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Optimization of a multi-channel transmit, Quadrature Receive Birdcage Coil

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Introduction:

Although ultra high field (7T to 9.4T) MRI has signal-to-noise ratio (SNR) advantages, the associated RF inhomogeneity is a challenge for some applications. This is mainly caused by RF wavelength effects [1]. Some methods for reducing transmit \mathbf{B}_1^+ field inhomogeneity [2-3] of multi-channel coils are proposed by varying amplitude and phase of individual driving ports. Normally, it is difficult to use the same method for receive of birdcage-like volume coils. In this work, we optimize by varying amplitude and phase of multiple driving voltages during transmission, and quadrature reception is used for a multi-port birdcage-like volume coil. For comparison, a conventional transceiver quadrature birdcage coil is also investigated. The optimization procedure is based on a set of \mathbf{B}_1^+ field of all modes of 12-rung birdcage loaded with a sphere phantom. They are used to estimate the modes distribution of the desired \mathbf{B}_1^+ (homogeneous) field, and then the port voltage distribution of each port, with singular value decomposition (SVD) method.

Methods:

Normally, there are n resonant modes and $(1+n/2)$ resonant frequencies for an n -rung birdcage coil. But we can generate all resonance modes at the same resonance frequency by controlling the amplitude and phases of driving voltage of each port for a multi-channel birdcage-like coil, regardless of the degree of degeneracy. The finite-difference time-domain (FDTD) method is used to calculate the transient \mathbf{B}_1 fields of each resonant mode through time-dependent Maxwell's equations at resonant frequency of 300MHz. A region of interest (ROI), $26 \times 26 \times 28 \text{ cm}^3$ is divided into a mesh of 2,366,000 Yee cells, where the basic element of 3D meshes in FDTD method is 2 mm/cell in each dimension. A 12-rung birdcage coil (20-cm i.d. and 21-cm length) is modeled in the ROI. The conductivity of copper ($5.95 \times 10^7 \text{ S/m}$) is assigned to the coil cells. Voltage sources are placed at each rung to model capacitors and driving ports. The phantom is a sphere with 16cm diameter ($\epsilon_r = 51.898$, $\sigma = 0.553 \text{ s/m}$) which represents average brain tissue at 300MHz. Transmit \mathbf{B}_1^+ fields and receive \mathbf{B}_1^- fields of each mode are calculated from two sets of transient \mathbf{B}_1 fields which are a quarter period apart in time [4]. The target \mathbf{B}_1^+ is assumed as a homogeneous $1.17 \mu\text{T}$ (for 5ms duration 90° pulse). By using SVD method, the coefficients of the mode distributions and the port voltage distribution for generating desired \mathbf{B}_1^+ field can be obtained [3]. For comparison, SNR of conventional transceiver birdcage and optimized multi-port birdcage are calculated by Eq.(1) [5], where τ is pulse duration, γ is gyromagnetic ratio, ρ is material density. The \mathbf{B}_1^- fields for both cases (calculated based on model1) are the same.

$$SNR \propto \frac{\sum_N \left| \sin(\gamma\tau) \left| \bar{B}_{1n}^+ \right| \left| \bar{B}_{1n}^- \right| \right|}{\sqrt{\sum_N SAR_n \times \rho_n \times \Delta V}} \quad (1)$$

Results:

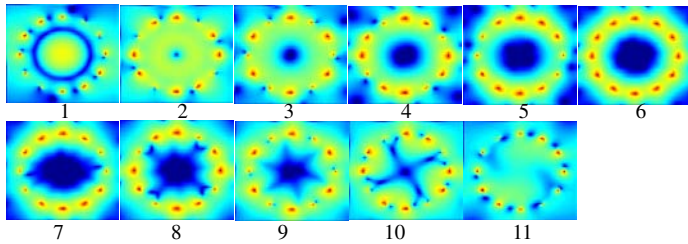


Fig.1, Amplitude patterns of 11 modes \mathbf{B}_1^+ field (phase patterns are not shown here)

The \mathbf{B}_1^+ field of the 11 modes for the 12-rung birdcage coil are shown in Fig.1 (the rung current is 0 for mode 0 of birdcage). The \mathbf{B}_1^+ field of mode 1, which is the operational mode for conventional birdcage, is extracted and shown in details in Fig.2. The 'peak' at center indicates wavelength effects. The \mathbf{B}_1^+ field of the multi-channel birdcage optimized by SVD method is illustrated in Fig. 3. The percentages of the samples on axial plane having a \mathbf{B}_1^+ field magnitude within $\pm 10\%$ of the average \mathbf{B}_1^+ field magnitude on that plane are 23.47% and 80.06% for conventional quadrature birdcage and optimized multi-channel birdcage-like coil, respectively. The homogeneity of \mathbf{B}_1^+ field improves dramatically by optimization. Compared with the SAR of conventional birdcage (2.72W/kg), the SAR of the optimized multi-channel birdcage increased slightly to 3.04 W/kg. After normalization, the relative SNR on central axial plane for conventional birdcage and optimized multi-channel birdcage are 1 and 1.73 respectively. The simulated image intensity of phantom is shown in Fig.4. Although the phantom in this work is homogeneous, this method also can fully handle heterogeneous samples.

Conclusions:

Compared with conventional transceiver quadrature birdcage, optimized multi-channel-transmit, quadrature-receive birdcage coil has dramatically improved \mathbf{B}_1^+ field homogeneity and relative SNR, with slight penalty of increased average SAR.

References:

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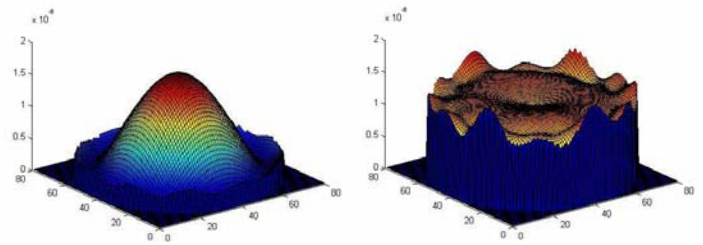


Fig.2 Non-optimized \mathbf{B}_1^+ field profile of conventional Birdcage (mode 1)

Fig.3 Optimized \mathbf{B}_1^+ field profile of multi-port driving Birdcage

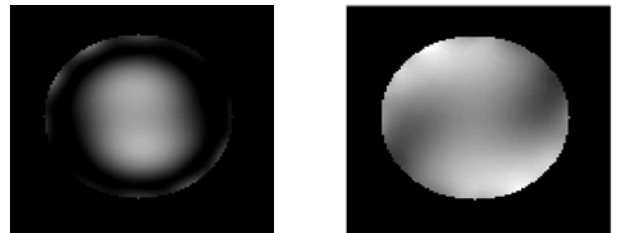


Fig.4, Axial signal intensity distributions for sphere phantom in conventional quadrature birdcage (left) and multi-port birdcage-like coils with optimized driving voltage distribution (right) at 300MHz

	\mathbf{B}_1^+ homogeneity within 10% variety*	Average SAR (W/kg)	Normalized SNR
Quadrature Birdcage	23.47%	2.72	1
Optimized multi-port coil	80.06%	3.04	1.73

Table11. \mathbf{B}_1^+ , SAR and SNR comparison for conventional birdcage and optimized multi-channel birdcage. *The percentages of samples on axial plane having \mathbf{B}_1^+ field magnitude within $\pm 10\%$ of the average \mathbf{B}_1^+ field magnitude on that plane