1	Running into fatigue: The effects of footwear on kinematics, kinetics, and energetics
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25 ABSTRACT

Purpose: Recent studies identified a redistribution of positive mechanical work from distal to 26 proximal joints during prolonged runs, which might partly explain the reduced running 27 economy observed with running-induced fatigue. Higher mechanical demand of plantar flexor 28 muscle-tendon-units, e.g., through minimal footwear, can lead to an earlier onset of fatigue, 29 which might affect the redistribution of lower extremity joint work during prolonged runs. 30 31 Therefore, the purpose of this study was to examine the effects of a racing-flat and cushioned running shoe on the joint-specific contributions to lower extremity joint work during a 32 33 prolonged fatiguing run.

Methods: On different days, eighteen runners performed two 10-km runs with near-maximal effort in a racing-flat and a cushioned shoe on an instrumented treadmill synchronized with a motion-capture-system. Joint kinetics and kinematics were calculated at 13 pre-determined distances throughout the run. The effects of shoes, distance, and their interaction were analyzed using a two-factor repeated-measures ANOVA.

Results: For both shoes, we found a redistribution of positive joint work from ankle (-6%) to knee (+3%) and hip (+3%) throughout the entire run. Negative ankle joint work was higher (p<0.01) with the racing-flat compared to the cushioned shoe. Initial differences in foot-strike patterns between shoes disappeared after 2 km of running distance.

43 Conclusion: Irrespective of the shoe design, alterations in the running mechanics occurred in 44 the first 2 km of the run, which might be attributed to the existence of a habituation rather than 45 fatigue effect. While we did not find a difference between shoes in the fatigue-related 46 redistribution of joint work from distal to more proximal joints, more systematical studies are 47 needed to explore the effects of specific footwear design features.

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- 49 Key Words: SHOE, ANKLE, JOINT TORQUE, RUNNING ENHANCEMENT, RUNNING
- 50 ECONOMY, RUNNING MECHANICS, HEELSTRIKE PATTERN

51 INTRODUCTION

Running economy is an essential predictor of distance running performance and is defined by the metabolic cost for a given submaximal running velocity (1). Running economy declines with running-induced fatigue, which is, among other factors, related to changes in running mechanics (2–5). In a recent publication, we demonstrated that energy generation shifts partly from distal to proximal joints during a near-maximal effort 10-km run, which likely has a detrimental effect on running economy because more proximal joints are less equipped for efficient energy generation (6).

Previous studies suggest that changes in running mechanics are not always in a linear relationship with running distance and sometimes exhibit a higher rate of change in the beginning compared to later stages of an exhausting run (7,8). In our previous work (6), we also observed a nonlinear response to the running distance, e.g., in the positive work of the ankle, knee, and hip joints as well as the flexion angle and torque of the knee. However, we did not analyze these qualitatively observed nonlinearities in detail.

We speculate that at least two processes influence the changes in running mechanics with 65 running distance: habituation and fatigue. Habituation might occur in the early stages of a run 66 to harmonize the current state of a runner's neuromuscular system with the running 67 environment, e.g., footwear or surface, and the requirements of the run (running distance and 68 velocity). On the other hand, fatigue is defined as the exercise-induced reduction in the ability 69 70 to generate muscle force or power due to changes in the neural drive or exhaustion of contractile function (9) and might, therefore, affect running mechanics during later stages of prolonged 71 runs. However, studies addressing running mechanics, especially joint kinetics, throughout 72 fatiguing runs are rare (10), and therefore, knowledge about the potential influence of 73 habituation and fatigue is limited. 74

Next to habituation and fatigue, footwear can also affect the running kinematics and 75 kinetics within the lower extremities (8,11–16). When assessed in an unfatigued state, running 76 with minimal footwear (very flexible, reduced cushioning, drop height, and mass compared to 77 cushioned running shoes) places a higher mechanical demand (higher joint torques, negative 78 power, and work) on the plantar flexor muscle-tendon-units in comparison to wearing more 79 cushioned shoes (13,15,17–19). However, whether this higher mechanical demand on ankle 80 81 plantar flexors in an unfatigued state amplifies the previously reported fatigue induced redistribution of joint work from the ankle towards more proximal joints throughout a fatiguing 82 83 run (6) is currently not known.

Running shoes are predominantly characterized by their mass, built-in cushioning 84 materials, longitudinal bending stiffness as well as motion control technologies incorporated 85 86 underneath the medial longitudinal arch (20–22). These design features not only affect running kinematics and kinetics but also running economy (22–24). A recent study demonstrated that 87 a prototype shoe incorporating a highly compliant and resilient midsole material with a full-88 length carbon-fiber plate was able to improve running economy on average by 4% (25). This 89 improvement appears to be partly due to superior energy storage within the midsole foam 90 material and reduced ankle plantarflexion torque (26). In case this lower mechanical 91 plantarflexion demand in the unfatigued state (26) would affect the fatigue-induced 92 93 redistribution of joint work, an additional pathway for the improvement of running economy 94 with cushioned running shoes may be conceivable.

Therefore, the purpose of this study was to investigate the difference between a typical racing flat shoe and a typical cushioned running shoe with regards to joint-specific contributions to lower extremity joint work during a fatiguing 10-km run with a near-maximal effort in rearfoot runners. We hypothesized that using a racing flat shoe in comparison to a cushioned shoe leads to a more pronounced and earlier fatigue-related redistribution of positive

work from distal to proximal joints during a fatiguing near-maximal effort run. This hypothesis 100 was motivated by the findings that wearing racing flat shoes requires a higher mechanical 101 demand at the ankle compared to cushioned shoes (13,15,19,26). Furthermore, we 102 hypothesized that separating a fatiguing near-maximal effort run into a habituation and fatigue 103 phase will reveal markedly larger changes in biomechanical parameters in the initial 104 habituation compared to the fatigue phase of running. The findings of the present study will 105 106 improve the understanding of habituation- and fatigue-related alterations in running mechanics and their interaction with footwear design in prolonged fatiguing runs. 107

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109 METHODS

110 **Participants**

We recruited a total of eighteen male competitive (n = 6) and recreational (n = 12) long-111 distance runners (age 24.4 \pm 3.7 years; body height 1.83 \pm 0.06 m; body mass 77.1 \pm 8.3 kg) 112 with a season-best time between 34:00 min and 54:30 min in a 10-km run. These eighteen 113 runners were a subset of the participants of a previous study (6) and were selected because they 114 showed a habitual rearfoot strike landing pattern during shod running. We focused the analysis 115 on rearfoot runners since we expected that cushioning systems would have the strongest effect 116 in this type of footfall pattern. All participants stated that they had experience in the use of 117 racing flats and cushioned shoes as well as running on a treadmill. Further, they were free of 118 119 any musculoskeletal injuries or impairments for at least the prior twelve months. Each participant signed informed written consent before participation. The University Ethics 120 Committee had approved the study protocol (No. 102/2017), and the protocol met all 121 requirements for human experimentation following the Declaration of Helsinki. 122

123

124 **Experimental protocol**

In a cross-sectional study design, all participants performed two separate 10-km treadmill 125 runs with near-maximal effort (105% of their season-best time throughout the 10-km distance 126 with an average running velocity of $3.6 \pm 1.1 \text{ m} \cdot \text{s}^{-1}$) as described in our previous study (6) with 127 at least seven recovery days between the runs. Participants used a different shoe type for each 128 run in a randomized order. Seven days before the first run, participants performed a run with a 129 self-determined running velocity and duration to familiarize themselves with both shoes and 130 131 the treadmill. Before each run, the participants executed a warm-up run in the test shoe at a self-determined running velocity with a duration of at least 5 minutes. The participants were 132 133 continuously encouraged and kept informed of the covered distance during both runs.

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135 Footwear properties

All participants wore two shoe types (Fig. 1, I). The first shoe condition (shoe_{Racing}) was a typical racing flat shoe (Adizero Pro 4, Adidas AG, Herzogenaurach, Germany) with a shoe mass of 0.170 kg (size: US 10). The other shoe condition (shoe_{Cushion}) was a typical cushioned running shoe without any additional support elements underneath the medial longitudinal arch of the foot (Glycerin 10, Brooks Sports Inc., Seattle, Washington, USA) with a shoe mass of 0.348 kg (size: US 10) (Fig. 1, I).

Both shoes underwent the 'Minimal Shoe Index' test (20), which indicates the minimalism of a running shoe. The 'Minimalist Shoe Index' describes shoes on a scale ranging from 1 (no minimalism at all) to 100 (perfectly minimal footwear). We found a score of 60 for shoe_{Racing}, and 18 for shoe_{Cushion} (see Appendix, Supplemental Table 1, 'Minimal Shoe Index' test).

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147 *** Insert Fig. 1 about here ***

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We performed two mechanical tests to evaluate the midsole material properties of theshoes in an unused state (Fig. 1, II and III).

In order to test longitudinal bending stiffness, each shoe was fixed on a rearfoot shoe last 151 which we had mounted on a moving apparatus (low-friction ball bearing sled) in a material 152 testing machine (Z020; Zwick GmbH & Co.KG, Ulm, Germany) to allow for a natural bending 153 behavior (Fig. 1, II). The longitudinal bending stiffness we tested is related to the bending 154 155 behavior of the forefoot and midfoot part of the shoe. The material testing machine executed 20 cycles with a vertical displacement of 50 mm and a vertical velocity of 15 mm \cdot s⁻¹. 156 157 Longitudinal bending stiffness was calculated by dividing vertical force by vertical displacement. Maximal bending stiffness and vertical force results were averaged over 20 158 cycles (Fig. 1, II). 159

To quantify cushioning properties of the midsole material, we mounted a rigid rearfoot-160 form in a material testing machine (Z020; Zwick GmbH & Co.KG, Ulm, Germany) and 161 compressed the midsole in a vertical direction with 2000 N (Fig. 1, III). This load is similar to 162 the average maximal vertical ground-reaction force (GRF) during stance phases in this study. 163 We calculated the mechanical energy stored and returned for both shoe conditions at a constant 164 compression velocity of 16 mm·s⁻¹ (Fig. 1, III). The mechanical test revealed a significant 165 difference between the shoe conditions in the deformation (shoe_{Racing} 10.1 mm vs. shoe_{Cushion} 166 13.6 mm) as well as the resilience values (energy return in shoe_{Racing} 63.9% vs. shoe_{Cushion} 167 73.1%) (Fig. 1, III), which are comparable to similar shoes reported in the literature (25). 168

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170 Running kinematics and kinetics

We captured joint kinematics with a 13 infrared camera motion capture system (250 Hz,
MX-F40; Vicon Motion Systems, Oxford, UK) and collected GRF data with four threedimensional force transducers (1000 Hz, MC3A-3-500-4876; AMTI Inc., Watertown, USA)

embedded in a single-belt treadmill (Treadmetrix, Park City, USA) synchronized with the 174 motion capture system. We attached the markers of the foot over the anatomical landmarks on 175 the upper of the shoe. All marker trajectories and GRF data were filtered with a recursive 4th 176 order Butterworth low-pass filter (cutoff frequency: 20 Hz) (27). As described in our previous 177 study (6), a three-dimensional inverse dynamics model of the total body was used to calculate 178 the kinematic and kinetic parameters of the lower extremity (28). The upright standing position 179 180 determined the neutral position of all joints (0° joint angles). We expressed joint torques in the anatomical coordinate system of the proximal segment. Throughout the entire stance phase, the 181 182 negative and positive work at the ankle, knee, and hip joint were calculated by numerical integration of the power-time curve. Positive work was determined by summing all positive 183 integrals and negative work by summing all negative integrals (29). 184

All spatiotemporal, joint kinematic, and joint kinetic parameters were determined during 185 the stance phase of the right leg and averaged over 20 stance phases at each of the 13 distances 186 (0 km, 0.2 km, 0.5 km, 1 km, and following each kilometer to 10 km). Firstly, we calculated 187 ankle dorsiflexion and knee joint flexion angles at foot touch-down (TD) as well as ankle 188 plantarflexion at toe-off (TO). In addition, to assess the footfall pattern of the runners, we 189 determined the angle between the foot and the treadmill surface at TD (foot- TS_{TD}). 190 Furthermore, we determined maximal joint angles and calculated maximal external joint 191 torques of ankle dorsiflexion, knee and hip flexion. We normalized maximal external joint 192 193 torques as well as negative and positive work at the ankle, knee, and hip joint to body mass. Subsequently, the relative joint-specific contributions to the total lower-extremity joint work 194 were calculated. All analyses were performed for the sagittal plane, separately for each 195 196 individual joint, as described in our previous studies (6,28).

At the end of the run, we determined the maximal heart rate (M51; Polar Electro, Kempele,
Finland), and the rating of perceived exertion using the Borg 6 – 20 scale (30).

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200 Statistical analysis

We used a two-factor repeated-measure analysis of variance (ANOVA) to detect possible main and interaction effects with two within-subjects factors (shoe condition and running distance). We calculated partial eta squared (η_p^2) as normalized effect size measure, which explains the proportion of the total variance related to main and interaction effects (shoe condition and running distance). The suggested norms from Cohen (31) were used for η_p^2 with 0.01 representing small, 0.06 medium, and 0.14 large effect.

In the case of a shoe condition main effect, we applied pairwise post-hoc comparisons using Fisher's least significant difference correction between the shoe conditions at each of the 13 distances. With respect to two intervals, we performed post-hoc tests for each parameter, regardless of whether we found a running distance main effect. We selected a first distance interval (0 - 2 km) in an attempt to capture habituation (HAB) effects based on qualitative observations in our previous study (6) and earlier findings (7,8). We considered the second distance interval (2 - 10 km) in an attempt to capture fatigue (FAT) processes.

To assess the validity of our assumption that the changes observed with running distance are related to habituation and fatigue processes, we fit different types of models to the results observed over running distance. We used three different models: A simple linear model (all data: 0 - 10 km), a quadratic model (all data: 0 - 10 km), and a bi-linear model (twocomponents: 0 - 2 km, and 2 - 10 km). We then calculated the sum of squared errors for each model as a measure of model fit.

All statistical analyses were performed using SPSS Statistics 23 (IBM Corp., Armonk, NY, USA) with the level of significance set at $\alpha = 0.05$. We present all results in the text and figures as group means and standard deviations.

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RESULTS 224

Heart rate and rating of perceived exertion 225

At the end of the run, we found no significant shoe main effect for heart rate (shoe_{Racing}: 226 176 ± 15 BPM; shoe_{Cushion}: 179 ± 15 BPM) and rating of perceived exertion (16.9 ± 1.3 ; 16.9227 \pm 1.7), respectively. 228

229

230 **Spatiotemporal parameters**

No significant shoe by distance interaction effects were found for spatiotemporal 231 232 parameters (Table 1). A significant shoe main effect was found for step frequency (Table 1), where step frequency was on average higher for shoe_{Racing} $(2.75 \pm 0.16 \text{ Hz})$ compared to 233 shoe_{Cushion} (2.72 ± 0.15 Hz), and for flight time (Table 1), which was on average shorter for 234 shoe_{Racing} (0.126 \pm 0.025 s) compared to shoe_{Cushion} (0.129 \pm 0.024 s). A significant distance 235 main effect was found for contact time, step length, and step frequency (Table 1). Contact time 236 and step length increased with running distance while step frequency decreased irrespective of 237 the shoe condition (see Appendix, Supplemental Table 2, Spatiotemporal parameters; 238 Supplemental Fig. 1 and 2, Fitting methods). 239

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*** Insert Table 1 about here *** 241

242

Joint work 243

No significant shoe by distance interaction effects or shoe main effects for any joint work 244 parameter other than for the negative work at the ankle were observed (Table 1), which was on 245 average 0.043 J·kg⁻¹ (corresponds to approx. 7%) higher with shoe_{Racing} throughout the entire 246 run than with shoe_{Cushion} (see Appendix, Supplemental Fig. 3, Joint work). Even though no 247 significant shoe main effect for the negative knee joint work was found (Table 1), it was 248

noticeable that the difference between both shoes throughout the entire run (negative knee joint work was on average $0.038 \text{ J}\cdot\text{kg}^{-1}$ smaller for shoe_{Racing} compared to shoe_{Cushion}) was similar to the difference in the negative work at the ankle joint (see Appendix, Supplemental Fig. 3, Joint work). Accordingly, we found a difference in relative contributions of the ankle and knee joint to the total negative lower-extremity joint work between the shoe conditions (Fig. 2; see Appendix, Supplemental Table 3, Relative joint work).

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- 256 *** Insert Fig. 2 about here ***
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Concerning the running distance, significant main effects were found for the positive work 258 at the ankle, knee, and hip joint, as well as for the negative work at the ankle joint (Table 1). 259 Irrespective of the shoe condition, we found that the positive work at the ankle joint decreased 260 significantly (P < 0.001) as well as the knee and hip joint increased significantly (knee: P < 0.001) 261 0.001; hip: 0.012 < P < 0.025) from the beginning (mean value of both shoe conditions for the 262 ankle: $0.68 \pm 0.12 \text{ J}\cdot\text{kg}^{-1}$; knee: $0.36 \pm 0.09 \text{ J}\cdot\text{kg}^{-1}$; hip: $0.26 \pm 0.13 \text{ J}\cdot\text{kg}^{-1}$) to the end of the run 263 (ankle: $0.61 \pm 0.14 \text{ J}\cdot\text{kg}^{-1}$; knee: $0.41 \pm 0.10 \text{ J}\cdot\text{kg}^{-1}$; hip: $0.30 \pm 0.16 \text{ J}\cdot\text{kg}^{-1}$). Detailed values for 264 each shoe condition can be found in the Appendix (Supplemental Fig. 3, Joint work). 265 Accordingly, independent of the shoe condition, we found a redistribution of relative positive 266 work from distal to proximal joints from the beginning (ankle 53.0%, knee 28.1%, hip 19.0%) 267 to the end of the run (46.9%, 31.2%, 21.9%). For more specific values please see Fig. 2 and 268 the Appendix (Supplemental Table 3, Relative joint work). 269

During the HAB phase, negative work at the ankle increased significantly (P = 0.031) for shoe_{Cushion} (Table 1; Fig. 3). For shoe_{Racing}, negative work at the knee and hip joint increased significantly (P < 0.05) during the HAB phase (Table 1; Fig. 3). Positive work at the ankle decreased significantly (P < 0.01) in the HAB and FAT phase, independent of the shoe

274	condition (Table 1; Fig. 3). The positive work at the knee and hip joint showed significant (P
275	< 0.05) increases only for the HAB phase irrespective of the shoe condition (Table 1; Fig. 3).
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277 *** Insert Fig. 3 about here ***

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279 Footwear differences at the beginning of the run

We identified several kinematic and kinetic differences between the shoe conditions at the beginning of the run, indicating a more plantarflexed foot strike pattern for shoe_{Racing} and a higher mechanical demand placed on plantar flexor muscle-tendon-units.

Specifically, at the 0-km distance we found a significantly (P = 0.012) higher negative 283 work at the ankle with shoe_{Racing} compared to shoe_{Cushion} (see Appendix, Supplemental Table 284 4, Pairwise comparisons between shoes; Supplemental Fig. 3, Joint work). The maximal ankle 285 dorsiflexion torque was higher for shoe_{Racing} compared to shoe_{Cushion}, but this difference was 286 not significant (P = 0.163) at the 0-km distance, but then significant (P = 0.034) at 0.2 km (Fig. 287 4). At the 0-km distance, the foot-TS_{TD} (P = 0.010), ankle dorsiflexion angle at TD (P < 0.001) 288 (Fig. 5), and maximal ankle dorsiflexion angle (P = 0.008) with shoe_{Racing} was decreased 289 significantly compared to shoe_{Cushion} (see Appendix, Supplemental Fig. 4, Maximal joint 290 angle). However, at the 0-km distance, the ankle plantarflexion angle at TO with shoe_{Racing} was 291 increased significantly (P = 0.002) compared to shoe_{Cushion} (Fig. 5). 292

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294 External joint torques

We could neither identify a shoe by distance interaction effect nor a significant shoe main effect for any joint torque parameters, but significant running distance main effects for all joint torques were found (Table 1). Maximal ankle dorsiflexion torque decreased significantly (P < 0.05) over the entire run for both shoe conditions (Fig. 4), although it should be noted that P = 0.05 for the FAT phase using shoe_{Cushion} (Table 1) and so this difference was not strictly significant. For both shoe conditions, a significant (P < 0.01) increase in maximal knee flexion torque (Fig. 4) was detected only during the HAB phase (Table 1).

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304 *** Insert Fig. 4 about here ***

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Joint angles

307 We found significant shoe by distance interaction effects for parameters describing the 308 foot strike pattern of runners, more precisely foot- TS_{TD} and ankle dorsiflexion angle at TD 309 Table 1).

A closer look at the post-hoc comparisons revealed that the interaction effects for foot-310 TS_{TD} and ankle dorsiflexion angle at TD were caused by a significant difference between the 311 shoe conditions that was only present during the HAB phase and disappeared during the FAT 312 phase (Fig. 5). In addition, we found only for shoe_{Racing} that the ankle dorsiflexion angle at TD 313 decreased significantly (P < 0.05) during the FAT phase (Fig. 5). We found a higher ankle 314 dorsiflexion angle at TD (Fig. 5), and a higher maximal ankle dorsiflexion angle (see Appendix, 315 Supplemental Fig. 4, Maximal joint angle) throughout the entire run, when using shoe_{Cushion} in 316 317 comparison to shoe_{Racing} (Fig. 5).

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319 *** Insert Fig. 5 about here ***

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The shoe by distance interaction effect for the ankle plantarflexion angle at TO (Table 1) was represented by a decrease in the ankle plantarflexion angle in the FAT phase only with

shoe_{Racing} (Fig. 5). There was a significant shoe main effect for the maximal ankle dorsiflexion 323 angle (Table 1). We found a decreased ankle plantarflexion angle at TO throughout the entire 324 run, when using shoe_{Cushion} in comparison to shoe_{Racing} (Fig. 5). A running distance main effect 325 for the maximal knee joint flexion angle and the knee joint flexion angle at TD was identified 326 (Table 1) indicating a more flexed knee joint configuration with increasing running distance. 327

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Fitting models of changes in running mechanics

While assessing the nonlinear nature of changes in running mechanics throughout the 10-330 331 km runs, we found for all joint work parameters that fitting a bi-linear model resulted in the smallest sum of squared errors compared to a linear or quadratic model. This finding was 332 independent of the shoe condition analyzed (see Appendix, Supplemental Table 5, Sum of 333 squared errors; Supplemental Fig. 5 and 6, Fitting methods). Similarly, we found for all joint 334 torque parameters and joint angle parameters (except for maximal ankle dorsiflexion when 335 using shoe_{Racing}, and maximal hip flexion torque using shoe_{Racing} and shoe_{Cushion}) that fitting a 336 bi-linear model resulted in a smaller sum of squared errors compared to fitting a linear or 337 quadratic model, independent of the shoe condition (see Appendix, Supplemental Table 5, Sum 338 of squared errors; Supplemental Fig. 7 - 10, Fitting methods). 339

340

DISCUSSION 341

The primary purpose of this study was to investigate the difference between a typical 342 racing flat shoe and a typical cushioned running shoe with regards to joint-specific 343 contributions to lower extremity joint work during a fatiguing 10-km run with a near-maximal 344 effort in rearfoot runners. We hypothesized that using a racing flat shoe in comparison to a 345 cushioned shoe leads to a more pronounced and earlier fatigue-related redistribution of positive 346 work from distal to proximal joints during a fatiguing near-maximal effort run. 347

The joint work magnitudes in the current study were comparable to previous studies analyzing running at similar velocities (11,19,32,33). Differences in the magnitude of lower extremity joint work might be explained by different experimental setups (overground vs. treadmill), skill levels of runners, or analysis details such as the segmentation of the foot (11,13,19,26,32,33), which can affect power calculations at more proximal joints (34).

While we identified significant effects of running distance for both absolute and relative positive work parameters indicating a redistribution of positive work from distal to proximal joints for both shoe conditions, we did not find a shoe by distance interaction effect for any joint work-related parameter. Consequently, our central hypothesis that using a racing flat shoe in comparison to a cushioned shoe leads to a more pronounced and earlier fatigue-related redistribution of positive work from distal to proximal joints during a fatiguing near-maximal effort run could not be accepted.

This result was not expected because, in accordance with the literature (13,15,19), we also found a higher mechanical demand at the ankle (+3% dorsiflexion torque; +8% negative work) for shoe_{Racing} compared to shoe_{Cushion} at the beginning of the run. However, this increased demand for shoe_{Racing} disappeared over the course of the run, which might partly explain the lack of difference in the redistribution of joint work between the shoe conditions (Fig. 2).

Next to the higher energy absorption capacity in the rear part of the midsole, shoe_{Cushion} 365 was characterized by a threefold higher longitudinal bending stiffness (Fig. 1). Previous studies 366 analyzing shorter running distances found an association between the longitudinal bending 367 stiffness of footwear and the length of the lever arm of the GRF at the ankle (28). However, in 368 this study (28), not all runners made use of this longer lever arm and increased internal ankle 369 plantarflexion torques. Instead, some runners prolonged the push-off period and thereby 370 avoided the generation of increased muscle forces (28). This subject specific response might 371 partly explain the inconsistent evidence provided by other studies reporting the response in 372

ankle joint torques to increased bending stiffness levels of footwear in the literature (11,32). An increase in GRF lever arm at the ankle along with higher energy absorption capacity of shoe_{Cushion} and the associated adaptations in foot strike behavior could influence fatigue-related reduction in ankle joint torque. Therefore, the increased bending stiffness of shoe_{Cushion} might also partly explain the lack of difference in the redistribution of joint work between the shoe conditions (Fig. 2).

379 The second hypothesis of this study was that separating a fatiguing near-maximal effort 10-km run into a habituation (HAB) and fatiguing (FAT) phase will reveal markedly larger 380 381 changes in biomechanical parameters in the initial HAB phase of running. Although the participants executed a warm-up run with self-determined velocity and duration before the 382 actual run, we observed a nonlinear behavior of several biomechanical variables over the 383 running distance. Such nonlinear behavior of biomechanical variables seems to be more 384 pronounced in recreational runners (6). To assess the validity of our assumption that the 385 changes observed with running distance are related to habituation and fatigue processes, we fit 386 different types of models to the results observed over running distance. We found that fitting a 387 bi-linear (two-components: 0 - 2 km, and 2 - 10 km) model or a quadratic model provided a 388 better fit to the data over running distance for most biomechanical variables compared to using 389 a simple linear model, independent of the used shoe condition. Specifically, we found 390 significant changes for more than half (shoe_{Racing}: n = 14; shoe_{Cushion}: n = 12) of the 20 analyzed 391 392 parameters during the HAB phase (Table 1). In particular, we observed that positive work at all lower extremity joints (see Appendix, Supplemental Fig. 3, Joint work), maximal ankle 393 dorsiflexion and knee joint flexion torques (Fig. 4) as well as maximal knee joint flexion angles 394 (see Appendix, Supplemental Fig. 4, Maximal joint angle) changed more substantially during 395 the HAB phase, independent of the shoe condition (Table 1). While further research is needed 396 to address this issue more specifically, we believe that these findings provide evidence in 397

support of our second hypothesis that changes in running mechanics in an intense, prolonged 398 run underlie HAB and FAT processes. It is noteworthy that when using shoe_{Cushion}, the ankle 399 angle at TD became less dorsiflexed (P < 0.001) (Fig. 5) and the negative work at the ankle 400 increased (P = 0.031) (Fig. 3) at a near-linear rate during the HAB phase compared to shoe_{Racing} 401 (see Appendix, Supplemental Fig. 5 and 10, Fitting methods). Such decreases in the ankle 402 dorsiflexion angle at TD were also found in other studies (8,35) during the first 5 minutes of a 403 404 30 minutes run (corresponding approximately to the 1-km distance in our study) and this was independent of the shoe midsole thickness. The more pronounced ankle dorsiflexion angle at 405 406 TD with shoe_{Cushion} at the beginning of the run might be related to differences in rearfoot construction (12), midsole thickness, and heel-toe drop height (8,13,14,22). While using a more 407 dorsiflexed ankle angle at TD might allow for a greater energy absorption by the foam materials 408 409 of shoe_{Cushion}, it might have led to a greater demand for the dorsiflexors of the ankle joint (i.e. mainly m. tibialis anterior) due a greater leverage of the GRF (12,36,37). It is possible that the 410 neuromuscular system tries to establish a balance between passive impact absorption and 411 mechanical demand of the dorsiflexors of the ankle joint during the HAB phase during 412 prolonged runs when wearing cushioned footwear. This hypothesis is in line with previous 413 research showing a decrease in ankle dorsiflexion angle at TD during prolonged runs (10) or 414 when performing a localized dorsiflexors fatigue protocol (38). This mechanism might have 415 been accentuated in this study given the relatively short familiarization time that each 416 417 participant had with the new shoe conditions, even though they were generally experienced with running with racing flat and cushioned shoes. 418

The difference in foot strike and ankle dorsiflexion angle at TD between the shoe conditions did not persist throughout the entire run, as the more pronounced rearfoot strike pattern when using shoe_{Cushion} decreased continuously during and disappeared at the end of the HAB phase. This finding challenges the assumptions from previous reports analyzing short bouts of running with previous short habituation to the shoe condition (12–15,32) that foot
strike behaviors between more minimalist and more cushioned shoes persist during prolonged
running. Since increased heel height can change the working conditions of ankle plantar flexor
muscle-tendon-units (12), it might be possible that runners adjusted their foot strike behavior
during the HAB phase in order to optimize the economy of power generation.

Further, habituation effects, regarding foot strike behavior, may be due to long-term 428 429 habituation effects, for example, habituation to barefoot running may take 8 weeks or longer (39). It is further conceivable that the participants may have been insufficiently accustomed to 430 431 running on a treadmill (40), or that the materials of the midsole of shoe_{Cushion} changed their properties throughout the HAB phase due to the repeated cyclic loading. Further, interactions 432 with changes in running mechanics outside the sagittal plane need to be considered (41). In 433 order to better understand the habituation of the neuromuscular system to different kinds of 434 shoes or other external constraints, future studies should consider and control in detail the short-435 term (warm-up phase before a test run) and longer-term habituation. These studies should also 436 address changes within the biomechanical properties of biological tissues involved in 437 generating propulsion and support. These changes might include, e.g., alterations in tendons 438 and ligaments stiffness or modifications in the contractile elements within muscle-tendon-439 units. In this context, recent work has identified that the fluid content of ankle plantar flexor 440 muscles undergoes a rapid initial increase followed by a decrease at slower rate during 75 441 minutes of running (42). Changes in muscle fluid content have been related to the active and 442 passive force generation potentials of muscles (43,44) and should therefore be considered when 443 investigating changes in joint mechanics during prolonged, intense activities. 444

In contrast to the HAB phase, few (shoe_{Racing}: n = 6; shoe_{Cushion}: n = 2) of the 20 analyzed parameters changed significantly (P < 0.05) during the FAT phase (Table 1). During the FAT phase, the foot-TS_{TD} and ankle dorsiflexion angle at TD were not different between the shoe

conditions (Fig. 5). Furthermore, in the FAT phase, maximal ankle dorsiflexion torques were 448 not different between shoes (Fig. 4). Therefore, we assume that the mechanical demand of 449 450 plantar flexor muscle-tendon-units was slightly higher in shoe_{Racing} only during the HAB phase and similar during the FAT phase, which might partly explain the comparable decline of 451 positive work at the ankle during this phase. In particular, positive work at the ankle decreased 452 at a near-linear rate during the FAT phase (see Appendix, Supplemental Fig. 6, Fitting 453 454 methods), independent of shoe condition (Table 1). However, it is noticeable that the decrease in positive work at the ankle during the FAT phase was higher for shoe_{Racing} compared to 455 456 shoe_{Cushion} (Fig. 3). This finding is similar to the delayed decrease in positive work at the ankle recently described by Cigoja at el. (45) for shoes with higher longitudinal bending stiffness. 457 Since shoe_{Cushion} had a higher bending stiffness than shoe_{Racing}, we speculate that the difference 458 in bending stiffness might have played a role in this distance specific difference between the 459 shoe conditions. 460

While this study provides a clear indication that changes in running biomechanics over 461 prolonged fatiguing runs are not necessarily a linear function of running distance, there is more 462 research needed to understand the mechanisms underlying this phenomenon. Based on the 463 current findings, we can only speculate that the changes during the HAB phase might be due 464 to a harmonization of the runners' neuromuscular system with the running environment, e.g., 465 footwear and surface, and the requirements of the task, e.g., running distance and velocity. In 466 contrast, the more linear changes during the FAT phase could be related to fatigue effects of 467 the involved muscle-tendon-units. 468

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470 LIMITATIONS

This study has several limitations. First, the mechanical test to analyze cushioning
properties of shoe midsoles was technically limited in the compression velocity of 16 mm·s⁻¹

due to the limits of our material testing machine (Fig. 1, III). Typical compression velocities 473 are approximately threefold higher during running and could be simulated with other material 474 testing machines (25). The mechanical test was also limited to a one-dimensional actuation of 475 force and allowed a general characterization of midsole mechanical energy storage and return 476 capabilities only in the rearfoot region of the shoe and not over the entire midsole as performed 477 in a previous study (25). Second, we investigated only one type of typical racing flat and 478 479 cushioned shoe. Third, we attached the reflective markers of the foot to the corresponding position on the shoe, which might not exactly represent the movement of the foot inside the 480 481 shoe, which may have affected our results. Fourth, we chose an explorative approach by using Fisher's least significant difference correction between the shoe conditions at each of the 13 482 distances, which has increased the statistical power to identify smaller differences between 483 footwear conditions, but at the same time has increased the risk for a type 1 error. Fifth, the 484 running economy was not directly quantified. Finally, the isometric or isokinetic force 485 capacities of the leg extensors before and after the prolonged fatiguing run were not 486 determined, therefore we can only speculate about potential fatigue effects in these muscle 487 groups. 488

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490 CONCLUSION

491 Our findings demonstrate that a typical racing flat shoe (with less cushioning material and 492 lower longitudinal bending stiffness) and a typical cushioned running shoe do not differ in the 493 fatigue-related redistribution of positive work from distal to proximal joints, despite small 494 differences in the timing of the redistribution between shoes.

Furthermore, irrespective of the analyzed shoe, the majority of the kinetic and kinematic alterations in the running mechanics occurred in the first 2 km of the 10 km fatiguing run, which might be attributed to the existence of a habituation rather than a fatigue effect, indicating a nonlinear response to the running distance. Despite the observed changes in the
habituation phase, positive work and maximal ankle dorsiflexion torque decreased
continuously between 2 and 10 km of the run, leading to the previously described redistribution
of positive work from distal to proximal joints. Overall, these findings improve the knowledge
on the role of footwear for fatigue-related alterations in running mechanics during prolonged
fatiguing runs.

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513 CONFLICTS OF INTEREST

The manufacturers of shoe_{Racing} (Adidas AG; Herzogenaurach, Germany) and shoe_{Cushion} (Brooks Sports Inc., Seattle, Washington, USA) were not involved in the study design or the collection, analysis, or interpretation of data. Authors S.W. and G.P.B. received funding from Brooks Running Inc., Seattle, WA, to perform work not related to this study. There are no other conflicts of interest to declare. The results of the present study are presented clearly, honestly, and without fabrication, falsification, or inappropriate data manipulation. The results of this study do not constitute an endorsement by the American College of Sports Medicine.

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675 FIGURE AND TABLE LEGENDS

FIG. 1: Footwear conditions (I): 'Adizero Pro 4' (Shoe_{Racing}) and ,Glycerin 10' (Shoe_{Cushion}). 676 Schematic illustration of the testing method (II) to quantify longitudinal bending properties of 677 the running shoes. The shoes were mounted in a material testing machine (Z020; Zwick GmbH 678 & Co.KG, Ulm, Germany) on a rearfoot shoe last, which was fixed on a moving apparatus 679 (low-friction ball bearing sledge) to give the freedom to bend where its sole construction allows 680 681 it to. The illustration presents the unloaded situation (gray) and the maximal bending situation (white) due to the vertical displacement (50 mm) of the load cell as well as the corresponding 682 683 vertical force at maximal vertical displacement (Force_{MVD}) to bend the forefoot and midfoot part of the shoe as well as the bending stiffness for both analyzed shoes. Schematic illustration 684 of the simple mechanical test (III) which was performed in a material testing machine (Z020; 685 Zwick GmbH & Co.KG, Ulm, Germany) to evaluate midsole material properties (energy 686 storage and return) by compressing the rearfoot midsole in vertical direction with 2000 N at a 687 constant compression velocity of 16 mm·s⁻¹. 688

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TABLE 1: Main effects of a two-factor repeated-measures ANOVA (P-values) with two 690 within-subjects factors (shoe condition and running distance) as well as the interaction effect 691 between both factors for spatiotemporal parameters, maximal (max) joint angles, joint angles 692 at foot touch-down (TD) and toe-off (TO), angle between the foot and the treadmill surface at 693 694 touch-down (foot-TS_{TD}), maximal external joint torques, and positive (pos) and negative (neg) joint work. The partial eta squared (η_p^2) values are presented as normalized effect sizes. The 695 last two columns show the pairwise comparisons (P-values) of 0 km and 2 km as well as 2 km 696 and 10 km of 10-km treadmill run with near-maximal effort for the shoes, 'Adizero Pro 4' 697 (Racing) and 'Glycerin 10' (Cushion). All significant differences (P < 0.05) are represented by 698 bold printed *P*-values. 699

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FIG. 2: Relative negative and positive work (mean \pm standard deviation) at the ankle (triangle), knee (circle), and hip (square) joint in both shoe conditions (left: shoe_{Racing}; right: shoe_{Cushion}) throughout the 10-km treadmill run with near-maximal effort. The first distance interval (0 – 2 km) was selected to assess potential habituation effects (grey area) and the second distance interval (2 – 10 km) to demonstrate fatiguing processes. Significant differences between 0 km and 2 km as well as 2 km and 10 km are represented by **P* < 0.05, ***P* < 0.01, and ****P* < 0.001, respectively.

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FIG. 3: Mean changes in negative and positive joint work during the habituation phase (HAB; corresponds to the distance of 0 - 2 km) and the fatigue phase (FAT; corresponds to the distance of 2 - 10 km) for shoe_{Racing} and shoe_{Cushion}. All significant changes are represented by **P* < 0.05, ***P* < 0.01, and ****P* < 0.001, respectively.

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FIG. 4: Maximum external torques (mean \pm standard deviation) at the ankle, knee, and hip 714 joint throughout the 10-km treadmill run with near-maximal effort in both shoe conditions (715 shoe_{Racing}: racing flat shoe; \circ shoe_{Cushion}: cushioned running shoe). The first distance interval 716 (0 - 2 km) was selected to assess potential habituation effects (grey area) and the second 717 distance interval (2 - 10 km) to demonstrate fatiguing processes. Significant differences 718 between 0 km and 2 km as well as 2 km and 10 km are represented by *P < 0.05, **P < 0.01, 719 and ***P < 0.001 for shoe_{Racing} as well as $^P < 0.05$, and $^P < 0.01$ for shoe_{Cushion}, respectively. 720 A significant (P < 0.05) shoe difference for the maximum external torque of ankle was found 721 for the 0.2-km distance and is represented by S. Further results of pairwise comparisons 722 between shoes can be found in the Appendix (Supplemental Table 4, Pairwise comparisons 723 between shoes). 724

FIG. 5: Selected kinematic parameters (mean \pm standard deviation) for both shoe conditions 726 (■ shoe_{Racing}: racing flat shoe; ○ shoe_{Cushion}: cushioned running shoe) throughout the 10-km 727 treadmill run with near-maximal effort. Top left: the angle between the foot and the treadmill 728 surface at touch-down (foot-TS_{TD}). Top right: ankle dorsiflexion angle at touch-down 729 (angle_{TD}). Bottom left: ankle plantarflexion angle at toe-off (angle_{TO}). Bottom right: knee joint 730 flexion angle at touch-down (knee_{TD}). The first distance interval (0 - 2 km) was selected to 731 assess potential habituation effects (grey area) and the second distance interval (2 - 10 km) to 732 demonstrate fatiguing processes. Significant differences between 0 km and 2 km as well as 2 733 km and 10 km are represented by *P < 0.05, **P < 0.01, and ***P < 0.001 for shoe_{Racing} as 734 well as $^{\wedge}P < 0.001$ for shoe_{Cushion}, respectively. Significant (P < 0.05) shoe differences are 735 represented by S. Further results of pairwise comparisons between shoes can be found in the 736 Appendix (Supplemental Table 4, Pairwise comparisons between shoes). 737

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739 SUPPLEMENTAL DIGITAL CONTENT

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