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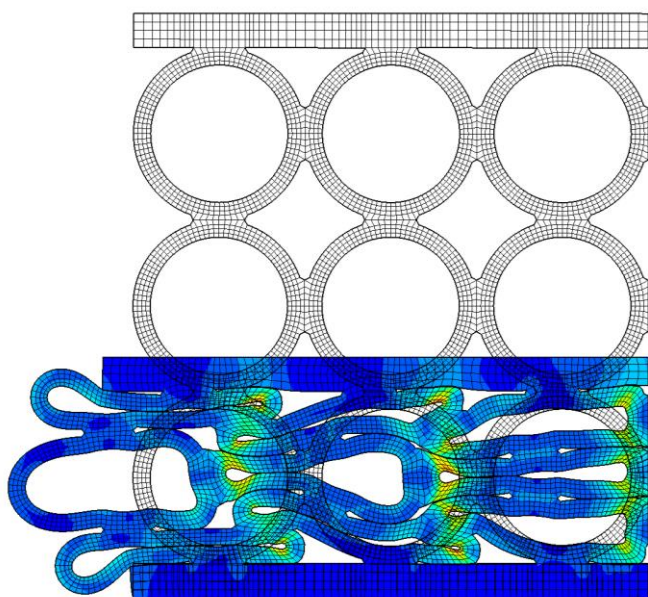
J R C T E C H N I C A L R E P O R T S

Pinball-based Contact-Impact Model with Parabolic Elements in EUROPLEXUS

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1. Introduction

Contact-impact algorithms are an important component of numerical simulation software in fast transient dynamics. Traditionally, contact algorithms have been based on so-called sliding lines and sliding surfaces, see e.g. the work of Hallquist and Benson [1-2].

However, sliding-based algorithms may present some difficulties in detecting contact in complex geometrical situations, especially in 3D. Therefore, starting from the mid-eighties, an alternative formulation based on a so-called pinball metaphor has been proposed by Belytschko and co-workers, see [4-10]. This approach is much more robust in detecting the contact.

The pinball contact-impact method has been implemented in EUROPLEXUS in [12-14], initially based upon a strong, Lagrange-multiplier based solution strategy of the contact constraints (see [11] for details of the method). Recently, the so-called Assembled Surface Normal (ASN) algorithm of Belytschko [3] and an alternative penalty-based solution of the contact constraints have also been introduced as an option in the code, see [15].

EUROPLEXUS [16] is a computer code for fast explicit transient dynamic analysis of fluid-structure systems jointly developed by the French Commissariat à l’Energie Atomique et aux Energies Alternatives (CEA Saclay) and by the Joint Research Centre of the European Commission (JRC Ispra).

Until now the pinball model was applicable only to linear-displacement elements, both of continuum and of structural (beam/shell) type. Recently, at Onera Lille (F) some crash calculations involving many contacts were attempted, initially with linear-displacement continuum elements (CAR4 in 2D). However, to improve accuracy and to help mitigate spurious locking phenomena, it was desired to perform the same calculations with parabolic elements [19], namely by the 9-node Lagrange element Q93.

The present work considers two different approaches to modeling contact with parabolic elements. The first approach uses a phantom mesh of linear-displacement elements, used only for contact detection, and superposed to the structural mesh made of parabolic elements. Such a technique is fully general and could be useful also in other special contact situations, not only with parabolic elements. The second approach is based on a (new) ‘native’ pinball formulation for the parabolic elements, which has now been developed and implemented in EUROPLEXUS.

This document is organized as follows:

- Section 2 presents the practical contact problem of interest, its solution with linear elements (including some solutions with an ALE formulation for solids) and its solution with parabolic elements using the phantom linear mesh for contact detection.

- Section 3 presents the new “native” pinball formulation for parabolic (continuum) elements, both in 2D (Q9 element shape, i.e. nine-node quadrilateral) and in 3D (C27 element shape, i.e. 27-node hexahedron). Some simple numerical examples are considered to check the new formulation.
- Section 4 presents the solution of the contact problem introduced in Section 2 by the new native parabolic pinball method.
- Some conclusions are given in Section 5.

The Appendix contains a listing of all the input files mentioned in the present report.

2. Practical contact problem

At Onera Lille a crash problem is being considered, in which a structure composed by an assembly of metallic rings is pressed between two metallic plates. A sketch of (a simplified version of) the problem in its initial configuration is given in Figure 1. A 2D plane strain analysis is performed and only one half of the structure is modelled thanks to symmetry.

The bottom plate is blocked in the vertical direction while the upper plate is subjected to an imposed displacement at constant velocity (apart from a short initial transient where the velocity is zero) of 1 mm/s. The model, shown in Figure 1, measures approximately 15 mm horizontally by 17 mm vertically. The final time of the calculation is set to 10 s, when the structure is completely crashed. The problem is therefore practically static and it can be anticipated that its solution with an explicit fast-transient dynamic code such as EUROPLEXUS will be expensive in terms of CPU time.

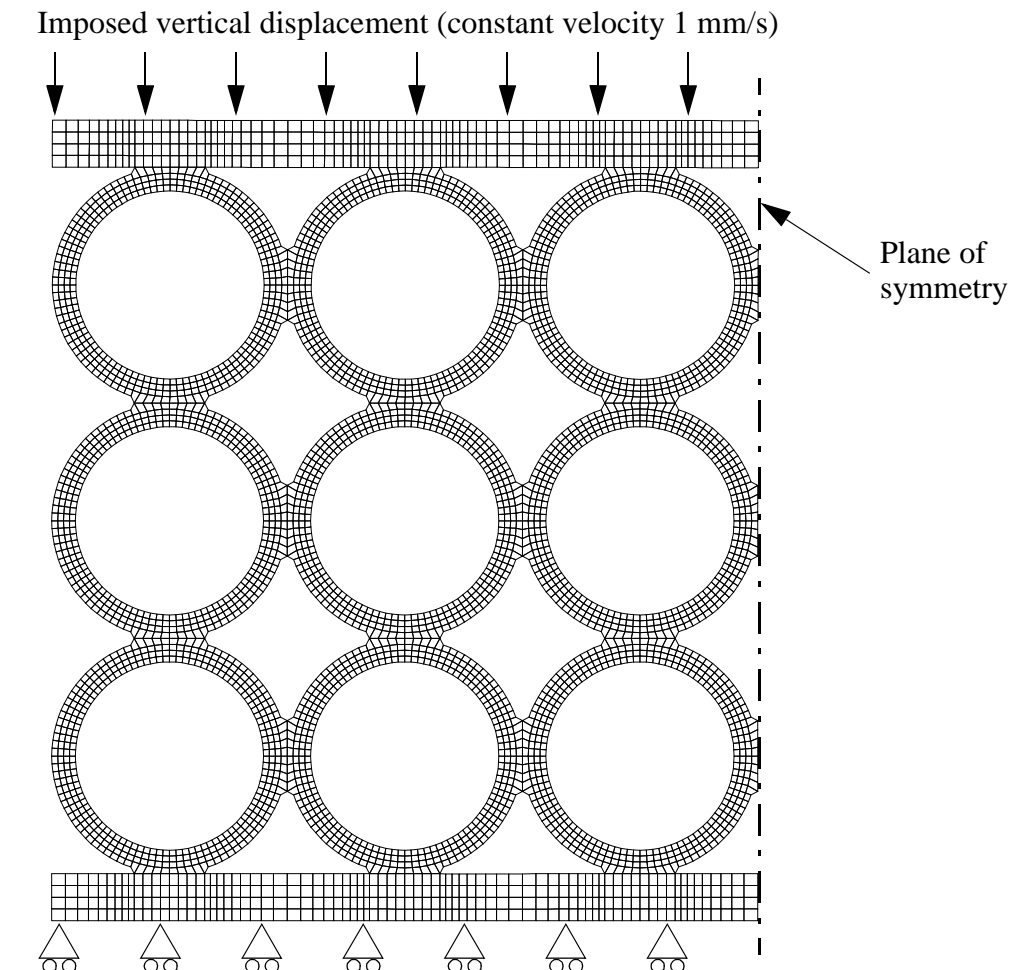


Figure 1 - Sketch of the structure crash problem (simplified version)

2.1 Solutions with CAR4 and CAR1

First, solutions are obtained with the linear-displacement elements. The CAR4 quadrilateral with 4 nodes and full integration (2×2 Gauss points) is employed. All performed calculations are summarized in Table 1.

Table 1 - Calculations of the structure crash problem by CAR4

Case	Mesh	Notes	Steps	CPU [s]	Els*step
CAR401	4080 CAR4	25 PINB SELF DMIN 0.1	741,850	5,463	3.03×10^9
CAR101	4080 CAR1	25 PINB SELF DMIN 0.1 CSTA 0.5	[1,000,000] t = 6.1 s	[6,803]	$[4, 1 \times 10^9]$
CAR102	4080 CAR1	25 PINB SELF DMIN 0.1 CSTA 0.5 NMAX 90000000	[1,387,817] t = 7.2 s	[9,977]	$[5.7 \times 10^9]$
CARM01	3264 CAR1 816 CAR4	1 PINB SELF DMIN 0.1 EQVF	[133,362] t = 0.75 s	[944]	$[5.4 \times 10^8]$
CARM02	3264 CAR1 816 CAR4	1 PINB SELF DMIN 0.1 EQVF CSTA 0.5	[1,813,754] t = 7.2 s	[14,386]	$[7.4 \times 10^9]$

CAR401

This calculation uses standard pinballs in the CAR4 elements. There are 25 zones with embedded pinballs, see Figure 2. Each of these is declared as a self-contacting body (PINB SELF). Hierarchic pinballs are activated by specifying a minimum pinball diameter of 0.1 mm (DMIN 0.1). A fast search of pinball contacts is activated for efficiency of the computation by the option OPTI PINS GRID.

CAR401
TIME: 0.00000E+00 STEP: 0

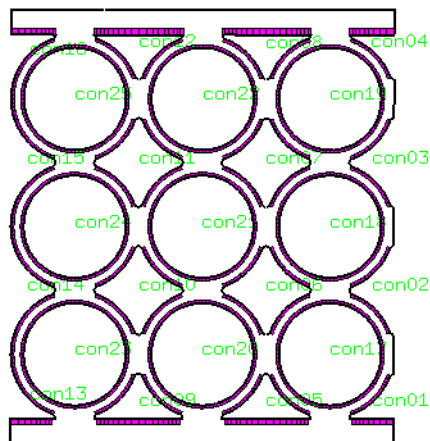


Figure 2 - Pinball zones

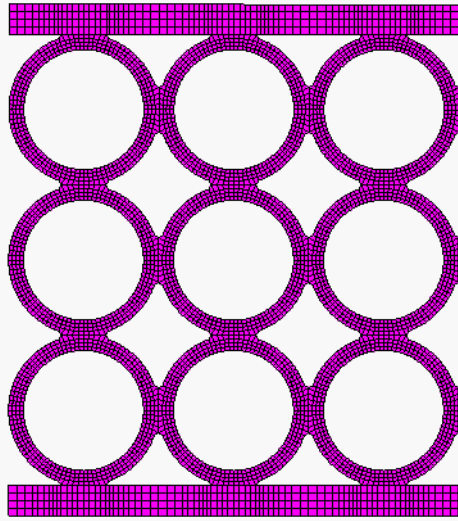
The progressive crushing of the structure (every 2.5 s) is illustrated in Figure 3. Figure 4 shows the final plastic strain. The first contacts appear at about 3.65 s. Figure 5 shows the final contacts in the structure. One can see that most of the contacts are physical, but there are some spurious self-contacts in the severely crashed internal parts of the rings (see inset in Figure 5), where the local radius of curvature becomes very small. This is due to the use of the `SELF` keyword, which allows self-contact between pinballs belonging to the same zone (i.e. to the same body), in contrast to the `BODY` keyword, that allows contact only between pinballs belonging to different bodies.

Figure 6 shows the imposed vertical displacement of the top plate which, as anticipated, was linear in time. Figure 7 shows the resulting crushing force vs. displacement of the top plate. The force is obtained by adding up all vertical nodal forces in the nodes on the upper part of the top plate.

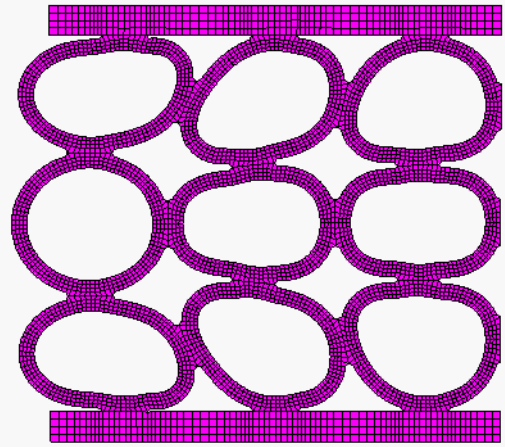
Since the experiment is quasi-static (very low crushing velocity) the effect of stress waves is very small and measuring the force on the bottom plate would give almost exactly the same result (apart from the sign of the force, of course). By comparison with some experimental results available at Onera, the crushing force has the right shape but it is too high (over-stiff behavior). This might be due to locking of the element and also partly (but to a much smaller extent) to the spurious contacts.

Hence, the interest in performing the same calculation with parabolic elements, which could be less prone to the locking phenomenon.

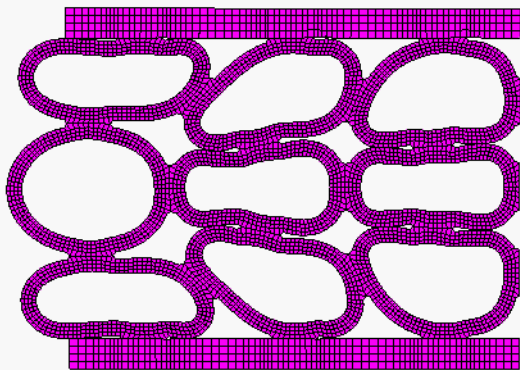
CAR401
TIME: 0.00000E+00 STEP: 0



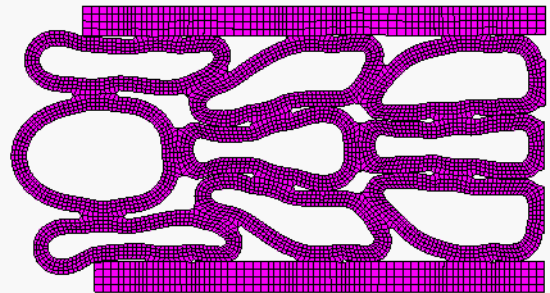
CAR401
TIME: 2.50000E+00 STEP: 147357



CAR401
TIME: 5.00000E+00 STEP: 310612



CAR401
TIME: 7.50000E+00 STEP: 501860



CAR401
TIME: 1.00000E+01 STEP: 741850

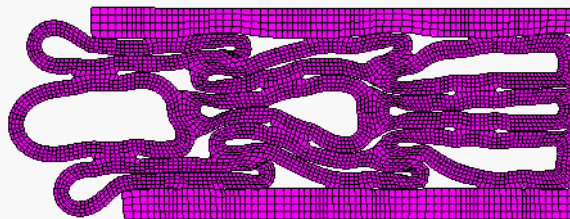


Figure 3 - Structure crushing in case CAR401

CAR401

TIME: 1.00000E+01 STEP: 741850

MAX: +1.54E+00

---: +7.00E-01

---: +6.50E-01

---: +6.00E-01

---: +5.50E-01

---: +5.00E-01

---: +4.50E-01

---: +4.00E-01

---: +3.50E-01

---: +3.00E-01

---: +2.50E-01

---: +2.00E-01

---: +1.50E-01

---: +1.00E-01

---: +5.00E-02

MIN: +0.00E+00

ECRO 3 [N/A]

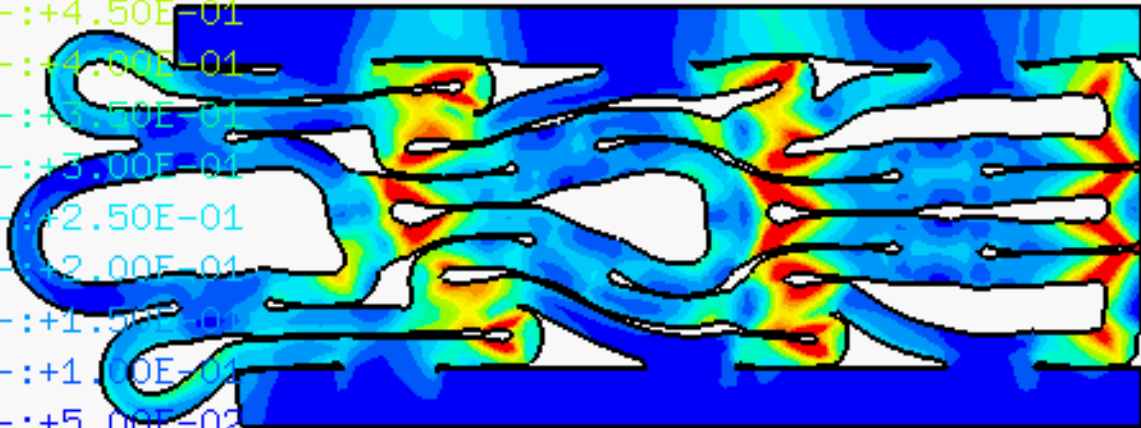


Figure 4 - Final plastic strain in case CAR401

CAR401

TIME: 1.00000E+01 STEP: 741850

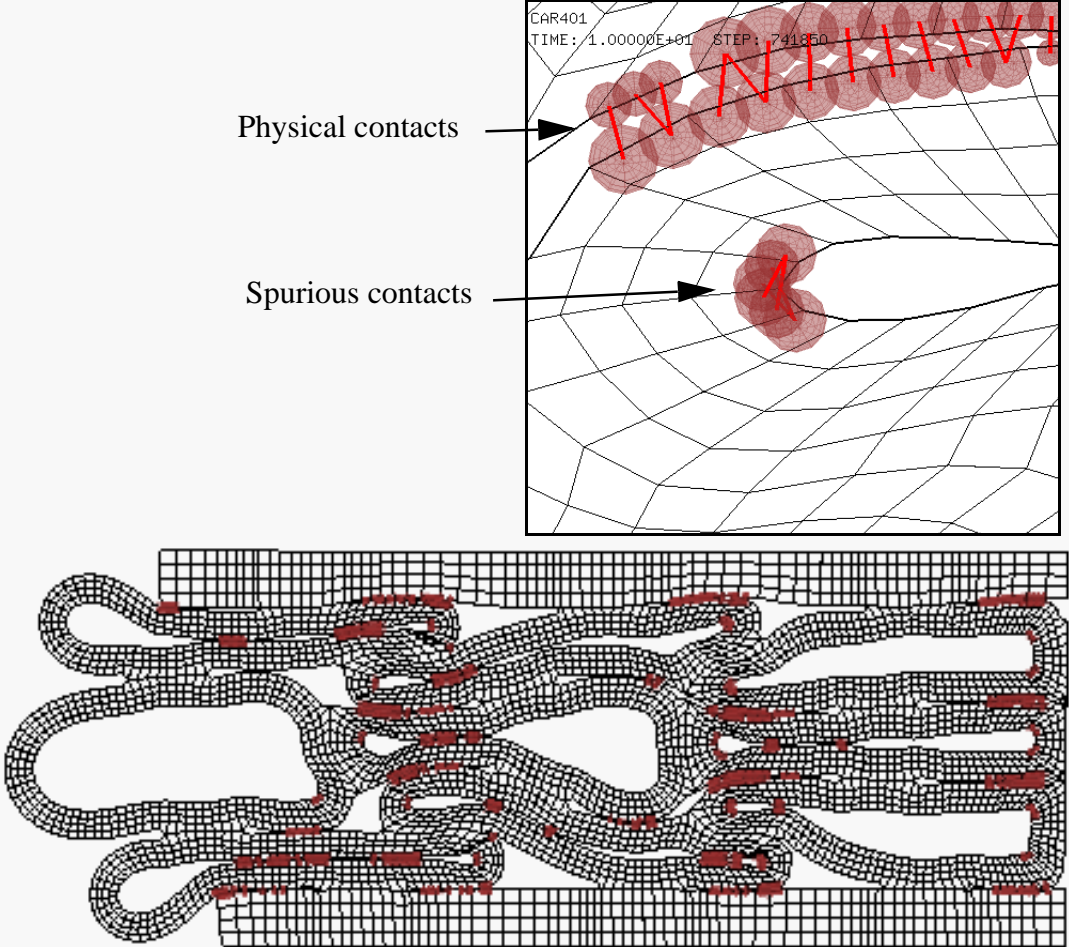


Figure 5 - Final contacts in case CAR401

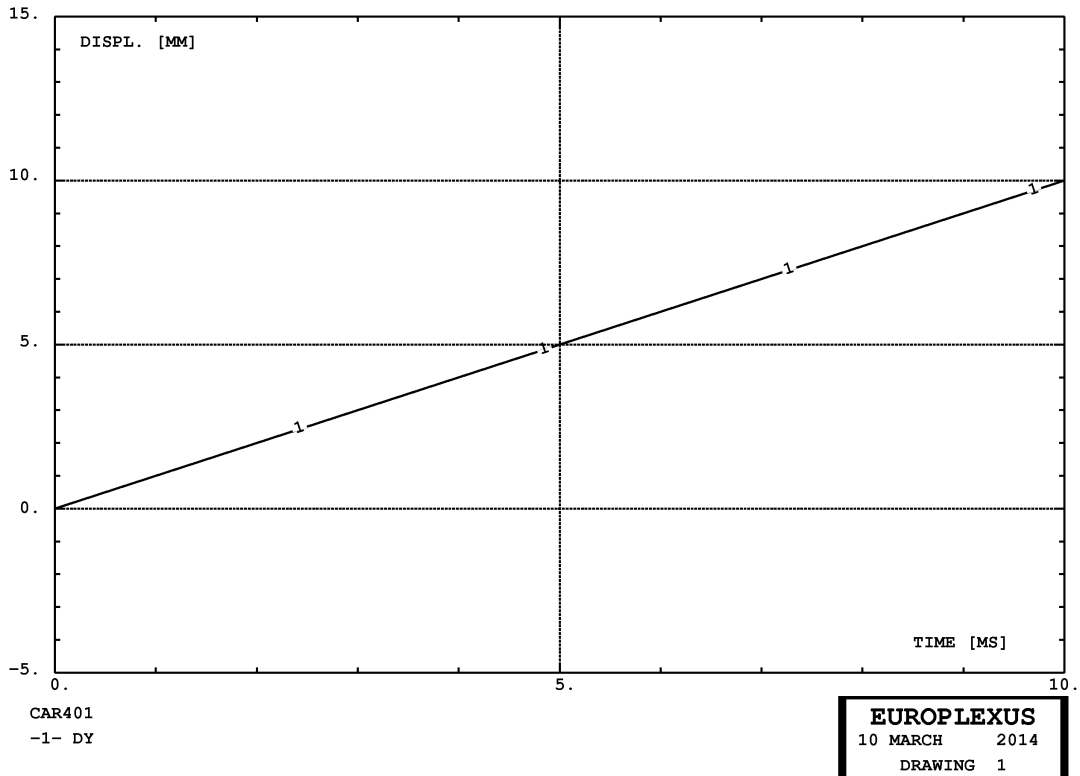


Figure 6 - Imposed displacement in case CAR401

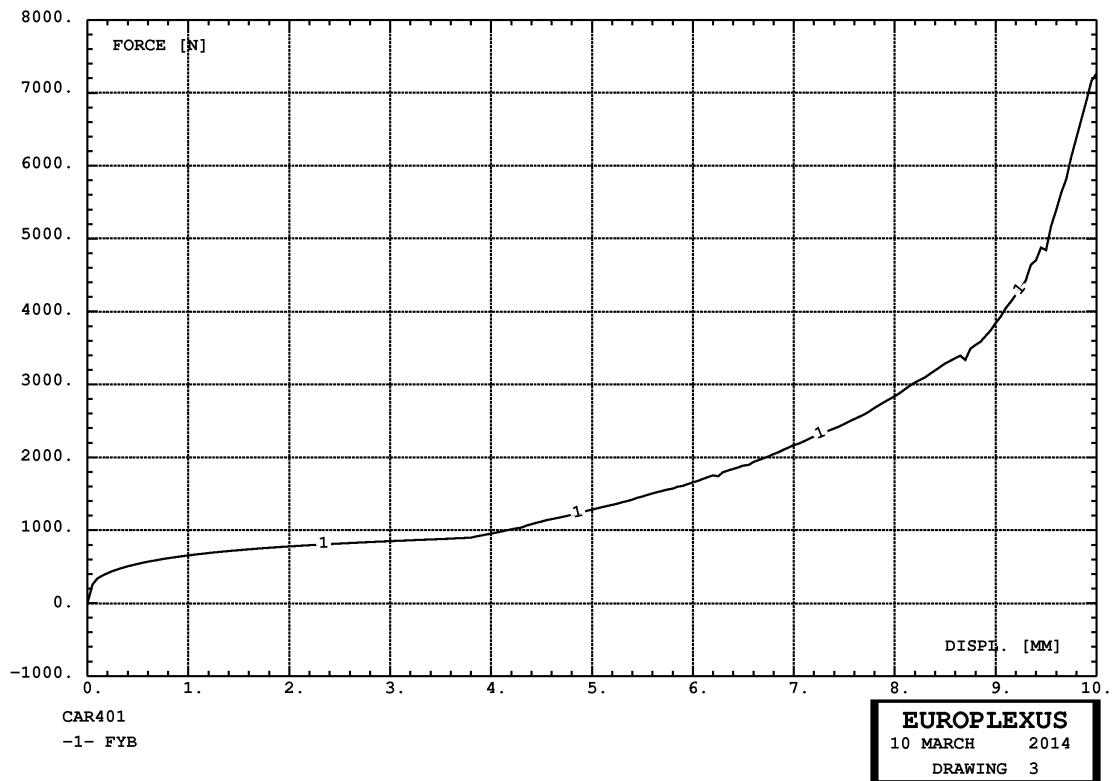


Figure 7 - Crushing force vs. imposed displacement in case CAR401

CAR101

This calculation is similar to CAR401 but uses the under-integrated linear quadrilateral CAR1 instead of the fully integrated CAR4. By using the standard critical step coefficient (CSTA 0.8) the calculation fails at step 142, time 1.4 ms, due to strong instabilities, as shown in Figures 8 (configuration), 9 (equivalent plastic strain) and 10 (spurious contacts).

By reducing the stability coefficient to CSTA 0.5 the calculation proceeds but stopped at step 1,000,000 which is the normal limit in EUROPLEXUS calculations, at time 6.1 s (it had been forgotten to increase this limit by specifying NMAX in the input file). Figure 11 shows the deformed shape and the contacts at this time. Some slight hourglassing is visible, but it is not likely to affect the results much. There are a few spurious contacts, as indicated by the red circles.

The equivalent plastic strain is shown in Figure 12 and reaches a maximum of about 46%.

CAR102

This calculation is identical to CAR101 (with CSTA 0.5) but NMAX 90000000 is specified in order to avoid premature stopping. The calculation was killed by hand at step 1,387,817, time 7.2 s, because the critical time step was decreasing rapidly (2.7×10^{-6} at that moment) so the calculation was not likely to be able to arrive at 10 s anyway.

Figure 13 shows the deformed configuration and the contacts at 7.2 s. Some hourglassing is evident, and this is probably one of the causes (together with strong folding) of the drastic decrease in stability step. The equivalent plastic strain is shown in Figure 14 and reaches a maximum of about 70%.

Finally, Figure 15 compares the crushing force with CAR4 (CAR401) and CAR1 (CAR102). The latter solution, although plagued by some mechanisms which make it fail prematurely, is much more ductile and in line with experimental results.

CARM01

This calculation is similar to CAR401 and CAR101 and uses a mixture of CAR1 and CAR4 elements in an attempt to obtain a solution without (strong) mechanisms, and as ductile as the case CAR102. One over every five elements is a CAR4, the remaining four being CAR1. The mixed mesh is obtained by a simple Cast3m procedure starting from the original CAR4 mesh (see Figure 16), where CAR4 elements are colored in red, CAR1 elements in green).

An initial attempt is done to run this case with the standard CSTA (0.8), which worked for case CAR401 (all CAR4). However, the calculation stopped at step 133,362 and time 0.75 s because of strong instabilities, see Figure 16. Some high spurious plastic strain develops because of the instability, see Figure 17.

CARM02

This calculation is identical to CARM01 but with CSTA 0.5. The calculation proceeded without instabilities, but it was intentionally stopped at step 1,813,754, time 7.2 s, because the critical step was becoming very low (1×10^{-6}), so that the calculation was unlikely to reach 10 s anyway.

Figure 18 shows the deformed mesh at time 7.2 s, Figure 19 shows the contacts (interestingly, there are no spurious contacts at this time), and Figure 20 shows the equivalent plastic strain, which attains a maximum value of 79%.

Indeed, this calculation shows very little overall hourglassing. Some hourglassing is still present in the strong folds, and this (combined with severe crushing) causes the drop of the stability step.

Finally, Figures 21 and 22 compare the crushing forces in the three solutions with linear quadrilaterals (CAR401, CAR102 and CARM02). Indeed, the two solutions with either CAR1 or a mix-up of CAR1 and CAR4 are in good agreement among them and in better agreement than the full CAR4 solution with the experimental results.

CAR101
TIME: 1.47527E-03 STEP: 142

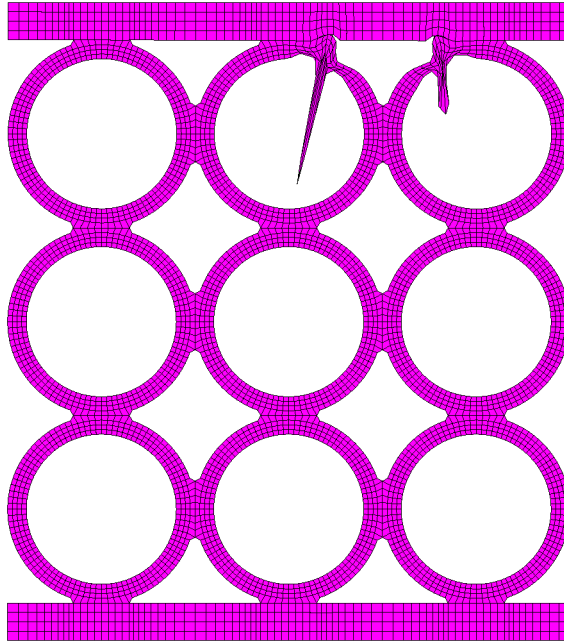


Figure 8 - Deformed shape with instabilities in case CAR101 with CSTA 0.8

CAR101
TIME: 1.47527E-03 STEP: 142

MAX: +9.81E+00
---: +9.46E+00
---: +8.78E+00
---: +8.06E+00
---: +7.36E+00
---: +6.66E+00
---: +5.96E+00
---: +5.28E+00
---: +4.59E+00
---: +3.89E+00
---: +3.19E+00
---: +2.49E+00
---: +1.79E+00
---: +1.09E+00
---: +3.80E-01
MIN: +0.00E+00
ECRO 3 [N/A]

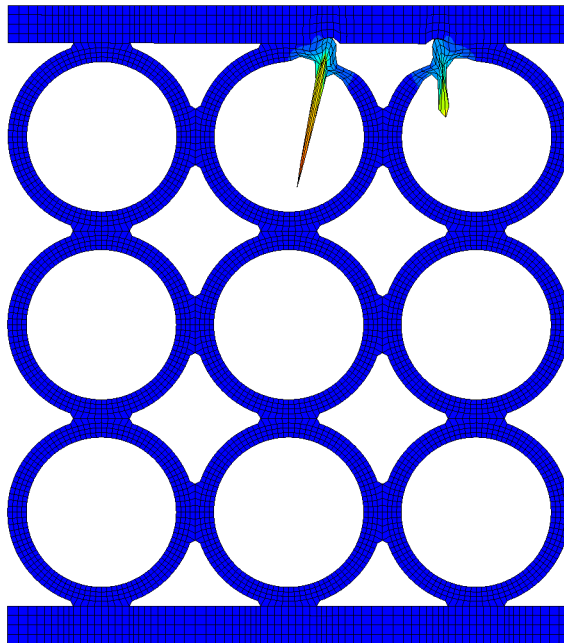


Figure 9 - Equivalent plastic strain in case CAR101 with CSTA 0.8

CAR101
TIME: 1.47527E-03 STEP: 142

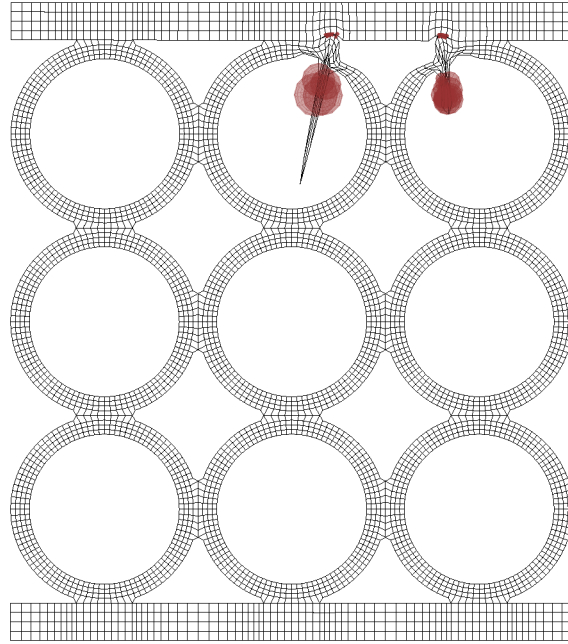


Figure 10 - Instabilities and spurious contacts in case CAR101 with CSTA 0.8

CAR101
TIME: 6.06745E+00 STEP: *****

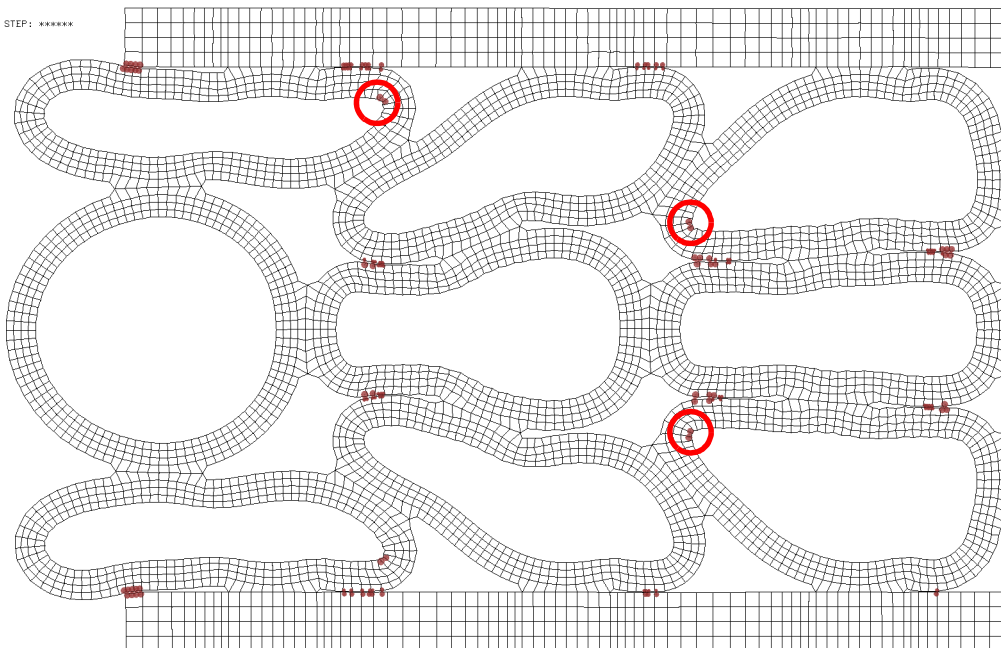


Figure 11 - Contacts in case CAR101 with CSTA 0.5 at 6.1 s

CAR101
TIME: 6.06749E+00 STEP: *****

MAX: +4.62E-01
---: +4.46E-01
---: +4.13E-01
---: +3.80E-01
---: +3.47E-01
---: +3.14E-01
---: +2.81E-01
---: +2.48E-01
---: +2.15E-01
---: +1.82E-01
---: +1.49E-01
---: +1.16E-01
---: +8.25E-02
---: +4.95E-02
---: +1.65E-02
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ECRO 3 [N/A]

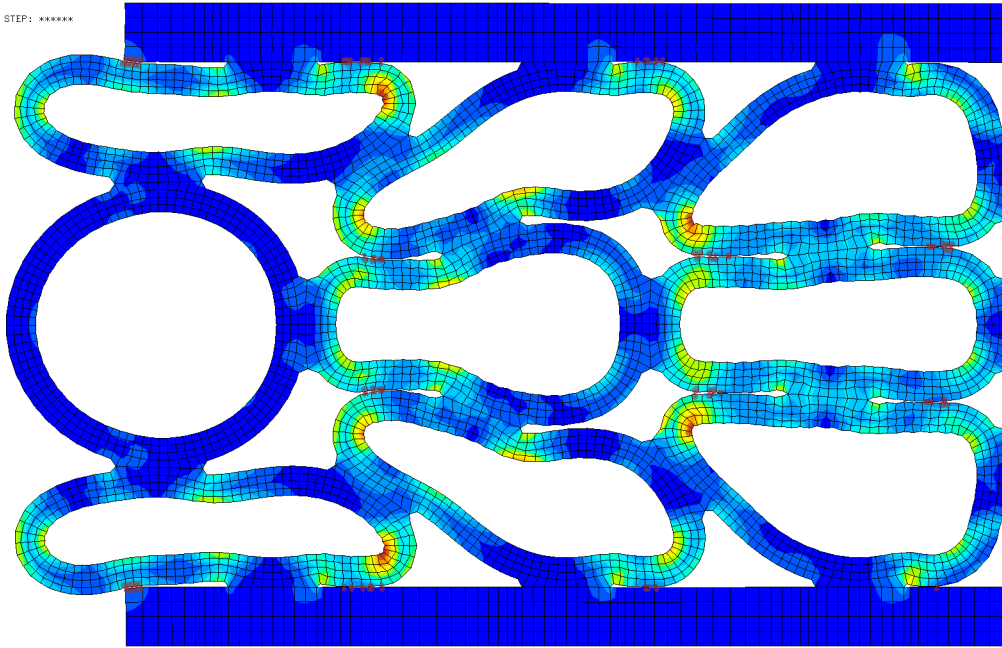


Figure 12 - Equivalent plastic strain in case CAR101 with CSTA 0.5 at 6.1 s

CAR102
TIME: 7.20000E+00 STEP: *****

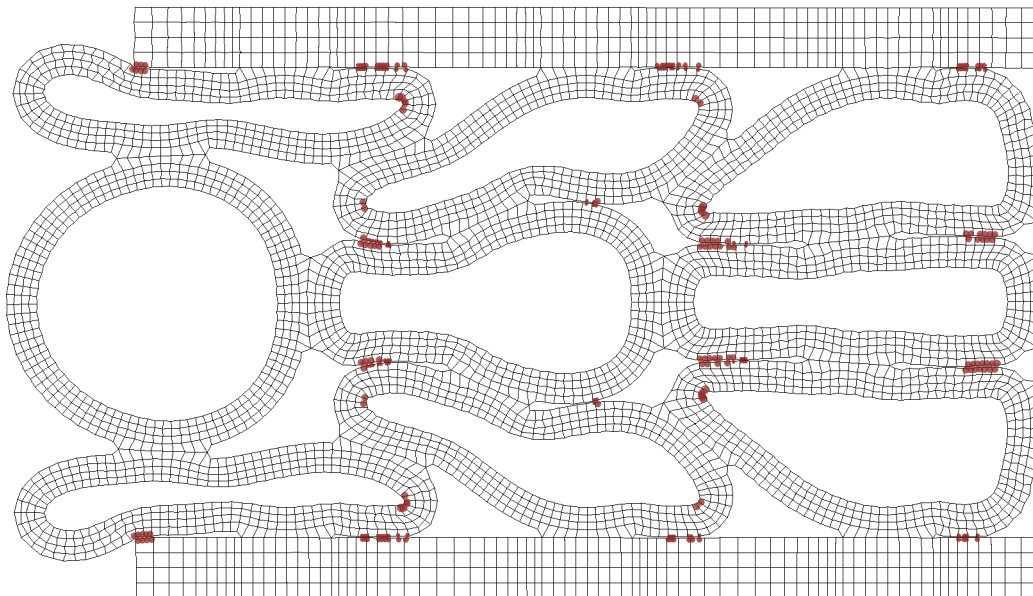


Figure 13 - Contacts in case CAR102 with CSTA 0.5 at 7.2 s

CAR102
 TIME: 7.20000E+00 STEP: *****

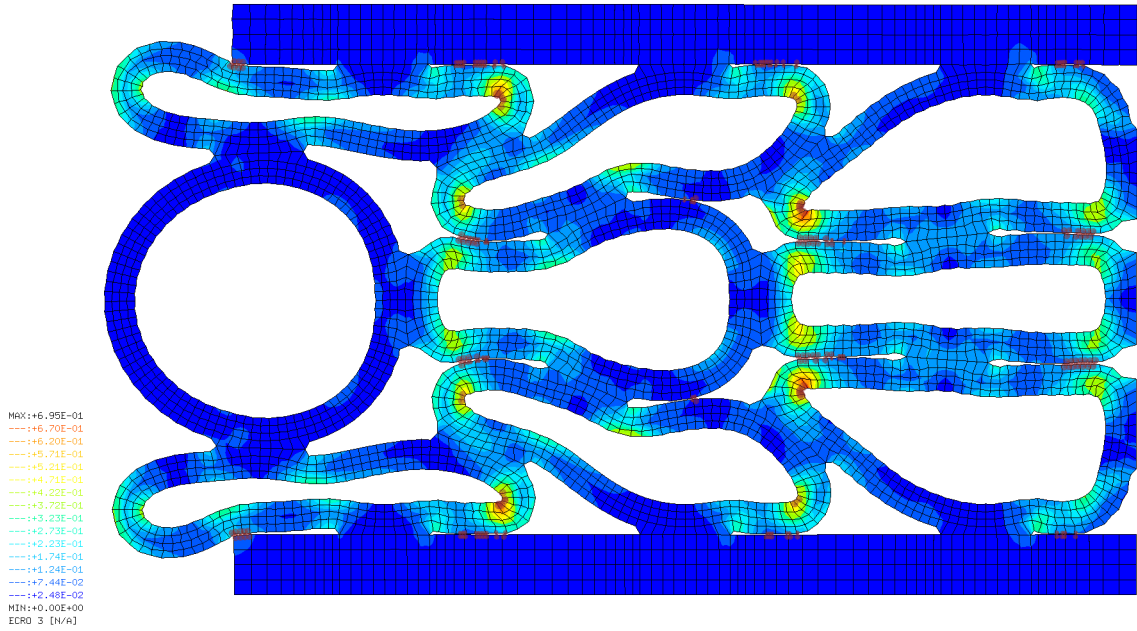


Figure 14 - Equivalent plastic strain in case CAR102 with CSTA 0.5 at 7.2 s

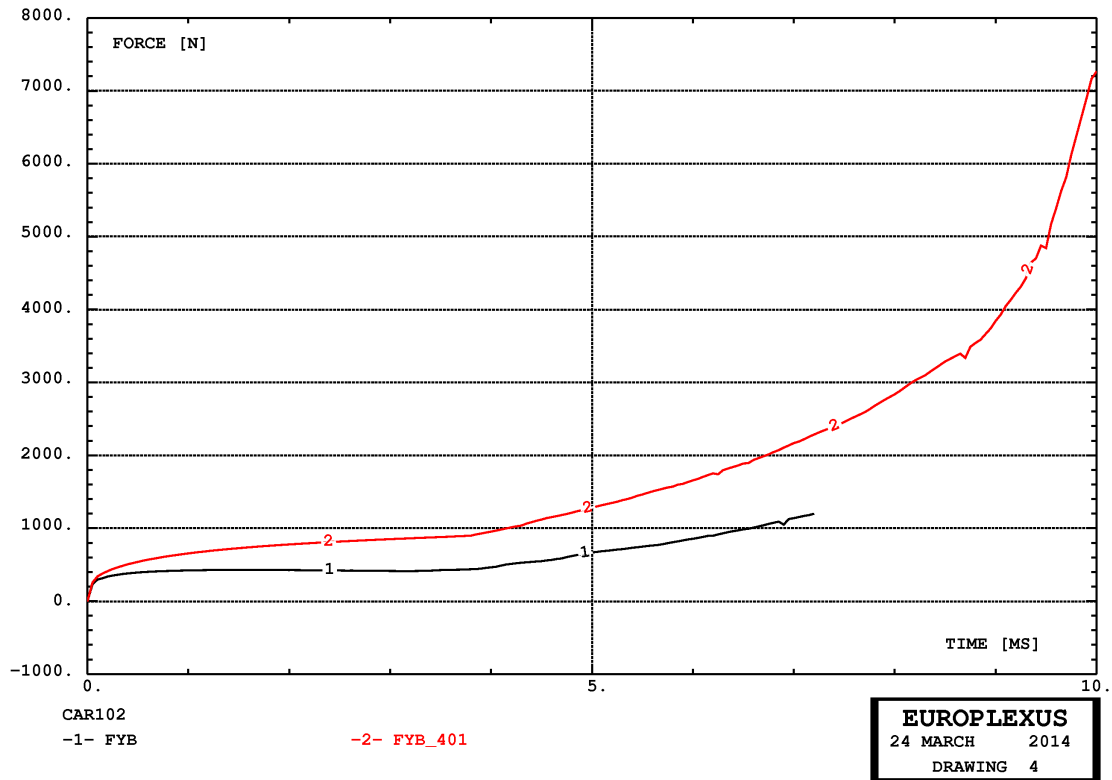


Figure 15 - Crushing force in case CAR102 compared with CAR401

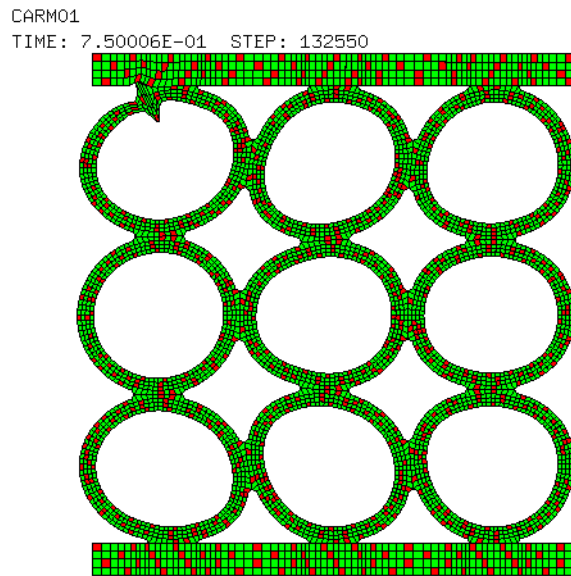


Figure 16 - Instabilities and spurious contacts in case CARM01 with CSTA 0.8

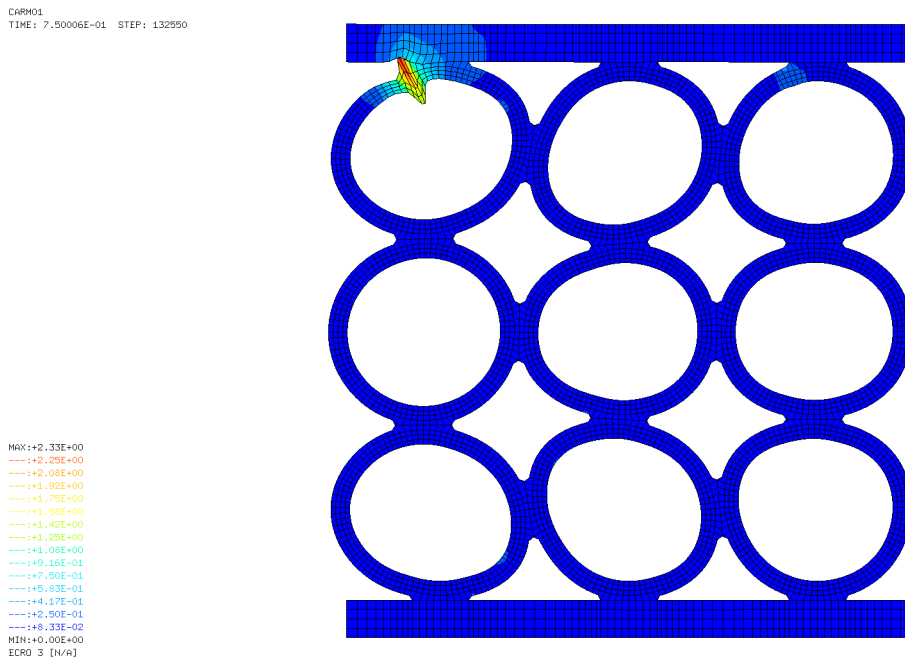


Figure 17 - Equivalent plastic strain in case CARM01 with CSTA 0.8

CARM02
TIME: 7.20000E+00 STEP: *****

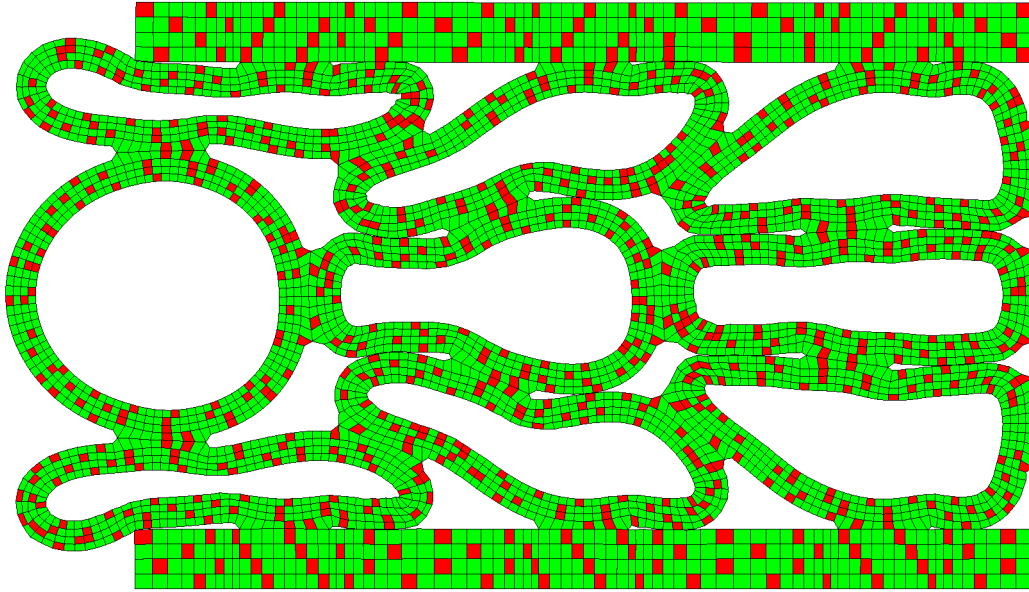


Figure 18 - Deformed mesh in case CARM02 with CSTA 0.5 at 7.2 s

CARM02
TIME: 7.20000E+00 STEP: *****

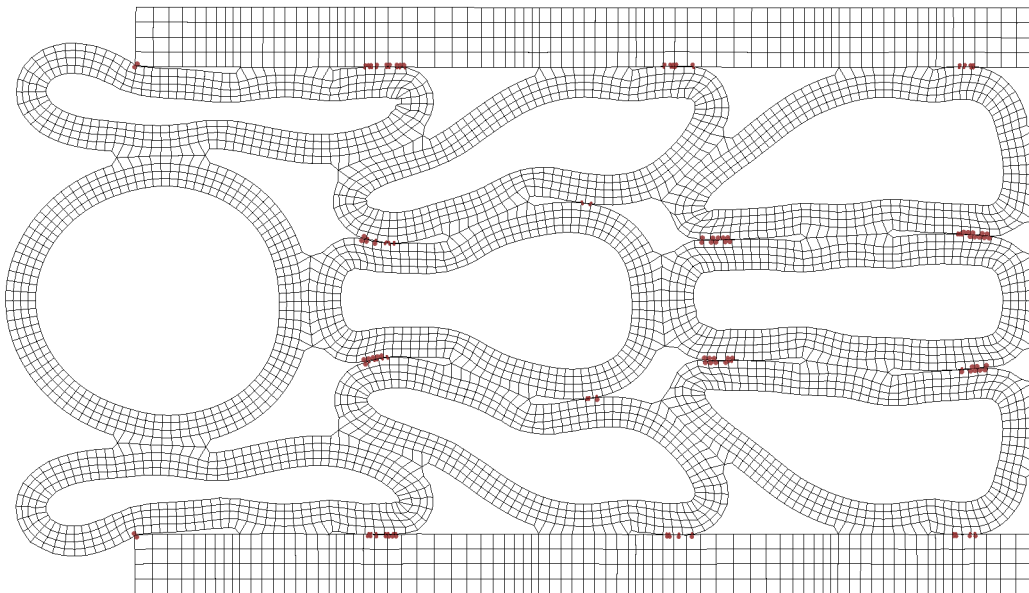


Figure 19 - Contacts in case CARM02 with CSTA 0.5 at 7.2 s

CARM02
 TIME: 7.20000E+00 STEP: *****

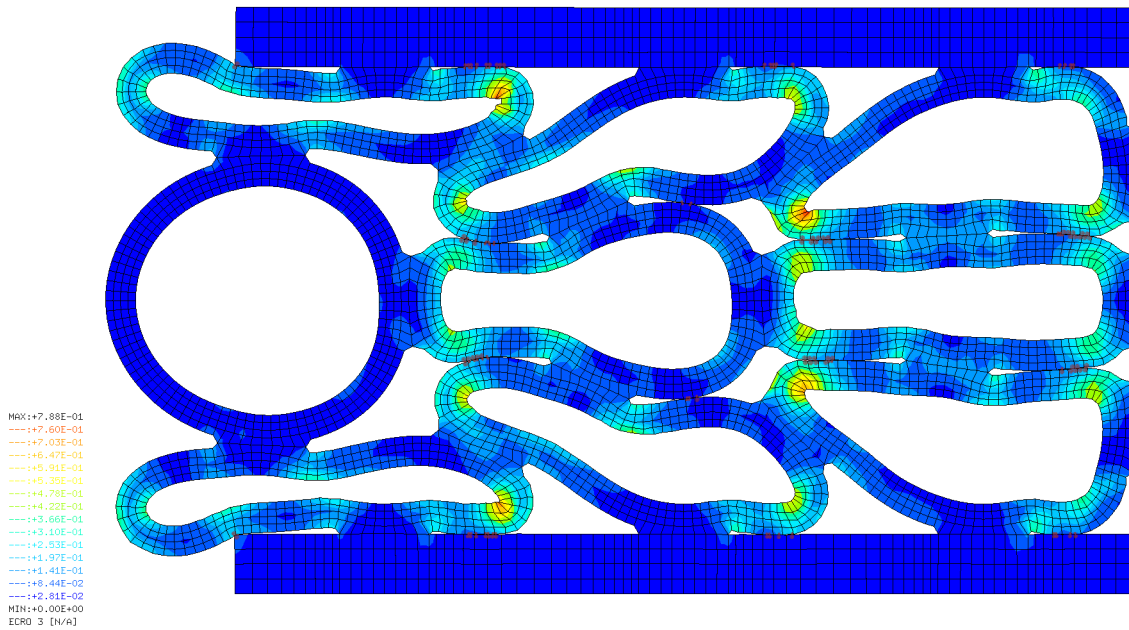


Figure 20 - Equivalent plastic strain in case CARM02 with CSTA 0.5 at 7.2 s

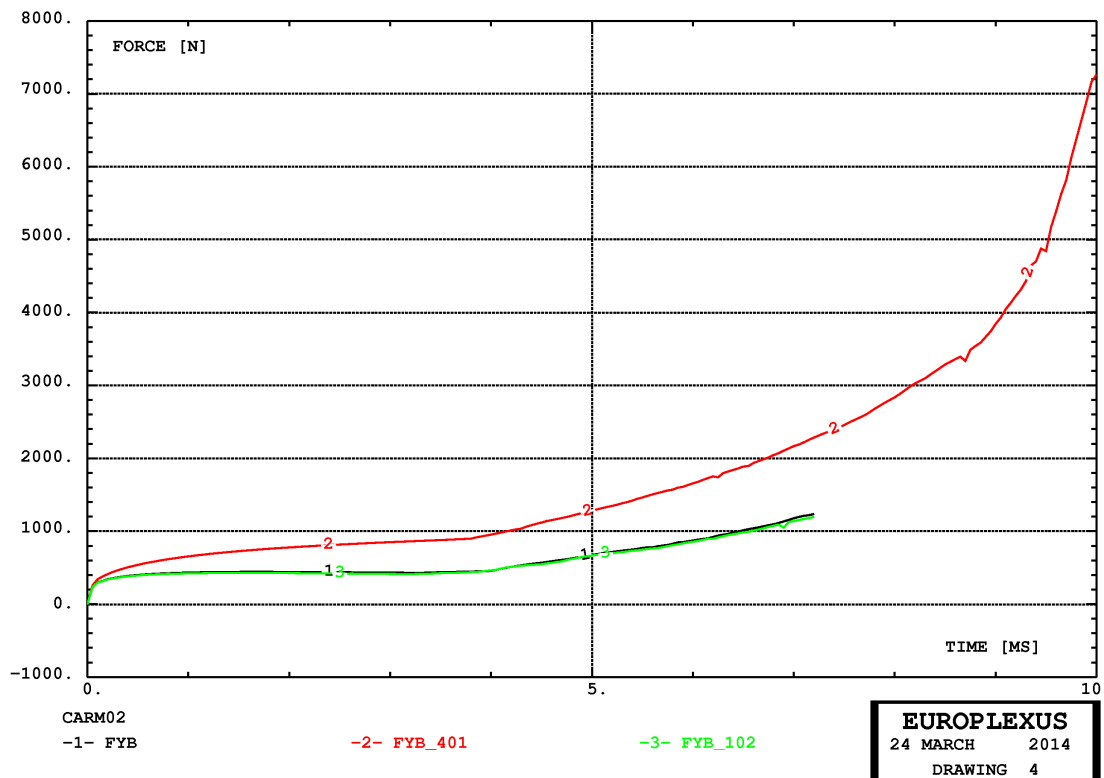


Figure 21 - Crushing force in case CARM02 compared with CAR401 and CAR102

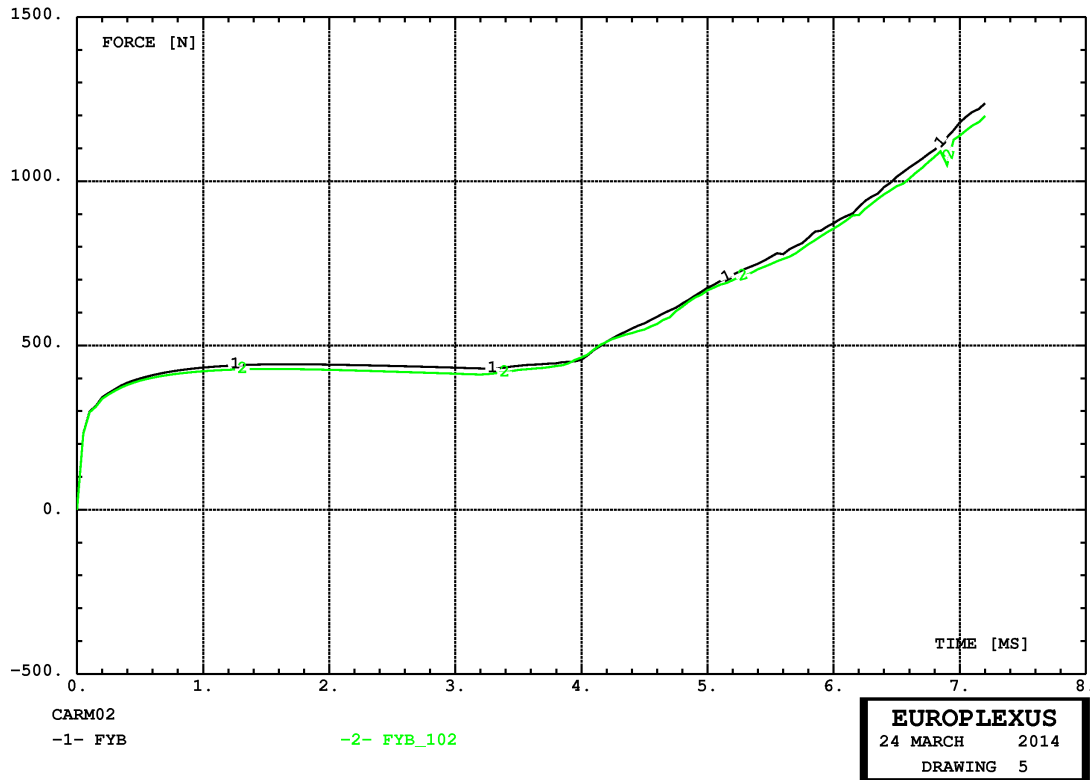


Figure 22 - Crushing force in case CARM02 compared with CAR102

2.2 ALE solutions

The simulations presented so far used a Lagrangian description of the continuum, whereby the mesh is “attached” to the material particles. This simplifies treatment of the structural problem, but suffers from a drastic reduction of the stability step as some of the elements (in the folds) get severely distorted, towards the end of the transient.

An alternative approach is to use an Arbitrary Lagrangian Eulerian (ALE) formulation, whereby the mesh moves in an arbitrary manner. Such technique is most commonly used with fluids, but an implementation for solid materials is present in EUROPLEXUS (although limited to 2D applications), see e.g. references [23-27].

All performed calculations are summarized in Table 2.

Table 2 - ALE calculations of the structure crash problem

Case	Mesh	Notes	Steps	CPU [s]	Els*step
CARA02	4080 Q42G	1 PINB SELF DMIN 0.1 PINS GRID EQVF CNOR	1,132,701	15,688	4.62×10^9
CARA03	4080 Q41N	1 PINB SELF DMIN 0.1 PINS GRID EQVF CNOR	[117,658] [1.06 s]	[886]	$[4.8 \times 10^8]$
CARA04	4080 Q42G	1 PINB SELF DMIN 0.1 PINS GRID EQVF CNOR crushing velocity 10 mm/s	114,118 1 s	1,929	$4,66 \times 10^8$
CARA05	4080 Q42G	1 PINB SELF DMIN 0.1 PINS GRID EQVF CNOR density 100 times larger	114,261 10 s	1,925	4.66×10^8
CARA06	4080 Q42N	1 PINB SELF DMIN 0.1 PINS GRID EQVF CNOR crushing velocity 10 mm/s	[102,455] 0.96 s	[1,762]	4.18×10^8
CARA07	4080 Q42	1 PINB SELF DMIN 0.1 PINS GRID EQVF CNOR crushing velocity 10 mm/s	90,068 1 s	1,618	3.67×10^8
CARA08	4080 Q41	1 PINB SELF DMIN 0.1 PINS GRID EQVF CNOR crushing velocity 10 mm/s	[23,705] 0.13 s	[304]	$[9.67 \times 10^7]$

CARA02

This calculation is similar to test CAR401 presented in Section 2.1, but uses the Q42G fully integrated four-node element in an ALE formulation. The mesh is read from a Cast3m file, produced via the READ operator (see file readq4.dgibi in Appendix) from the mesh embedded in the CAR401 input file.

For simplicity (of the user) a single zone of pinballs is declared (`SELF DMIN 0.1`) containing all the elements on the surface of the model (`elep` object, defined in `readq4.dgibi`).

Giuliani's automatic rezoning algorithm is used to drive the ALE mesh motion, i.e., for all nodes internal to the model. The nodes on the surface are Lagrangian.

Figure 23 shows the initial configuration with, highlighted, the surface nodes which are treated as Lagrangian. Figure 24 shows the final deformed configuration with the contacts. No spurious contacts (not even in the folds) are observed. Note how the mesh rezoning algorithm keeps the mesh more regular internally than in the Lagrangian solutions presented previously. Despite this, the calculation is more expensive in terms of CPU, partly because of the necessary transport calculation (which are avoided in Lagrangian), partly because the solution requires more steps. In fact, the critical time step becomes smaller than in the case CAR401 since the behavior of the model is more ductile (and thus in better overall agreement with the experiments), and very high local plasticization (perhaps not physical) is observed in the folds.

Figure 25 shows the final plastic strain distribution, which attains huge values (2,200%) at a tiny spot in a fold. The same map but at a slightly earlier time (8.85 s instead of 10 s) is shown in Figure 26, where the maximum strain is "only" 149%.

Figure 27 shows the crushing force as a function of the imposed displacement. Since the imposed displacement is linear in time (10 mm in 10 s), this curve also represents the crushing force in time (by just changing the horizontal scale units from mm to s). Figure 28 compares the upper and lower plate forces, with a change in sign to make the two directly comparable. The two curves are practically exactly superposed, showing that this case is static, i.e. wave propagation (and inertia forces) plays no role. Finally, Figure 29 compares the crushing forces of cases CAR401 (in red), CAR102 (in green) and CARA02 (present case, in black). The present solution is more ductile than the CAR4 solution, but stiffer than the CAR1 solution.

CARA03

This calculation is similar to test CARA02 but uses the Q41N reduced-integrated four-node element in an ALE formulation. The calculation stopped prematurely (at 1.06 s of physical time) due to strong mechanisms, see Figure 30.

CARA02
TIME: 0.00000E+00 STEP: 0

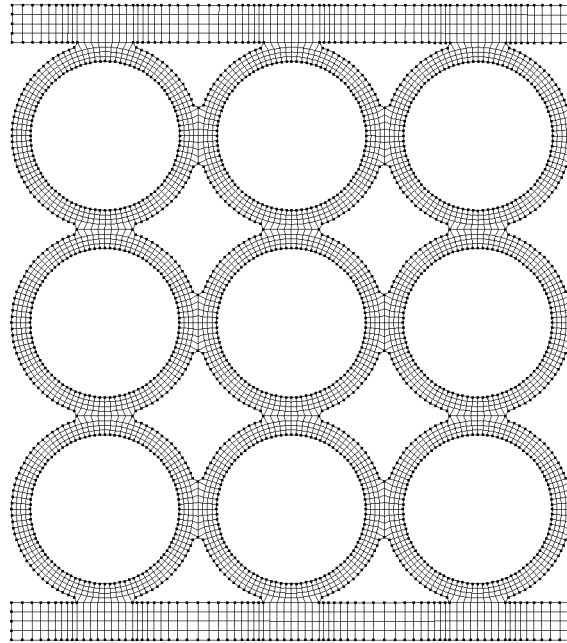


Figure 23 - Initial configuration and Lagrangian (surface) nodes in case CARA02

CARA02
TIME: 1.00000E+01 STEP: *****

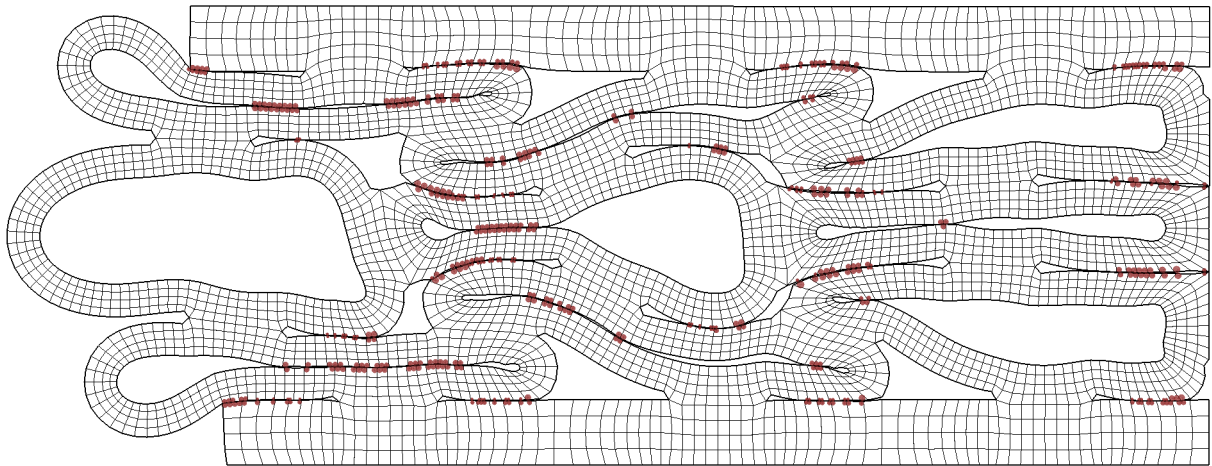


Figure 24 - Final configuration with contacts in case CARA02

CARA02
TIME: 1.00000E+01 STEP: *****

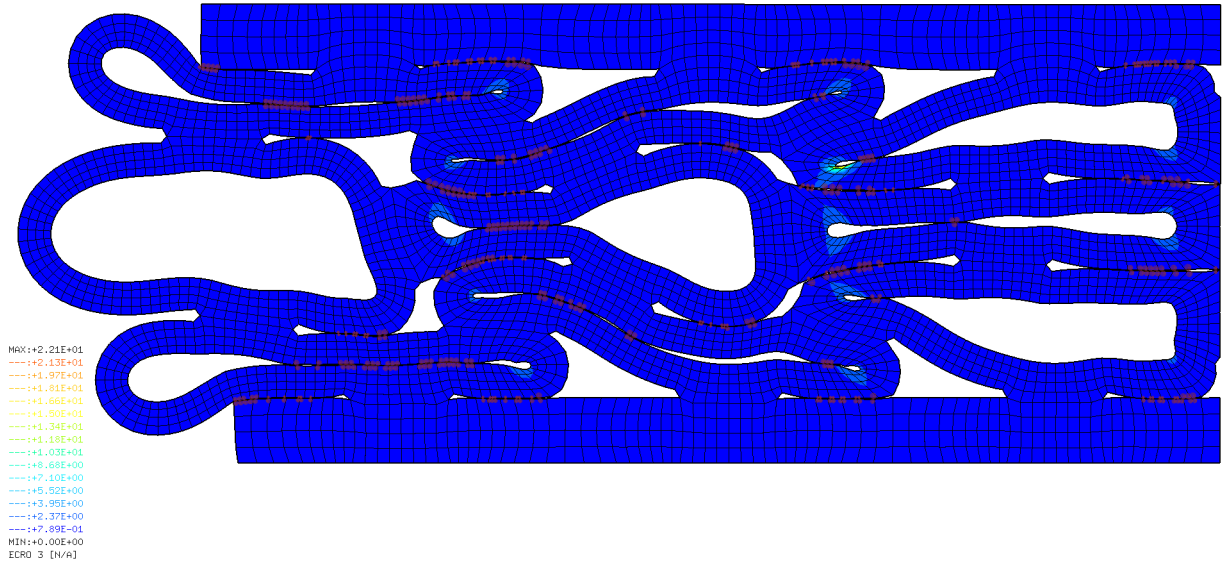


Figure 25 - Final configuration with plastic strain in case CARA02

CARA02
TIME: 8.85000E+00 STEP: 880801

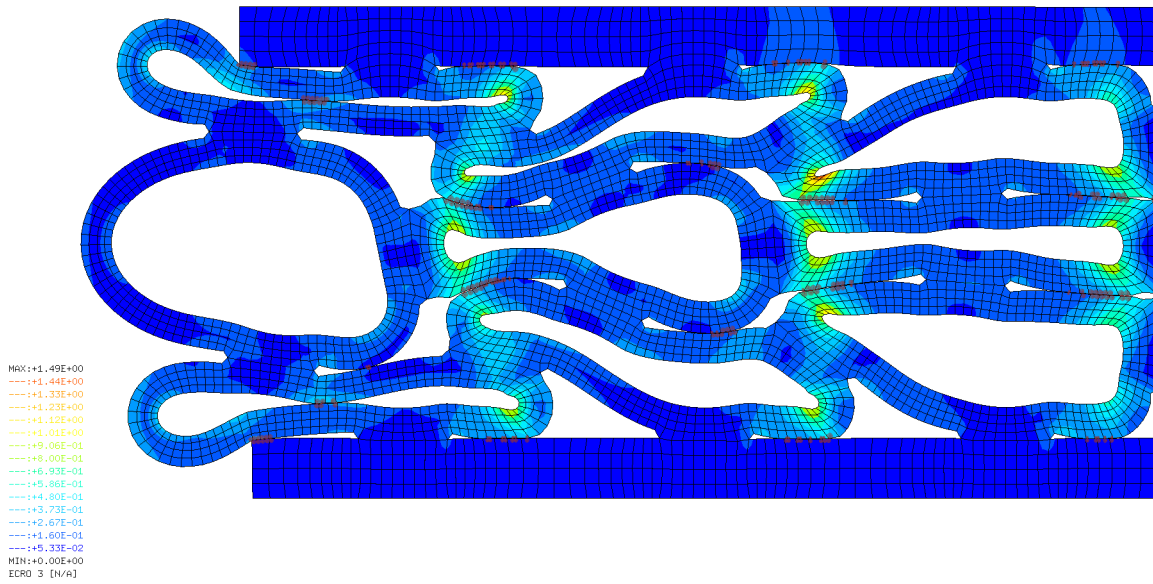


Figure 26 - Configuration at 8.85 s with plastic strain in case CARA02

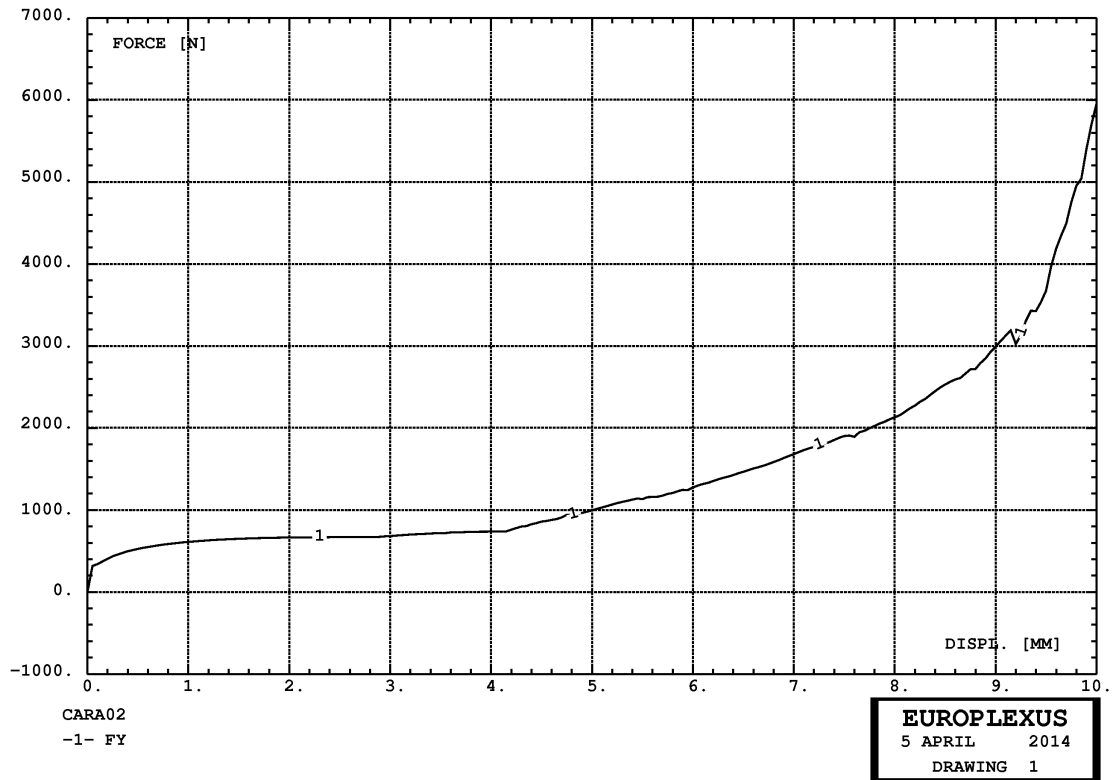


Figure 27 - Crushing force vs. imposed displacement in case CARA02

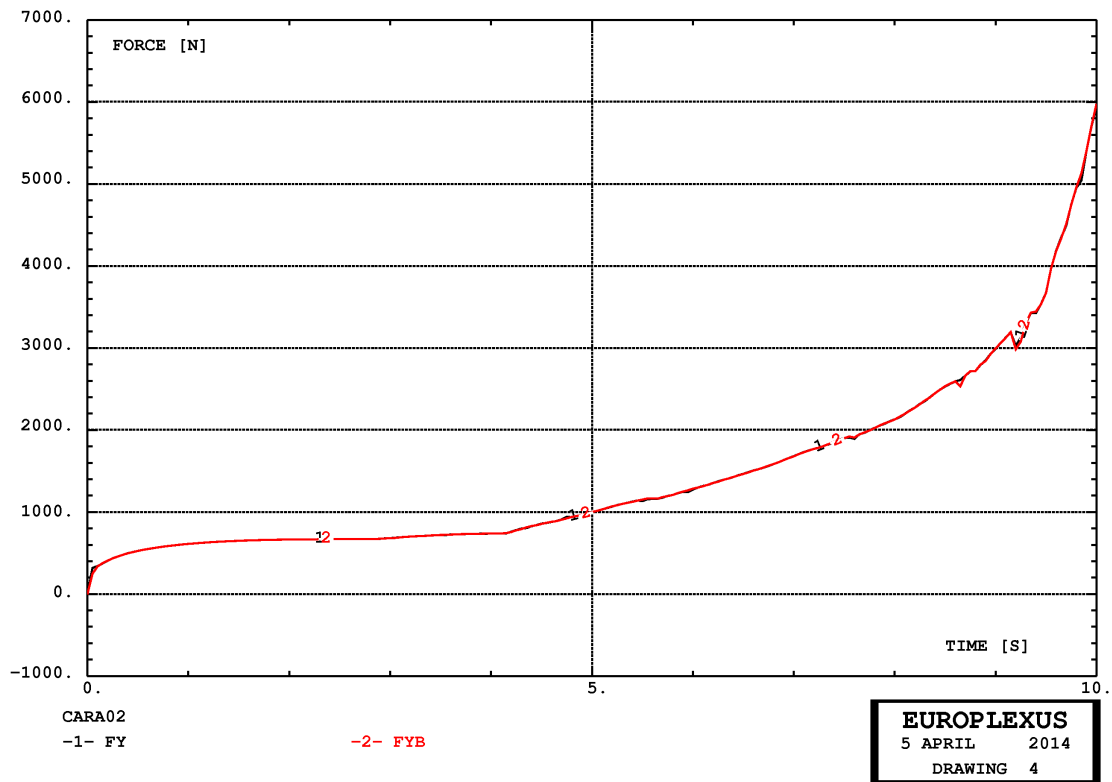


Figure 28 - Upper plate and lower plate forces in case CARA02

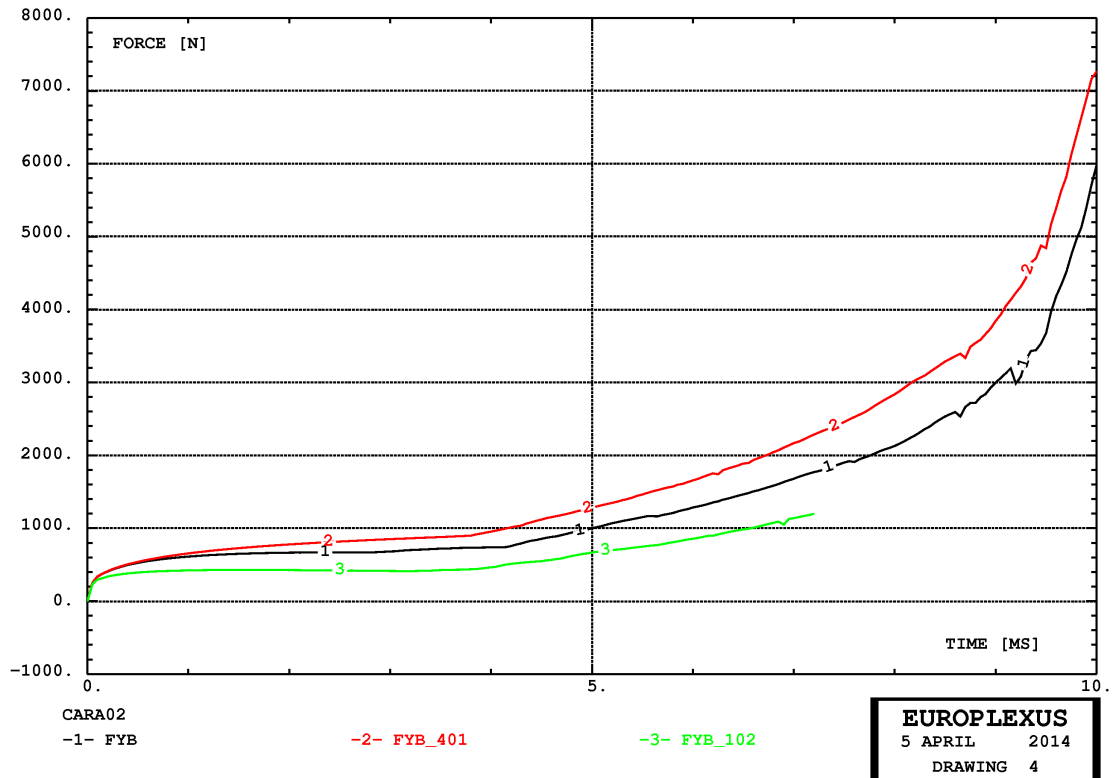


Figure 29 - Comparison of crushing forces in cases CARA02, CAR401 and CAR102

CARA03
TIME: 1.05000E+00 STEP: 114184

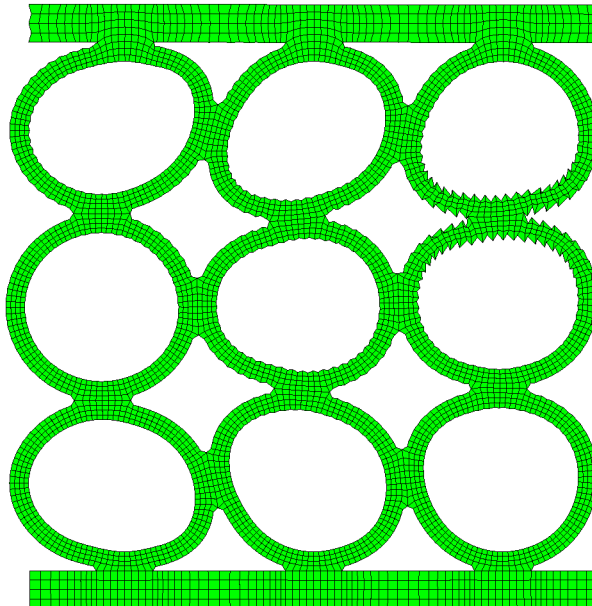


Figure 30 - Deformed mesh with mechanisms in case CARA03

2.2.1 Speeding up the calculations

From what observed previously e.g. in case CARA02 (Figure 28), it appears that the present test case can be considered as static and therefore it lends itself very badly to simulations by an explicit code such as EUROPLEXUS, which aims at fast transient dynamics. Solutions require millions of steps and thus the CPU time is large, although these are just 2D calculations and with relatively few elements.

It makes therefore sense trying to reduce the CPU time, possibly without sacrificing the quality of the solutions. Two alternative (but similar) approaches are tested here:

- I Increase the crushing velocity. For example, by using a 10 times larger crushing velocity (10 mm/s instead of 1 mm/s) the total number of steps, and thus the CPU time, should become about ten times smaller. A speed of 10 mm/s is still so small that no significant dynamic effects should be observed (but this will have to be verified a posteriori). Of course, the time scale of the response will become 10 times shorter (for the same crushing displacement).*
- II Increase the density of the material. For example, by multiplying the density by a factor 100, the critical time step will be increased by a factor 10, again resulting in a speed-up of about 10. In this case the time scale remains the same.*

CARA04

This calculation is similar to test CARA02 but uses a ten times larger (10 mm/s instead of 1 mm/s) crushing velocity. The calculation completed in 10% of the steps and 12.3% of the CPU of the previous case, as expected, i.e. a speed-up factor of 8.1.

Figure 31 shows the initial contour and the deformed mesh at 0.35 s, when the first contacts occur. Figure 32 shows the final mesh with the contacts and Figure 33 the plastic strain, which reaches a local maximum of 580%.

The crushing forces in the upper and lower plates are shown in Figure 34. They are identical, except in a very short time interval at the beginning of the transient. This is partly due to the fact that an imposed velocity is applied without setting an initial velocity in the upper plate nodes. However, the test can still be considered as static, since the two curves are identical over the large majority of the transient, and in particular in the last phase when most contacts and plasticization occur.

As a matter of fact, the crushing forces in the three cases CARA02, CARA03 and CARA04 are practically identical, as shown in Figure 35, despite the fact that the latter calculation costs only 1/10 of the others. In particular, the curves of cases CARA02 and CARA04 (complete calculations) are almost superposed.

CARA05

This calculation is similar to test CARA02 but uses a hundred times larger material density, so that the stability time step is ten times larger. Again, the calculation completed in 10% of the steps and 12.3% of the CPU of case CARA02, as expected, i.e. a speed-up factor of 8.1 (the same as in case CARA04).

Figure 36 shows the final deformed mesh with the contacts and Figure 37 the final plastic strain that reaches a local maximum of 166%.

Figure 38 shows the upper and lower plate forces and Figure 39 compares the crushing force with those of the previous solutions from CARA02 on. All these solutions are very similar.

CARA04
TIME: 3.50011E-01 STEP: 24915

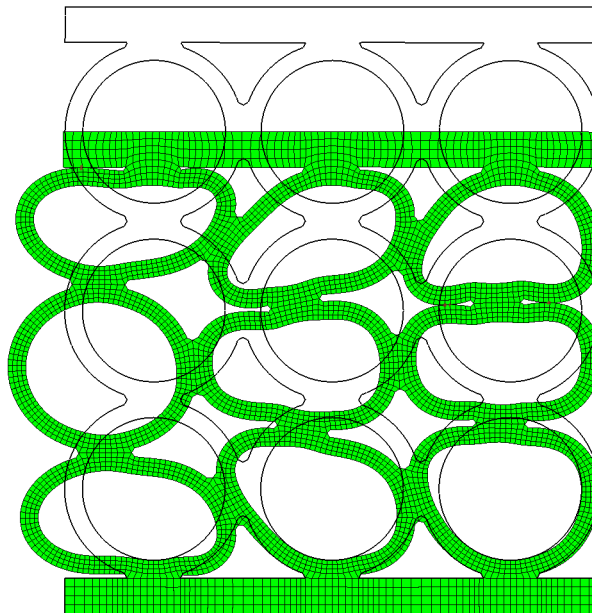


Figure 31 - Initial contour and deformed mesh at 0.35 s in case CARA04

CARA04
TIME: 1.00000E+00 STEP: 114118

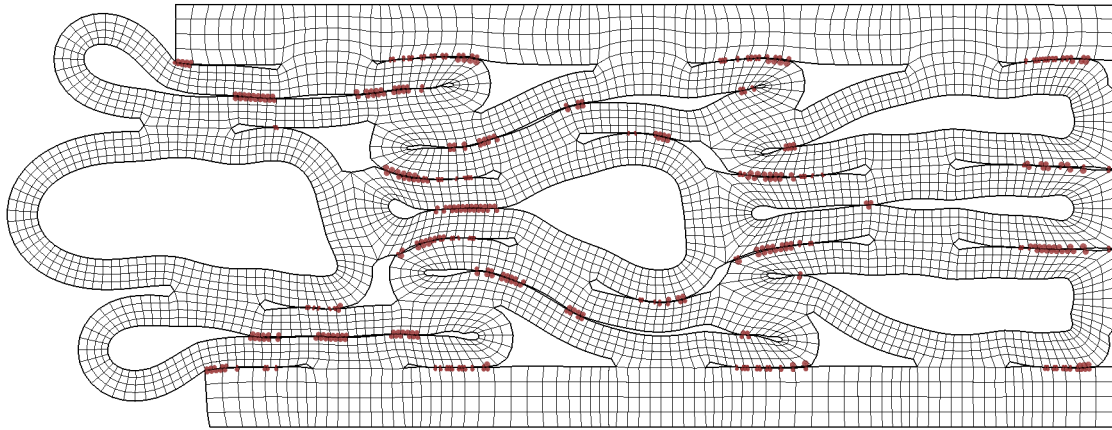


Figure 32 - Final mesh with contacts in case CARA04

CARA04
TIME: 1.00000E+00 STEP: 114118

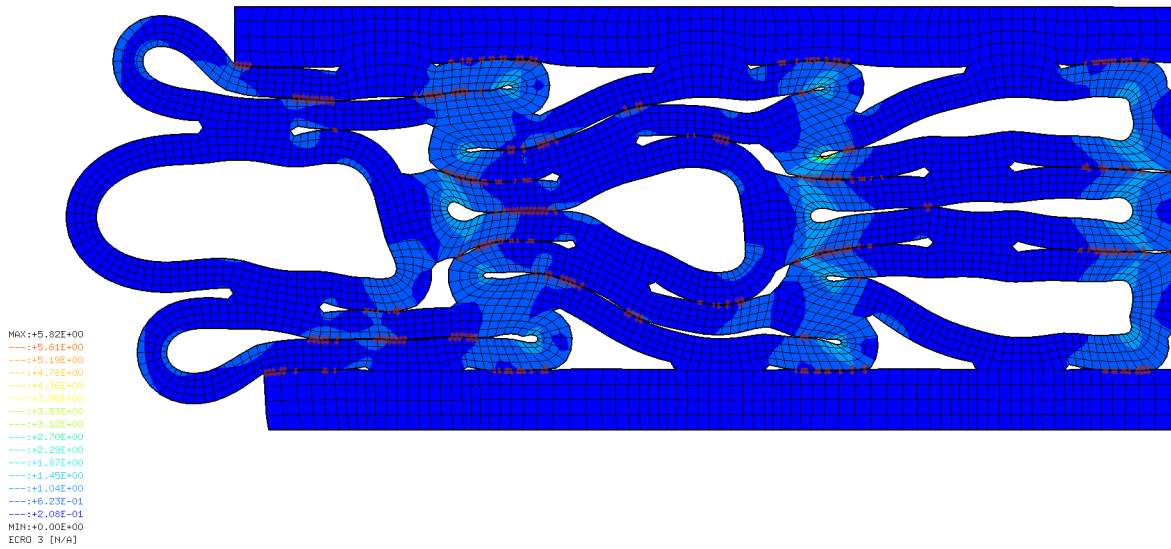


Figure 33 - Final mesh with plastic strain in case CARA04

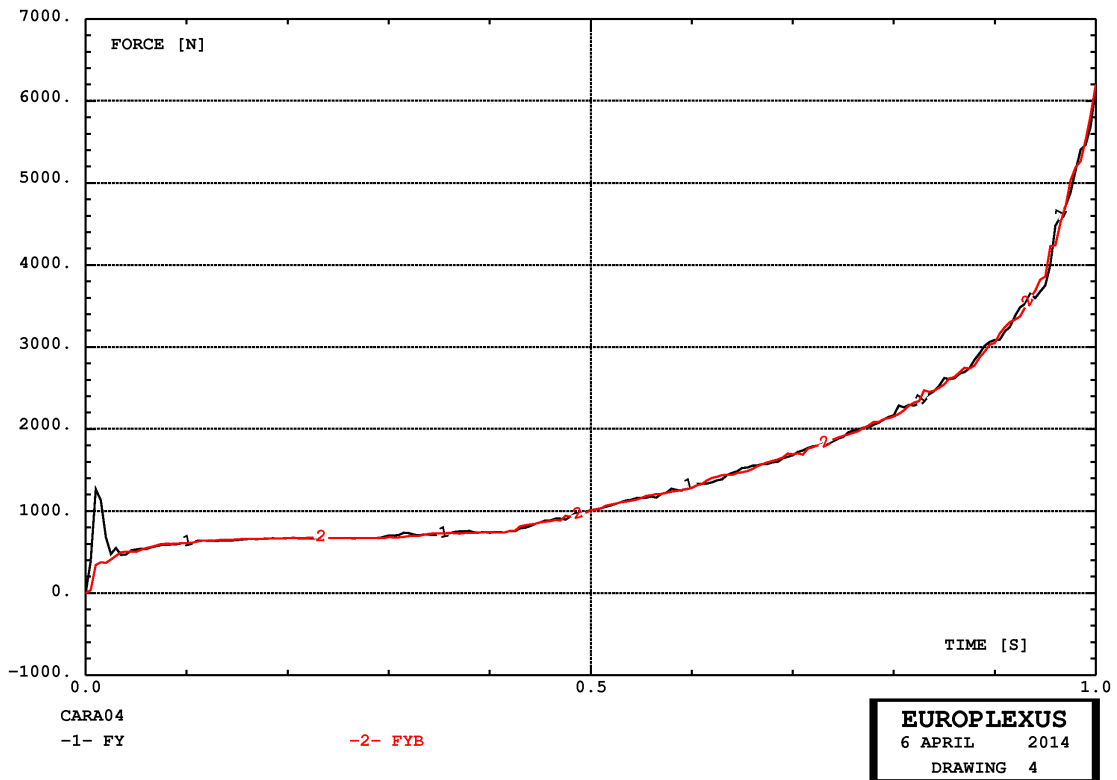


Figure 34 - Upper and lower plate forces in case CARA04

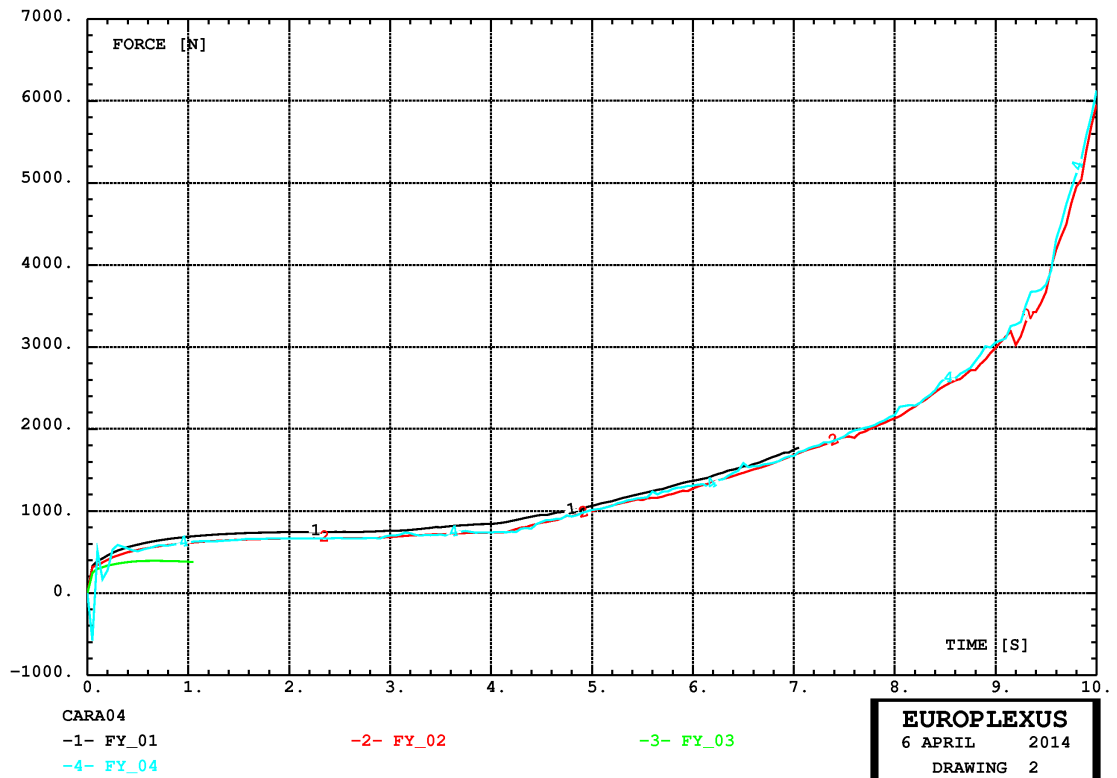


Figure 35 - Comparison of crushing forces in cases CARA02, CARA03 and CARA04

CARA05
TIME: 1.00000E+01 STEP: 114261

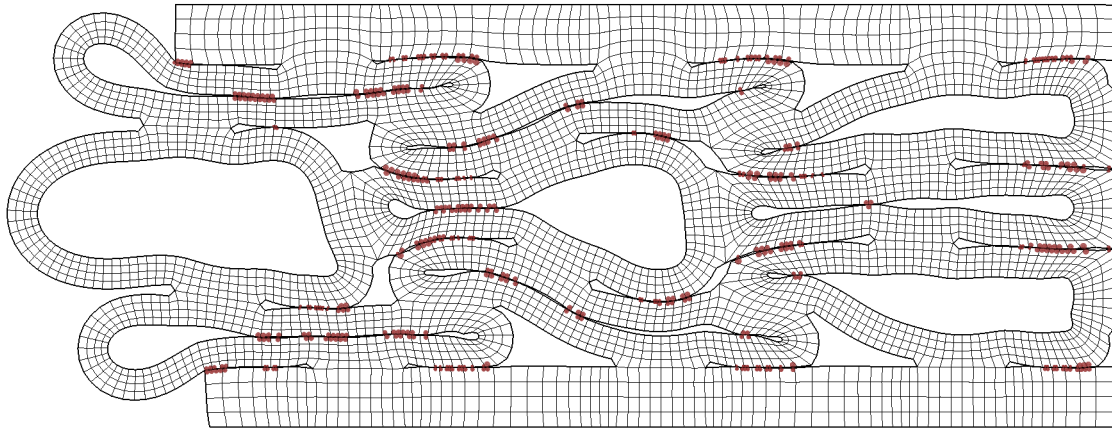


Figure 36 - Final mesh with contacts in case CARA05

CARA05
TIME: 1.00000E+01 STEP: 114261

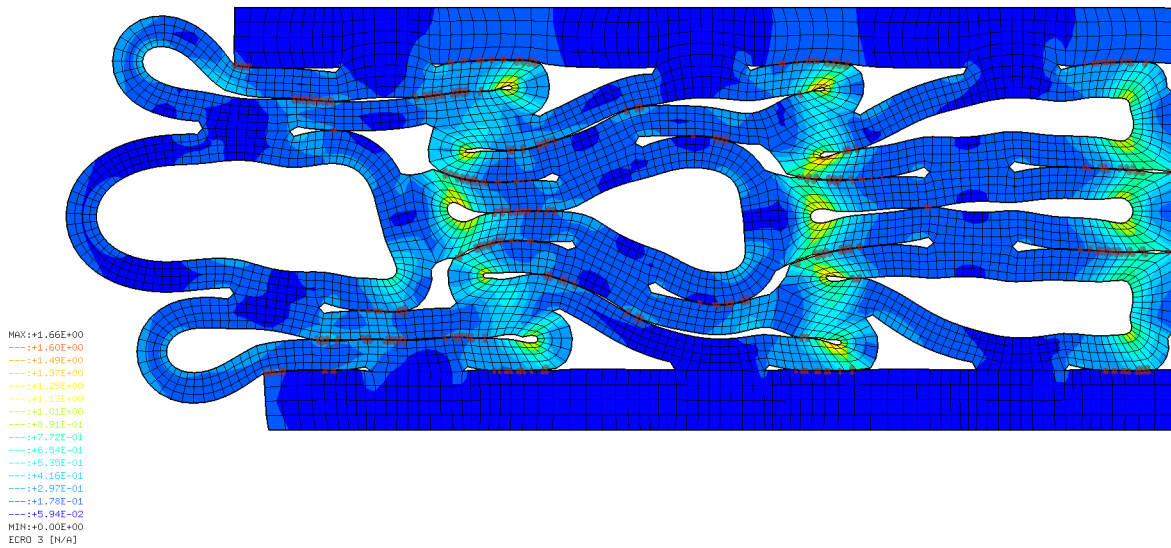


Figure 37 - Final mesh with plastic strain in case CARA05

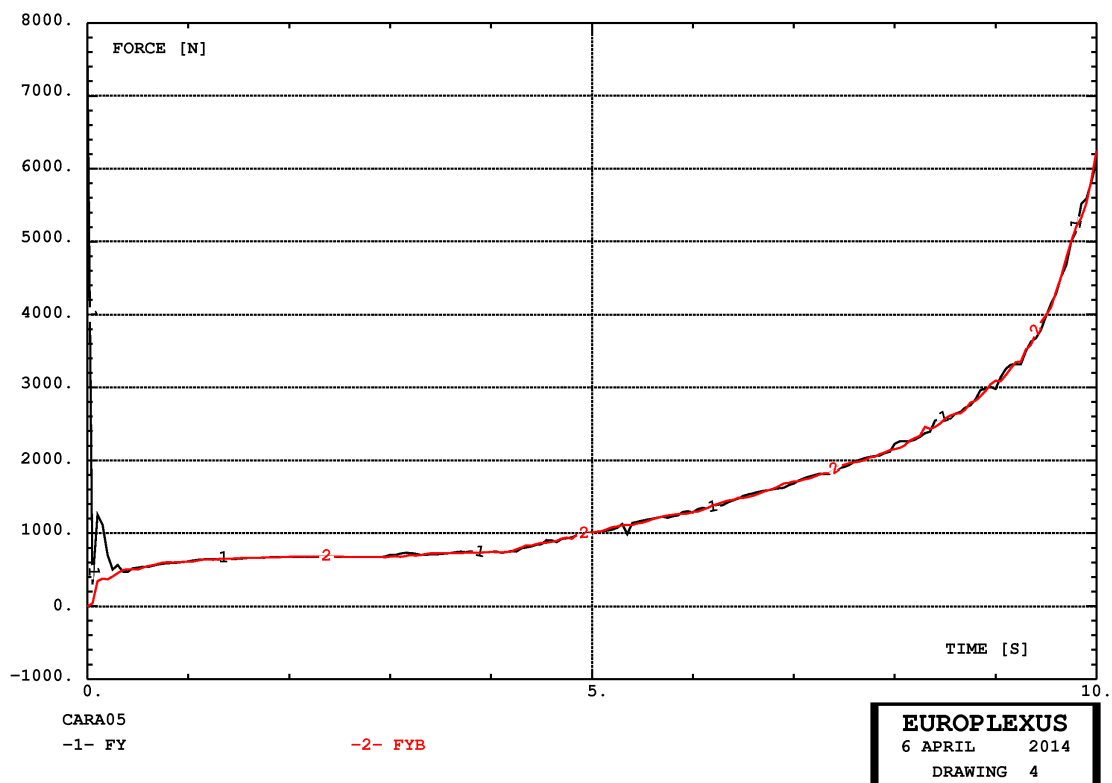


Figure 38 - Upper and lower plate forces in case CARA05

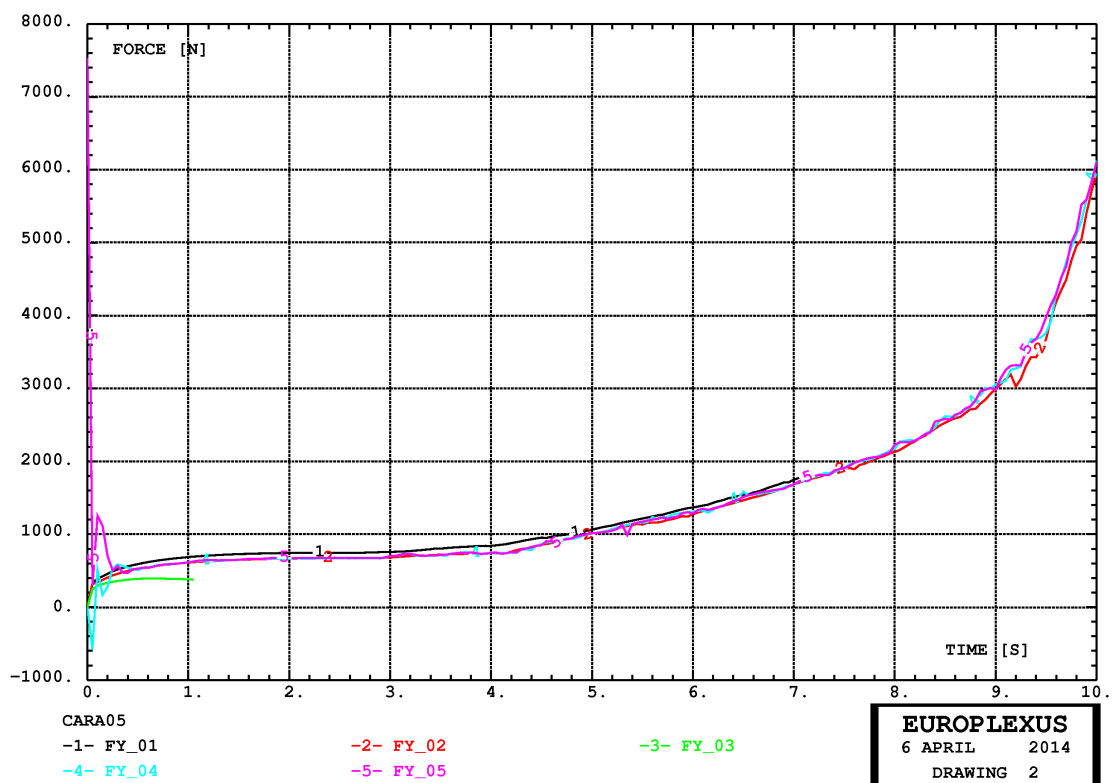


Figure 39 - Crushing forces in cases CARA02, CARA03, CARA04 and CARA05

In the next three solutions, a constant crushing velocity is imposed instead of a (nearly) linear imposed displacement. Moreover, all nodes of the upper surface of the upper plate have an initial velocity equal to the crushing velocity, so as to minimize the initial oscillations and jumps in the (upper) crushing force. Moreover, the lower-plate force is used in the plots rather than the upper one since initially it is more regular and after a very short period the two forces are identical anyway.

CARA06

This calculation is similar to test CARA04 (crushing velocity of 10 mm/s) but uses the Q42N fully-integrated 4-node quadrilateral for ALE formulation in solids. The calculation stopped at 0.96 s, i.e. almost at the final time of 1 s, because the Jacobian of an element became zero due to excessive local deformation.

Details of the solution are shown in Figures 40 to 43. The crushing forces are shown in Figures 44 and 45 and are similar to the previous solutions.

CARA07

This calculation is similar to test CARA06 but uses the Q42 fully-integrated 4-node quadrilateral for ALE formulation in solids. The calculation arrives at the final time of 1 s, in about the same steps and CPU time as the previous ones.

Details of the solution are shown in Figures 46 and 47. The crushing forces are shown in Figures 48 and 49 and are slightly higher (stiffer solution) the previous solutions.

CARA08

This calculation is similar to test CARA06 but uses the Q41 reduced-integrated 4-node quadrilateral for ALE formulation in solids. The calculation was plagued by strong mechanisms and stopped at 0.13 s, see Figure 40.

CARA06
TIME: 9.95003E-01 STEP: 101317

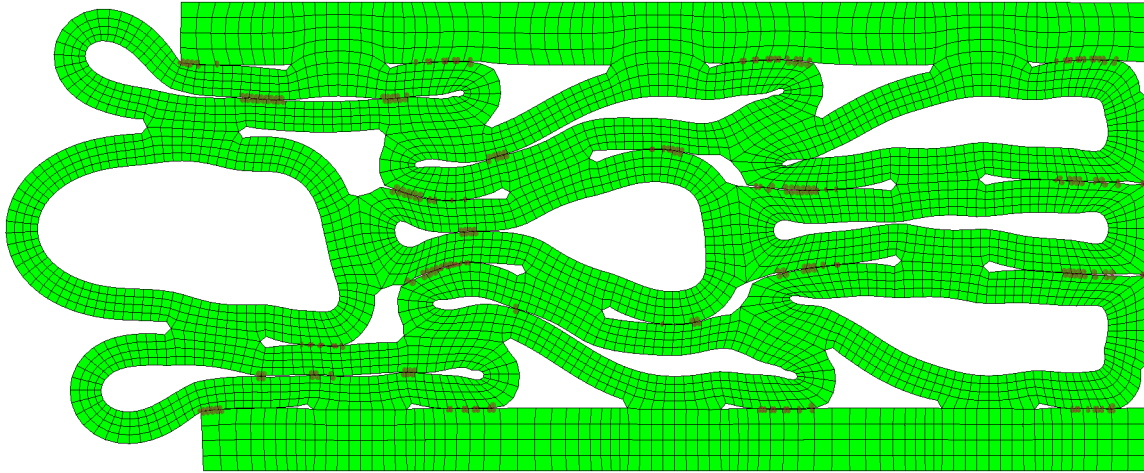


Figure 40 - Near-final mesh with contacts in case CARA06

CARA06
TIME: 9.95003E-01 STEP: 101317

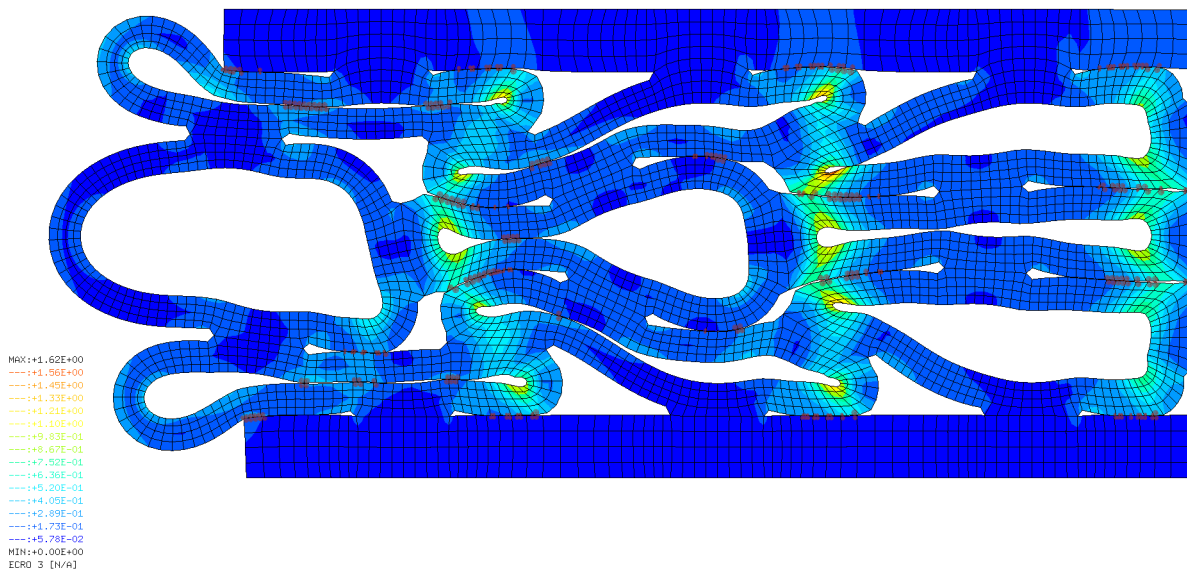


Figure 41 - Near-final plastic strains in case CARA06

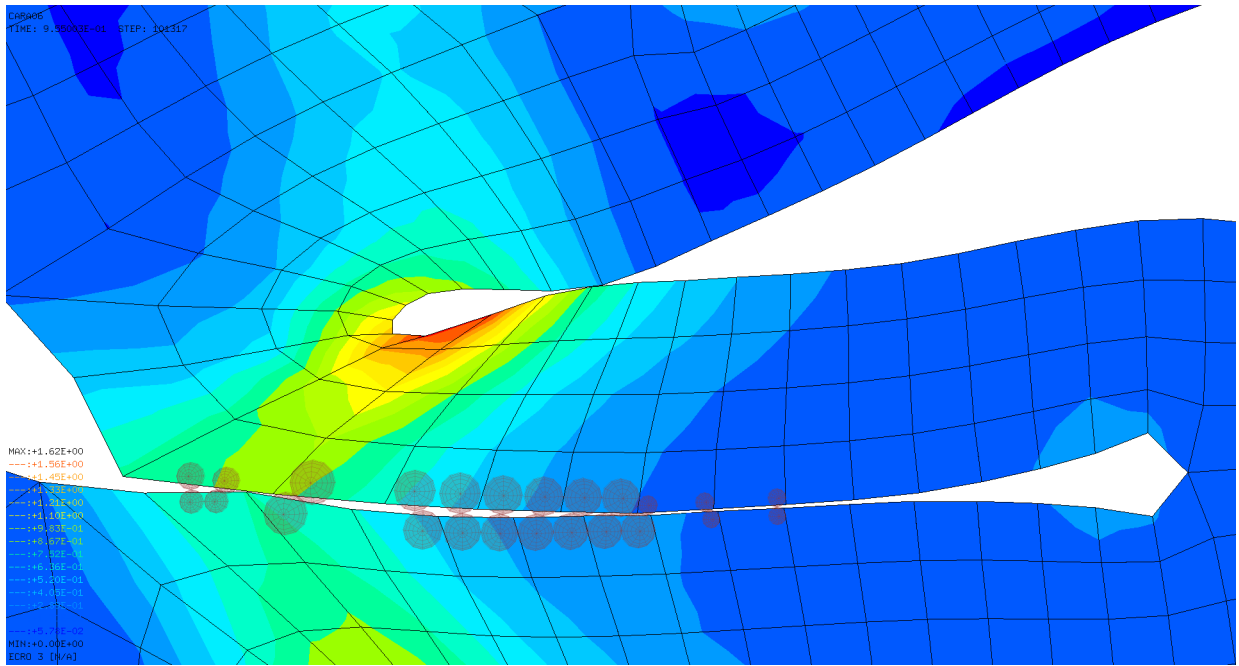


Figure 42 - Near-final plastic strains in case CARA06 (detail)

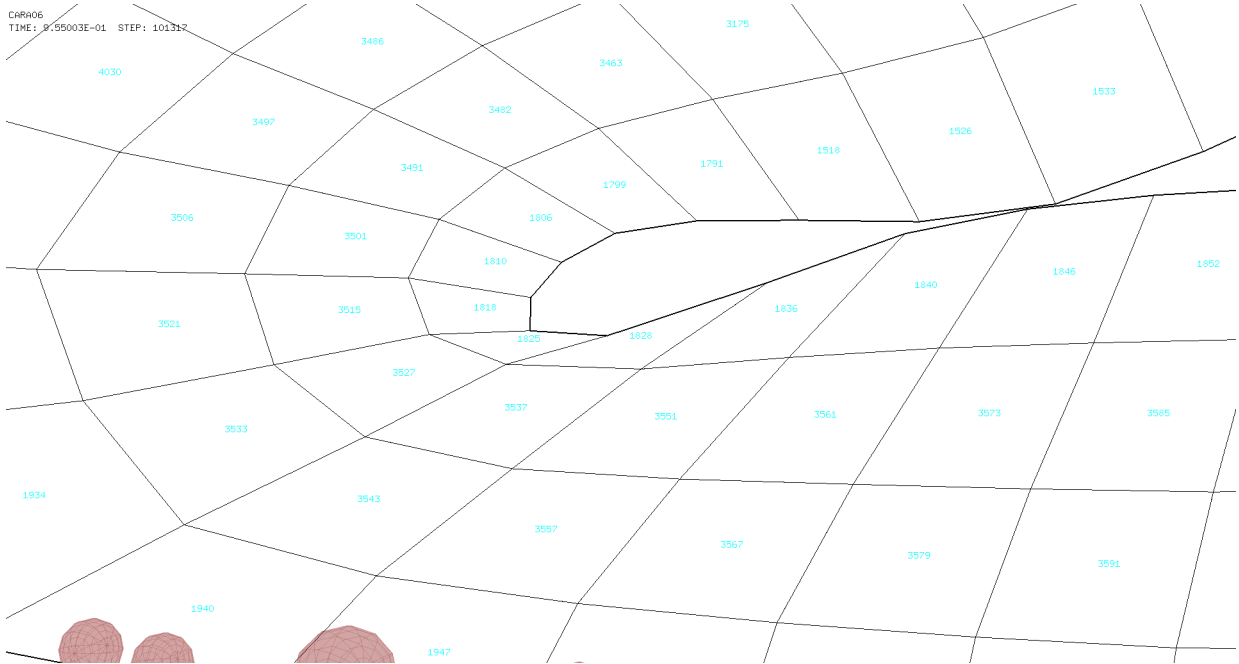


Figure 43 - Excessively deformed element in case CARA06

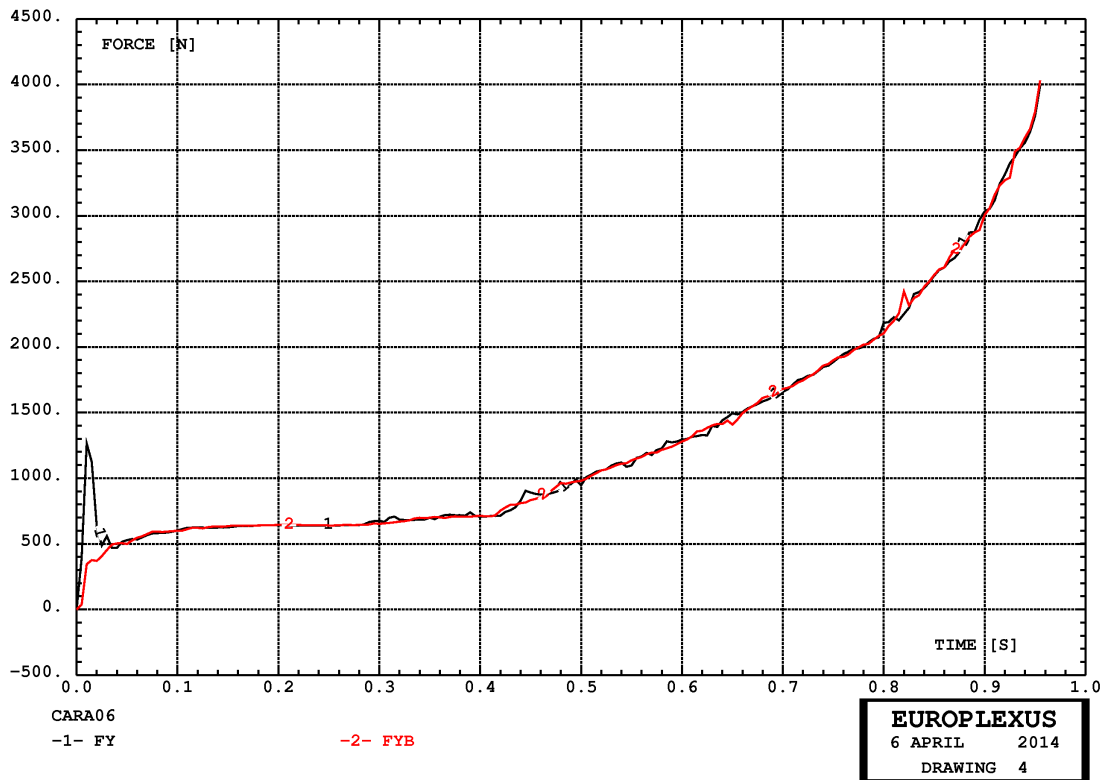


Figure 44 - Upper and lower plate forces in case CARA06

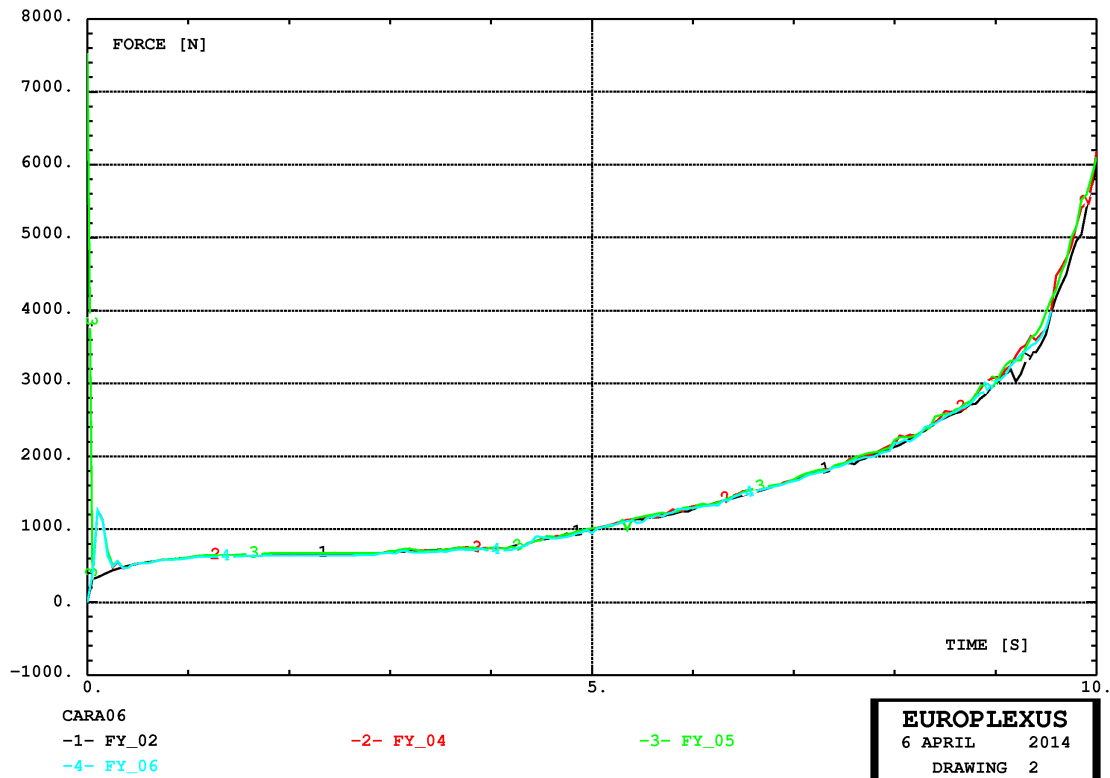


Figure 45 - Crushing forces in cases CARA02, CARA04, CARA05 and CARA06

CARA07
TIME: 1.00000E+00 STEP: 90068

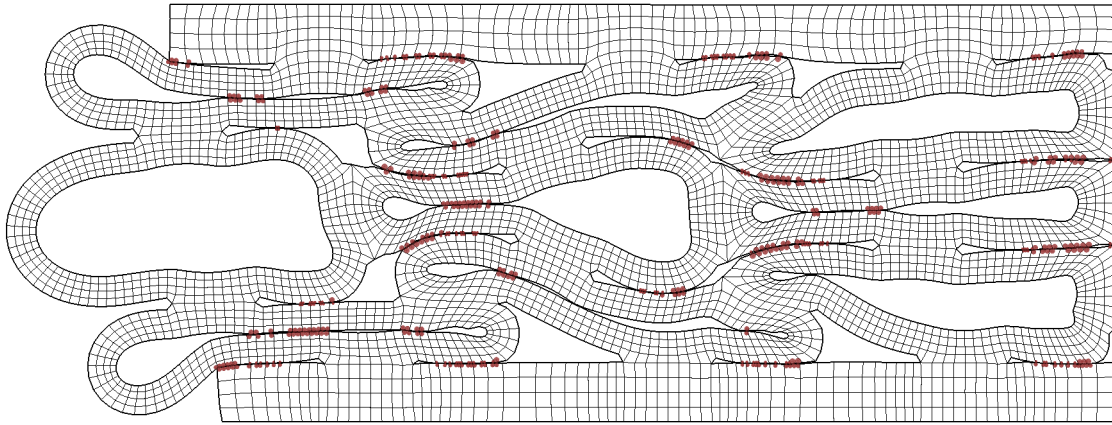


Figure 46 - Final mesh with contacts in case CARA07

CARA07
TIME: 1.00000E+00 STEP: 90068

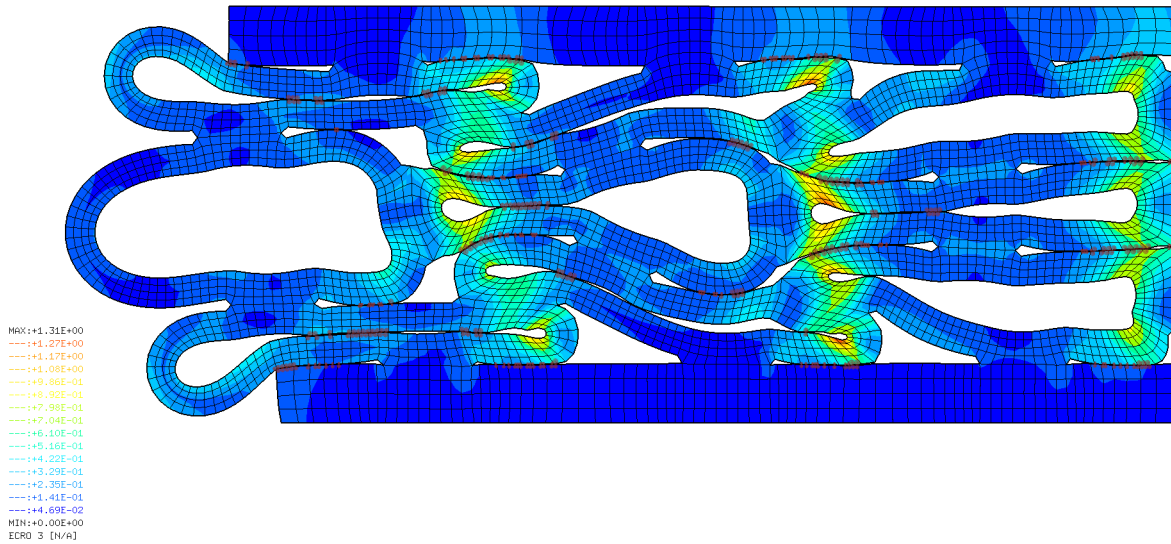


Figure 47 - Final plastic strains in case CARA07

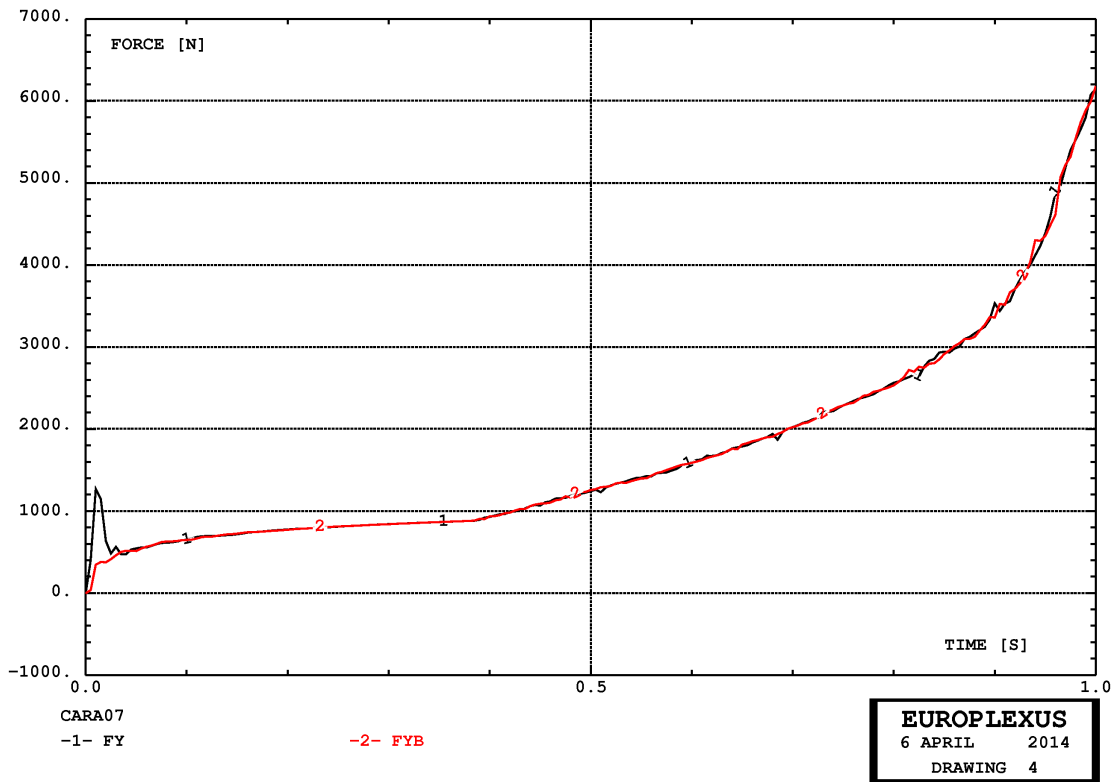


Figure 48 - Upper and lower plate forces in case CARA07

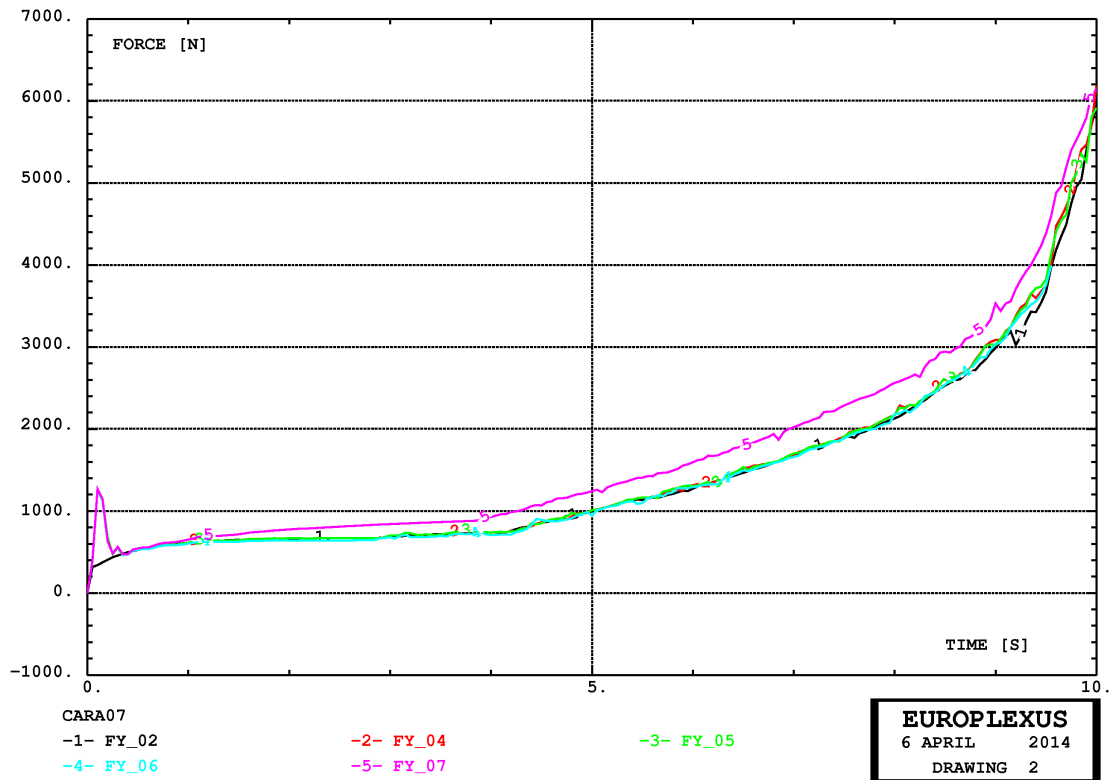


Figure 49 - Crushing forces in cases CARA02, CARA04, CARA05, CARA06 and CARA07

CARA08
TIME: 1.25001E-01 STEP: 18904

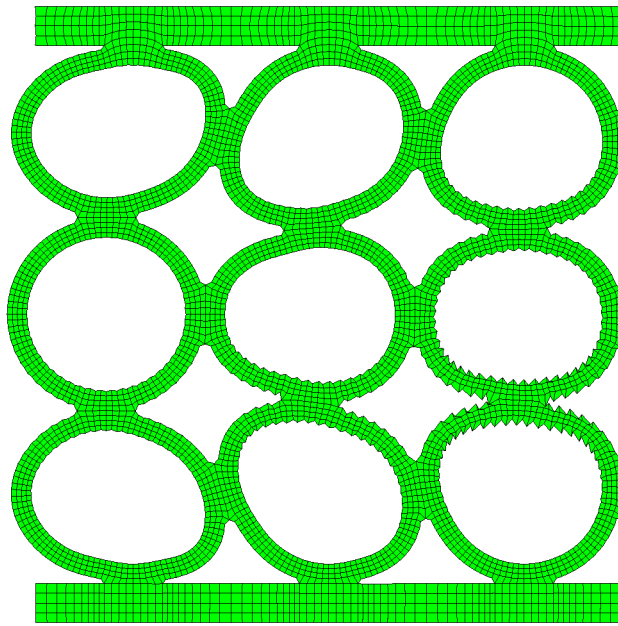


Figure 50 - Deformed mesh with mechanisms in case CARA08

2.3 Solutions with Q93 and phantom elements for the contact

As mentioned in the Introduction, one way of modeling contact in elements which are not capable of hosting pinballs (such as the parabolic elements, *prior to the present work*) is to use a “ghost” or “phantom” mesh of other elements (allowing for pinballs) in addition to the elements used to model the actual structure.

The ghost mesh is simply superposed to the physical mesh, and the nodes of the two meshes are merged. For example, in the Cast3m mesh generator one would “eliminate” the (repeated) nodes of the two meshes by giving a small tolerance `tol`:

```
elim tol (mesh1 et mesh2);
```

In this way, the (contact) forces applied to the ghost mesh are “felt” also by the physical mesh. The ghost mesh is assigned a FANT material with zero density in EUROPLEXUS. This means that the ghost elements are not calculated during the transient, i.e. their internal forces are always zero.

The only purpose of the ghost elements is to detect the contact. Pinballs are assigned to the ghost elements in the normal way.

This technique is fully general and can be used in different ways.

Let us consider a first example. EUROPLEXUS currently lacks a directive for associating pinballs to the nodes, rather than to the elements. However, this can be done by the following strategy (we assume Cast3m as pre-processor for simplicity). Let us say that we want to assign pinballs of a given (small) diameter D to all nodes on the surface of a 3D projectile named `proj`, and meshed by continuum elements. Then in Cast3m:

```
surproj = ENVE proj;  
projnod = CHAN POI1 surproj;
```

The first command extracts the “envelope” of the (solid) projectile, resulting in a surface mesh made (for example) of triangles and quadrangles. The second command generates a mesh of material point elements (single-node elements) occupying the nodes of the surface.

Once read the mesh in EUROPLEXUS, we assign PMAT (material point one-node) elements to the `projnod` object. Next, we assign a diameter to these elements in the `COMP EPAI` directive: note that this is only for visualization of the nodes, and is not used for the contact. Next, we assign a FANT material with zero density to these elements. Finally, we assign pinballs of the desired diameter D to these “elements” (in fact, to the nodes). Since these elements possess just one node, the diameter of the associated pinball is fixed and hierarchic pinballs cannot be used with them.

Returning now to the case of interest here, there are several ways in which one can use the ghost mesh technique. Some possibilities are illustrated in Figure 51.

In the top part of the Figure, we use linear 4-node quadrilaterals as ghost elements. Two such elements, labeled Q4_1 and Q4_2, respectively, are superposed and merged with the nine-node element considered, covering the “quadrants” of the element adjacent to the face possibly subjected to contact. These elements and the corresponding (parent) pinballs are drawn in cyan and magenta, respectively, for clearness. Of course, to increase the precision of contact detection one could use hierarchic pinballs. All the options for “normal” pinballs are available.

In the bottom part of the Figure, we use linear 2-node (segment) elements as ghosts. They are attached to the bottom face of the Q9 element. Again only the associated parent pinballs are shown, but of course one should in this case prescribe a thickness associated with these pinballs in order to increase contact detection accuracy.

Yet another possibility (not shown) would be that of placing pinballs only at the nodes by using the PMAT as ghost elements, as explained previously. In this case, however, contact could be overlooked if the diameter of such pinballs is too small. Normally in such cases one would have to assign nodal pinballs to one contacting surface and body or line pinballs to the other contacting surface, but this of course can be very difficult (if not impossible) in the present case because we are dealing with self-contact.

In the calculation of the ring crash problem with Q9 elements we have adopted the first technique shown in Figure 51, i.e. we have used quadrilaterals (Q41L) as ghost elements.

Generation of the parabolic elements mesh

A mesh composed of parabolic rather than linear elements can be directly generated in the Cast3m mesh generator as follows. First of all, in the declaration of the element types to be used one should take the parabolic type rather than the linear type. In our 2D case, this means OPTI ELEM QUA8 instead of OPTI ELEM QUA4.

Note that in this way 8-node quadrilaterals (and/or 6-node triangles) are generated, since Cast3m is primarily a static code and does not use the 9-node elements typical of dynamics. However, once a mesh composed of QUA8 (say sur8) has been generated, it is possible to transform it in QUA9 (by adding the central node), ready to be sent to EUROPLEXUS, using the CHAN command:

```
sur9 = CHAN QUA9 sur8;
```

In the present case we have chosen not to generate the mesh anew, but to convert the existing QUA4 4-node mesh used in test QUA401 of Section 2.1 into a QUA9 mesh with the same number of ele-

ments (i.e., each QUA4 is transformed into an equivalent QUA9). Thus, not only central but also mid-side nodes should be generated and added and the above mentioned technique based on the CHAN operator cannot be used for this.

To this end, two Gibiane procedures have been written (listed in the Appendix):

- `pxq42q92 .proc` takes a single QUA4 element (4 nodes) in input, generates 4 new mid-side nodes and a central node and outputs a single QUA9 element.
- `pxq92q4 .proc` takes a single QUA9 element in input and generates four new QUA4 elements, one for each “quadrant” of the QUA9. This procedure can be used to generate the phantom elements for the contact.

Then, we have proceeded as follows (see file `readq4 .dgibi` in the Appendix):

- The QUA4 mesh (in free format in file `QUA401.epx`) has been extracted from the input file and set in the so-called “write” format of Cast3m in a file called `mesh4 .write`. This means simply adding an initial line giving the space dimension (2) and the total number of nodes (4948), then the list of x and y coordinates of nodal points (4948 lines), then a line specifying the number of nodes per element (4), the number of elements (4080) and the element type (QUA4), and finally the element connectivity, i.e. 4080 lines, each containing the four node indexes of an element.
- The mesh (`sur4`) has been read into Cast3m by means of the READ operator (note that the READ and WRITE operators have been developed in the JRC version of Cast3m and are only available in this version).
- An equivalent QUA9 mesh `sur9` has been obtained by the `pxq42q92` procedure applied to each QUA4 element in a loop. Duplicated nodes are simply removed by Cast3m’s ELIM operator.
- The “external” elements of the `sur9` mesh, i.e. those having at least one side on the mesh envelope, have been extracted:

```
peau9 = CONT sur9;
elpeau9 = sur9 ELEM APPU LARG peau9;
```

- The ghost elements for contact have been obtained by transforming each `elpeau9` element into four QUA4 via the `pxq92q4` procedure.

The resulting QUA9 mesh and the corresponding ghost QUA4 mesh are shown in Figures 52 and 53. Note that with this technique, two layers of ghost QUA4 elements are produced along the surface of the structure mesh. Only one layer would suffice of course and the “internal” layer is redundant (as

long as there is no element failure and erosion). However, the two layers have been retained for simplicity of mesh generation.

Another simplification is that here a single SELF zone is declared for pinball contact, rather than distinguishing the 25 separate zones like in case QUA401. This drastically simplifies the contact input directive (but at the expense of some more laborious calculations for the code) and the risk of obtaining more spurious contacts than in case QUA401.

All performed calculations are summarized in Table 3.

Table 3 - Calculations of the structure crash problem by Q93 with ghost elements for contact

Case	Mesh	Notes	Steps	CPU [s]	Els*step
Q93_02	4080 Q93 + 7328 Q41L	1 PINB SELF DMIN 0.1 OPTI PINS GRID EQVF CNOR	1,595,017 ^a	40,313	6.51×10^9

a. The calculation stopped at 9.1 s of physical time instead of 10 s due to an unexpected reboot of the PC

Q93_02

This calculation uses Q93 nine-node parabolic elements for the structure and Q41L four-node linear quadrilaterals for the ghost mesh, see Figure 53. The calculation was brutally stopped at 9.1 s of physical time instead of 10 s, due to an unexpected reboot of the computer (MS-Windows Update).

This calculation was considerably slower than the QUA401 calculation because, having replaced each QUA4 by a QUA9, the number of nodes and of Gauss points has more than doubled, and the stability step has halved.

The same minimum pinball diameter (DMIN 0.1) as in the QUA401 calculation has been kept, while it would have been probably more appropriate to halve it.

The additional option EQVF is an attempt to reduce the onset of spurious contacts between neighboring elements. The CNOR option should help reduce the redundancy of contact constraints, and use “smoother” normal approximations for the contact normal directions.

Figure 54 shows the progressive crushing of the structure until 9.1 s of physical time. Figure 55 shows the plastic strain distribution at 9.1 s. Note that, as indicated by the red arrow, some apparently parasitic plasticization takes place in the zone contained in the red circle (actually, in a single element). This element is subjected to strange vibrations during the test and plasticization occurs very early during the crushing process, and seems therefore completely non-physical. This phenomenon is currently under investigation, but see Section 4 for a possible explanation.

Figure 56 shows the final contacts at 9.1 s. Again, many spurious contacts occur, as highlighted in the zoom on the same Figure. This seems to be due to too large diameter of the pinballs. As anticipated, it would have been better to use $DMIN = 0.05$ instead of $DMIN = 0.1$).

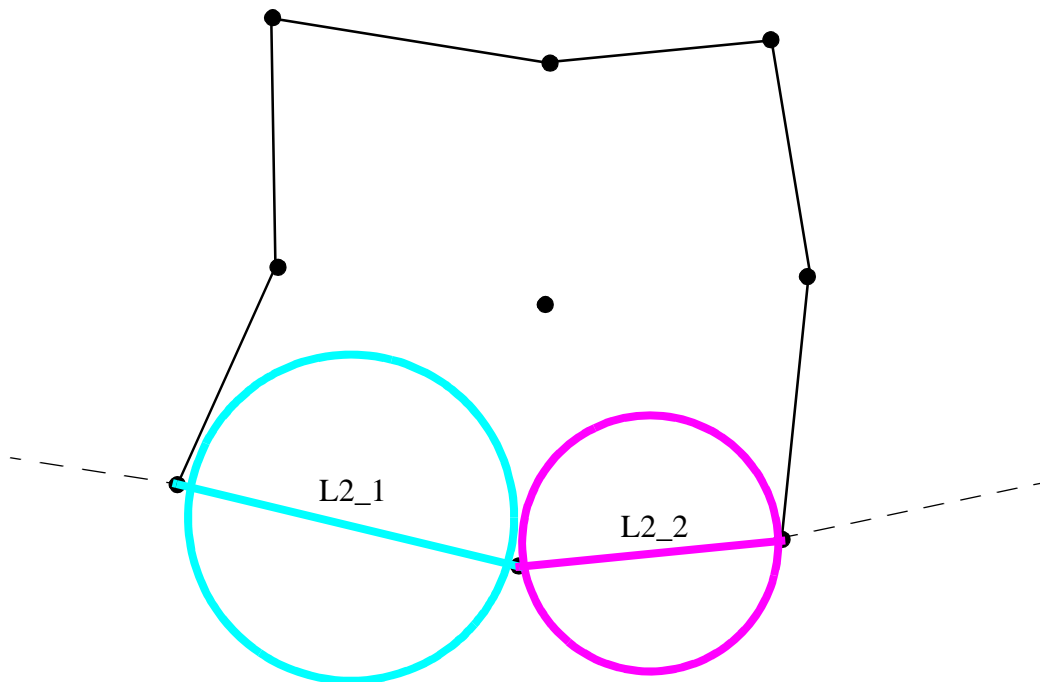
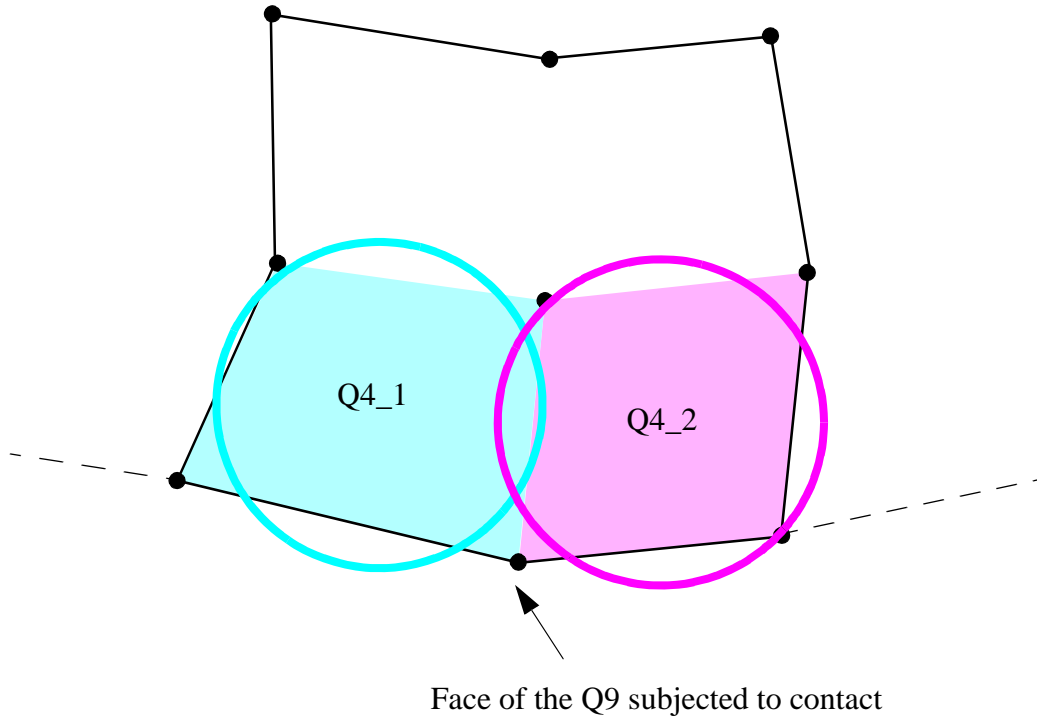
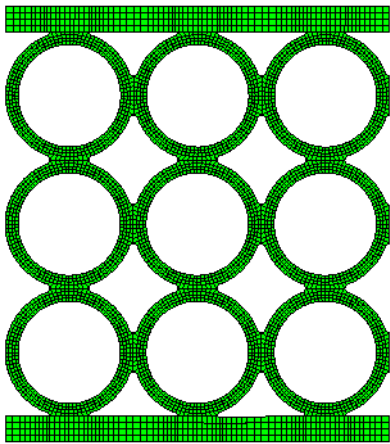


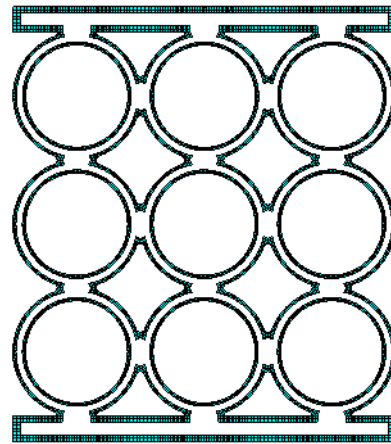
Figure 51 - Ghost mesh techniques to compute contact on parabolic elements

Q93_02
TIME: 0.00000E+00 STEP: 0

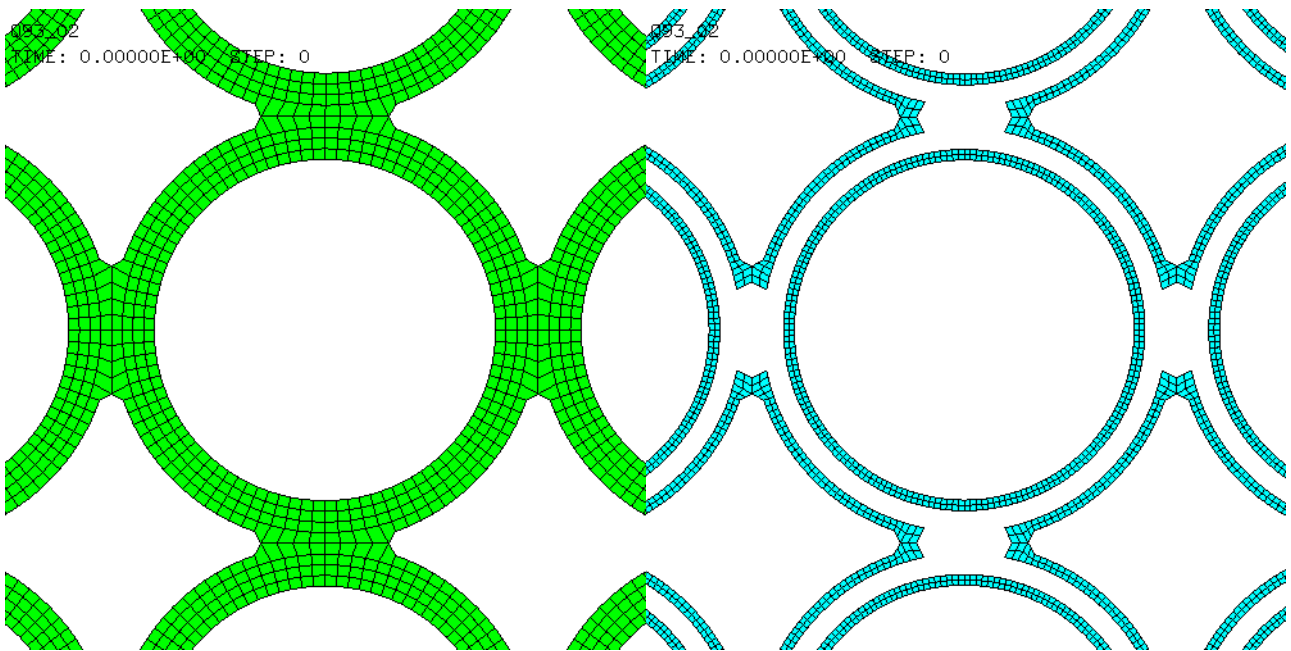


QUA9 mesh

Q93_02
TIME: 0.00000E+00 STEP: 0



QUA4 mesh (ghost)



zoom of the QUA9 and QUA4 meshes

Figure 52 - Structure and ghost meshes for case Q93_02

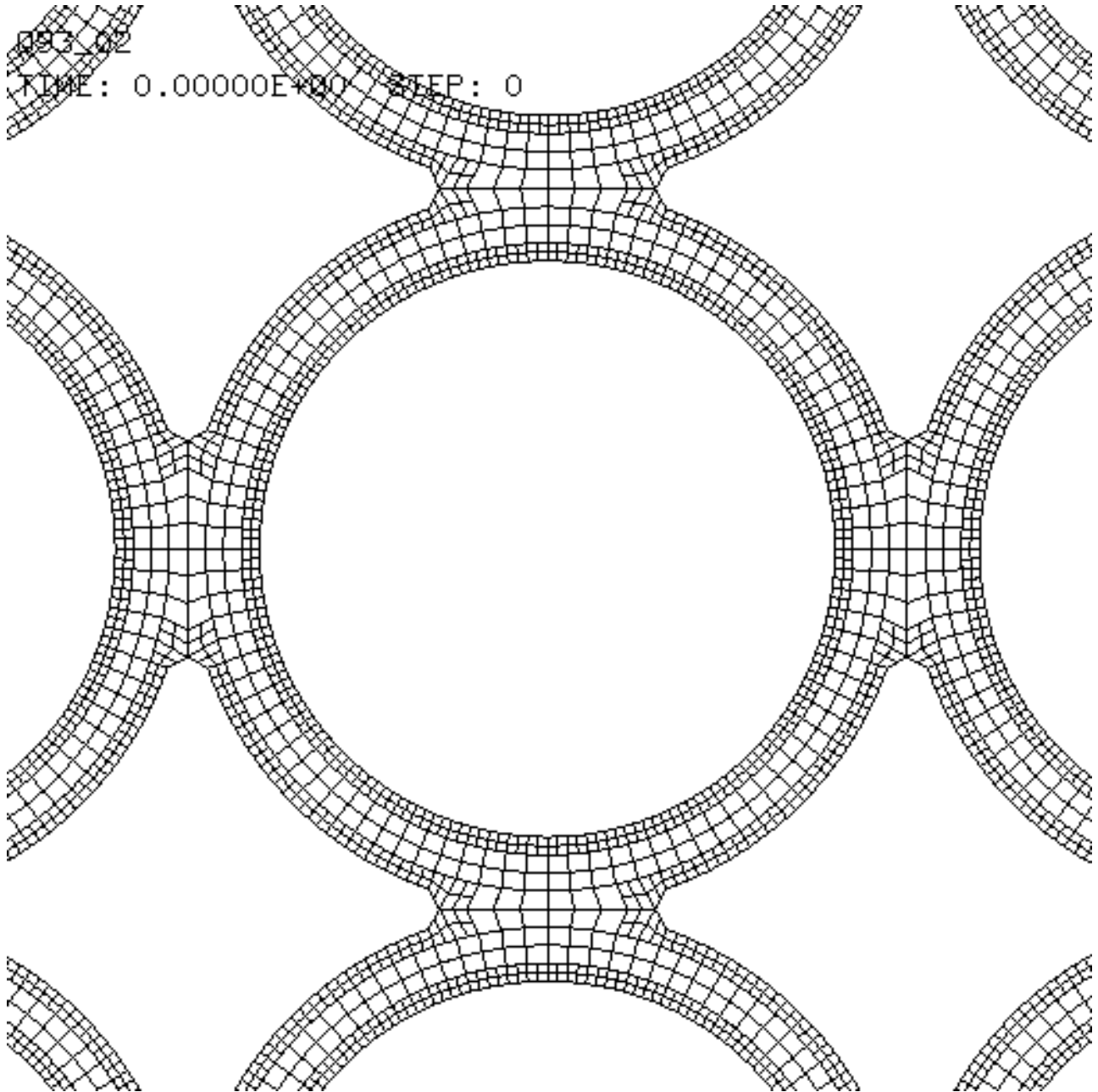
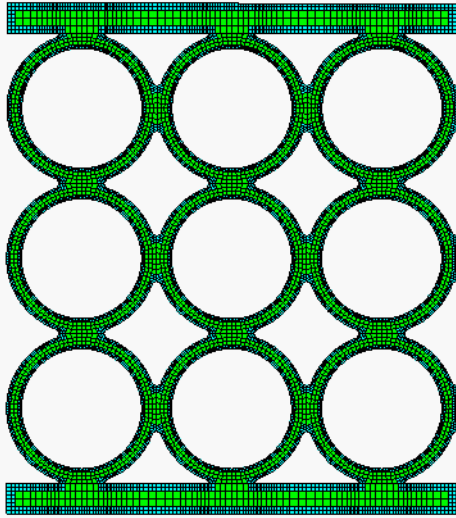
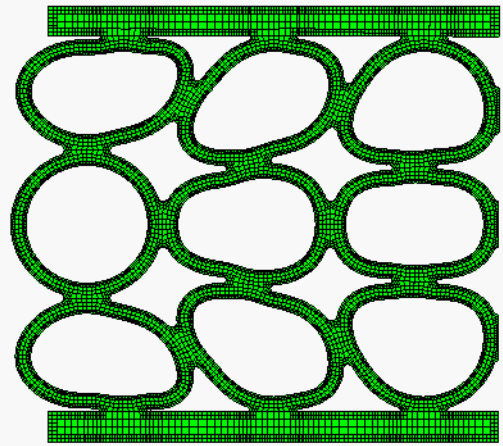


Figure 53 - Structure and ghost meshes superposed for test Q93_02

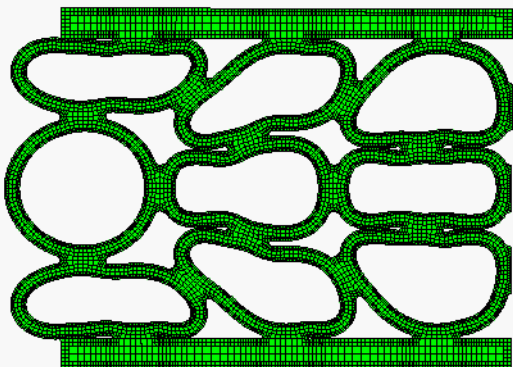
Q93_02
TIME: 0.00000E+00 STEP: 0



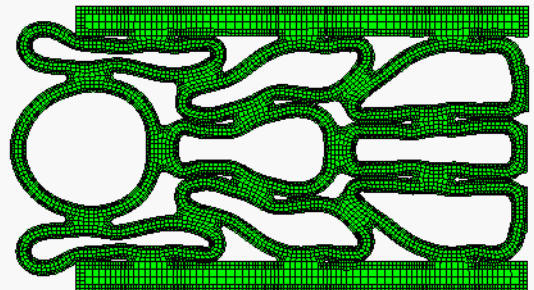
Q93_02
TIME: 2.50000E+00 STEP: 342929



Q93_02
TIME: 5.00000E+00 STEP: 771441



Q93_02
TIME: 7.50000E+00 STEP: *****



Q93_02
TIME: 9.10000E+00 STEP: *****

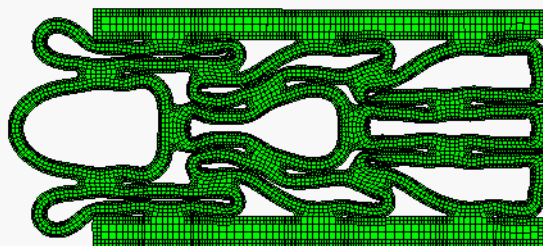


Figure 54 - Structure crushing in case Q93_02

Q93_02

TIME: 9.10000E+00 STEP: *****

MAX: +9.35E+02

---: +7.00E-01

---: +6.50E-01

---: +6.00E-01

---: +5.50E-01

---: +5.00E-01

---: +4.50E-01

---: +4.00E-01

---: +3.50E-01

---: +3.00E-01

---: +2.50E-01

---: +2.00E-01

---: +1.50E-01

---: +1.00E-01

---: +5.00E-02

MIN: +0.00E+00

ECRO 3 [N/A]

Parasitic plasticization ?

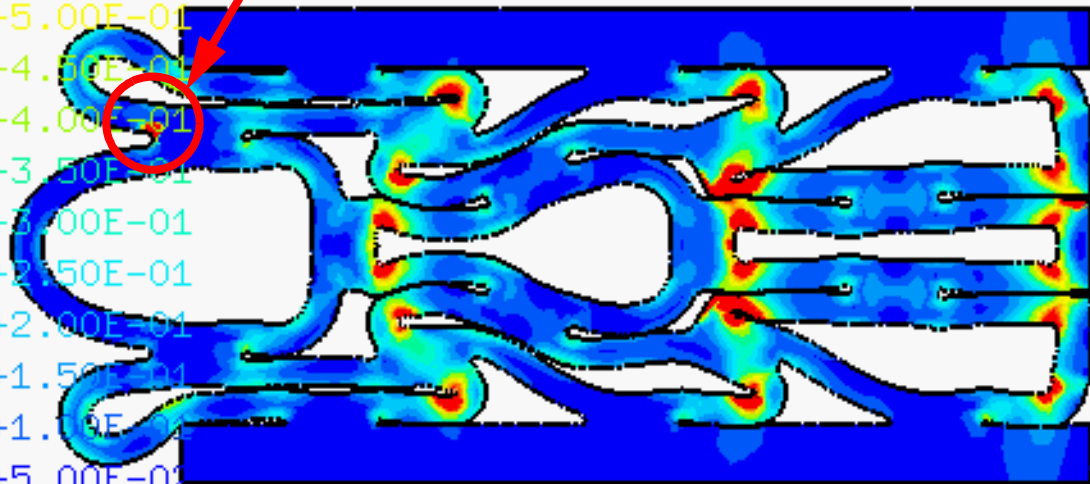


Figure 55 - Final plastic strain (at 9.1 s) in case Q93_02

Q93_02

TIME: 9.10000E+00 STEP: ****

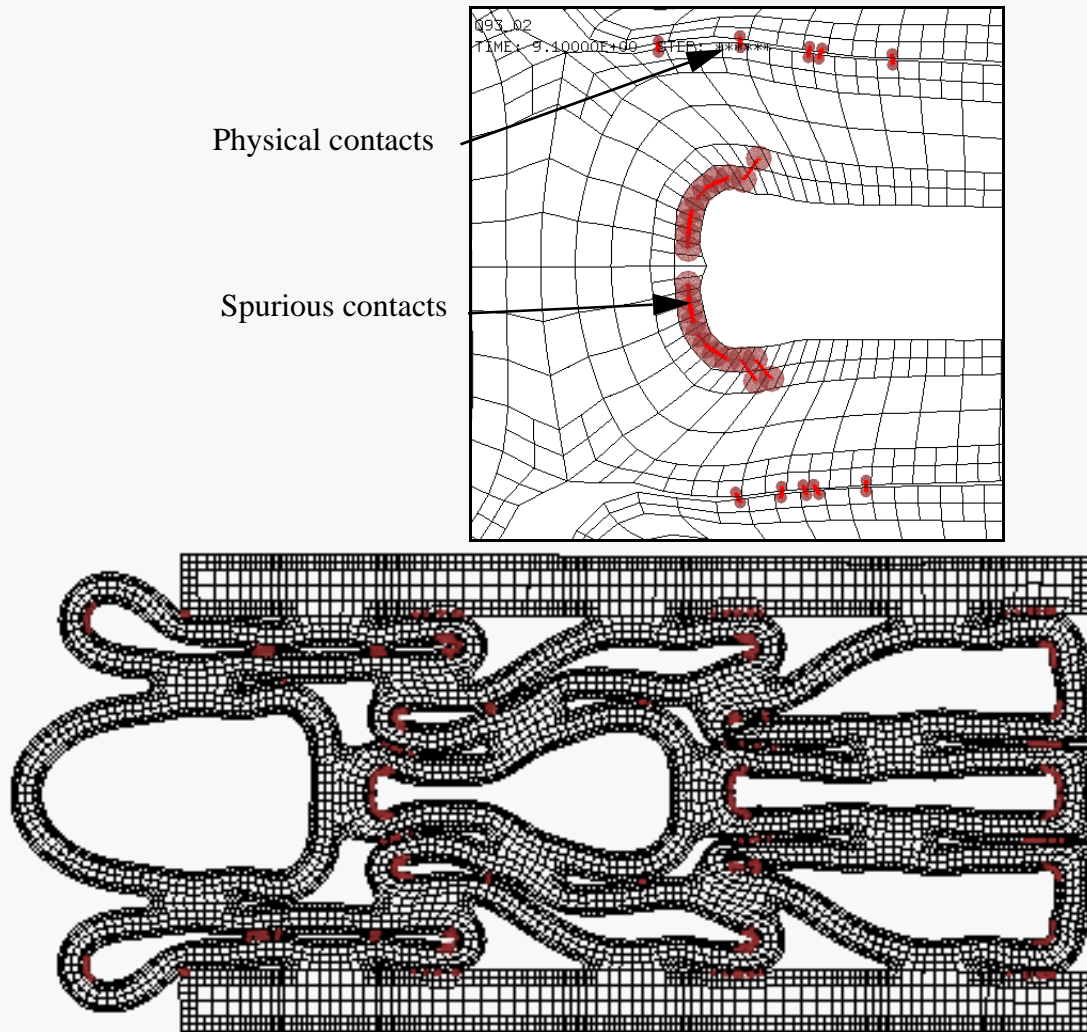


Figure 56 - Final contacts (at 9.1 s) in case Q93_02

Finally, Figure 57 compares the crushing force of case Q93_02 with the result of case QUA401. The Q9 solution exhibits some strong oscillations towards the end of the transient. These are possibly due to the parasitic contacts and will have to be analyzed. In any case, the force intensity is much lower than in the QUA4 case and in better accordance with experimentally observed values.

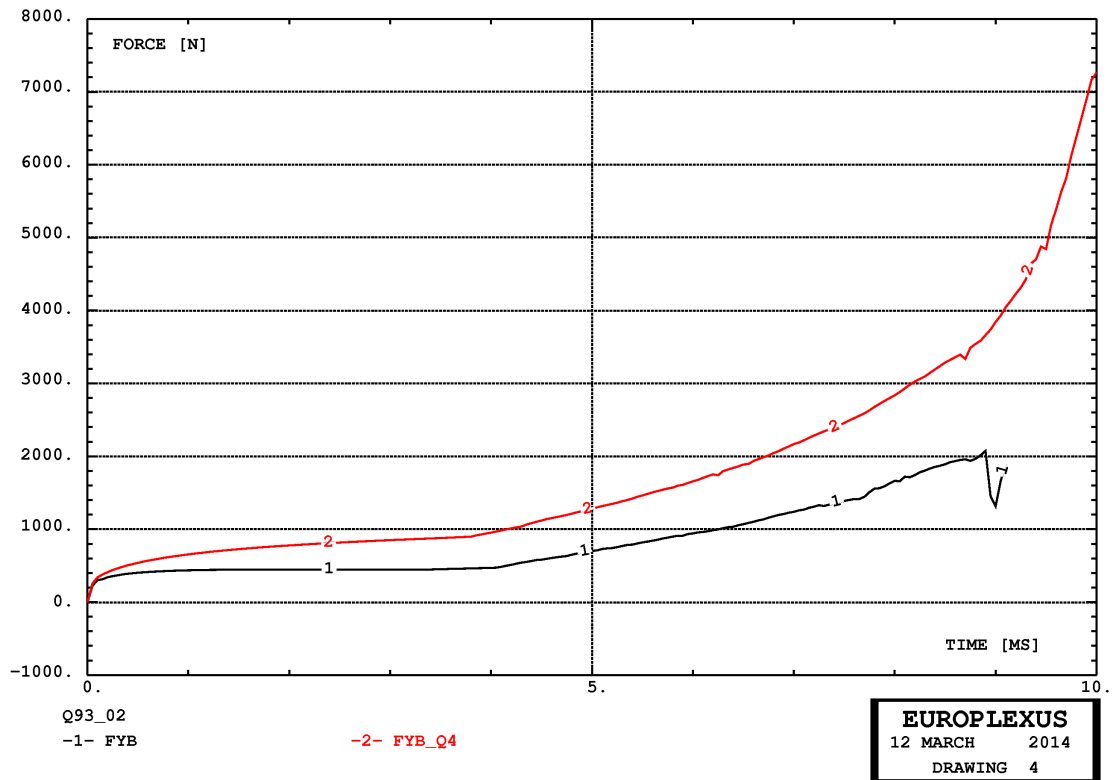


Figure 57 - Crushing force vs. imposed displacement in cases CAR401 and Q93_02

3. Pinball formulation for parabolic elements

We present now the native pinball formulation for parabolic elements. In 2D, the Q9 (continuum) element shape, i.e. the 9-node quadrilateral, will be considered. In 3D, the C27 (continuum) element shape, i.e. the 27-node hexahedron, will be considered, see [19] for details.

The pinballs construction for such elements is standard (see e.g. reference [13]), but we need to develop inverse mapping routines for such elements, in analogy with what had been done for the simpler (linear-displacement) element shapes, see references [17-18].

3.1 Inverse mapping for the parabolic 9-node quadrilateral in 2D space

The bi-parabolic quadrilateral in 2D space is shown in Figure 58. The element is one of the first implemented in EUROPLEXUS and dates back to the eighties, having been first implemented in the EURDYN-2 code at JRC Ispra [20-22]. The element formulation is summarized in reference [19]. However, the actual local numbering of the element nodes implemented in EUROPLEXUS is *not* the one mentioned in [19] (first the corner nodes, then the mid-sides and finally the central node), but the one shown in Figure 58, i.e. *circular* numbering (in order to make it compatible with the QUA9 element shape of the Cast3m pre-processor). With the numbering of Figure 58 the shape functions are:

$$\begin{aligned}
 N_1(\xi, \eta) &= \frac{1}{4}\xi\eta(\xi - 1)(\eta - 1) & N_5(\xi, \eta) &= \frac{1}{4}\xi\eta(\xi + 1)(\eta + 1) \\
 N_2(\xi, \eta) &= \frac{1}{2}\eta(1 - \xi^2)(\eta - 1) & N_6(\xi, \eta) &= \frac{1}{2}\eta(1 - \xi^2)(\eta + 1) \\
 N_3(\xi, \eta) &= \frac{1}{4}\xi\eta(\xi + 1)(\eta - 1) & N_7(\xi, \eta) &= \frac{1}{4}\xi\eta(\xi - 1)(\eta + 1) \\
 N_4(\xi, \eta) &= \frac{1}{2}\xi(\xi + 1)(1 - \eta^2) & N_8(\xi, \eta) &= \frac{1}{2}\xi(\xi - 1)(1 - \eta^2) \\
 N_9(\xi, \eta) &= (1 - \xi^2)(1 - \eta^2)
 \end{aligned} \tag{1}$$

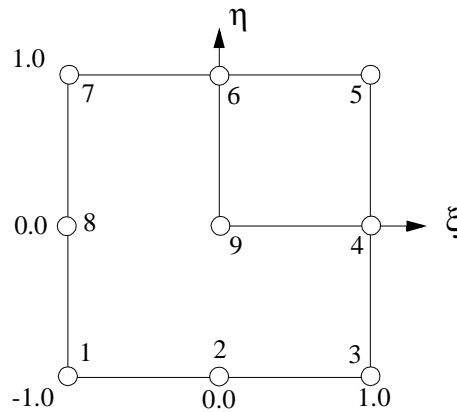


Figure 58 - The bi-parabolic 9-node 2D quadrilateral

and direct coordinate mapping is:

$$x = \sum_{I=1}^9 N_I x_I \quad ; \quad y = \sum_{I=1}^9 N_I y_I \quad (2)$$

By developing (2) with (1) we get:

$$\begin{aligned} F_1(\xi, \eta) &= a_1 \xi^2 \eta^2 + b_1 \xi^2 \eta + c_1 \xi \eta^2 + d_1 \xi \eta + e_1 \xi^2 + f_1 \eta^2 + g_1 \xi + h_1 \eta + i_1 - 4x = 0 \\ F_2(\xi, \eta) &= a_2 \xi^2 \eta^2 + b_2 \xi^2 \eta + c_2 \xi \eta^2 + d_2 \xi \eta + e_2 \xi^2 + f_2 \eta^2 + g_2 \xi + h_2 \eta + i_2 - 4y = 0 \end{aligned} \quad (3)$$

with:

$$\begin{aligned} a_1 &= x_1 - 2x_2 + x_3 - 2x_4 + x_5 - 2x_6 + x_7 - 2x_8 + 4x_9 & a_2 &= y_1 - 2y_2 + y_3 - 2y_4 + y_5 - 2y_6 + y_7 - 2y_8 + 4y_9 \\ b_1 &= -x_1 + 2x_2 - x_3 + x_5 - 2x_6 + x_7 & b_2 &= -y_1 + 2y_2 - y_3 + y_5 - 2y_6 + y_7 \\ c_1 &= -x_1 + x_3 - 2x_4 + x_5 - x_7 + 2x_8 & c_2 &= -y_1 + y_3 - 2y_4 + y_5 - y_7 + 2y_8 \\ d_1 &= x_1 - x_3 + x_5 - x_7 & d_2 &= y_1 - y_3 + y_5 - y_7 \\ e_1 &= 2x_4 + 2x_8 - 4x_9 & e_2 &= 2y_4 + 2y_8 - 4y_9 \\ f_1 &= 2x_2 + 2x_6 - 4x_9 & f_2 &= 2y_2 + 2y_6 - 4y_9 \\ g_1 &= 2x_4 - 2x_8 & g_2 &= 2y_4 - 2y_8 \\ h_1 &= -2x_2 + 2x_6 & h_2 &= -2y_2 + 2y_6 \\ i_1 &= 4x_9 & i_2 &= 4y_9 \end{aligned} \quad (4)$$

The system (3) being non-linear, it is not easy to be solved analytically. We prefer to resort to a numerical solution, obtained by the well-known Newton-Raphson iterative method. To this end, we re-formulate the problem by posing:

$$\underline{\chi} = \begin{bmatrix} \xi \\ \eta \end{bmatrix} \quad ; \quad \underline{F}(\underline{\chi}) = \begin{bmatrix} F_1(\xi, \eta) \\ F_2(\xi, \eta) \end{bmatrix} = \begin{bmatrix} F_1(\underline{\chi}) \\ F_2(\underline{\chi}) \end{bmatrix} \quad (5)$$

We search the value $\underline{\chi}^*$ of the independent variable for which we have $\underline{F}(\underline{\chi}^*) = \underline{0}$.

The Newton-Raphson method poses:

$$\underline{F}(\underline{\chi}) = \underline{F}(\underline{\chi}_0) + \left. \frac{\partial \underline{F}}{\partial \underline{\chi}} \right|_{\underline{\chi}_0} (\underline{\chi} - \underline{\chi}_0) \quad (6)$$

By imposing that $\underline{F}(\underline{\chi}) = \underline{0}$ we obtain:

$$\Delta \underline{\chi} = \underline{\chi} - \underline{\chi}_0 = \left[\left. \frac{\partial \underline{F}}{\partial \underline{\chi}} \right|_{\underline{\chi}_0} \right]^{-1} [0 - \underline{F}(\underline{\chi}_0)]. \quad (7)$$

The problem is solved iteratively:

1. Initialization: set $\xi_0 = 0$, $\eta_0 = 0$ (the centroid of the quadrilateral) so that $\underline{\chi}_0 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$,
and pose $\underline{\chi}^* = \underline{\chi}_0$.
2. Compute $F(\underline{\chi}^*)$ and $\left. \frac{\partial F}{\partial \underline{\chi}} \right|_{\underline{\chi}^*}$.
3. Compute $\Delta \underline{\chi} = \underline{\chi} - \underline{\chi}^* = \left[\left. \frac{\partial F}{\partial \underline{\chi}} \right|_{\underline{\chi}^*} \right]^{-1} (0 - F(\underline{\chi}^*))$.
4. Pose $\underline{\chi}^* \leftarrow \underline{\chi}^* + \Delta \underline{\chi}$.
5. Check for convergence: if $|\Delta \underline{\chi}| > \varepsilon$, then goto 2.

A graphical interpretation of this procedure for a function of only one variable is given in Figure 59.

From (5) and (3) we may write:

$$\frac{\partial F}{\partial \underline{\chi}} = \begin{bmatrix} \frac{\partial F_1}{\partial \xi} & \frac{\partial F_1}{\partial \eta} \\ \frac{\partial F_2}{\partial \xi} & \frac{\partial F_2}{\partial \eta} \end{bmatrix} \quad (8)$$

or, equivalently:

$$\frac{\partial F}{\partial \underline{\chi}} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \quad (9)$$

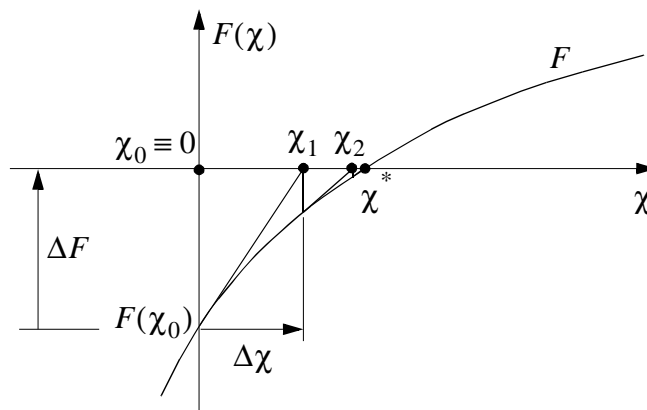


Figure 59 - The Newton-Raphson method for a function of one variable

having posed:

$$\begin{aligned}
\partial F_1/\partial \xi &= A = 2a_1\xi\eta^2 + 2b_1\xi\eta + c_1\eta^2 + d_1\eta + 2e_1\xi + g_1 \\
\partial F_1/\partial \eta &= B = 2a_1\xi^2\eta + b_1\xi^2 + 2c_1\xi\eta + d_1\xi + 2f_1\eta + h_1 \\
\partial F_2/\partial \xi &= C = 2a_2\xi\eta^2 + 2b_2\xi\eta + c_2\eta^2 + d_2\eta + 2e_2\xi + g_2 \\
\partial F_2/\partial \eta &= D = 2a_2\xi^2\eta + b_2\xi^2 + 2c_2\xi\eta + d_2\xi + 2f_2\eta + h_2
\end{aligned} \tag{10}$$

We obtain therefore:

$$\left[\frac{\partial F}{\partial \underline{\chi}} \right]^{-1} = \begin{bmatrix} \frac{\alpha_{11}}{\bar{D}} & \frac{\alpha_{21}}{\bar{D}} \\ \frac{\alpha_{12}}{\bar{D}} & \frac{\alpha_{22}}{\bar{D}} \end{bmatrix} \tag{11}$$

where:

$$\bar{D} = \det \begin{bmatrix} A & B \\ C & D \end{bmatrix} = AD - BC \quad (\text{must be } \neq 0!) \tag{12}$$

and:

$$\begin{aligned}
\alpha_{11} &= (-1)^{1+1} \cdot \text{cofactor}_{11} = D \\
\alpha_{12} &= (-1)^{1+2} \cdot \text{cofactor}_{12} = -C \\
\alpha_{21} &= (-1)^{2+1} \cdot \text{cofactor}_{21} = -B \\
\alpha_{22} &= (-1)^{2+2} \cdot \text{cofactor}_{22} = A
\end{aligned} \tag{13}$$

With (12) and (13), Eq. (11) becomes:

$$\left[\frac{\partial F}{\partial \underline{\chi}} \right]^{-1} = \frac{1}{AD - BC} \begin{bmatrix} D & -B \\ -C & A \end{bmatrix} \tag{14}$$

Then we may write:

$$\Delta \underline{\chi} = \underline{\chi} - \underline{\chi}^* = \begin{bmatrix} \xi \\ \eta \end{bmatrix} - \begin{bmatrix} \xi^* \\ \eta^* \end{bmatrix} = \begin{bmatrix} \xi - \xi^* \\ \eta - \eta^* \end{bmatrix} = -\frac{1}{AD - BC} \begin{bmatrix} D & -B \\ -C & A \end{bmatrix} \begin{bmatrix} F_1(\underline{\chi}^*) \\ F_2(\underline{\chi}^*) \end{bmatrix} \tag{15}$$

and finally:

$$\begin{aligned}
\xi - \xi^* &= \Delta \xi = -\frac{1}{AD - BC} [DF_1(\underline{\chi}^*) - BF_2(\underline{\chi}^*)] \\
\eta - \eta^* &= \Delta \eta = -\frac{1}{AD - BC} [-CF_1(\underline{\chi}^*) + AF_2(\underline{\chi}^*)]
\end{aligned} \tag{16}$$

3.2 Inverse mapping for the parabolic 27-node hexahedron in 3D space

The 27-node Lagrange parabolic element (C27) for 3D analysis in fast transient dynamics is shown in Figure 60 in the so-called parent element configuration, i.e. for normalized coordinates $-1 \leq \xi \leq 1$, $-1 \leq \eta \leq 1$, $-1 \leq \zeta \leq 1$. The local element numbering is as follows [19]: first the 8 vertex nodes, then the 6 (mid-)face nodes, then the 12 (mid-)corner nodes, and finally the central node.

The nodal shape functions $N_I(\xi, \eta, \zeta)$, $I = 1, \dots, 27$ are obtained by blending of the 1-D parabolic shape functions $L_K(\delta)$, $K = 1, \dots, 3$ given by (17):

$$\begin{aligned} L_1(\delta) &= \frac{1}{2}\delta(\delta-1) = \frac{\delta^2}{2} - \frac{\delta}{2} \\ L_2(\delta) &= (1+\delta)(1-\delta) = 1 - \delta^2, \\ L_3(\delta) &= \frac{1}{2}\delta(\delta+1) = \frac{\delta^2}{2} + \frac{\delta}{2} \end{aligned} \quad (17)$$

and result in the following expressions. For the 8 vertex nodes:

$$\begin{aligned} N_1(\xi, \eta, \zeta) &= L_1(\xi)L_1(\eta)L_1(\zeta) & N_5(\xi, \eta, \zeta) &= L_1(\xi)L_1(\eta)L_3(\zeta) \\ N_2(\xi, \eta, \zeta) &= L_3(\xi)L_1(\eta)L_1(\zeta) & N_6(\xi, \eta, \zeta) &= L_3(\xi)L_1(\eta)L_3(\zeta) \\ N_3(\xi, \eta, \zeta) &= L_3(\xi)L_3(\eta)L_1(\zeta) & N_7(\xi, \eta, \zeta) &= L_3(\xi)L_3(\eta)L_3(\zeta) \\ N_4(\xi, \eta, \zeta) &= L_1(\xi)L_3(\eta)L_1(\zeta) & N_8(\xi, \eta, \zeta) &= L_1(\xi)L_3(\eta)L_3(\zeta) \end{aligned} \quad (18)$$

For the 6 face nodes:

$$\begin{aligned} N_9(\xi, \eta, \zeta) &= L_2(\xi)L_2(\eta)L_1(\zeta) & N_{12}(\xi, \eta, \zeta) &= L_2(\xi)L_3(\eta)L_2(\zeta) \\ N_{10}(\xi, \eta, \zeta) &= L_2(\xi)L_1(\eta)L_2(\zeta) & N_{13}(\xi, \eta, \zeta) &= L_1(\xi)L_2(\eta)L_2(\zeta) \\ N_{11}(\xi, \eta, \zeta) &= L_3(\xi)L_2(\eta)L_2(\zeta) & N_{14}(\xi, \eta, \zeta) &= L_2(\xi)L_2(\eta)L_3(\zeta) \end{aligned} \quad (19)$$

For the 12 corner nodes:

$$\begin{aligned} N_{15}(\xi, \eta, \zeta) &= L_2(\xi)L_1(\eta)L_1(\zeta) & N_{21}(\xi, \eta, \zeta) &= L_3(\xi)L_3(\eta)L_2(\zeta) \\ N_{16}(\xi, \eta, \zeta) &= L_3(\xi)L_2(\eta)L_1(\zeta) & N_{22}(\xi, \eta, \zeta) &= L_1(\xi)L_3(\eta)L_2(\zeta) \\ N_{17}(\xi, \eta, \zeta) &= L_2(\xi)L_3(\eta)L_1(\zeta) & N_{23}(\xi, \eta, \zeta) &= L_2(\xi)L_1(\eta)L_3(\zeta) \\ N_{18}(\xi, \eta, \zeta) &= L_1(\xi)L_2(\eta)L_1(\zeta) & N_{24}(\xi, \eta, \zeta) &= L_3(\xi)L_2(\eta)L_3(\zeta) \\ N_{19}(\xi, \eta, \zeta) &= L_1(\xi)L_1(\eta)L_2(\zeta) & N_{25}(\xi, \eta, \zeta) &= L_2(\xi)L_3(\eta)L_3(\zeta) \\ N_{20}(\xi, \eta, \zeta) &= L_3(\xi)L_1(\eta)L_2(\zeta) & N_{26}(\xi, \eta, \zeta) &= L_1(\xi)L_2(\eta)L_3(\zeta) \end{aligned} \quad (20)$$

Finally, for the central node:

$$N_{27}(\xi, \eta, \zeta) = L_2(\xi)L_2(\eta)L_2(\zeta). \quad (21)$$

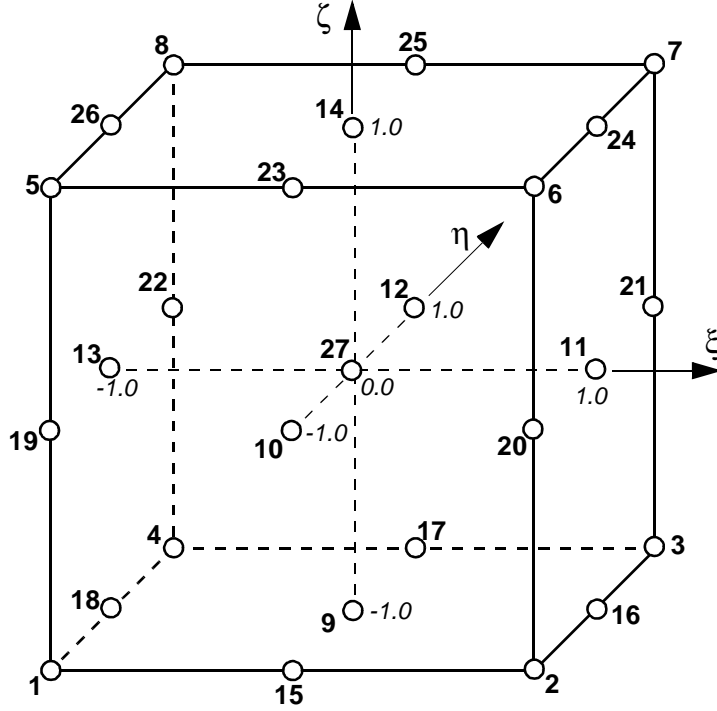


Figure 60 - The 27-node Lagrange parabolic element in 3D (C27)

The coordinate mapping is:

$$x = \sum_{I=1}^{27} N_I x_I \quad ; \quad y = \sum_{I=1}^{27} N_I y_I \quad ; \quad z = \sum_{I=1}^{27} N_I z_I \quad (22)$$

By developing (22) with (18-21) we get:

$$\begin{aligned}
F_1(\xi, \eta, \zeta) &= a_1 \xi^2 \eta^2 \zeta^2 + b_1 \xi^2 \eta^2 \zeta + c_1 \xi^2 \eta \zeta^2 + d_1 \xi \eta^2 \zeta^2 + e_1 \xi^2 \eta \zeta + f_1 \xi \eta^2 \zeta + g_1 \xi \eta \zeta^2 + \\
&+ h_1 \xi^2 \eta^2 + i_1 \xi^2 \zeta^2 + j_1 \eta^2 \zeta^2 + k_1 \xi \eta \zeta + l_1 \xi^2 \eta + m_1 \xi^2 \zeta + n_1 \xi \eta^2 + o_1 \xi \zeta^2 + \\
&+ p_1 \eta^2 \zeta + q_1 \eta \zeta^2 + r_1 \xi \eta + s_1 \xi \zeta + t_1 \eta \zeta + u_1 \xi^2 + v_1 \eta^2 + w_1 \zeta^2 + X_1 \xi + Y_1 \eta + Z_1 \zeta + A_1 - 8x = 0 \\
F_2(\xi, \eta, \zeta) &= a_2 \xi^2 \eta^2 \zeta^2 + b_2 \xi^2 \eta^2 \zeta + c_2 \xi^2 \eta \zeta^2 + d_2 \xi \eta^2 \zeta^2 + e_2 \xi^2 \eta \zeta + f_2 \xi \eta^2 \zeta + g_2 \xi \eta \zeta^2 + \\
&+ h_2 \xi^2 \eta^2 + i_2 \xi^2 \zeta^2 + j_2 \eta^2 \zeta^2 + k_2 \xi \eta \zeta + l_2 \xi^2 \eta + m_2 \xi^2 \zeta + n_2 \xi \eta^2 + o_2 \xi \zeta^2 + \\
&+ p_2 \eta^2 \zeta + q_2 \eta \zeta^2 + r_2 \xi \eta + s_2 \xi \zeta + t_2 \eta \zeta + u_2 \xi^2 + v_2 \eta^2 + w_2 \zeta^2 + X_2 \xi + Y_2 \eta + Z_2 \zeta + A_2 - 8y = 0 \\
F_3(\xi, \eta, \zeta) &= a_3 \xi^2 \eta^2 \zeta^2 + b_3 \xi^2 \eta^2 \zeta + c_3 \xi^2 \eta \zeta^2 + d_3 \xi \eta^2 \zeta^2 + e_3 \xi^2 \eta \zeta + f_3 \xi \eta^2 \zeta + g_3 \xi \eta \zeta^2 + \\
&+ h_3 \xi^2 \eta^2 + i_3 \xi^2 \zeta^2 + j_3 \eta^2 \zeta^2 + k_3 \xi \eta \zeta + l_3 \xi^2 \eta + m_3 \xi^2 \zeta + n_3 \xi \eta^2 + o_3 \xi \zeta^2 + \\
&+ p_3 \eta^2 \zeta + q_3 \eta \zeta^2 + r_3 \xi \eta + s_3 \xi \zeta + t_3 \eta \zeta + u_3 \xi^2 + v_3 \eta^2 + w_3 \zeta^2 + X_3 \xi + Y_3 \eta + Z_3 \zeta + A_3 - 8z = 0
\end{aligned} \quad (23)$$

where capital letters for the coefficients X_i, Y_i, Z_i ($i = 1, 2, 3$) have been used in order to avoid confusion with the nodal coordinates x_I, y_I, z_I ($I = 1, \dots, 27$).

The 27 coefficients a_1, \dots, A_1 are given by:

$$\begin{aligned}
a_1 &= 4x_9 + x_8 + x_7 + x_6 + x_5 + x_4 + x_3 - 8x_{27} - 2x_{26} - 2x_{25} - 2x_{24} - 2x_{23} - 2x_{22} - 2x_{21} - 2x_{20} + x_2 - 2x_{19} - 2x_{18} - 2x_{17} - \\
&\quad 2x_{16} - 2x_{15} + 4x_{14} + 4x_{13} + 4x_{12} + 4x_{11} + 4x_{10} + x_1 \\
b_1 &= -4x_9 + x_8 + x_7 + x_6 + x_5 - x_4 - x_3 - 2x_{26} - 2x_{25} - 2x_{24} - 2x_{23} - x_2 + 2x_{18} + 2x_{17} + 2x_{16} + 2x_{15} + 4x_{14} - x_1 \\
c_1 &= x_8 + x_7 - x_6 - x_5 + x_4 + x_3 - 2x_{25} + 2x_{23} - 2x_{22} - 2x_{21} + 2x_{20} - x_2 + 2x_{19} - 2x_{17} + 2x_{15} + 4x_{12} - 4x_{10} - x_1 \\
d_1 &= -x_8 + x_7 + x_6 - x_5 - x_4 + x_3 + 2x_{26} - 2x_{24} + 2x_{22} - 2x_{21} - 2x_{20} + x_2 + 2x_{19} + 2x_{18} - 2x_{16} - 4x_{13} + 4x_{11} - x_1 \\
e_1 &= x_8 + x_7 - x_6 - x_5 - x_4 - x_3 - 2x_{25} + 2x_{23} + x_2 + 2x_{17} - 2x_{15} + x_1 \\
f_1 &= -x_8 + x_7 + x_6 - x_5 + x_4 - x_3 + 2x_{26} - 2x_{24} - x_2 - 2x_{18} + 2x_{16} + x_1 \\
g_1 &= -x_8 + x_7 - x_6 + x_5 - x_4 + x_3 + 2x_{22} - 2x_{21} + 2x_{20} - x_2 - 2x_{19} + x_1 \\
h_1 &= 8x_{27} + 2x_{22} + 2x_{21} + 2x_{20} + 2x_{19} - 4x_{13} - 4x_{12} - 4x_{11} - 4x_{10} \\
i_1 &= -4x_9 + 8x_{27} + 2x_{26} + 2x_{24} + 2x_{18} + 2x_{16} - 4x_{14} - 4x_{13} - 4x_{11} \\
j_1 &= -4x_9 + 8x_{27} + 2x_{25} + 2x_{23} + 2x_{17} + 2x_{15} - 4x_{14} - 4x_{12} - 4x_{10} \\
k_1 &= -x_8 + x_7 - x_6 + x_5 + x_4 - x_3 + x_2 - x_1 \\
l_1 &= 2x_{22} + 2x_{21} - 2x_{20} - 2x_{19} - 4x_{12} + 4x_{10} \\
m_1 &= 4x_9 + 2x_{26} + 2x_{24} - 2x_{16} - 4x_{14} - 2x_{18} \\
n_1 &= -2x_{22} + 2x_{21} + 2x_{20} - 2x_{19} + 4x_{13} - 4x_{11} \\
o_1 &= -2x_{26} + 2x_{24} - 2x_{18} + 2x_{16} + 4x_{13} - 4x_{11} \\
p_1 &= 4x_9 + 2x_{25} + 2x_{23} - 2x_{17} - 2x_{15} - 4x_{14} \\
q_1 &= 2x_{25} - 2x_{23} + 2x_{17} - 2x_{15} - 4x_{12} + 4x_{10} \\
r_1 &= -2x_{22} + 2x_{21} - 2x_{20} + 2x_{19} \\
s_1 &= -2x_{26} + 2x_{24} + 2x_{18} - 2x_{16} \\
t_1 &= 2x_{25} - 2x_{23} - 2x_{17} + 2x_{15} \\
u_1 &= -8x_{27} + 4x_{13} + 4x_{11} \\
v_1 &= -8x_{27} + 4x_{12} + 4x_{10} \\
w_1 &= 4x_9 - 8x_{27} + 4x_{14} \\
X_1 &= -4x_{13} + 4x_{11} \\
Y_1 &= 4x_{12} - 4x_{10} \\
Z_1 &= -4x_9 + 4x_{14} \\
A_1 &= 8x_{27}
\end{aligned} \tag{24}$$

The coefficients a_2, \dots, A_2 and a_3, \dots, A_3 are given by the same expressions (4) but with y_I or, respectively, z_I in place of x_I .

The system (23) being non-linear, it is not easy to be solved analytically. We prefer to resort to a numerical solution, obtained by the well-known Newton-Raphson iterative method. To this end, we re-formulate the problem by posing:

$$\underline{\chi} = \begin{bmatrix} \xi \\ \eta \\ \zeta \end{bmatrix} \quad ; \quad \underline{F}(\underline{\chi}) = \begin{bmatrix} F_1(\xi, \eta, \zeta) \\ F_2(\xi, \eta, \zeta) \\ F_3(\xi, \eta, \zeta) \end{bmatrix} = \begin{bmatrix} F_1(\underline{\chi}) \\ F_2(\underline{\chi}) \\ F_3(\underline{\chi}) \end{bmatrix} \tag{25}$$

We search the value $\underline{\chi}^*$ of the independent variable for which we have $\underline{F}(\underline{\chi}^*) = \underline{0}$.

The Newton-Raphson method poses:

$$\underline{F}(\underline{\chi}) = \underline{F}(\underline{\chi}_0) + \left. \frac{\partial \underline{F}}{\partial \underline{\chi}} \right|_{\underline{\chi}_0} (\underline{\chi} - \underline{\chi}_0) \quad (26)$$

By imposing that $\underline{F}(\underline{\chi}) = \underline{0}$ we obtain:

$$\Delta \underline{\chi} = \underline{\chi} - \underline{\chi}_0 = \left[\left. \frac{\partial \underline{F}}{\partial \underline{\chi}} \right|_{\underline{\chi}_0} \right]^{-1} [\underline{0} - \underline{F}(\underline{\chi}_0)]. \quad (27)$$

The problem is solved iteratively:

1. Initialization: set $\xi_0 = 0$, $\eta_0 = 0$, $\zeta = 0$ (the centroid of the hexahedron) so that

$$\underline{\chi}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \text{ and pose } \underline{\chi}^* = \underline{\chi}_0.$$

2. Compute $\underline{F}(\underline{\chi}^*)$ and $\left. \frac{\partial \underline{F}}{\partial \underline{\chi}} \right|_{\underline{\chi}^*}$.

3. Compute $\Delta \underline{\chi} = \underline{\chi} - \underline{\chi}^* = \left[\left. \frac{\partial \underline{F}}{\partial \underline{\chi}} \right|_{\underline{\chi}^*} \right]^{-1} (\underline{0} - \underline{F}(\underline{\chi}^*))$.

4. Pose $\underline{\chi}^* \leftarrow \underline{\chi}^* + \Delta \underline{\chi}$.

5. Check for convergence: if $|\Delta \underline{\chi}| > \varepsilon$, then goto 2.

A graphical interpretation of this procedure for a function of only one variable is given in Figure 61.

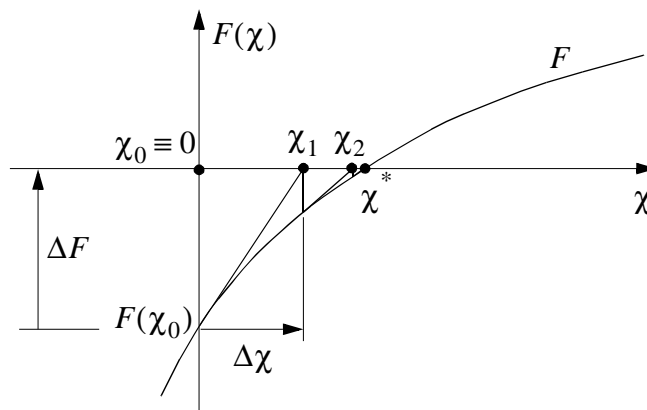


Figure 61 - The Newton-Raphson method for a function of one variable

From (25) and (23) we may write:

$$\frac{\partial F}{\partial \underline{\chi}} = \begin{bmatrix} \frac{\partial F_1}{\partial \xi} & \frac{\partial F_1}{\partial \eta} & \frac{\partial F_1}{\partial \zeta} \\ \frac{\partial F_2}{\partial \xi} & \frac{\partial F_2}{\partial \eta} & \frac{\partial F_2}{\partial \zeta} \\ \frac{\partial F_3}{\partial \xi} & \frac{\partial F_3}{\partial \eta} & \frac{\partial F_3}{\partial \zeta} \end{bmatrix} \quad (28)$$

or, equivalently:

$$\frac{\partial F}{\partial \underline{\chi}} = \begin{bmatrix} A & B & C \\ D & E & F \\ G & H & I \end{bmatrix} \quad (29)$$

having posed:

$$\begin{aligned} \partial F_1 / \partial \xi &= A = 2a_1 \xi \eta^2 \zeta^2 + 2b_1 \xi \eta^2 \zeta + 2c_1 \xi \eta \zeta^2 + d_1 \eta^2 \zeta^2 + 2e_1 \xi \eta \zeta + f_1 \eta^2 \zeta + g_1 \eta \zeta^2 + \\ &\quad + 2h_1 \xi \eta^2 + 2i_1 \xi \zeta^2 + k_1 \eta \zeta + 2l_1 \xi \eta + 2m_1 \xi \zeta + n_1 \eta^2 + o_1 \zeta^2 + r_1 \eta + s_1 \zeta + 2u_1 \xi + X_1 \\ \partial F_1 / \partial \eta &= B = 2a_1 \xi^2 \eta \zeta^2 + 2b_1 \xi^2 \eta \zeta + c_1 \xi^2 \zeta^2 + 2d_1 \xi \eta \zeta^2 + e_1 \xi^2 \zeta + 2f_1 \xi \eta \zeta + g_1 \xi \zeta^2 + \\ &\quad + 2h_1 \xi^2 \eta + 2j_1 \eta \zeta^2 + k_1 \xi \zeta + l_1 \xi^2 + 2n_1 \xi \eta + 2p_1 \eta \zeta + q_1 \zeta^2 + r_1 \xi + t_1 \zeta + 2v_1 \eta + Y_1 \\ \partial F_1 / \partial \zeta &= C = 2a_1 \xi^2 \eta^2 \zeta + b_1 \xi^2 \eta^2 + 2c_1 \xi^2 \eta \zeta + 2d_1 \xi \eta^2 \zeta + e_1 \xi^2 \eta + f_1 \xi \eta^2 + 2g_1 \xi \eta \zeta + \\ &\quad + 2i_1 \xi^2 \zeta + 2j_1 \eta^2 \zeta + k_1 \xi \eta + m_1 \xi^2 + 2o_1 \xi \zeta + p_1 \eta^2 + 2q_1 \eta \zeta + s_1 \xi + t_1 \eta + 2w_1 \zeta + Z_1 \\ \partial F_2 / \partial \xi &= D = 2a_2 \xi \eta^2 \zeta^2 + 2b_2 \xi \eta^2 \zeta + 2c_2 \xi \eta \zeta^2 + d_2 \eta^2 \zeta^2 + 2e_2 \xi \eta \zeta + f_2 \eta^2 \zeta + g_2 \eta \zeta^2 + \\ &\quad + 2h_2 \xi \eta^2 + 2i_2 \xi \zeta^2 + k_2 \eta \zeta + 2l_2 \xi \eta + 2m_2 \xi \zeta + n_2 \eta^2 + o_2 \zeta^2 + r_2 \eta + s_2 \zeta + 2u_2 \xi + X_2 \\ \partial F_2 / \partial \eta &= E = 2a_2 \xi^2 \eta \zeta^2 + 2b_2 \xi^2 \eta \zeta + c_2 \xi^2 \zeta^2 + 2d_2 \xi \eta \zeta^2 + e_2 \xi^2 \zeta + 2f_2 \xi \eta \zeta + g_2 \xi \zeta^2 + \\ &\quad + 2h_2 \xi^2 \eta + 2j_2 \eta \zeta^2 + k_2 \xi \zeta + l_2 \xi^2 + 2n_2 \xi \eta + 2p_2 \eta \zeta + q_2 \zeta^2 + r_2 \xi + t_2 \zeta + 2v_2 \eta + Y_2 \\ \partial F_2 / \partial \zeta &= F = 2a_2 \xi^2 \eta^2 \zeta + b_2 \xi^2 \eta^2 + 2c_2 \xi^2 \eta \zeta + 2d_2 \xi \eta^2 \zeta + e_2 \xi^2 \eta + f_2 \xi \eta^2 + 2g_2 \xi \eta \zeta + \\ &\quad + 2i_2 \xi^2 \zeta + 2j_2 \eta^2 \zeta + k_2 \xi \eta + m_2 \xi^2 + 2o_2 \xi \zeta + p_2 \eta^2 + 2q_2 \eta \zeta + s_2 \xi + t_2 \eta + 2w_2 \zeta + Z_2 \\ \partial F_3 / \partial \xi &= G = 2a_3 \xi \eta^2 \zeta^2 + 2b_3 \xi \eta^2 \zeta + 2c_3 \xi \eta \zeta^2 + d_3 \eta^2 \zeta^2 + 2e_3 \xi \eta \zeta + f_3 \eta^2 \zeta + g_3 \eta \zeta^2 + \\ &\quad + 2h_3 \xi \eta^2 + 2i_3 \xi \zeta^2 + k_3 \eta \zeta + 2l_3 \xi \eta + 2m_3 \xi \zeta + n_3 \eta^2 + o_3 \zeta^2 + r_3 \eta + s_3 \zeta + 2u_3 \xi + X_3 \\ \partial F_3 / \partial \eta &= H = 2a_3 \xi^2 \eta \zeta^2 + 2b_3 \xi^2 \eta \zeta + c_3 \xi^2 \zeta^2 + 2d_3 \xi \eta \zeta^2 + e_3 \xi^2 \zeta + 2f_3 \xi \eta \zeta + g_3 \xi \zeta^2 + \\ &\quad + 2h_3 \xi^2 \eta + 2j_3 \eta \zeta^2 + k_3 \xi \zeta + l_3 \xi^2 + 2n_3 \xi \eta + 2p_3 \eta \zeta + q_3 \zeta^2 + r_3 \xi + t_3 \zeta + 2v_3 \eta + Y_3 \\ \partial F_3 / \partial \zeta &= I = 2a_3 \xi^2 \eta^2 \zeta + b_3 \xi^2 \eta^2 + 2c_3 \xi^2 \eta \zeta + 2d_3 \xi \eta^2 \zeta + e_3 \xi^2 \eta + f_3 \xi \eta^2 + 2g_3 \xi \eta \zeta + \\ &\quad + 2i_3 \xi^2 \zeta + 2j_3 \eta^2 \zeta + k_3 \xi \eta + m_3 \xi^2 + 2o_3 \xi \zeta + p_3 \eta^2 + 2q_3 \eta \zeta + s_3 \xi + t_3 \eta + 2w_3 \zeta + Z_3 \end{aligned} \quad (30)$$

We obtain therefore:

$$\left[\frac{\partial \bar{F}}{\partial \bar{\chi}} \right]^{-1} = \begin{bmatrix} \frac{\alpha_{11}}{\bar{D}} & \frac{\alpha_{21}}{\bar{D}} & \frac{\alpha_{31}}{\bar{D}} \\ \frac{\alpha_{12}}{\bar{D}} & \frac{\alpha_{22}}{\bar{D}} & \frac{\alpha_{32}}{\bar{D}} \\ \frac{\alpha_{13}}{\bar{D}} & \frac{\alpha_{23}}{\bar{D}} & \frac{\alpha_{33}}{\bar{D}} \end{bmatrix} \quad (31)$$

where:

$$\bar{D} = \det \begin{bmatrix} A & B & C \\ D & E & F \\ G & H & I \end{bmatrix} = A(EI - FH) - B(DI - FG) + C(DH - EG) \quad (\text{must be } \neq 0!) \quad (32)$$

and:

$$\begin{aligned} \alpha_{11} &= (-1)^{1+1} \cdot \text{cofactor}_{11} = EI - FH \\ \alpha_{12} &= (-1)^{1+2} \cdot \text{cofactor}_{12} = -(DI - FG) \\ \alpha_{13} &= (-1)^{1+3} \cdot \text{cofactor}_{13} = DH - EG \\ \alpha_{21} &= (-1)^{2+1} \cdot \text{cofactor}_{21} = -(BI - CH) \\ \alpha_{22} &= (-1)^{2+2} \cdot \text{cofactor}_{22} = AI - CG \\ \alpha_{23} &= (-1)^{2+3} \cdot \text{cofactor}_{23} = -(AH - BG) \\ \alpha_{31} &= (-1)^{3+1} \cdot \text{cofactor}_{31} = BF - CE \\ \alpha_{32} &= (-1)^{3+2} \cdot \text{cofactor}_{32} = -(AF - CD) \\ \alpha_{33} &= (-1)^{3+3} \cdot \text{cofactor}_{33} = AE - BD \end{aligned} \quad (33)$$

With (32) and (33), Eq. (31) becomes:

$$\left[\frac{\partial \bar{F}}{\partial \bar{\chi}} \right]^{-1} = \frac{1}{A(EI - FH) - B(DI - FG) + C(DH - EG)} \begin{bmatrix} (EI - FH) & -(BI - CH) & (BF - CE) \\ -(DI - FG) & (AI - CG) & -(AF - CD) \\ (DH - EG) & -(AH - BG) & (AE - BD) \end{bmatrix} \quad (34)$$

Then we may write:

$$\Delta \underline{\chi} = \underline{\chi} - \underline{\chi}^* = \begin{bmatrix} \xi \\ \eta \\ \zeta \end{bmatrix} - \begin{bmatrix} \xi^* \\ \eta^* \\ \zeta^* \end{bmatrix} = \begin{bmatrix} \xi - \xi^* \\ \eta - \eta^* \\ \zeta - \zeta^* \end{bmatrix} = \frac{1}{A(EI - FH) - B(DI - FG) + C(DH - EG)} \begin{bmatrix} (EI - FH) & -(BI - CH) & (BF - CE) \\ -(DI - FG) & (AI - CG) & -(AF - CD) \\ (DH - EG) & -(AH - BG) & (AE - BD) \end{bmatrix} \begin{bmatrix} F_1(\underline{\chi}^*) \\ F_2(\underline{\chi}^*) \\ F_3(\underline{\chi}^*) \end{bmatrix} \quad (35)$$

and finally:

$$\begin{aligned} \xi - \xi^* = \Delta \xi &= -\frac{[(EI - FH)F_1(\underline{\chi}^*) - (BI - CH)F_2(\underline{\chi}^*) + (BF - CE)F_3(\underline{\chi}^*)]}{A(EI - FH) - B(DI - FG) + C(DH - EG)} \\ \eta - \eta^* = \Delta \eta &= -\frac{[-(DI - FG)F_1(\underline{\chi}^*) + (AI - CG)F_2(\underline{\chi}^*) - (AF - CD)F_3(\underline{\chi}^*)]}{A(EI - FH) - B(DI - FG) + C(DH - EG)}. \quad (36) \\ \zeta - \zeta^* = \Delta \zeta &= -\frac{[(DH - EG)F_1(\underline{\chi}^*) - (AH - BG)F_2(\underline{\chi}^*) + (AE - BD)F_3(\underline{\chi}^*)]}{A(EI - FH) - B(DI - FG) + C(DH - EG)} \end{aligned}$$

The algebraic manipulations to obtain the coefficients (24) are tedious and error-prone. Therefore, use has been made of the free software Maxima in order to do part of the work. The input for the Maxima code is listed in the appendix (see file `test03.wxm`) and an example of printed output from Maxima is shown in Figure 62.

```
(%i43) expand(Sx8);
(%o43) 4 a9 x^2 y^2 z^2 + a8 x^2 y^2 z^2 + a7 x^2 y^2 z^2 + a6 x^2 y^2 z^2 + a5 x^2 y^2 z^2 + a4 x^2 y^2
z^2 + a3 x^2 y^2 z^2 - 8 a27 x^2 y^2 z^2 - 2 a26 x^2 y^2 z^2 - 2 a25 x^2 y^2 z^2 - 2 a24 x^2 y^2 z^2 - 2
a23 x^2 y^2 z^2 - 2 a22 x^2 y^2 z^2 - 2 a21 x^2 y^2 z^2 - 2 a20 x^2 y^2 z^2 + a2 x^2 y^2 z^2 - 2 a19 x^2
y^2 z^2 - 2 a18 x^2 y^2 z^2 - 2 a17 x^2 y^2 z^2 - 2 a16 x^2 y^2 z^2 - 2 a15 x^2 y^2 z^2 + 4 a14 x^2 y^2
z^2 + 4 a13 x^2 y^2 z^2 + 4 a12 x^2 y^2 z^2 + 4 a11 x^2 y^2 z^2 + 4 a10 x^2 y^2 z^2 + a1 x^2 y^2 z^2 - a8
x y^2 z^2 + a7 x y^2 z^2 + a6 x y^2 z^2 - a5 x y^2 z^2 - a4 x y^2 z^2 + a3 x y^2 z^2 + 2 a26 x y^2 z^2 -
2 a24 x y^2 z^2 + 2 a22 x y^2 z^2 - 2 a21 x y^2 z^2 - 2 a20 x y^2 z^2 + a2 x y^2 z^2 + 2 a19 x y^2
z^2 + 2 a18 x y^2 z^2 - 2 a16 x y^2 z^2 - 4 a13 x y^2 z^2 + 4 a11 x y^2 z^2 - a1 x y^2 z^2 - 4 a9 y^2
z^2 + 8 a27 y^2 z^2 + 2 a25 y^2 z^2 + 2 a23 y^2 z^2 + 2 a17 y^2 z^2 + 2 a15 y^2 z^2 - 4 a14 y^2 z^2 - 4
a12 y^2 z^2 - 4 a10 y^2 z^2 + a8 x^2 y z^2 + a7 x^2 y z^2 - a6 x^2 y z^2 - a5 x^2 y z^2 + a4 x^2 y z^2 +
a3 x^2 y z^2 - 2 a25 x^2 y z^2 + 2 a23 x^2 y z^2 - 2 a22 x^2 y z^2 - 2 a21 x^2 y z^2 + 2 a20 x^2 y
z^2 - a2 x^2 y z^2 + 2 a19 x^2 y z^2 - 2 a17 x^2 y z^2 + 2 a15 x^2 y z^2 + 4 a12 x^2 y z^2 - 4 a10 x^2
y z^2 - a1 x^2 y z^2 - a8 x y z^2 + a7 x y z^2 - a6 x y z^2 + a5 x y z^2 - a4 x y z^2 + a3 x y z^2 + 2
a22 x y z^2 - 2 a21 x y z^2 + 2 a20 x y z^2 - a2 x y z^2 - 2 a19 x y z^2 + a1 x y z^2 + 2 a25 y
z^2 - 2 a23 y z^2 + 2 a17 y z^2 - 2 a15 y z^2 - 4 a12 y z^2 + 4 a10 y z^2 - 4 a9 x^2 z^2 + 8 a27 x^2
z^2 + 2 a26 x^2 z^2 + 2 a24 x^2 z^2 + 2 a18 x^2 z^2 + 2 a16 x^2 z^2 - 4 a14 x^2 z^2 - 4 a13 x^2 z^2 - 4
a11 x^2 z^2 - 2 a26 x z^2 + 2 a24 x z^2 - 2 a18 x z^2 + 2 a16 x z^2 + 4 a13 x z^2 - 4 a11 x z^2 + 4
a9 z^2 - 8 a27 z^2 + 4 a14 z^2 - 4 a9 x^2 y^2 z + a8 x^2 y^2 z + a7 x^2 y^2 z + a6 x^2 y^2 z + a5 x^2
y^2 z - a4 x^2 y^2 z - a3 x^2 y^2 z - 2 a26 x^2 y^2 z - 2 a25 x^2 y^2 z - 2 a24 x^2 y^2 z - 2 a23 x^2
y^2 z - a2 x^2 y^2 z + 2 a18 x^2 y^2 z + 2 a17 x^2 y^2 z + 2 a16 x^2 y^2 z + 2 a15 x^2 y^2 z + 4 a14
x^2 y^2 z - a1 x^2 y^2 z - a8 x y^2 z + a7 x y^2 z + a6 x y^2 z - a5 x y^2 z + a4 x y^2 z - a3 x y^2 z
+ 2 a26 x y^2 z - 2 a24 x y^2 z - a2 x y^2 z - 2 a18 x y^2 z + 2 a16 x y^2 z + a1 x y^2 z + 4 a9
y^2 z + 2 a25 y^2 z + 2 a23 y^2 z - 2 a17 y^2 z - 2 a15 y^2 z - 4 a14 y^2 z + a8 x^2 y z + a7 x^2 y
z - a6 x^2 y z - a5 x^2 y z - a4 x^2 y z - a3 x^2 y z - 2 a25 x^2 y z + 2 a23 x^2 y z + a2 x^2 y z +
2 a17 x^2 y z - 2 a15 x^2 y z + a1 x^2 y z - a8 x y z + a7 x y z - a6 x y z + a5 x y z + a4 x y
z - a3 x y z + a2 x y z - a1 x y z + 2 a25 y z - 2 a23 y z - 2 a17 y z + 2 a15 y z + 4 a9 x^2 z
+ 2 a26 x^2 z + 2 a24 x^2 z - 2 a18 x^2 z - 2 a16 x^2 z - 4 a14 x^2 z - 2 a26 x z + 2 a24 x z + 2
a18 x z - 2 a16 x z - 4 a9 z + 4 a14 z + 8 a27 x^2 y^2 z + 2 a22 x^2 y^2 z + 2 a21 x^2 y^2 z + 2 a20 x^2
y^2 z + 2 a19 x^2 y^2 z - 4 a13 x^2 y^2 z - 4 a12 x^2 y^2 z - 4 a11 x^2 y^2 z - 4 a10 x^2 y^2 z - 2 a22 x y^2 z + 2
a21 x y^2 z + 2 a20 x y^2 z - 2 a19 x y^2 z + 4 a13 x y^2 z - 4 a11 x y^2 z - 8 a27 y^2 z + 4 a12 y^2 z + 4 a10
y^2 z + 2 a22 x^2 y z + 2 a21 x^2 y z - 2 a20 x^2 y z - 2 a19 x^2 y z - 4 a12 x^2 y z + 4 a10 x^2 y z - 2 a22 x
y z + 2 a21 x y z - 2 a20 x y z + 2 a19 x y z + 4 a12 y z - 4 a10 y z - 8 a27 x^2 z + 4 a13 x^2 z + 4 a11 x^2 z -
4 a13 x z + 4 a11 x z + 8 a27
```

Figure 62 - Output from the Maxima symbolic calculation package

3.3 Simple numerical examples

The “native” pinball formulation for parabolic elements introduced above is now tested on some simple numerical examples.

We start from 2D and consider the “perfect” impact of two quadrilaterals, as shown in Figure 63. Each quadrilateral measures 2×2 m and has an initial velocity of 100 m/s in the vertical direction (with opposite signs as shown). The initial gap between the two quadrilaterals is zero, although in Figure 63 a certain gap is shown for clarity. A total of 100 time steps is performed.

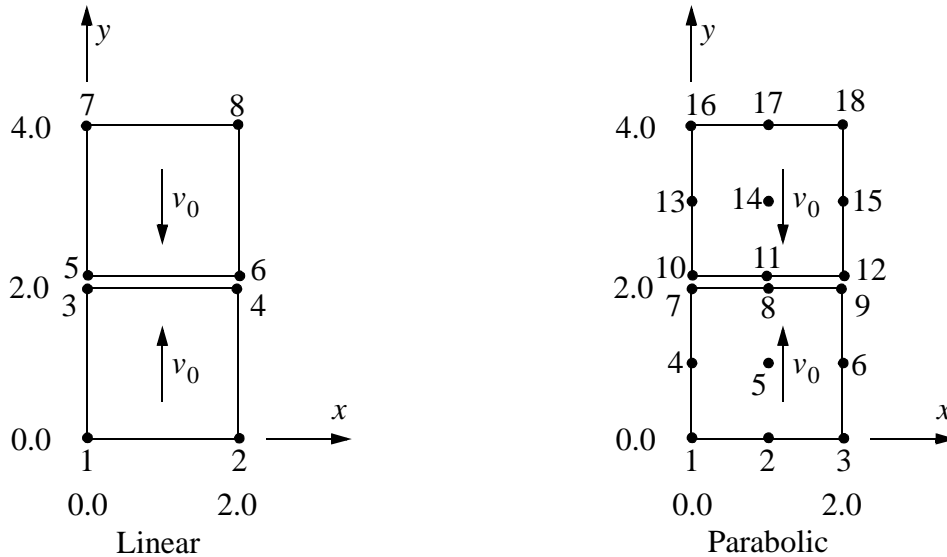


Figure 63 - Definition and initial mesh of the quadrilateral impact problem

First, a reference solution is obtained by means of linear elements (Q41L and Q42L), see left part of Figure 63. Then, the same problem is solved with quadratic elements (Q92 and Q93) using the native pinball formulation for such elements. All performed calculations are summarized in Table 4.

Case	Mesh	Notes	Steps	CPU [s]	Els*step
PBQ401	2 Q41L	0-level pinballs	100	0.55	202
PBQ402	2 Q41L	MLEV 1 EQVF	100	0.55	202
PBQ403	2 Q41L	MLEV 2 EQVF	100	0.55	202
PBQ404	2 Q41L	MLEV 3 EQVF	100	0.64	202
PBQ421	2 Q42L	0-level pinballs	100	0.58	202
PBQ422	2 Q42L	MLEV 1 EQVF	100	0.66	202
PBQ423	2 Q42L	MLEV 2 EQVF	100	0.58	202
PBQ424	2 Q42L	MLEV 3 EQVF	100	0.55	202

Table 4 - Calculations for the quadrilateral impact problem in 2D with linear elements

3.3.1 2D solutions with linear elements

PBQ401

This test uses 0-level (parent) pinballs. The vertical displacement of node 1 is plotted in Figure 64 for this test case and the following 7 cases (all solutions with linear elements). The initial and final configuration for this solution are shown in Figure 65. The solution is degenerated, in the sense that all nodes are instantaneously stopped at step 0, due to the fact that only one element is used on each side of the impact, and the contact points are at the centres of the parent pinballs, which coincide with the element centroids. Therefore, the contact force is equally distributed on all nodes and the effect is that the velocity becomes instantly zero at the initial step. No rebound occurs.

PBQ402

This test is similar to PBQ401 but uses level 1 pinballs (MLEV 1). Additionally, the EQVF option is activated, according to which the volume of the final (contacting) pinballs is equivalent to the volume of the corresponding parent element portion. The solution is shown in Figure 66. In this case some rebound occurs.

PBQ403

This test is similar to PBQ402 but uses MLEV 2. A solution is obtained despite the fact that some redundancies in the contact constraints can occur in this case, and is shown in Figure 67. In this case some rebound occurs.

PBQ404

This test is similar to PBQ403 but uses MLEV 3. A solution is obtained despite the fact that several redundancies in the contact constraints occur in this case, and is shown in Figure 68. In this case some rebound occurs.

PBQ421

This test is similar to PBQ401 but uses the fully integrated element Q42L instead of the reduced-integrated element Q41L. The solution is shown in Figure 69. Like in case PBQ401, no rebound occurs.

PBQ422

This test is similar to PBQ402 but uses the fully integrated element Q42L instead of the reduced-integrated element Q41L. The solution is shown in Figure 70.

PBQ423

This test is similar to PBQ403 but uses the fully integrated element Q42L instead of the reduced-integrated element Q41L. The solution is shown in Figure 71.

PBQ424

This test is similar to PBQ404 but uses the fully integrated element Q42L instead of the reduced-integrated element Q41L. The solution is shown in Figure 72.

We may conclude that in the case of linear elements, the solutions as far as contact is concerned are identical with the reduced integrated and with the fully integrated element.

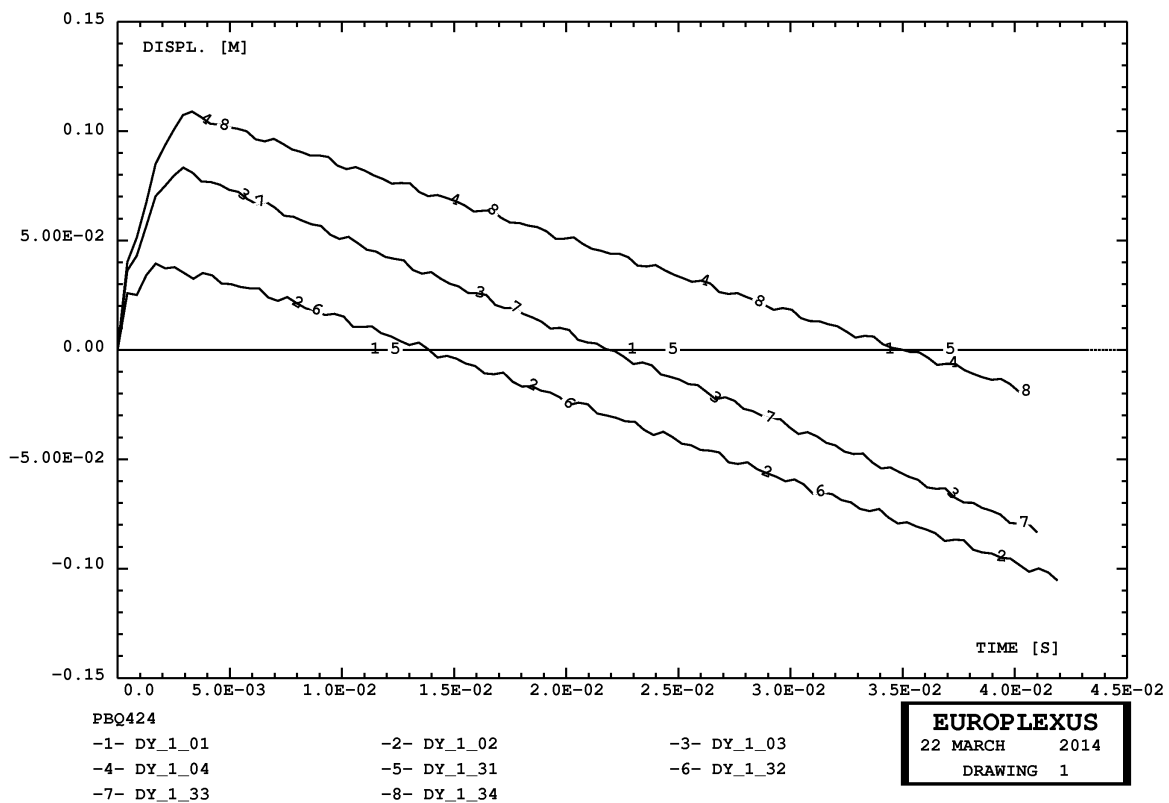


Figure 64 - Vertical displacement of node 1 in the 8 linear element solutions PBQXXX

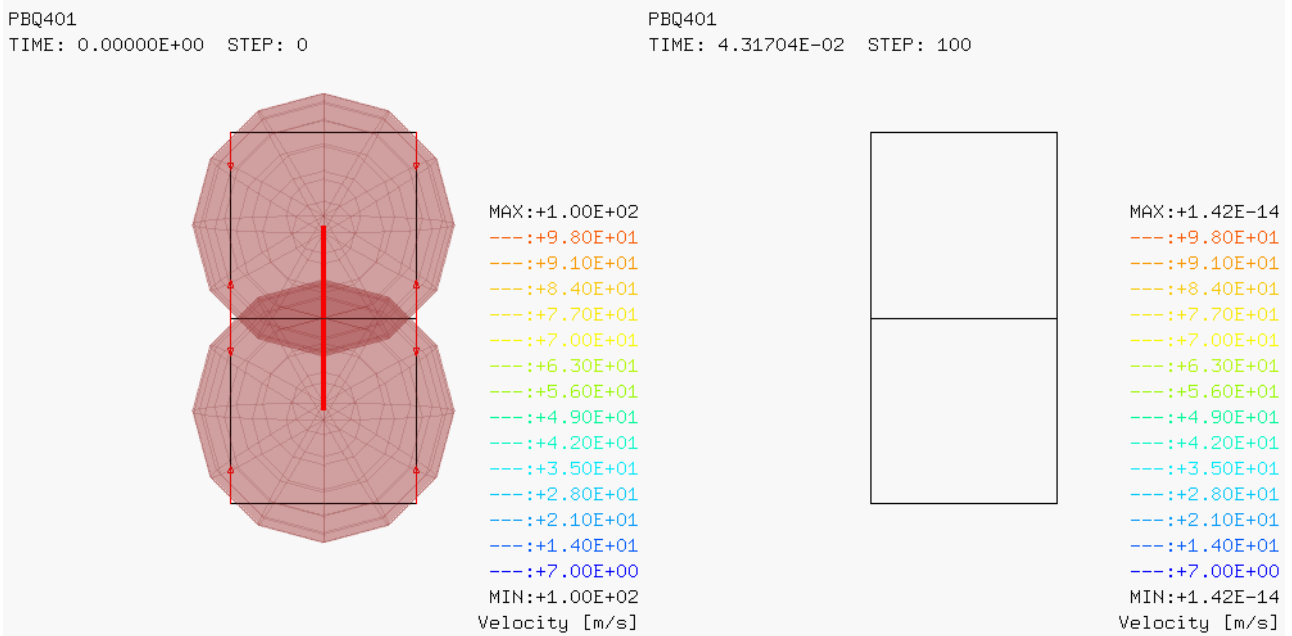


Figure 65 - Initial and final configurations for test PBQ401

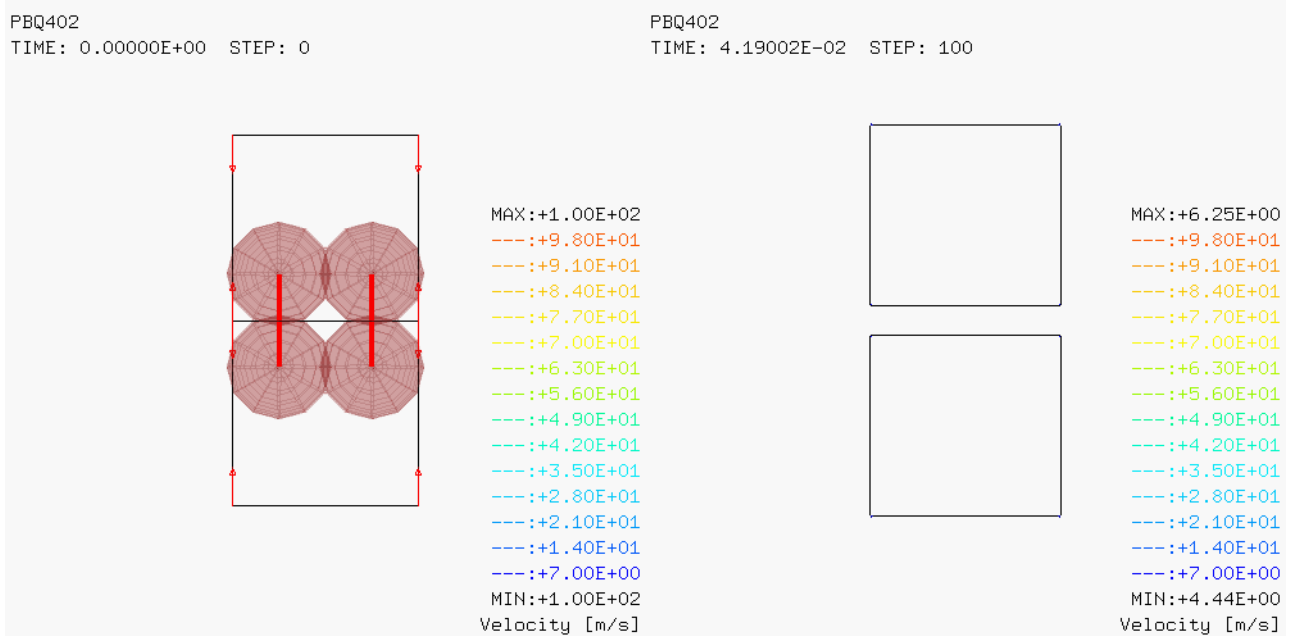


Figure 66 - Initial and final configurations for test PBQ402

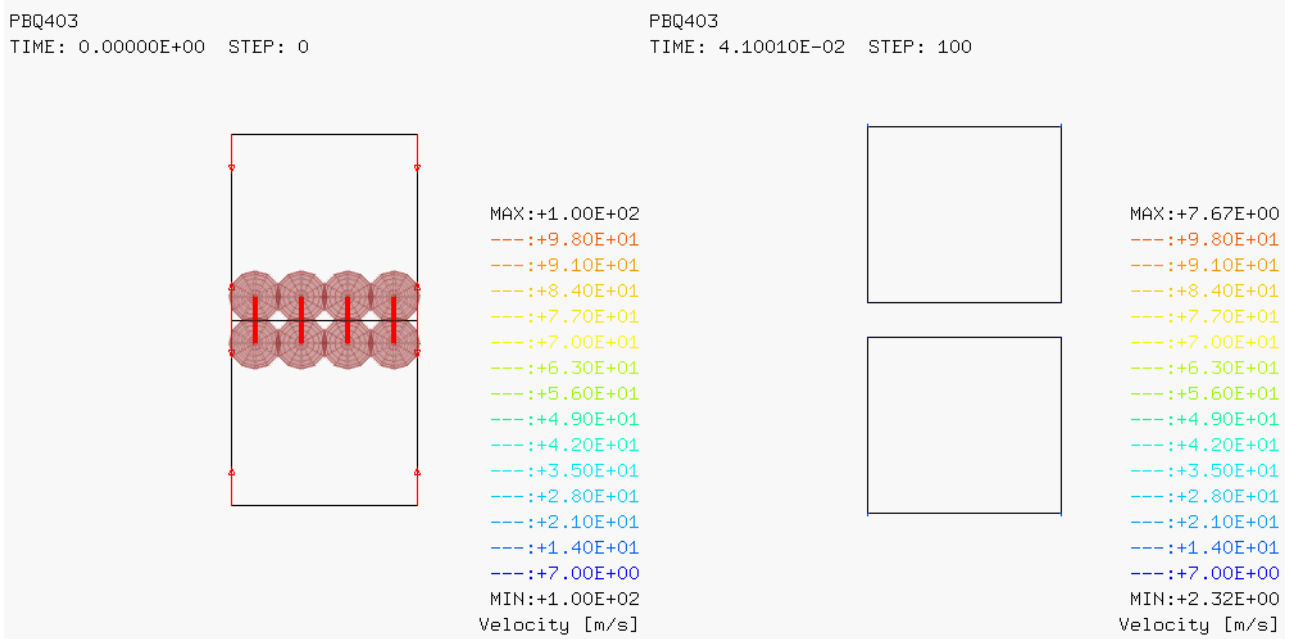


Figure 67 - Initial and final configurations for test PBQ403

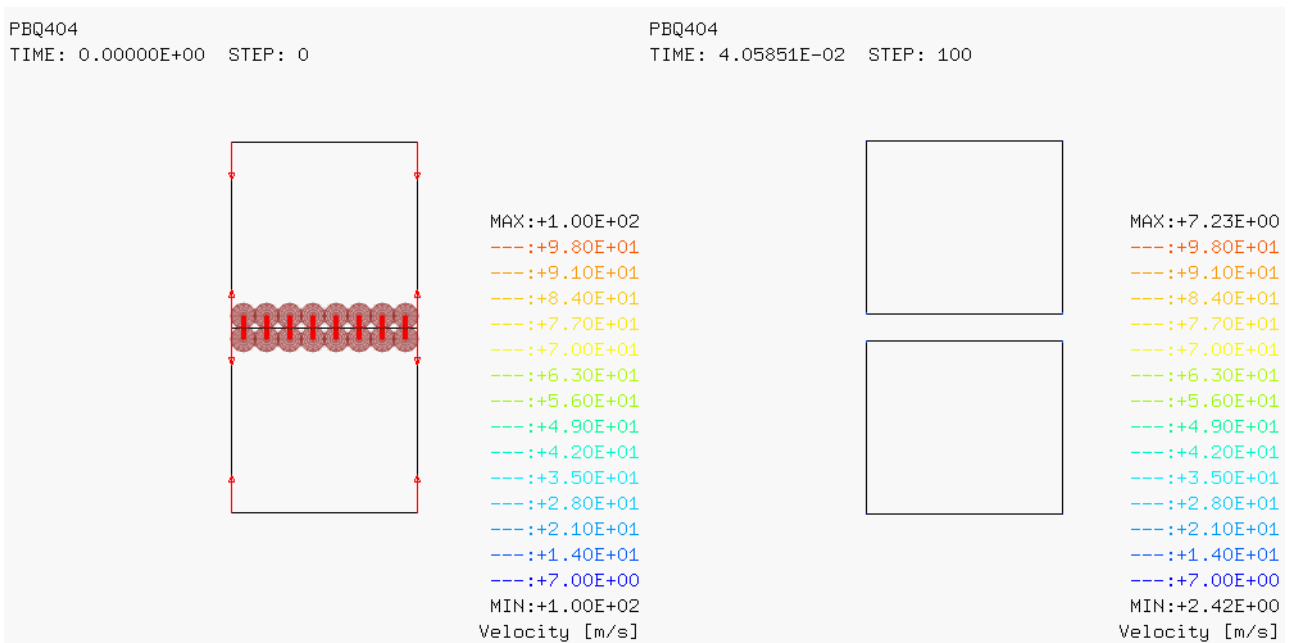
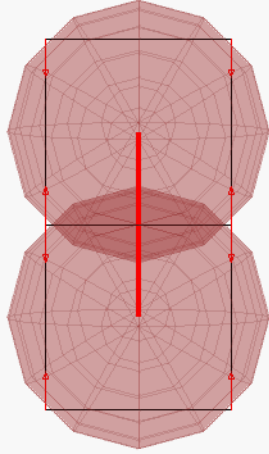


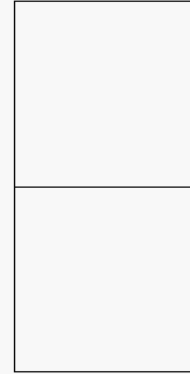
Figure 68 - Initial and final configurations for test PBQ404

PBQ421
 TIME: 0.00000E+00 STEP: 0



MAX:+1.00E+02
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+1.00E+02
 Velocity [m/s]

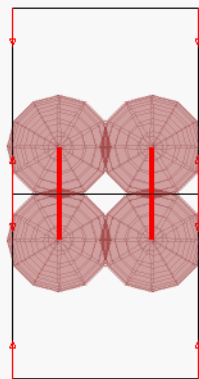
PBQ421
 TIME: 4.31704E-02 STEP: 100



MAX:+1.42E-14
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+1.42E-14
 Velocity [m/s]

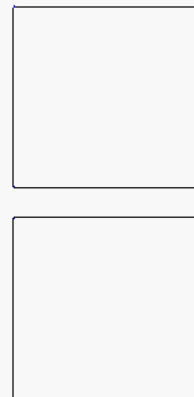
Figure 69 - Initial and final configurations for test PBQ421

PBQ422
 TIME: 0.00000E+00 STEP: 0



MAX:+1.00E+02
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+1.00E+02
 Velocity [m/s]

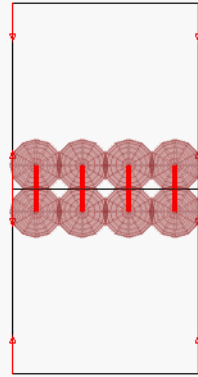
PBQ422
 TIME: 4.19002E-02 STEP: 100



MAX:+6.25E+00
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+4.44E+00
 Velocity [m/s]

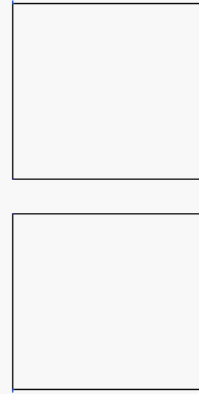
Figure 70 - Initial and final configurations for test PBQ422

PBQ423
TIME: 0.00000E+00 STEP: 0



MAX: +1.00E+02
---: +9.80E+01
---: +9.10E+01
---: +8.40E+01
---: +7.70E+01
---: +7.00E+01
---: +6.30E+01
---: +5.60E+01
---: +4.90E+01
---: +4.20E+01
---: +3.50E+01
---: +2.80E+01
---: +2.10E+01
---: +1.40E+01
---: +7.00E+00
MIN: +1.00E+02
Velocity [m/s]

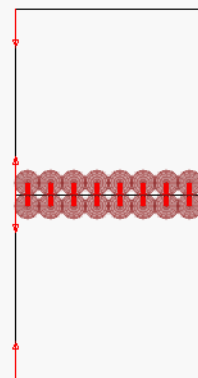
PBQ423
TIME: 4.10010E-02 STEP: 100



MAX: +7.67E+00
---: +9.80E+01
---: +9.10E+01
---: +8.40E+01
---: +7.70E+01
---: +7.00E+01
---: +6.30E+01
---: +5.60E+01
---: +4.90E+01
---: +4.20E+01
---: +3.50E+01
---: +2.80E+01
---: +2.10E+01
---: +1.40E+01
---: +7.00E+00
MIN: +2.32E+00
Velocity [m/s]

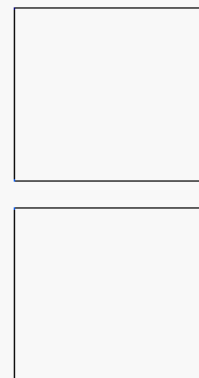
Figure 71 - Initial and final configurations for test PBQ423

PBQ424
TIME: 0.00000E+00 STEP: 0



MAX: +1.00E+02
---: +9.80E+01
---: +9.10E+01
---: +8.40E+01
---: +7.70E+01
---: +7.00E+01
---: +6.30E+01
---: +5.60E+01
---: +4.90E+01
---: +4.20E+01
---: +3.50E+01
---: +2.80E+01
---: +2.10E+01
---: +1.40E+01
---: +7.00E+00
MIN: +1.00E+02
Velocity [m/s]

PBQ424
TIME: 4.05851E-02 STEP: 100



MAX: +7.23E+00
---: +9.80E+01
---: +9.10E+01
---: +8.40E+01
---: +7.70E+01
---: +7.00E+01
---: +6.30E+01
---: +5.60E+01
---: +4.90E+01
---: +4.20E+01
---: +3.50E+01
---: +2.80E+01
---: +2.10E+01
---: +1.40E+01
---: +7.00E+00
MIN: +2.42E+00
Velocity [m/s]

Figure 72 - Initial and final configurations for test PBQ424

3.3.2 2D solutions with parabolic elements

Next, we consider the same test cases but by using the parabolic elements Q92 (with reduced 2×2 integration) and Q93 (with full 3×3 integration). The initial configuration is the one shown in the right part of Figure 63. All performed calculations with the parabolic elements are summarized in Table 5 (square brackets indicate prematurely stopped calculations).

Case	Mesh	Notes	Steps	CPU [s]	Els*step
PBQ901	2 Q92	0-level pinballs	100	0.70	202
PBQ902	2 Q92	MLEV 1 EQVF	100	0.66	202
PBQ903	2 Q92	MLEV 2 EQVF	100	0.67	202
PBQ904	2 Q92	MLEV 3 EQVF	100	0.66	202
PBQ931	2 Q93	0-level pinballs	100	0.59	202
PBQ932	2 Q93	MLEV 1 EQVF	[93]	[0.64]	[188]
PBQ933	2 Q93	MLEV 2 EQVF	100	0.58	202
PBQ934	2 Q93	MLEV 3 EQVF	[44]	[0.36]	[90]

Table 5 - Calculations for the quadrilateral impact problem in 2D with parabolic elements

PBQ901

This test uses 0-level (parent) pinballs. The vertical displacement of node 5 is plotted in Figure 73 for this test case and the following 7 cases (all solutions with parabolic elements). The initial and final configuration for this solution are shown in Figure 74. The solution is subjected to strong mechanisms. Like in the PBQ401 case, the contact points in this case are the centers of the (parent) pinballs, i.e. the centroid of the two quadrilateral elements. However, unlike in the linear case, now a node (the ninth node of each element) is present at that point. Therefore, at step 0 only this node “feels” the contact force, while all other nodes continue undisturbed their motion. This seems to activate an hourglass mode of the parabolic element.

PBQ902

This test is similar to PBQ901 but uses level 1 pinballs (MLEV 1). Additionally, the EQVF option is activated, according to which the volume of the final (contacting) pinballs is equivalent to the volume of the corresponding parent element portion. Some hourglassing appears also in this case. The final configuration is shown in Figure 75.

PBQ903

This test is similar to PBQ902 but uses MLEV 2. A solution is obtained despite the fact that some redundancies in the contact constraints can occur in this case. No hourglassing occurs. The final configuration is plotted in Figure 76, showing some rebound.

PBQ904

This test is similar to PBQ903 but uses MLEV 3. A solution is obtained despite the fact that many redundancies in the contact constraints occur in this case, and is shown in Figure 77. Strangely, strong hourglassing occurs only in one of the elements.

PBQ931

This test is similar to PBQ901 but uses the fully integrated element Q93 instead of the reduced-integrated element Q92. The solution is shown in Figure 78. Like in case PBQ401, no rebound occurs.

PBQ932

This test is similar to PBQ902 but uses the fully integrated element Q93 instead of the reduced-integrated element Q92. The solution is shown in Figure 79. Strong hourglass occurs and the solution stops at step 93.

PBQ933

This test is similar to PBQ903 but uses the fully integrated element Q93 instead of the reduced-integrated element Q92. The solution is shown in Figure 80. No hourglass is developed and some rebound occurs.

PBQ934

This test is similar to PBQ904 but uses the fully integrated element Q93 instead of the reduced-integrated element Q92. The solution is shown in Figure 81 and is characterized by strong hourglassing, so that the solution stops at step 44.

We may conclude that in the case of parabolic elements, solutions of this simple problem seem to be very unstable and are characterized by strong hourglassing, except in the case MLEV 2. Furthermore, the hourglassing is even stronger in the case of fully integrated element (Q93) than in the case of reduced integrated element (Q92), which seems contrary to expectation.

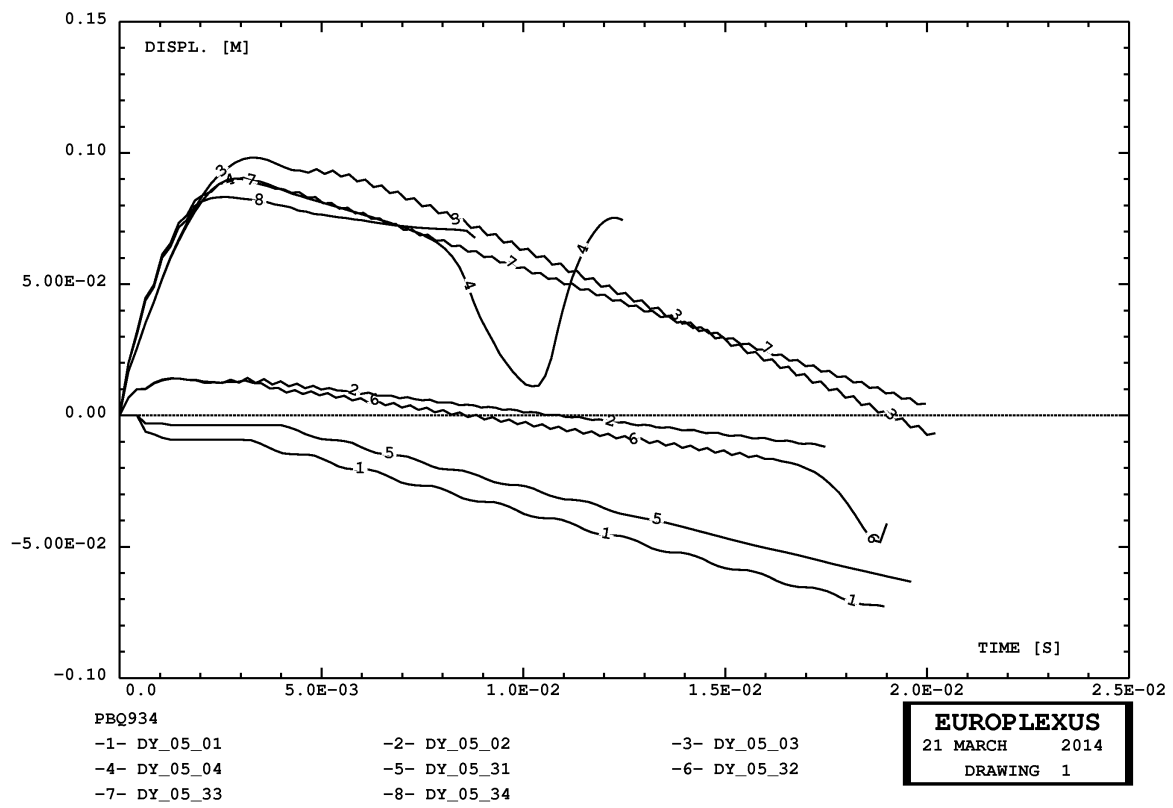


Figure 73 - Vertical displacement of node 1 in the 8 linear element solutions PBQXXX

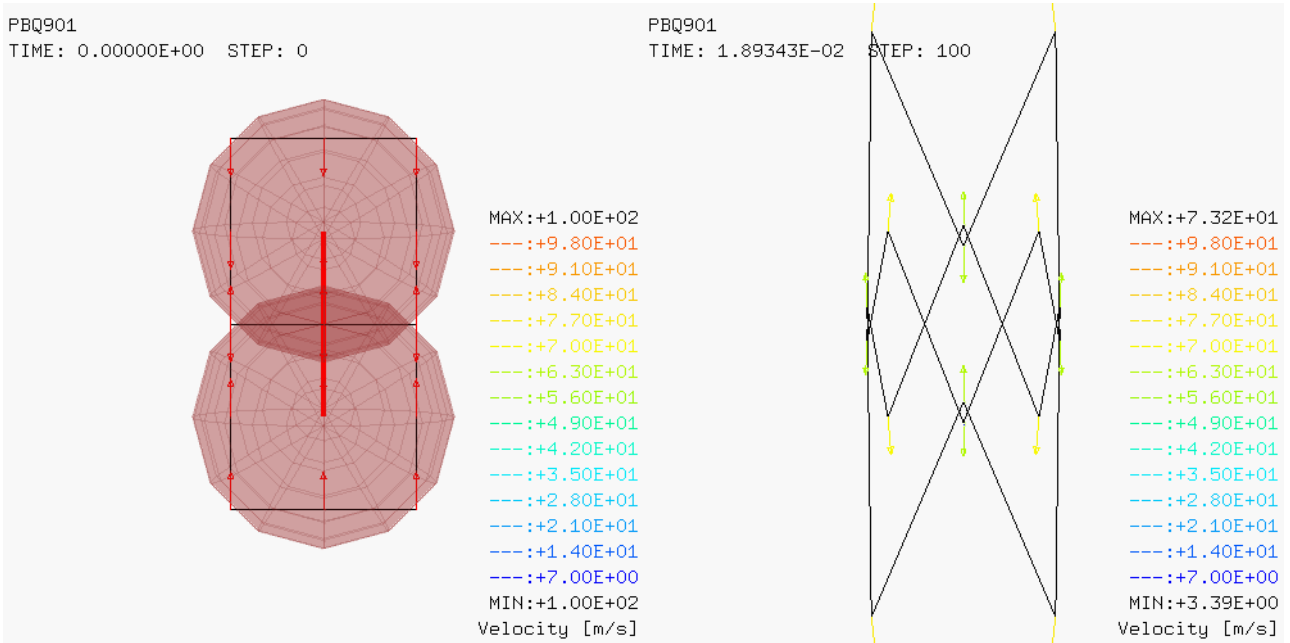


Figure 74 - Initial and final configurations for test PBQ901

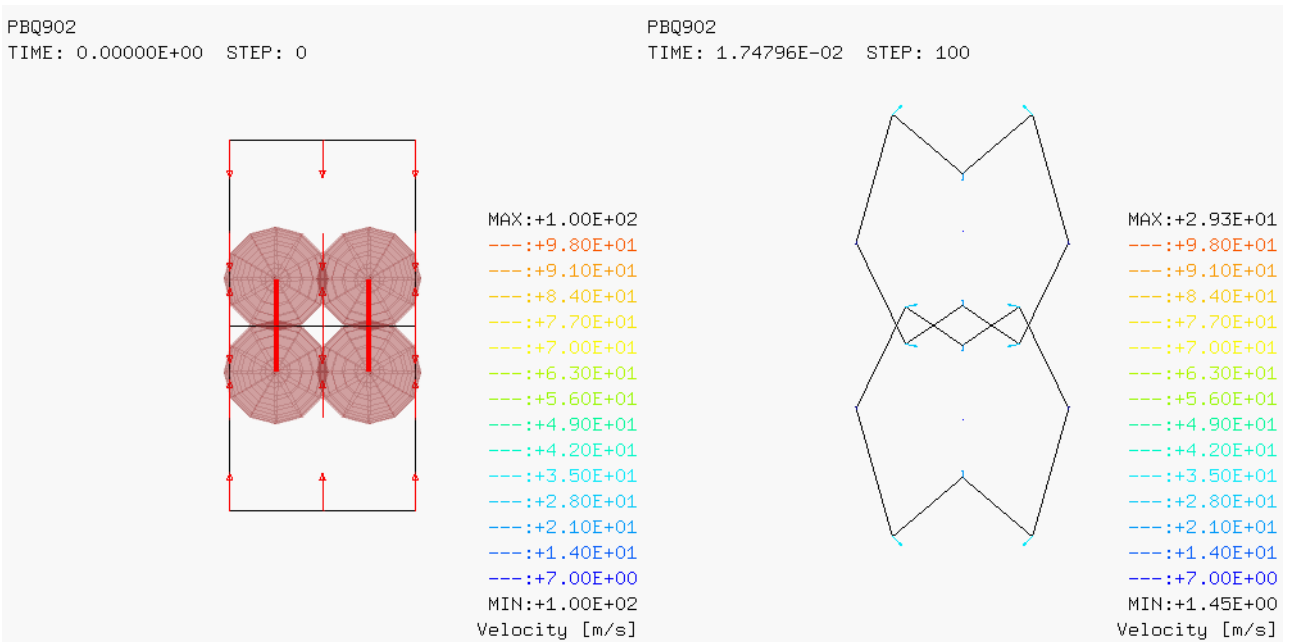


Figure 75 - Initial and final configurations for test PBQ902

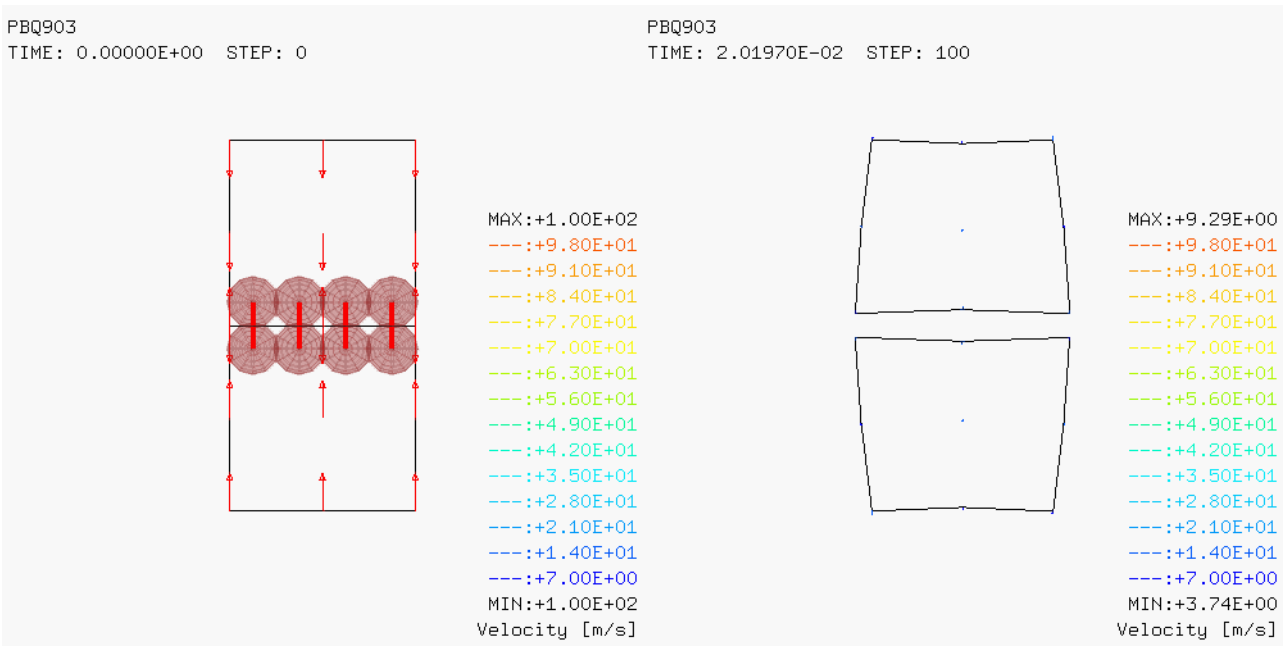


Figure 76 - Initial and final configurations for test PBQ903

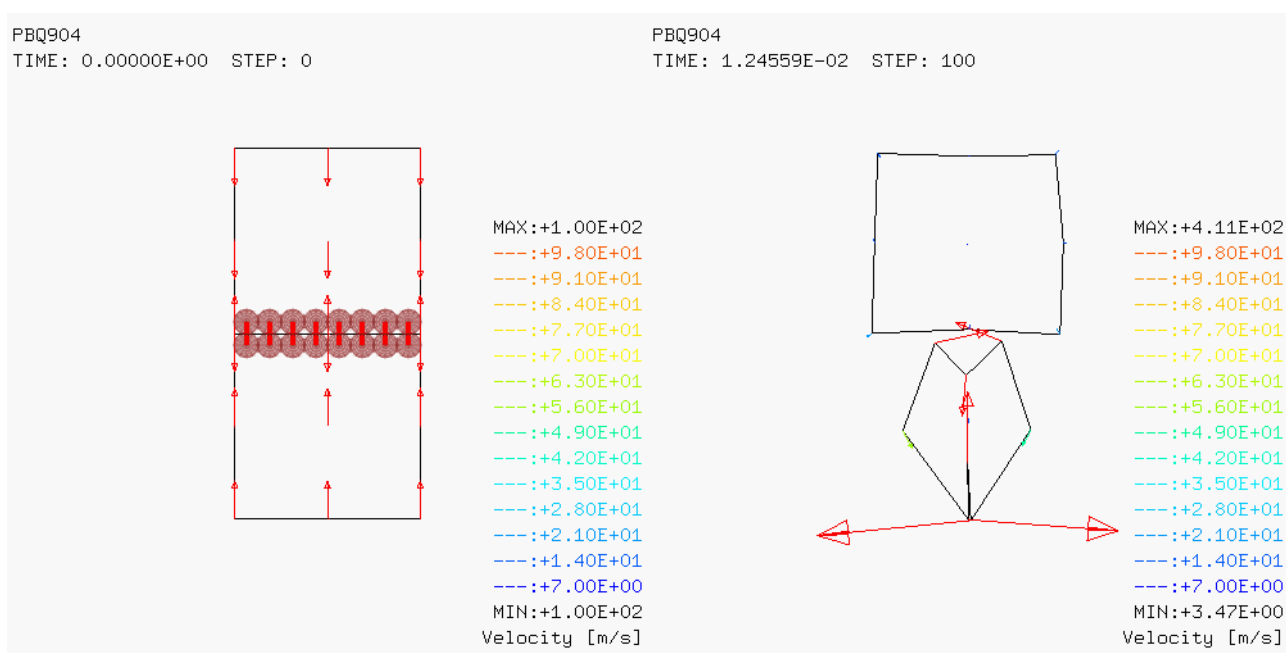


Figure 77 - Initial and final configurations for test PBQ904

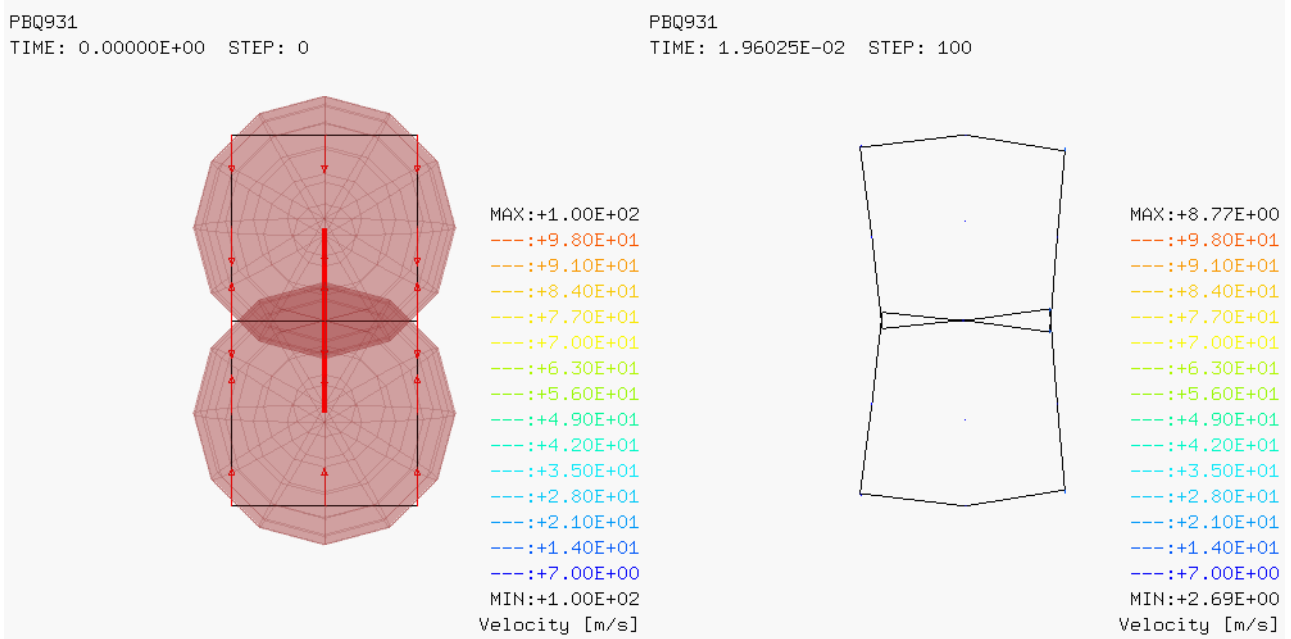


Figure 78 - Initial and final configurations for test PBQ931

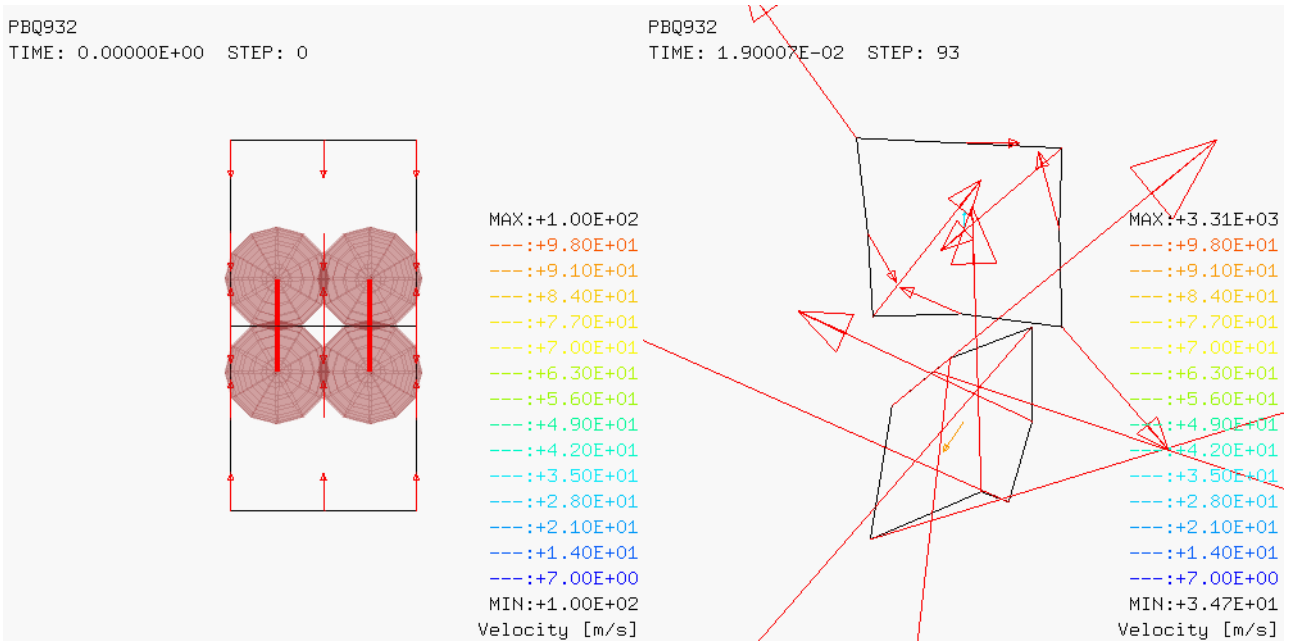


Figure 79 - Initial and final configurations for test PBQ932

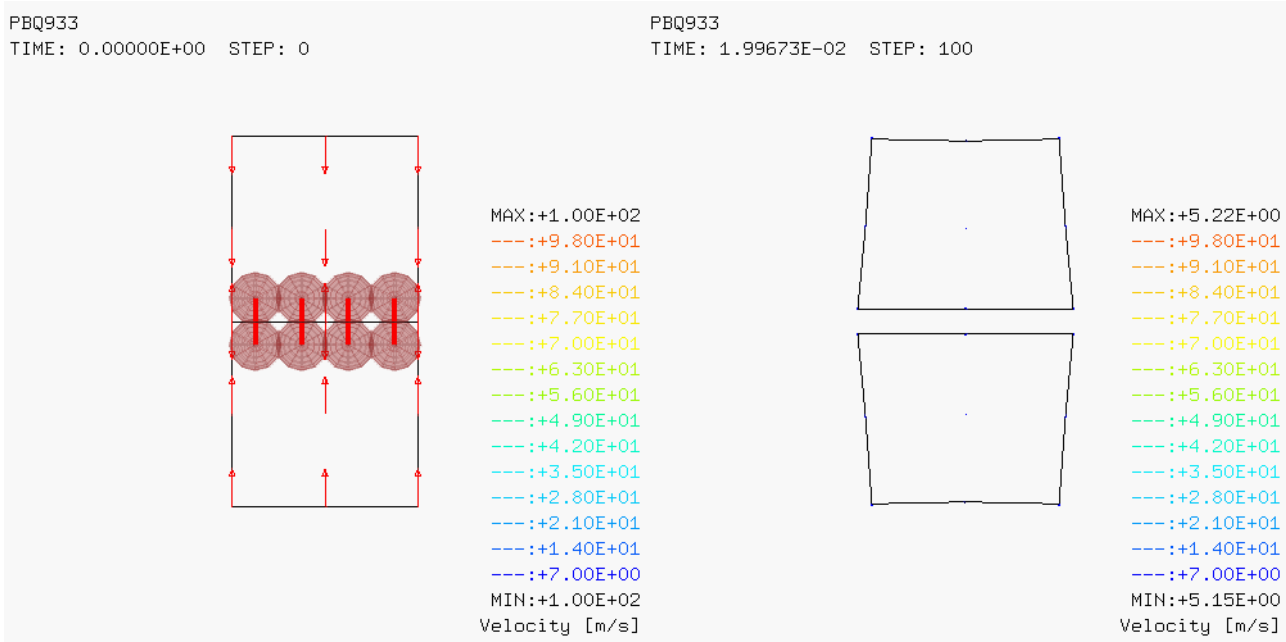


Figure 80 - Initial and final configurations for test PBQ933

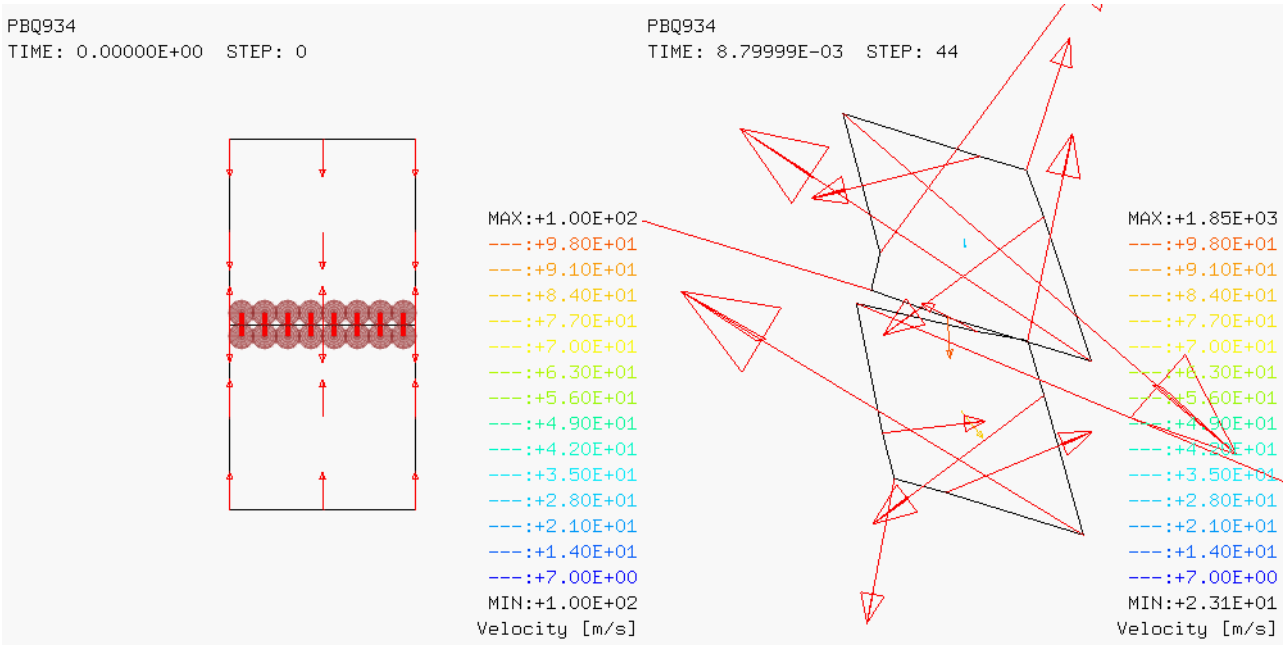


Figure 81 - Initial and final configurations for test PBQ934

3.3.3 3D solutions with linear elements

We consider now the 3D equivalent of the impact problem of Section 3.3 whereby, instead of two quadrilaterals, we have two hexahedra. Each hexahedron measures $2 \times 2 \times 2$ m and has an initial velocity of 100 m/s in the vertical (now z) direction (with opposite signs in the two elements). The initial gap between the two hexahedra is zero. A total of 100 time steps is performed.

First, a reference solution is obtained by means of linear elements (CUBE and CUB8). Then, the same problem is solved with quadratic elements (C272 and C273) using the native pinball formulation for such elements. All performed calculations with linear elements are summarized in Table 6.

Case	Mesh	Notes	Steps	CPU [s]	Els*step
PBCU01	2 CUBE	0-level pinballs	100	0.59	202
PBCU02	2 CUBE	MLEV 1 EQVF	100	0.61	202
PBCU03	2 CUBE	MLEV 2 EQVF	100	0.72	202
PBCU04	2 CUBE	MLEV 3 EQVF	[0]	[0]	[0]
PBC801	2 CUB8	0-level pinballs	100	0.55	202
PBC802	2 CUB8	MLEV 1 EQVF	[9]	[0.12]	[20]
PBC803	2 CUB8	MLEV 2 EQVF	[11]	[0.17]	[24]
PBC804	2 CUB8	MLEV 3 EQVF	[0]	[0]	[0]

Table 6 - Calculations for the hexahedral impact problem in 3D with linear elements

PBCU01

This test uses 0-level (parent) pinballs. The vertical displacement of node 1 is plotted in Figure 82 for this test case and the following 5 cases (all obtained solutions with linear elements). The initial and final configuration for this solution are shown in Figure 83. The solution is degenerated, in the sense that all nodes are instantaneously stopped at step 0, due to the fact that only one element is used on each side of the impact, and the contact points are at the centres of the parent pinballs, which coincide with the element centroids. Therefore, the contact force is equally distributed on all nodes and the effect is that the velocity becomes instantly zero at the initial step. No rebound occurs.

PBCU02

This test is similar to PBCU01 but uses level 1 pinballs (MLEV 1). Additionally, the EQVF option is activated, according to which the volume of the final (contacting) pinballs is equivalent to the volume of the corresponding parent element portion. The solution is shown in Figure 84. In this case some rebound occurs.

PBCU03

This test is similar to PBCU02 but uses MLEV 2. A solution is obtained despite the fact that some redundancies in the contact constraints can occur in this case, and is shown in Figure 85. In this case some rebound occurs.

PBCU04

This test is similar to PBCU03 but uses MLEV 3. No solution is obtained because there are too many redundant constraints and the system of constraints cannot be solved.

PBC801

This test is similar to PBCU01 but uses the fully integrated element CUB8 instead of the reduced-integrated element CUBE. The solution is shown in Figure 86. Like in case PBQ401, no rebound occurs.

PBC802

This test is similar to PBCU02 but uses the fully integrated element CUB8 instead of the reduced-integrated element CUBE. The solution stops at step 9 because of large instabilities. The last obtained configuration is shown in Figure 87.

PBC803

This test is similar to PBCU03 but uses the fully integrated element CUB8 instead of the reduced-integrated element CUBE. The solution stops at step 11 because of large instabilities. The last obtained configuration is shown in Figure 88.

PBC804

This test is similar to PBCU04 but uses the fully integrated element CUB8 instead of the reduced-integrated element CUBE. No solution is obtained because there are too many redundant constraints and the system of constraints cannot be solved.

We may conclude that in the case of linear elements, the 3D solutions as far as contact is concerned are similar to the 2D case, with the reduced integrated element. However, with the fully integrated element strong instabilities occur and no solution can be obtained.

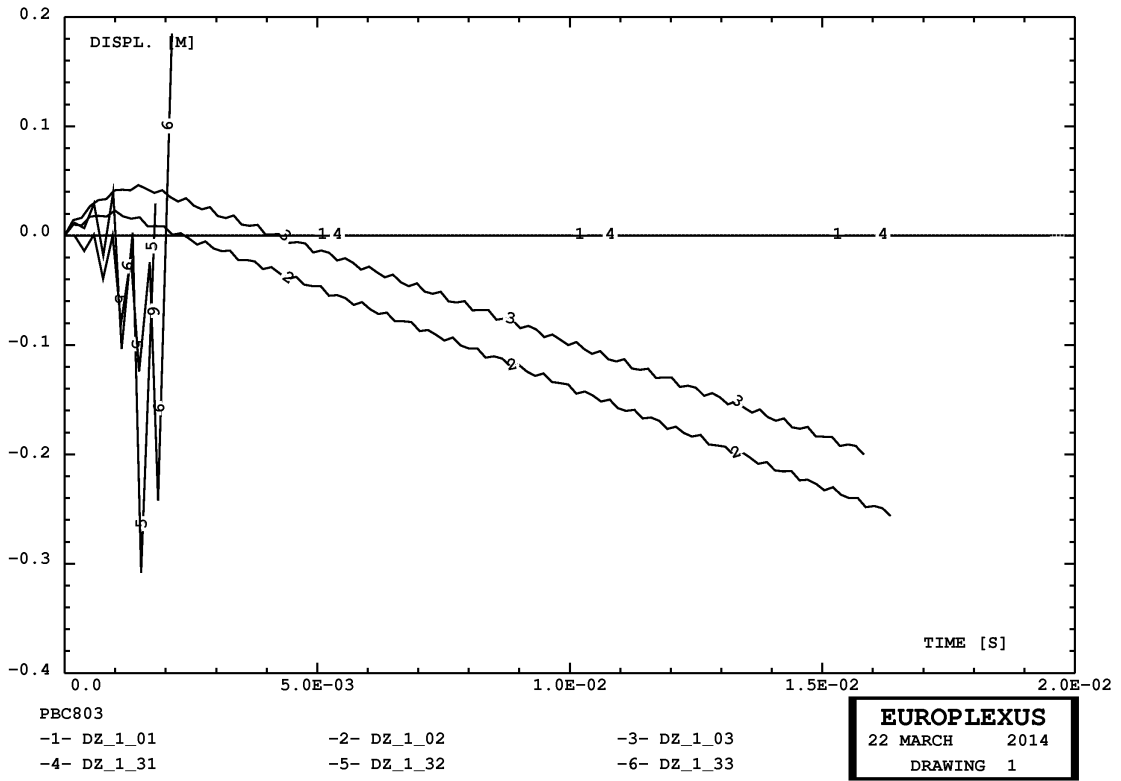


Figure 82 - Vertical displacement of node 1 in the 6 linear element solutions PBCXXX

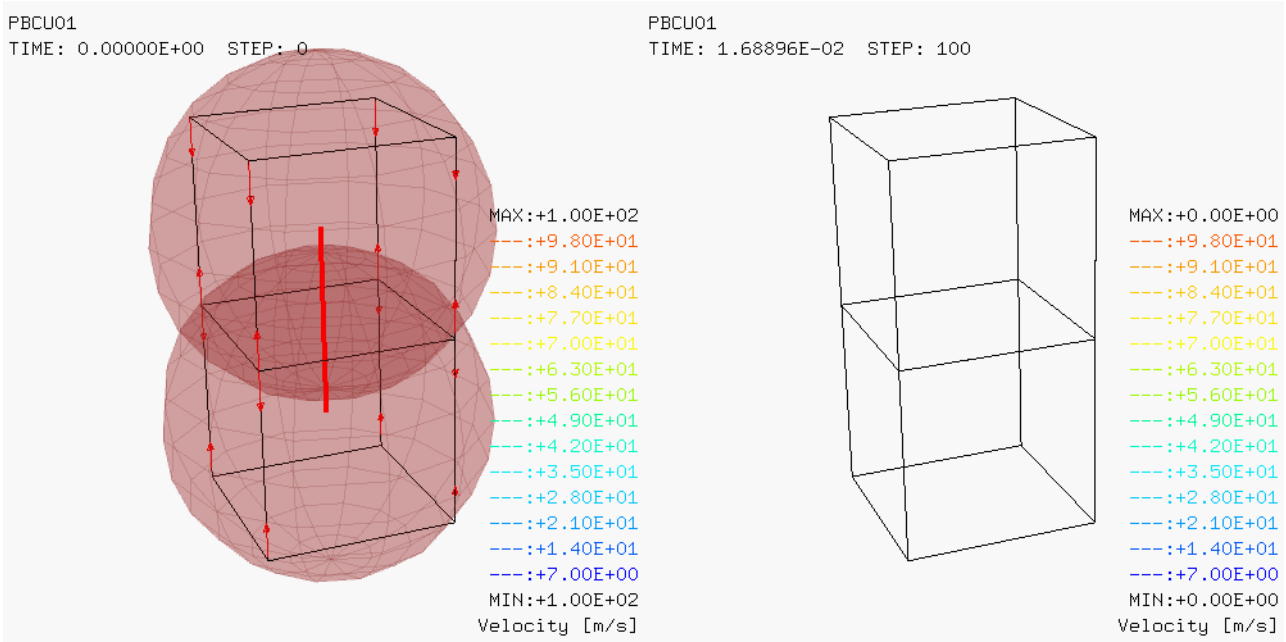


Figure 83 - Initial and final configurations for test PBCU01

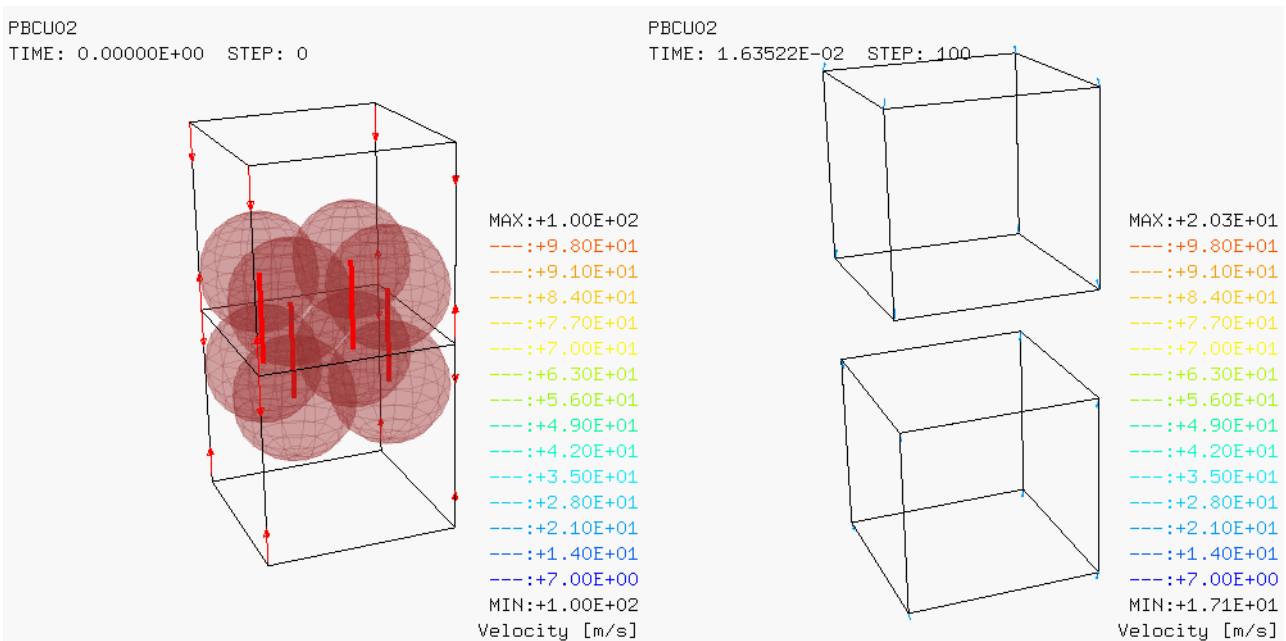
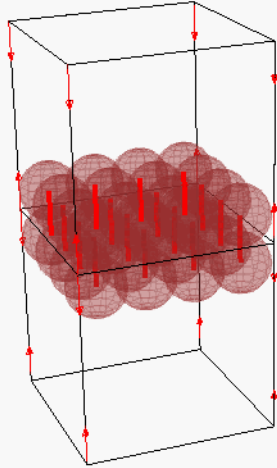


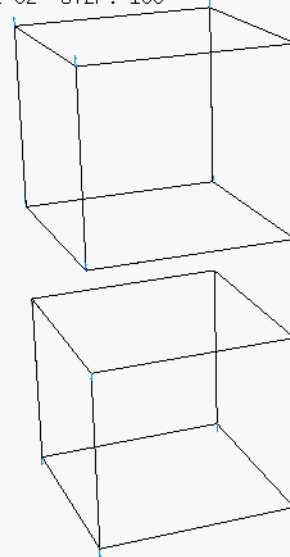
Figure 84 - Initial and final configurations for test PBCU02

PBCU03
 TIME: 0.00000E+00 STEP: 0



MAX:+1.00E+02
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+1.00E+02
 Velocity [m/s]

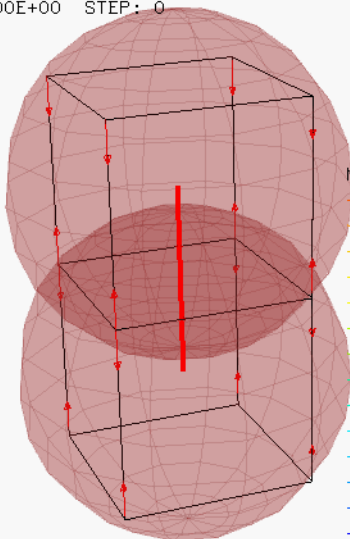
PBCU03
 TIME: 1.58209E-02 STEP: 100



MAX:+1.94E+01
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+1.42E+01
 Velocity [m/s]

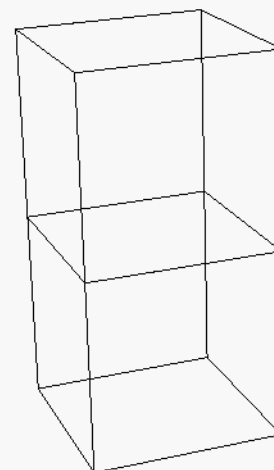
Figure 85 - Initial and final configurations for test PBCU03

PBC801
 TIME: 0.00000E+00 STEP: 0



MAX:+1.00E+02
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+1.00E+02
 Velocity [m/s]

PBC801
 TIME: 1.95024E-02 STEP: 100



MAX:+0.00E+00
 ---:+9.80E+01
 ---:+9.10E+01
 ---:+8.40E+01
 ---:+7.70E+01
 ---:+7.00E+01
 ---:+6.30E+01
 ---:+5.60E+01
 ---:+4.90E+01
 ---:+4.20E+01
 ---:+3.50E+01
 ---:+2.80E+01
 ---:+2.10E+01
 ---:+1.40E+01
 ---:+7.00E+00
 MIN:+0.00E+00
 Velocity [m/s]

Figure 86 - Initial and final configurations for test PBC801

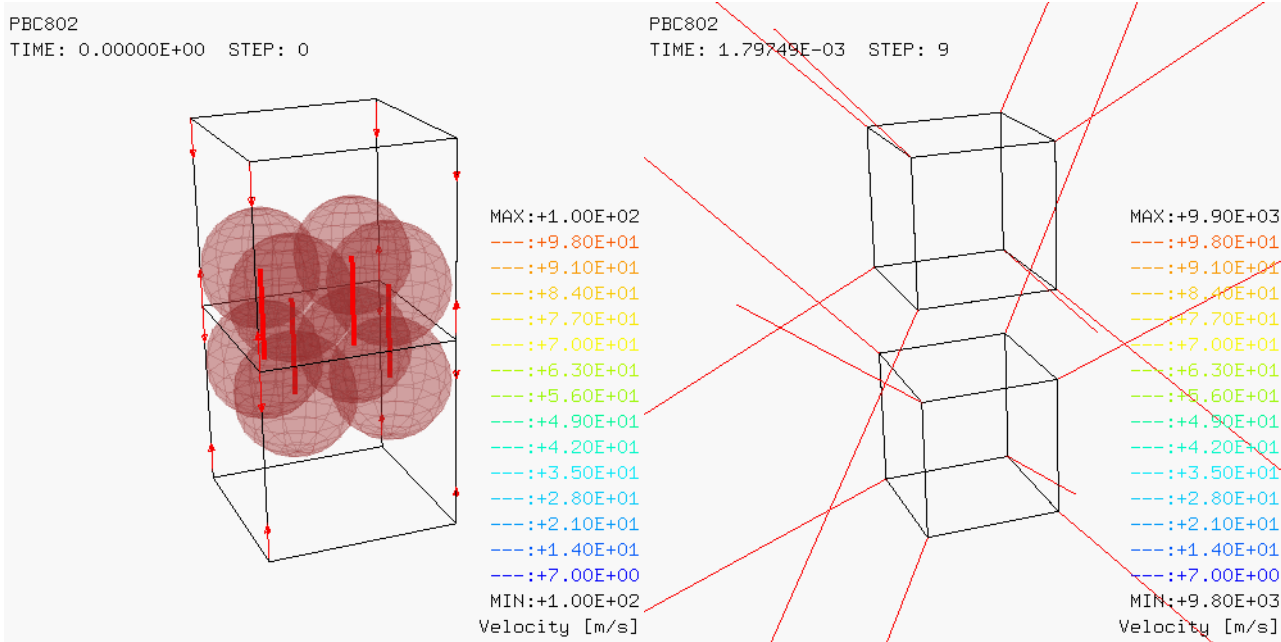


Figure 87 - Initial and final configurations for test PBC802

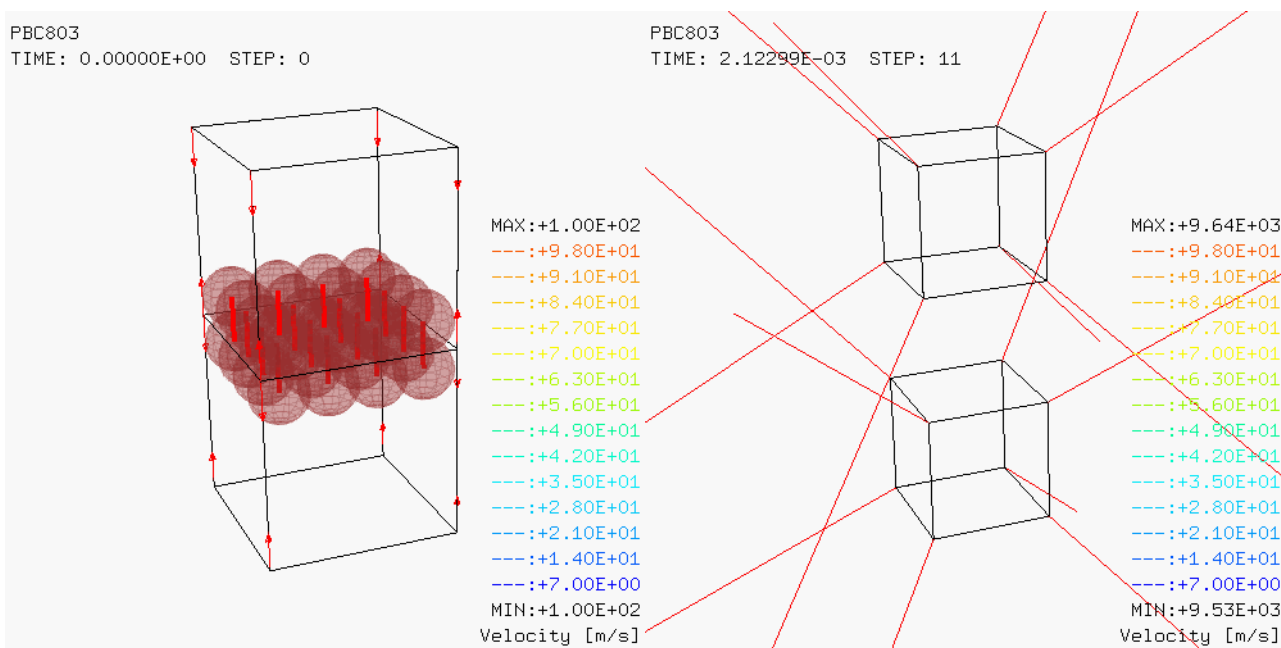


Figure 88 - Initial and final configurations for test PBC803

3.3.4 3D solutions with parabolic elements

Next, we consider the same test cases but by using the parabolic elements C272 (with reduced $2 \times 2 \times 2$ integration) and C273 (with full $3 \times 3 \times 3$ integration). All performed calculations with the parabolic elements are summarized in Table 7 (square brackets indicate prematurely stopped calculations).

Case	Mesh	Notes	Steps	CPU [s]	Els*step
PBC201	2 C272	0-level pinballs	100	1.00	202
PBC202	2 C272	MLEV 1 EQVF	[15]	[0.31]	[32]
PBC203	2 C272	MLEV 2 EQVF	[19]	[0.36]	[40]
PBC204	2 C272	MLEV 3 EQVF	[0]	[0]	[0]
PBC231	2 C273	0-level pinballs	[17]	[0.23]	[36]
PBC232	2 C273	MLEV 1 EQVF	[16]	[0.36]	[34]
PBC233	2 C273	MLEV 2 EQVF	[20]	[0.86]	[42]
PBC234	2 C273	MLEV 3 EQVF	[0]	[0]	[0]

Table 7 - Calculations for the hexahedral impact problem in 3D with parabolic elements

PBC201

This test uses 0-level (parent) pinballs. The vertical displacement of node 27 is plotted in Figure 89 for this test case and the following 5 cases (all solutions with parabolic elements). The initial and final configuration for this solution are shown in Figure 90. The solution arrives at step 100 but is subjected to strong mechanisms.

PBC202

This test is similar to PBC201 but uses level 1 pinballs (MLEV 1). Additionally, the EQVF option is activated, according to which the volume of the final (contacting) pinballs is equivalent to the volume of the corresponding parent element portion. Strong hourglassing appears in this case and the solution stops at step 15. The final configuration is shown in Figure 91.

PBC203

This test is similar to PBC202 but uses MLEV 2. Strong hourglassing appears in this case and the solution stops at step 19. The final configuration is shown in Figure 92.

PBC204

This test is similar to PBC203 but uses MLEV 3. No solution can be obtained because there are too many redundant constraints.

PBC231

This test is similar to PBC201 but uses the fully integrated element C273 instead of the reduced-integrated element C272. Strong hourglassing appears in this case and the solution stops at step 17. The solution is shown in Figure 93.

PBC232

This test is similar to PBC202 but uses the fully integrated element C273 instead of the reduced-integrated element C272. The solution is shown in Figure 94. Strong hourglass occurs and the solution stops at step 16.

PBC233

This test is similar to PBC203 but uses the fully integrated element C273 instead of the reduced-integrated element C272. The solution is shown in Figure 95. Strong hourglass occurs and the solution stops at step 20.

PBC234

This test is similar to PBC204 but uses the fully integrated element Q93 instead of the reduced-integrated element Q92. No solution can be obtained because there are too many redundant constraints.

We may conclude that in the case of 3D parabolic elements, solutions of this simple problem seem to be very unstable and are characterized by strong hourglassing. No valid solution can be obtained.

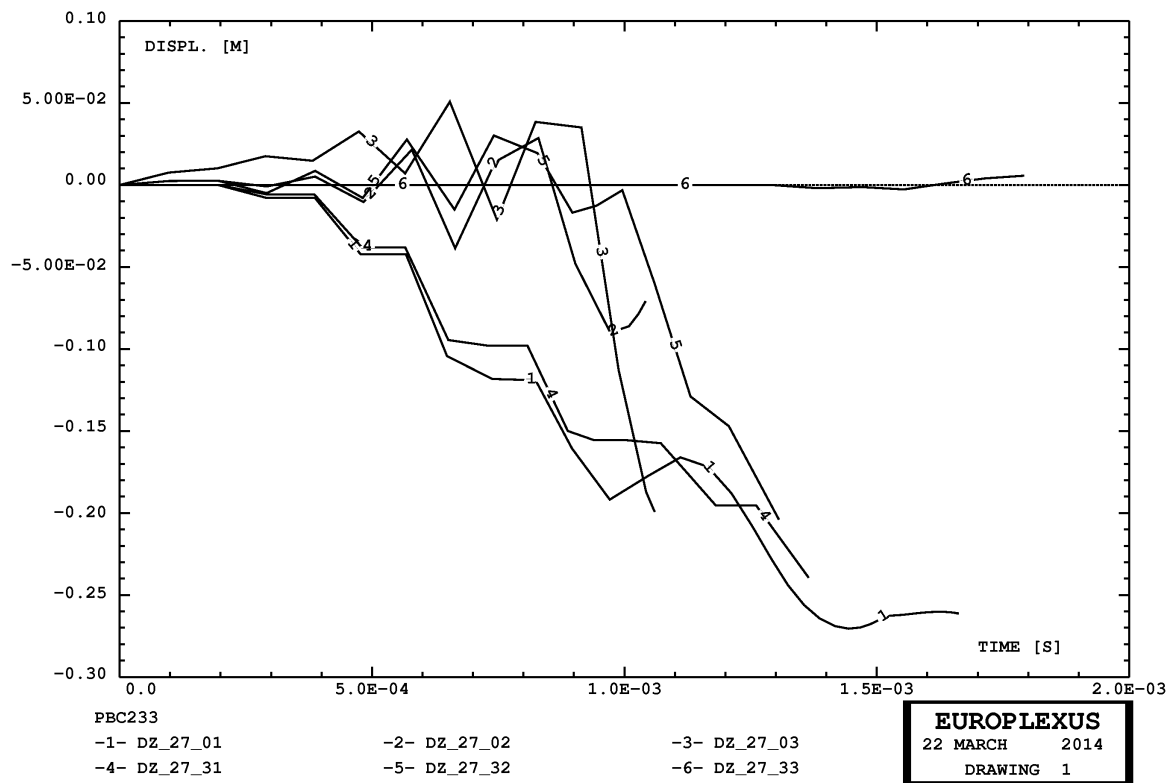


Figure 89 - Vertical displacement of node 27 in the 6 parabolic element solutions PBCXXX

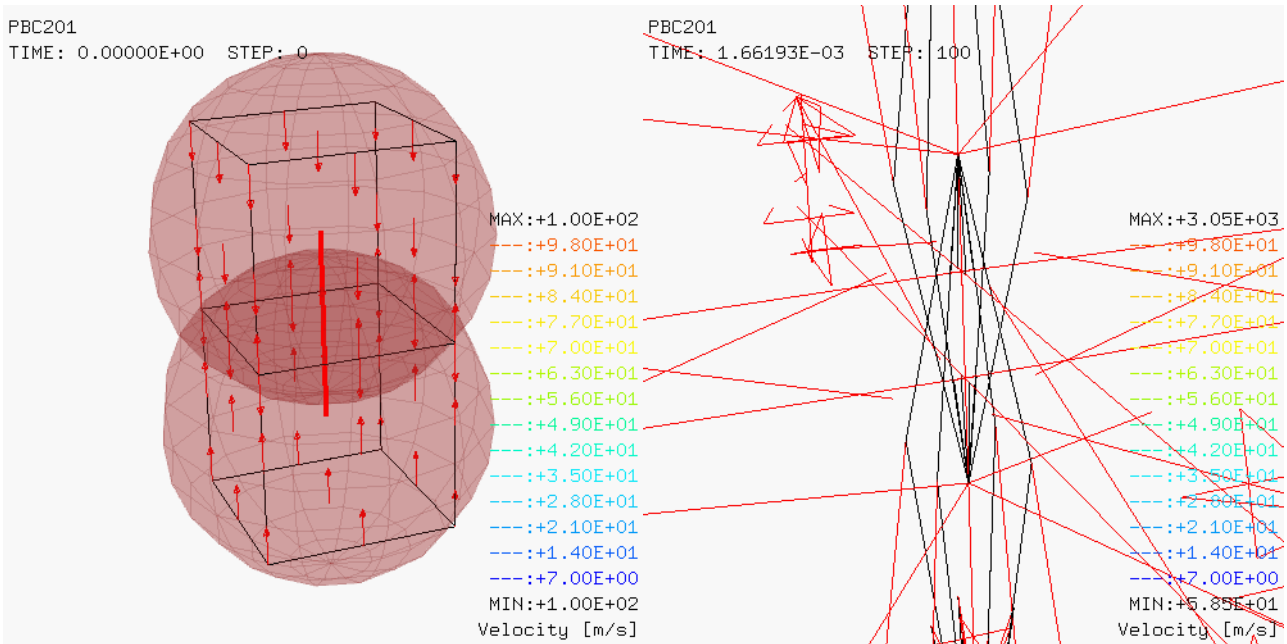


Figure 90 - Initial and final configurations for test PBC201

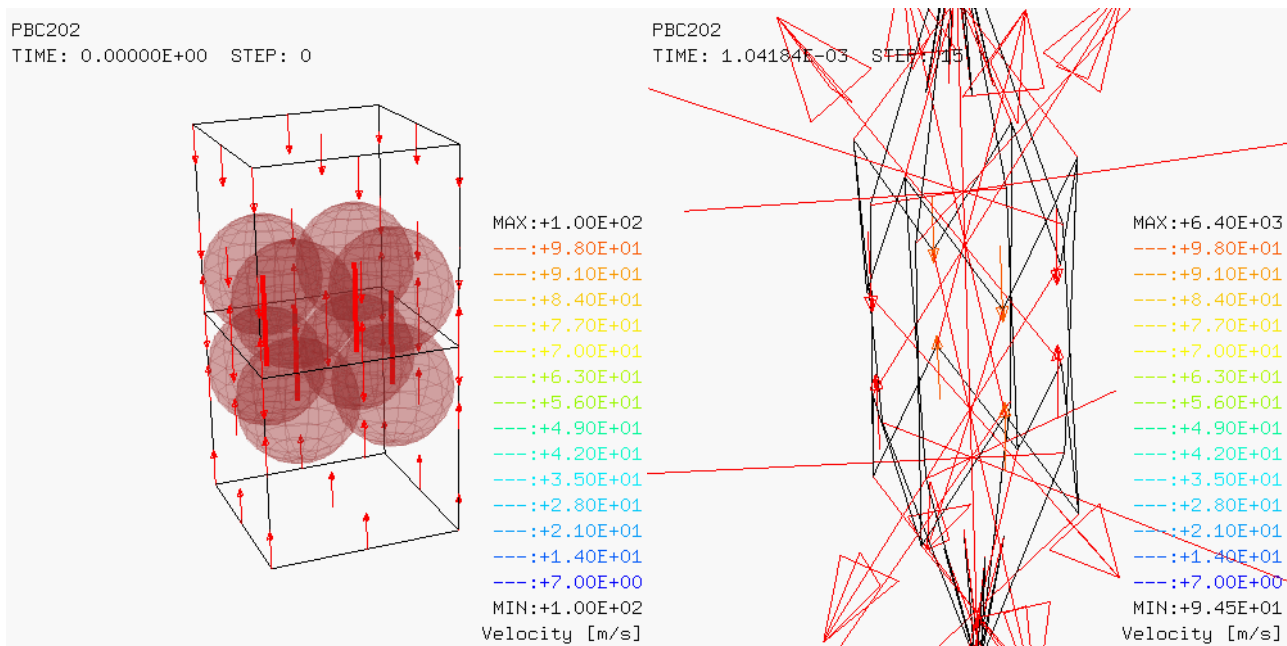


Figure 91 - Initial and final configurations for test PBC202

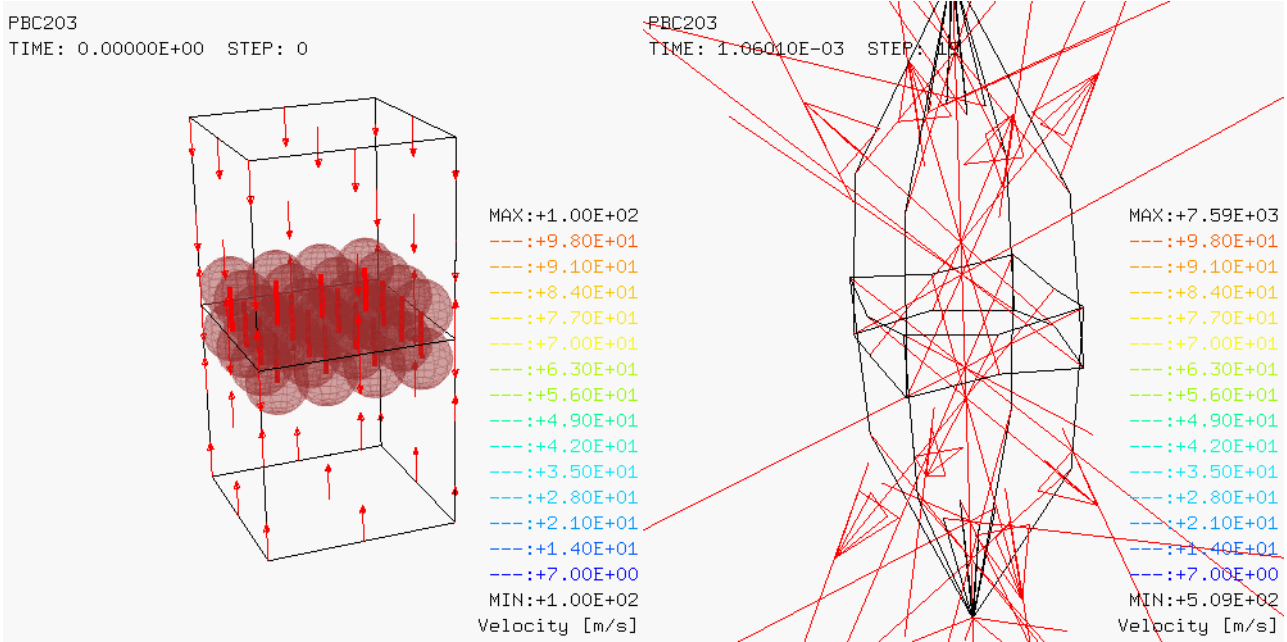


Figure 92 - Initial and final configurations for test PBC203

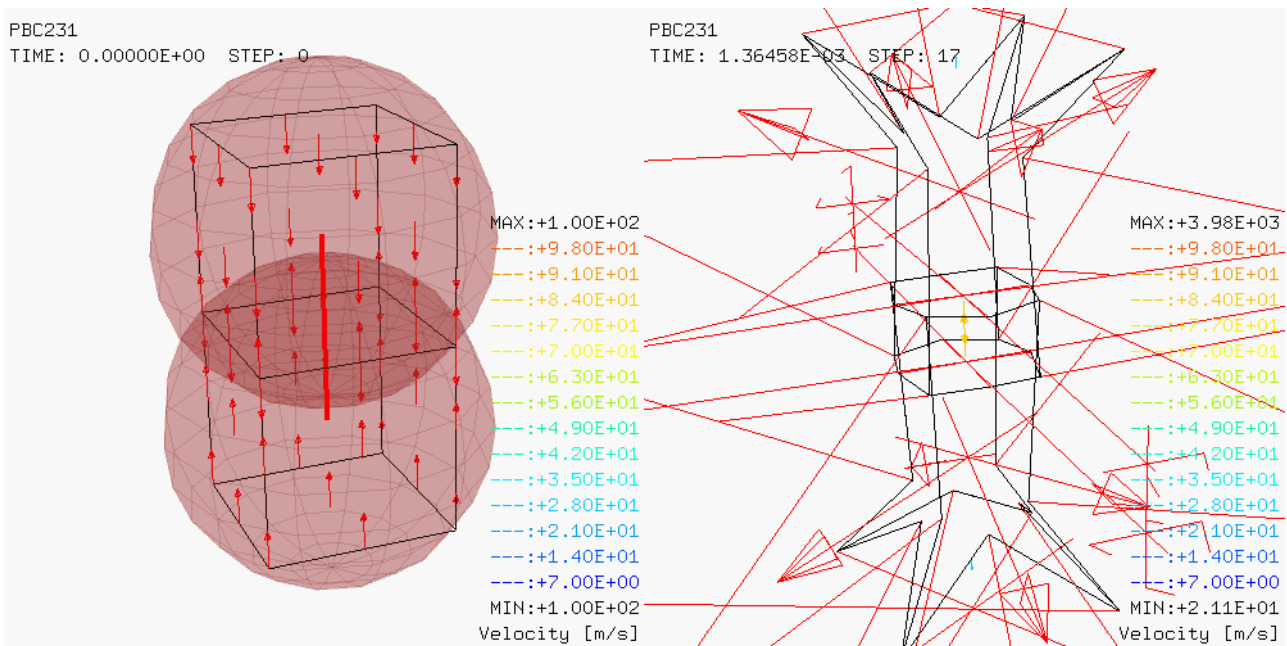


Figure 93 - Initial and final configurations for test PBC231

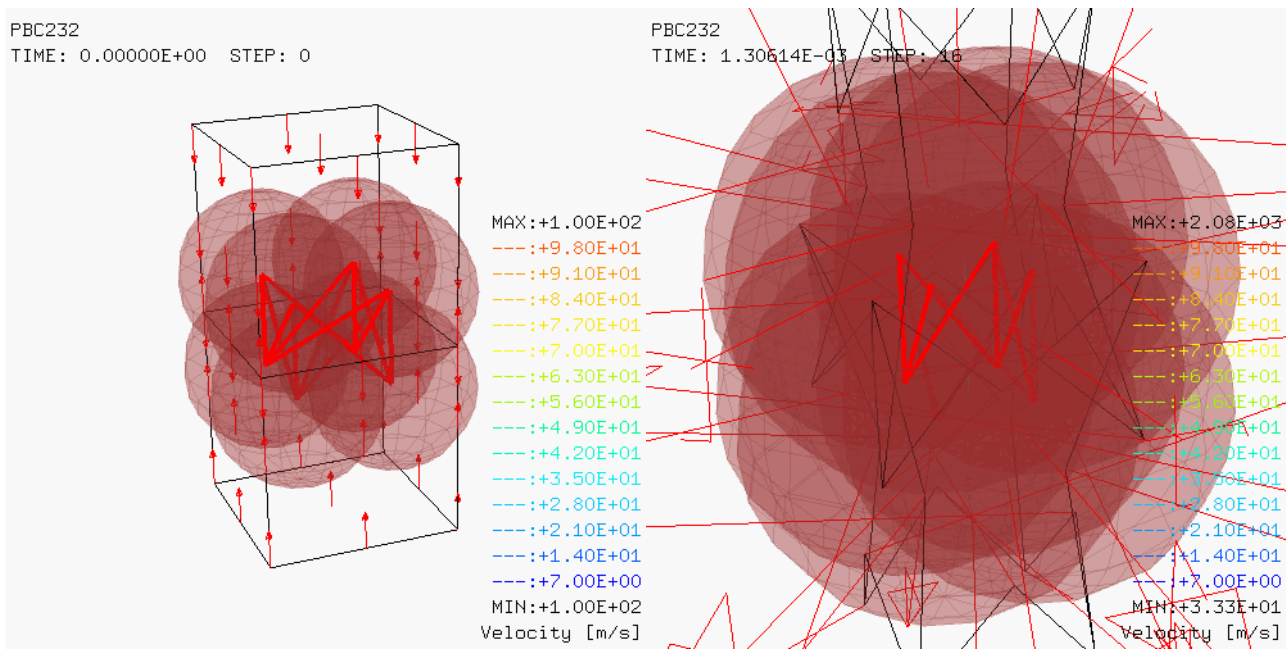


Figure 94 - Initial and final configurations for test PBC232

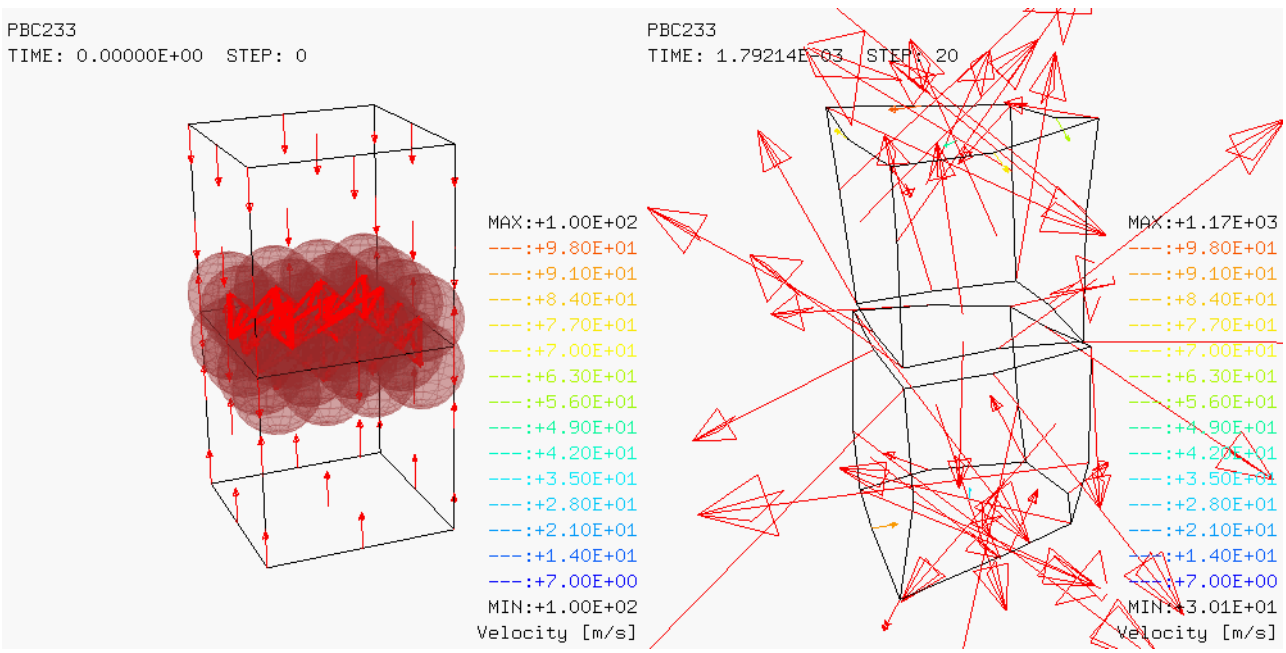


Figure 95 - Initial and final configurations for test PBC233

4. Contact problem with native parabolic pinballs

We return now to the structure crushing problem of Section 2 and attempt to solve it with the new “native” pinball formulations for parabolic elements, i.e. by using the Q93 fully-integrated 9-node quadrilateral. All performed calculations are summarized in Table 8.

Table 8 - Calculations of the structure crash problem by Q93 and native pinballs

Case	Mesh	Notes	Steps	CPU [s]	Els*step
Q93_03	4080 Q93	1 PINB SELF DMIN 0.1 EQVF	2,149,425	38,116	8.77×10^9
Q92_03	4080 Q92	1 PINB SELF DMIN 0.1 EQVF	[164,536]	[1,755]	$[6.71 \times 10^8]$
Q9M_03 ^a	3264 Q92 816 Q93	1 PINB SELF DMIN 0.1 EQVF	8,827,232	231,252	3.60×10^{10}
Q9M_04 ^a	3264 Q92 816 Q93	1 PINB SELF DMIN 0.1 EQVF OPTI PART PLIN	[126,574] t = 2.26 s	[8,988]	$[1.98 \times 10^9]$
Q9M_05 ^a	3264 Q92 816 Q93	1 PINB SELF DMIN 0.1 EQVF OPTI PART PLIN CSTA 0.5	[535,675] t = 5.99 s	[43,815]	$[8.09 \times 10^9]$
Q95_03	4080 Q95	1 PINB SELF DMIN 0.1 EQVF	[511,060]	[10,008]	$[2.08 \times 10^9]$

a. These calculations were performed at JRC on \sm02.

Q93_03

This calculation uses standard native pinballs in the Q93 elements. The mesh has been obtained by Cast3m from that of case QUA401 by transforming each QUA4 into a QUA9 via the pxq42q92 Gibiane procedure already described in Section 2.3.

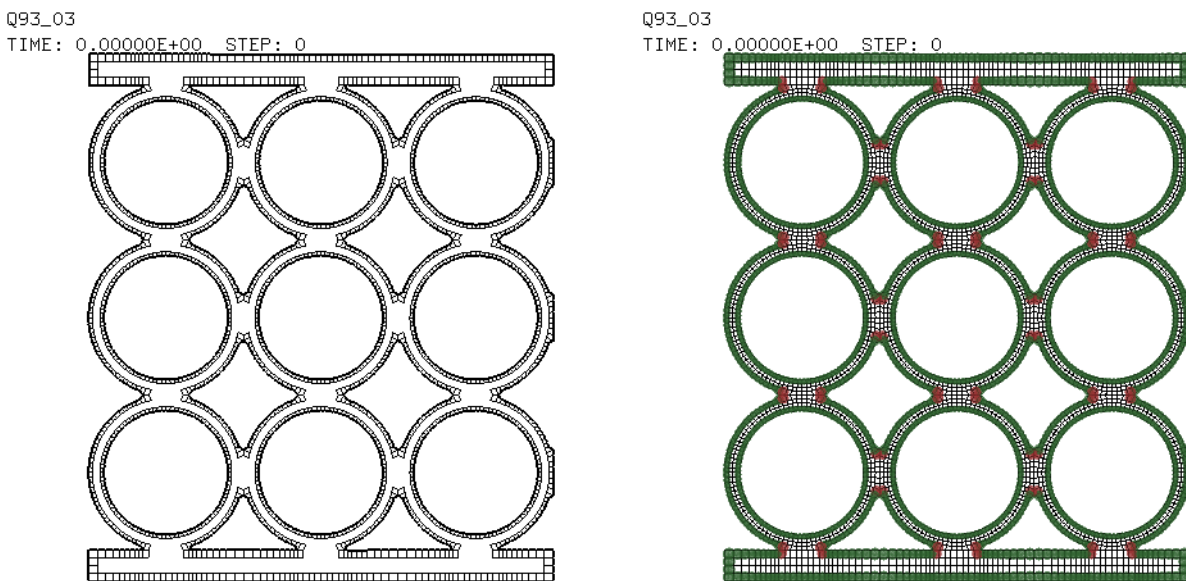


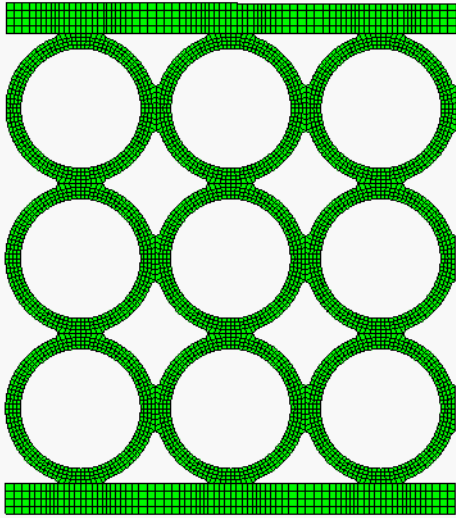
Figure 96 - Pinballs zone in case Q93_03

For simplicity (of the user, but not of the code) there is just one zone with embedded pinballs, which encompasses the whole external surface of the model, see Figure 96. The zone is declared as a self-contacting body (PINB SELF). Hierarchic pinballs are activated by specifying a minimum pinball diameter of 0.1 mm (DMIN 0.1). A fast search of pinball contacts is activated for efficiency of the computation by the option OPTI PINS GRID.

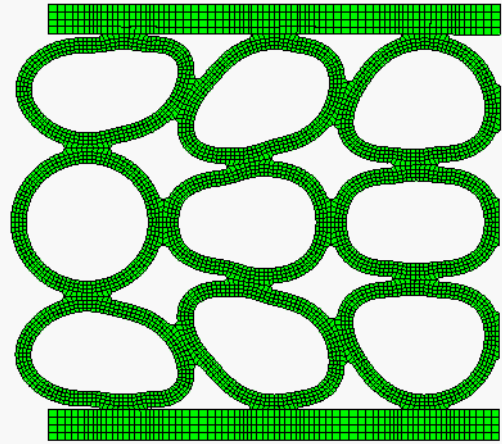
The progressive crushing of the structure (every 2.5 s) is illustrated in Figure 97. Figure 98 shows the final plastic strain. The first contacts appear at about 3.65 s. There remains, like in case Q93_02, a strange occurrence of large (non-physical) plastic strains localized in a couple of elements (see red circles in Figure 98. This spurious plasticization appears very early in the transient, starting from 0.1 s of physical time. It might be due to a meshing problem, or to a locally too distorted shape of the element in the initial configuration. The problem is under investigation.

Figure 99 shows the final contacts in the structure. All the contacts seem physical in this solution.

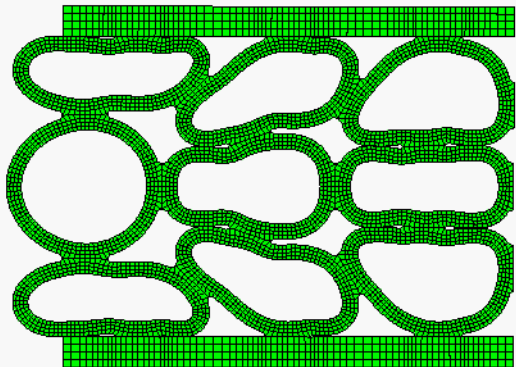
Q93_03
TIME: 0.00000E+00 STEP: 0



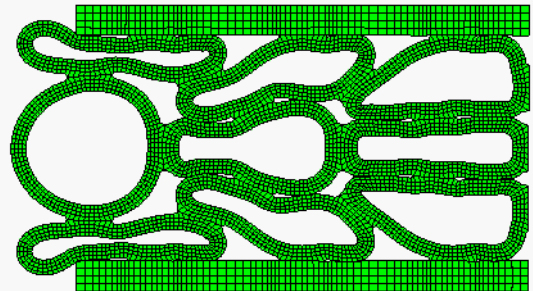
Q93_03
TIME: 2.50000E+00 STEP: 342929



Q93_03
TIME: 5.00000E+00 STEP: 795691



Q93_03
TIME: 7.50000E+00 STEP: ****



Q93_03
TIME: 1.00000E+01 STEP: ****

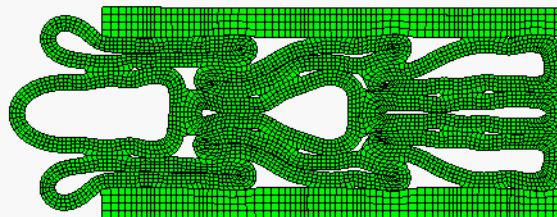
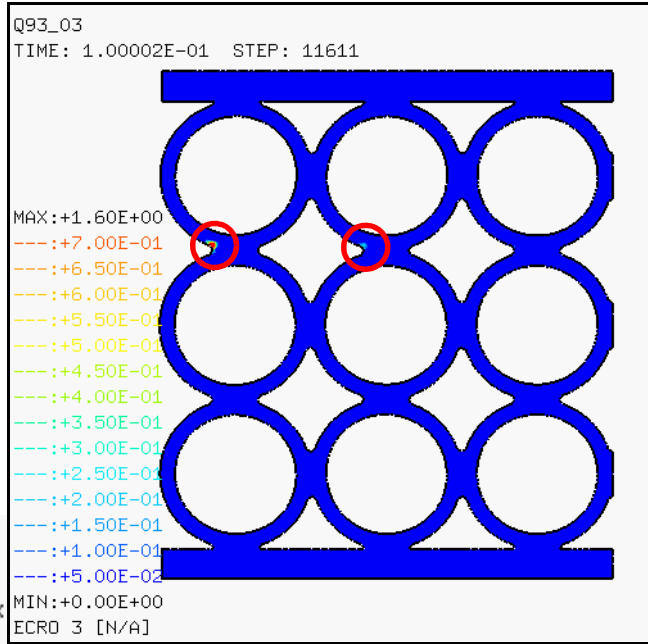


Figure 97 - Structure crushing in case Q93_03

spurious plasticization
from t = 0.1 s



Q93_03
TIME: 1.00000E+01 STEP: *

MAX:+1.50E+03
---:+7.00E-01
---:+6.50E-01
---:+6.00E-01
---:+5.50E-01
---:+5.00E-01
---:+4.50E-01
---:+4.00E-01
---:+3.50E-01
---:+3.00E-01
---:+2.50E-01
---:+2.00E-01
---:+1.50E-01
---:+1.00E-01
---:+5.00E-02
MIN:+0.00E+00
ECRO 3 [N/A]

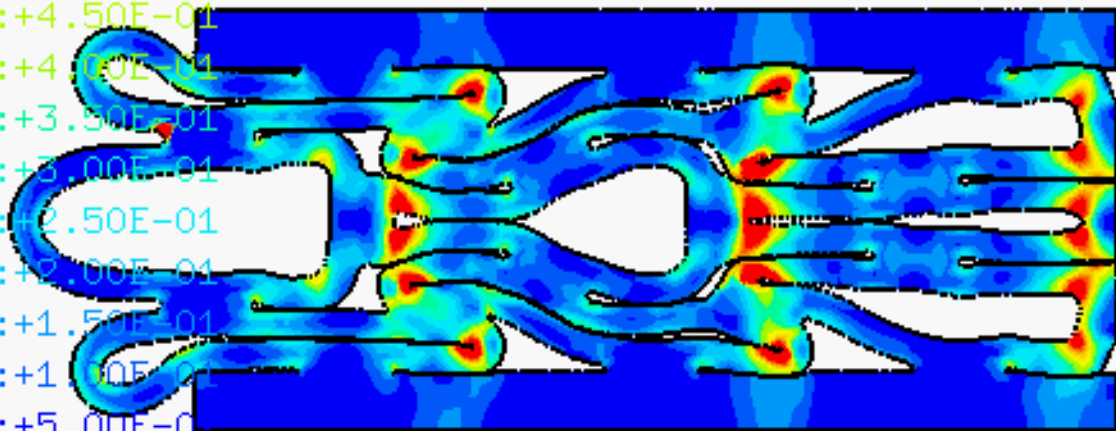
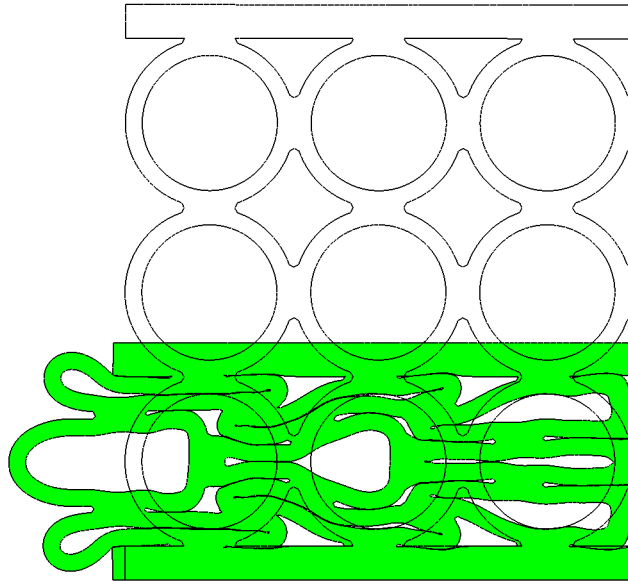


Figure 98 - Final plastic strain in case Q93_03

Q93_03
TIME: 1.00000E+01 STEP: *****



Q93_03
TIME: 1.00000E+01 STEP: *****

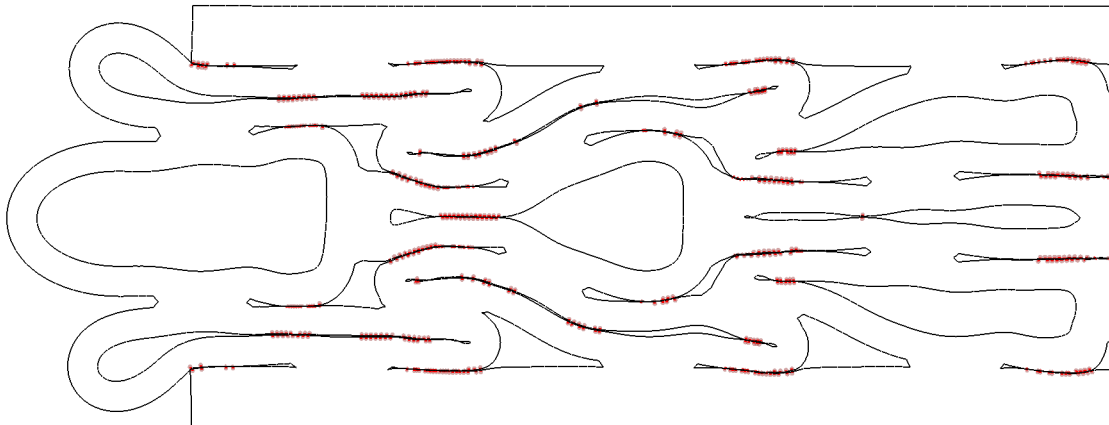


Figure 99 - Final contacts in case Q93_03

Figure 100 shows the resulting crushing force vs. displacement of the top plate. The force is obtained by adding all vertical nodal forces in the nodes on the upper part of the top plate.

Finally, Figure 101 compares the crushing force obtained in the three solutions:

- CAR401, with the CAR4 linear element, red curve, is too stiff
- Q93_02, with Q93 parabolic element and superposed ghost Q41L elements for the contact, green curve, is more ductile (in better accordance with the experiments), but presents some strong oscillations at about 9 s when the crushing is almost complete.

- Q93_03, with Q93 parabolic elements and “native” pinballs, black curve, is ductile and presents no oscillations.

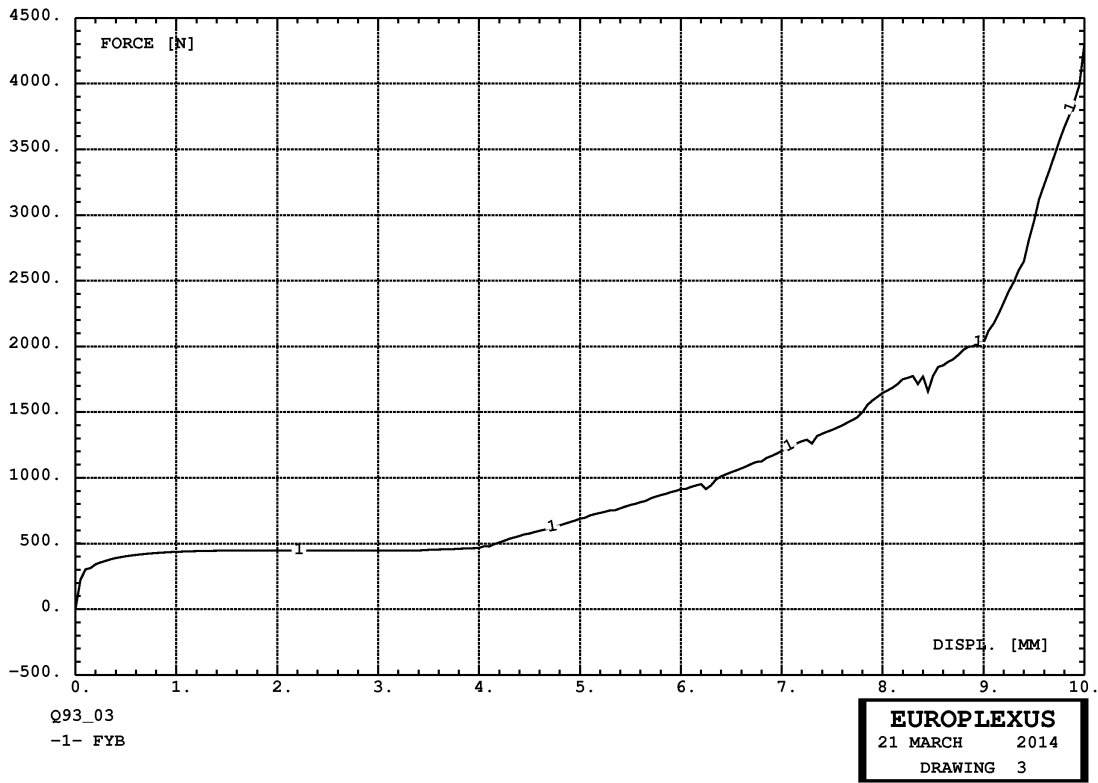


Figure 100 - Crushing force vs. imposed displacement in case Q93_03

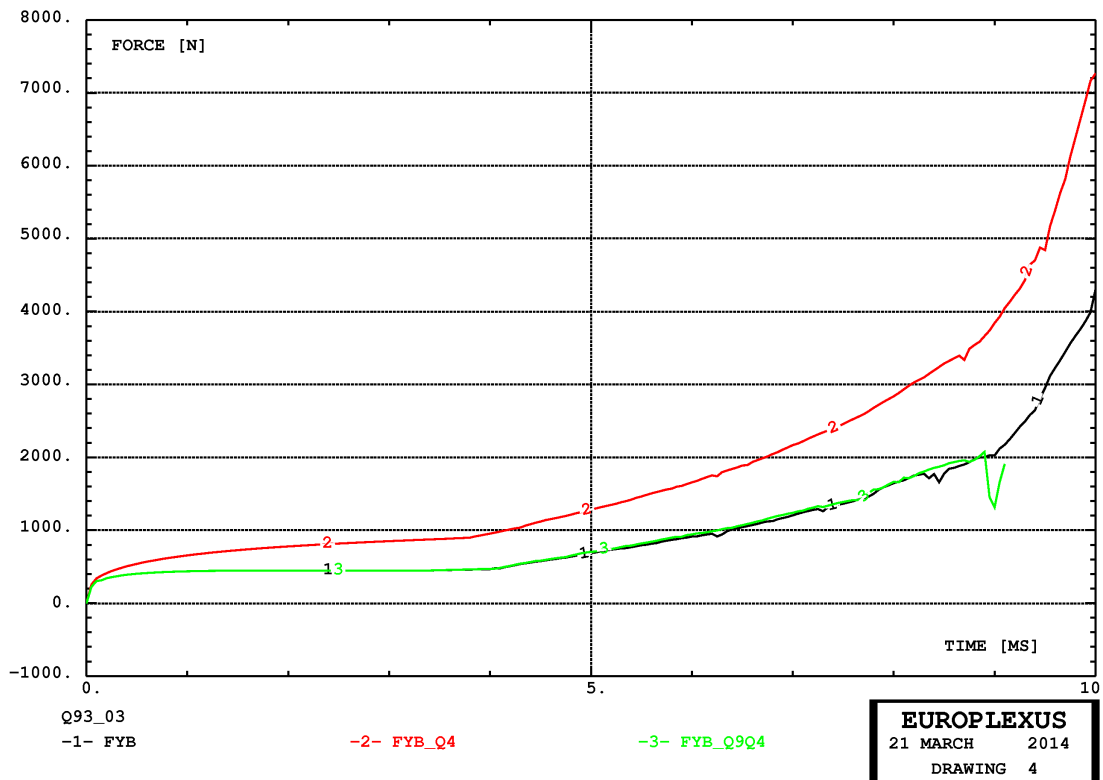


Figure 101 - Crushing force vs. imposed displacement in case Q93_03

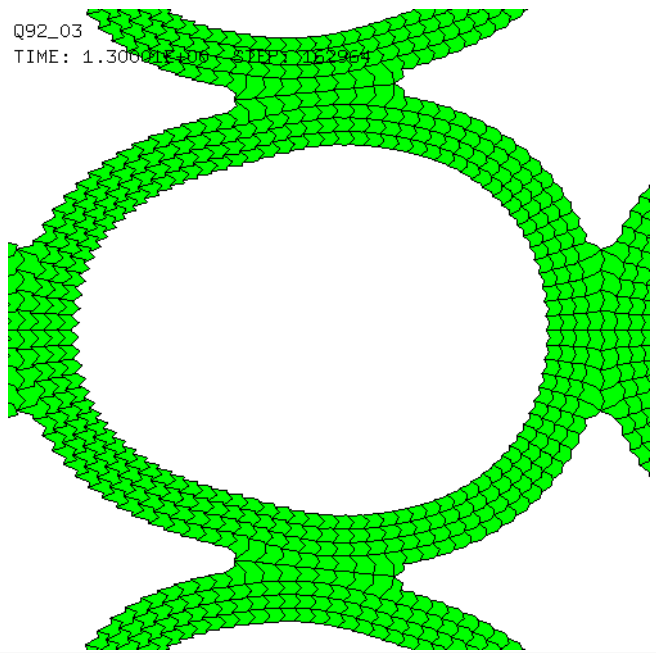
Q92_03

This calculation is identical to Q93_03 but uses the Q92 reduced-integrated element instead of the Q93 fully integrated element. The scope is to see whether the spurious early plastic deformation noted in the previous test depends on the type of numerical integration.

This calculation stopped at step 164,536 at a time of 1.31 s, because of “negative area” in one of the elements. No contact has occurred yet at this time. The failure is due to the onset of hourglass modes, which are known to affect the (under-integrated) Q92. However, the calculation is useful because:

- No early plasticization occurs, showing that this phenomenon is peculiar of the Q93 (fully integrated) element. Some analysis of the problem leads to think that the phenomenon is related to the heavily irregular initial shape of the element in which the phenomenon occurs. This element has an angle of about 130° in the initial configuration and this is by no means advisable. An element *can* undergo very large *distortions*, but its *initial* shape should be relatively regular (especially as angles are concerned). No attempt has been made to modify the mesh because this was not readily available, but a test in such sense would be quite interesting.
- Despite the hourglass, the Q92 solution remains *very precise* in terms of strains, stresses and crushing force until the end of the calculation. The calculation crash is due purely to a geometrical issue (a negative area) which, unfortunately, is fatal. This is very well known, and logical since hourglass modes are zero-energy modes by definition, so they produce no strains and no stresses.

Figure 102 shows the mesh at 1.3 s, with the typical hourglass modes. Figure 103 shows the equivalent plastic strain distribution at the same time. Finally, Figure 104 compares the crushing force (black curve) with the one obtained with the Q93 element (in cyan), the one obtained with the ghost mesh (in green) and the one obtained with the QUA4 element (in red). The agreement between the first three solution mentioned is remarkably good.



Zoom showing the
hourglass modes

Q92_03
TIME: 1.30001E+00 STEP: 162964

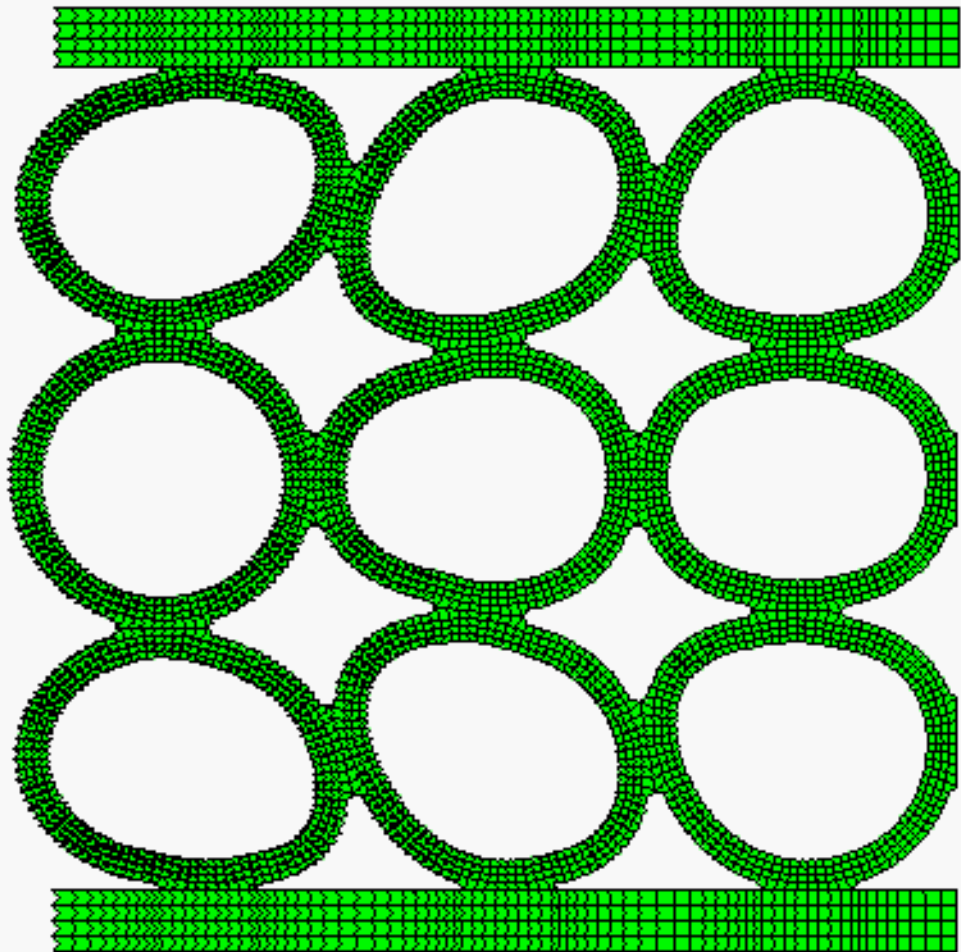


Figure 102 - Distorted mesh with hourglass modes in case Q92_03

Q92_03

TIME: 1.30001E+00 STEP: 162964

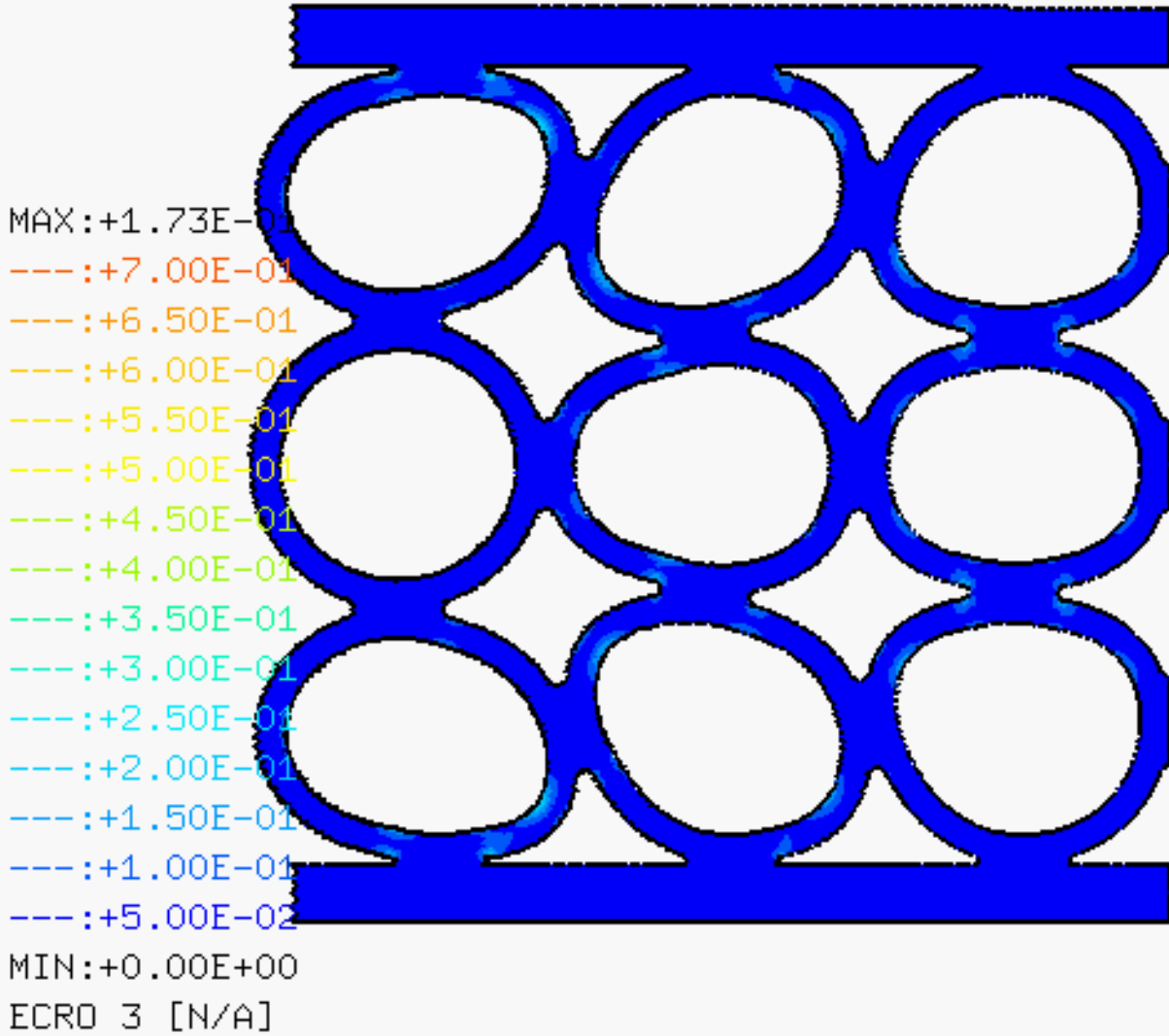


Figure 103 - Equivalent plastic strain in case Q92_03

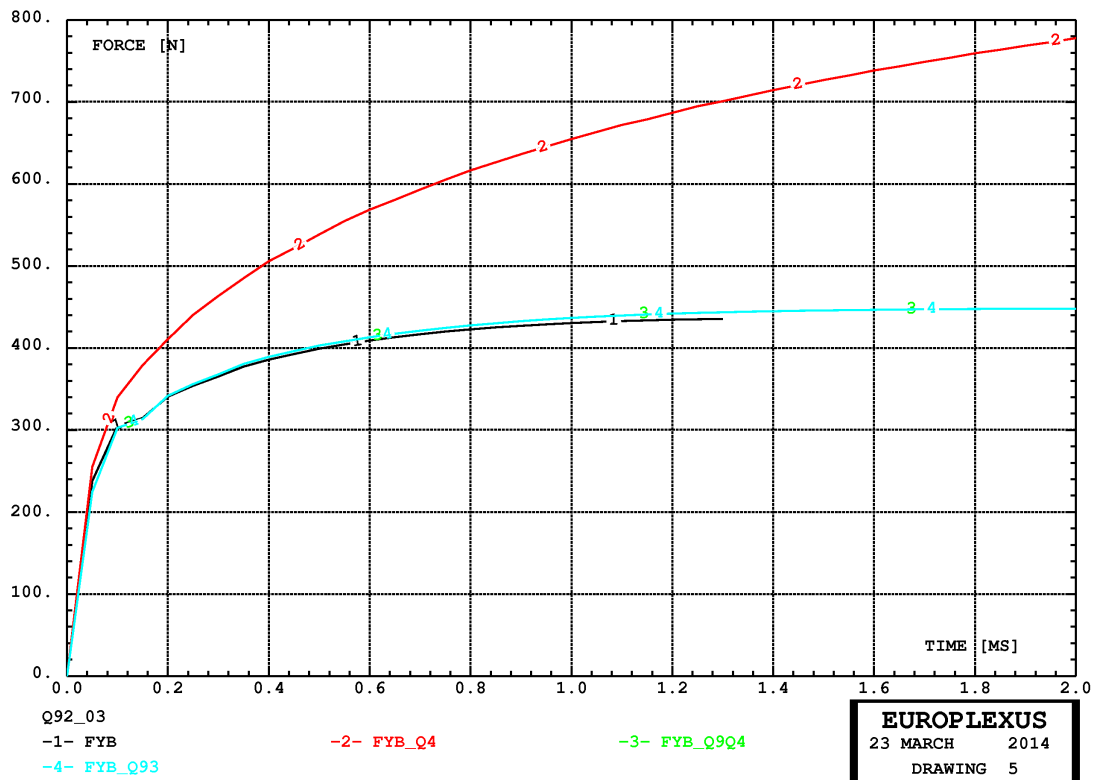


Figure 104 - Crushing force in case Q92_03 compared with previous solutions

Q9M_03

This calculation is identical to Q93_03 but uses a mixture of Q92 and Q93 elements, namely one Q93 every 5 elements (the remaining four being Q92). The scope is to obtain a solution with the advantages of the reduced-integrated element Q92 (cheap, no spurious early plasticization), but without its drawbacks (hourglassing).

The mixed mesh is obtained in Cast3m by an ad-hoc procedure, see file `readq4q9mixed.dgibi` in the Appendix. This results in 3,264 Q92 and 816 Q93.

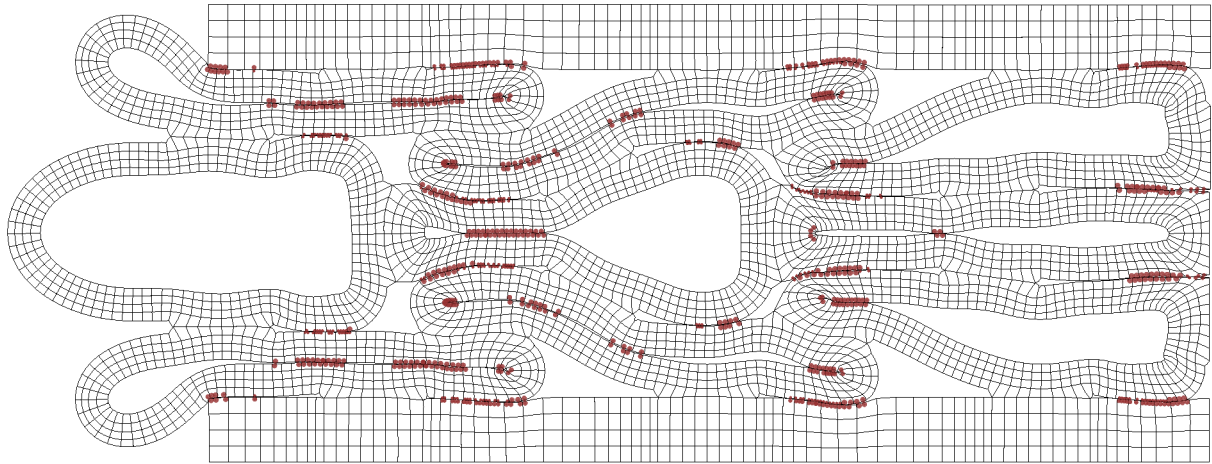
This calculation became very slow at step 3,516,188 and time 8.77 s because the critical step of an element became very small ($\Delta t = 7. \times 10^{-8}$) and the calculation could hardly advance, due to severe distortion of elements near the folds. The CPU at 8.77 s was 52,637 s. However, the energy check was still perfectly OK at that time so the solution was (repeated and) left to continue on a different machine (\\sm02 at JRC), and terminated normally at step 8,827,232 with a total CPU time of 231,252 s for 10 s of physical time.

The solution was (as could be expected) slightly more ductile than with Q93 and for this reason some elements near the folds became very distorted. A calculation with time step partitioning could per-

haps make it until 10 s of physical time with more reasonable CPU, but it remains to try (see cases Q9M_04 and Q9M_05 below). No sign of (significant) hourglassing is present in this solution, except perhaps in the most severely distorted elements at the folds, but this is difficult to distinguish from physical distortion.

Figure 105 shows the final configuration, showing a few contacts. More details are visible in Figure 106. Figure 107 shows the equivalent plastic strain, reaching a maximum of 163% in some folds. No spurious early plasticization is observed. The deformation with the element types (green for the Q92, red for the Q93) is shown in Figure 108.

Q9M_03
TIME: 1.00000E+01 STEP: *****



Q9M_03
TIME: 1.00000E+01 STEP: *****

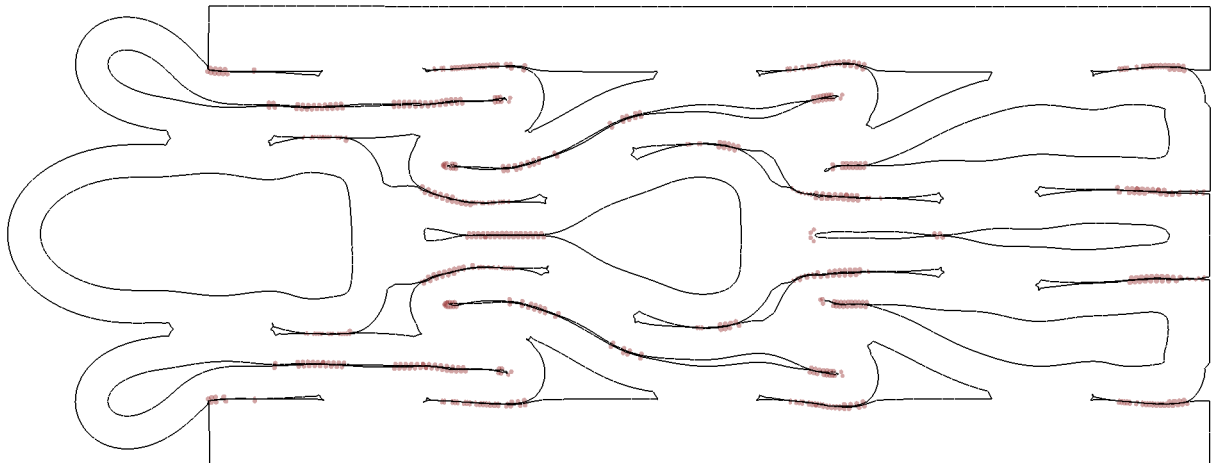


Figure 105 - Distorted mesh with contacts at 8.75 s in case Q9M_03

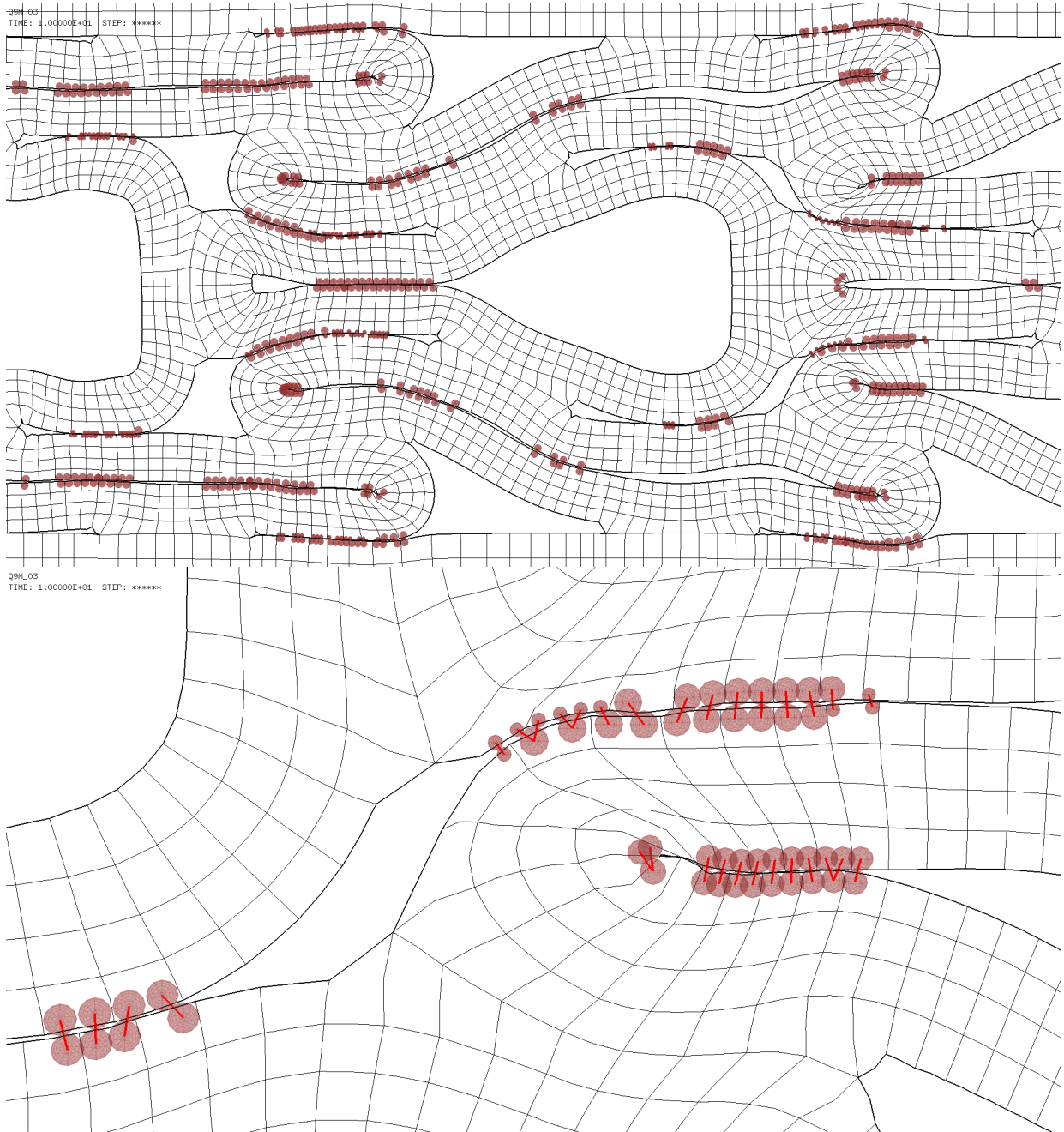


Figure 106 - Distorted mesh and contact details at 8.75 s in case Q9M_03

Q9M_03
TIME: 1.00000E+01 STEP: *****

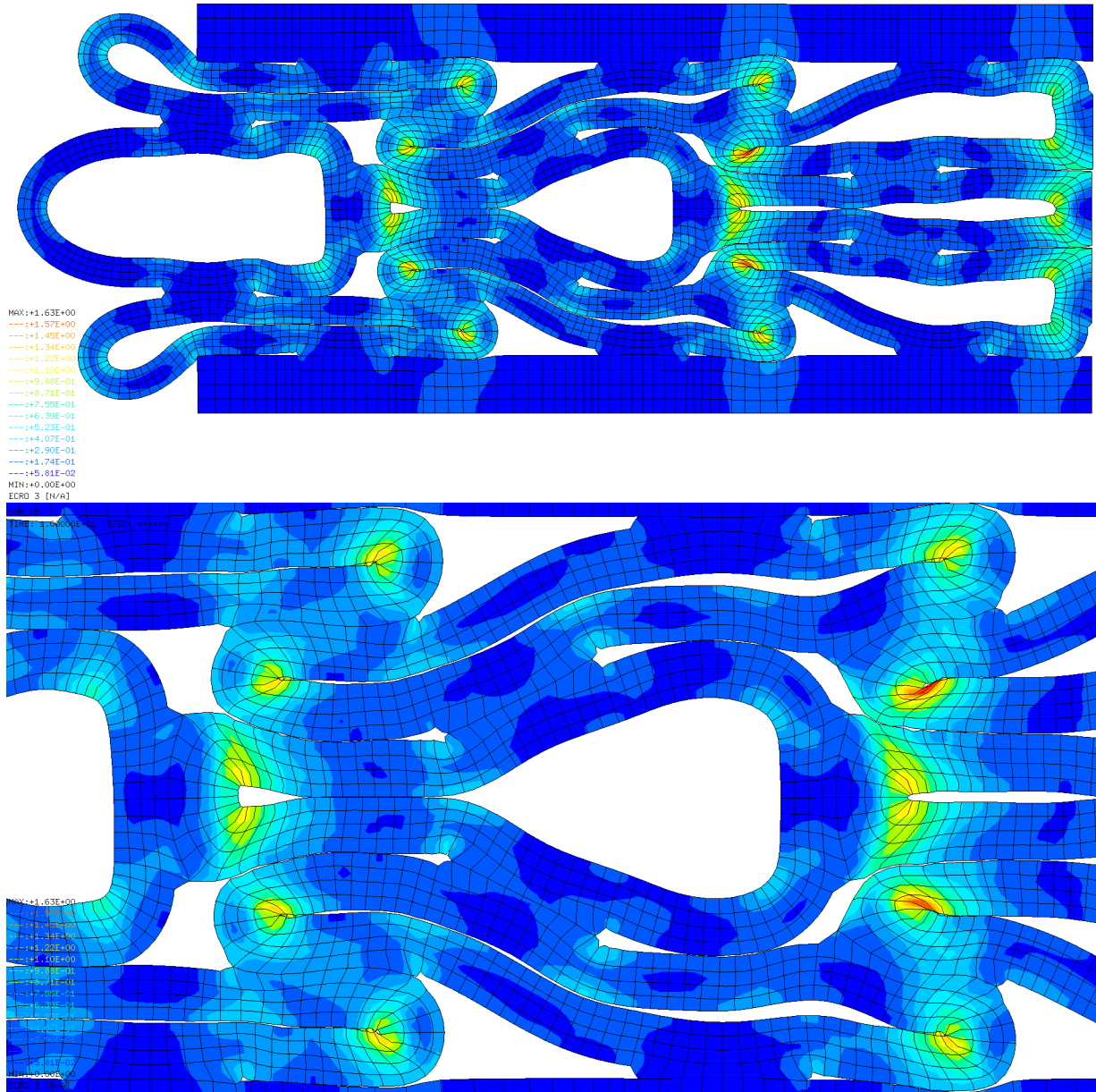


Figure 107 - Equivalent plastic strain at 8.75 s in case Q9M_03

Q9M_03
TIME: 0.00000E+00 STEP: 0

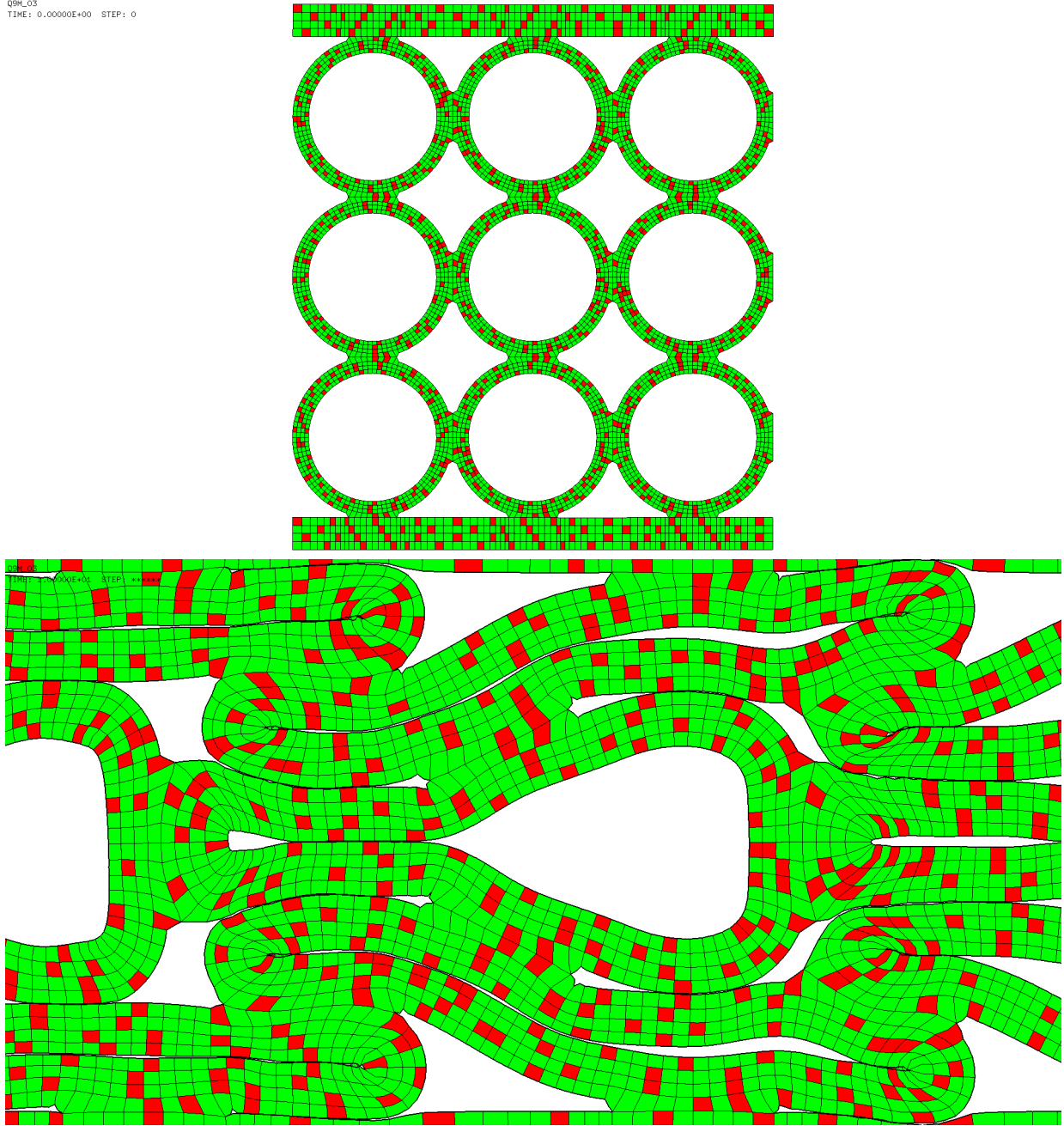


Figure 108 - Element types in case Q9M_03

Figures 109 and 110 compare the crushing force with those of previous solutions and Figure 111 compares the critical time step with that of the calculation with all Q93.

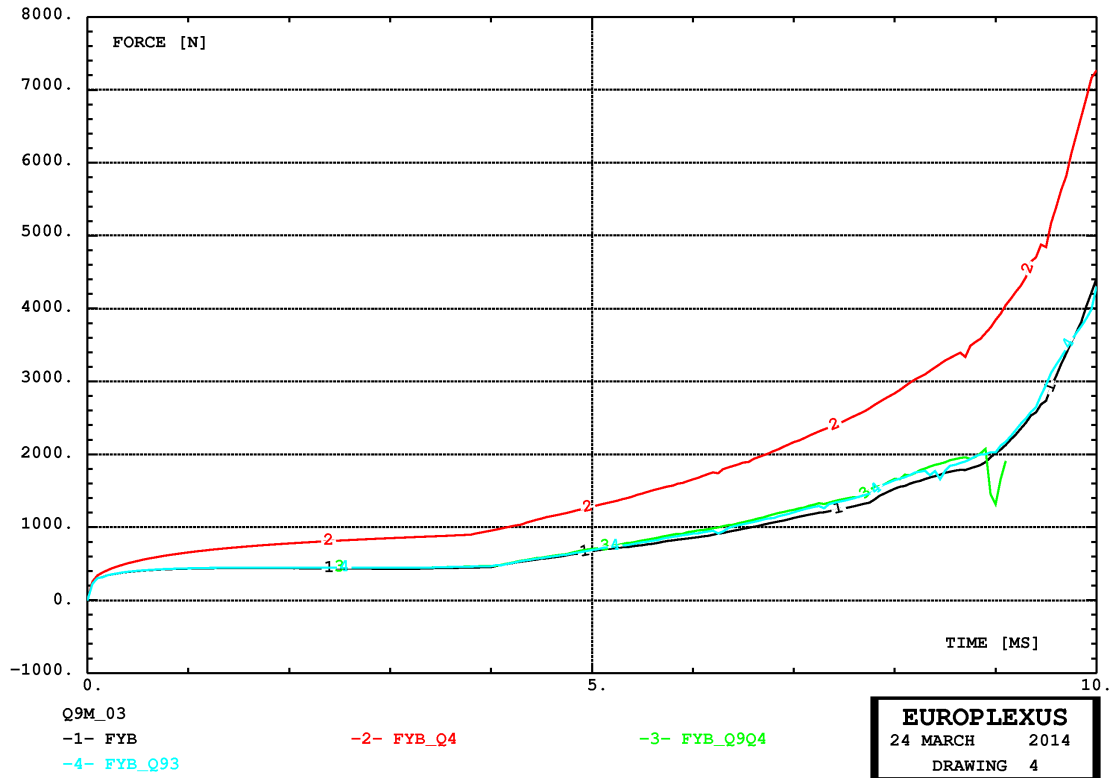


Figure 109 - Crushing force in case Q9M_03 compared with previous solutions

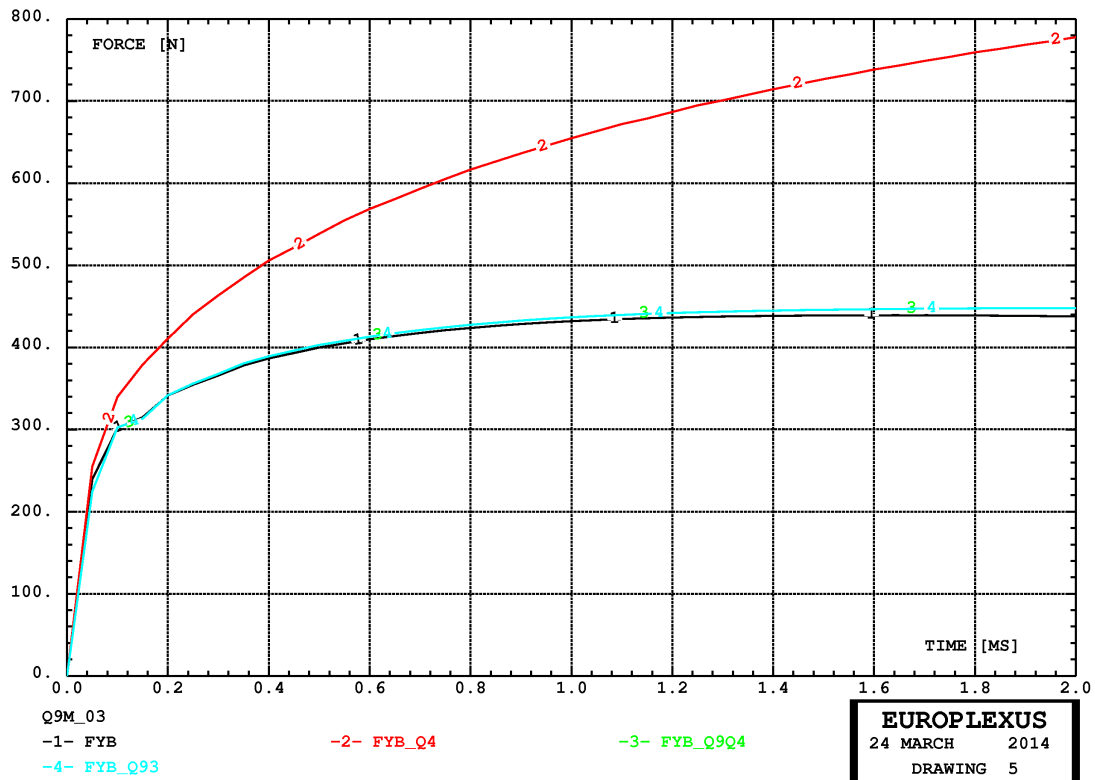


Figure 110 - Crushing force (detail) in case Q9M_03 compared with previous solutions

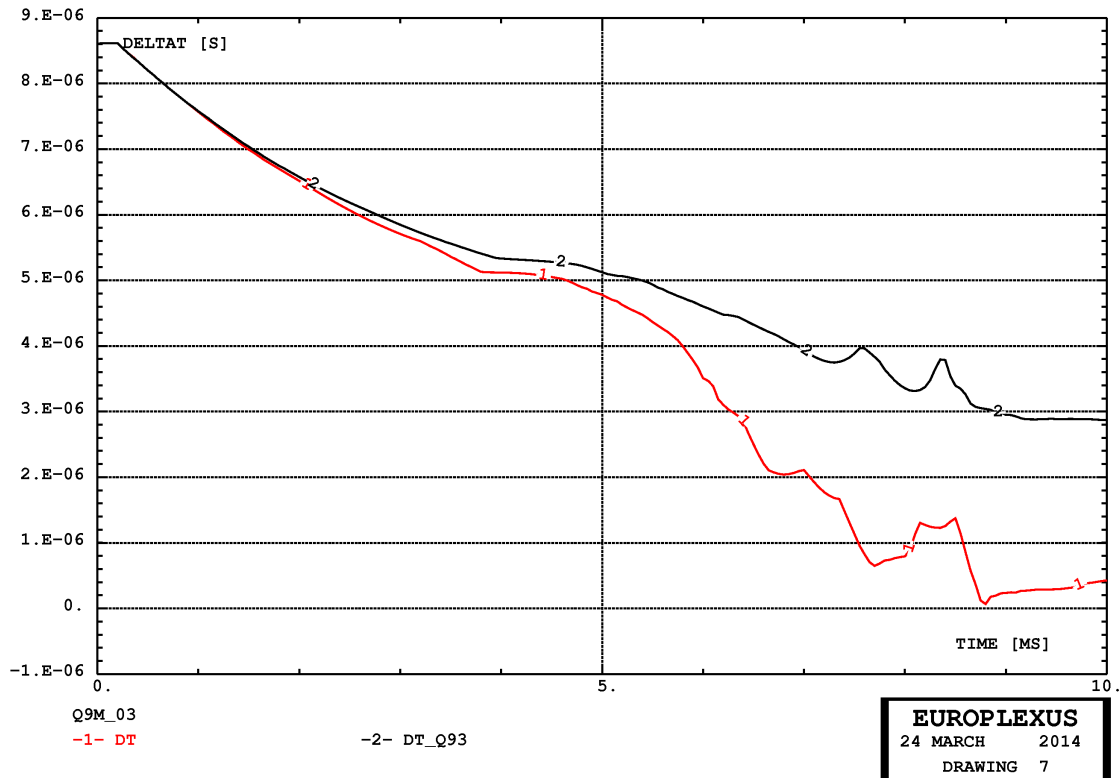


Figure 111 - Critical step in case Q9M_03 (red) and Q93_03 (black)

Q9M_04

This calculation is identical to Q93_03 but uses the OPTI PART PLIN option (spatial time step partitioning) in an attempt to reduce the CPU time. The calculation is unstable and stops at step 126,574, at a physical time of 2.26 s. This may happen with space partitioning since all elements are time-integrated with a local time step, which is therefore much closer to the stability limit of the element itself.

Figure 112 shows the distorted mesh with element types (Q93 in red, Q92 in green). In Figure 113 some local instabilities can be noted near the bottom of the model. Due to instabilities, almost the whole model plasticizes, as shown in Figure 114. A maximum equivalent plastic strain of 936 is reached, which is of course totally un-physical.

Q9M_05

This calculation is identical to Q93_04 but uses CSTA 0.5. The calculation is stable initially, but it stops at step 535,675, at a physical time of 5.99 s, due to the Jacobian becoming zero (too distorted element) in element 3370.

Figure 115 shows the distorted mesh with the element types (Q93 in red, Q92 in green). Figure 116 shows the contacts. Note that some strange element deformation takes place at contacts near the top and bottom of the model, between the plates and the rings.

Figure 117 shows the equivalent plastic strain. Spurious plasticization of the above mentioned contacting elements can be observed.

Figure 118 compares the crushing force (in black) with those of other solutions (in color). The crushing force is correct until about 5.5 s (see also Figure 119), when local oscillations start to appear probably due to the above-mentioned wrong contacts.

Finally, Figure 120 compares the critical time steps of the various solutions.

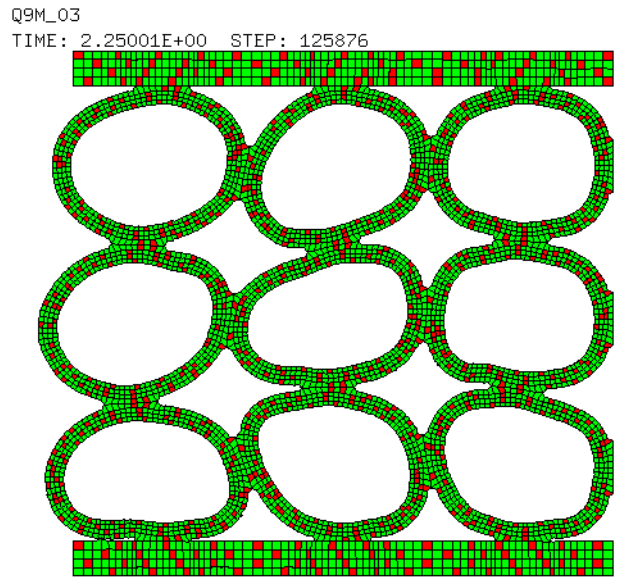


Figure 112 - Distorted mesh with element types in case Q9M_04

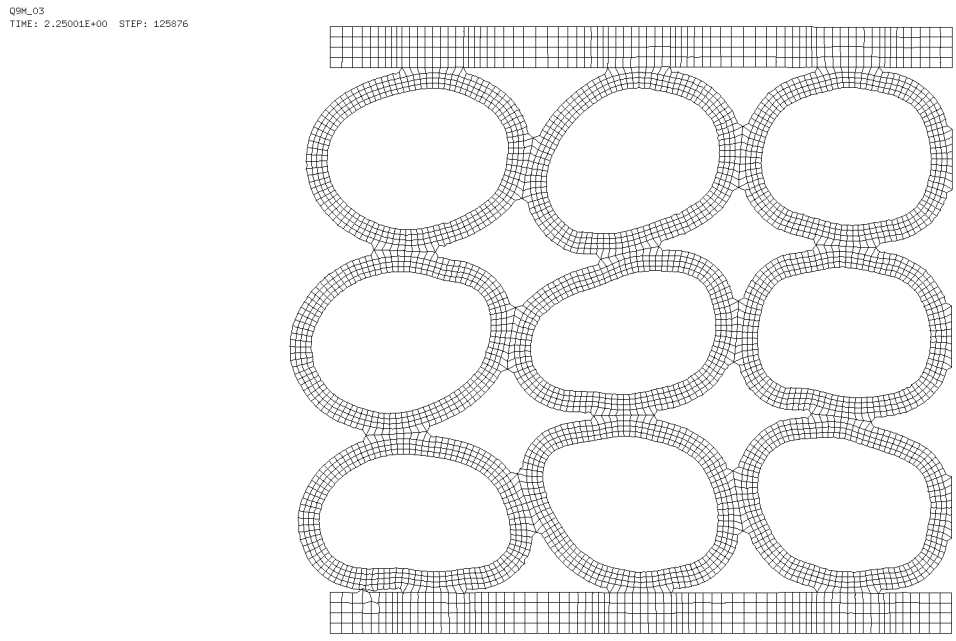
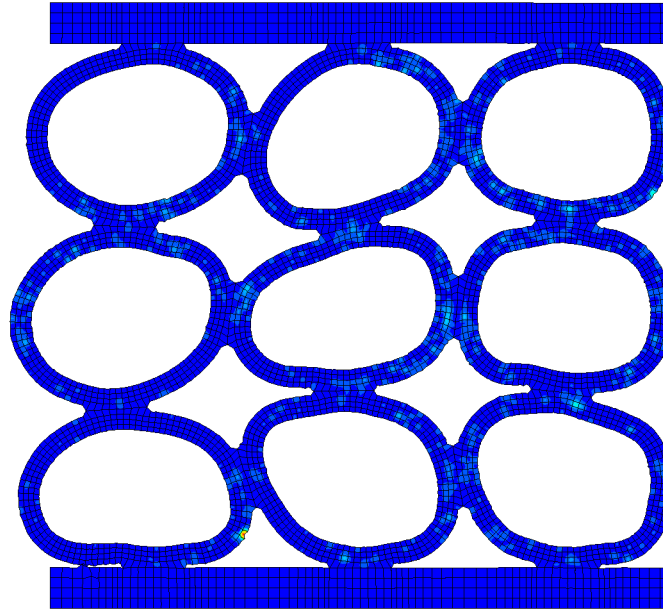


Figure 113 - Distorted mesh and some local instabilities in case Q9M_04

Q9M_03
TIME: 2.25001E+00 STEP: 125876

MAX:+9.36E+02
---:+9.02E+02
---:+8.35E+02
---:+7.69E+02
---:+7.02E+02
---:+6.35E+02
---:+5.68E+02
---:+5.01E+02
---:+4.34E+02
---:+3.68E+02
---:+3.01E+02
---:+2.34E+02
---:+1.67E+02
---:+1.00E+02
---:+3.94E+01
MIN:+2.13E-02
ECRO 3 [N/A]



Q9M_03
TIME: 2.25001E+00 STEP: 125876

MAX:+9.36E+02
---:+7.00E-01
---:+6.50E-01
---:+6.00E-01
---:+5.50E-01
---:+5.00E-01
---:+4.50E-01
---:+4.00E-01
---:+3.50E-01
---:+3.00E-01
---:+2.50E-01
---:+2.00E-01
---:+1.50E-01
---:+1.00E-01
---:+5.00E-02
MIN:+2.13E-02
ECRO 3 [N/A]

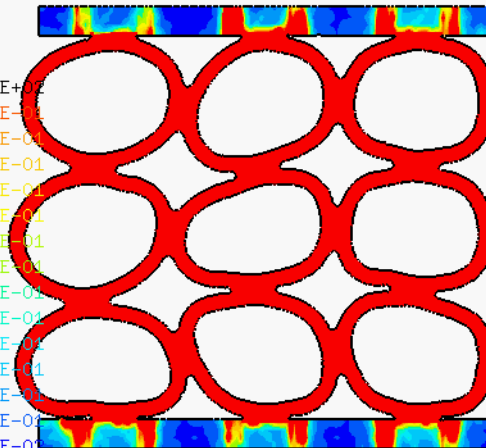


Figure 114 - Equivalent plastic strain (at two different scales) in case Q9M_04

Q9M_05
TIME: 5.95001E+00 STEP: 532239

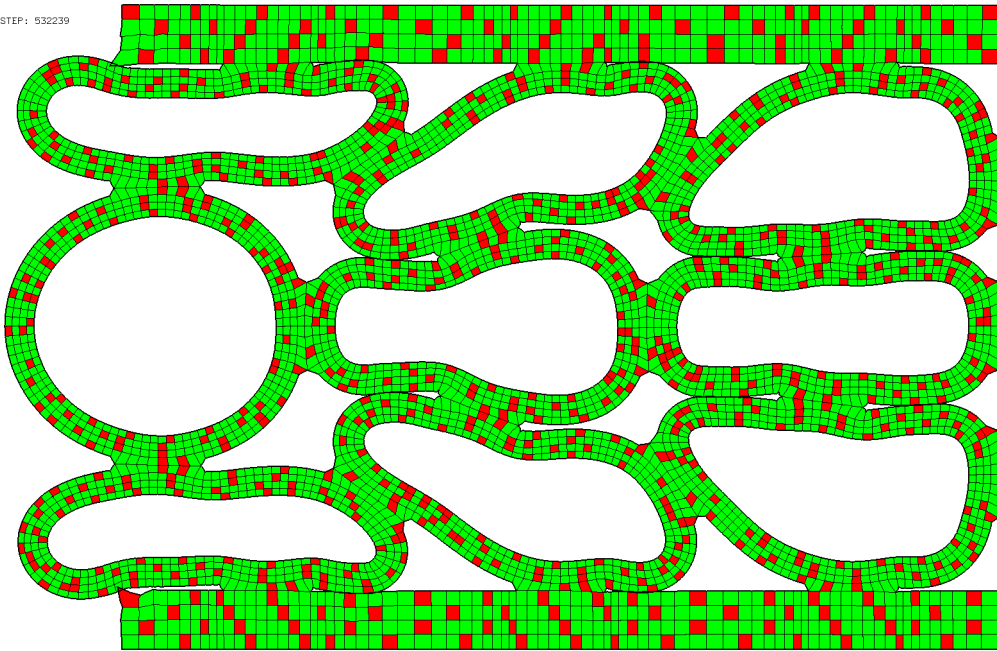


Figure 115 - Distorted mesh with element types in case Q9M_05

Q9M_05
TIME: 5.95001E+00 STEP: 532239

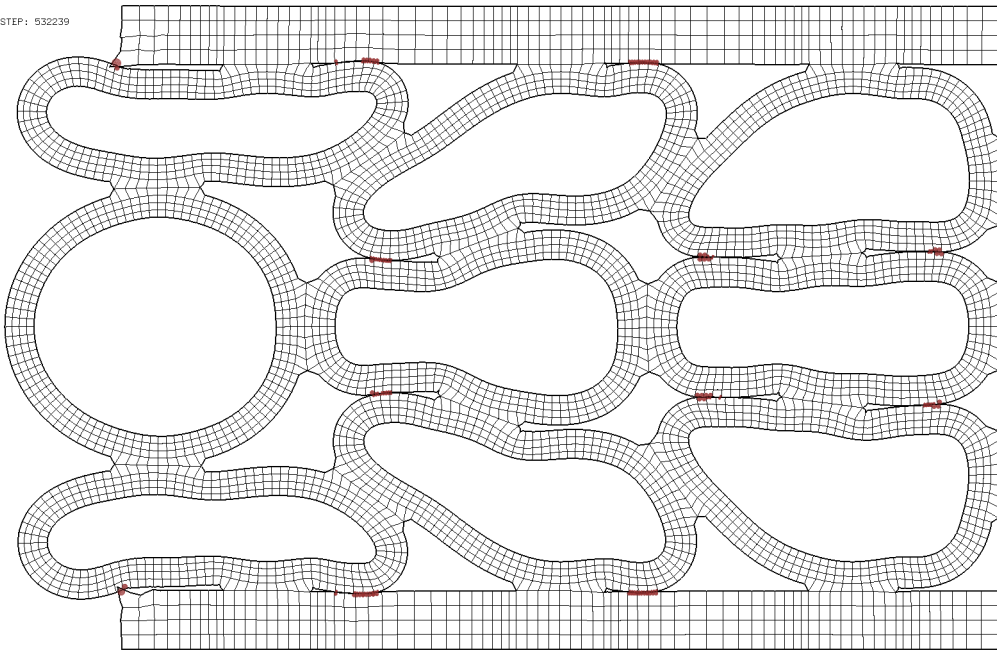


Figure 116 - Distorted mesh with contacts in case Q9M_05

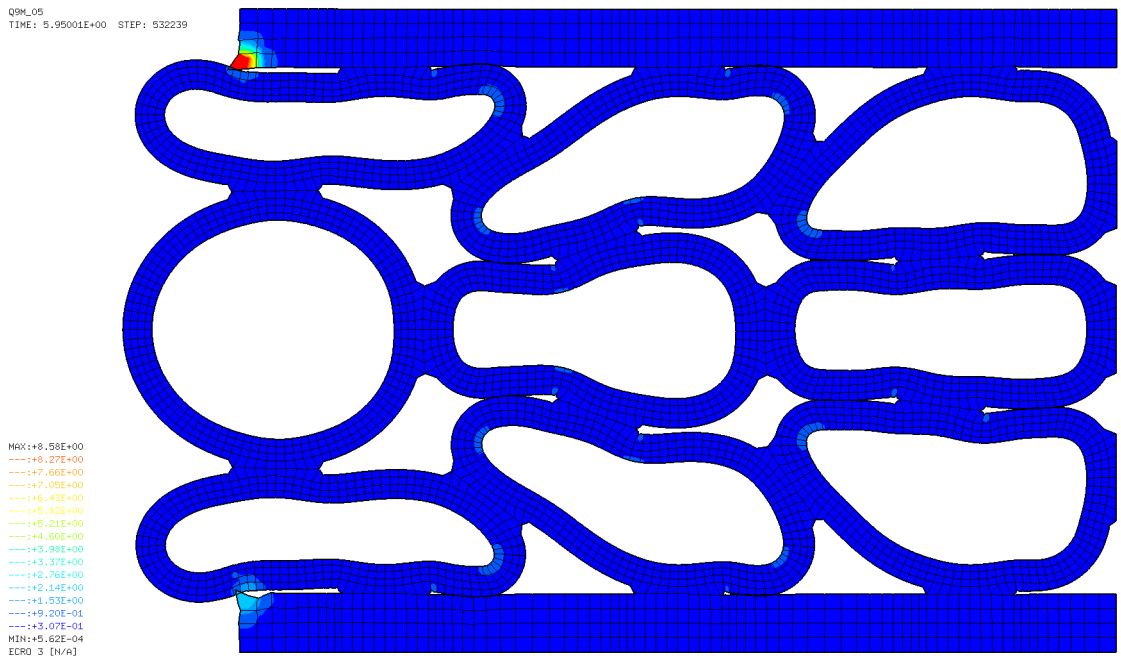


Figure 117 - Equivalent plastic strain in case Q9M_05

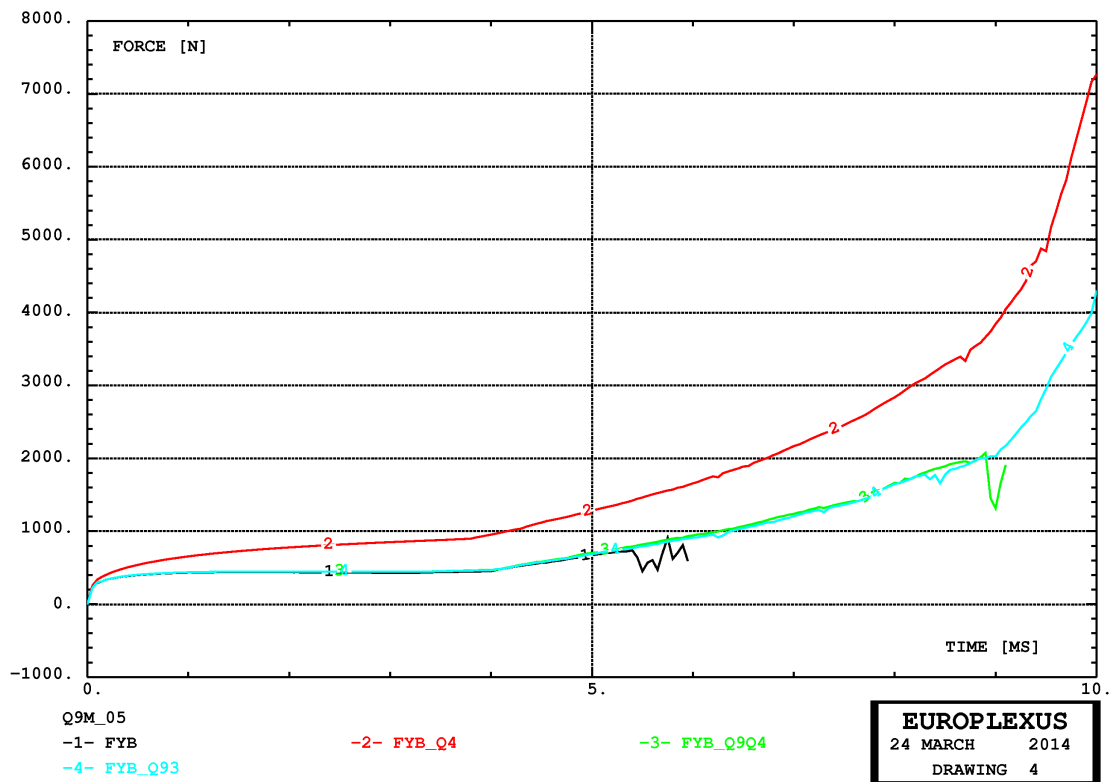


Figure 118 - Crushing force in case Q9M_05 compared with other solutions

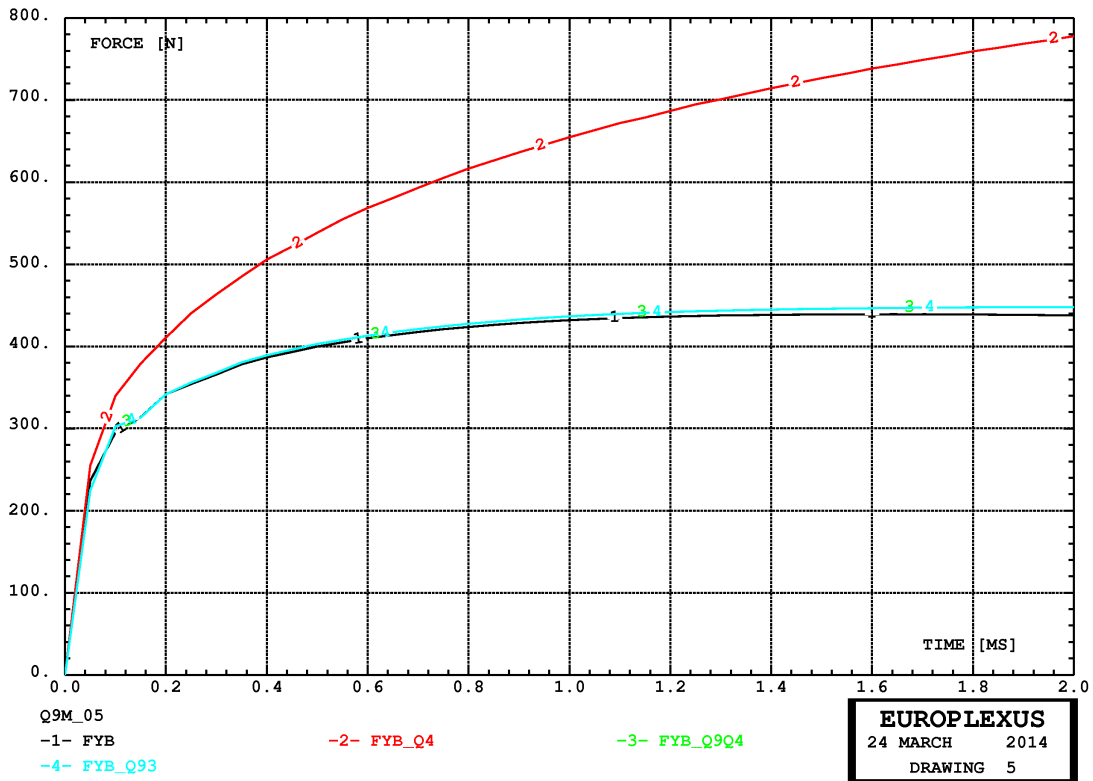


Figure 119 - Crushing force (zoom) in case Q9M_05 compared with other solutions

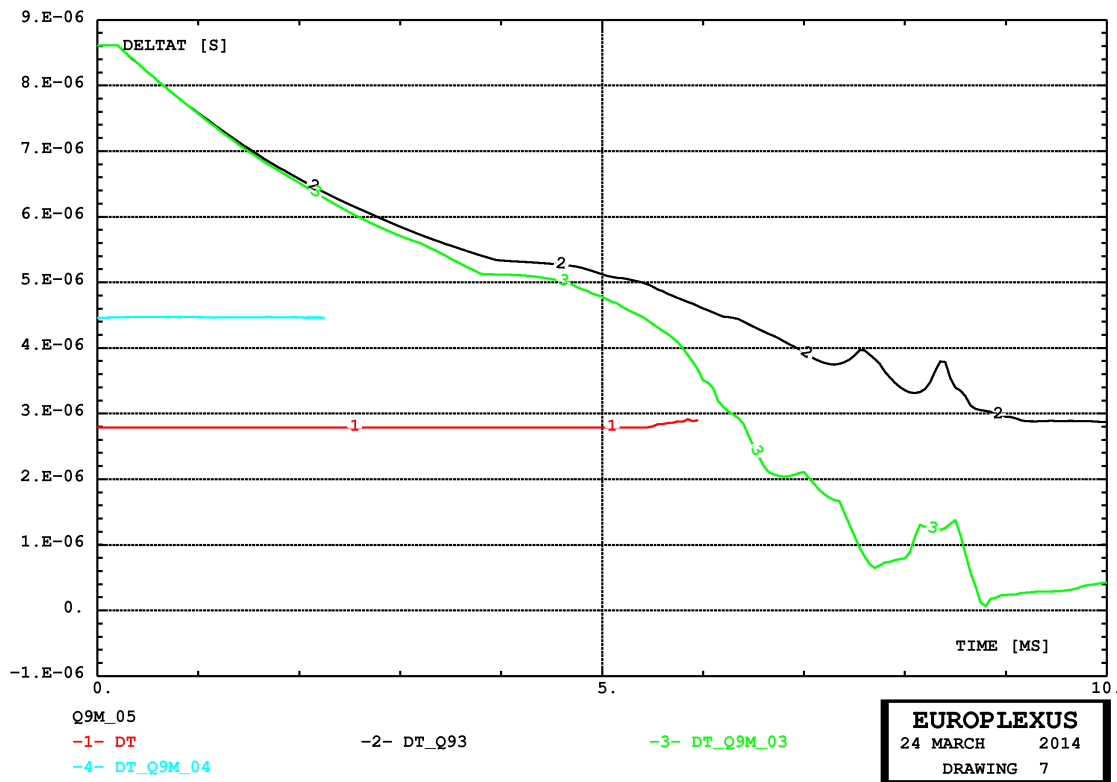


Figure 120 - Critical time step in case Q9M_05 compared with other solutions

Q95_03

This calculation is identical to Q93_03 but uses the Q95 element. This element uses a combination of full and reduced integration in an attempt to avoid both the mechanisms and the locking phenomena. It had been tentatively developed at the end of the eighties, but has been rarely (if ever) used since. This calculation is therefore just for curiosity.

The calculation stopped at step 511,060, at time 3.4 s, because of 0 Jacobian in element 1494. The Q95 element therefore is not completely free of hourglass modes.

Figure 121 shows the near-final configuration (3.4 s), showing a few contacts and some hourglassing. Figures 122 and 123 show the final equivalent plastic strain. No spurious early plasticization is observed.

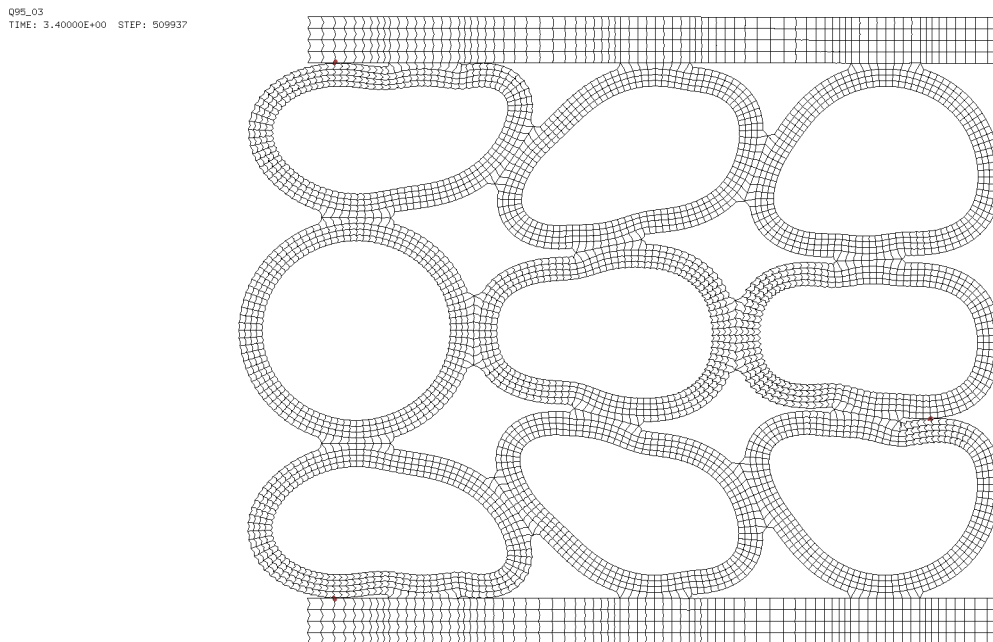


Figure 121 - Distorted mesh with contacts and hourglass modes in case Q95_03

Q95_03
TIME: 3.40000E+00 STEP: 509937

MAX: +1.25E-01
--- +1.21E-01
--- +1.12E-01
--- +1.03E-01
--- +9.40E-02
--- +8.50E-02
--- +7.61E-02
--- +6.71E-02
--- +5.82E-02
--- +4.92E-02
--- +4.03E-02
--- +3.13E-02
--- +2.24E-02
--- +1.34E-02
--- +4.45E-03
MIN: +0.00E+00
ECRO 3 [N/A]

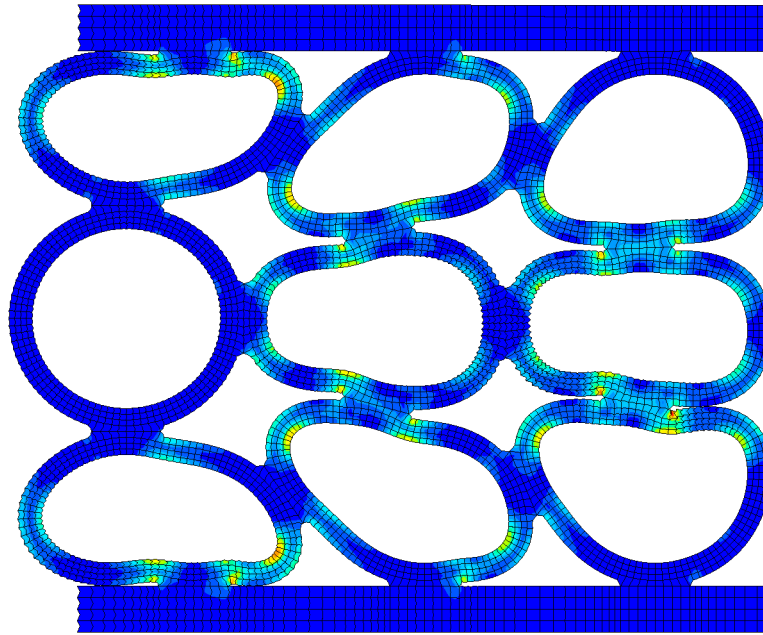


Figure 122 - Equivalent plastic strain in case Q95_03

Q95_03

TIME: 3.40000E+00 STEP: 509937

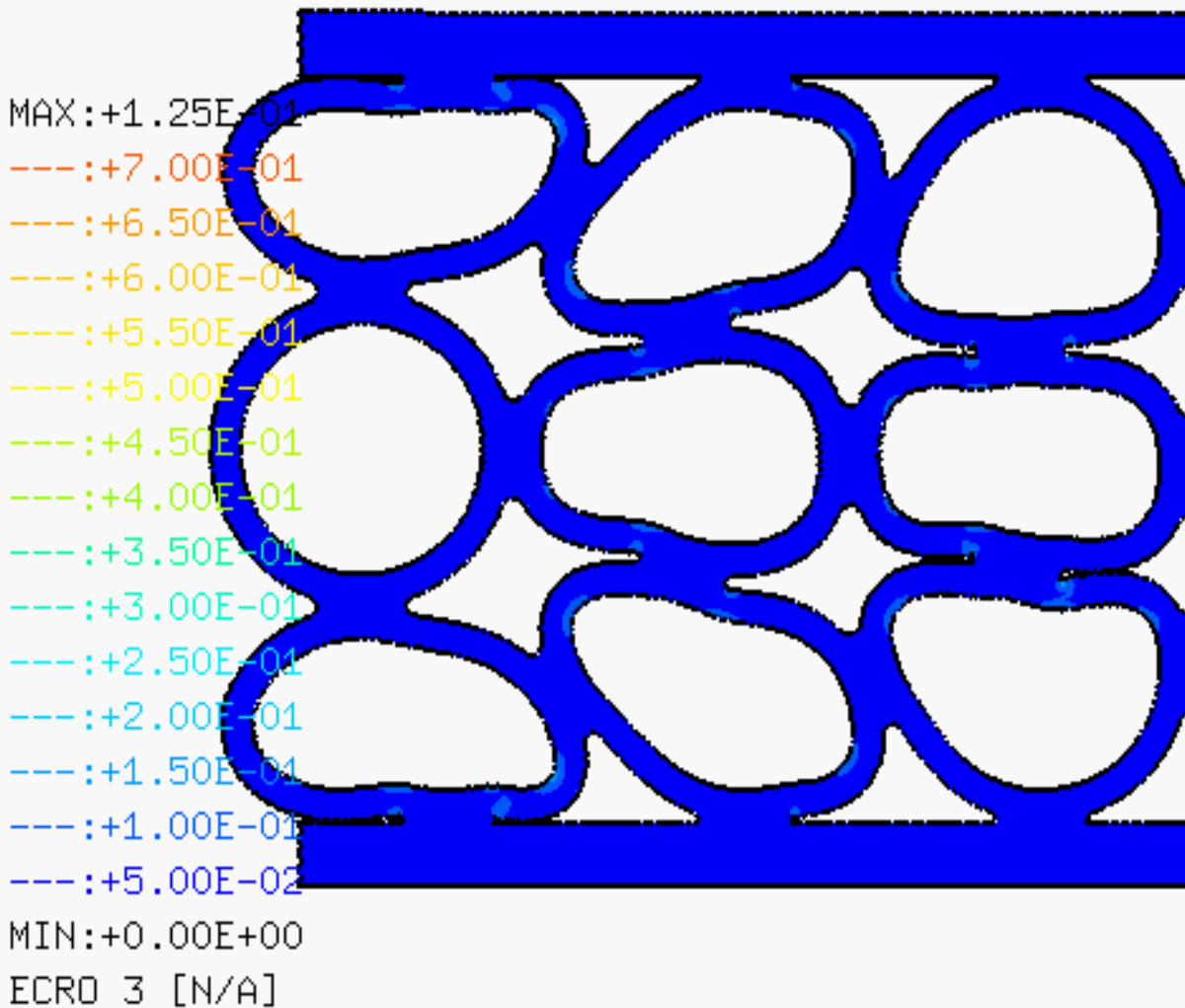


Figure 123 - Equivalent plastic strain (standard scale) in case Q95_03

Figure 124 compares the crushing force with those of previous solutions. The present solution is in good agreement with the previous QUA9 solutions, and only slightly more ductile.

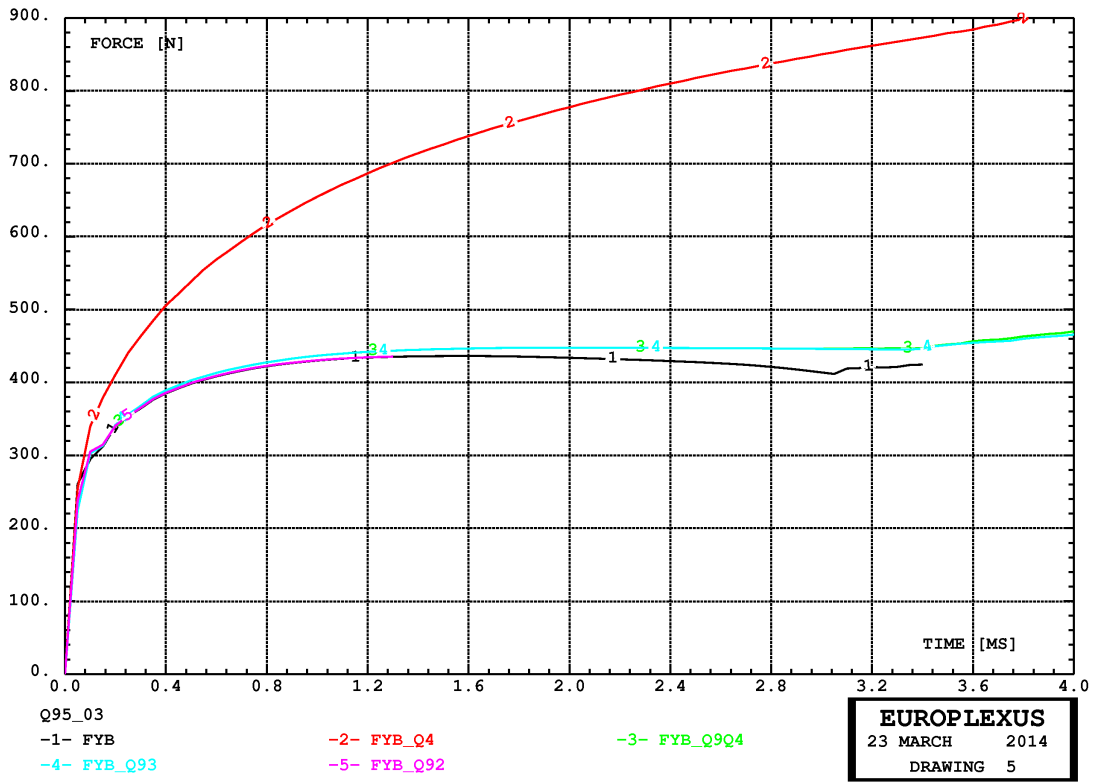


Figure 124 - Crushing force in case Q95_03 compared with previous solutions

5. Conclusions

In this report a native pinball formulation for parabolic elements has been presented, see Section 3. Although the basic tests performed with the new formulation show some problems (especially, but not exclusively, in 3D), the new formulation has been used with relatively good results in a realistic 2D application.

Concerning the practical contact problem of interest, *three alternative approaches* have been tested. The *first approach*, shown in Section 2.1, uses linear elements either fully integrated (CAR4), or reduced-integrated (CAR1) or a mixture of the two in the same calculation.

A complete solution (**CAR401**) up to 10 s of physical time can be obtained with the CAR4, despite some spurious contacts, but the response is too stiff in terms of crushing force with respect to experimental results. This is possibly due to locking phenomena in the fully integrated CAR4 element.

The CAR1 element suffers from mechanisms, so a purely CAR1 solution cannot be obtained because of strong hourglassing. With a mixture of CAR4 and CAR1 a solution (**CARM02**) could be obtained only until 7.2 s, when some hourglassing appeared and element distortion caused a large drop in stability step. Although incomplete, this solution shows a more ductile behavior and the crushing force is in much better agreement than the CAR4 solution with experimental observations.

ALE solutions with the four-node quadrilateral elements specialized for metal forming applications (Q41, Q42, Q41N, Q42N, Q42G) were also obtained. The under-integrated elements (Q41, Q41N) suffer from mechanisms, like their Lagrangian counterparts. The fully-integrated elements give over-stiff solutions, but less stiff than the corresponding Lagrangian elements. Despite ALE and internal mesh rezoning, localized excessive deformation of some elements near the folds cannot be completely avoided, although it is less pronounced than in Lagrangian solutions.

The *second approach*, shown in Section 2.3, uses quadratic elements (Q93) with a superposed ghost mesh of linear elements to detect the contact. A solution could be obtained until almost the final time (**Q93_02**) and was interrupted just accidentally. Some spurious plasticization occurs early in the calculation, due to overly irregular initial shape of some elements (this behavior could be avoided by using Q92 instead of Q93 for these elements), and some spurious contacts. Towards the end of the transient, some oscillations are observed in the crushing force (possibly due to spurious contacts), but until then the solution is as ductile as the CARM02 solution mentioned above. Therefore, the Q93 seems not to suffer from locking in this case.

The *third approach*, shown in Section 4, uses quadratic elements (Q93, Q92 or Q95) with the new native pinball technique for contact detection. A solution with Q93 only (**Q93_03**) has been obtained until the final time. The same spurious localized plasticization as in case Q93_02 remains, but there

are no spurious contacts in the final configuration, and the crushing force is smooth (no oscillations) and as ductile as the best previous solutions. A solution with only Q92 is attempted but, as expected, it suffers from strong mechanisms. A mixed-mesh solution (Q92 and Q93) is also obtained (**Q9M_03**). However, this solution is more expensive than the purely Q93 solution because of greater localized element deformation, while the crushing force is nearly identical. An attempt of using time step partitioning to reduce the CPU time is not particularly successful.

A final comment concerns the **comparison of the present numerical simulations with experimental results**. At Onera, crushing experiments are being performed, but on a much larger array of tubes, of approximately 8 by 8. Here we have considered a simpler set-up involving only 3 by 3 tubes so as to reduce the CPU time of the simulations and make it possible to perform many more parametric studies. Experimental curves for this reduces set-up are not available and therefore cannot be presented here. However, from a few simulations of the full array done at Onera (where parallel machines are available for this purpose) it has been shown that in general the numerical results are “stiffer” than the observed ones. Therefore, any solution which yields a lower crushing force goes in the right direction. Work is also ongoing on a better calibration of the material parameters, especially as concerns the welded joints of the tubes. Once completed the assessment of the various contact and other models being tested, the best ones will be chosen and complete solutions of the full array will be obtained for direct comparison with the experimental curves (but this is left for a forthcoming publication).

6. References

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Fast Transient Continuum Mechanics. EUR 16327 EN, 1995.

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Appendix

Sample input files

This Section contains, in alphabetical file order, the listings of all input files related to the examples which were proposed in the previous Sections.

car101.epx

```

CARI01
ECHO
! CONV WIN
DPLA
$ *** Group B *** Geometry and mesh *****
GEOM
  LIBR POIN 4948 CAR1 4080 TERM
!   LIBR POIN 4950 CAR1 4080 PMAT 2 TERM
$ *** Group B *** Nodes *****
1.50000E+01 5.95437E-30

. . . (skip for brevity)

14949
14950
$ *** Group C *** Geometrics complements *****
COMPLEMENT
!   GROU 2 'p0' LECT 4081 TERM
!   'pl' LECT 4082 TERM
!   EPAI 0.1 LECT p0 pl TERM
  NGROU 3
    'noeuds_bas'
$ ---Gr: 42 NOEUDES_BAS NbNode: 79 ---$
LECT
  1      6      11      16      21      26      31
  36     41     46     51     56     57     70
  78     80     94     104    107    118    130
  134    142    156    161    166    167    168
  169    170    171    172    190    215    236
  242    257    262    263    286    294    296
  320    330    333    354    366    370    388
  402    407    412    413    414    415    416
  417    418    446    481    512    518    543
  548    577    585    616    626    655    667
  694    708    713    714    715    716    717
  718    719 TERM
'noeuds_haut'
$ ---Gr: 43 NOEUDES_HAUT NbNode: 79 ---$
LECT
  4267   4268   4269   4270   4271   4272   4273
  4274   4275   4309   4314   4348   4353   4387
  4392   4421   4426   4455   4460   4493   4530
  4535   4548   4549   4550   4551   4552   4553
  4554   4555   4556   4576   4585   4590   4610
  4619   4624   4644   4653   4658   4678   4687
  4692   4707   4712   4731   4754   4781   4794
  4795   4796   4797   4798   4799   4800   4801
  4802   4812   4821   4826   4836   4845   4850
  4860   4869   4874   4884   4893   4898   4903
  4908   4913   4918   4923   4928   4933   4938
  4943   4948 TERM
$ ---Gr: 44 NOEUDES_SYM NbNode: 35 ---$
'noeuds_sym'
LECT
  2      3      4      5      528    562    601
  640    679    725    767    805    839    1933
  1967   2006   2045   2084   2130   2172   2210
  2243   3333   3370   3411   3452   3493   3538
  3579   3616   3648   4456   4457   4458   4459

TERM
GROU 25
$ ---Gr: 17 CONTACT_INTER_001 NbElem: 22 ---$
'con01'
LECT
  676    682    689    694    700    706    756
  757    758    759    760    761    762    763
  764    765    766    767    768    769    770
  771 TERM
$ ---Gr: 18 CONTACT_INTER_002 NbElem: 28 ---$
'con02'
LECT
  949    955    962    967    973    979    1029
  1030   1031   1032   1033   1034   1035   1036
  1415   1421   1428   1433   1439   1445   1495
  1496   1497   1498   1499   1500   1501   1502

TERM
$ ---Gr: 19 CONTACT_INTER_003 NbElem: 28 ---$
'con03'
LECT
  1182   1188   1195   1200   1206   1212   1262
  1263   1264   1265   1266   1267   1268   1269
  1935   1941   1948   1953   1959   1965   2015
  2016   2017   2018   2019   2020   2021   2022

TERM
$ ---Gr: 20 CONTACT_INTER_004 NbElem: 23 ---$
'con04'
LECT
  1503   1662   1668   1675   1680   1686   1692
  1742   1743   1744   1745   1746   1747   1748
  1749   1750   1751   1752   1753   1754   1755
  1756   1757 TERM
$ ---Gr: 21 CONTACT_INTER_005 NbElem: 44 ---$
'con05'
LECT
  675    679    681    686    688    692    693
  698    699    704    705    710    740    741

```

```

  742    743    744    745    746    747    748
  749    750    751    752    753    754    755
  772    773    774    775    776    777    778
  779    780    781    782    783    784    785
  786    787 TERM
$ ---Gr: 22 CONTACT_INTER_006 NbElem: 56 ---$
'con06'
LECT
  948    952    954    959    961    965    966
  971    972    977    978    983    1013   1014
  1015   1016   1017   1018   1019   1020   1021
  1022   1023   1024   1025   1026   1027   1028
  1414   1418   1420   1425   1427   1431   1432
  1437   1438   1443   1444   1449   1479   1480
  1481   1482   1483   1484   1485   1486   1487
  1488   1489   1490   1491   1492   1493   1494

TERM
$ ---Gr: 23 CONTACT_INTER_007 NbElem: 56 ---$
'con07'
LECT
  1181   1185   1187   1192   1194   1198   1199
  1204   1205   1210   1211   1216   1246   1247
  1248   1249   1250   1251   1252   1253   1254
  1255   1256   1257   1258   1259   1260   1261
  1934   1938   1940   1945   1947   1951   1952
  1957   1958   1963   1964   1969   1999   2000
  2001   2002   2003   2004   2005   2006   2007
  2008   2009   2010   2011   2012   2013   2014

TERM
$ ---Gr: 24 CONTACT_INTER_008 NbElem: 46 ---$
'con08'
LECT
  1504   1505   1661   1665   1667   1672   1674
  1678   1679   1684   1685   1690   1691   1696
  1726   1727   1728   1729   1730   1731   1732
  1733   1734   1735   1736   1737   1738   1739
  1740   1741   1758   1759   1760   1761   1762
  1763   1764   1765   1766   1767   1768   1769
  1770   1771   1772   1773 TERM
$ ---Gr: 25 CONTACT_INTER_009 NbElem: 44 ---$
'con09'
LECT
  678    680    684    685    690    691    696
  697    702    703    708    709    724    725
  726    727    728    729    730    731    732
  733    734    735    736    737    738    739
  788    789    790    791    792    793    794
  795    796    797    798    799    800    801
  802    803 TERM
$ ---Gr: 26 CONTACT_INTER_010 NbElem: 56 ---$
'con10'
LECT
  951    953    957    958    963    964    969
  970    975    976    981    982    997    998
  999   1000   1001   1002   1003   1004   1005
  1006   1007   1008   1009   1010   1011   1012
  1417   1419   1423   1424   1429   1430   1435
  1436   1441   1442   1447   1448   1463   1464
  1465   1466   1467   1468   1469   1470   1471
  1472   1473   1474   1475   1476   1477   1478

TERM
$ ---Gr: 27 CONTACT_INTER_011 NbElem: 56 ---$
'con11'
LECT
  1184   1186   1190   1191   1196   1197   1202
  1203   1208   1209   1214   1215   1230   1231
  1232   1233   1234   1235   1236   1237   1238
  1239   1240   1241   1242   1243   1244   1245
  1937   1939   1943   1944   1949   1950   1955
  1956   1961   1962   1967   1968   1983   1984
  1985   1986   1987   1988   1989   1990   1991
  1992   1993   1994   1995   1996   1997   1998

TERM
$ ---Gr: 28 CONTACT_INTER_012 NbElem: 46 ---$
'con12'
LECT
  1506   1507   1664   1666   1670   1671   1676
  1677   1682   1683   1688   1689   1694   1695
  1710   1711   1712   1713   1714   1715   1716
  1717   1718   1719   1720   1721   1722   1723
  1724   1725   1774   1775   1776   1777   1778
  1779   1780   1781   1782   1783   1784   1785
  1786   1787   1788   1789 TERM
$ ---Gr: 29 CONTACT_EXTER_001 NbElem: 27 ---$
'con13'
LECT
  523    524    525    526    527    528    529
  530    677    683    687    695    701    707
  711    712    713    714    715    716    717
  718    719    720    721    722    723 TERM
$ ---Gr: 30 CONTACT_EXTER_002 NbElem: 38 ---$
'con14'
LECT
  950    956    960    968    974    980    984
  985    986    987    988    989    990    991
  992    993    994    995    996    1416   1422
  1426   1434   1440   1446   1450   1451   1452
  1453   1454   1455   1456   1457   1458   1459
  1460   1461   1462 TERM
$ ---Gr: 31 CONTACT_EXTER_003 NbElem: 38 ---$
'con15'
LECT
  1183   1189   1193   1201   1207   1213   1217
  1218   1219   1220   1221   1222   1223   1224
  1225   1226   1227   1228   1229   1936   1942
  1946   1954   1960   1966   1970   1971   1972
  1973   1974   1975   1976   1977   1978   1979
  1980   1981   1982 TERM
$ ---Gr: 32 CONTACT_EXTER_004 NbElem: 28 ---$
'con16'
LECT
  1508   1509   1510   1511   1512   1513   1514
  1515   1516   1663   1669   1673   1681   1687
  1693   1697   1698   1699   1700   1701   1702
  1703   1704   1705   1706   1707   1708   1709

TERM
$ ---Gr: 33 CONTACT_TUBE_001 NbElem: 96 ---$
'con17'

```



```

LECT
532 533 540 541 547 548 551
554 559 560 563 566 569 572
577 578 581 584 587 590 593
596 649 650 651 652 653 654
655 656 657 658 659 660 661
662 663 664 665 666 667 668
669 670 671 672 673 674 805
806 813 814 820 821 824 827
832 833 836 839 842 845 850
851 854 857 860 863 866 869
922 923 924 925 926 927 928
929 930 931 932 933 934 935
936 937 938 939 940 941 942
943 944 945 946 947 TERM

$---Gr: 34 CONTACT_TUBE_002 NbElem: 96 ---$
'con18'
LECT
1038 1039 1046 1047 1053 1054 1057
1060 1065 1066 1069 1072 1075 1078
1083 1084 1087 1090 1093 1096 1099
1102 1155 1156 1157 1158 1159 1160
1161 1162 1163 1164 1165 1166 1167
1168 1169 1170 1171 1172 1173 1174
1175 1176 1177 1178 1179 1180 1271
1272 1279 1280 1286 1287 1290 1293
1298 1299 1302 1305 1308 1311 1316
1317 1320 1323 1326 1329 1332 1335
1388 1389 1390 1391 1392 1393 1394
1395 1396 1397 1398 1399 1400 1401
1402 1403 1404 1405 1406 1407 1408
1409 1410 1411 1412 1413 TERM

$---Gr: 35 CONTACT_TUBE_003 NbElem: 96 ---$
'con19'
LECT
1518 1519 1526 1527 1533 1534 1537
1540 1545 1546 1549 1552 1555 1558
1563 1564 1567 1570 1573 1576 1579
1582 1635 1636 1637 1638 1639 1640
1641 1642 1643 1644 1645 1646 1647
1648 1649 1650 1651 1652 1653 1654
1655 1656 1657 1658 1659 1660 1791
1792 1799 1800 1806 1807 1810 1813
1818 1819 1822 1825 1828 1831 1836
1837 1840 1843 1846 1849 1852 1855
1908 1909 1910 1911 1912 1913 1914
1915 1916 1917 1918 1919 1920 1921
1922 1923 1924 1925 1926 1927 1928
1929 1930 1931 1932 1933 TERM

$---Gr: 36 CONTACT_TUBE_004 NbElem: 96 ---$
'con20'
LECT
531 536 539 542 545 546 550
553 557 558 562 565 568 571
575 576 580 583 586 589 592
595 623 624 625 626 627 628
629 630 631 632 633 634 635
636 637 638 639 640 641 642
643 644 645 646 647 648 804
809 812 815 818 819 823 826
830 831 835 838 841 844 848
849 853 856 859 862 865 868
896 897 898 899 900 901 902
903 904 905 906 907 908 909
910 911 912 913 914 915 916
917 918 919 920 921 TERM

$---Gr: 37 CONTACT_TUBE_005 NbElem: 96 ---$
'con21'
LECT
1037 1042 1045 1048 1051 1052 1056
1059 1063 1064 1068 1071 1074 1077
1081 1082 1086 1089 1092 1095 1098
1101 1129 1130 1131 1132 1133 1134
1135 1136 1137 1138 1139 1140 1141
1142 1143 1144 1145 1146 1147 1148
1149 1150 1151 1152 1153 1154 1270
1275 1278 1281 1284 1285 1289 1292
1296 1297 1301 1304 1307 1310 1314
1315 1319 1322 1325 1328 1331 1334
1362 1363 1364 1365 1366 1367 1368
1369 1370 1371 1372 1373 1374 1375
1376 1377 1378 1379 1380 1381 1382
1383 1384 1385 1386 1387 TERM

$---Gr: 38 CONTACT_TUBE_006 NbElem: 96 ---$
'con22'
LECT
1517 1522 1525 1528 1531 1532 1536
1539 1543 1544 1548 1551 1554 1557
1561 1562 1566 1569 1572 1575 1578
1581 1609 1610 1611 1612 1613 1614
1615 1616 1617 1618 1619 1620 1621
1622 1623 1624 1625 1626 1627 1628
1629 1630 1631 1632 1633 1634 1790
1795 1798 1801 1804 1805 1809 1812
1816 1817 1821 1824 1827 1830 1834
1835 1839 1842 1845 1848 1851 1854
1882 1883 1884 1885 1886 1887 1888
1889 1890 1891 1892 1893 1894 1895
1896 1897 1898 1899 1900 1901 1902
1903 1904 1905 1906 1907 TERM

$---Gr: 39 CONTACT_TUBE_007 NbElem: 96 ---$
'con23'
LECT
534 535 537 538 543 544 549
552 555 556 561 564 567 570
573 574 579 582 585 588 591
594 597 598 599 600 601 602
603 604 605 606 607 608 609
610 611 612 613 614 615 616
617 618 619 620 621 622 807
808 810 811 816 817 822 825
828 829 834 837 840 843 846
847 852 855 858 861 864 867
870 871 872 873 874 875 876
877 878 879 880 881 882 883
884 885 886 887 888 889 890
891 892 893 894 895 TERM

$---Gr: 40 CONTACT_TUBE_008 NbElem: 96 ---$
'con24'
LECT
1040 1041 1043 1044 1049 1050 1055
1058 1061 1062 1067 1070 1073 1076
1079 1080 1085 1088 1091 1094 1097
1100 1103 1104 1105 1106 1107 1108
1109 1110 1111 1112 1113 1114 1115
1116 1117 1118 1119 1120 1121 1122
1123 1124 1125 1126 1127 1128 1273
1274 1276 1277 1282 1283 1288 1291
1294 1295 1300 1303 1306 1309 1312
1313 1318 1321 1324 1327 1330 1333
1336 1337 1338 1339 1340 1341 1342
1343 1344 1345 1346 1347 1348 1349
1350 1351 1352 1353 1354 1355 1356
1357 1358 1359 1360 1361 TERM

$---Gr: 41 CONTACT_TUBE_009 NbElem: 96 ---$
'con25'
LECT
1520 1521 1523 1524 1529 1530 1535
1538 1541 1542 1547 1550 1553 1556
1559 1560 1565 1568 1571 1574 1577
1580 1583 1584 1585 1586 1587 1588
1589 1590 1591 1592 1593 1594 1595
1596 1597 1598 1599 1600 1601 1602
1603 1604 1605 1606 1607 1608 1793
1794 1796 1797 1802 1803 1808 1811
1814 1815 1820 1823 1826 1829 1832
1833 1838 1841 1844 1847 1850 1853
1856 1857 1858 1859 1860 1861 1862
1863 1864 1865 1866 1867 1868 1869
1870 1871 1872 1873 1874 1875 1876
1877 1878 1879 1880 1881 TERM

$ *** Group C1 *** Materials *****
MATERIAU
! PANT 0.0 LECT p0 p1 TERM
VMIS ISOT RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.09330593672421208
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608

LECT 1 PAS 1 4080 TERM
$----- Load Case considere : "Default" -----$
LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
BLOQ 1 LECT 4460 TERM
DEPLA 2 -1. FONCT 1 LECT noeuds_haut TERM

PINB
$---Gr: 17 CONTACT_INTER_001 NbElem: 22 ---$
SELF DMIN 0.1
LECT con01 TERM
$---Gr: 18 CONTACT_INTER_002 NbElem: 28 ---$
SELF DMIN 0.1
LECT con02 TERM
$---Gr: 19 CONTACT_INTER_003 NbElem: 28 ---$
SELF DMIN 0.1
LECT con03 TERM
$---Gr: 20 CONTACT_INTER_004 NbElem: 23 ---$
SELF DMIN 0.1
LECT con04 TERM
$---Gr: 21 CONTACT_INTER_005 NbElem: 44 ---$
SELF DMIN 0.1
LECT con05 TERM
$---Gr: 22 CONTACT_INTER_006 NbElem: 56 ---$
SELF DMIN 0.1
LECT con06 TERM
$---Gr: 23 CONTACT_INTER_007 NbElem: 56 ---$
SELF DMIN 0.1
LECT con07 TERM
$---Gr: 24 CONTACT_INTER_008 NbElem: 46 ---$
SELF DMIN 0.1
LECT con08 TERM
$---Gr: 25 CONTACT_INTER_009 NbElem: 44 ---$
SELF DMIN 0.1
LECT con09 TERM
$---Gr: 26 CONTACT_INTER_010 NbElem: 56 ---$
SELF DMIN 0.1
LECT con10 TERM
$---Gr: 27 CONTACT_INTER_011 NbElem: 56 ---$
SELF DMIN 0.1

```

```
LECT con11 TERM
$--Gr: 28 CONTACT_INTER_012 NbElem: 46 ---$
SELF DMIN 0.1
LECT con12 TERM
$--Gr: 29 CONTACT_EXTER_001 NbElem: 27 ---$
SELF DMIN 0.1
LECT con13 TERM
$--Gr: 30 CONTACT_EXTER_002 NbElem: 38 ---$
SELF DMIN 0.1
LECT con14 TERM
$--Gr: 31 CONTACT_EXTER_003 NbElem: 38 ---$
SELF DMIN 0.1
LECT con15 TERM
$--Gr: 32 CONTACT_EXTER_004 NbElem: 28 ---$
SELF DMIN 0.1
LECT con16 TERM
$--Gr: 33 CONTACT_TUBE_001 NbElem: 96 ---$
SELF DMIN 0.1
LECT con17 TERM
$--Gr: 34 CONTACT_TUBE_002 NbElem: 96 ---$
SELF DMIN 0.1
LECT con18 TERM
$--Gr: 35 CONTACT_TUBE_003 NbElem: 96 ---$
SELF DMIN 0.1
LECT con19 TERM
$--Gr: 36 CONTACT_TUBE_004 NbElem: 96 ---$
SELF DMIN 0.1
LECT con20 TERM
$--Gr: 37 CONTACT_TUBE_005 NbElem: 96 ---$
SELF DMIN 0.1
LECT con21 TERM
$--Gr: 38 CONTACT_TUBE_006 NbElem: 96 ---$
SELF DMIN 0.1
LECT con22 TERM
$--Gr: 39 CONTACT_TUBE_007 NbElem: 96 ---$
SELF DMIN 0.1
LECT con23 TERM
$--Gr: 40 CONTACT_TUBE_008 NbElem: 96 ---$
SELF DMIN 0.1
LECT con24 TERM
$--Gr: 41 CONTACT_TUBE_009 NbElem: 96 ---$
SELF DMIN 0.1
LECT con25 TERM
FONCT 1 TABLE 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
$----- Directives Generales -----$
ECRITURE
$
DEPL TFRE 0.1 !FREQ 1000
POINT LECT 4460 TERM
$
FICHIER SPLI ALICE TFRE 0.05 !TFREQ 50.0000
$
POIN LECT 1 PAS 1 4948 TERM
$
ELEM LECT 1 PAS 1 4080 TERM
$
Donnees Fichier ALICE Temps
$
FICHIER ALICE TEMPS TFREQ 0.05
!
POIN LECT TOUS TERM
!
ELEM LECT TOUS TERM
$
Donnees Fichier PARAVIEW
$
FICHIER FORMAT PVTK TFREQ 0.5
!
GROUP AUTO
!
VARI DEPL VITE FEXT ACCE CONT EPST ECRO PINB
$
Regions
$
"OPTION" de Calcul : methode Pas, amortissement
$
OPTION
PAS AUTO CSTA 0.5
STEP IO
PASMINI 1.00000E-12
LOG 1
PINS GRID DGRI
$
"OPTION" liee a la fragmentation
$
"OPTION" liee a l'amortissement
$
QUASI STATIQUE 50.0E-3 0.7
$
AMORT LINE 0.5
$
"OPTION" liee aux multi-domaines
$
Directives du Pas de Calcul
$
Tps_depart - Pas_fixe - Nbr_pas_max - Tps_Final
$
CALCUL TINI 0.00 DTMIN 1E-12 DTMAX 1E-04 TFIN 10.0 !NMAX 100
FIN
```

car101a.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car101.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
!
Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN
```

car101b.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car101.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
!
Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN
```

car101c.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car101.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
!
Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN
```

car101d.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car101.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
TRAC 4 44 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN
```

car102.epx

```
CAR102
ECHO
!CONV WIN
DPLA
$ *** Group B *** Geometry and mesh *****
GEOM
LIBR POIN 4948 CAR1 4080 TERM
!
LIBR POIN 4950 CAR1 4080 PMAT 2 TERM
$ *** Group B *** Nodes *****
1.50000E+01 5.95437E-30
. . . (skip for brevity)
```

```

14949          3444          3483          3484          3445
14950
$ *** Group C *** Geometrics complements *****
COMPLEMENT
! GROU 2 'p0' LECT 4081 TERM
! 'pl' LECT 4082 TERM
! EPAI 0.1 LECT p0 pl TERM
  NROU 3
    'noeuds_bas'
$ ---Gr: 42 NOEUDES_BAS NbNode: 79 ---$
LECT
  1      6      11      16      21      26      31
  36     41     46     51     56     57     70
  78     80     94     104    107    118    130
  134    142    156    161    166    167    168
  169    170    171    172    190    215    236
  242    257    262    263    286    294    296
  320    330    333    354    366    370    388
  402    407    412    413    414    415    416
  417    418    446    481    512    518    543
  548    577    585    616    626    655    667
  694    708    713    714    715    716    717
  718    719 TERM
    'noeuds_haut'
$ ---Gr: 43 NOEUDES_HAUT NbNode: 79 ---$
LECT
  4267   4268   4269   4270   4271   4272   4273
  4274   4275   4309   4314   4348   4353   4387
  4392   4421   4426   4455   4460   4493   4530
  4535   4548   4549   4550   4551   4552   4553
  4554   4555   4556   4576   4585   4590   4610
  4619   4624   4644   4653   4658   4678   4687
  4692   4707   4712   4731   4754   4781   4794
  4795   4796   4797   4798   4799   4800   4801
  4802   4812   4821   4826   4836   4845   4850
  4860   4869   4874   4884   4893   4898   4903
  4908   4913   4918   4923   4928   4933   4938
  4943   4948 TERM
$ ---Gr: 44 NOEUDES_SYM NbNode: 35 ---$
    'noeuds_sym'
LECT
  2      3      4      5      528    562    601
  640    679    725    767    805    839    1933
  1967   2006   2045   2084   2130   2172   2210
  2243   3333   3370   3411   3452   3493   3538
  3579   3616   3648   4456   4457   4458   4459
TERM
GROU 25
$ ---Gr: 17 CONTACT_INTER_001 NbElem: 22 ---$
    'con01'
LECT
  676    682    689    694    700    706    756
  757    758    759    760    761    762    763
  764    765    766    767    768    769    770
  771 TERM
$ ---Gr: 18 CONTACT_INTER_002 NbElem: 28 ---$
    'con02'
LECT
  949    955    962    967    973    979    1029
  1030   1031   1032   1033   1034   1035   1036
  1415   1421   1428   1433   1439   1445   1495
  1496   1497   1498   1499   1500   1501   1502
TERM
$ ---Gr: 19 CONTACT_INTER_003 NbElem: 28 ---$
    'con03'
LECT
  1182   1188   1195   1200   1206   1212   1262
  1263   1264   1265   1266   1267   1268   1269
  1935   1941   1948   1953   1959   1965   2015
  2016   2017   2018   2019   2020   2021   2022
TERM
$ ---Gr: 20 CONTACT_INTER_004 NbElem: 23 ---$
    'con04'
LECT
  1503   1662   1668   1675   1680   1686   1692
  1742   1743   1744   1745   1746   1747   1748
  1749   1750   1751   1752   1753   1754   1755
  1756   1757 TERM
$ ---Gr: 21 CONTACT_INTER_005 NbElem: 44 ---$
    'con05'
LECT
  675    679    681    686    688    692    693
  698    699    704    705    710    740    741
  742    743    744    745    746    747    748
  749    750    751    752    753    754    755
  772    773    774    775    776    777    778
  779    780    781    782    783    784    785
  786    787 TERM
$ ---Gr: 22 CONTACT_INTER_006 NbElem: 56 ---$
    'con06'
LECT
  948    952    954    959    961    965    966
  971    972    977    978    983    1013   1014
  1015   1016   1017   1018   1019   1020   1021
  1022   1023   1024   1025   1026   1027   1028
  1414   1418   1420   1425   1427   1431   1432
  1437   1438   1443   1444   1449   1479   1480
  1481   1482   1483   1484   1485   1486   1487
  1488   1489   1490   1491   1492   1493   1494
TERM
$ ---Gr: 23 CONTACT_INTER_007 NbElem: 56 ---$
    'con07'
LECT
  1181   1185   1187   1192   1194   1198   1199
  1204   1205   1210   1211   1216   1246   1247
  1248   1249   1250   1251   1252   1253   1254
  1255   1256   1257   1258   1259   1260   1261
  1934   1938   1940   1945   1947   1951   1952
  1957   1958   1963   1964   1969   1999   2000
  2001   2002   2003   2004   2005   2006   2007
  2008   2009   2010   2011   2012   2013   2014
TERM
$ ---Gr: 24 CONTACT_INTER_008 NbElem: 46 ---$
    'con08'
LECT
  1504   1505   1661   1665   1667   1672   1674
1678    1679    1684    1685    1690    1691    1696
1726    1727    1728    1729    1730    1731    1732
1733    1734    1735    1736    1737    1738    1739
1740    1741    1758    1759    1760    1761    1762
1763    1764    1765    1766    1767    1768    1769
1770    1771    1772    1773 TERM
$ ---Gr: 25 CONTACT_INTER_009 NbElem: 44 ---$
    'con09'
LECT
  678    680    684    685    690    691    696
  697    702    703    708    709    724    725
  726    727    728    729    730    731    732
  733    734    735    736    737    738    739
  788    789    790    791    792    793    794
  795    796    797    798    799    800    801
  802    803 TERM
$ ---Gr: 26 CONTACT_INTER_010 NbElem: 56 ---$
    'con10'
LECT
  951    953    957    958    963    964    969
  970    975    976    981    982    997    998
  999    1000   1001   1002   1003   1004   1005
  1006   1007   1008   1009   1010   1011   1012
  1417   1419   1423   1424   1429   1430   1435
  1436   1441   1442   1447   1448   1463   1464
  1465   1466   1467   1468   1469   1470   1471
  1472   1473   1474   1475   1476   1477   1478
TERM
$ ---Gr: 27 CONTACT_INTER_011 NbElem: 56 ---$
    'con11'
LECT
  1184    1186    1190    1191    1196    1197    1202
  1203    1208    1209    1214    1215    1230    1231
  1232    1233    1234    1235    1236    1237    1238
  1239    1240    1241    1242    1243    1244    1245
  1937    1939    1943    1944    1949    1950    1955
  1956    1961    1962    1967    1968    1983    1984
  1985    1986    1987    1988    1989    1990    1991
  1992    1993    1994    1995    1996    1997    1998
TERM
$ ---Gr: 28 CONTACT_INTER_012 NbElem: 46 ---$
    'con12'
LECT
  1506    1507    1664    1666    1670    1671    1676
  1677    1682    1683    1688    1689    1694    1695
  1710    1711    1712    1713    1714    1715    1716
  1717    1718    1719    1720    1721    1722    1723
  1724    1725    1774    1775    1776    1777    1778
  1779    1780    1781    1782    1783    1784    1785
  1786    1787    1788    1789 TERM
$ ---Gr: 29 CONTACT_EXTER_001 NbElem: 27 ---$
    'con13'
LECT
  523    524    525    526    527    528    529
  530    677    683    687    695    701    707
  711    712    713    714    715    716    717
  718    719    720    721    722    723 TERM
$ ---Gr: 30 CONTACT_EXTER_002 NbElem: 38 ---$
    'con14'
LECT
  950    956    960    968    974    980    984
  985    986    987    988    989    990    991
  992    993    994    995    996    1416   1422
  1426   1434   1440   1446   1450   1451   1452
  1453   1454   1455   1456   1457   1458   1459
  1460   1461   1462 TERM
$ ---Gr: 31 CONTACT_EXTER_003 NbElem: 38 ---$
    'con15'
LECT
  1183    1189    1193    1201    1207    1213    1217
  1218    1219    1220    1221    1222    1223    1224
  1225    1226    1227    1228    1229    1936   1942
  1946   1954   1960   1966   1970   1971   1972
  1973   1974   1975   1976   1977   1978   1979
  1980   1981   1982 TERM
$ ---Gr: 32 CONTACT_EXTER_004 NbElem: 28 ---$
    'con16'
LECT
  1508    1509    1510    1511    1512    1513    1514
  1515    1516    1663    1669    1673    1681    1687
  1693    1697    1698    1699    1700    1701    1702
  1703    1704    1705    1706    1707    1708    1709
TERM
$ ---Gr: 33 CONTACT_TUBE_001 NbElem: 96 ---$
    'con17'
LECT
  532    533    540    541    547    548    551
  554    559    560    563    566    569    572
  577    578    581    584    587    590    593
  596    649    650    651    652    653    654
  655    656    657    658    659    660    661
  662    663    664    665    666    667    668
  669    670    671    672    673    674    805
  806    813    814    820    821    824    827
  832    833    836    839    842    845    850
  851    854    857    860    863    866    869
  922    923    924    925    926    927    928
  929    930    931    932    933    934    935
  936    937    938    939    940    941    942
  943    944    945    946    947 TERM
$ ---Gr: 34 CONTACT_TUBE_002 NbElem: 96 ---$
    'con18'
LECT
  1038    1039    1046    1047    1053    1054    1057
  1060    1065    1066    1069    1072    1075    1078
  1083    1084    1087    1090    1093    1096    1099
  1102    1155    1156    1157    1158    1159    1160
  1161    1162    1163    1164    1165    1166    1167
  1168    1169    1170    1171    1172    1173    1174
  1175    1176    1177    1178    1179    1180    1271
  1272    1279    1280    1286    1287    1290    1293
  1298    1299    1302    1305    1308    1311    1316
  1317    1320    1323    1326    1329    1332    1335
  1388    1389    1390    1391    1392    1393    1394
  1395    1396    1397    1398    1399    1400    1401
  1402    1403    1404    1405    1406    1407    1408
  1409    1410    1411    1412    1413 TERM
$ ---Gr: 35 CONTACT_TUBE_003 NbElem: 96 ---$

```

```

'con19'
LECT
1518 1519 1526 1527 1533 1534 1537
1540 1545 1546 1549 1552 1555 1558
1563 1564 1567 1570 1573 1576 1579
1582 1635 1636 1637 1638 1639 1640
1641 1642 1643 1644 1645 1646 1647
1648 1649 1650 1651 1652 1653 1654
1655 1656 1657 1658 1659 1660 1661
1792 1799 1800 1806 1807 1810 1813
1818 1819 1822 1825 1828 1831 1836
1837 1840 1843 1846 1849 1852 1855
1908 1909 1910 1911 1912 1913 1914
1915 1916 1917 1918 1919 1920 1921
1922 1923 1924 1925 1926 1927 1928
1929 1930 1931 1932 1933 TERM
$---Gr: 36 CONTACT_TUBE_004 NbElem: 96 ---$
'con20'
LECT
531 536 539 542 545 546 550
553 557 558 562 565 568 571
575 576 580 583 586 589 592
595 623 624 625 626 627 628
629 630 631 632 633 634 635
636 637 638 639 640 641 642
643 644 645 646 647 648 649
809 812 815 818 819 823 826
830 831 835 838 841 844 848
849 853 856 859 862 865 868
896 897 898 899 900 901 902
903 904 905 906 907 908 909
910 911 912 913 914 915 916
917 918 919 920 921 TERM
$---Gr: 37 CONTACT_TUBE_005 NbElem: 96 ---$
'con21'
LECT
1037 1042 1045 1048 1051 1052 1056
1059 1063 1064 1068 1071 1074 1077
1081 1082 1086 1089 1092 1095 1098
1101 1129 1130 1131 1132 1133 1134
1135 1136 1137 1138 1139 1140 1141
1142 1143 1144 1145 1146 1147 1148
1149 1150 1151 1152 1153 1154 1270
1275 1278 1281 1284 1285 1289 1292
1296 1297 1301 1304 1307 1310 1314
1315 1319 1322 1325 1328 1331 1334
1362 1363 1364 1365 1366 1367 1368
1369 1370 1371 1372 1373 1374 1375
1376 1377 1378 1379 1380 1381 1382
1383 1384 1385 1386 1387 TERM
$---Gr: 38 CONTACT_TUBE_006 NbElem: 96 ---$
'con22'
LECT
1517 1522 1525 1528 1531 1532 1536
1539 1543 1544 1548 1551 1554 1557
1561 1562 1566 1569 1572 1575 1578
1581 1609 1610 1611 1612 1613 1614
1615 1616 1617 1618 1619 1620 1621
1622 1623 1624 1625 1626 1627 1628
1629 1630 1631 1632 1633 1634 1790
1795 1798 1801 1804 1805 1809 1812
1816 1817 1821 1824 1827 1830 1834
1835 1839 1842 1845 1848 1851 1854
1882 1883 1884 1885 1886 1887 1888
1889 1890 1891 1892 1893 1894 1895
1896 1897 1898 1899 1900 1901 1902
1903 1904 1905 1906 1907 TERM
$---Gr: 39 CONTACT_TUBE_007 NbElem: 96 ---$
'con23'
LECT
534 535 537 538 543 544 549
552 555 556 561 564 567 570
573 574 579 582 585 588 591
594 597 598 599 600 601 602
603 604 605 606 607 608 609
610 611 612 613 614 615 616
617 618 619 620 621 622 807
808 810 811 816 817 822 825
828 829 834 837 840 843 846
847 852 855 858 861 864 867
870 871 872 873 874 875 876
877 878 879 880 881 882 883
884 885 886 887 888 889 890
891 892 893 894 895 TERM
$---Gr: 40 CONTACT_TUBE_008 NbElem: 96 ---$
'con24'
LECT
1040 1041 1043 1044 1049 1050 1055
1058 1061 1062 1067 1070 1073 1076
1079 1080 1085 1088 1091 1094 1097
1100 1103 1104 1105 1106 1107 1108
1109 1110 1111 1112 1113 1114 1115
1116 1117 1118 1119 1120 1121 1122
1123 1124 1125 1126 1127 1128 1273
1274 1276 1277 1282 1283 1288 1291
1294 1295 1300 1303 1306 1309 1312
1313 1318 1321 1324 1327 1330 1333
1336 1337 1338 1339 1340 1341 1342
1343 1344 1345 1346 1347 1348 1349
1350 1351 1352 1353 1354 1355 1356
1357 1358 1359 1360 1361 TERM
$---Gr: 41 CONTACT_TUBE_009 NbElem: 96 ---$
'con25'
LECT
1520 1521 1523 1524 1529 1530 1535
1538 1541 1542 1547 1550 1553 1556
1559 1560 1565 1568 1571 1574 1577
1580 1583 1584 1585 1586 1587 1588
1589 1590 1591 1592 1593 1594 1595
1596 1597 1598 1599 1600 1601 1602
1603 1604 1605 1606 1607 1608 1793
1794 1796 1797 1802 1803 1808 1811
1814 1815 1820 1823 1826 1829 1832
1833 1838 1841 1844 1847 1850 1853
1856 1857 1858 1859 1860 1861 1862
1863 1864 1865 1866 1867 1868 1869
1870 1871 1872 1873 1874 1875 1876
1877 1878 1879 1880 1881 TERM
$ *** Group C1 *** Materials *****
MATERIAU
!
FANT 0.0 LECT p0 p1 TERM
VMIS ISOT RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.8078444043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.09330593672421208
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT 1 PAS 1 4080 TERM
$----- Load Case considere : "Default" -----$
LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
BLOQ 1 LECT 4460 TERM
DEPLA 2 -1. FONCT 1 LECT noeuds_haut TERM
PINB
$---Gr: 17 CONTACT_INTER_001 NbElem: 22 ---$
SELF DMIN 0.1
LECT con01 TERM
$---Gr: 18 CONTACT_INTER_002 NbElem: 28 ---$
SELF DMIN 0.1
LECT con02 TERM
$---Gr: 19 CONTACT_INTER_003 NbElem: 28 ---$
SELF DMIN 0.1
LECT con03 TERM
$---Gr: 20 CONTACT_INTER_004 NbElem: 23 ---$
SELF DMIN 0.1
LECT con04 TERM
$---Gr: 21 CONTACT_INTER_005 NbElem: 44 ---$
SELF DMIN 0.1
LECT con05 TERM
$---Gr: 22 CONTACT_INTER_006 NbElem: 56 ---$
SELF DMIN 0.1
LECT con06 TERM
$---Gr: 23 CONTACT_INTER_007 NbElem: 56 ---$
SELF DMIN 0.1
LECT con07 TERM
$---Gr: 24 CONTACT_INTER_008 NbElem: 46 ---$
SELF DMIN 0.1
LECT con08 TERM
$---Gr: 25 CONTACT_INTER_009 NbElem: 44 ---$
SELF DMIN 0.1
LECT con09 TERM
$---Gr: 26 CONTACT_INTER_010 NbElem: 56 ---$
SELF DMIN 0.1
LECT con10 TERM
$---Gr: 27 CONTACT_INTER_011 NbElem: 56 ---$
SELF DMIN 0.1
LECT con11 TERM
$---Gr: 28 CONTACT_INTER_012 NbElem: 46 ---$
SELF DMIN 0.1
LECT con12 TERM
$---Gr: 29 CONTACT_EXTER_001 NbElem: 27 ---$
SELF DMIN 0.1
LECT con13 TERM
$---Gr: 30 CONTACT_EXTER_002 NbElem: 38 ---$
SELF DMIN 0.1
LECT con14 TERM
$---Gr: 31 CONTACT_EXTER_003 NbElem: 38 ---$
SELF DMIN 0.1
LECT con15 TERM
$---Gr: 32 CONTACT_EXTER_004 NbElem: 28 ---$
SELF DMIN 0.1
LECT con16 TERM
$---Gr: 33 CONTACT_TUBE_001 NbElem: 96 ---$
SELF DMIN 0.1
LECT con17 TERM
$---Gr: 34 CONTACT_TUBE_002 NbElem: 96 ---$
SELF DMIN 0.1
LECT con18 TERM
$---Gr: 35 CONTACT_TUBE_003 NbElem: 96 ---$
SELF DMIN 0.1
LECT con19 TERM
$---Gr: 36 CONTACT_TUBE_004 NbElem: 96 ---$
SELF DMIN 0.1
LECT con20 TERM
$---Gr: 37 CONTACT_TUBE_005 NbElem: 96 ---$
SELF DMIN 0.1
LECT con21 TERM
$---Gr: 38 CONTACT_TUBE_006 NbElem: 96 ---$
SELF DMIN 0.1

```

```
LECT con22 TERM
$--Gr: 39 CONTACT_TUBE_007 NbElem: 96 ---$
SELF DMIN 0.1
LECT con23 TERM
$--Gr: 40 CONTACT_TUBE_008 NbElem: 96 ---$
SELF DMIN 0.1
LECT con24 TERM
$--Gr: 41 CONTACT_TUBE_009 NbElem: 96 ---$
SELF DMIN 0.1
LECT con25 TERM
FONCT 1 TABLE 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
$----- Directives Generales -----$
ECRITURE
$ DEPL TFRE 0.1 !FREQ 1000
POINT LECT 4460 TERM
$ Donnees Fichier ALICE
FICHIER SPLI ALICE TFRE 0.05 !TFREQ 50.0000
$ POIN LECT 1 PAS 1 4948 TERM
$ ELEM LECT 1 PAS 1 4080 TERM
$ Donnees Fichier ALICE Temps
FICHIER ALICE TEMPS TFREQ 0.05
$ POIN LECT TOUS TERM
$ ELEM LECT TOUS TERM
$ Donnees Fichier PARAVIEW
FICHIER FORMAT PVTK TFREQ 0.5
$ GROUP AUTO
$ VARI DEPL VITE FEXT ACCE CONT EPST ECRO PINB
$ Regions
$ "OPTION" de Calcul : methode Pas, amortissement
OPTION
PAS AUTO CSTA 0.5
STEP IO
PASMINI 1.0000E-12
LOG 1
PINS GRID DGRI
$ "OPTION" liee a la fragmentation
$ "OPTION" liee a l'amortissement
$ QUASI STATIQUE 50.0E-3 0.7
$ AMORT LINE 0.5
$ "OPTION" liee aux multi-domaines
$ Directives du Pas de Calcul
$ Tps_depart - Pas_fixe - Nbr_pas_max - Tps_Final
$ CALCUL TINI 0.00 DTMIN 1E-12 DTMAX 1E-04 TFIN 10.0 NMAX 90000000
FIN
```

car102a.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car102.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----$
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
! VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
! RIGH 1.00000E+00 0.00000E+00 0.00000E+00
! UP 0.00000E+00 1.00000E+00 0.00000E+00
! FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----$
FIN
```

car102b.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car102.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----$
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
! VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
! RIGH 1.00000E+00 0.00000E+00 0.00000E+00
! UP 0.00000E+00 1.00000E+00 0.00000E+00
! FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
```

```
ENDPLAY
*-----$
FIN
```

car102c.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car102.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----$
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
! VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
! RIGH 1.00000E+00 0.00000E+00 0.00000E+00
! UP 0.00000E+00 1.00000E+00 0.00000E+00
! FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----$
FIN
```

car102d.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car102.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyh' FICH 'car401d.pun' RENA 'fyh_401'
TRAC 4 44 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN
```

car401.epx

```
CAR401
ECHO
!CONV WIN
DPLA
$ *** Group B *** Geometry and mesh *****
GEOM
LIBR POIN 4948 CAR4 4080 TERM
! LIBR POIN 4950 CAR4 4080 PMAT 2 TERM
$ *** Group B *** Nodes *****
1.50000E+01 5.95437E-30
. . . (skip for brevity)
3444 3483 3484 3445
14949
14950
$ *** Group C *** Geometrics complements *****
COMPLEMENT
! GROU 2 'p0' LECT 4081 TERM
! 'pl' LECT 4082 TERM
! EPAI 0.1 LECT p0 pl TERM
NGROU 3
'noeuds_bas'
$--Gr: 42 NOEUDES_BAS NbNode: 79 ---$
LECT
1 6 11 16 21 26 31
36 41 46 51 56 57 70
78 80 94 104 107 118 130
134 142 156 161 166 167 168
169 170 171 172 190 215 236
242 257 262 263 286 294 296
320 330 333 354 366 370 388
402 407 412 413 414 415 416
417 418 446 481 512 518 543
548 577 585 616 626 655 667
694 708 713 714 715 716 717
718 719 TERM
'noeuds_haut'
$--Gr: 43 NOEUDES_HAUT NbNode: 79 ---$
LECT
4267 4268 4269 4270 4271 4272 4273
4274 4275 4309 4314 4348 4353 4387
4392 4421 4426 4455 4460 4493 4530
4535 4548 4549 4550 4551 4552 4553
4554 4555 4556 4576 4585 4590 4610
4619 4624 4644 4653 4658 4678 4687
4692 4707 4712 4731 4754 4781 4794
```



```

LECT
1037 1042 1045 1048 1051 1052 1056
1059 1063 1064 1068 1071 1074 1077
1081 1082 1086 1089 1092 1095 1098
1101 1129 1130 1131 1132 1133 1134
1135 1136 1137 1138 1139 1140 1141
1142 1143 1144 1145 1146 1147 1148
1149 1150 1151 1152 1153 1154 1270
1275 1278 1281 1284 1285 1289 1292
1296 1297 1301 1304 1307 1310 1314
1315 1319 1322 1325 1328 1331 1334
1362 1363 1364 1365 1366 1367 1368
1369 1370 1371 1372 1373 1374 1375
1376 1377 1378 1379 1380 1381 1382
1383 1384 1385 1386 1387 TERM
$---Gr: 38 CONTACT_TUBE_006 NbElem: 96 ---$
'con22'
LECT
1517 1522 1525 1528 1531 1532 1536
1539 1543 1544 1548 1551 1554 1557
1561 1562 1566 1569 1572 1575 1578
1581 1609 1610 1611 1612 1613 1614
1615 1616 1617 1618 1619 1620 1621
1622 1623 1624 1625 1626 1627 1628
1629 1630 1631 1632 1633 1634 1790
1795 1798 1801 1804 1805 1809 1812
1816 1817 1821 1824 1827 1830 1834
1835 1839 1842 1845 1848 1851 1854
1882 1883 1884 1885 1886 1887 1888
1889 1890 1891 1892 1893 1894 1895
1896 1897 1898 1899 1900 1901 1902
1903 1904 1905 1906 1907 TERM
$---Gr: 39 CONTACT_TUBE_007 NbElem: 96 ---$
'con23'
LECT
534 535 537 538 543 544 549
552 555 556 561 564 567 570
573 574 579 582 585 588 591
594 597 598 599 600 601 602
603 604 605 606 607 608 609
610 611 612 613 614 615 616
617 618 619 620 621 622 807
808 810 811 816 817 822 825
828 829 834 837 840 843 846
847 852 855 858 861 864 867
870 871 872 873 874 875 876
877 878 879 880 881 882 883
884 885 886 887 888 889 890
891 892 893 894 895 TERM
$---Gr: 40 CONTACT_TUBE_008 NbElem: 96 ---$
'con24'
LECT
1040 1041 1043 1044 1049 1050 1055
1058 1061 1062 1067 1070 1073 1076
1079 1080 1085 1088 1091 1094 1097
1100 1103 1104 1105 1106 1107 1108
1109 1110 1111 1112 1113 1114 1115
1116 1117 1118 1119 1120 1121 1122
1123 1124 1125 1126 1127 1128 1273
1274 1276 1277 1282 1283 1288 1291
1294 1295 1300 1303 1306 1309 1312
1313 1318 1321 1324 1327 1330 1333
1336 1337 1338 1339 1340 1341 1342
1343 1344 1345 1346 1347 1348 1349
1350 1351 1352 1353 1354 1355 1356
1357 1358 1359 1360 1361 TERM
$---Gr: 41 CONTACT_TUBE_009 NbElem: 96 ---$
'con25'
LECT
1520 1521 1523 1524 1529 1530 1535
1538 1541 1542 1547 1550 1553 1556
1559 1560 1565 1568 1571 1574 1577
1580 1583 1584 1585 1586 1587 1588
1589 1590 1591 1592 1593 1594 1595
1596 1597 1598 1599 1600 1601 1602
1603 1604 1605 1606 1607 1608 1793
1794 1796 1797 1802 1803 1808 1811
1814 1815 1820 1823 1826 1829 1832
1833 1838 1841 1844 1847 1850 1853
1856 1857 1858 1859 1860 1861 1862
1863 1864 1865 1866 1867 1868 1869
1870 1871 1872 1873 1874 1875 1876
1877 1878 1879 1880 1881 TERM
$ *** Group Cl *** Materials *****
MATERIAU
! FANT 0.0 LECT p0 p1 TERM
VMIS ISOT RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075559371
358.247494301277 0.0118129933922129
390.499112131117 0.01697621000816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022

```

```

959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
$-----LECT----- 1 PAS 1 4080 TERM
$-----Load Case considere : "Default" -----$
LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
BLOQ 1 LECT 4460 TERM
DEPLA 2 -1. FONCT 1 LECT noeuds_haut TERM
PINB
$---Gr: 17 CONTACT_INTER_001 NbElem: 22 ---$
SELF DMIN 0.1
LECT con01 TERM
$---Gr: 18 CONTACT_INTER_002 NbElem: 28 ---$
SELF DMIN 0.1
LECT con02 TERM
$---Gr: 19 CONTACT_INTER_003 NbElem: 28 ---$
SELF DMIN 0.1
LECT con03 TERM
$---Gr: 20 CONTACT_INTER_004 NbElem: 23 ---$
SELF DMIN 0.1
LECT con04 TERM
$---Gr: 21 CONTACT_INTER_005 NbElem: 44 ---$
SELF DMIN 0.1
LECT con05 TERM
$---Gr: 22 CONTACT_INTER_006 NbElem: 56 ---$
SELF DMIN 0.1
LECT con06 TERM
$---Gr: 23 CONTACT_INTER_007 NbElem: 56 ---$
SELF DMIN 0.1
LECT con07 TERM
$---Gr: 24 CONTACT_INTER_008 NbElem: 46 ---$
SELF DMIN 0.1
LECT con08 TERM
$---Gr: 25 CONTACT_INTER_009 NbElem: 44 ---$
SELF DMIN 0.1
LECT con09 TERM
$---Gr: 26 CONTACT_INTER_010 NbElem: 56 ---$
SELF DMIN 0.1
LECT con10 TERM
$---Gr: 27 CONTACT_INTER_011 NbElem: 56 ---$
SELF DMIN 0.1
LECT con11 TERM
$---Gr: 28 CONTACT_INTER_012 NbElem: 46 ---$
SELF DMIN 0.1
LECT con12 TERM
$---Gr: 29 CONTACT_EXTER_001 NbElem: 27 ---$
SELF DMIN 0.1
LECT con13 TERM
$---Gr: 30 CONTACT_EXTER_002 NbElem: 38 ---$
SELF DMIN 0.1
LECT con14 TERM
$---Gr: 31 CONTACT_EXTER_003 NbElem: 38 ---$
SELF DMIN 0.1
LECT con15 TERM
$---Gr: 32 CONTACT_EXTER_004 NbElem: 28 ---$
SELF DMIN 0.1
LECT con16 TERM
$---Gr: 33 CONTACT_TUBE_001 NbElem: 96 ---$
SELF DMIN 0.1
LECT con17 TERM
$---Gr: 34 CONTACT_TUBE_002 NbElem: 96 ---$
SELF DMIN 0.1
LECT con18 TERM
$---Gr: 35 CONTACT_TUBE_003 NbElem: 96 ---$
SELF DMIN 0.1
LECT con19 TERM
$---Gr: 36 CONTACT_TUBE_004 NbElem: 96 ---$
SELF DMIN 0.1
LECT con20 TERM
$---Gr: 37 CONTACT_TUBE_005 NbElem: 96 ---$
SELF DMIN 0.1
LECT con21 TERM
$---Gr: 38 CONTACT_TUBE_006 NbElem: 96 ---$
SELF DMIN 0.1
LECT con22 TERM
$---Gr: 39 CONTACT_TUBE_007 NbElem: 96 ---$
SELF DMIN 0.1
LECT con23 TERM
$---Gr: 40 CONTACT_TUBE_008 NbElem: 96 ---$
SELF DMIN 0.1
LECT con24 TERM
$---Gr: 41 CONTACT_TUBE_009 NbElem: 96 ---$
SELF DMIN 0.1
LECT con25 TERM
FONCT 1 TABLE 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
$-----Directives Generales -----$
ECRITURE
$ DEPL TFRE 0.1 !FREQ 1000 impressions LISTING $
POINT LECT 4460 TERM Donnees Fichier ALICE $
$ FICHIER SPLI ALICE TFRE 0.05 !TFREQ 50.0000 $
$ POIN LECT 1 PAS 1 4948 TERM $
$ ELEM LECT 1 PAS 1 4080 TERM $
$ Donnees Fichier ALICE Temps $
! FICHIER ALICE TEMPS TFREQ 0.05
! POIN LECT TOUS TERM
! ELEM LECT TOUS TERM
$ Donnees Fichier PARAVIEW $
! FICHIER FORMAT PVTK TFREQ 0.5
! GROUP AUTO
! VARI DEPL VITE FEXT ACCE CONT EPST ECRO PINB
$ Regions
$ "OPTION" de Calcul : methode Pas, amortissement $
OPTION
PAS AUTO
STEP IO
PASMINI 1.00000E-12
LOG 1

```

```

PINS GRID DGRI
$ "OPTION" liee a la fragmentation $
$ "OPTION" liee a l'amortissement $
$ QUASI STATIQUE 50.0E-3 0.7
$ AMORT LINE 0.5
$ "OPTION" liee aux multi-domaines $
$ Directives du Pas de Calcul $
$ Tps depart - Pas_fixe - Nbr_pas_max - Tps_Final $
CALCUL TINI 0.00 DTMIN 1E-12 DTMAX 1E-04 TFIN 10.0 !NMAX 100
FIN

```

```

FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----
PIN

```

car401a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car401.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----
FIN

```

car401d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car401.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
FIN

```

cara01.epx

```

CARA01
ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q42G sur4 TERM
COMP EPAI 1. LECT sur4 TERM
NGRO 3
'noeuds_sym' LECT nodlag TERM COND X GT 14.95
'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM
AUTO AUTR
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39

```

car401b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car401.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----
FIN

```

```

222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.001882184326777593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005645
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur4 TERM

```

car401c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'car401.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HPRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPFE 10 COMP -1 REND

```

```

LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
BLOQ 1 LECT 4460 TERM
DEPL 2 -1. FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elepin TERM
FONCT 1 TABLE 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF CNOR
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
PIN

```

cara01a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara01.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----

```



```

PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

cara01b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara01.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  LINE HEOU SPRE
  ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
  TEXT ISCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

cara01c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara01.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  LINE HEOU SPRE
  FACE HFRO
  PINB CDES
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

cara01d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara01.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM

```

```

COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

```

cara01e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara01.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN

```

cara02.epx

```

CARA02
ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q42G sur4 TERM
COMP EPAI 1. LECT sur4 TERM
NGRO 3
  'noeuds_sym' LECT nodlag TERM COND X GT 14.95
  'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
  'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM
AUTO AUTR
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
  222.35 0.00112525303643725
  228.192645571222 0.00117982108082602
  230.758344471793 0.001217805387003
  234.450726613396 0.00128649153144431
  239.764555869277 0.00141338337990525
  243.897432663364 0.00153429874829638
  247.411863292444 0.00165208432840306
  250.528021456793 0.00176785435959915
  253.359622970924 0.00188218432677593
  258.417356319849 0.00210778014331907
  262.901922592959 0.00233047531676599
  272.525831528572 0.00287917930935512
  280.709612952488 0.00342059520724944
  306.337249091751 0.00555028972212425
  326.269365384357 0.00765116075599371
  358.247494301277 0.0118129933922129
  390.499112131117 0.0169762100816352
  417.924578503771 0.0221150029276507
  464.338948360747 0.0323498934633641
  503.807844043327 0.0425496348382759
  538.803931461142 0.0527267405438317
  570.604298738599 0.0628876735766123
  599.971697212392 0.0730362940142328
  627.405291846074 0.0831751279951724
  653.253096704044 0.0933059367242108
  677.76931865327 0.103430006673347
  734.395540393597 0.128716576621425
  785.850853879881 0.153976978005465
  833.369446403083 0.179217456712566
  877.759003278812 0.204442100219022
  959.251671749752 0.254854512508855
  1033.30271513801 0.305229264752723
  1165.57077256009 0.405898637512956
  1282.84956691385 0.506492153678714
  1389.41887249881 0.607031472026816
  1579.77020835558 0.807994788503824
  1748.85 1.00884893724696
  2418.75489508018 2.0122406624245
  5336.94734929116 10.0270088428608
  LECT sur4 TERM
LINK COUP SPLT NONE
  BLOQ 12 LECT noeuds_bas TERM
  BLOQ 1 LECT noeuds_sym TERM
  DEPL 2 -1. FONC 1 LECT noeuds_haut TERM
  PINB SELF DMIN 0.1 LECT elepin TERM
FONCT 1 TABLE 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
  FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
  'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
  PASM 1.0E-12
  LOG 1
  PINS GRID DGRI EQVF CNOR
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

```

cara02a.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
FIN

cara02b.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SPRE
ISO FILL FIEL ECR0 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
FIN

cara02c.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SPRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KPRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
FIN

cara02d.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara02.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

cara02e.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara02.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fy' FICH 'cara01e.pun' RENA 'fy_01'
RCOU 24 'fy' FICH 'cara02e.pun' RENA 'fy_02'
TRAC 14 24 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN

cara03.epx

CARA03
ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q4IN sur4 TERM
COMP EPAI 1. LECT sur4 TERM
NGRO 3
'noeuds_sym' LECT nodlag TERM COND X GT 14.95
'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM
AUTO AUTR
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348832759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.85085379881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.85 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur4 TERM
LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPL 2 -1. FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elepin TERM

```

FONCT 1 TABLE 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF CNOR
CALC TIMI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

```

```

TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDEPLAY
*-----
PIN

```

cara03a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDEPLAY
*-----
FIN

```

cara03d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyb' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
PIN

```

cara03e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fy' FICH 'cara01e.pun' RENA 'fy_01'
RCOU 24 'fy' FICH 'cara02e.pun' RENA 'fy_02'
RCOU 34 'fy' FICH 'cara03e.pun' RENA 'fy_03'
TRAC 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
PIN

```

cara03b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HBOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDEPLAY
*-----
FIN

```

cara04.epx

```

CARA04
ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q42G sur4 TERM
COMP EPAI 1. LECT sur4 TERM
NGRO 3
'noeuds_sym' LECT nodlag TERM COND X GT 14.95
'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM
AUTO AUTR
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764558692777 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.005502897212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.07330362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714

```

cara03c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HBOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1

```

```

1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur4 TERM
LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
VITE 2 -10 FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elepin TERM
FONC 1 TABLE 2 0 1 100 1
INIT VITE 2 -10 LECT noeuds_haut TERM
ECRI DEPL TPRE 0.01 POIN LECT 4460 TERM
FICH SPLI ALIC TPRE 0.005
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
LOG 1
PINS GRID DGRI EQVF CNOR
CALC TINI 0.0 TFIN 1.0
FIN

```

```

!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SPRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara04a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara04.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara04d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara04.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

```

cara04e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara04.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fy' FICH 'cara01e.pun' RENA 'fy_01'
RCOU 24 'fy' FICH 'cara02e.pun' RENA 'fy_02'
RCOU 34 'fy' FICH 'cara03e.pun' RENA 'fy_03'
RCOU 44 'fy' FICH 'cara04e.pun' RENA 'fy_04'
TRAC 14 24 34 44 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN

```

cara04b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara04.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SPRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara05.epx

```

CARA05
ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q42G sur4 TERM
COMP EPAI 1. LECT sur4 TERM
NGRO 3
'noeuds_sym' LECT nodlag TERM COND X GT 14.95
'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM
AUTO AUTR
MATE VM23 RO 0.825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123

```

cara04c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara04.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00

```

```

599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur4 TERM
LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
VITE 2 -1 FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elepin TERM
FONC 1 TABLE 2 0 1 100 1
INIT VITE 2 -1 LECT noeuds_haut TERM
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
LOG 1
PINS GRID DGRI EQVF CNOR
CALC TINI 0.0 TFIN 10.0
FIN

```

```

OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 201 FPS 25 KFRE 10 COMP -1 REND
FRQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

cara05a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara05.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 201 FPS 25 KFRE 10 COMP -1 REND
FRQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

cara05d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara05.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyb' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

```

cara05b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara05.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 201 FPS 25 KFRE 10 COMP -1 REND
FRQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

cara05e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara05.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyb' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fy' FICH 'cara01e.pun' RENA 'fy_01'
RCOU 24 'fy' FICH 'cara02e.pun' RENA 'fy_02'
RCOU 34 'fy' FICH 'cara03e.pun' RENA 'fy_03'
RCOU 44 'fy' FICH 'cara04e.pun' RENA 'fy_04'
RCOU 54 'fy' FICH 'cara05e.pun' RENA 'fy_05'
TRAC 14 24 34 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ ROSE
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN

```

cara06.epx

```

CARA06
ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q42N sur4 TERM
COMP EPAI 1. LECT sur4 TERM
NGRO 3
'noeuds_sym' LECT nodlag TERM COND X GT 14.95
'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM
AUTO AUTR
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.76455869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593

```

cara05c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara05.ali' GARD PSCR

```

```

258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608

LECT sur4 TERM
LINK COUP SPLT NONE
  BLOQ 12 LECT noeuds_bas TERM
  BLOQ 1 LECT noeuds_sym TERM
  VITE 2 -10 FONC 1 LECT noeuds_haut TERM
  PINB SELF DMIN 0.1 LECT elepin TERM
FONC 1 TABLE 2 0 1 100 1
INIT VITE 2 -10 LECT noeuds_haut TERM
ECRI DEPL TFRE 0.01 POIN LECT 4460 TERM
  FICH SPLI ALIC TFRE 0.005
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
  'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
  LOG 1
  PINS GRID DGRI EQVF CNOR
CALC TINI 0.0 TFIN 1.0
FIN

```

cara06a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara06.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  COLO PAPE
  SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara06b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara06.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  LINE HEOU SPRE
  ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
  TEXT ISCA
  COLO PAPE
  SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND

```

```

GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara06c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara06.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  !LINE HEOU SPRE
  FACE HFRO
  PINB CDES
  COLO PAPE
  SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara06d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara06.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

```

cara06e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara06.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 24 'fy' FICH 'cara02e.pun' RENA 'fy_02'
RCOU 44 'fy' FICH 'cara04e.pun' RENA 'fy_04'
RCOU 54 'fy' FICH 'cara05e.pun' RENA 'fy_05'
RCOU 64 'fy' FICH 'cara06e.pun' RENA 'fy_06'
TRAC 24 44 54 64 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN

```

cara07.epx

```

CARA07
ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q42 sur4 TERM
COMP EPAI 1. LECT sur4 TERM
  NGRO 3
  'noeuds_sym' LECT nodlag TERM COND X GT 14.95
  'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
  'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
  COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM

```

```

AUTO AUTR
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348832759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608

LECT sur4 TERM
LINK COUP SPLT NONE
BLOQ 12 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
VITE 2 -10 FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elepin TERM
FONC 1 TABLE 2 0 1 100 1
INIT VITE 2 -10 LECT noeuds_haut TERM
ECRI DEPL TPFE 0.01 POIN LECT 4460 TERM
FICH SPLI ALIC TPFE 0.005
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
LOG 1
PINS GRID DGRI EQVF CNOR
CALC TIMI 0.0 TFIN 1.0
FIN

```

cara07a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara07.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara07b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara07.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01

```

```

!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara07c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara07.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
FIN

```

cara07d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara07.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy 4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

```

cara07e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara07.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 24 'fy' FICH 'cara02e.pun' RENA 'fy_02'
RCOU 44 'fy' FICH 'cara04e.pun' RENA 'fy_04'
RCOU 54 'fy' FICH 'cara05e.pun' RENA 'fy_05'
RCOU 64 'fy' FICH 'cara06e.pun' RENA 'fy_06'
RCOU 74 'fy' FICH 'cara07e.pun' RENA 'fy_07'
TRAC 24 44 54 64 74 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ ROSE
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN

```

cara08.epx

CARA08

```

ECHO
!CONV WIN
CAST mesh
ALE DPLA
DIME NALE 1 NBLE 3180 TERM
GEOM Q41 sur4 TERM
COMP EPAI 1. LECT sur4 TERM
  NGRO 3
  'noeuds_sym' LECT nodlag TERM COND X GT 14.95
  'noeuds_haut' LECT nodlag TERM COND Y GT 16.95
  'noeuds_bas' LECT nodlag TERM COND Y LT 0.05
  COUL VERT LECT sur4 TERM
GRIL LAGR LECT nodlag TERM
  AUTO AUTR
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
  TRAC 39
    222.35 0.00112525303643725
    228.192645571222 0.00117982108082602
    230.758344471793 0.001217805387003
    234.450726613396 0.00128649153144431
    239.764555869277 0.00141338337990525
    243.897432663364 0.00153429874829638
    247.411863292444 0.00165208432840306
    250.528021456793 0.00176785435959915
    253.359622970924 0.00188218432677593
    258.417356319849 0.00210778014331907
    262.901922592959 0.00233047531676599
    272.525831528572 0.00287917930935512
    280.709612952488 0.00342059520724944
    306.337249091751 0.0055502897212425
    326.269365384357 0.00765116075599371
    358.247494301277 0.0118129933922129
    390.499112131117 0.0169762100816352
    417.924578503771 0.0221150029276507
    464.338948360747 0.0323498934633641
    503.807844043327 0.0425496348382759
    538.803931461142 0.0527267405438317
    570.604298738599 0.0628876735766123
    599.971697212392 0.0730362940142328
    627.405291846074 0.0831751279951724
    653.253096704044 0.0933059376242108
    677.76931865327 0.10343000673347
    734.395540393597 0.128716576621425
    785.850853879881 0.153976978005465
    833.369446403083 0.179217456712566
    877.759003278812 0.204442100219022
    959.251671749752 0.254854512508855
    1033.30271513801 0.305229264752723
    1165.57077256009 0.405898637512956
    1282.84956691385 0.506492153678714
    1389.41887249881 0.607031472026816
    1579.77020835558 0.807994788503824
    1748.55 1.00884893724696
    2418.75489508018 2.012240624245
    5336.94734929116 10.0270088428608
  LECT sur4 TERM
LINK COUP SPLT NONE
  BLOQ 12 LECT noeuds_bas TERM
  BLOQ 1 LECT noeuds_sym TERM
  VITE 2 -10 FONC 1 LECT noeuds_haut TERM
  PINB SELF DMIN 0.1 LECT elepin TERM
FONC 1 TABLE 2 0 1 100 1
INIT VITE 2 -10 LECT noeuds_haut TERM
ECRI DEPL TPFE 0.01 POIN LECT 4460 TERM
  FICH SPLI ALIC TPFE 0.005
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
  'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
  LOG 1
  PINS GRID DGRI EQVF CNOR
CALC TINI 0.0 TFIN 1.0
FIN

```

cara08a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara08.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  COLO PAPE
  SLER CAM1 1 NFRA 1
  TRAC OFFS FICH AVI NOCL NFTO 201 FPS 25 KPRE 10 COMP -1 REND
  FREQ 1
  GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
  GO
  TRAC OFFS FICH AVI CONT REND
  ENDFPLAY
*****
FIN

```

cara08b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara08.ali' GARD PSCR
OPTI PRIN

```

```

SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  LINE HEOU SFRE
  ISO FILL FIEL ECR0 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
  TEXT ISCA
  COLO PAPE
  SLER CAM1 1 NFRA 1
  TRAC OFFS FICH AVI NOCL NFTO 201 FPS 25 KPRE 10 COMP -1 REND
  FREQ 1
  GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
  GO
  TRAC OFFS FICH AVI CONT REND
  ENDFPLAY
*****
FIN

```

cara08c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara08.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*****
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
  LINE HEOU SFRE
  FACE HFRO
  PINB CDES
  COLO PAPE
  SLER CAM1 1 NFRA 1
  TRAC OFFS FICH AVI NOCL NFTO 201 FPS 25 KPRE 10 COMP -1 REND
  FREQ 1
  GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
  GO
  TRAC OFFS FICH AVI CONT REND
  ENDFPLAY
*****
FIN

```

cara08d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara08.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyb' FICH 'car401d.pun' RENA 'fyb_401'
RCOU 54 'fyb' FICH 'car102d.pun' RENA 'fyb_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

```

cara08e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'cara08.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dyh' DEPL COMP 2 NOEU LECT 350 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fy' MULC 3 -1.0
COUR 5 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
LIST 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fy' FICH 'cara01e.pun' RENA 'fy_01'
RCOU 24 'fy' FICH 'cara02e.pun' RENA 'fy_02'
RCOU 34 'fy' FICH 'cara03e.pun' RENA 'fy_03'
RCOU 44 'fy' FICH 'cara08e.pun' RENA 'fy_04'

```


TRAC 14 24 34 44 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 4 5 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN

carm01.epx

CARM01
ECHO
!CONV WIN
CAST MESH
DPLA
GEOM CAR1 sur41 CAR4 sur42 TERM
COMP NGRO 3
'noeuds_sym' LECT elpeau4 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau4 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau4 TERM COND Y LT 0.05
COUL VERT LECT sur41 TERM
ROUG LECT sur42 TERM
MATE VMIS ISOT RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.002010778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.011812993922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876375766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur4 TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPL 2 -1. FONCT 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elpeau4 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALICE TFRE 0.05
OPTI PAS AUTO
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.00 TFIN 10.0 NMAX 900000000
FIN

carm01a.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm01.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

carm01b.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm01.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
ISO FILL FIEL ECR0 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

carm01c.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm01.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

carm01d.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm01.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'Eyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'Eyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
FIN

carm02.epx

CARM02
ECHO
!CONV WIN
CAST MESH
DPLA
GEOM CAR1 sur41 CAR4 sur42 TERM
COMP NGRO 3
'noeuds_sym' LECT elpeau4 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau4 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau4 TERM COND Y LT 0.05
COUL VERT LECT sur41 TERM
ROUG LECT sur42 TERM
MATE VMIS ISOT RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725

```

228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.09330593267242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur4 TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPL 2 -1. FONCT 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elpeau4 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALICE TFRE 0.05
OPTI PAS AUTO CSTA 0.5
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.00 TFIN 10.0 NMAX 900000000
FIN

```

carm02a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

carm02b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
TEXT ISCA

```

```

COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

carm02c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

carm02d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'carm02.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_4267' DEPL COMP 2 NOEU LECT 4267 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyt' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyt' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 44 'fyt' FICH 'car401d.pun' RENA 'fyt_401'
RCOU 54 'fyt' FICH 'car102d.pun' RENA 'fyt_102'
TRAC 4 44 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
TRAC 4 54 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR VERT
FIN

```

pb201.epx

```

PBC201
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C272 2 TERM
0 0 1 0 0 1 1 0 0 1 0
0 0 1 0 1 1 1 1 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0.5 1 0 1.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY LECT 1 TERM
BODY LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00

```

```

!      Q      8.06707E-01  5.64863E-01 -8.68241E-02 -1.50384E-01
      VIEW  3.09976E-01  8.85244E-01 -3.46784E-01
      RIGH  9.39693E-01 -3.40719E-01 -2.98090E-02
      UP    1.44544E-01  3.16630E-01  9.37471E-01
      FOV   2.48819E+01

!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
      SLER CAM1 1 NFRA 1
      TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KPFE 10 COMP -1 REND
      FREQ 1
      GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
      GO
      TRAC OFFS FICH AVI CONT REND
      ENDFLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_27' DEPL COMP 3 NOEU LECT 27 TERM
COUR 2 'dz_54' DEPL COMP 3 NOEU LECT 54 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pb202.epx

```

PBC202
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C272 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0.5 1 0 1.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
      PINB BODY MLEV 1 LECT 1 TERM
      BODY MLEV 1 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
      VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 15
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
!      Q      8.06707E-01  5.64863E-01 -8.68241E-02 -1.50384E-01
      VIEW  3.09976E-01  8.85244E-01 -3.46784E-01
      RIGH  9.39693E-01 -3.40719E-01 -2.98090E-02
      UP    1.44544E-01  3.16630E-01  9.37471E-01
      FOV   2.48819E+01

!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
      SLER CAM1 1 NFRA 1
      TRAC OFFS FICH AVI NOCL NPTO 16 FPS 15 KPFE 10 COMP -1 REND
      FREQ 1
      GOTR LOOP 14 OFFS FICH AVI CONT NOCL REND
      GO
      TRAC OFFS FICH AVI CONT REND
      ENDFLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_27' DEPL COMP 3 NOEU LECT 27 TERM
COUR 2 'dz_54' DEPL COMP 3 NOEU LECT 54 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pb203.epx

```

PBC203
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C272 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0.5 1 0 1.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
      PINB BODY MLEV 2 LECT 1 TERM
      BODY MLEV 2 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
      VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 19
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
!      Q      8.06707E-01  5.64863E-01 -8.68241E-02 -1.50384E-01
      VIEW  3.09976E-01  8.85244E-01 -3.46784E-01
      RIGH  9.39693E-01 -3.40719E-01 -2.98090E-02
      UP    1.44544E-01  3.16630E-01  9.37471E-01
      FOV   2.48819E+01

!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
      SLER CAM1 1 NFRA 1
      TRAC OFFS FICH AVI NOCL NPTO 20 FPS 15 KPFE 10 COMP -1 REND
      FREQ 1
      GOTR LOOP 18 OFFS FICH AVI CONT NOCL REND
      GO
      TRAC OFFS FICH AVI CONT REND
      ENDFLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_27' DEPL COMP 3 NOEU LECT 27 TERM
COUR 2 'dz_54' DEPL COMP 3 NOEU LECT 54 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pb204.epx

```

PBC204
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C272 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0.5 1 0 1.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
      PINB BODY MLEV 3 LECT 1 TERM
      BODY MLEV 3 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
      VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100

```

```

*=====
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
UP 1.44544E-01 3.16630E-01 9.37471E-01
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 101 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 99 FPS 15 KFRE 5 COMP -1 REND
FREQ 1
GOTR LOOP 7 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_27' DEPL COMP 3 NOEU LECT 27 TERM
COUR 2 'dz_54' DEPL COMP 3 NOEU LECT 54 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
PIN

```

```

LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
PIN

```

pb232 .epx

```

PBC232
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C273 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0.5 1 1 0.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 1 LECT 1 TERM
BODY MLEV 1 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 16
*=====

```

pb231 .epx

```

PBC231
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C273 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0.5 1 1 0.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY LECT 1 TERM
BODY LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 17
*=====

```

```

PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
UP 1.44544E-01 3.16630E-01 9.37471E-01
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 17 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 15 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_27' DEPL COMP 3 NOEU LECT 27 TERM
COUR 2 'dz_54' DEPL COMP 3 NOEU LECT 54 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
PIN

```

pb233 .epx

```

PBC233
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C273 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0.5 1 1 0.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 2 LECT 1 TERM
BODY MLEV 2 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1

```

```

FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 20
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
HIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
UP 1.44544E-01 3.16630E-01 9.37471E-01
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 21 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 19 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_27' DEPL COMP 3 NOEU LECT 27 TERM
COUR 2 'dz_54' DEPL COMP 3 NOEU LECT 54 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
FIN

```

pb234.epx

```

PBC234
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 54 C273 2 TERM
0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 0 0 1 1
0.5 0.5 0 0.5 0 0.5 1 0.5 0.5 0.5 1 0.5 0 0.5 0.5 0.5 0.5 1
0.5 0 0 1 0.5 0 0.5 1 0 0 0.5 0 0 0.5 1 0 0.5 1 1 0.5 0 1 0.5
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0.5 0.5 0.5
0 0 1 1 0 1 1 1 0 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
0.5 0.5 1 0.5 0 1.5 1 0.5 1.5 0.5 1 1.5 0 0.5 1.5 0.5 0.5 2
0.5 0 1 1 0.5 1 0.5 1 1 0 0.5 1 0 0 1.5 1 0 1.5 1 1 1.5 0 1 1.5
0.5 0 2 1 0.5 2 0.5 1 2 0 0.5 2 0.5 0.5 1.5
1 2 3 4 5 6 7 8 9 10 11 12 13
14 15 16 17 18 19 20 21 22 23 24 25 26 27
28 29 30 31 32 33 34 35 36 37 38 39 40
41 42 43 44 45 46 47 48 49 50 51 52 53 54
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 3 LECT 1 TERM
BODY MLEV 3 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 27 TERM
VITE 3 -100 LECT 28 PAS 1 54 TERM
ECRI DEPL VITE ACCE FINT PEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
HIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
UP 1.44544E-01 3.16630E-01 9.37471E-01
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
FIN

```

```

SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_27' DEPL COMP 3 NOEU LECT 27 TERM
COUR 2 'dz_54' DEPL COMP 3 NOEU LECT 54 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
FIN

```

pb2a11.epx

```

Comparison of results with C272/C273
ECHO
RESU ALIC 'pb233.ali' GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 331 'dz_27_33' DEPL COMP 2 NOEU LECT 27 TERM
COUR 332 'dz_54_33' DEPL COMP 2 NOEU LECT 54 TERM
RCOU 11 'dz_27' FICH 'pb201.pun' RENA 'dz_27_01'
RCOU 12 'dz_54' FICH 'pb201.pun' RENA 'dz_54_01'
RCOU 21 'dz_27' FICH 'pb202.pun' RENA 'dz_27_02'
RCOU 22 'dz_54' FICH 'pb202.pun' RENA 'dz_54_02'
RCOU 31 'dz_27' FICH 'pb203.pun' RENA 'dz_27_03'
RCOU 32 'dz_54' FICH 'pb203.pun' RENA 'dz_54_03'
RCOU 311 'dz_27' FICH 'pb231.pun' RENA 'dz_27_31'
RCOU 312 'dz_54' FICH 'pb231.pun' RENA 'dz_54_31'
RCOU 321 'dz_27' FICH 'pb232.pun' RENA 'dz_27_32'
RCOU 322 'dz_54' FICH 'pb232.pun' RENA 'dz_54_32'
TRAC 11 21 31 311 321 331 AXES 1.0 'DISPL. [M]' YZER
TRAC 12 22 32 312 322 332 AXES 1.0 'DISPL. [M]' YZER
*****
FIN

```

pb801.epx

```

PBC801
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUB8 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY LECT 1 TERM
BODY LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT PEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
HIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
UP 1.44544E-01 3.16630E-01 9.37471E-01
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
FIN

```

pb802.epx

```

PBC802
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUB8 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0

```

```

0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
  PINB BODY MLEV 1 LECT 1 TERM
      BODY MLEV 1 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
      VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 9
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
      Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
      VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
      RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
      UP 1.44544E-01 3.16630E-01 9.37471E-01
      FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTO 10 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 8 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
FIN

```

```

TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
FIN

```

pbcr804.epx

```

PBC804
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUB8 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
  PINB BODY MLEV 3 LECT 1 TERM
      BODY MLEV 3 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
      VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
      Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
      VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
      RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
      UP 1.44544E-01 3.16630E-01 9.37471E-01
      FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTO 101 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
FIN

```

pbcr803.epx

```

PBC803
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUB8 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
  PINB BODY MLEV 2 LECT 1 TERM
      BODY MLEV 2 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
      VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 11
*****
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
      Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
      VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
      RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
      UP 1.44544E-01 3.16630E-01 9.37471E-01
      FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTO 12 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 10 OFFS FICH AVI CONT NOCL REND
GO

```

pbcu01.epx

```

PBCU01
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUBE 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
  PINB BODY LECT 1 TERM
      BODY LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
      VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT
      LNKS STAT DIAG DUMP

```

```

CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
  VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
  RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
  UP 1.44544E-01 3.16630E-01 9.37471E-01
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
  FACE HPRO
  PINB CDES JOIN
  VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
  TEXT VSCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KPRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

pbcu02.epx

```

PBCU02
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUBE 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
  TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
  LECT tous TERM
LINK COUP
  PINB BODY MLEV 1 LECT 1 TERM
  BODY MLEV 1 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
  VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
  FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
  PINS DUMP STAT EQVF
  LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
  VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
  RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
  UP 1.44544E-01 3.16630E-01 9.37471E-01
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
  FACE HPRO
  PINB CDES JOIN
  VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
  TEXT VSCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KPRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

pbcu03.epx

```

PBCU03
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUBE 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
  TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
  LECT tous TERM
LINK COUP
  PINB BODY MLEV 2 LECT 1 TERM
  BODY MLEV 2 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
  VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
  FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
  PINS DUMP STAT EQVF
  LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
  VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
  RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
  UP 1.44544E-01 3.16630E-01 9.37471E-01
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE
  FACE HPRO
  PINB CDES JOIN
  VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
  TEXT VSCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KPRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

pbcu04.epx

```

PBCU04
ECHO
!CONV WIN
LAGR TRID
GEOM LIBR POIN 16 CUBE 2 TERM
0 0 0 1 0 0 1 1 0 0 1 0
0 0 1 1 0 1 1 1 1 0 1 1
0 0 1 1 0 1 1 1 1 0 1 1
0 0 2 1 0 2 1 1 2 0 1 2
1 2 3 4 5 6 7 8
9 10 11 12 13 14 15 16
OPTI DUMP DPMA
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
  TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
  LECT tous TERM
LINK COUP
  PINB BODY MLEV 3 LECT 1 TERM
  BODY MLEV 3 LECT 2 TERM
INIT VITE 3 100 LECT 1 PAS 1 8 TERM
  VITE 3 -100 LECT 9 PAS 1 16 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
  FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
  PINS DUMP STAT EQVF
  LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE -1.77482E+00 -5.99653E+00 3.54494E+00
! Q 8.06707E-01 5.64863E-01 -8.68241E-02 -1.50384E-01
  VIEW 3.09976E-01 8.85244E-01 -3.46784E-01
  RIGH 9.39693E-01 -3.40719E-01 -2.98090E-02
  UP 1.44544E-01 3.16630E-01 9.37471E-01
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.00000E-01 5.00000E-01 1.00000E+00
!RSPPHERE: 1.83467E+00
!RADIUS : 7.33869E+00
!ASPECT : 1.00000E+00
!NEAR : 5.50402E+00
!FAR : 1.10080E+01
SCEN GEOM NAVI FREE

```

```

FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dz_1' DEPL COMP 3 NOEU LECT 1 TERM
COUR 2 'dz_13' DEPL COMP 3 NOEU LECT 13 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pbcuall.epx

```

Comparison of results with CUBE/CUB8
ECHO
RESU ALIC 'pbc803.ali' GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 331 'dz_1_33' DEPL COMP 2 NOEU LECT 1 TERM
COUR 332 'dz_13_33' DEPL COMP 2 NOEU LECT 13 TERM
RCOU 11 'dz_1' FICH 'pbcu01.pun' RENA 'dz_1_01'
RCOU 12 'dz_13' FICH 'pbcu01.pun' RENA 'dz_13_01'
RCOU 21 'dz_1' FICH 'pbcu02.pun' RENA 'dz_1_02'
RCOU 22 'dz_13' FICH 'pbcu02.pun' RENA 'dz_13_02'
RCOU 31 'dz_1' FICH 'pbcu03.pun' RENA 'dz_1_03'
RCOU 32 'dz_13' FICH 'pbcu03.pun' RENA 'dz_13_03'
RCOU 311 'dz_1' FICH 'pbc801.pun' RENA 'dz_1_31'
RCOU 312 'dz_13' FICH 'pbc801.pun' RENA 'dz_13_31'
RCOU 321 'dz_1' FICH 'pbc802.pun' RENA 'dz_1_32'
RCOU 322 'dz_13' FICH 'pbc802.pun' RENA 'dz_13_32'
TRAC 11 21 31 311 321 331 AXES 1.0 'DISPL. [M]' YZER
TRAC 12 22 32 312 322 332 AXES 1.0 'DISPL. [M]' YZER
*****
PIN

```

pbq401.epx

```

PBQ401
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q41L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY LECT 1 TERM
BODY LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT PEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSFPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

```

AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pbq402.epx

```

PBQ402
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q41L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 1 LECT 1 TERM
BODY MLEV 1 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT PEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSFPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pbq403.epx

```

PBQ403
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q41L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 2 LECT 1 TERM
BODY MLEV 2 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT PEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00

```



```

RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

```

LAGR CPLA
GEOM LIBR POIN 8 Q42L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY LECT 1 TERM
BODY LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

pbq404 . epx

```

PBQ404
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q41L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 3 LECT 1 TERM
BODY MLEV 3 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

```

PBQ422
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q42L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 1 LECT 1 TERM
BODY MLEV 1 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE

```

pbq422 . epx

pbq421 . epx

```

PBQ421
ECHO
!CONV WIN

```

```

PBQ422
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q42L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 1 LECT 1 TERM
BODY MLEV 1 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE

```

```

SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

```

INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pbq423.epx

```

PBQ423
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q42L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 2 LECT 1 TERM
BODY MLEV 2 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

```

PBQ423
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q42L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 2 LECT 1 TERM
BODY MLEV 2 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 4 TERM
VITE 2 -100 LECT 5 PAS 1 8 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*****
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_1' DEPL COMP 2 NOEU LECT 1 TERM
COUR 2 'dy_7' DEPL COMP 2 NOEU LECT 7 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*****
PIN

```

pbq4a11.epx

```

Comparison of results with Q41L/Q42L
ECHO
RESU ALIC 'pbq424.ali' GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 341 'dy_1_34' DEPL COMP 2 NOEU LECT 1 TERM
COUR 342 'dy_7_34' DEPL COMP 2 NOEU LECT 7 TERM
RCOU 11 'dy_1' FICH 'pbq401.pun' RENA 'dy_1_01'
RCOU 12 'dy_7' FICH 'pbq401.pun' RENA 'dy_7_01'
RCOU 21 'dy_1' FICH 'pbq402.pun' RENA 'dy_1_02'
RCOU 22 'dy_7' FICH 'pbq402.pun' RENA 'dy_7_02'
RCOU 31 'dy_1' FICH 'pbq403.pun' RENA 'dy_1_03'
RCOU 32 'dy_7' FICH 'pbq403.pun' RENA 'dy_7_03'
RCOU 41 'dy_1' FICH 'pbq404.pun' RENA 'dy_1_04'
RCOU 42 'dy_7' FICH 'pbq404.pun' RENA 'dy_7_04'
RCOU 311 'dy_1' FICH 'pbq421.pun' RENA 'dy_1_31'
RCOU 312 'dy_7' FICH 'pbq421.pun' RENA 'dy_7_31'
RCOU 321 'dy_1' FICH 'pbq422.pun' RENA 'dy_1_32'
RCOU 322 'dy_7' FICH 'pbq422.pun' RENA 'dy_7_32'
RCOU 331 'dy_1' FICH 'pbq423.pun' RENA 'dy_1_33'
RCOU 332 'dy_7' FICH 'pbq423.pun' RENA 'dy_7_33'
TRAC 11 21 31 41 311 321 331 341 AXES 1.0 'DISPL. [M]' YZER
TRAC 12 22 32 42 312 322 332 342 AXES 1.0 'DISPL. [M]' YZER
*****
PIN

```

pbq901.epx

```

PBQ901
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q92 2 TERM
0 0 1 0 2 0
0 1 1 1 2 1
0 2 1 2 2 2
0 2 1 2 2 2
0 3 1 3 2 3
0 4 1 4 2 4
1 2 3 6 9 8 7 4 5
10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY LECT 1 TERM
BODY LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*****
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00

```

pbq424.epx

```

PBQ424
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 8 Q42L 2 TERM
0 0 2 0
0 2 2 2
0 2 2 2
0 4 2 4
1 2 4 3
5 6 8 7
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 3 LECT 1 TERM
BODY MLEV 3 LECT 2 TERM

```

```

VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

pbq902.epx

```

PBQ902
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q92 2 TERM
0 0 1 0 2 0
0 1 1 1 2 1
0 2 1 2 2 2
0 2 1 2 2 2
0 3 1 3 2 3
0 4 1 4 2 4
1 2 3 6 9 8 7 4 5
10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 1 LECT 1 TERM
BODY MLEV 1 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

pbq903.epx

```

PBQ903
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q92 2 TERM
0 0 1 0 2 0
0 1 1 1 2 1
0 2 1 2 2 2
0 2 1 2 2 2
0 3 1 3 2 3
0 4 1 4 2 4
1 2 3 6 9 8 7 4 5
10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 2 LECT 1 TERM
BODY MLEV 2 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
FACE HFRO
PINB CDES JOIN
VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
TEXT VSCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
FIN

```

pbq904.epx

```

PBQ904
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q92 2 TERM
0 0 1 0 2 0
0 1 1 1 2 1
0 2 1 2 2 2
0 2 1 2 2 2
0 3 1 3 2 3
0 4 1 4 2 4
1 2 3 6 9 8 7 4 5
10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
LECT tous TERM
LINK COUP
PINB BODY MLEV 3 LECT 1 TERM
BODY MLEV 3 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
PINS DUMP STAT EQVF
LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00

```

```

!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
PIN

```

```

0 1 1 1 2 1
0 2 1 2 2 2
0 2 1 2 2 2
0 3 1 3 2 3
0 4 1 4 2 4
1 2 3 6 9 8 7 4 5
10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
      PINB BODY MLEV 1 LECT 1 TERM
      BODY MLEV 1 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
      VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 93 !100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 94 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 92 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
PIN

```

pbq931.epx

```

PBQ931
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q93 2 TERM
0 0 1 0 2 0
0 1 1 1 2 1
0 2 1 2 2 2
0 2 1 2 2 2
0 3 1 3 2 3
0 4 1 4 2 4
1 2 3 6 9 8 7 4 5
10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
      PINB BODY LECT 1 TERM
      BODY LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
      VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA
      COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 101 FPS 15 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*=====
PIN

```

```

PBQ933
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q93 2 TERM
0 0 1 0 2 0
0 1 1 1 2 1
0 2 1 2 2 2
0 2 1 2 2 2
0 3 1 3 2 3
0 4 1 4 2 4
1 2 3 6 9 8 7 4 5
10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
      PINB BODY MLEV 2 LECT 1 TERM
      BODY MLEV 2 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
      VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCE FINT FEXT FLIA FDEC CONT ECRO FREQ 1
      FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
      PINS DUMP STAT EQVF
      LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 100
*=====
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
      FACE HFRO
      PINB CDES JOIN
      VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
      TEXT VSCA

```

pbq933.epx

```

PBQ932
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q93 2 TERM
0 0 1 0 2 0

```

pbq932.epx

```

PBQ932
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q93 2 TERM
0 0 1 0 2 0

```

```

      COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 101 FPS 15 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 99 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*-----
FIN

```

pbq934.epx

```

PBQ934
ECHO
!CONV WIN
LAGR CPLA
GEOM LIBR POIN 18 Q93 2 TERM
  0 0 1 0 2 0
  0 1 1 1 2 1
  0 2 1 2 2 2
  0 2 1 2 2 2
  0 3 1 3 2 3
  0 4 1 4 2 4
  1 2 3 6 9 8 7 4 5
  10 11 12 15 18 17 16 13 14
OPTI DUMP DPMA
COMP EPAI 1. LECT tous TERM
MATE VM23 RO 8000. YOUN 1.D11 NU 0.3 ELAS 2.D8
      TRAC 3 2.D8 2.D-3 3.D8 1. 3.1D8 2.
      LECT tous TERM
LINK COUP
  PINB BODY MLEV 3 LECT 1 TERM
      BODY MLEV 3 LECT 2 TERM
INIT VITE 2 100 LECT 1 PAS 1 9 TERM
VITE 2 -100 LECT 10 PAS 1 18 TERM
ECRI DEPL VITE ACCB FINT FEXT FLIA FDEC CONT ECRO FRBQ 1
  FICH ALIC FREQ 1
OPTI PAS AUTO NOTE LOG 1
  PINS DUMP STAT EQVF
  LNKS STAT DIAG DUMP
CALC TINI 0. TEND 0.1D0 NMAX 44 1100
*-----
PLAY
CAME 1 EYE 1.00000E+00 2.00000E+00 1.56752E+01
!
  Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 1.00000E+00 2.00000E+00 0.00000E+00
!RSFPHERE: 3.13503E+00
!RADIUS : 1.56752E+01
!ASPECT : 1.00000E+00
!NEAR : 1.22266E+01
!FAR : 2.19452E+01
SCEN GEOM NAVI FREE
  FACE HFRO
  PINB CDES JOIN
  VECT SCCO FIEL VITE SCAL USER PROG 7 PAS 7 98 TERM
  TEXT VSCA
  COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 45 FPS 15 KPFE 10 COMP -1 REND
FREQ 1
GOTR LOOP 43 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----
SUIT
Post-treatment from Alice file
ECHO
RESU ALIC GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 1 'dy_05' DEPL COMP 2 NOEU LECT 5 TERM
COUR 2 'dy_14' DEPL COMP 2 NOEU LECT 14 TERM
TRAC 1 2 AXES 1.0 'DISPL. [M]'
LIST 1 2 AXES 1.0 'DISPL. [M]'
*-----
FIN

```

pbq9all.epx

```

Comparison of results with Q92/Q93
ECHO
RESU ALIC 'pbq934.ali' GARD PSCR
SORT GRAP
AXTE 1.0 'Time [s]'
COUR 341 'dy_05_34' DEPL COMP 2 NOEU LECT 5 TERM
COUR 342 'dy_14_34' DEPL COMP 2 NOEU LECT 14 TERM
RCOU 11 'dy_05' FICH 'pbq901.pun' RENA 'dy_05_01'
RCOU 12 'dy_14' FICH 'pbq901.pun' RENA 'dy_14_01'
RCOU 21 'dy_05' FICH 'pbq902.pun' RENA 'dy_05_02'
RCOU 22 'dy_14' FICH 'pbq902.pun' RENA 'dy_14_02'
RCOU 31 'dy_05' FICH 'pbq903.pun' RENA 'dy_05_03'
RCOU 32 'dy_14' FICH 'pbq903.pun' RENA 'dy_14_03'
RCOU 41 'dy_05' FICH 'pbq904.pun' RENA 'dy_05_04'
RCOU 42 'dy_14' FICH 'pbq904.pun' RENA 'dy_14_04'
RCOU 311 'dy_05' FICH 'pbq931.pun' RENA 'dy_05_31'

```

```

RCOU 312 'dy_14' FICH 'pbq931.pun' RENA 'dy_14_31'
RCOU 321 'dy_05' FICH 'pbq932.pun' RENA 'dy_05_32'
RCOU 322 'dy_14' FICH 'pbq932.pun' RENA 'dy_14_32'
RCOU 331 'dy_05' FICH 'pbq933.pun' RENA 'dy_05_33'
RCOU 332 'dy_14' FICH 'pbq933.pun' RENA 'dy_14_33'
TRAC 11 21 31 41 311 321 331 341 AXES 1.0 'DISPL. [M]' YZER
TRAC 12 22 32 42 312 322 332 342 AXES 1.0 'DISPL. [M]' YZER
*-----
PIN

```

pxq42q92.proc

```

'DEBPROC' pxq42q92 q4*'MAILLAGE';
*
*-----
* Transforms a q4 (in 2d !!!) into a q9 by creating:
* - 4 new mid-side nodes
* - 1 new central node
*
* Input :
* -----
* q4 : a mesh containing just one q4 (in 2d)
* Output :
* -----
* q9 : mesh containing one q9 (in 3d; meshed as qua9)
*-----
*
hh = chan poil q4;
*
p01 = hh poin 1;
p02 = hh poin 2;
p03 = hh poin 3;
p04 = hh poin 4;
*
n01 = noeuv p01;
n02 = noeuv p02;
n03 = noeuv p03;
n04 = noeuv p04;
*
x01 y01 = coor p01;
x02 y02 = coor p02;
x03 y03 = coor p03;
x04 y04 = coor p04;
*
x05 = (x01 + x02) / 2.0;
y05 = (y01 + y02) / 2.0;
p05 = x05 y05;
n05 = noeuv p05;
*
x06 = (x02 + x03) / 2.0;
y06 = (y02 + y03) / 2.0;
p06 = x06 y06;
n06 = noeuv p06;
*
x07 = (x03 + x04) / 2.0;
y07 = (y03 + y04) / 2.0;
p07 = x07 y07;
n07 = noeuv p07;
*
x08 = (x01 + x04) / 2.0;
y08 = (y01 + y04) / 2.0;
p08 = x08 y08;
n08 = noeuv p08;
*
x09 = (x01 + x02 + x03 + x04) / 4.0;
y09 = (y01 + y02 + y03 + y04) / 4.0;
p09 = x09 y09;
n09 = noeuv p09;
*
* Q9 element in 2D (meshed as "qua9")
*
*q9 = manu qua9 p01 p02 p03 p04 p05 p06 p07 p08 p09;
q9 = manu qua9 p01 p05 p02 p06 p03 p07 p04 p08 p09;
*
finproc q9;

```

pxq92q4.proc

```

'DEBPROC' pxq92q4 q9*'MAILLAGE';
*
*-----
* Transforms a q9 (in 2d !!!) into four q4, one for each
* "quadrant" of the q9
*
* Input :
* -----
* q9 : a mesh containing just one q9 (in 2d)
* Output :
* -----
* q4 : mesh containing four q4 (in 2d; meshed as qua4)
*-----
*
hh = chan poil q9;
*
p01 = hh poin 1;
p02 = hh poin 2;
p03 = hh poin 3;
p04 = hh poin 4;
p05 = hh poin 5;
p06 = hh poin 6;
p07 = hh poin 7;
p08 = hh poin 8;
p09 = hh poin 9;
*
q41 = manu qua4 p01 p02 p09 p08;
q42 = manu qua4 p02 p03 p04 p09;
q43 = manu qua4 p09 p04 p05 p06;
q44 = manu qua4 p08 p09 p06 p07;
*
q4 = q41 et q42 et q43 et q44;
*
finproc q4;

```

q92_03.epx

Q92_03
ECHO
! CONV WIN
CAST mesh
DPLA
GEOM Q92 sur9 TERM
COMP EPAI 1. LECT sur9 TERM
NGRO 3
'noeuds_sym' LECT elpeau9 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau9 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau9 TERM COND Y LT 0.05
COUL VERT LECT sur9 TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur9 TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPLA 2 -1. FONC 1 LECT noeuds_haut TERM
PINB SELP DMIN 0.1 LECT elpeau9 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TPFE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TPFE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

OPTI PRIN
SORT VISU NSTO 1

PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECR0 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
SUPP LECT sur9 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 27 FPS 25 KFRE 10 COMP -1
OBJE LECT sur9 TERM REND
FREQ 1
GOTR LOOP 25 OFFS FICH AVI CONT NOCL
OBJE LECT sur9 TERM REND
GO
TRAC OFFS FICH AVI CONT
OBJE LECT sur9 TERM REND
ENDPLAY

FIN

q92_03c.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q92_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1

PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 27 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 25 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY

FIN

q92_03a.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q92_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1

PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 27 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 25 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY

FIN

q92_03d.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q92_03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_1226' DEPL COMP 2 NOEU LECT 1226 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyt' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyt' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fyt' FICH 'car401d.pun' RENA 'fyt_g4'
RCOU 24 'fyt' FICH 'q93_02d.pun' RENA 'fyt_g9q4'
RCOU 34 'fyt' FICH 'q93_03d.pun' RENA 'fyt_g93'
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
XMIN 0 XMAX 2 DX 0.2 YMIN 0 YMAX 800 DY 100
COLO NOIR ROUG VERT TURQ
FIN

q93_02.epx

Q93_02
ECHO
! CONV WIN
CAST mesh
DPLA
GEOM Q93 sur9 Q41L sur4p TERM
COMP EPAI 1. LECT sur9 sur4p TERM
NGRO 3
'noeuds_sym' LECT sur4p TERM COND X GT 14.95
'noeuds_haut' LECT sur4p TERM COND Y GT 16.95

q92_03b.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q92_03.ali' GARD PSCR

```
'noeuds_bas' LECT sur4p TERM COND Y LT 0.05
COUL VERT LECT sur9 TERM
TURQ LECT sur4p TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.042549634882759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur9 TERM
FANT 0.0
LECT sur4p TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPLA 2 -1. POND 1 LECT noeuds_haut TERM
PINB SELP DMIN 0.1 LECT sur4p TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TPFE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TPFE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF CNOR
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN
```

q93_02a.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 183 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 181 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN
```

q93_02b.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
```

```
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECR0 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
SUPP LECT sur9 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 183 FPS 25 KFRE 10 COMP -1
OBJE LECT sur9 TERM REND
FREQ 1
GOTR LOOP 181 OFFS FICH AVI CONT NOCL
OBJE LECT sur9 TERM REND
GO
TRAC OFFS FICH AVI CONT
OBJE LECT sur9 TERM REND
ENDPLAY
*=====
FIN
```

q93_02c.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_02.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 183 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 181 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN
```

q93_02d.epx

```
Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_02.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_1226' DEPL COMP 2 NOEU LECT 1226 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyb' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyb' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fyb' FICH 'car401d.pun' RENA 'fyb_q4'
TRAC 4 14 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG
FIN
```

q93_03.epx

```
Q93_03
ECHO
!CONV WIN
CAST mesh
DPLA
GEOM Q93 sur9 TERM
COMP EPAI 1. LECT sur9 TERM
NGRO 3
'noeuds_sym' LECT elpeau9 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau9 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau9 TERM COND Y LT 0.05
COUL VERT LECT sur9 TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
```

```

272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.0055502897212425
326.269365384357 0.00765116075599371
358.247494301277 0.011812993392129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.1034300066733347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608

LECT sur9 TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPLA 2 -1. FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elpeau9 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

```

q93_03a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSFPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

q93_03b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSFPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
SUPP LECT sur9 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1
OBJE LECT sur9 TERM REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL

```

```

OBJE LECT sur9 TERM REND
GO
TRAC OFFS FICH AVI CONT
OBJE LECT sur9 TERM REND
ENDPLAY
*=====
FIN

```

q93_03c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSFPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

q93_03d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_1226' DEPL COMP 2 NOEU LECT 1226 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyh' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyh' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fyh' FICH 'car401d.pun' RENA 'fyt_g4'
RCOU 24 'fyh' FICH 'q93_02d.pun' RENA 'fyt_g9g4'
TRAC 4 14 24 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT
COUR 5 'dt' DT1
TRAC 5 AXES 1.0 'DELTAT [s]' YZER XGRD YGRD
LIST 5 AXES 1.0 'DELTAT [s]' YZER XGRD YGRD
FIN

```

q93_03e.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q93_03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'ecr1_gp1' ECRO COMP 1 GAUS 1 ELEM LECT 4071 TERM
COUR 2 'ecr1_gp2' ECRO COMP 1 GAUS 2 ELEM LECT 4071 TERM
COUR 3 'ecr1_gp3' ECRO COMP 1 GAUS 3 ELEM LECT 4071 TERM
COUR 4 'ecr1_gp4' ECRO COMP 1 GAUS 4 ELEM LECT 4071 TERM
COUR 5 'ecr1_gp5' ECRO COMP 1 GAUS 5 ELEM LECT 4071 TERM
COUR 6 'ecr1_gp6' ECRO COMP 1 GAUS 6 ELEM LECT 4071 TERM
COUR 7 'ecr1_gp7' ECRO COMP 1 GAUS 7 ELEM LECT 4071 TERM
COUR 8 'ecr1_gp8' ECRO COMP 1 GAUS 8 ELEM LECT 4071 TERM
COUR 9 'ecr1_gp9' ECRO COMP 1 GAUS 9 ELEM LECT 4071 TERM
TRAC 1 2 3 4 5 6 7 8 9 AXES 1.0 'HYDR [PA]' YZER
COUR 21 'ecr2_gp1' ECRO COMP 2 GAUS 1 ELEM LECT 4071 TERM
COUR 22 'ecr2_gp2' ECRO COMP 2 GAUS 2 ELEM LECT 4071 TERM
COUR 23 'ecr2_gp3' ECRO COMP 2 GAUS 3 ELEM LECT 4071 TERM
COUR 24 'ecr2_gp4' ECRO COMP 2 GAUS 4 ELEM LECT 4071 TERM
COUR 25 'ecr2_gp5' ECRO COMP 2 GAUS 5 ELEM LECT 4071 TERM
COUR 26 'ecr2_gp6' ECRO COMP 2 GAUS 6 ELEM LECT 4071 TERM
COUR 27 'ecr2_gp7' ECRO COMP 2 GAUS 7 ELEM LECT 4071 TERM
COUR 28 'ecr2_gp8' ECRO COMP 2 GAUS 8 ELEM LECT 4071 TERM
COUR 29 'ecr2_gp9' ECRO COMP 2 GAUS 9 ELEM LECT 4071 TERM
TRAC 21 22 23 24 25 26 27 28 29 AXES 1.0 'VMIS [PA]' YZER
COUR 31 'ecr3_gp1' ECRO COMP 3 GAUS 1 ELEM LECT 4071 TERM
COUR 32 'ecr3_gp2' ECRO COMP 3 GAUS 2 ELEM LECT 4071 TERM
COUR 33 'ecr3_gp3' ECRO COMP 3 GAUS 3 ELEM LECT 4071 TERM
COUR 34 'ecr3_gp4' ECRO COMP 3 GAUS 4 ELEM LECT 4071 TERM
COUR 35 'ecr3_gp5' ECRO COMP 3 GAUS 5 ELEM LECT 4071 TERM
COUR 36 'ecr3_gp6' ECRO COMP 3 GAUS 6 ELEM LECT 4071 TERM
COUR 37 'ecr3_gp7' ECRO COMP 3 GAUS 7 ELEM LECT 4071 TERM
COUR 38 'ecr3_gp8' ECRO COMP 3 GAUS 8 ELEM LECT 4071 TERM
COUR 39 'ecr3_gp9' ECRO COMP 3 GAUS 9 ELEM LECT 4071 TERM
TRAC 31 32 33 34 35 36 37 38 39 AXES 1.0 'PL_STR. [-]' YZER

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```

COUR 41 'ecr4_gp1' ECRO COMP 4 GAUS 1 ELEM LECT 4071 TERM
COUR 42 'ecr4_gp2' ECRO COMP 4 GAUS 2 ELEM LECT 4071 TERM
COUR 43 'ecr4_gp3' ECRO COMP 4 GAUS 3 ELEM LECT 4071 TERM
COUR 44 'ecr4_gp4' ECRO COMP 4 GAUS 4 ELEM LECT 4071 TERM
COUR 45 'ecr4_gp5' ECRO COMP 4 GAUS 5 ELEM LECT 4071 TERM
COUR 46 'ecr4_gp6' ECRO COMP 4 GAUS 6 ELEM LECT 4071 TERM
COUR 47 'ecr4_gp7' ECRO COMP 4 GAUS 7 ELEM LECT 4071 TERM
COUR 48 'ecr4_gp8' ECRO COMP 4 GAUS 8 ELEM LECT 4071 TERM
COUR 49 'ecr4_gp9' ECRO COMP 4 GAUS 9 ELEM LECT 4071 TERM
TRAC 41 42 43 44 45 46 47 48 49 AXES 1.0 'EPSX [-]' YZER

COUR 51 'ecr5_gp1' ECRO COMP 5 GAUS 1 ELEM LECT 4071 TERM
COUR 52 'ecr5_gp2' ECRO COMP 5 GAUS 2 ELEM LECT 4071 TERM
COUR 53 'ecr5_gp3' ECRO COMP 5 GAUS 3 ELEM LECT 4071 TERM
COUR 54 'ecr5_gp4' ECRO COMP 5 GAUS 4 ELEM LECT 4071 TERM
COUR 55 'ecr5_gp5' ECRO COMP 5 GAUS 5 ELEM LECT 4071 TERM
COUR 56 'ecr5_gp6' ECRO COMP 5 GAUS 6 ELEM LECT 4071 TERM
COUR 57 'ecr5_gp7' ECRO COMP 5 GAUS 7 ELEM LECT 4071 TERM
COUR 58 'ecr5_gp8' ECRO COMP 5 GAUS 8 ELEM LECT 4071 TERM
COUR 59 'ecr5_gp9' ECRO COMP 5 GAUS 9 ELEM LECT 4071 TERM
TRAC 51 52 53 54 55 56 57 58 59 AXES 1.0 'EPSY [-]' YZER

COUR 61 'ecr6_gp1' ECRO COMP 6 GAUS 1 ELEM LECT 4071 TERM
COUR 62 'ecr6_gp2' ECRO COMP 6 GAUS 2 ELEM LECT 4071 TERM
COUR 63 'ecr6_gp3' ECRO COMP 6 GAUS 3 ELEM LECT 4071 TERM
COUR 64 'ecr6_gp4' ECRO COMP 6 GAUS 4 ELEM LECT 4071 TERM
COUR 65 'ecr6_gp5' ECRO COMP 6 GAUS 5 ELEM LECT 4071 TERM
COUR 66 'ecr6_gp6' ECRO COMP 6 GAUS 6 ELEM LECT 4071 TERM
COUR 67 'ecr6_gp7' ECRO COMP 6 GAUS 7 ELEM LECT 4071 TERM
COUR 68 'ecr6_gp8' ECRO COMP 6 GAUS 8 ELEM LECT 4071 TERM
COUR 69 'ecr6_gp9' ECRO COMP 6 GAUS 9 ELEM LECT 4071 TERM
TRAC 61 62 63 64 65 66 67 68 69 AXES 1.0 'EPSXY [-]' YZER

COUR 71 'ecr7_gp1' ECRO COMP 7 GAUS 1 ELEM LECT 4071 TERM
COUR 72 'ecr7_gp2' ECRO COMP 7 GAUS 2 ELEM LECT 4071 TERM
COUR 73 'ecr7_gp3' ECRO COMP 7 GAUS 3 ELEM LECT 4071 TERM
COUR 74 'ecr7_gp4' ECRO COMP 7 GAUS 4 ELEM LECT 4071 TERM
COUR 75 'ecr7_gp5' ECRO COMP 7 GAUS 5 ELEM LECT 4071 TERM
COUR 76 'ecr7_gp6' ECRO COMP 7 GAUS 6 ELEM LECT 4071 TERM
COUR 77 'ecr7_gp7' ECRO COMP 7 GAUS 7 ELEM LECT 4071 TERM
COUR 78 'ecr7_gp8' ECRO COMP 7 GAUS 8 ELEM LECT 4071 TERM
COUR 79 'ecr7_gp9' ECRO COMP 7 GAUS 9 ELEM LECT 4071 TERM
TRAC 71 72 73 74 75 76 77 78 79 AXES 1.0 'YIELD [PA]' YZER

COUR 81 'ecr8_gp1' ECRO COMP 8 GAUS 1 ELEM LECT 4071 TERM
COUR 82 'ecr8_gp2' ECRO COMP 8 GAUS 2 ELEM LECT 4071 TERM
COUR 83 'ecr8_gp3' ECRO COMP 8 GAUS 3 ELEM LECT 4071 TERM
COUR 84 'ecr8_gp4' ECRO COMP 8 GAUS 4 ELEM LECT 4071 TERM
COUR 85 'ecr8_gp5' ECRO COMP 8 GAUS 5 ELEM LECT 4071 TERM
COUR 86 'ecr8_gp6' ECRO COMP 8 GAUS 6 ELEM LECT 4071 TERM
COUR 87 'ecr8_gp7' ECRO COMP 8 GAUS 7 ELEM LECT 4071 TERM
COUR 88 'ecr8_gp8' ECRO COMP 8 GAUS 8 ELEM LECT 4071 TERM
COUR 89 'ecr8_gp9' ECRO COMP 8 GAUS 9 ELEM LECT 4071 TERM
TRAC 81 82 83 84 85 86 87 88 89 AXES 1.0 'EPSZ [-]' YZER

COUR 111 'con1_gp1' CONT COMP 1 GAUS 1 ELEM LECT 4071 TERM
COUR 112 'con1_gp2' CONT COMP 1 GAUS 2 ELEM LECT 4071 TERM
COUR 113 'con1_gp3' CONT COMP 1 GAUS 3 ELEM LECT 4071 TERM
COUR 114 'con1_gp4' CONT COMP 1 GAUS 4 ELEM LECT 4071 TERM
COUR 115 'con1_gp5' CONT COMP 1 GAUS 5 ELEM LECT 4071 TERM
COUR 116 'con1_gp6' CONT COMP 1 GAUS 6 ELEM LECT 4071 TERM
COUR 117 'con1_gp7' CONT COMP 1 GAUS 7 ELEM LECT 4071 TERM
COUR 118 'con1_gp8' CONT COMP 1 GAUS 8 ELEM LECT 4071 TERM
COUR 119 'con1_gp9' CONT COMP 1 GAUS 9 ELEM LECT 4071 TERM
TRAC 111 112 113 114 115 116 117 118 119 AXES 1.0 'SX [PA]' YZER

COUR 121 'con2_gp1' CONT COMP 2 GAUS 1 ELEM LECT 4071 TERM
COUR 122 'con2_gp2' CONT COMP 2 GAUS 2 ELEM LECT 4071 TERM
COUR 123 'con2_gp3' CONT COMP 2 GAUS 3 ELEM LECT 4071 TERM
COUR 124 'con2_gp4' CONT COMP 2 GAUS 4 ELEM LECT 4071 TERM
COUR 125 'con2_gp5' CONT COMP 2 GAUS 5 ELEM LECT 4071 TERM
COUR 126 'con2_gp6' CONT COMP 2 GAUS 6 ELEM LECT 4071 TERM
COUR 127 'con2_gp7' CONT COMP 2 GAUS 7 ELEM LECT 4071 TERM
COUR 128 'con2_gp8' CONT COMP 2 GAUS 8 ELEM LECT 4071 TERM
COUR 129 'con2_gp9' CONT COMP 2 GAUS 9 ELEM LECT 4071 TERM
TRAC 121 122 123 124 125 126 127 128 129 AXES 1.0 'SY [PA]' YZER

COUR 131 'con3_gp1' CONT COMP 3 GAUS 1 ELEM LECT 4071 TERM
COUR 132 'con3_gp2' CONT COMP 3 GAUS 2 ELEM LECT 4071 TERM
COUR 133 'con3_gp3' CONT COMP 3 GAUS 3 ELEM LECT 4071 TERM
COUR 134 'con3_gp4' CONT COMP 3 GAUS 4 ELEM LECT 4071 TERM
COUR 135 'con3_gp5' CONT COMP 3 GAUS 5 ELEM LECT 4071 TERM
COUR 136 'con3_gp6' CONT COMP 3 GAUS 6 ELEM LECT 4071 TERM
COUR 137 'con3_gp7' CONT COMP 3 GAUS 7 ELEM LECT 4071 TERM
COUR 138 'con3_gp8' CONT COMP 3 GAUS 8 ELEM LECT 4071 TERM
COUR 139 'con3_gp9' CONT COMP 3 GAUS 9 ELEM LECT 4071 TERM
TRAC 131 132 133 134 135 136 137 138 139 AXES 1.0 'SXY [PA]' YZER

COUR 141 'con4_gp1' CONT COMP 4 GAUS 1 ELEM LECT 4071 TERM
COUR 142 'con4_gp2' CONT COMP 4 GAUS 2 ELEM LECT 4071 TERM
COUR 143 'con4_gp3' CONT COMP 4 GAUS 3 ELEM LECT 4071 TERM
COUR 144 'con4_gp4' CONT COMP 4 GAUS 4 ELEM LECT 4071 TERM
COUR 145 'con4_gp5' CONT COMP 4 GAUS 5 ELEM LECT 4071 TERM
COUR 146 'con4_gp6' CONT COMP 4 GAUS 6 ELEM LECT 4071 TERM
COUR 147 'con4_gp7' CONT COMP 4 GAUS 7 ELEM LECT 4071 TERM
COUR 148 'con4_gp8' CONT COMP 4 GAUS 8 ELEM LECT 4071 TERM
COUR 149 'con4_gp9' CONT COMP 4 GAUS 9 ELEM LECT 4071 TERM
TRAC 141 142 143 144 145 146 147 148 149 AXES 1.0 'SZ [PA]' YZER

```

FIN

q95_03.epx

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Q95_03
ECHO
! CONV WIN
CAST mesh
DPLA
GEOM Q95 sur9 TERM
COMP EPAI 1. LECT sur9 TERM
NGRO 3
'noeuds_sym' LECT elpeau9 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau9 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau9 TERM COND Y LT 0.05
COUL VERT LECT sur9 TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35

```

```

TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.01181229933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242180
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.85 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608

```

```

LECT sur9 TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DBPLA 2 -1. FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elpeau9 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

```

q95_03a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q95_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
! NAVIGATION MODE: ROTATING CAMERA
! CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
! RSPPHERE: 1.27387E+01
! RADIUS : 4.84072E+01
! ASPECT : 1.00000E+00
! INEAR : 3.56685E+01
! FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 69 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 67 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

q95_03b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q95_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
! NAVIGATION MODE: ROTATING CAMERA
! CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
! RSPPHERE: 1.27387E+01
! RADIUS : 4.84072E+01
! ASPECT : 1.00000E+00
! INEAR : 3.56685E+01

```

```

!FAR      : 7.38847E+01
SCEN GEOM NAVI FREE
          LINE HEOU SFRE
          ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
          SUPP LECT sur9 TERM
          TEXT ISCA
          COLO PAPE
          SLER CAM1 1 NFRA 1
          TRAC OFFS FICH AVI NOCL NPTO 69 FPS 25 KPRE 10 COMP -1
          OBJE LECT sur9 TERM REND
FREQ 1
GOTR LOOP 67 OFFS FICH AVI CONT NOCL
          OBJE LECT sur9 TERM REND
GO
TRAC OFFS FICH AVI CONT
          OBJE LECT sur9 TERM REND
ENDPLAY
*=====
FIN

```

q95_03c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q95_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
  VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
  RIGH 1.00000E+00 0.00000E+00 0.00000E+00
  UP 0.00000E+00 1.00000E+00 0.00000E+00
  FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
          LINE HEOU SFRE
          FACE HFRO
          PINB CDES
          COLO PAPE
          SLER CAM1 1 NFRA 1
          TRAC OFFS FICH AVI NOCL NPTO 69 FPS 25 KPRE 10 COMP -1 REND
          FREQ 1
          GOTR LOOP 67 OFFS FICH AVI CONT NOCL REND
          GO
          TRAC OFFS FICH AVI CONT REND
          ENDPLAY
          *=====
          FIN

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q95_03d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q95_03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_1226' DBPL COMP 2 NOBU LECT 1226 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyt' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyt' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fyt' FICH 'car401d.pun' RENA 'fyt_q4'
RCOU 24 'fyt' FICH 'q93_02d.pun' RENA 'fyt_q9q4'
RCOU 34 'fyt' FICH 'q93_03d.pun' RENA 'fyt_q93'
RCOU 44 'fyt' FICH 'q92_03d.pun' RENA 'fyt_q92'
TRAC 4 14 24 34 44 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ ROSE
TRAC 4 14 24 34 44 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
          XMIN 0 XMAX 4 DX 0.4 YMIN 0 YMAX 900 DY 100
COLO NOIR ROUG VERT TURQ ROSE
FIN

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q95_03e.epx

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Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q95_03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'ecr1_gp1' ECRO COMP 1 GAUS 1 ELEM LECT 4071 TERM
COUR 2 'ecr1_gp2' ECRO COMP 1 GAUS 2 ELEM LECT 4071 TERM
COUR 3 'ecr1_gp3' ECRO COMP 1 GAUS 3 ELEM LECT 4071 TERM
COUR 4 'ecr1_gp4' ECRO COMP 1 GAUS 4 ELEM LECT 4071 TERM
COUR 5 'ecr1_gp5' ECRO COMP 1 GAUS 5 ELEM LECT 4071 TERM
COUR 6 'ecr1_gp6' ECRO COMP 1 GAUS 6 ELEM LECT 4071 TERM
COUR 7 'ecr1_gp7' ECRO COMP 1 GAUS 7 ELEM LECT 4071 TERM
COUR 8 'ecr1_gp8' ECRO COMP 1 GAUS 8 ELEM LECT 4071 TERM
COUR 9 'ecr1_gp9' ECRO COMP 1 GAUS 9 ELEM LECT 4071 TERM
TRAC 1 2 3 4 5 6 7 8 9 AXES 1.0 'HYDR [PA]' YZER

COUR 21 'ecr2_gp1' ECRO COMP 2 GAUS 1 ELEM LECT 4071 TERM
COUR 22 'ecr2_gp2' ECRO COMP 2 GAUS 2 ELEM LECT 4071 TERM
COUR 23 'ecr2_gp3' ECRO COMP 2 GAUS 3 ELEM LECT 4071 TERM
COUR 24 'ecr2_gp4' ECRO COMP 2 GAUS 4 ELEM LECT 4071 TERM
COUR 25 'ecr2_gp5' ECRO COMP 2 GAUS 5 ELEM LECT 4071 TERM
COUR 26 'ecr2_gp6' ECRO COMP 2 GAUS 6 ELEM LECT 4071 TERM
COUR 27 'ecr2_gp7' ECRO COMP 2 GAUS 7 ELEM LECT 4071 TERM
COUR 28 'ecr2_gp8' ECRO COMP 2 GAUS 8 ELEM LECT 4071 TERM

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COUR 29 'ecr2_gp9' ECRO COMP 2 GAUS 9 ELEM LECT 4071 TERM
TRAC 21 22 23 24 25 26 27 28 29 AXES 1.0 'VMIS [PA]' YZER

COUR 31 'ecr3_gp1' ECRO COMP 3 GAUS 1 ELEM LECT 4071 TERM
COUR 32 'ecr3_gp2' ECRO COMP 3 GAUS 2 ELEM LECT 4071 TERM
COUR 33 'ecr3_gp3' ECRO COMP 3 GAUS 3 ELEM LECT 4071 TERM
COUR 34 'ecr3_gp4' ECRO COMP 3 GAUS 4 ELEM LECT 4071 TERM
COUR 35 'ecr3_gp5' ECRO COMP 3 GAUS 5 ELEM LECT 4071 TERM
COUR 36 'ecr3_gp6' ECRO COMP 3 GAUS 6 ELEM LECT 4071 TERM
COUR 37 'ecr3_gp7' ECRO COMP 3 GAUS 7 ELEM LECT 4071 TERM
COUR 38 'ecr3_gp8' ECRO COMP 3 GAUS 8 ELEM LECT 4071 TERM
COUR 39 'ecr3_gp9' ECRO COMP 3 GAUS 9 ELEM LECT 4071 TERM
TRAC 31 32 33 34 35 36 37 38 39 AXES 1.0 'PL_STR. [-]' YZER

COUR 41 'ecr4_gp1' ECRO COMP 4 GAUS 1 ELEM LECT 4071 TERM
COUR 42 'ecr4_gp2' ECRO COMP 4 GAUS 2 ELEM LECT 4071 TERM
COUR 43 'ecr4_gp3' ECRO COMP 4 GAUS 3 ELEM LECT 4071 TERM
COUR 44 'ecr4_gp4' ECRO COMP 4 GAUS 4 ELEM LECT 4071 TERM
COUR 45 'ecr4_gp5' ECRO COMP 4 GAUS 5 ELEM LECT 4071 TERM
COUR 46 'ecr4_gp6' ECRO COMP 4 GAUS 6 ELEM LECT 4071 TERM
COUR 47 'ecr4_gp7' ECRO COMP 4 GAUS 7 ELEM LECT 4071 TERM
COUR 48 'ecr4_gp8' ECRO COMP 4 GAUS 8 ELEM LECT 4071 TERM
COUR 49 'ecr4_gp9' ECRO COMP 4 GAUS 9 ELEM LECT 4071 TERM
TRAC 41 42 43 44 45 46 47 48 49 AXES 1.0 'EPSX [-]' YZER

COUR 51 'ecr5_gp1' ECRO COMP 5 GAUS 1 ELEM LECT 4071 TERM
COUR 52 'ecr5_gp2' ECRO COMP 5 GAUS 2 ELEM LECT 4071 TERM
COUR 53 'ecr5_gp3' ECRO COMP 5 GAUS 3 ELEM LECT 4071 TERM
COUR 54 'ecr5_gp4' ECRO COMP 5 GAUS 4 ELEM LECT 4071 TERM
COUR 55 'ecr5_gp5' ECRO COMP 5 GAUS 5 ELEM LECT 4071 TERM
COUR 56 'ecr5_gp6' ECRO COMP 5 GAUS 6 ELEM LECT 4071 TERM
COUR 57 'ecr5_gp7' ECRO COMP 5 GAUS 7 ELEM LECT 4071 TERM
COUR 58 'ecr5_gp8' ECRO COMP 5 GAUS 8 ELEM LECT 4071 TERM
COUR 59 'ecr5_gp9' ECRO COMP 5 GAUS 9 ELEM LECT 4071 TERM
TRAC 51 52 53 54 55 56 57 58 59 AXES 1.0 'EPSY [-]' YZER

COUR 61 'ecr6_gp1' ECRO COMP 6 GAUS 1 ELEM LECT 4071 TERM
COUR 62 'ecr6_gp2' ECRO COMP 6 GAUS 2 ELEM LECT 4071 TERM
COUR 63 'ecr6_gp3' ECRO COMP 6 GAUS 3 ELEM LECT 4071 TERM
COUR 64 'ecr6_gp4' ECRO COMP 6 GAUS 4 ELEM LECT 4071 TERM
COUR 65 'ecr6_gp5' ECRO COMP 6 GAUS 5 ELEM LECT 4071 TERM
COUR 66 'ecr6_gp6' ECRO COMP 6 GAUS 6 ELEM LECT 4071 TERM
COUR 67 'ecr6_gp7' ECRO COMP 6 GAUS 7 ELEM LECT 4071 TERM
COUR 68 'ecr6_gp8' ECRO COMP 6 GAUS 8 ELEM LECT 4071 TERM
COUR 69 'ecr6_gp9' ECRO COMP 6 GAUS 9 ELEM LECT 4071 TERM
TRAC 61 62 63 64 65 66 67 68 69 AXES 1.0 'EPSXY [-]' YZER

COUR 71 'ecr7_gp1' ECRO COMP 7 GAUS 1 ELEM LECT 4071 TERM
COUR 72 'ecr7_gp2' ECRO COMP 7 GAUS 2 ELEM LECT 4071 TERM
COUR 73 'ecr7_gp3' ECRO COMP 7 GAUS 3 ELEM LECT 4071 TERM
COUR 74 'ecr7_gp4' ECRO COMP 7 GAUS 4 ELEM LECT 4071 TERM
COUR 75 'ecr7_gp5' ECRO COMP 7 GAUS 5 ELEM LECT 4071 TERM
COUR 76 'ecr7_gp6' ECRO COMP 7 GAUS 6 ELEM LECT 4071 TERM
COUR 77 'ecr7_gp7' ECRO COMP 7 GAUS 7 ELEM LECT 4071 TERM
COUR 78 'ecr7_gp8' ECRO COMP 7 GAUS 8 ELEM LECT 4071 TERM
COUR 79 'ecr7_gp9' ECRO COMP 7 GAUS 9 ELEM LECT 4071 TERM
TRAC 71 72 73 74 75 76 77 78 79 AXES 1.0 'YIELD [PA]' YZER

COUR 81 'ecr8_gp1' ECRO COMP 8 GAUS 1 ELEM LECT 4071 TERM
COUR 82 'ecr8_gp2' ECRO COMP 8 GAUS 2 ELEM LECT 4071 TERM
COUR 83 'ecr8_gp3' ECRO COMP 8 GAUS 3 ELEM LECT 4071 TERM
COUR 84 'ecr8_gp4' ECRO COMP 8 GAUS 4 ELEM LECT 4071 TERM
COUR 85 'ecr8_gp5' ECRO COMP 8 GAUS 5 ELEM LECT 4071 TERM
COUR 86 'ecr8_gp6' ECRO COMP 8 GAUS 6 ELEM LECT 4071 TERM
COUR 87 'ecr8_gp7' ECRO COMP 8 GAUS 7 ELEM LECT 4071 TERM
COUR 88 'ecr8_gp8' ECRO COMP 8 GAUS 8 ELEM LECT 4071 TERM
COUR 89 'ecr8_gp9' ECRO COMP 8 GAUS 9 ELEM LECT 4071 TERM
TRAC 81 82 83 84 85 86 87 88 89 AXES 1.0 'EPSZ [-]' YZER

COUR 111 'con1_gp1' CONT COMP 1 GAUS 1 ELEM LECT 4071 TERM
COUR 112 'con1_gp2' CONT COMP 1 GAUS 2 ELEM LECT 4071 TERM
COUR 113 'con1_gp3' CONT COMP 1 GAUS 3 ELEM LECT 4071 TERM
COUR 114 'con1_gp4' CONT COMP 1 GAUS 4 ELEM LECT 4071 TERM
COUR 115 'con1_gp5' CONT COMP 1 GAUS 5 ELEM LECT 4071 TERM
COUR 116 'con1_gp6' CONT COMP 1 GAUS 6 ELEM LECT 4071 TERM
COUR 117 'con1_gp7' CONT COMP 1 GAUS 7 ELEM LECT 4071 TERM
COUR 118 'con1_gp8' CONT COMP 1 GAUS 8 ELEM LECT 4071 TERM
COUR 119 'con1_gp9' CONT COMP 1 GAUS 9 ELEM LECT 4071 TERM
TRAC 111 112 113 114 115 116 117 118 119 AXES 1.0 'SX [PA]' YZER

COUR 121 'con2_gp1' CONT COMP 2 GAUS 1 ELEM LECT 4071 TERM
COUR 122 'con2_gp2' CONT COMP 2 GAUS 2 ELEM LECT 4071 TERM
COUR 123 'con2_gp3' CONT COMP 2 GAUS 3 ELEM LECT 4071 TERM
COUR 124 'con2_gp4' CONT COMP 2 GAUS 4 ELEM LECT 4071 TERM
COUR 125 'con2_gp5' CONT COMP 2 GAUS 5 ELEM LECT 4071 TERM
COUR 126 'con2_gp6' CONT COMP 2 GAUS 6 ELEM LECT 4071 TERM
COUR 127 'con2_gp7' CONT COMP 2 GAUS 7 ELEM LECT 4071 TERM
COUR 128 'con2_gp8' CONT COMP 2 GAUS 8 ELEM LECT 4071 TERM
COUR 129 'con2_gp9' CONT COMP 2 GAUS 9 ELEM LECT 4071 TERM
TRAC 121 122 123 124 125 126 127 128 129 AXES 1.0 'SY [PA]' YZER

COUR 131 'con3_gp1' CONT COMP 3 GAUS 1 ELEM LECT 4071 TERM
COUR 132 'con3_gp2' CONT COMP 3 GAUS 2 ELEM LECT 4071 TERM
COUR 133 'con3_gp3' CONT COMP 3 GAUS 3 ELEM LECT 4071 TERM
COUR 134 'con3_gp4' CONT COMP 3 GAUS 4 ELEM LECT 4071 TERM
COUR 135 'con3_gp5' CONT COMP 3 GAUS 5 ELEM LECT 4071 TERM
COUR 136 'con3_gp6' CONT COMP 3 GAUS 6 ELEM LECT 4071 TERM
COUR 137 'con3_gp7' CONT COMP 3 GAUS 7 ELEM LECT 4071 TERM
COUR 138 'con3_gp8' CONT COMP 3 GAUS 8 ELEM LECT 4071 TERM
COUR 139 'con3_gp9' CONT COMP 3 GAUS 9 ELEM LECT 4071 TERM
TRAC 131 132 133 134 135 136 137 138 139 AXES 1.0 'SXY [PA]' YZER

COUR 141 'con4_gp1' CONT COMP 4 GAUS 1 ELEM LECT 4071 TERM
COUR 142 'con4_gp2' CONT COMP 4 GAUS 2 ELEM LECT 4071 TERM
COUR 143 'con4_gp3' CONT COMP 4 GAUS 3 ELEM LECT 4071 TERM
COUR 144 'con4_gp4' CONT COMP 4 GAUS 4 ELEM LECT 4071 TERM
COUR 145 'con4_gp5' CONT COMP 4 GAUS 5 ELEM LECT 4071 TERM
COUR 146 'con4_gp6' CONT COMP 4 GAUS 6 ELEM LECT 4071 TERM
COUR 147 'con4_gp7' CONT COMP 4 GAUS 7 ELEM LECT 4071 TERM
COUR 148 'con4_gp8' CONT COMP 4 GAUS 8 ELEM LECT 4071 TERM
COUR 149 'con4_gp9' CONT COMP 4 GAUS 9 ELEM LECT 4071 TERM
TRAC 141 142 143 144 145 146 147 148 149 AXES 1.0 'SZ [PA]' YZER

FIN

```

q9m_03.epx

Q9M_03
ECHO
! CONV WIN
CAST mesh
DPLA
GEOM Q92 sur92 Q93 sur93 TERM
COMP EPAI 1. LECT sur9 TERM
NGRO 3
'noeuds_sym' LECT elpeau9 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau9 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau9 TERM COND Y LT 0.05
COUL VERT LECT sur92 TERM
ROUG LECT sur93 TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.0014133837990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.011812993922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850858379881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur9 TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPLA 2 -1. PONC 1 LECT noeuds_haut TERM
PINB SELP DMIN 0.1 LECT elpeau9 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PAS AUTO
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

RESU SPLI ALIC 'q9m_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1

PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
! NAVIGATION MODE: ROTATING CAMERA
! CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
! RSPHERE : 1.27387E+01
! RADIUS : 4.84072E+01
! ASPECT : 1.00000E+00
! NEAR : 3.56685E+01
! FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECRO 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
SUPP LECT sur9 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1
OBJE LECT sur9 TERM REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL
OBJE LECT sur9 TERM REND
GO
TRAC OFFS FICH AVI CONT
OBJE LECT sur9 TERM REND
ENDPLAY

FIN

q9m_03c.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1

PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
! NAVIGATION MODE: ROTATING CAMERA
! CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
! RSPHERE : 1.27387E+01
! RADIUS : 4.84072E+01
! ASPECT : 1.00000E+00
! NEAR : 3.56685E+01
! FAR : 7.38847E+01
SCEN GEOM NAVI FREE
! LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY

FIN

q9m_03a.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_03.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1

PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
! NAVIGATION MODE: ROTATING CAMERA
! CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
! RSPHERE : 1.27387E+01
! RADIUS : 4.84072E+01
! ASPECT : 1.00000E+00
! NEAR : 3.56685E+01
! FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 201 FPS 25 KFPE 10 COMP -1 REND
FREQ 1
GOTR LOOP 199 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY

FIN

q9m_03d.epx

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_03.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_1226' DEPL COMP 2 NOEU LECT 1226 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'f' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'f' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'f' FICH 'car401d.pun' RENA 'f' q4
RCOU 24 'f' FICH 'q93_02d.pun' RENA 'f' q94
RCOU 34 'f' FICH 'q93_03d.pun' RENA 'f' q93
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
XMIN 0 XMAX 2 DX 0.2 YMIN 0 YMAX 800 DY 100
COLO NOIR ROUG VERT TURQ
COUR 5 'dt' DTI
TRAC 5 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
LIST 5 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
RCOU 35 'dt' FICH 'q93_03d.pun' RENA 'dt' q93
TRAC 5 35 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
COLO ROUG NOIR
FIN

q9m_03b.epx

Post treatment (visualization from alice file)
ECHO

q9m_04.epx

Q9M_03
ECHO
! CONV WIN

```

CAST mesh
DPLA
GEOM Q92 sur92 Q93 sur93 TERM
COMP EPAI 1. LECT sur9 TERM
NGRO 3
'noeuds_sym' LECT elpeau9 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau9 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau9 TERM COND Y LT 0.05
COUL VERT LECT sur92 TERM
ROUG LECT sur93 TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.0055502897212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur9 TERM
LINK COUP SPLIT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPLA 2 -1. FONC 1 LECT noeuds_haut TERM
PINB SELF DMIN 0.1 LECT elpeau9 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TFRE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TFRE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PART PLIN
PASM 1.0E-12
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

```

q9m_04a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_04.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
!
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
HIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 46 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 44 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----
FIN

```

q9m_04b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_04.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01

```

```

! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
HIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECR0 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
SUPP LECT sur9 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 46 FPS 25 KFRE 10 COMP -1
OBJE LECT sur9 TERM REND
FREQ 1
GOTR LOOP 44 OFFS FICH AVI CONT NOCL
OBJE LECT sur9 TERM REND
GO
TRAC OFFS FICH AVI CONT
OBJE LECT sur9 TERM REND
ENDPLAY
*-----
FIN

```

q9m_04c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_04.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*-----
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
!
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
HIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NFTP 46 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 44 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*-----
FIN

```

q9m_04d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_04.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_1226' DEPL COMP 2 NOEU LECT 1226 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'f' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'f' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'f' FICH 'car401d.pun' RENA 'f'g4'
RCOU 24 'f' FICH 'q93_02d.pun' RENA 'f'gq4'
RCOU 34 'f' FICH 'q93_03d.pun' RENA 'f'gq3'
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
XMIN 0 XMAX 2 DX 0.2 YMIN 0 YMAX 800 DY 100
COLO NOIR ROUG VERT TURQ
COUR 5 'dt' DT1
TRAC 5 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
LIST 5 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
RCOU 35 'dt' FICH 'q93_03d.pun' RENA 'dt_q93'
RCOU 45 'dt' FICH 'q9m_03d.pun' RENA 'dt_q9m_03'
TRAC 5 35 45 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
COLO ROUG NOIR VERT
FIN

```

q9m_05.epx

```

Q9M_05
ECHO
!CONV WIN
CAST mesh
DPLA
GEOM Q92 sur92 Q93 sur93 TERM
COMP EPAI 1. LECT sur9 TERM
NGRO 3

```

```

'noeuds_sym' LECT elpeau9 TERM COND X GT 14.95
'noeuds_haut' LECT elpeau9 TERM COND Y GT 16.95
'noeuds_bas' LECT elpeau9 TERM COND Y LT 0.05
COUL VERT LECT sur92 TERM
ROUG LECT sur93 TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525306343725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.850853879881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489508018 2.0122406624245
5336.94734929116 10.0270088428608
LECT sur9 TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
DEPLA 2 -1. FONC 1 LECT noeuds_haut TERM
PINB SELP DMIN 0.1 LECT elpeau9 TERM
FONC 1 TABL 4 0. 0. 0.0001 0. 1.0001 1. 100.0001 100.
ECRI DEPL TPFE 0.1 POIN LECT 4460 TERM
FICH SPLI ALIC TPFE 0.05
REGI 'HAUT' TOUT POIN LECT noeuds_haut TERM
'BAS' TOUT POIN LECT noeuds_bas TERM
OPTI PART PLIN
CSTA 0.5
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.0 DTMI 1.E-12 DTMA 1.E-04 TFIN 10.0 NMAX 900000000
FIN

```

q9m_05a.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_05.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 120 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 118 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

q9m_05b.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_05.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01

```

```

!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
LINE HEOU SFRE
ISO FILL FIEL ECR0 3 SCAL USER PROG 0.05 PAS 0.05 0.7 TERM
SUPP LECT sur9 TERM
TEXT ISCA
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 120 FPS 25 KFRE 10 COMP -1
OBJE LECT sur9 TERM REND
FREQ 1
GOTR LOOP 118 OFFS FICH AVI CONT NOCL
OBJE LECT sur9 TERM REND
GO
TRAC OFFS FICH AVI CONT
OBJE LECT sur9 TERM REND
ENDPLAY
*=====
FIN

```

q9m_05c.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_05.ali' GARD PSCR
OPTI PRIN
SORT VISU NSTO 1
*=====
PLAY
CAME 1 EYE 5.56399E+00 8.50620E+00 4.84072E+01
! Q 1.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
VIEW 0.00000E+00 0.00000E+00 -1.00000E+00
RIGH 1.00000E+00 0.00000E+00 0.00000E+00
UP 0.00000E+00 1.00000E+00 0.00000E+00
FOV 2.48819E+01
!NAVIGATION MODE: ROTATING CAMERA
!CENTER : 5.56399E+00 8.50620E+00 0.00000E+00
!RSPHERE: 1.27387E+01
!RADIUS : 4.84072E+01
!ASPECT : 1.00000E+00
!NEAR : 3.56685E+01
!FAR : 7.38847E+01
SCEN GEOM NAVI FREE
!LINE HEOU SFRE
FACE HFRO
PINB CDES
COLO PAPE
SLER CAM1 1 NFRA 1
TRAC OFFS FICH AVI NOCL NPTO 120 FPS 25 KFRE 10 COMP -1 REND
FREQ 1
GOTR LOOP 118 OFFS FICH AVI CONT NOCL REND
GO
TRAC OFFS FICH AVI CONT REND
ENDPLAY
*=====
FIN

```

q9m_05d.epx

```

Post treatment (visualization from alice file)
ECHO
RESU SPLI ALIC 'q9m_05.ali' GARD PSCR
OPTI PRIN
SORT GRAP
AXTE 1.0 'Time [ms]'
COUR 1 'dy_1226' DEPL COMP 2 NOEU LECT 1226 TERM
COUR 2 'dy' MULC 1 -1.0
COUR 3 'fyt' FLIA COMP 2 ZONE LECT noeuds_haut TERM
COUR 4 'fyt' FLIA COMP 2 ZONE LECT noeuds_bas TERM
TRAC 2 AXES 1.0 'DISPL. [MM]' YZER XGRD YGRD
TRAC 3 4 AXES 1.0 'FORCE [N]'
LIST 3 4 AXES 1.0 'FORCE [N]'
TRAC 4 AXES 1.0 'FORCE [N]' XAXE 2 1.0 'DISPL. [MM]' YZER XGRD YGRD
RCOU 14 'fyt' FICH 'car401d.pun' RENA 'fyt_q4'
RCOU 24 'fyt' FICH 'q93_02d.pun' RENA 'fyt_q9q4'
RCOU 34 'fyt' FICH 'q93_03d.pun' RENA 'fyt_q93'
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
COLO NOIR ROUG VERT TURQ
TRAC 4 14 24 34 AXES 1.0 'FORCE [N]' YZER XGRD YGRD
XMIN 0 XMAX 2 DX 0.2 YMIN 0 YMAX 800 DY 100
COLO NOIR ROUG VERT TURQ
COUR 5 'dt' DT1
TRAC 5 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
LIST 5 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
RCOU 35 'dt' FICH 'q93_03d.pun' RENA 'dt_q93'
RCOU 45 'dt' FICH 'q9m_03d.pun' RENA 'dt_q9m_03'
RCOU 55 'dt' FICH 'q9m_04d.pun' RENA 'dt_q9m_04'
TRAC 5 35 45 55 AXES 1.0 'DELTAT [S]' YZER XGRD YGRD
COLO ROUG NOIR VERT TURQ
FIN

```

readq4.dgibi

```

opti echo 1;
opti dime 2 elem qua4;
opti trac psc ftra 'readq4_mesh.ps';
opti sauv form 'mesh_q4.msh';
sur4 = read 'mesh4.write' mesh elem;
trac qual sur4;
tol = 0.0001;

nodlag = cont sur4;
elepin = sur4 elem appu larg nodlag;
elim tol (sur4 et nodlag);
trac qual nodlag;

```

```

trac qual elepin;

mesh = sur4;

tass mesh;
sauv form mesh;
fin;

readq4a.dgibi
opti echo 1;
opti donn 'pxq42q92.proc';
opti donn 'pxq92q4.proc';
opti dime 2 elem qua4;
opti trac psc ftra 'readq4_mesh.ps';
opti sauv form 'mesh_g9q4.msh';
sur4 = read 'mesh4.write' mesh elem;
trac qual sur4;

```

```

i = 0;
repe loop1 (nbel sur4);
  i = i + 1;
  q4i = sur4 elem i;
  q9i = pxq42q92 q4i;
  si (ega i 1);
  sur9 = q9i;
  sinon;
  sur9 = sur9 et q9i;
  fin;
fin loop1;

tol = 0.001;

elim tol (sur4 et sur9);
trac qual sur9;

peau9 = cont sur9;
trac qual peau9;

elpeau9 = sur9 elem appu larg peau9;
trac qual elpeau9;

i = 0;
repe loop2 (nbel elpeau9);
  i = i + 1;
  q9i = elpeau9 elem i;
  q44i = pxq92q4 q9i;
  si (ega i 1);
  sur4p = q44i;
  sinon;
  sur4p = sur4p et q44i;
  fin;
fin loop2;

trac qual sur4p;

mesh = sur9 et sur4p;
elim tol mesh;

trac qual mesh;

tass mesh;
sauv form mesh;
fin;

```

readq4q9mixed.dgibi

```

opti echo 1;
opti donn 'pxq42q92.proc';
opti dime 2 elem qua4;
opti trac psc ftra 'readq4_mesh.ps';
opti sauv form 'mesh_g9mixed.msh';
sur4 = read 'mesh4.write' mesh elem;
trac qual sur4;

i = 0;
repe loop1 (nbel sur4);
  i = i + 1;
  q4i = sur4 elem i;
  q9i = pxq42q92 q4i;
  si (ega i 1);
  sur9 = q9i;
  sinon;
  sur9 = sur9 et q9i;
  fin;
fin loop1;

tol = 0.001;

elim tol (sur4 et sur9);

trac qual sur9;

peau9 = cont sur9;
trac qual peau9;

elpeau9 = sur9 elem appu larg peau9;
trac qual elpeau9;

i = 0;
n = 0;
j = 0;
repe loop3 (nbel sur9);
  i = i + 1;
  j = j + 1;
  si (ega j 5);
  q9i = sur9 elem i;
  n = n + 1;
  si (ega n 1);
  sur93 = q9i;
  sinon;
  sur93 = sur93 et q9i;
  fin;

```

```

j = 0;
fin;
fin loop3;
sur92 = diff sur9 sur93;

mesh = sur9;
elim tol mesh;

trac qual mesh;
trac qual sur93;
trac qual sur92;

tass mesh;
sauv form mesh;
fin;

```

self01.epx

```

SELF01
ECHO
CONV WIN
CAST mesh
LAGR DPLA
GEOM Q42L mesh TERM
COMP EPAI 1. LECT mesh TERM
NGRO 3
'noeuds_sym' LECT mesh TERM COND X LT 0.1
'noeuds_haut' LECT mesh TERM COND Y GT 11.9
'noeuds_bas' LECT mesh TERM COND Y LT 0.1
COUL VERT LECT mesh TERM
MATE VM23 RO 0.00825 YOUN 197600.0 NU 0.29 ELAS 222.35
TRAC 39
222.35 0.00112525303643725
228.192645571222 0.00117982108082602
230.758344471793 0.001217805387003
234.450726613396 0.00128649153144431
239.764555869277 0.00141338337990525
243.897432663364 0.00153429874829638
247.411863292444 0.00165208432840306
250.528021456793 0.00176785435959915
253.359622970924 0.00188218432677593
258.417356319849 0.00210778014331907
262.901922592959 0.00233047531676599
272.525831528572 0.00287917930935512
280.709612952488 0.00342059520724944
306.337249091751 0.00555028972212425
326.269365384357 0.00765116075599371
358.247494301277 0.0118129933922129
390.499112131117 0.0169762100816352
417.924578503771 0.0221150029276507
464.338948360747 0.0323498934633641
503.807844043327 0.0425496348382759
538.803931461142 0.0527267405438317
570.604298738599 0.0628876735766123
599.971697212392 0.0730362940142328
627.405291846074 0.0831751279951724
653.253096704044 0.0933059367242108
677.76931865327 0.103430006673347
734.395540393597 0.128716576621425
785.85085379881 0.153976978005465
833.369446403083 0.179217456712566
877.759003278812 0.204442100219022
959.251671749752 0.254854512508855
1033.30271513801 0.305229264752723
1165.57077256009 0.405898637512956
1282.84956691385 0.506492153678714
1389.41887249881 0.607031472026816
1579.77020835558 0.807994788503824
1748.55 1.00884893724696
2418.75489580018 2.0122406624245
5336.94734929116 10.0270088428608
LECT mesh TERM
LINK COUP SPLT NONE
BLOQ 2 LECT noeuds_bas TERM
BLOQ 1 LECT noeuds_sym TERM
VITE 2 -1.0 FONC 1 LECT noeuds_haut TERM
PINB BODY MLEV 2 LECT plaq1 TERM
SELF MLEV 2 LECT ring TERM
BODY MLEV 2 LECT plaq2 TERM
FONC 1 TABL 2 0 100 100 100
INIT VITE 2 -100 LECT noeuds_haut TERM
ECRI DEPL TPRE 0.1 POIN LECT 1 TERM
FICH ALIC FREQ 1
OPTI PAS AUTO
LOG 1
PINS GRID DGRI EQVF
CALC TINI 0.0 TFIN 80.E-3
FIN

```

test03.wxm

```

/* [wxMaxima batch file version 1] [ DO NOT EDIT BY HAND! ]*/
/* [ Created with wxMaxima version 13.04.2 ] */

/* [wxMaxima: input start ] */
L1x : (1/2)*x*(x-1);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
L2x : (1+x)*(1-x);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
L3x : (1/2)*x*(x+1);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
L1y : (1/2)*y*(y-1);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
L2y : (1+y)*(1-y);
/* [wxMaxima: input end ] */

```

```

/* [wxMaxima: input start ] */
L3y : (1/2)*y*(y+1);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
L1z : (1/2)*z*(z-1);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
L2z : (1+z)*(1-z);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
L3z : (1/2)*z*(z+1);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N1 : L1x*L1y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N2 : L3x*L1y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N3 : L3x*L3y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N4 : L1x*L3y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N5 : L1x*L1y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N6 : L3x*L1y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N7 : L3x*L3y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N8 : L1x*L3y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N9 : L2x*L2y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N10 : L2x*L1y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N11 : L3x*L2y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N12 : L2x*L3y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N13 : L1x*L2y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N14 : L2x*L2y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N15 : L2x*L1y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N16 : L3x*L2y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N17 : L2x*L3y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N18 : L1x*L2y*L1z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N19 : L1x*L1y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N20 : L3x*L1y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N21 : L3x*L3y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N22 : L1x*L3y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N23 : L2x*L1y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N24 : L3x*L2y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N25 : L2x*L3y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N26 : L1x*L2y*L3z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
N27 : L2x*L2y*L2z;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
Sx : N1*a1+N2*a2+N3*a3+N4*a4+N5*a5+N6*a6+N7*a7+N8*a8+N9*a9+
N10*a10+N11*a11+N12*a12+N13*a13+N14*a14+N15*a15+N16*a16+N17*a17+N18*a18+
N19*a19+N20*a20+N21*a21+N22*a22+N23*a23+N24*a24+N25*a25+N26*a26+N27*a27;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
Sy : N1*b1+N2*b2+N3*b3+N4*b4+N5*b5+N6*b6+N7*b7+N8*b8+N9*b9+
N10*b10+N11*b11+N12*b12+N13*b13+N14*b14+N15*b15+N16*b16+N17*b17+N18*b18+
N19*b19+N20*b20+N21*b21+N22*b22+N23*b23+N24*b24+N25*b25+N26*b26+N27*b27;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
Sz : N1*c1+N2*c2+N3*c3+N4*c4+N5*c5+N6*c6+N7*c7+N8*c8+N9*c9+
N10*c10+N11*c11+N12*c12+N13*c13+N14*c14+N15*c15+N16*c16+N17*c17+N18*c18+
N19*c19+N20*c20+N21*c21+N22*c22+N23*c23+N24*c24+N25*c25+N26*c26+N27*c27;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
Sx8 : 8*Sx;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
Sy8 : 8*Sy;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
Sz8 : 8*Sz;
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
expand(Sx8);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
expand(Sy8);
/* [wxMaxima: input end ] */

/* [wxMaxima: input start ] */
expand(Sz8);
/* [wxMaxima: input end ] */

/* Maxima can't load/batch files which end with a comment! */
"Created with wxMaxima"$

```

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Abstract

Contact-impact algorithms are an important component of numerical simulation software in fast transient dynamics. Traditionally, contact algorithms have been based on so-called sliding lines and sliding surfaces. However, sliding-based algorithms may present some difficulties in detecting contact in complex geometrical situations, especially in 3D. The pinball contact-impact method as an alternative formulation has been implemented in EUROPLEXUS, initially based upon a strong Lagrange-multiplier based solution strategy of the contact constraints.

Recently, at Onera Lille (F) some crash calculations involving many contacts were attempted, initially with linear-displacement continuum elements (CAR4 in 2D). However, to improve accuracy and to help mitigate spurious locking phenomena, it was desired to perform the same calculations with parabolic elements, namely by the 9-node Lagrange element Q93.

The present work considers two different approaches to modeling contact with parabolic elements. The first approach uses a phantom mesh of linear-displacement elements, used only for contact detection, and superposed to the structural mesh made of parabolic elements. Such a technique is fully general and could be useful also in other special contact situations, not only with parabolic elements. The second approach is based on a (new) 'native' pinball formulation for the parabolic elements, which has now been developed and implemented in EUROPLEXUS.

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