NPS-57Fu72051A

NAVAL POSTGRADUATE SCHOOL Monterey, California



DENSITY INHOMOGENEITY IN A LASER

CAVITY DUE TO ENERGY RELEASE

by

Allen E. Fuhs

May 1972

Approved for public release; distribution unlimited.

CORE

Provided by Calhoun, Institutional Archive of the Naval Postgr

NAVAL POSTGRADUATE SCHOOL Monterey, California

Rear Admiral A. S. Goodfellow, Jr., USN Superintendent

Milton U. Clauser Provost

ABSTRACT:

Density gradients, which refract laser light within the cavity, degrade beam quality. In addition to wall influences and viscous effects which cause density gradients, there is another mechanism. This mechanism, which is due to wakes and compression waves from heat (vibration energy to translation and rotation) addition in a supersonic stream, appears to have been overlooked. The appropriate equation is stated and discussed. A semigraphical solution procedure is outlined. Contours of constant density have been calculated for circular and rectangular cavities. Graphs of the isodensity contours are given.

DENSITY INHOMOGENEITY IN A LASER

CAVITY DUE TO ENERGY RELEASE

by

Dr. Allen E. Fuhs Professor of Aeronautics Naval Postgraduate School Monterey, California 93940

Beam quality is degraded when there are density gradients in the lasing medium. The density gradients refract the light within the cavity. Considerable effort has been devoted by engineers and scientists working with gas dynamic lasers to measure and correct density variations arising from wakes, boundary layers and wall irregularities. Another mechanism exists to cause density gradients, and it appears that this mechanism has been overlooked or ignored.

Heat addition in a supersonic stream causes compression waves which radiate from the energy release region. When the laser radiation is created by stimulated emission (e.g. CO₂ laser), there is also a transfer of vibrational energy to translational and rotational degrees of freedom. This is effectively heat addition and can be treated as a energy-per-unit-volume-and-per-unit-time term in the energy equation.

Using the results from the paper by Tsien and Bielock (1), the following equation can be derived (2) for distributed energy sources

$$\frac{\Delta \rho(\mathbf{x},\mathbf{y})}{\rho} = \frac{(\gamma-1)M}{2a^{3}\beta\rho} \int_{0}^{S} h(\mathbf{x},\mathbf{y}) \sin \mu \, dS$$
(1)
$$- \frac{\gamma-1}{a^{2} U\rho} - \int_{\mathbf{x}'} \int_{\mathbf{y}'} h(\mathbf{x}',\mathbf{y}')\delta(\mathbf{y}-\mathbf{y}')\mathbf{I}(\mathbf{x}-\mathbf{x}')d\mathbf{x}'d\mathbf{y}$$

Equation (1) is applicable to a planar geometry; planes normal to the beam are considered. The symbols have the following meaning;

γ	ratio of heat capacity of lasing medium			
М	Mach number			
a β	local speed of sound (M ² -1) ^{1/2}			
ρ	density			
h(x',y')	energy released at (x',y') per unit at volume and unit time			
μ	Mach angle equal to arcsin of 1/M			
S	distance along a characteristic			
U	local flow velocity			
δ(y-y')	delta function			
$I(x-x^{i})$	unit function, zero for $x-x' < 0$ and unit for $x-x' > 0$			

The first integral yields the density variation along a characteristic. When h(x,y) = constant, the change in density is proportional to the length of characteristic imbedded within the energy release region. When h(x,y) is variable, the element of characteristic length dS is weighted by h(x,y).

The second integral results from the wake of the energy release region. Note that it is opposite in sign to the first integral. The change in density is proportional to the length of streamline imbedded in the energy release zone upstream of the observation point. This is true if h(x,y) is a constant. These facts concerning the proportionality of $\Delta p/\rho$ to the length of characteristic and streamline traversing the

3

energy release region suggest a semigraphical calculation procedure. This is illustrated in Figure 1 for point P with a flow at M = 4. As illustrated, the right running characteristic R has a length of 7.0, the wake streamline W has a length of 8.5, and the left running characteristic L, a length of 10.2. The length of characteristics must be multiplied by sin μ . It has been assumed that h(x,y) is a constant within the circle and zero outside the circle. Waves reflected from the walls have been neglected.

It is necessary to evaluate the value of h for typical laser operating conditions. A gas dynamic laser has an efficiency of approximately 1 percent based on the chemical energy which increased the medium temperature from a room value to 1500°K or so. The increase in enthalpy of the gas mixture is 550 BTU/lbm. Consider the flow of gas through a volume with a shape of a cube having 1 ft sides. For typical conditions this gives a flow of 40 lbm/sec through the cube. Assume the cube is the laser cavity and that 1 percent of the energy is removed as radiation. A CO2 laser has a quantum efficiency of 40%. It is assumed that 1.5% of the energy, which had been frozen in vibration, is transferred to translation and rotation. For these conditions h has a value of 330 BTU/sec ft³. Using appropriate values for M, a, ρ , etc., it is found that

and

$$\frac{\Delta \rho}{\rho} = 0.023 \text{ per foot of characteristic length}$$

$$\frac{\Delta \rho}{\rho} = 0.052 \text{ per foot of streamline in equity}$$

 $\rho = -0.052$ per foot of streamline in cavity

Using these values of $\Delta \rho / \rho$ per foot of length, the density contours were calculated for both a square and a circular cavity. Figure 2 shows

4

the results for a circular cavity. Flow is from left to right. At the top of the cavity there is a region of large positive $\Delta \rho / \rho$ due to the fact the wake is small and the left running characteristic within the cavity is long. At the extreme downstream edge of the cavity $\Delta \rho / \rho$ is large negative. For this position there is a long wake within the circle which dominates the compression due to characteristics. At the top of the cavity the 0, +.001, +.002, and +.003 contours have a slope nearly equal to the slope of a left running characteristic. This causes a near loop in the +.003 contour.

In Figure 3 the feature most readily obvious is the slope of the density contours in the upper part of the figure. These might be diagnosed as resulting from waves originating at the upper wall. However, these are due to energy release in a supersonic stream. Along the upper surface the density decreases going downstream. Along the laser centerline the density increases slightly as one moves downstream. In the upper downstream corner there is a strong density gradient.

The analysis of this note has focused on two cases where h(x,y) is constant. For the circular case with a real laser, the value of h is best described as Gaussian. This solution is straightforward but extremely tedious. A computer program seems appropriate for the problem of variable h(x,y).

This note has demonstrated that the energy release can cause $\Delta \rho / \rho$ values somewhat less than viscous flow effects but nonetheless significant. Furthermore, since the $\Delta \rho / \rho$ may be oriented nearly along characteristics, these may be confused with waves originating at a wall.

5

REFERENCES

- l. H. S. Tsien and M. Beilock, "Heat Source in a Uniform Flow," J. Aero Sci, <u>16</u>, p. 756, 1948.
- A. E. Fuhs, "Quasi Area Rule for Heat Addition in Transonic and Supersonic Flight Regimes," AF Aero Propulsion Laboratory TR-72-10, WPAFB, Ohio, 1972.





Fractional density contours due to energy release in Fig. 2: a circular laser cavity. Only top half is shown due to symmetry.



Fig. 3 : Fractional density contours due to energy release in a square cavity.

		No.	Copies
l.	Defense Documentation Center Cameron Station Alexandria, Virginia 22314		20
2.	Library, Code 0212 Naval Postgraduate School Monterey, California 93940		2
3.	Dean of Research Administration Naval Postgraduate School Monterey, California 93940		l
4.	Department of Aeronautics Naval Postgraduate School Monterey, California 93940		
	Professor R. W. Bell, Chairman Professor R. E. Ball Professor M. Bank Professor J. A. J. Bennett Professor D. J. Collins Professor O. Biblarz Professor O. Biblarz Professor A. E. Fuhs Professor T. H. Gawain Professor R. A. Hess Professor G. Hokenson Professor G. Hokenson Professor C. H. Kahr Professor D. M. Layton Professor G. H. Lindsey Professor J. A. Miller Professor J. A. Miller Professor M. F. Platzer Professor M. F. Platzer Professor M. H. Redlin Professor M. Schlachter Professor L. V. Schmidt Professor R. P. Shreeve Professor R. D. Zucker		
5.	Professor G. E. Schacher, Code 61Sq Department of Physics Naval Postgraduate School Monterey, California 93940		l
6.	Professor O. Heinz, Code 61Hz Department of Physics Naval Postgraduate School Monterey, California 93940		l

7.	Professor N. E. J. Boston, Code 58Bb Department of Oceanography Naval Postgraduate School Monterey, California 93940	1
8.	Professor A. Cooper, Code 61Cr Department of Physics Naval Postgraduate School Monterey, California 93940	1
9.	Professor Schwirzke, Code 61Sw Department of Physics Naval Postgraduate School Monterey, California 93940	l
10.	Professor Ciglio, Code 61 Cl Department of Physics Naval Postgraduate School Monterey, California 93940	l
11.	Professor Kalmbach, Code 61Kb Department of Physics Naval Postgraduate School Monterey, California 93940	l
12.	Professor Neighbours, Code 61Nb Department of Physics Naval Postgraduate School Monterey, California 93940	1
13.	Professor Tao, Code 52Tv Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	l
14.	Professor Davidson, Code 51Ds Department of Meteorology Naval Postgraduate School Monterey, California 93940	l
15.	Professor Tolles, Code 5417 Department of Material Science and Chemistry Naval Postgraduate School Monterey, California 93940	l
16.	Professor Powers, Code 52Po Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	1

17.	Gene Crittenden Naval Research Labs Washington, D. C. 20390	1
18.	Dr. John McCallum Naval Research Labs Washington, D. C. 20390	1
19.	CAPT James Wilson, USN Naval Ordnance Systems Command Washington, D. C. 20360	1
20.	Col. Donald Lamberson AFWL Kirtland AFB, New Mexico	1
21.	Ernest G. Brock North American Rockwell Corp. Downey, California 90240	1
22.	James R. Carter Naval Weapons Center China Lake, Calif. 93555	1
23.	Robert J. Collins University of Minnesota Minneapolis, Minnesota 55400	1
24.	Robert S. Cooper MIT Lincoln Laboratory Lexington, Massachusetts 02173	1
25.	Jack D. Daugherty AVCO Everett Research Lab Everett, Massachusetts 02149	1
26.	Anthony J. DeMaria United Aircraft Research Labs East Hartford, Connecticut 06108	1
27.	George A. Emmons U. S. Army Missile Command Redstone Arsenal, Alabama 35809	1
28.	William C. Eppers, Jr. Air Force Avionics Lab Wright-Patterson AFB, Ohio 45433	1
29.	Peter A. Franken The University of Michigan Ann Arbor, Michigan 48103	1

30.	Harold Jacobs U. S. Army Electronics Command Fort Monmouth, New Jersey 07703	l
31.	Walter B. Jennings, Jr. U. S. Army Missile Command Redstone Arsenal, Alabama 35809	l
32.	CAPT Dale A. Holmes Air Force Weapons Laboratory Kirtland AFB, New Mexico 87117	l
33.	John M. Hood, Jr. Naval Electronics Lab Center San Diego, California 92100	1
34.	Thomas B. Dowd Executive Secretary Fifth DoD Conference on Laser Tech Office of Naval Research Boston, Massachusetts 02100	1
35.	Frank A. Horrigan Raytheon Research Division Walham, Massachusetts 02154	1
36.	A. Fenner Milton Naval Research Lab Washington, D. C. 20390	1
37.	Edwin N. Myers Office of Secretary of Defense (ODDR&E) Washington, D. C. 20000	l
38.	Fred W. Quelie, Jr. Office of Naval Research Boston, Massachusetts 02100	1
39.	Howard R. Schlossberg Air Force Cambridge Research Lab Bedford, Massachusetts 01730	1
40.	William C. Schoonover Air Force Avionics Lab Wright-Patterson AFB, Ohio 45433	1
4 1 .	Walter R. Sooy Naval Research Laboratory	1

42.	C. Martin Stickley Advanced Research Projects Agency Arlington, Virginia 22200	l
43.	Malcolm L. Stitch Union Carbide Corporation Korad Division Santa Monica, California 90406	1
44.	Robert B. Watson Office of Chief of Research and Development Department of the Army Washington, D. C. 20000	1
45.	Eric J. Woodbury Hughes Aircraft Company Culver City, California 90230	l
46.	George J. Zissis The University of Michigan Ann Arbor, Michigan 48103	1

Security Classification			1.			
DOCUMENT CONTROL DATA , R & D						
(Security classification of title, body of abstrac	(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)					
1 ORIGINATING ACTIVITY (Corporate author)		28. REPORT SECURITY CLASSIFICATION				
Naval Postgraduate School		Unclassified				
Monterey, California 93940		2b. GROUP				
3. REPORT TITLE						
Density Inhomogeneity in a Las	ser Cavity Due to Ener	rgy Release	9			
4 DESCRIPTIVE NOTES (Type of report and, inclusive d	lates)					
5. AUTHOR(S) (First name, middle initial, last name)						
Allen E. Fuhs						
			· · · · · ·			
6. REPORT DATE	78. TOTAL NO. O	FPAGES	75, NO. OF REFS			
May 1972	16		2			
88. CONTRACT OR GRANT NO.	98. ORIGINATOR'S	S REPORT NUMB	1ER(5)			
	NPS - 57Fu	72051A				
b. PROJECT NO.						
c. 90. OTHER REPORT NO(S) (Any other numbers that may be assign this report)			ner numbere that may be assigned			
d						
10. DISTRIBUTION STATEMENT						
This document has been approve	ed for public release	and sale;	its distribution			
is unlimited.						
11. SUPPLEMENTARY NOTES	12. SPONSORING	MILITARY ACTIN	VITY			
Naval Postgraduate School						
Monterey, California 93940						

13. ABSTRACT

INCLASS TETED

Density gradients, which refract laser light within the cavity, degrade beam quality. In addition to wall influences and viscous effects which cause density gradients, there is another mechanism. This mechanism, which is due to wakes and compression waves from heat (vibration energy to translation and rotation) addition in a supersonic stream, appears to have been overlooked. This appropriate equation is stated and discussed. A semigraphical solution procedure is outlined. Contours of constant density have been calculated for circular and rectangular cavities. Graphs of the isodensity contours are given.

Security Classification

UNCLASSIFIED

S/N 0101-807-6821

Security Classification

14 KEY WORDS	LINKA		LINKB		LINK C	
	ROLE	wт	ROLE	wт	ROLE	wт
Gas dynamic lasers						
Electrical lasers						
Been quality		1		-		
Deam duarroy						
Supersonic heat addition						
						-
			-		-	
						-
DD 1 NOV 41 473 (BACK)	UNCLA	SSIFTE	D			

-





.