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Robust level-set-based inverse lithography

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Abstract: Level-set based inverse lithography technology (ILT) treats photomask design for microlithography as an inverse mathematical problem, interpreted with a time-dependent model, and then solved as a partial differential equation with finite difference schemes. This paper focuses on developing level-set based ILT for partially coherent systems, and upon that an expectation-oriented optimization framework weighting the cost function by random process condition variables. These include defocus and aberration to enhance robustness of layout patterns against process variations. Results demonstrating the benefits of defocus-aberration-aware level-set based ILT are presented.

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OCIS codes: (110.3960) Microlithography; (110.5220) Photolithography; (110.1758) Computational imaging.

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1. Introduction

Optical projection lithography remains the predominant microlithography technology until the foreseeable future as shrinkage of integrated circuit device dimension outpaces introduction of shorter-exposure wavelengths and higher-numerical-aperture lenses extending to sub-0.35 k_1 regime and minimum design pitches to sub-100nm. Due to the wave nature of light, as dimensions approach sizes comparable to or smaller than the wavelength of the light used in the photolithography process, the bandlimited imaging system introduces undesirable distortions and artifacts. Along the way, resolution enhancement techniques (RET) [1, 2] are essential in optical lithography, which include modified illumination schemes and optical proximity correction (OPC). The latter predistorts the mask patterns such that printed patterns are as close to the desired shapes as possible. Rule-based OPC [3, 4], in which various geometries are treated by different empirical rules, and model-based OPC, which is more complex and involves the

computation of a weighted sum of pre-simulated results for simple edges and corners that are stored in a library, are two main approaches to OPC. Moving beyond model-based OPC, inverse lithography technology (ILT) is becoming a strong candidate for 32nm and below low- k_1 regime.

Inverse model-based techniques invert the imaging model and attempt to directly synthesize the optimized mask pattern, and are not constrained by the topology of the original design [5]. Early works include branch and bound algorithm [6] and the “bacteria” algorithm [7] with very limited applicability due to their high computation complexity. Since the mid-1990s, iterative methods have been applied to generate binary masks [8] and phase shifting masks (PSMs) [9, 10, 11], treating the problem as an inverse problem and solving it by an optimization process. Meanwhile, Poonawala and Milanfar designed a model-based OPC system and developed a faster optimization algorithm using steepest-descent [12, 13], which has been further improved by Chan et al. using an active set method and conjugate gradient [11, 14]. Applications of ILT are also reported in pixelated mask technology [15], double exposure lithography [16], manufacturability enhancement [17] and designs specifically taking into account robustness to variations, such as focal length [18].

Level-set method [19] offers a feasible alternative to inverse lithography. It has been applied in “forward” optical lithography [20] and inverse imaging problems [21] involving obstacles [22, 23], and in nonlinear deblurring and noise removal [24]. Level set approaches for ILT has been explored in [5, 25], and in [26], Shen et al. presented systematic level-set formulations and developed finite-difference schemes to solve them with high fidelity and robustness for a coherent imaging system. It should also be noted while the above-mentioned algorithms enrich the weaponry for solving inverse lithography problems, the current performance still falls short, and is not yet fully applicable to real-world manufacturing [27, 28]. One such concern is that they are mostly applied to calculate solutions under nominal conditions, without taking process variation into account. Consequently, various efforts have been made to incorporate process conditions such as defocus and aberration variations into OPC algorithms for robust design of printed patterns [29, 30].

This paper focuses on the development of algorithms for photomask synthesis using level-set based inverse lithography problem in partially coherent systems. A statistical method is proposed to incorporate process variations into the optimization framework, which treats defocus and aberrations as random variables, taking their statistical properties into account, and develops an optimization framework which aims to minimize the pattern difference between the printed wafer upon various defocus and aberration conditions and the target pattern. A complete set of level-set formulations of the optimization problem is provided with computationally efficient solutions.

2. The Constrained level set time-dependent model formulation

2.1. Mathematical model for partially coherent systems

The projection lithography imaging process can be described as a forward model

$$I(\mathbf{x}) = \mathcal{T}\{U(\mathbf{x})\}, \quad (1)$$

where the boldface \mathbf{x} denotes spatial coordinates (x,y) , and $\mathcal{T}\{\cdot\}$ maps the input intensity function $U(\mathbf{x})$ to the output intensity function $I(\mathbf{x})$. Due to the lowpass nature of the optical lithography imaging system, $I(\mathbf{x})$ is typically a blurred version of $U(\mathbf{x})$. Suppose the desired circuit pattern is $I_0(\mathbf{x})$. The objective of inverse lithography is to find a predistorted input intensity function $\hat{U}(\mathbf{x})$ which minimizes its distance with the desired output, i.e.,

$$\hat{U}(\mathbf{x}) = \arg \min_{U(\mathbf{x})} d(I_0(\mathbf{x}), \mathcal{T}\{U(\mathbf{x})\}), \quad (2)$$

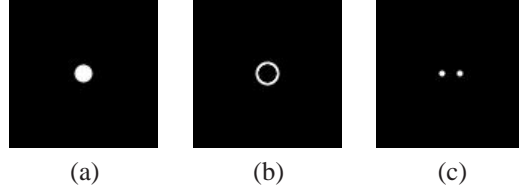


Fig. 1. Common illumination sources: (a) conventional, (b) annular, and (c) dipole.

in which $d(\cdot, \cdot)$ is an appropriately defined distance metric, such as the ℓ_2 norm.

The lithography process $\mathcal{S}\{\cdot\}$ in Eq. (1) can be divided into two functional blocks, namely the projection optics effects (aerial image formation) and resist effects. The resist effects can be approximated using a logarithmic sigmoid function [13]

$$\text{sig}(U(\mathbf{x})) = \frac{1}{1 + e^{-a(U(\mathbf{x}) - t_r)}}, \quad (3)$$

with a being the steepness of the sigmoid and t_r being the threshold.

The nonlinear nature of aerial image formation in partially coherent systems has been understood since the early development of optical coherence theory [31, 32], but the complexity of the calculations involved has limited use of the theory for actual optical design. In partially coherent imaging, the mask is illuminated by light traveling in various directions. In [33], the concept of effective source is developed to help understand the mechanism of partially coherent imaging. Radiation of partially coherent light has been shown to be an expansion of coherent modes added incoherently in the image plane. The expansion uses a basis of orthogonal functions which are eigenfunctions of the mutual coherence function [34], however, computation of the eigenfunctions is a difficult process which leads to complicated functions and expensive computation complexity in terms of both speed and memory requirement. Alternatively, the Fourier expansion model [35, 36] is applied to decompose the partially coherent imaging systems as the sum of coherent systems.

According to the Hopkins diffraction model, the light intensity distribution exposed on the wafer in partially coherent imaging is bilinear and can be described as

$$I_{\text{aerial}}(\mathbf{x}) = \int \int_{-\infty}^{\infty} U^*(\mathbf{x}_1)U(\mathbf{x}_2)\gamma(\mathbf{x}_1 - \mathbf{x}_2)H^*(\mathbf{x} - \mathbf{x}_1)H(\mathbf{x} - \mathbf{x}_2) d\mathbf{x}_1 d\mathbf{x}_2, \quad (4)$$

where $\mathbf{x} = (x, y)$, $\mathbf{x}_1 = (x_1, y_1)$ and $\mathbf{x}_2 = (x_2, y_2)$. $U(\mathbf{x})$ is the mask pattern, $\gamma(\mathbf{x}_1 - \mathbf{x}_2)$ is the complex degree of coherence and $H(\mathbf{x})$ represents the amplitude impulse response of the optical system, namely point spread function (PSF). The term $\gamma(\mathbf{x}_1 - \mathbf{x}_2)$ is generally a complex number, whose magnitude represents the extent of optical interaction between two spatial locations $\mathbf{x}_1 = (x_1, y_1)$ and $\mathbf{x}_2 = (x_2, y_2)$ of the light source. It is the inverse Fourier transform of the image of the illumination shape $\Gamma(\mathbf{x})$ in the lens pupil. Common illumination sources are shown in Fig. 1, which include conventional circular, annular, and dipole, all introducing partial coherence into illumination.

If the object intensity vanishes outside a square area A defined by $\mathbf{x} \in [-\frac{G}{2}, \frac{G}{2}]$, for computations involved in (4), the only values of $\gamma(\mathbf{x})$ needed are those inside the square area A_γ defined by $\mathbf{x} \in [-G, G]$. We can expand $\gamma(\mathbf{x})$ as a 2-D Fourier series of periodicity $2G$ in both the x and y directions, and therefore, $\gamma(\mathbf{x})$ can be rewritten as

$$\gamma(\mathbf{x}) = \sum_{\mathbf{m}} \Gamma_{\mathbf{m}} e^{j\omega_0 \mathbf{m} \cdot \mathbf{x}}, \quad (5)$$

and also

$$\Gamma_{\mathbf{m}} = \frac{1}{G^2} \int_{A_\gamma} \gamma(\mathbf{x}) e^{j\omega_0 \mathbf{m} \cdot \mathbf{x}} d\mathbf{x}, \quad (6)$$

where $j = \sqrt{-1}$, $\omega_0 = \pi/G$, $\mathbf{m} = (m_x, m_y)$, m_x and m_y being integers within the range of $[-D, D]$, and $\mathbf{m} \cdot \mathbf{x} = m_x x + m_y y$. Substituting (5) into (4), the light intensity on the wafer is given by

$$I_{\text{aerial}}(\mathbf{x}) = \sum_{\mathbf{m}} \Gamma_{\mathbf{m}} |U(\mathbf{x}) * H_{\mathbf{m}}(\mathbf{x})|^2, \quad (7)$$

where

$$H_{\mathbf{m}}(\mathbf{x}) = H(\mathbf{x}) e^{j\omega_0 \mathbf{m} \cdot \mathbf{x}}. \quad (8)$$

Combining the aerial image formation in (7) and the logarithmic sigmoid function in (3) describing resist effects, we have the image formation equation for a partially coherent imaging system as

$$I(\mathbf{x}) = \text{sig}\left(\sum_{\mathbf{m}} \Gamma_{\mathbf{m}} |U(\mathbf{x}) * H_{\mathbf{m}}(\mathbf{x})|^2\right). \quad (9)$$

It is observed from (7) that the partially coherent image is equal to the superposition of coherent systems. In what follows, we will drop the arguments \mathbf{x} whenever there is no ambiguity.

2.2. Time-dependent model formulation in partially coherent imaging

Development of the time-dependent scheme in partially coherent imaging is in principle similar to that in coherent imaging [26]. The inverse lithography problem can be treated as an obstacle reconstruction problem [22, 23], which is an inverse problem involving obstacles where the desired unknown is a region consisting of several subregions. We give U a level set description by introducing an unknown function $\phi(\mathbf{x})$, which is related to U by defining

$$U(\mathbf{x}) = \begin{cases} U_{\text{int}} & \text{for } \{\mathbf{x} : \phi(\mathbf{x}) < 0\} \\ U_{\text{ext}} & \text{for } \{\mathbf{x} : \phi(\mathbf{x}) > 0\} \end{cases}, \quad (10)$$

where $U_{\text{int}} = 1$ and $U_{\text{ext}} = 0$ if we are dealing with binary masks. Now we can define the inverse lithography problem as finding $\phi(\mathbf{x})$ such that $\mathcal{I}(U) \approx I_0$. Solving this with a least squares fit to the approximation is equivalent to seeking the minimizer of

$$F(U) = \frac{1}{2} |\mathcal{I}(U) - I_0|^2. \quad (11)$$

The boundary of the subregions in U where $U = U_{\text{int}}$ is governed by the zero level set of ϕ , namely, $\phi(\mathbf{x}) = 0$. If ϕ depends on both \mathbf{x} and time t such that the evolution of the subregions in U is associated with $\phi(\mathbf{x}, t)$, following the steps in [26], we arrive at the time-dependent model

$$\frac{\partial \phi}{\partial t} = -|\nabla \phi| \alpha(\mathbf{x}, t), \quad (12)$$

with $\alpha(\mathbf{x}, t)$ being defined as

$$\begin{aligned} \alpha(\mathbf{x}, t) &= -J(U)^T (\mathcal{I}(U) - I_0) \\ &= \frac{1}{2} \frac{\partial}{\partial U} (I - I_0)^2 \\ &= \frac{1}{2} \frac{\partial}{\partial U} \left(\text{sig}\left(\sum_{\mathbf{m}} \Gamma_{\mathbf{m}} |U * H_{\mathbf{m}}|^2\right) - I_0 \right)^2 \\ &= a \left\{ \sum_{\mathbf{m}} \Gamma_{\mathbf{m}} H_{\mathbf{m}} * [(I_0 - I) \odot I \odot (1 - I) \odot (H_{\mathbf{m}} * U)] \right\}, \end{aligned} \quad (13)$$

where $J(U)$ is the Jacobian of $\mathcal{F}(U)$ at U and \odot denotes element-by-element multiplication. Eq. (12) is a partial differential equation (PDE). Once ϕ and α are defined at every grid point on the Cartesian grid, Eq. (12) can be solved using finite-difference methods with first-order temporal and second-order spatial accuracy as suggested in [26]. It should be noted the inverse lithography problem is non-convex with multiple local minima. Since we use finite-difference schemes to solve the PDE, there is no guarantee of reaching the global minimum. However, ILT is an ill-posed problem and it is often not necessary to arrive at the global minimum. Any good local minimum (where goodness is defined using data-fidelity and user-defined properties) can suffice as an acceptable solution.

2.3. Aberration-aware statistical model

We have thus far assumed nominal conditions where the image always lies on the focal plane and the image wavefronts is spherical. However, in optical lithography, the emerging wavefronts from the pupil are in general aspherical [34], even if the lens surfaces are spherical. Deviation of wavefronts, also known as aberration, is studied extensively in the Nijboer-Zernike theory [37, 38, 39]. Aberration function Φ can be represented as Zernike polynomials [39],

$$\Phi(\rho, \theta) = \sum_{n,m} c_n^m R_n^m(\rho) \cos m\theta, \quad (14)$$

where ρ, θ are the polar coordinates in the exit pupil function, and $c_n^m R_n^m(\rho) \cos m\theta$ is a polynomial of the Zernike set with c_n^m being aberration coefficient. For example, one of the most widely studied aberrations, defocus [34], or the focus error f between the image plane and focal plane, can be expressed as $f = c_2^0 \rho^2$ where c_2^0 is the aberration coefficient for defocus. As a reasonable assumption, the coefficients are modeled as independent, normally distributed random variables with zero mean and identical non-zero variance. PSF in an ideal case where there exists no defocus and aberrations is taken as the inverse Fourier transform of a disc function [34], denoted as H_0 in this paper. Aberration terms are incorporated into the PSF by multiplying an exponential term with aberration function as power in the frequency domain, i.e. [37]

$$\mathcal{F}(H) = \mathcal{F}(H_0) \times e^{j\Phi}, \quad (15)$$

where \mathcal{F} denotes Fourier transform.

To enable the computation of optimum mask patterns minimizing deviation of images from their targets not only at nominal but also over a range of aberrations, the objective function takes expectations of the difference under various aberration conditions to optimize the average performance of layouts. The optimization problem we aim to solve becomes

$$U_{\text{optimal}} = \min_U \mathcal{E} \{ \|I - I_0\|_2^2 \}, \quad (16)$$

where $\|\cdot\|_2^2$ denotes the square of the ℓ_2 norm and \mathcal{E} denotes expectation. One should note this expectation-orient minimizing problem practically weights the cost function $\|I - I_0\|_2^2$ by the statistical probability of aberration terms appearing over a range. Previous efforts in [18, 29, 30] developed various algorithms to solve the inverse lithography problem in Eq.(16). Yet in the framework of level-set-based ILT in partially coherent systems, a stable explicit time-dependent model can be applied,

$$\frac{\partial \phi}{\partial t} = -|\nabla \phi| \alpha(\mathbf{x}, t), \quad (17)$$

in which $\alpha(\mathbf{x}, t)$ is computed as

$$\begin{aligned}
\alpha(\mathbf{x}, t) &= \frac{1}{2} \frac{\partial}{\partial U} \mathcal{E} \{ (I - I_0)^2 \} \\
&= \frac{1}{2} \frac{\partial}{\partial U} \mathcal{E} \left\{ \left(\text{sig} \left(\sum_{\mathbf{m}} \Gamma_{\mathbf{m}} |U * H_{\mathbf{m}}|^2 \right) - I_0 \right)^2 \right\} \\
&= a \times \mathcal{E} \left\{ \sum_{\mathbf{m}} \Gamma_{\mathbf{m}} H_{\mathbf{m}} * [(I_0 - I) \odot I \odot (1 - I) \odot (H_{\mathbf{m}} * U)] \right\}. \quad (18)
\end{aligned}$$

One should notice that Eq. (17) takes the same form as Eq. (12) with a different computation of $\alpha(\mathbf{x}, t)$, therefore Eq. (17) is also a PDE which could be solved by the proposed finite difference schemes in [26]. The computation stops after a certain number of iterations or when the value of the cost function has decreased below a certain threshold value.

3. Numerical results

We apply the inverse lithography technique outlined above to designing various circuit patterns for partially coherent systems. We use the same imaging system parameters: $\lambda = 193\text{nm}$, $NA = 1.35$, resolution $\Delta x = 10\text{nm/pixel}$, steepness of the sigmoid function $a = 85$, threshold $t_r = 0.3$, and therefore the same PSF $H_0(\mathbf{x})$ with the same size as that of the target pattern which is 101×101 for various experiments. The optimization stops after 50 iterations. In this paper, we apply the proposed algorithms on binary masks. However, it should be noted the same framework can be readily applied to phase-shifting masks (PSMs) by applying different levels sets to corresponding phases in the PSMs. Figure. 2(a) shows the target pattern, and (b), (c) and (d) are the output patterns under circular, annular, and dipole source illuminations in Fig. 1(a), (b) and (c), respectively. Respective pattern errors are also given.

In Fig. 3, input pattern derived using the proposed level-set based ILT in partially coherent imaging under nominal condition with circular, annular and dipole illumination are presented. The first column denotes the input pattern, the second column aerial image and the third column the output pattern. Combining the data in Fig. 2 and Fig. 3, we can see that the input pattern developed using the proposed level-set based ILT greatly improves pattern quality in partially coherent imaging systems under commonly used illumination sources.

Another set of simulation is given in Fig. 4 applying the proposed statistical method to target pattern in Fig. 2(a) with circular source in Fig. 1(a) as an example to test its effectiveness against aberrations. It should be noted that the optimal input mask pattern is computed by averaging the output patterns under different aberration conditions weighted by the statistical probability of the aberration coefficient. Consequently, for any specific aberration, PSF $H(\mathbf{x})$ should be computed by degrading $H_0(\mathbf{x})$ with aberrations as in Eq. (15). For defocus aberration, conventionally, the relationship between the defocus coefficient c_2^0 and the real image space coordinate z by paraxial approximation can be described as [39]

$$c_2^0 = 2 \frac{\pi}{\lambda} z \left(1 - \sqrt{(1 - NA^2)} \right) \approx z \frac{\pi NA^2}{\lambda}, \quad (19)$$

therefore, defocus term is incorporated into the amplitude spread function $H(\mathbf{x})$ by multiplying

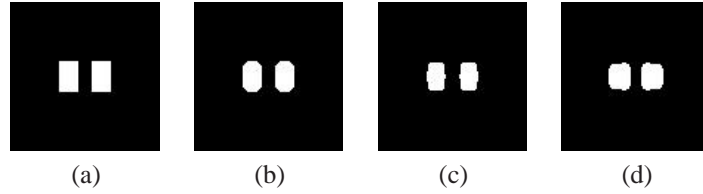


Fig. 2. (a) Target pattern of size 101×101 . (b) Output pattern under circular source, resulting in a pattern error of 45 pixels. (c) Output pattern under annular source, resulting in a pattern error of 116 pixels. (d) Output pattern under dipole source, resulting in a pattern error of 144 pixels.

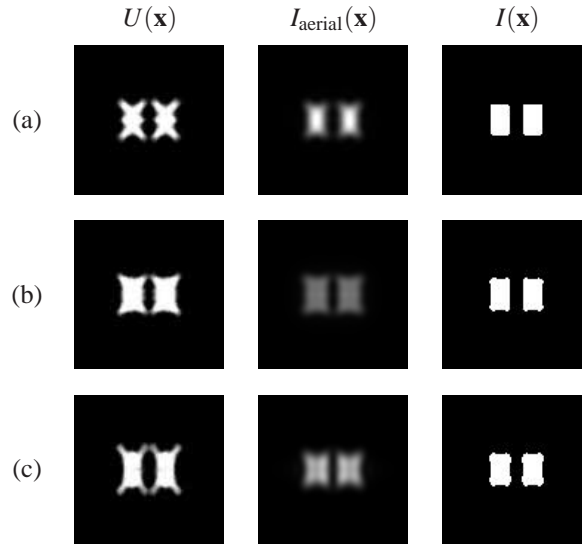


Fig. 3. Simulation of lithographic imaging with different mask patterns computed using level-set based ILT. The first column denotes the input $U(\mathbf{x})$, the second column $I_{\text{aerial}}(\mathbf{x})$, and the third column $I(\mathbf{x})$. Rows (a), (b) and (c) use the derived pattern under circular illumination, annular illumination, and dipole illumination as input, resulting in pattern errors of 5, 24, and 45 pixels respectively.

an exponential term with power,

$$\begin{aligned}
 jc_2^0 \rho^2 &\approx j\pi z \frac{NA^2}{\lambda} \rho^2 = j\pi z \frac{NA^2}{\lambda} \left[\left(u \frac{\lambda}{NA} \right)^2 + \left(v \frac{\lambda}{NA} \right)^2 \right] \\
 &= j\pi \lambda z (u^2 + v^2) \\
 &= j\pi \lambda z \left[\left(m \frac{1}{N\Delta x} \right)^2 + \left(n \frac{1}{N\Delta x} \right)^2 \right] \\
 &= j\pi \lambda z \frac{m^2 + n^2}{(N\Delta x)^2}, \tag{20}
 \end{aligned}$$

in which N is the image size and (u, v) and (m, n) are the frequency coordinates and normal-

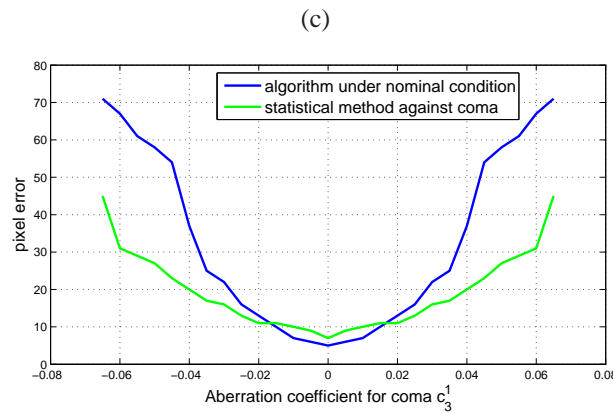
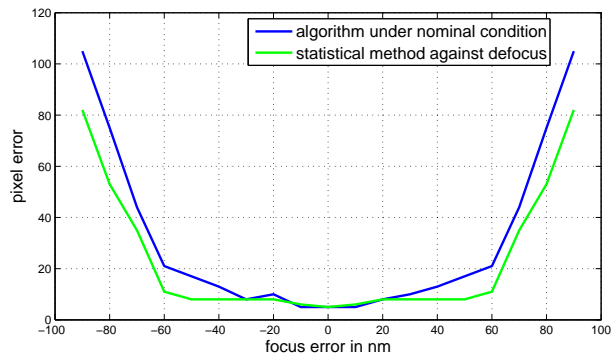


Fig. 4. Performances of the proposed level-set based statistical method with aberration variations. (a) focus-aware input mask pattern computed using the statistical method. (b) coma-aware input mask pattern computed using the statistical method. (c) Comparison of pixel errors under different focus errors. (d) Comparison of pixel errors under different coma.

ized frequency coordinates corresponding to spatial coordinates (x, y) respectively, in the frequency domain of the nominal PSF $H_0(\mathbf{x})$. We first construct the optimal input mask pattern with defocus variation using the statistical method described in Section 2.3 and then compare the generated results with that of the optimal input mask pattern constructed under nominal conditions presented in $U(\mathbf{x})$ of Fig. 3(a). The optimal input mask pattern with defocus variation is presented in Fig. 4(a). It should be noted that since we are not introducing large aberration parameters and small weights accompany large aberration parameters, big difference in mask patterns obtained under nominal condition and using the statistical method in Fig. 4(a) is not expected. Figure. 4(c) plots the performance of the statistical method versus optimization only under nominal conditions with a defocus range of (-90nm, 90nm). It is observed that while under nominal conditions, the optimal input mask pattern under nominal condition outperforms the input mask computed using the statistical method, which is not a surprise since the former is intended specifically for nominal conditions and the latter is not, the input mask computed with statistical variability accounted for improves pattern fidelity with focus variation, obtaining fewer pattern errors than the optimal input mask pattern computed under the nominal condition. This is because the expectation operation tends to compensate the distortion brought by different defocus conditions on the input pattern mask. In Fig. 4(b), the input mask computed with statistical identity of coma variation accounted for is presented. The Zernike polynomial for coma is given as $c_3^1(3\rho^3 - 2\rho) \cos \theta$, and coma term can be incorporated into the PSF $H(\mathbf{x})$ by multiplying nominal PSF $H_0(\mathbf{x})$ with an exponential term with power,

$$\begin{aligned}
jc_3^1(3\rho^3 - 2\rho) \cos \theta &= \\
&= jc_3^1 \left[3 \left(\sqrt{\left(\frac{u\lambda}{NA}\right)^2 + \left(\frac{v\lambda}{NA}\right)^2} \right)^3 - 2 \sqrt{\left(\frac{u\lambda}{NA}\right)^2 + \left(\frac{v\lambda}{NA}\right)^2} \right] \cos \theta \\
&= jc_3^1 \left[3 \frac{\lambda^3}{NA^3} (u^2 + v^2)^{\frac{3}{2}} - 2 \frac{\lambda}{NA} (u^2 + v^2)^{\frac{1}{2}} \right] \cos \theta \\
&= jc_3^1 \left[3 \frac{\lambda^3}{(N\Delta x NA)^3} (m^2 + n^2)^{\frac{3}{2}} - 2 \frac{\lambda}{N\Delta x NA} (m^2 + n^2)^{\frac{1}{2}} \right] \cos \theta. \quad (21)
\end{aligned}$$

Figure. 4(d) plots the performance of the statistical method versus optimization only under nominal conditions with a coma range c_3^1 of (-0.08, 0.08). Likewise, we observe similar results in Fig. 4(d) as that in Fig. 4(c). These observations justify the proposed statistical algorithm in producing aberration-aware input mask pattern for critical structures.

It should be noted that when two or more aberrations are present, the root mean square deformation of the combined aberration $\Delta\Phi_{rms} = \sqrt{\sum_{n,m} c_n^{m2}}$ becomes a chi-square distributed random variable with degree of freedom equal to the number of Zernike polynomials in the combined aberration. Incorporating aberration terms in the ASF similarly as in Eq. (20) and Eq. (21), the proposed algorithm can produce aberration-aware input masks against this combined aberration using the proposed level-set-based statistical method.

4. Conclusion

In this paper, we investigate level-set formulations for photomask design in optical microlithography for partially coherent systems with computationally efficient solutions. The inverse lithography problem is described as a constrained time-dependent model with the form of a partial differential equation which is solved by available finite-difference schemes. The proposed level-set-based ILT enables computation of optimum mask patterns to minimize deviations of

images from their targets not only at nominal but also over a range of aberrations. The statistical optimization framework proposed in this paper offers algorithmic insights of how the cost functions are weighted by statistical probability of aberration coefficients to optimize average layout performance which shows great robustness against aberrations.

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