LECT 151 TERM
    'bidon' LECT 1 TERM
    NGRO 7 'p0' LECT 1 TERM
    'p0p' LECT 102 TERM
    'p1' LECT 101 TERM
    'p1p' LECT 202 TERM
    'pa' LECT 26 TERM
    'pmid' LECT 51 TERM
    'pb' LECT 76 TERM
WAVE 4 PLAN X 0.5 Y 0 NX 1 NY 0 TO 0 C 613.568783589856 ! shock wave
    MAXL 4 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 NX 1 NY 0 TO 0 C 295.278289836459 ! c.d. wave
    MAXL 4 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 NX 1 NY 0 TO 0 C 18.2004723251679 ! r.wave (right)
    MAXL 4 H1 0.015 H2 0.05
PLAN X 0.5 Y 0 NX -1 NY 0 TO 0 C 387.298334620742 ! r. wave (left)
    MAXL 4 H1 0.015 H2 0.05
MATE GAZP RO 10 GAMM 1.5 PINI 1.E6 PREF 1.E5
    LECT bar1 TERM
    GAZP RO 1 GAMM 1.5 PINI 1.E5 PREF 1.E5
    LECT bar2 _tria TERM
*
**** Material with no elements, then isolated from the rest.
* In this way it is taken into account in the dimension of ECRO
* in the extension region. One can check that this material
* does not affect the final result.
*
CREB
    PINI 1.2 PREF 1.2 TINI 1.090909090909
    KSIO 0.0 ! Unburnt region.
    KO 0.0
*
    TMAX 6000.
    R 1.0
    NESP 2
    ORDP 0
    NLHS 1
*
COMP1
    MMOL 1.0 H0 -4.2 CREA 1.
    CV0 2.5
    YMAS 0.7 ! Mass fraction if the unburnt region
*
COMP2
    MMOL 1.0 H0 -4.2 CREA -1.
    CV0 2.5
    YMAS 0.3 ! Mass fraction if the unburnt region
*
LECT NONE TERM
*
FANT 1.0 LECT bidon TERM
LINK COUP BLOQ 1 LECT p0 p0p pl plp TERM
    BLOQ 2 LECT bar TERM
ECRI COOR DEPL VITE ACCE FEXT CONT ECRO TFRE 0.3E-3
    FICH ALIC TEMP FREQ 1
        POIN LECT pa pmid pb TERM
        ELEM LECT ea eb TERM
        FICH ALIC TFRE 1.0E-5
OPTI NOTE STEP IO
    AMOR QUAD 4.0 LINE 0.2
    csta 0.25
    log 1
CALC TINI 0. TEND 0.60E-3
=====
SUIT
Post-treatment (space curves from alice file)
ECHO
RESU ALIC GARD PSCR
COMP NGRO 1 'xaxo' LECT 1 PAS 1 101 TERM
SORT GRAP
!PERF 'fetrol1.pun'
AXTE 1.0 'Time [s]'
*
* Attention: le SUPP /LECT/ est **mandatoire** dans les directives ci-dessous
* car sinon on risque de traiter les noeuds de l'element "bidon" comme
* faisant partie de l'abscisse curviligne (qui doit etre basee seulement
* sur les TRIA)
* En general, il est toujours une bonne idee de specifier le SUPPort,
* s'il y a des doutes ...
*
SCOU 61 'p_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    SUPP LECT bar TERM
    ECRO COMP 1
SCOU 62 'ro_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    SUPP LECT bar TERM
    ECRO COMP 2
SCOU 65 'vx_61' NSTO 61 SAXE 1.0 'curr_abscissa' LECT xaxo TERM
    SUPP LECT bar TERM
    VITE COMP 1
DCOU 71 'p_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 1
DCOU 72 'r_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 2
DCOU 75 'v_ana' SHTU GAMM 1.5 ROM 10 ROP 1 EINT 2.0E5 LENM 0.5 LENP 0.5
    TIME 0.60E-3 NRAR 30 VARI 5
TRAC 61 71 AXES 1.0 'PRESS. [PA]'
COLO NOIR ROUG
LIST 61 AXES 1.0 'PRESS. [PA]'
TRAC 62 72 AXES 1.0 'DENS. [KG/M3]'
COLO NOIR ROUG
LIST 62 AXES 1.0 'DENS. [KG/M3]'
TRAC 65 75 AXES 1.0 'VELOC. [M/S]'
COLO NOIR ROUG
LIST 65 AXES 1.0 'VELOC. [M/S]'
*
QUAL ECRO COMP 1 LECT ea TERM REFE 9.99949E+5 TOLE 2.E-2
    ECRO COMP 1 LECT eb TERM REFE 2.81068E+5 TOLE 2.E-2
    ECRO COMP 2 LECT ea TERM REFE 9.99966E+0 TOLE 2.E-2
    ECRO COMP 2 LECT eb TERM REFE 1.92601E+0 TOLE 2.E-2
=====
SUIT
Post treatment (BMPs from alice file)
ECHO
RESU ALIC GARD PSCR
OPTI PRIN
SORT VISU NSTO 61
PLAY
CAME 1 EYE 5.00000E-01 5.00000E-03 3.00015E-01
!
    Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
    VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
    RIGH 1.00000E+00 0.00000E+00 0.00000E+00
    UP 0.00000E+00 1.00000E+00 0.00000E+00
    FOV 5.25000E+01
SCEN GEOM NAVI FREE
    LINE HEBOU
    ISO FILL FIEL VITE SCAL USER PROG 20 PAS 20 280 TERM
    SUPP LECT bar TERM
    TEXT ISCA
    COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP OBJE LECT bar TERM REND
SCEN GEOM NAVI FREE
    LINE HEBOU
    ISO FILL FIEL ECRO 2 SCAL USER PROG 1 PAS 0.6 8.8 TERM
    SUPP LECT bar TERM
    TEXT ISCA
    COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS SIZE 1400 400 FICH BMP OBJE LECT bar TERM REND
ENDPLAY
=====
FIN
=====



---



pxhex2t2.proc



---



```

'DEBPROC' pxhex2t2 hexa*MAILLAGE';
*
*-----
* Splits a hexahedron into 24 tetrahedra.
* First, the hexahedron is split into 6 pyramids,
* one for each face, by introducing an extra node
* at the centre of the hexahedron.
* Then, each pyramid is split into 4 tetrahedra,
* by adding an extra node at the centre of the

```


```

```

* corresponding face of the hexahedron.
* This produces twice as much tetrahedra as
* the procedure pxhex2te, and they are worse
* shaped (thinner), but the advantage
* is that the resulting mesh is symmetric.
*
* Input :
* -----
*      hexa : a mesh containing just one hexahedron
* Output :
* -----
*      tetr : mesh containing 24 tetrahedra
* -----
hh = chan poil hexa;
*h = hh elem 1;
*
p1 = hh poin 1;
p2 = hh poin 2;
p3 = hh poin 3;
p4 = hh poin 4;
p5 = hh poin 5;
p6 = hh poin 6;
p7 = hh poin 7;
p8 = hh poin 8;
*
n1 = noeul p1;
n2 = noeul p2;
n3 = noeul p3;
n4 = noeul p4;
n5 = noeul p5;
n6 = noeul p6;
n7 = noeul p7;
n8 = noeul p8;
*
x1 y1 z1 = coor p1;
x2 y2 z2 = coor p2;
x3 y3 z3 = coor p3;
x4 y4 z4 = coor p4;
x5 y5 z5 = coor p5;
x6 y6 z6 = coor p6;
x7 y7 z7 = coor p7;
x8 y8 z8 = coor p8;
*
x9 = (x1 + x2 + x3 + x4 + x5 + x6 + x7 + x8) / 8.0;
y9 = (y1 + y2 + y3 + y4 + y5 + y6 + y7 + y8) / 8.0;
z9 = (z1 + z2 + z3 + z4 + z5 + z6 + z7 + z8) / 8.0;
*
p9 = x9 y9 z9;
*
* Pyramid # 1
*
x10 = (x1 + x2 + x3 + x4) / 4.0;
y10 = (y1 + y2 + y3 + y4) / 4.0;
z10 = (z1 + z2 + z3 + z4) / 4.0;
*
p10 = x10 y10 z10;
t1 = manu tet4 p1 p2 p10 p9;
t2 = manu tet4 p2 p3 p10 p9;
t3 = manu tet4 p3 p4 p10 p9;
t4 = manu tet4 p4 p1 p10 p9;
*
* Pyramid # 2
*
x11 = (x1 + x2 + x5 + x6) / 4.0;
y11 = (y1 + y2 + y5 + y6) / 4.0;
z11 = (z1 + z2 + z5 + z6) / 4.0;
*
p11 = x11 y11 z11;
t5 = manu tet4 p2 p1 p11 p9;
t6 = manu tet4 p6 p2 p11 p9;
t7 = manu tet4 p5 p6 p11 p9;
t8 = manu tet4 p1 p5 p11 p9;
*
* Pyramid # 3
*
x12 = (x2 + x3 + x6 + x7) / 4.0;
y12 = (y2 + y3 + y6 + y7) / 4.0;
z12 = (z2 + z3 + z6 + z7) / 4.0;
*
p12 = x12 y12 z12;
t9 = manu tet4 p3 p2 p12 p9;
t10 = manu tet4 p7 p3 p12 p9;
t11 = manu tet4 p6 p7 p12 p9;
t12 = manu tet4 p2 p6 p12 p9;
*
* Pyramid # 4
*
x13 = (x3 + x4 + x7 + x8) / 4.0;
y13 = (y3 + y4 + y7 + y8) / 4.0;
z13 = (z3 + z4 + z7 + z8) / 4.0;
*
p13 = x13 y13 z13;
t13 = manu tet4 p4 p3 p13 p9;
t14 = manu tet4 p3 p7 p13 p9;
t15 = manu tet4 p7 p8 p13 p9;
t16 = manu tet4 p8 p4 p13 p9;
*
* Pyramid # 5
*
x14 = (x1 + x4 + x5 + x8) / 4.0;
y14 = (y1 + y4 + y5 + y8) / 4.0;
z14 = (z1 + z4 + z5 + z8) / 4.0;
*
p14 = x14 y14 z14;
t17 = manu tet4 p1 p4 p14 p9;
t18 = manu tet4 p4 p8 p14 p9;
t19 = manu tet4 p8 p5 p14 p9;
t20 = manu tet4 p5 p1 p14 p9;
*
* Pyramid # 6
*
x15 = (x5 + x6 + x7 + x8) / 4.0;
y15 = (y5 + y6 + y7 + y8) / 4.0;
z15 = (z5 + z6 + z7 + z8) / 4.0;
*
p15 = x15 y15 z15;
t21 = manu tet4 p6 p5 p15 p9;
*
t22 = manu tet4 p7 p6 p15 p9;
t23 = manu tet4 p8 p7 p15 p9;
t24 = manu tet4 p5 p8 p15 p9;
*
tetr = t1 et t2 et t3 et t4 et t5 et t6
      et t7 et t8 et t9 et t10 et t11 et t12
      et t13 et t14 et t15 et t16 et t17 et t18
      et t19 et t20 et t21 et t22 et t23 et t24;
*
finproc tetr;

```

## pxhex2te.proc

```

'DEBCPROC' pxhex2te hexa*'MAILLAGE';
*
* -----
* Splits a hexahedron into 12 tetrahedra.
* First, the hexahedron is split into 6 pyramids,
* one for each face, by introducing an extra node
* at the centre of the hexahedron.
* Then, each pyramid is split into 2 tetrahedra.
* This is done along the plane that passes
* across the node (on the 4-node face of the pyramid)
* with the LOWEST global index, thus possible
* neighbours on the other side of the face will
* be split consistently.
* The advantage of this algorithm is that it is
* independent from the neighbours and yields
* consistent tetrahedra (faces are coincident).
*
* Input :
* -----
*      hexa : a mesh containing just one hexahedron
* Output :
* -----
*      tetr : mesh containing 12 tetrahedra
* -----
hh = chan poil hexa;
*h = hh elem 1;
*
p1 = hh poin 1;
p2 = hh poin 2;
p3 = hh poin 3;
p4 = hh poin 4;
p5 = hh poin 5;
p6 = hh poin 6;
p7 = hh poin 7;
p8 = hh poin 8;
*
n1 = noeul p1;
n2 = noeul p2;
n3 = noeul p3;
n4 = noeul p4;
n5 = noeul p5;
n6 = noeul p6;
n7 = noeul p7;
n8 = noeul p8;
*
x1 y1 z1 = coor p1;
x2 y2 z2 = coor p2;
x3 y3 z3 = coor p3;
x4 y4 z4 = coor p4;
x5 y5 z5 = coor p5;
x6 y6 z6 = coor p6;
x7 y7 z7 = coor p7;
x8 y8 z8 = coor p8;
*
x9 = (x1 + x2 + x3 + x4 + x5 + x6 + x7 + x8) / 8.0;
y9 = (y1 + y2 + y3 + y4 + y5 + y6 + y7 + y8) / 8.0;
z9 = (z1 + z2 + z3 + z4 + z5 + z6 + z7 + z8) / 8.0;
*
p9 = x9 y9 z9;
*
* Pyramid # 1
*
x10 = (x1 + x2 + x3 + x4) / 4.0;
y10 = (y1 + y2 + y3 + y4) / 4.0;
z10 = (z1 + z2 + z3 + z4) / 4.0;
*
p10 = x10 y10 z10;
t1 = manu tet4 p1 p2 p10 p9;
t2 = manu tet4 p2 p3 p10 p9;
t3 = manu tet4 p3 p4 p10 p9;
t4 = manu tet4 p4 p1 p10 p9;
*
* Pyramid # 2
*
x11 = (x1 + x2 + x5 + x6) / 4.0;
y11 = (y1 + y2 + y5 + y6) / 4.0;
z11 = (z1 + z2 + z5 + z6) / 4.0;
*
p11 = x11 y11 z11;
t5 = manu tet4 p2 p1 p11 p9;
t6 = manu tet4 p6 p2 p11 p9;
t7 = manu tet4 p5 p6 p11 p9;
t8 = manu tet4 p1 p5 p11 p9;
*
* Pyramid # 3
*
x12 = (x2 + x3 + x6 + x7) / 4.0;
y12 = (y2 + y3 + y6 + y7) / 4.0;
z12 = (z2 + z3 + z6 + z7) / 4.0;
*
p12 = x12 y12 z12;
t9 = manu tet4 p3 p2 p12 p9;
t10 = manu tet4 p7 p3 p12 p9;
t11 = manu tet4 p6 p7 p12 p9;
t12 = manu tet4 p2 p6 p12 p9;
*
* Pyramid # 4
*
x13 = (x3 + x4 + x7 + x8) / 4.0;
y13 = (y3 + y4 + y7 + y8) / 4.0;
z13 = (z3 + z4 + z7 + z8) / 4.0;
*
p13 = x13 y13 z13;
t13 = manu tet4 p4 p3 p13 p9;
t14 = manu tet4 p3 p7 p13 p9;
t15 = manu tet4 p7 p8 p13 p9;
t16 = manu tet4 p8 p4 p13 p9;
*
* Pyramid # 5
*
x14 = (x1 + x4 + x5 + x8) / 4.0;
y14 = (y1 + y4 + y5 + y8) / 4.0;
z14 = (z1 + z4 + z5 + z8) / 4.0;
*
p14 = x14 y14 z14;
t17 = manu tet4 p1 p4 p14 p9;
t18 = manu tet4 p4 p8 p14 p9;
t19 = manu tet4 p8 p5 p14 p9;
t20 = manu tet4 p5 p1 p14 p9;
*
* Pyramid # 6
*
x15 = (x5 + x6 + x7 + x8) / 4.0;
y15 = (y5 + y6 + y7 + y8) / 4.0;
z15 = (z5 + z6 + z7 + z8) / 4.0;
*
p15 = x15 y15 z15;
t21 = manu tet4 p6 p5 p15 p9;
*
t22 = manu tet4 p7 p6 p15 p9;
t23 = manu tet4 p8 p7 p15 p9;
t24 = manu tet4 p5 p8 p15 p9;
*
tetr = t1 et t2 et t3 et t4 et t5 et t6
      et t7 et t8 et t9 et t10 et t11 et t12
      et t13 et t14 et t15 et t16 et t17 et t18
      et t19 et t20 et t21 et t22 et t23 et t24;
*
finproc tetr;

```

```

*
* Pyramid # 4
*
nlow = n4; ilow = 1;
si ( n1 < nlow ) ; nlow = n1; ilow = 2; finsi;
si ( n5 < nlow ) ; nlow = n5; ilow = 1; finsi;
si ( n8 < nlow ) ; nlow = n8; ilow = 2; finsi;
si ( ilow ega 1 );
  t7 = manu tet4 p4 p8 p5 p9;
  t8 = manu tet4 p5 p1 p4 p9;
sinon;
  t7 = manu tet4 p1 p4 p8 p9;
  t8 = manu tet4 p8 p5 p1 p9;
finsi;
*
* Pyramid # 5
*
nlow = n1; ilow = 1;
si ( n2 < nlow ) ; nlow = n2; ilow = 2; finsi;
si ( n3 < nlow ) ; nlow = n3; ilow = 1; finsi;
si ( n4 < nlow ) ; nlow = n4; ilow = 2; finsi;
si ( ilow ega 1 );
  t9 = manu tet4 p1 p2 p3 p9;
  t10 = manu tet4 p3 p4 p1 p9;
sinon;
  t9 = manu tet4 p4 p1 p2 p9;
  t10 = manu tet4 p2 p3 p4 p9;
finsi;
*
* Pyramid # 6
*
nlow = n3; ilow = 1;
si ( n4 < nlow ) ; nlow = n4; ilow = 2; finsi;
si ( n8 < nlow ) ; nlow = n8; ilow = 1; finsi;
si ( n7 < nlow ) ; nlow = n7; ilow = 2; finsi;
si ( ilow ega 1 );
  t11 = manu tet4 p3 p7 p8 p9;
  t12 = manu tet4 p8 p4 p3 p9;
sinon;
  t11 = manu tet4 p4 p3 p7 p9;
  t12 = manu tet4 p7 p8 p4 p9;
finsi;
*
tetr = t1 et t2 et t3 et t4 et t5 et t6
      et t7 et t8 et t9 et t10 et t11 et t12;
*
finproc tetr;

```

**pxordpoi.proc**

```

$$$$ PXORDPOI
*
* pour ordonner une serie de points PLIN en partant de P1
*
* Input:
* =====
* PLIN = objet MAILLAGE de type POI1 (ligne de points)
* P1   = premier point de la ligne (typ POINT)
*
* Output:
* ======
* PORDO = objet MAILLAGE de type POI1 (ligne de points) contenant
*         les points ordonnees a partir de P1
*
'DEBPROC' PXORDPOI PLIN*'MAILLAGE' P1*'POINT' ;
-----
*
PORDO=P1;
PPA=P1;
NE='NBEL' PLIN;
*
I=0;
'REPETER' LAB1 (NE-1);
 I=I + 1;
* mess I;
PLIN= 'DIPP' ((PPA 'ET' PPA) 'ELEM' 1) PLIN;
PPA=PLIN 'POIN' 'PROC' PPA;
PORDO=PORDO 'ET' PPA;
'FIN' LAB1;
*
'FINPROC' PORDO;

```

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European Commission

**EUR 26632 EN – Joint Research Centre – Institute for the Protection and Security of the Citizen**

Title: Adaptivity in CEA's Fluid Elements in EUROPLEXUS

Authors: Folco Casadei, Martin Larcher, Georgios Valsamos

Luxembourg: Publications Office of the European Union

2014 – 43 pp. – 21.0 x 29.7 cm

EUR – Scientific and Technical Research series – ISSN 1831-9424

ISBN 978-92-79-37968-0

doi:10.2788/72737

#### **Abstract**

The present work completes the implementation of adaptivity routines by extending them to CEA's fluid finite elements both in 2D (TRIA and CAR1) and in 3D (TETR and CUBE). The CAR1 is treated like other 2D quadrilaterals (Q41L, FL24) as far as geometrical issues are concerned. In addition to the solid case, the activation of adaptivity for fluids requires the suitable treatment of transport terms which arise in the Eulerian or ALE forms of the governing equations. For the CEA's fluid finite elements mentioned above (TRIA, CAR1, TETR and CUBE) this is done in routines tr2me.ff (for the 2D case) and tr3me.ff (for the 3D case), respectively. Therefore, most modifications for the current implementation are concentrated in those two routines. Actually, a special version of the routines is written, valid for the mesh adaptive case.

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