



Calhoun: The NPS Institutional Archive

Theses and Dissertations

Thesis Collection

1983

Analysis and testing of the thermal design of the electrical package in the U.S. Army's Upgraded Logic Module (ULM).

Keebler, Henry C.,III.

Monterey, California. Naval Postgraduate School



Calhoun is a project of the Dudley Knox Library at NPS, furthering the precepts and goals of open government and government transparency. All information contained herein has been approved for release by the NPS Public Affairs Officer.

Dudley Knox Library / Naval Postgraduate School
411 Dyer Road / 1 University Circle
Monterey, California USA 93943

<http://www.nps.edu/library>



NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

ANALYSIS AND TESTING OF THE THERMAL DESIGN
OF THE ELECTRONIC PACKAGE IN THE U.S. ARMY'S
UPGRADED LOGIC MODULE (ULM)

by

Henry C. Keebler III

September 1983

Thesis Advisor:

M. Kelleher

Approved for public release; distribution unlimited.

T21-223

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Analysis and Testing of the Thermal Design of the Electronic Package in the U.S. Army's Upgraded Logic Module (ULM)		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis; September 1983
7. AUTHOR(s) Henry C. Keebler III		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		12. REPORT DATE September 1983
		13. NUMBER OF PAGES 111
14. MONITORING AGENCY NAME & ADDRESS(if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Upgraded Logic Module (ULM) Thermal Design Electronic Packaging		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The U.S. Army has developed an Upgraded Logic Module (ULM) for use in its Infantry Direct Fire Simulator System (IDFSS). It is designed to analyze data collected from associated instrumentation according to prescribed programming, to report results back to the system control via a telemetry interface, and it can be backpack mounted. The thermal environment existing at Ft. Hunter Liggett,		

20. ABSTRACT (Continued)

Ca. (the primary operating environment for the ULM) during the summer will add an abnormal thermal load to the ULM operating environment in the backpack.

A mock-up of the actual ULM was built to model the heat dissipation of all the components and tested in different environments using extreme power consumption rates. The actual ULM was tested with typical power consumption rates and various environmental temperatures, including solar loading. Under typical operating conditions, the ULM will remain within manufacturer's tolerances for individual component temperatures. However slight increases in power consumption rates will severely stress the reliability limits of certain components, and the reliability of the entire system cannot be predicted.

Approved for public release; distribution unlimited.

Analysis and Testing of the Thermal Design
of the Electronic Package in the U.S. Army's
Upgraded Logic Module (ULM)

by

Henry C. Keebler III
Captain, United States Army
B.S., United States Military Academy, 1973

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN MECHANICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL

September 1983

ABSTRACT

The U.S. Army has developed an Upgraded Logic Module (ULM) for use in its Infantry Direct Fire Simulator System (IDFSS). It is designed to analyze data collected from associated instrumentation according to prescribed programming, to report results back to the system control via a telemetry interface, and it can be backpack mounted.

The thermal environment existing at Ft. Hunter Liggett, Ca. (the primary operating environment for the ULM) during the summer will add an abnormal thermal load to the ULM operating environment in the backpack.

A mock-up of the actual ULM was built to model the heat dissipation of all the components and tested in different environments using extreme power consumption rates. The actual ULM was tested with typical power consumption rates and various environmental temperatures, including solar loading. Under typical operating conditions, the ULM will remain within manufacturer's tolerances for individual component temperatures. However slight increases in power consumption rates will severely stress the reliability limits of certain components, and the reliability of the entire system cannot be predicted.

TABLE OF CONTENTS

I.	INTRODUCTION -----	7
	A. BACKGROUND OF THE ULM -----	7
	B. OBJECTIVES -----	9
	C. DEVICE DESCRIPTION -----	10
II.	TEST PROCEDURE -----	17
	A. PRELIMINARY SETUP -----	17
	B. CONDUCT OF TESTS -----	27
III.	EVALUATION OF RESULTS -----	33
	A. RESULTS -----	33
	B. DISCUSSION -----	50
	C. CONCLUSION -----	56
APPENDIX A:	EQUIPMENT LIST -----	59
APPENDIX B:	THERMOCOUPLE CALIBRATION -----	60
APPENDIX C:	PROGRAM LISTING -----	68
APPENDIX D:	ULM DATA RUN 1 AUG 83 -----	73
APPENDIX E:	ULM DATA RUN 12 AUG 83 -----	80
APPENDIX F:	MODEL DATA RUN 15 AUG 1983 (48.8C AMBIENT) -----	89
APPENDIX G:	MODEL DATA RUN 15 AUG 1983 (37.7C AMBIENT) -----	99
LIST OF REFERENCES -----		110
INITIAL DISTRIBUTION LIST -----		111

LIST OF FIGURES

1.1	MODEL (top) AND ULM (bottom) -----	11
1.2	CPU BOARD -----	13
1.3	I/O BOARD -----	14
2.1	MODEL CPU BOARD -----	23
2.2	MODEL I/O BOARD -----	24
2.3	SCHEMATIC OF POWER SETUP -----	26
2.4	SCHEMATIC OF DATA ACQUISITION SETUP -----	26
3.1	1 AUGUST 1983 - graph 1 -----	34
3.2	1 AUGUST 1983 - graph 2 -----	35
3.3	1 AUGUST 1983 - graph 3 -----	36
3.4	12 AUGUST 1983 - graph 1 -----	38
3.5	12 AUGUST 1983 - graph 2 -----	39
3.6	12 AUGUST 1983 - graph 3 -----	40
3.7	12 AUGUST 1983 - graph 4 -----	41
3.8	12 AUGUST 1983 - graph 5 -----	42
3.9	15 AUGUST 1983 (AMBIENT = 48.8C) - graph 1 -	44
3.10	15 AUGUST 1983 (AMBIENT = 48.8C) - graph 2 -	45
3.11	15 AUGUST 1983 (AMBIENT = 48.8C) - graph 3 -	46
3.12	15 AUGUST 1983 (AMBIENT = 37.7C) - graph 1 -	47
3.13	15 AUGUST 1983 (AMBIENT = 37.7C) - graph 2 -	48
3.14	15 AUGUST 1983 (AMBIENT = 37.7C) - graph 3 -	49
3.15	THERMAL RESISTANCE OF PACK AIR TO AMBIENT --	55
3.16	ENERGY BALANCE ON THE BACKPACK -----	57

I. INTRODUCTION

A. BACKGROUND OF THE ULM

The U.S. Army Combat Developments Experimentation Command (CDEC), conducts combat experiments at Ft. Hunter Liggett, California, often involving infantry and vehicle players in mock battle. These experiments are designed to test various weapons systems, strategies, vehicles, and personnel under equally varied conditions.

Players are generally instrumented to monitor the battle activity and are linked to a main computer system via telemetry devices. The instrumentation utilized must operate under dusty conditions, high vibration, and in temperatures ranging from 10 fahrenheit in the winter to 120 fahrenheit in the summer.

Prior to the experiment, player instrumentation is planned and designed to fit the particular parameters of the experiment. Maximum use of existing equipment is planned whenever possible. However, due to the uniqueness of many of the experiments--in terms of equipment and scope--new devices, cables, and mounting hardware must be designed or existing inventory modified. For these reasons and due to the high frequency of new experiments, there is a constant process of upgrading and re-designing existing equipment to meet the needs of the current experiment--with little regard given to the uses for future requirements.

The unfortunate consequences of this type of design process are many:

- Existing hardware--although functionally adequate--may not be compatible with other existing hardware.
- Due to modifications, documentation is often poor and usually only addresses the experiment of the original design.
- These poorly designed functional modules are extremely difficult for new personnel to use in the planning of new experiments.
- Finally, much of the equipment has become obsolete and hard to maintain.

For these reasons CDEC has developed the Upgraded Logic Module (ULM) to replace the Logic Module of the Infantry Direct Fire Simulator System. The objectives of the ULM design are:

- Support the infantry player with minimum size and weight, yet allow expansion of functions where size and weight are not critical.
- Fit the existing backpack.
- Use a microprocessor such that the inherent flexibility of the program memory can be used to meet future requirements without re-design.
- Provide input and output interfaces with sufficient flexibility to support the diverse player configurations.
- Be compatible with existing units and cables to the maximum possible extent.
- Use conventional packaging techniques to simplify parts procurement, assembly, maintenance, and repair.
- Provide hermetic sealing to protect against dust.
- Provide general purpose bus interfaces for adding other developed equipment.

- Partition the hardware and firmware into sharply defined functional modules to make the design easier to understand, to simplify the documentation, and to provide the ability to meet future requirements by redesigning a module instead of the entire ULM [Ref. 1].

B. OBJECTIVES

The thermal characteristics of the ULM were a prime consideration during the design process. Components chosen were specifically required to be capable of operation in the high temperature of the ULM. It was recognized that the small size of the ULM and the large number of integrated circuits could challenge the stress limits of current micro-electronic packaging techniques [Ref. 2]. Additionally the high ambient temperatures existing at Ft. Hunter Liggett during the summer months would place an additional thermal load on the ULM which cannot be accurately predicted.

Thus the purpose of this test and analysis is to check the thermal performance of the ULM. Specifically tests were designed to:

- Determine if the ULM operating under typical conditions of power consumption and environment would remain within the reliability limits specified by manufacturers for their individual components.
- Attempt to predict performance under off-design conditions.

Using resistors to produce the heating characteristics of the individual internal components, a model was designed and constructed to simulate the power dissipation of the actual ULM. To accomplish the above objectives, both the

model and the ULM were instrumented with thermocouples to measure temperatures at specific locations and on specific components.

C. DEVICE DESCRIPTION

The Upgraded Logic Model (ULM) is an integral part of the Infantry Direct Fire Simulator System (IDFSS) responsible for the collection of data from infantrymen instrumented in connection with a combat development experiment. It analyzes data according to its programming for that experiment and reports results via a telemetry interface back to the system control computer center.

The ULM consists of two circuit boards housed in a machined cast aluminum case with outside dimensions of 1.75x5x10 in. The circuit boards are made of multi-layered glass epoxy and copper circuits. The fully populated boards and case weigh approximately five pounds. Its power consumption is rated at a maximum of 15 watts at 5 volts, with a typical usage of 7 to 9 watts at 5 volts [Ref. 3].

The case is made of two separate halves, each containing one of the circuit boards and one of the connectors shown in Figure 1.1. The half containing the J1 connector houses the CPU board, and the one containing the J2 connector houses the I/O board. The two boards are connected by a fifty pin ribbon connector, and when the two halves are assembled, the tops of the components from each board face each other. The

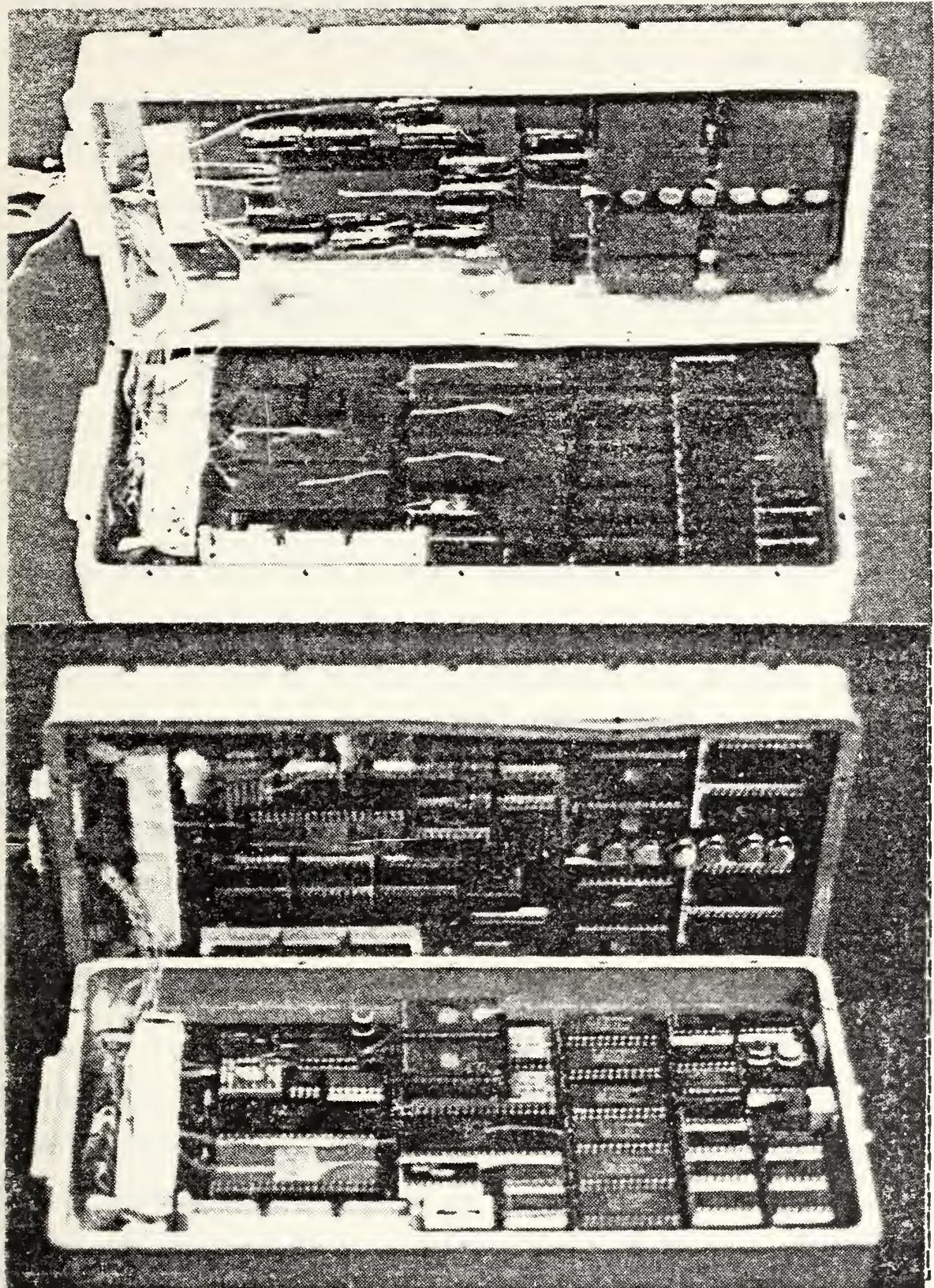


Figure 1.1 MODEL (top) AND ULM (bottom).

boards are fastened by 12 hex head machine screws with a gasket between the two halves of the case for dust protection.

The circuitry consists of a Central Processing Unit (CPU) Board and an Input/Output (I/O) Board, depicted in Figures 1.2 and 1.3. The CPU Board contains over 60 separate electronic components, including the Z8002 16 bit CPU(u3).

The I/O Board also contains approximately 60 electronic components, including two Z-8 Micro-computer processors (u2,ull) and the ZCIO I/O chips(u1). The larger socket mounted dual-in-line pin (DIP) devices are listed in Tables 1 and 2, and are shown in Figures 1.2 and 1.3. All components are rated by the manufacturer for maximum case temperature tolerances to 125 C, except the following devices:

u3 of the CPU

u1,u2,ull,ul2, and u13 of the I/O

which are rated at 85 C.

The ULM is equipped with two connectors, one for power input and the other for I/O signals and testing. For this evaluation, the ULM was specially wired to give typical power consumption rates for the system without using the I/O connector. This allowed an I/O connector modification to accommodate the many thermocouple wires to be inserted into the case. However this also prevented the ULM from being tested under atypical power consumption rates.

ULM CPU BOARD SHOWING COMPONENT AND THERMOCOUPLE (TC) LOCATIONS

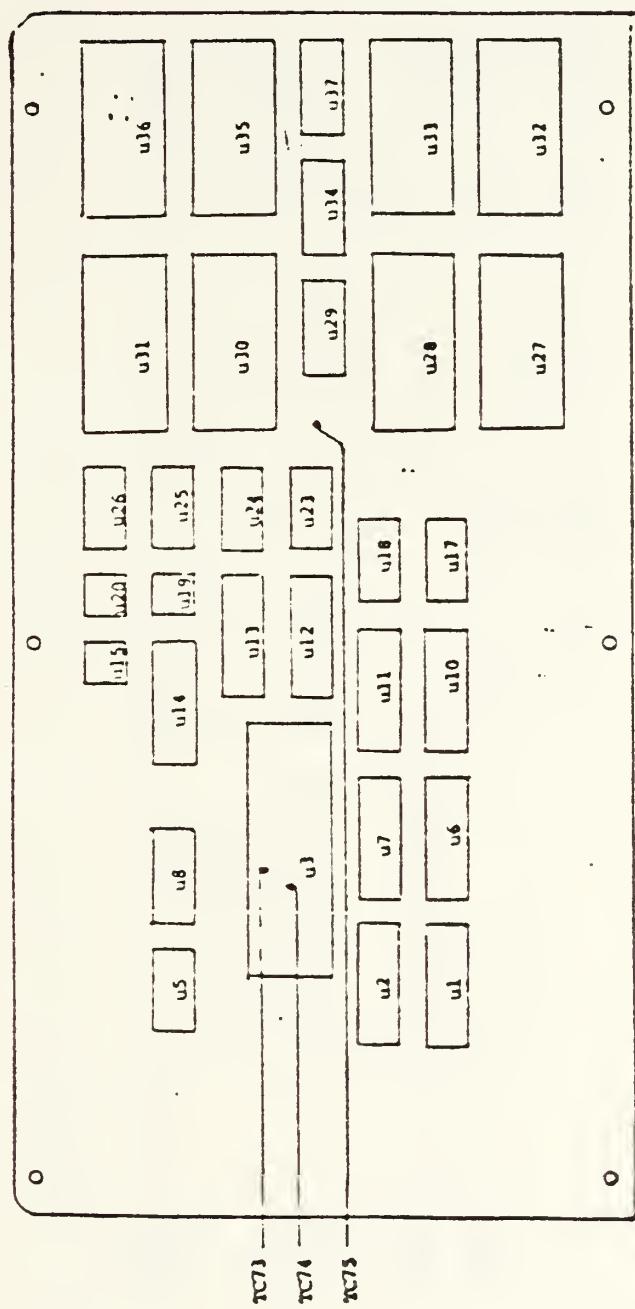


Figure 1.2 CPU BOARD.

UIM I/O BOARD SHOWING COMPONENT AND THERMOCOUPLE (TC) LOCATIONS

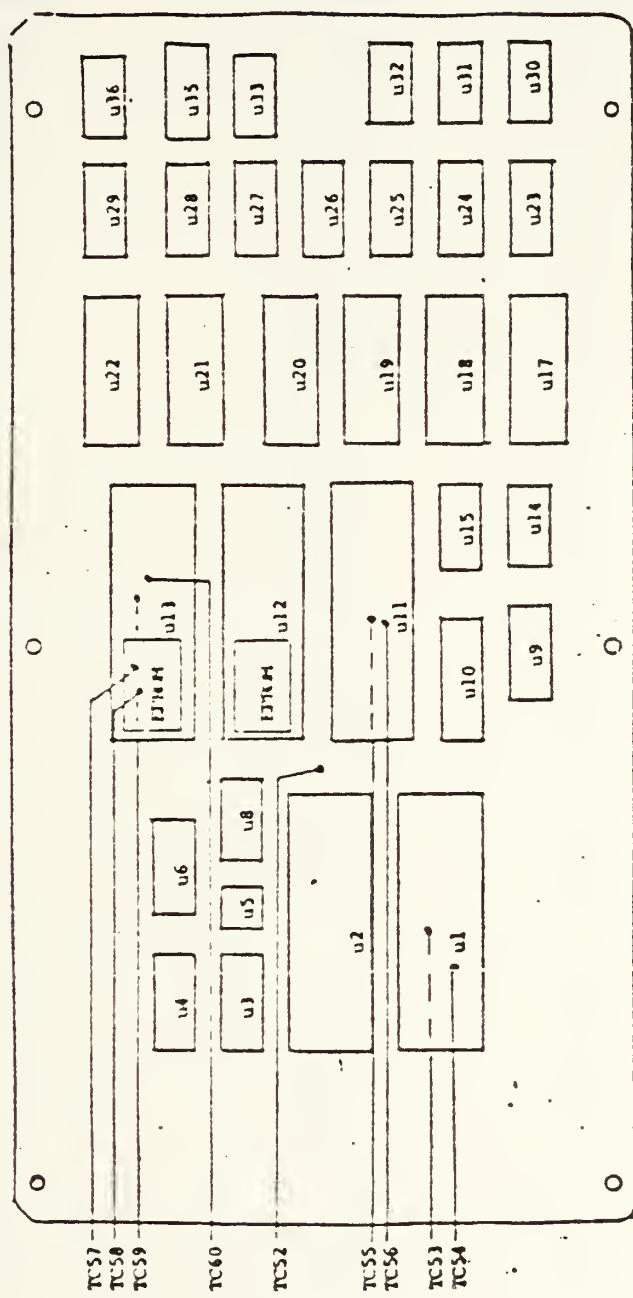


Figure 1.3 I/O BOARD.

TABLE 1

CPU MODEL DATA

<u>UNIT</u>	<u>I (ma)</u>	<u>R (ohms)</u>	<u>POWER (w)</u>
1	90	55.55	.45
2	90	55.55	.45
3	300	16.67	1.5
5	10	500.	.05
6	50	100.	.25
7	50	100.	.25
8	30	166.67	.15
10	90	55.	.45
11	90	55.	.45
12	40	125.	.20
13	120	41.66	.60
14	40	125.	.20
15-23	0	0	0
24	7	714.29	.04
25	6	833.33	.03
26	0	0	0
27	10	500.	.05
28	60	83.3	.30
29	0	0	0
30	60	83.3	.30
31	90	55.55	.45
32	10	500	.05
33	60	83.3	.3
34	0	0	0
35	60	83.3	.3
36	90	55.55	.45
37	0	0	0
38	40	125.	.2

TABLE 2

I/O MODEL DATA

<u>UNIT</u>	<u>I (ma)</u>	<u>R (ohms)</u>	<u>POWER (w)</u>
1	250	20.0	1.25
2	250	20.0	1.25
3	0	0	0
4	0	0	0
5	50	100.	.25
6	0	0	0
8	0	0	0
9	26	192.3	.13
10	120	41.67	.60
11	250	20.	1.25
12	180	27.7	.90
13	180	27.7	.90
14-27	0	0	0
29	80	62.5	.40
30	54	92.6	.27
31	54	92.6	.27
32-36	0	0	0

II. TEST PROCEDURE

A. PRELIMINARY SETUP

Test procedures for the ULM and the model were determined by various limitations--primarily equipment availability and facilities. Initially, the actual ULM was not available for testing, and a model was presumed to be the primary vehicle for this analysis.

The questions were:

- How to fabricate the model to simulate the thermal characteristics of the ULM?
- How to instrument the individual components?
- How to simulate the various conditions under which the ULM would operate?

The last two questions also applied to the actual ULM when it was learned one would be available for testing. Fortunately, most of the solutions to these problems were equally applicable to the ULM, with only some modification.

Using an actual ULM case, two unpopulated ULM circuit boards, the ULM technical drawings, and power consumption rates--which were all provided by CDEC--the model was fabricated. To simulate the individual components in terms of thermal energy dissipation, resistors were used as heaters and scaled to the component's power dissipation rate shown in Tables 1 and 2. For most of the DIP components with 16 pins or less, DIP resistor networks were wired to meet the calculated resistance required and then

mounted into DIP sockets. Required resistances shown in Tables 1 and 2, were calculated based on power consumption rates of individual components at 5 volts. Using the relation:

$$\text{power} = \text{current} * \text{voltage}$$

the current was calculated, and using Ohm's Law:

$$\text{voltage} = \text{current} * \text{resistance}$$

an equivalent resistance was calculated for each component. For DIP components with more than 16 pins, the DIP resistor networks were not readily available. Therefore similar resistor networks were fabricated using single resistors - wired into DIP adapters, forming an equivalent resistor network. Covers were added to these heaters to simulate a more even heat dissipation on the surface of the component, and to maintain geometric similitude. Each component was then placed in the exact position on the board as occupied by its actual counterpart.

Before beginning model fabrication, the decision to use type-T thermocouples for temperature measurement was made. As the critical temperatures for all components were well within the range of the type-T (copper constantan) thermocouples, and the thermocouple wire and connectors were readily available, this was a logical choice. Due to the small area of consideration and to minimize disturbances

to the internal natural convection of the air, 30 gauge wire was chosen for fabricating the thermocouples.

Next a determination was made concerning which specific components were to be instrumented. This was based on elements with the lowest critical temperatures and the highest heat dissipation from Tables 1 and 2. Additionally, thermocouples were placed on the boards, in the air gap between the boards, and on the inside and outside of the case to determine the various thermal resistances of the heat flow path. These locations are listed in Tables 3, 4, and 5 and shown in Figures 1.2, 1.3, 2.1, and 2.2. The thermocouples were fabricated in lengths of approximately 24 in. and connected to 15 ft. lengths of type T thermocouple extension wire.

The thermocouples were then calibrated using the HP 3054 Data Acquisition System and the Rosemount calibration bath (see Appendix B). Two D-style 50 pin connectors used on the ULM were also used on the model. One was used to provide power to the unit, while the other was modified and used as a passageway for the thermocouple wires. The modification was accomplished by drilling out 8 of the pins in the center of the connector with space to accommodate the bundle of thermocouple wires. A slit large enough for one wire was cut in the top of the connector to the hole to facilitate the removal and insertion of the thermocouple

Table 3

MODEL I/O BOARD THERMOCOUPLES (TC)

<u>TC</u>	<u>COMPONENT/LOCATION</u>
61	u2 bottom
62	u2 top
63	u1 bottom
64	u1 top
65	u10 top
66	u10 bottom
67	ull bottom
68	ull top
69	u12 bottom
70	u12 top
71	u13 bottom
72	u13 top

MODEL CPU BOARD THERMOCOUPLES (TC)

<u>TC</u>	<u>COMPONENT/LOCATION</u>
41	u3 bottom
42	u3 top
43	board bottom vicinity u30 and u35
44	board bottom vicinity u10 and u17
45	inside wall of j2 (case)
46	inside wall of j1 (case)
47	board top vicinity u10 and u17
48	board top vicinity u20 and u26
49	board top vicinity u30 and u35
50	board top vicinity u27 and u32
51	air vicinity u30 and u28
52	air vicinity u2 and ull

Table 4

ULM I/O BOARD THERMOCOUPLES (TC)

<u>TC</u>	<u>COMPONENT/LOCATION</u>
53	ul bottom
54	ul top
55	ull bottom
56	ull top
57	ul3 bottom eeprom
58	ul3 top eeprom
59	ul3 bottom
60	ul3 top

ULM CPU BOARD THERMOCOUPLES (TC)

<u>TC</u>	<u>COMPONENT/LOCATION</u>
73	u3 bottom
74	u3 top
75	air vicinity u30
76	air vicinity u38

Table 5
COMMON THERMOCOUPLES (TC)

<u>TC</u>	<u>COMPONENT/LOCATION</u>
45	J2 inside (case)
46	J1 inside (case)
53	ambient air for model runs after 13 AUG 1983--see note
72	ambient air for ULM on 12 AUG 1983--see note
77	ambient air for all runs prior to 13 AUG 1983-- see note
77	backpack air for all runs from 12 AUG 1982-- see note
78	inside front wall of case
79	J2 outside (case)
80	J1 outside (case)

NOTE: Changes to thermocouple locations were required on 12 AUG 1983.

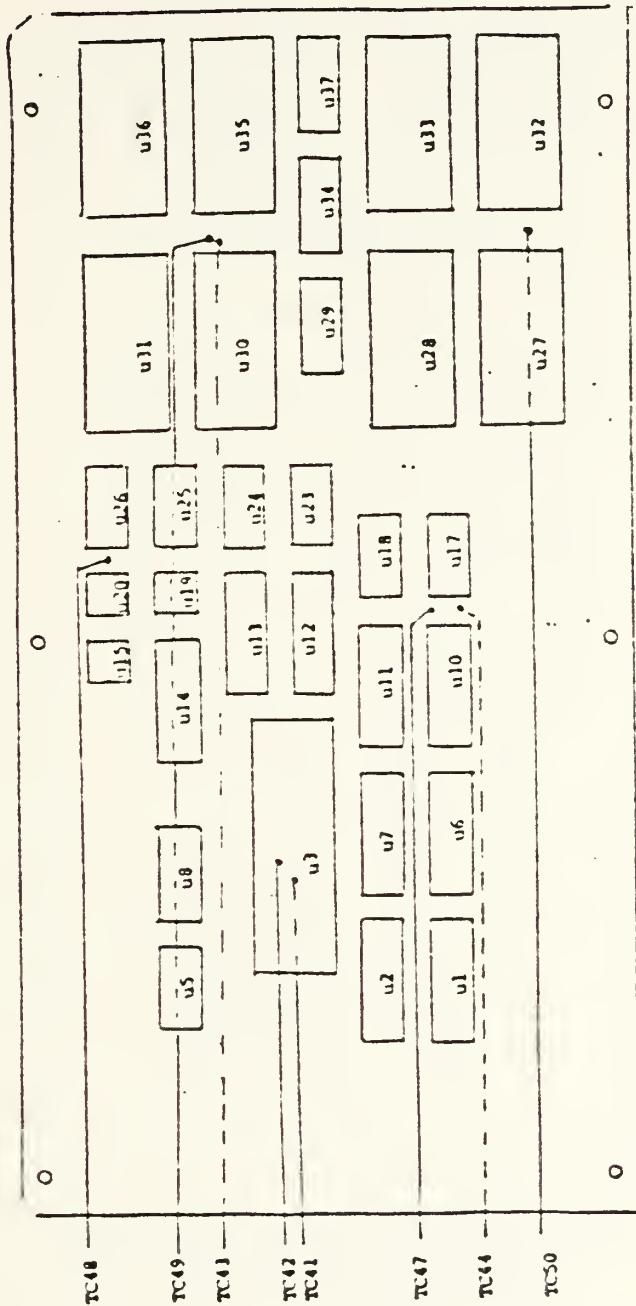
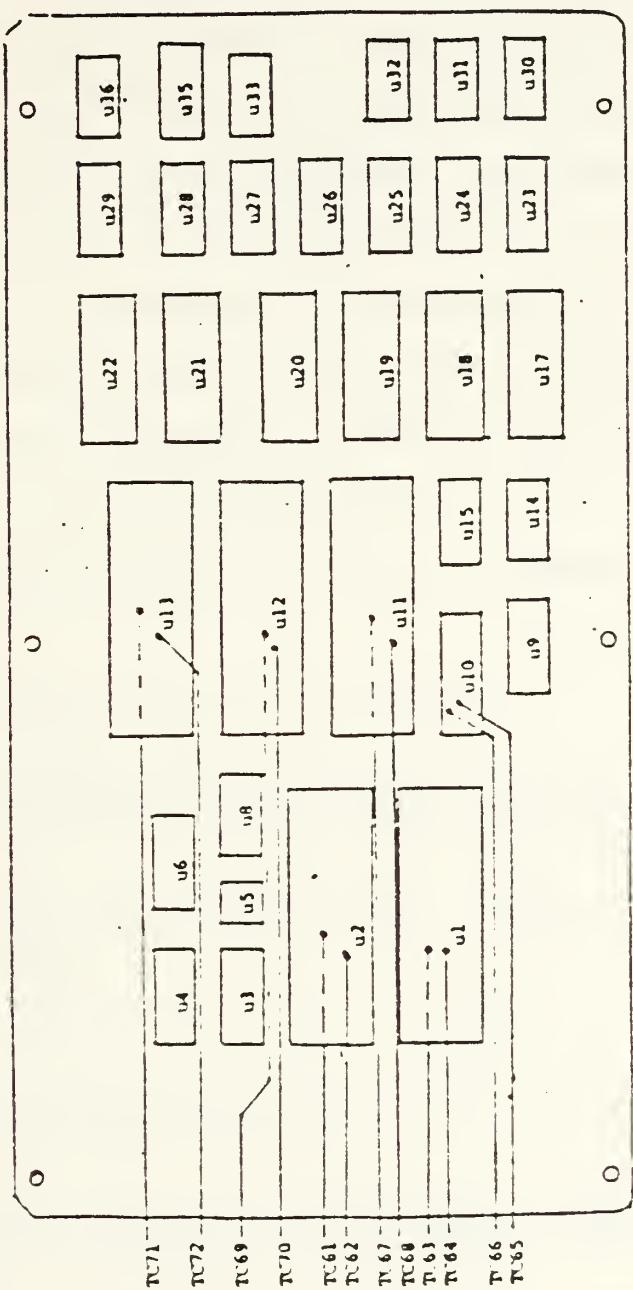


Figure 2.1 MODEL CPU BOARD.



MODEL I/O BOARD SHOWING COMPONENT AND THERMOCOUPLE (TC) LOCATIONS

Figure 2.2 MODEL I/O BOARD.

wires individually. The unit was made almost air tight by packing the hole with silicon rubber sealant.

Power to the ULM was provided by a Lambda 60 volt power supply capable of voltage and current limitation. A Dana Digital Multimeter Model 4200 was used to monitor and adjust the power to the ULM/model, and check resistances. For gathering data, the HP3054 Data Acquisition System was utilized. It consisted of the HP3456 Digital Voltmeter for reading compensated EMF values from the thermocouples and the HP3497 Data Acquisition Control unit for controlling data flow. An HP 9826 computer was used to control the HP3054 and to store data on 5.25 in. floppy disks (see Appendix A).

The system was set up as follows:

- A calibrated 2 ohm resistor was put in series with the load (model/ULM) to obtain accurate current measurements for calculating input power.
- A junction board containing a switch for reading the voltages of the resistor and the load was fabricated.
- The schematic is shown in Figure 2.3.
- Power to the unit was controlled by the settings on the Lambda power supply.
- Temperature was measured by using the thermocouples, the HP3054 system, and the HP9826 computer. The schematic is shown in Figure 2.4.

The actual ULM circuit boards and a backpack became available for testing at this point. It was then decided that the actual ULM would be instrumented similarly to the

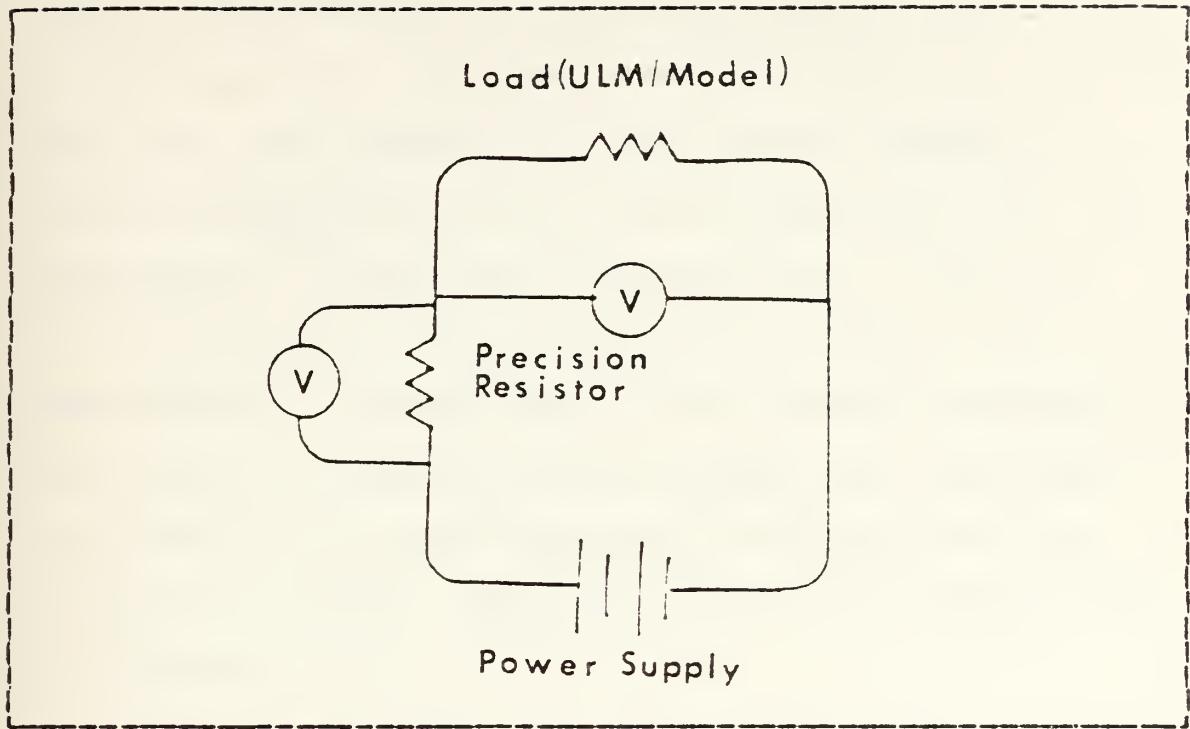


Figure 2.3 SCHEMATIC OF POWER SETUP.

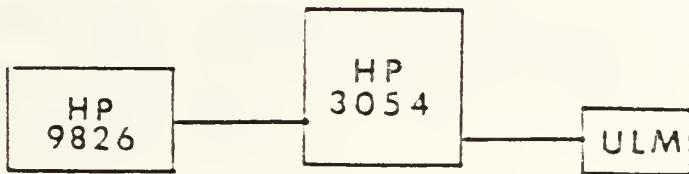


Figure 2.4 SCHEMATIC OF DATA ACQUISITION SETUP.

model. Unfortunately, the ULM could operate only in its typical operating range, and therefore could not be tested under max power ratings. An environmental chamber with variable temperature control was available for use. The environmental chamber had a maximum limit of 48.8C on its control system and was the size of a small room--approximately 40 square feet. This allowed the backpack and ULM to be placed within the chamber in a stabilized environment while being monitored and controlled from outside the chamber. The test procedure was implemented as follows:

- The ULM and model would be run under room temperature conditions to test for proper operation of the systems and to ascertain the operating characteristics of each.
- The ULM would then be installed in the environmental chamber to determine the ambient temperature at which critical temperatures would be reached.
- The ULM and data acquisition system were then transported to Ft. Hunter Liggett on a typical summer day for testing in the ULM's actual environment.
- The model then replaced the ULM in the backpack and tests were again conducted in the environmental chamber. This time runs were conducted in an attempt to exactly simulate power and environmental conditions of all the ULM tests.

B. CONDUCT OF TESTS

This section will cover the specific procedures of all runs performed in the analysis. Data from the runs are contained in Appendices D through G. 40 thermocouples were assembled and divided between the ULM boards, model

boards, the case, and external locations, which are listed in Table 3. Programs were written to automate the data acquisition process. All programs were in Hewlett Packard Basic 2.0 programming language. Specific programs were written for:

- Data acquisition and storage during the calibration procedures. These are contained in Appendix B.
- Calculation and storage of second order polynomial coefficients for calibration corrections of each thermocouple. This program is listed in Appendix B.
- Data acquisition and storage of temperatures for each thermocouple of the model. This program is in Appendix C.
- Data acquisition and storage of temperatures for the ULM thermocouples. This program is listed in Appendix C.

The data acquisition programs for the model and the ULM were interactive and required the following input:

- Month, day, hour, minute and second of the start of the run. This was required to set the internal clock of the HP 3497 control device.
- Voltage readings for the load and the calibrated resistor for calculation of the power and current values.
- The time interval for the wait between data sets.
- Number of data sets to be taken automatically.

The ULM model was first tested on 16 July 1983 in Halligan Hall, room 103. Using the setup previously explained, the model was placed on its side on a wooden board. The ambient temperature of the room was 24C (73F). The purpose of the test was to:

- Check the operation of the model and the system.
- Obtain data for further planning of test procedures.

After studying initial data, it was obvious some of the heaters were not operational. The overall resistance of the system was approximately 3.1 ohms and was checked before and after the tests. However, when power was applied, some of the solder connections were non-conducting electrically. This required resoldering and reassembly of the model boards. The next test for the model was conducted on 18 July 1983 in the same location and under the same conditions as the first test. Power was set at 10.71 watts, and 10 runs were taken at 60 minute intervals. Power was increased to 15 watts--the maximum power level predicted by CDEC for their critical maximum temperature of 85 C. Therefore, to prevent damage to the components, this test was terminated. An examination of this initial data taken at room temperature indicated that if the ULM and the model were to react similarly, the ULM would have problems operating in extreme conditions.

On 26 July the first ULM test was conducted for the same purpose as the first test on the model. However, this test was conducted with the ULM instrumented and placed inside the backpack. The pack was placed in a horizontal position in the same location and under the same conditions as the model test. 10 readings were taken at 5 minute intervals to obtain transient temperature data. Power was

set at 8.72 watts. Next, 8 readings were taken at 30 minute intervals to obtain steady state data. The settings resulted in a power level of 8.71 watts. Since power could not be incremented to maximum on the ULM, lower temperatures--as compared to the model--were obtained on the ULM.

It was noticed there was a danger of cutting the thermocouple wires when inserting and extracting the module to and from the backpack. Therefore it was decided to complete all tests on the ULM before conducting tests on the model. The environmental chamber was then modified to accept the cabling for control of the power and thermocouples. It was heated to 48.8C (120F), the maximum setting for the chamber. For this temperature, it generally took 3 days to reach a constant internal temperature; therefore it was decided to start at this maximum setting. If this was too extreme for the ULM it would be faster to cool down the chamber than to heat it.

On 1 Aug 1983 the ULM was tested in the environmental chamber with the backpack in an upright position (this would be the usual position when carried by an instrumented soldier). 8 samples were taken in 5 minute intervals at a power level of 8.09 watts. 20 readings were then taken in 30 minute intervals with a power level of 7.59 watts at the same settings. The maximum temperature achieved was 78C (173F) on the CPU (u3). It was evident that none of

the components would reach their critical temperatures under these conditions at typical power levels.

The ULM's next test was conducted at Ft. Hunter Liggett, Ca. on 12 Aug 1983. This was done to determine the effect that solar loading in the actual environment would have on the system. The backpack was placed in direct sunlight on a concrete pad in a vertical position. This test was started at 0800 hrs. and ended at 1500 hrs. on a typical summer day for that region. Ambient temperatures were taken from a location in the shade near the backpack. Some tests were initially taken to examine the sun's effect on internal pack temperatures. 10 samples were taken at 5 minute intervals with the ambient temperature ranging from 21.4C to 23.7C. Power was turned on, and 15 readings were taken at 5 minute intervals at a power level of 7.93 watts. The ambient temperature ranged from 24.1C to 29.1C. Next, 10 samples were taken at 15 minute intervals with power now at 7.56 watts. Ambient temperature for this run ranged from 30.3C to 34.5C. Due to the changing direction of the sun's rays, the backpack was reoriented to maintain full irradiation by the sun. This required moving the backpack off the concrete slab onto the dirt. 8 samples were then taken at 15 minute intervals with power at 7.44 watts with no change to the power settings. Ambient temperature ranged from 35.2C to 37.4C. Again none of the components reached its critical temperature. This completed testing of the ULM.

Returning to the Naval Postgraduate School, the model was placed in the backpack and tests were conducted in the environmental chamber to duplicate--for comparison-- conditions of the ULM tests. On 14 Aug 1983 the model was tested with 8 samples taken at 5 minute intervals and a power level of 7.9 watts. Ambient temperature was at 43.3C for this run. Next, 20 samples were taken at 15 minute intervals at the same power level. On 15 Aug 1983 the temperature was set to 48.8C to duplicate the ULM's run on 1 Aug 1983. 8 samples were taken at 5 minute intervals at a power level of 7.91 watts. 20 samples were taken at 15 minute intervals, with power now at 7.97 watts. The final test run was taken--also on 15 Aug 1983--at 37.7C for obtaining data to compare steady state with and without solar loading at the same ambient temperature. 15 samples were taken at 5 minute intervals and power set at 7.72 watts. Next, 24 samples were taken at 30 minute intervals with power now at 6.62 watts.

III. EVALUATION OF RESULTS

A. RESULTS

Results are presented in this section with a summary of the observations of each test followed by the corresponding graphs produced from test data. The graphs depict the thermocouple temperatures plotted against time with either ambient or backpack temperatures, or both, shown for comparison purposes.

The test on 1 August 1983 was conducted at a constant temperature of 48.8C in the environmental chamber. The following are observations from data taken during these runs:

- None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures achieved are shown in Figures 3.1 to 3.3 and are listed here as:

ull = 77.2C
u3 = 78.6C
ul3 = 72.8C
ul = 61.1C

- Steady state was achieved at between 130 and 140 minutes after power was applied.
- Temperatures of internal and external portions of the case are:

internal J1 (TC46) = 56.0C
external J2 (TC80) = 54.4C

There were no unexpected trends or observations resulting from this test.

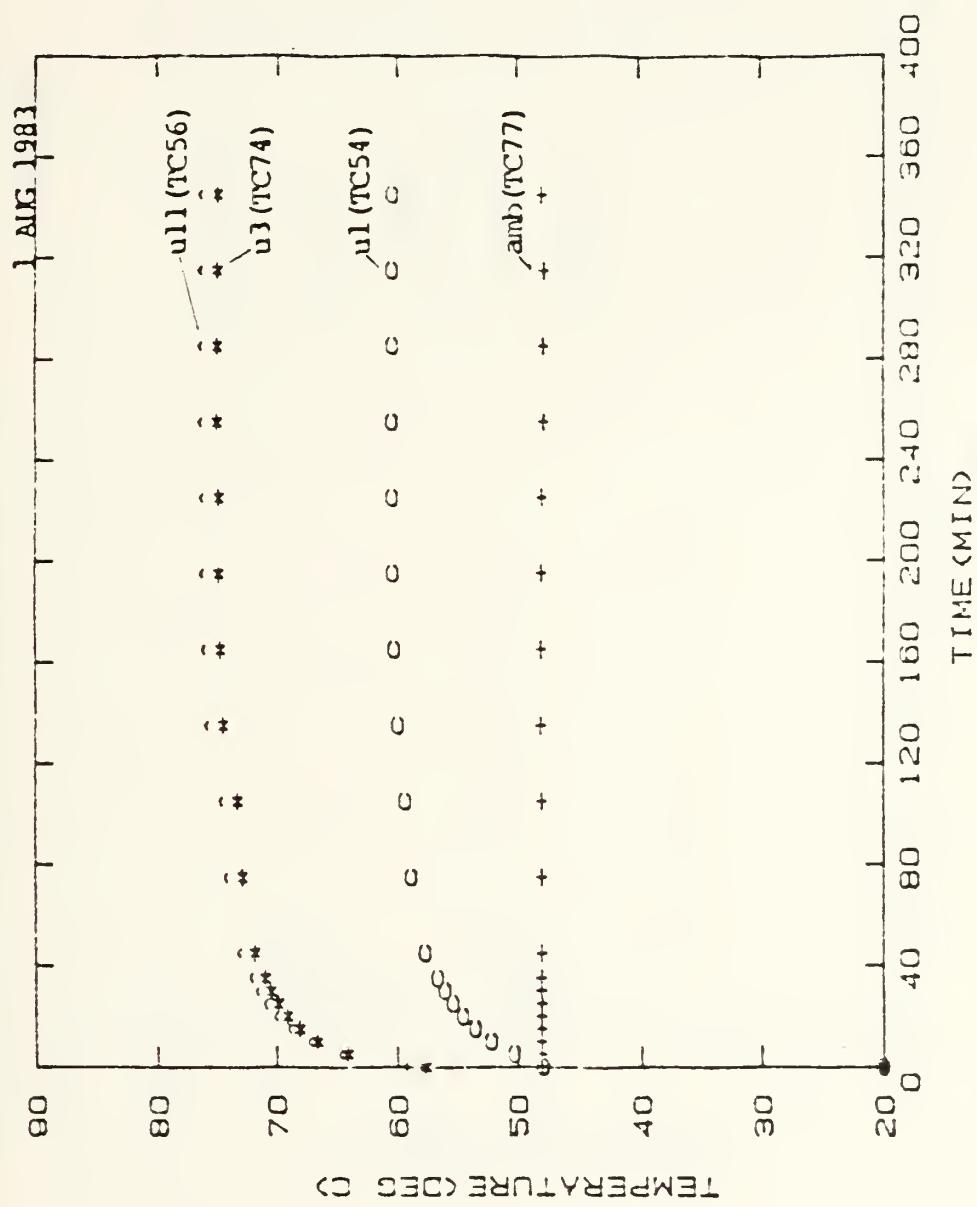


Figure 3.1 1 AUGUST 1983 - graph 1.

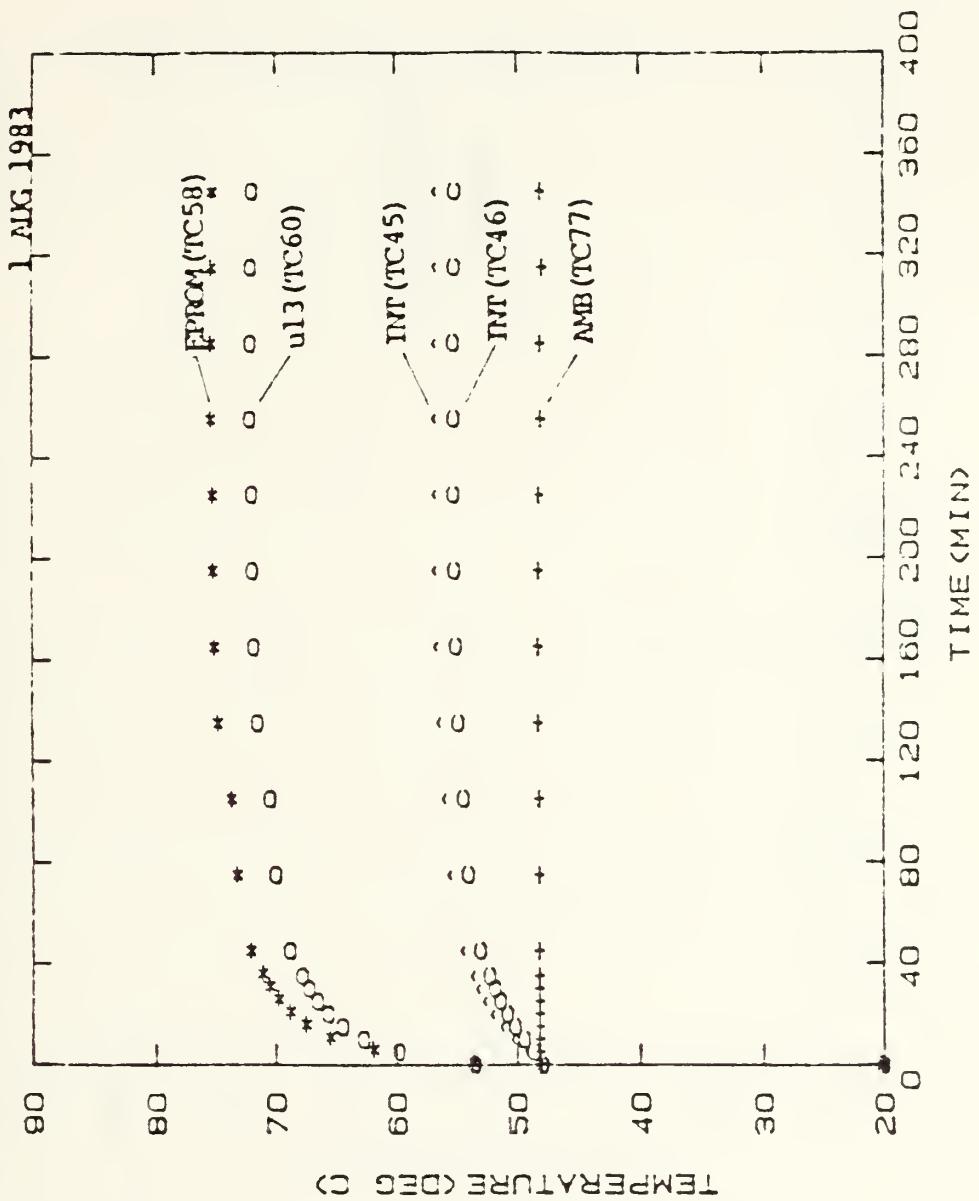


Figure 3.2 1 AUGUST 1983 graph 2.

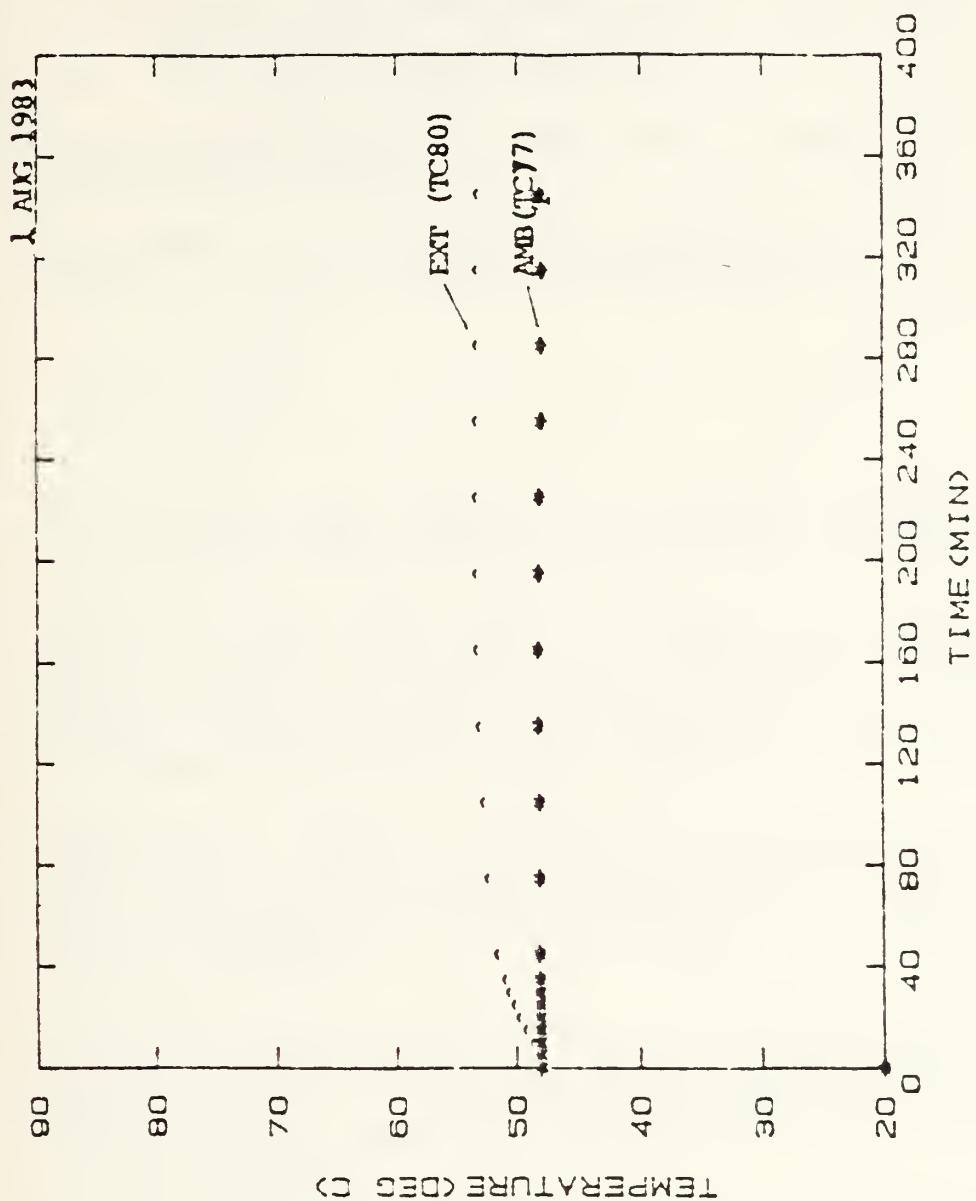


Figure 3.3 1 AUGUST 1983 - graph 3.

The test conducted at Ft. Hunter Liggett experienced ambient temperatures ranging from 21C to 38C and fluctuated due to occasional wind currents. This test began at 0800 hrs. on 12 August 1983, and terminated at 1530 hrs. on the same day. The following was observed:

- None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures achieved are shown in Figures 3.4 to 3.8 and are listed here as:

$$u_{11} = 78.78\text{C}$$

$$u_3 = 79.16\text{C}$$

$$u_{13} = 78.4\text{C}$$

$$u_1 = 64.3\text{C}$$

- The internal pack temperature reached a maximum of 60.8C--22.8C above ambient--as a result of solar loading and internal heat produced by the ULM.
- Although steady state was not reached (due to ambient temperature fluctuations), the effects of transient heating appears to have taken between 130 to 140 minutes. This is due to the heating by the components as opposed to external solar loading.
- Apparently, moving of the pack disturbed the external thermocouple (TC80) causing it to give spurious readings after 250 minutes as seen in Figure 3.5. This is most likely a result of loose connections at the thermocouple connectors.
- The sudden jump in temperature at 30 minutes (for TC's 54, 56, 58, 60 and 74) is a result of the power switch being turned on. Temperature increases prior to 30 minutes are due only to the effect of solar radiation on the backpack.

The first 15 August 1983 test on the model was conducted in the environmental chamber at an ambient temperature of 48.8C. Observations resulting from this test are:

12 AUG 1983

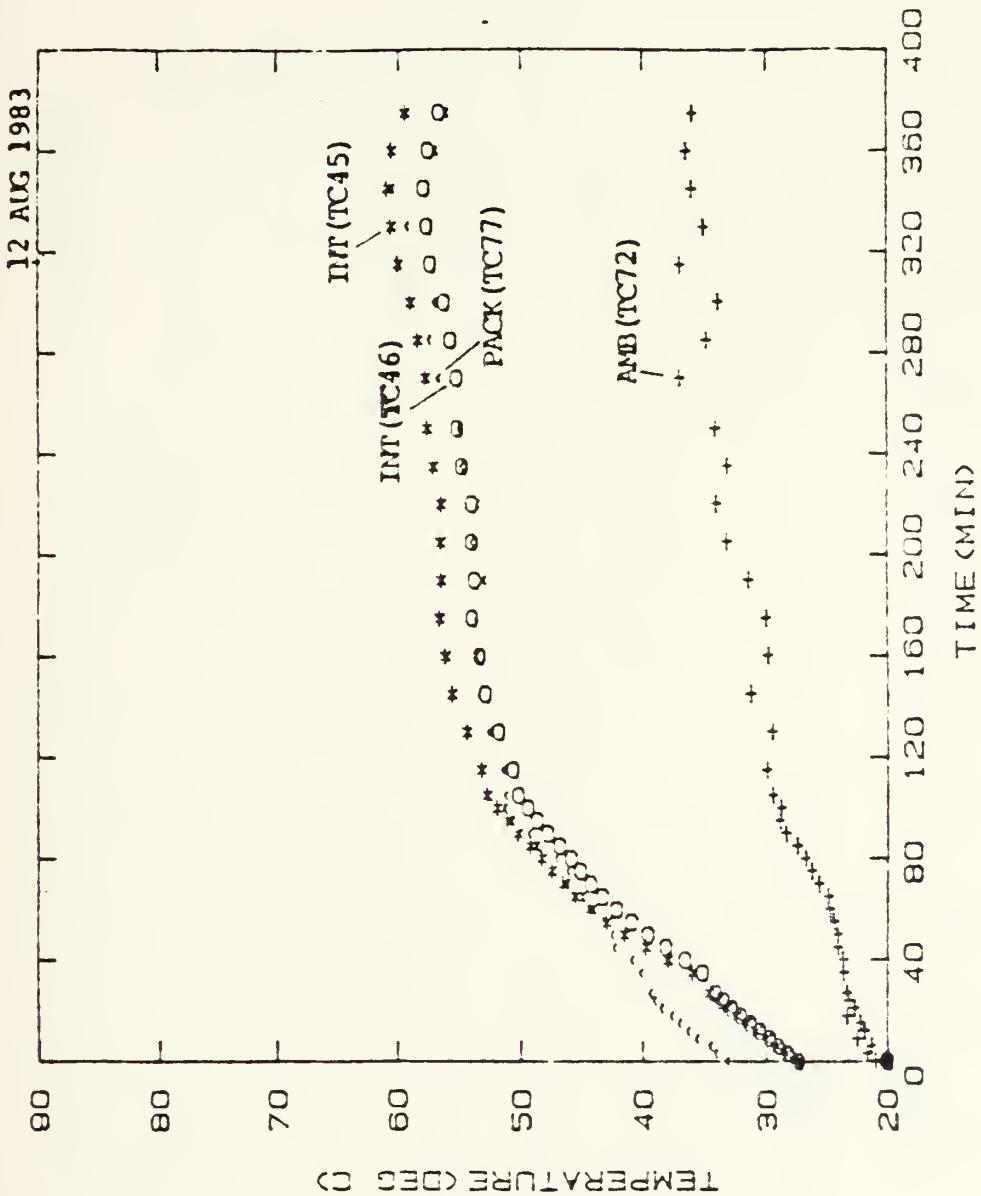


Figure 3.4 12 AUGUST 1983 - graph 1.

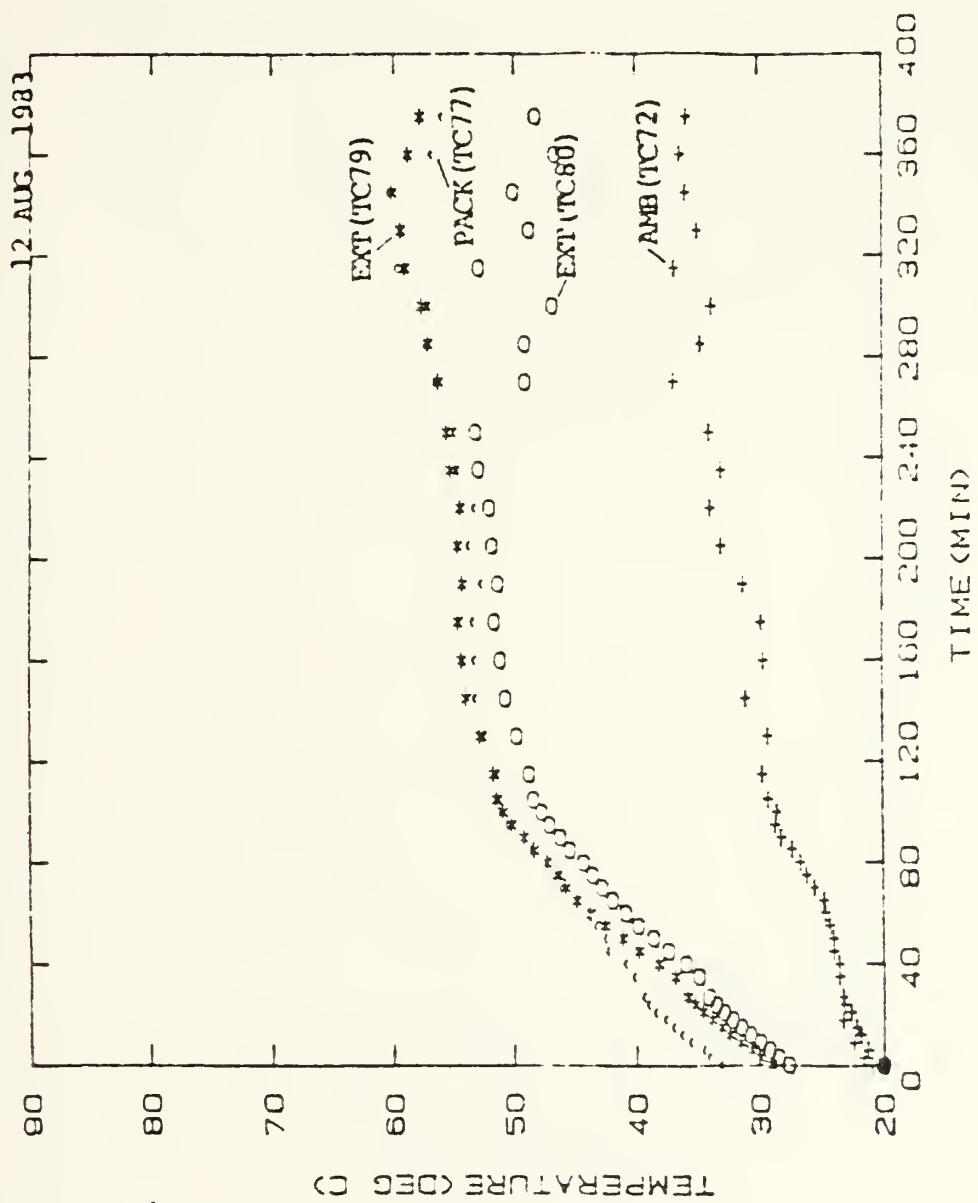


Figure 3.5 12 AUGUST 1983 - graph 2.

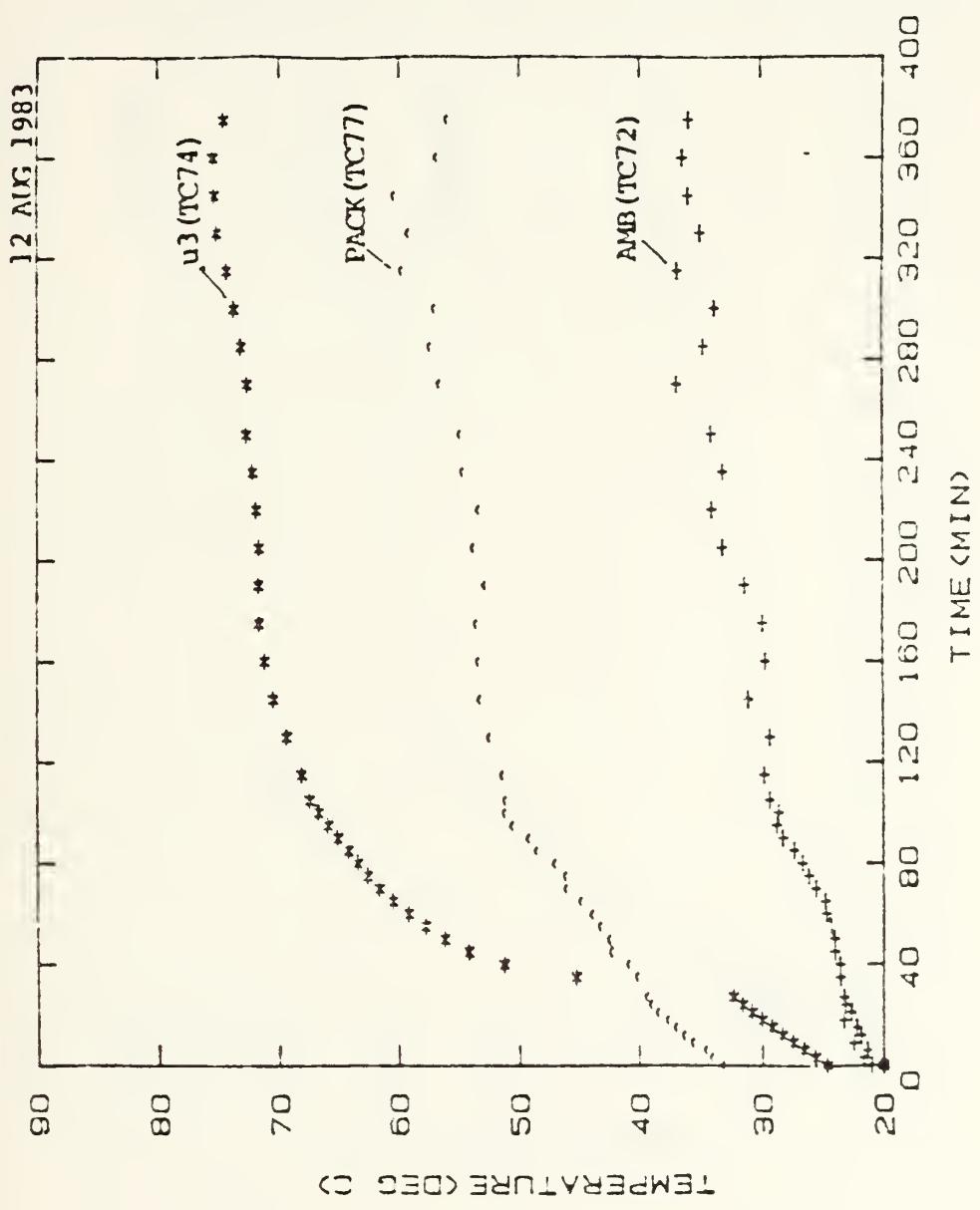


Figure 3.6 12 AUGUST 1983 - graph 3.

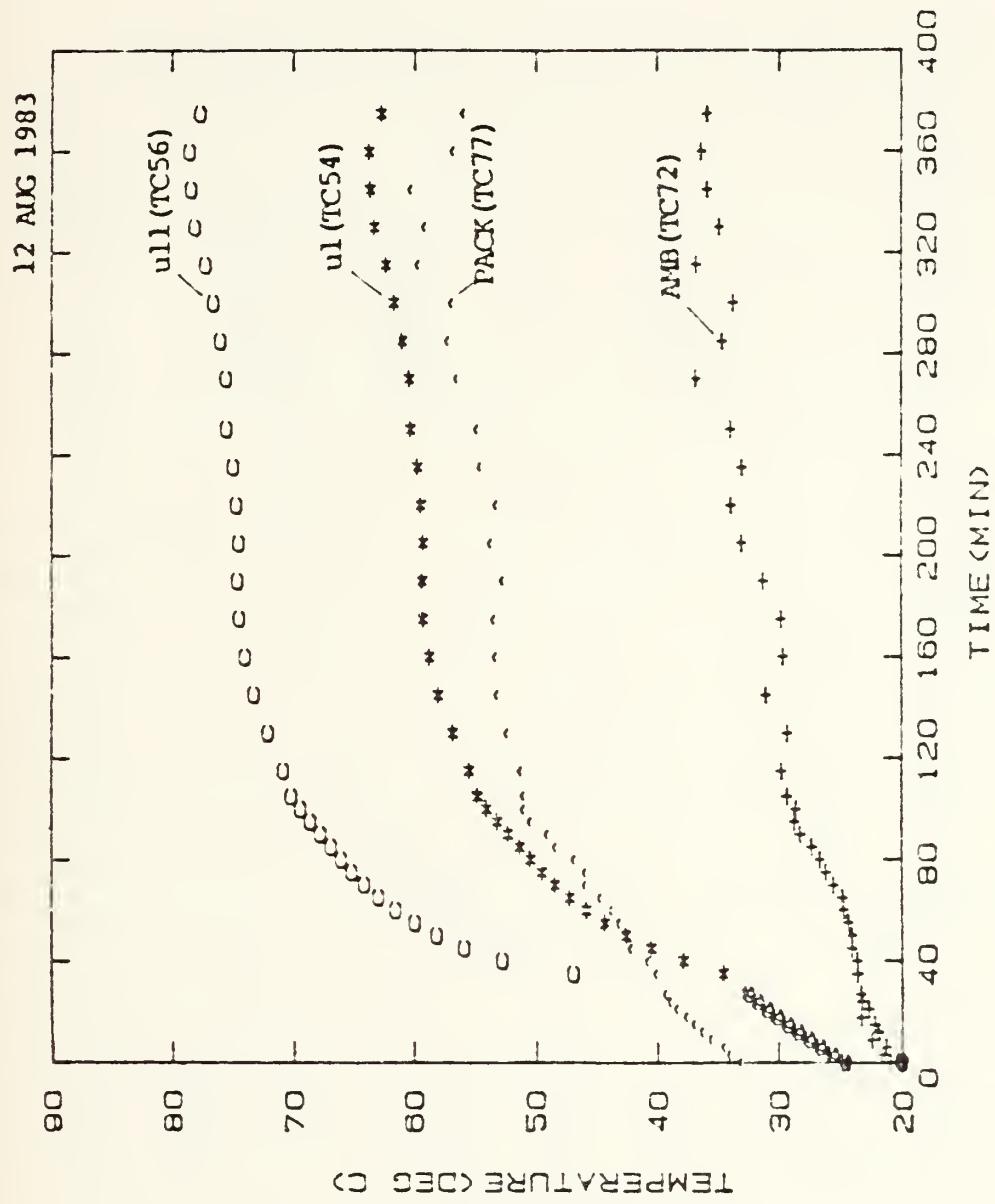


Figure 3.7 12 AUGUST 1983 - graph 4.

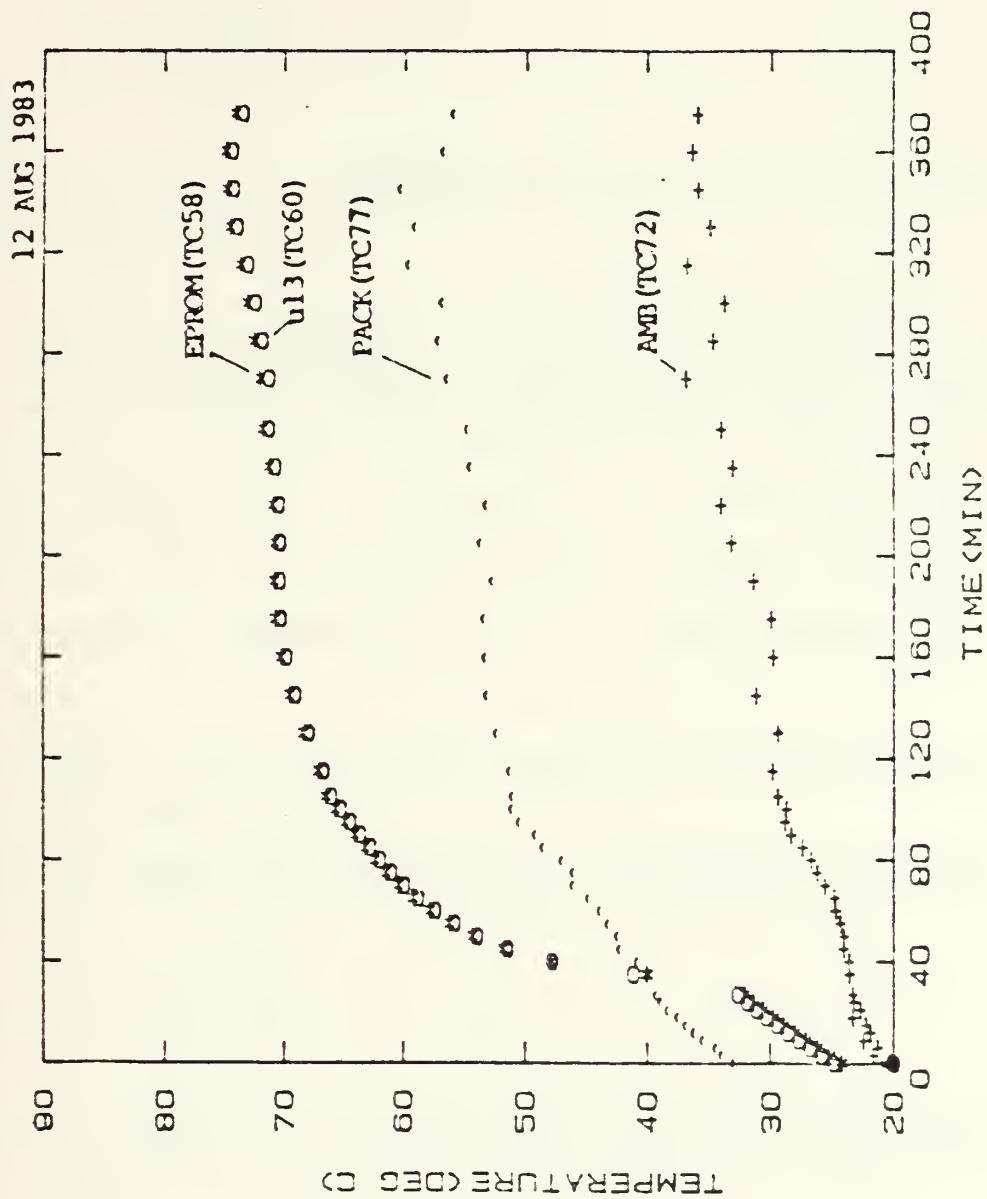


Figure 3.8 12 AUGUST 1983 - graph 5.

- None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures achieved are shown in Figures 3.9 to 3.11 and are listed here as:

$u_{11} = 76.11^\circ\text{C}$
 $u_3 = 66.80^\circ\text{C}$
 $u_{13} = 77.54^\circ\text{C}$
 $u_1 = 84.58^\circ\text{C}$

- As a result of internal heat produced by the ULM, the internal pack temperature reached a maximum of $54.8^\circ\text{C} - 6^\circ\text{C}$ above ambient.
- Unexpected temperature fluctuations occurred at 45, 120, and 300 minutes on TC's 42, 64, 68 and 72. Since the only thermocouples experiencing these fluctuations were attached to powered components, this may have been caused by a power fluctuation of the power supply.

The second test of the model on 15 August 1983 was conducted again in the environmental chamber set this time to an ambient temperature of 37.7°C . Observations from this test are:

- None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures achieved are shown in Figures 3.12 to 3.14 and are listed here as:

$u_{11} = 60.22^\circ\text{C}$
 $u_3 = 52.33^\circ\text{C}$
 $u_{13} = 63.60^\circ\text{C}$
 $u_1 = 68.78^\circ\text{C}$

- As a result of internal heat produced by the model, the internal pack temperature reached a maximum of 41.1°C .
- Steady state was achieved between 80 and 120 minutes after power was applied.
- Unexpected temperature fluctuations occurred in TC's 53 and 68, between 5 and 15 minutes. These fluctuations cannot be explained.

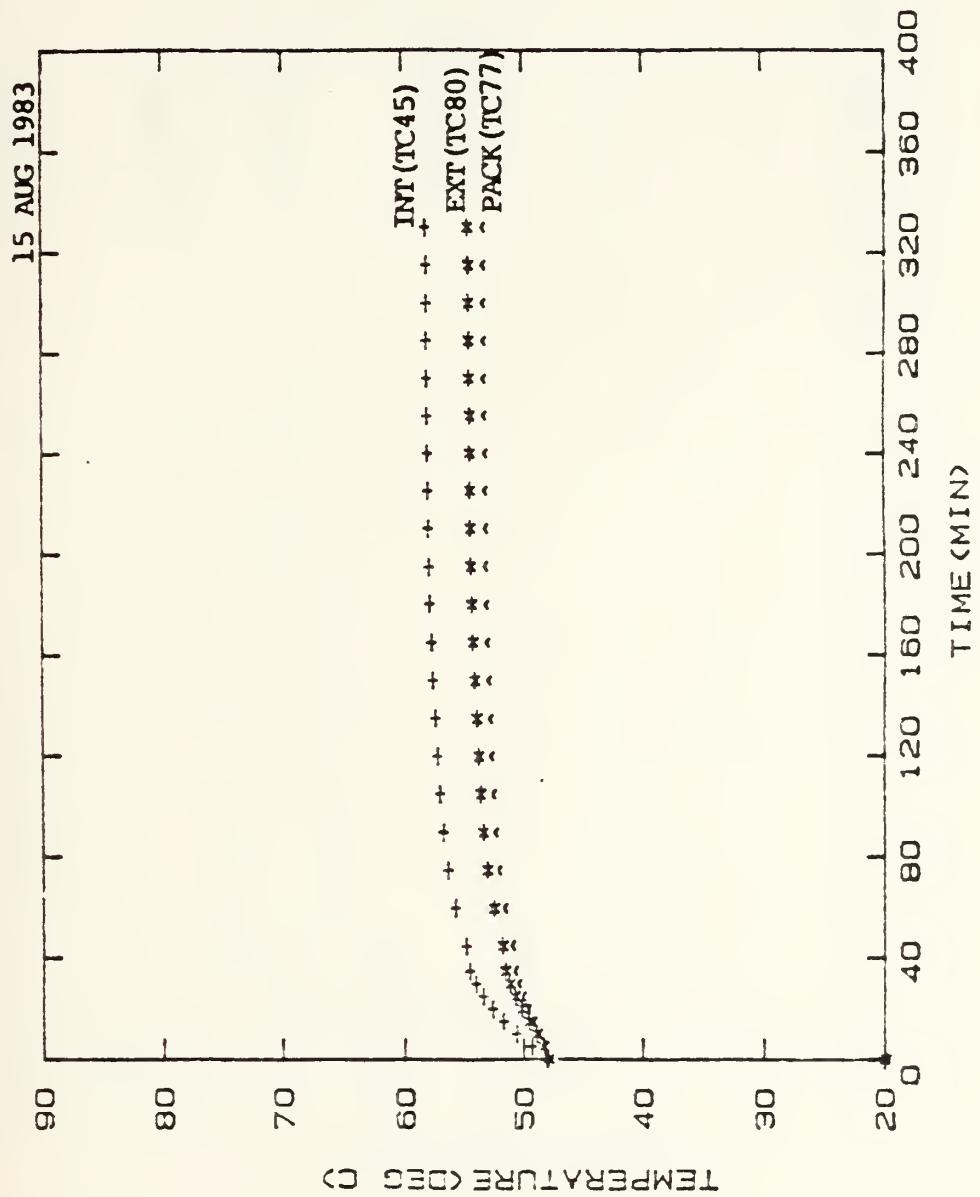


Figure 3.9 15 AUGUST 1983 (AMBIENT = 48.8C) - graph 1.

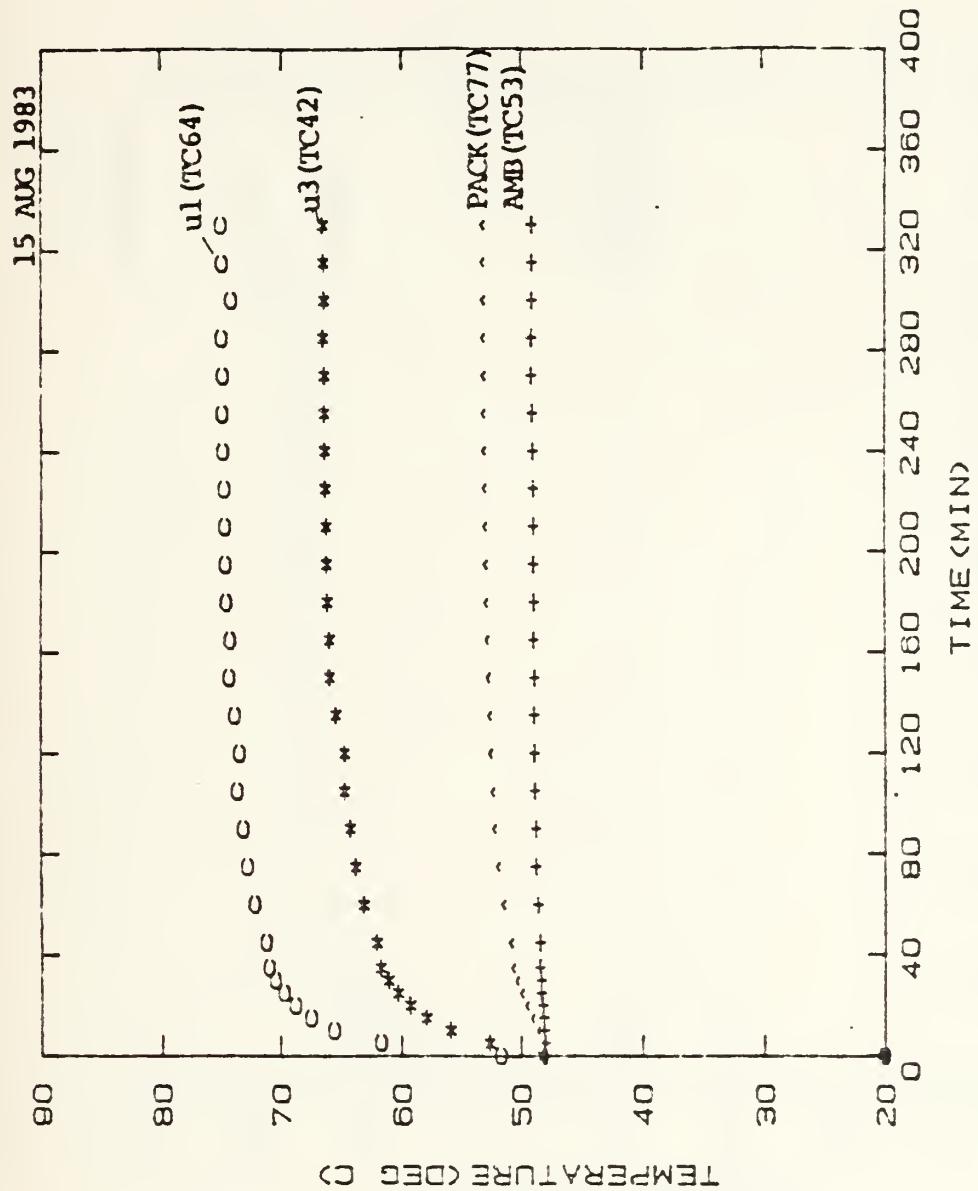


Figure 3.10 15 AUGUST 1983 (AMBIENT = 48.8C) - graph 2.

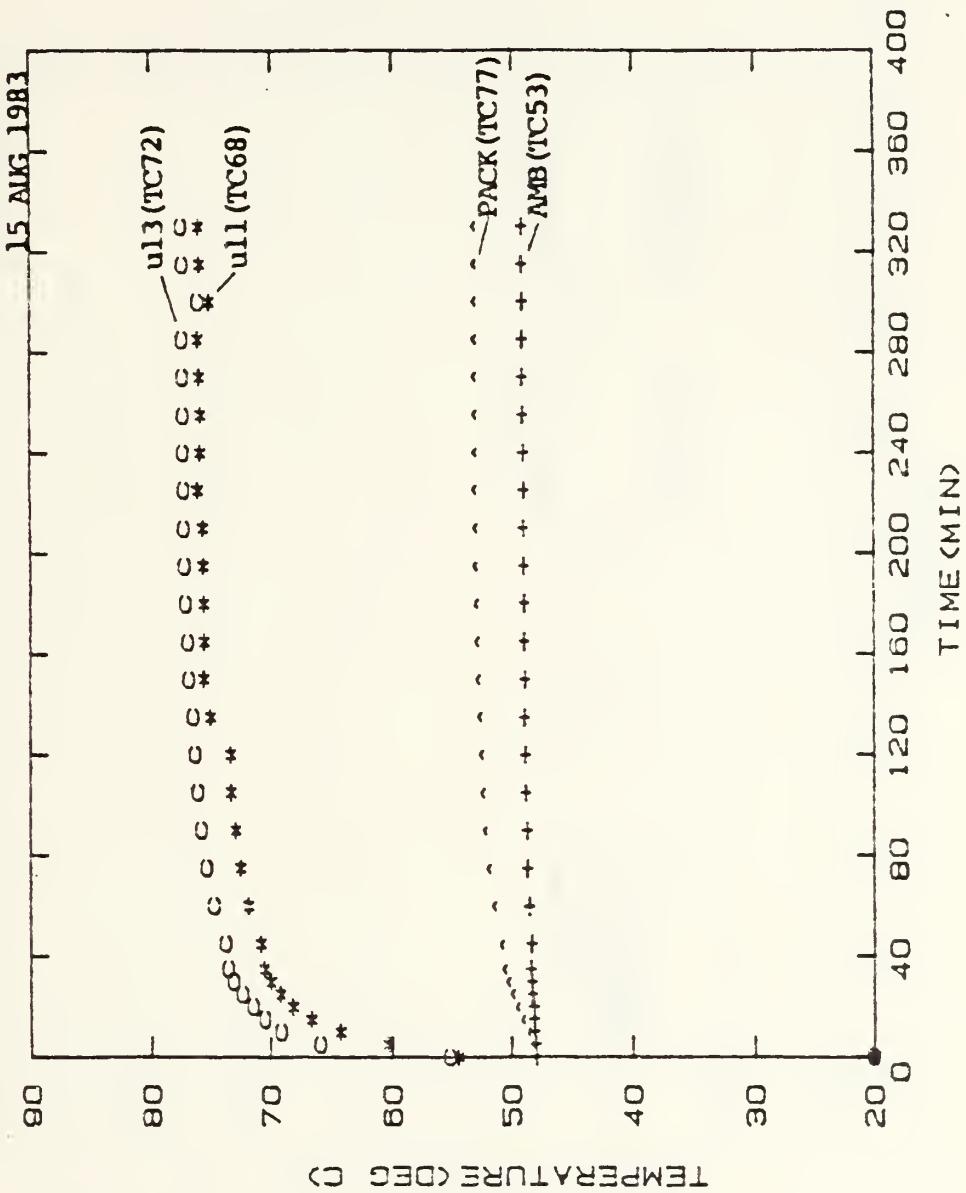


Figure 3.11 15 AUGUST 1983 (AMBIENT = 48.8°C) - graph 3.

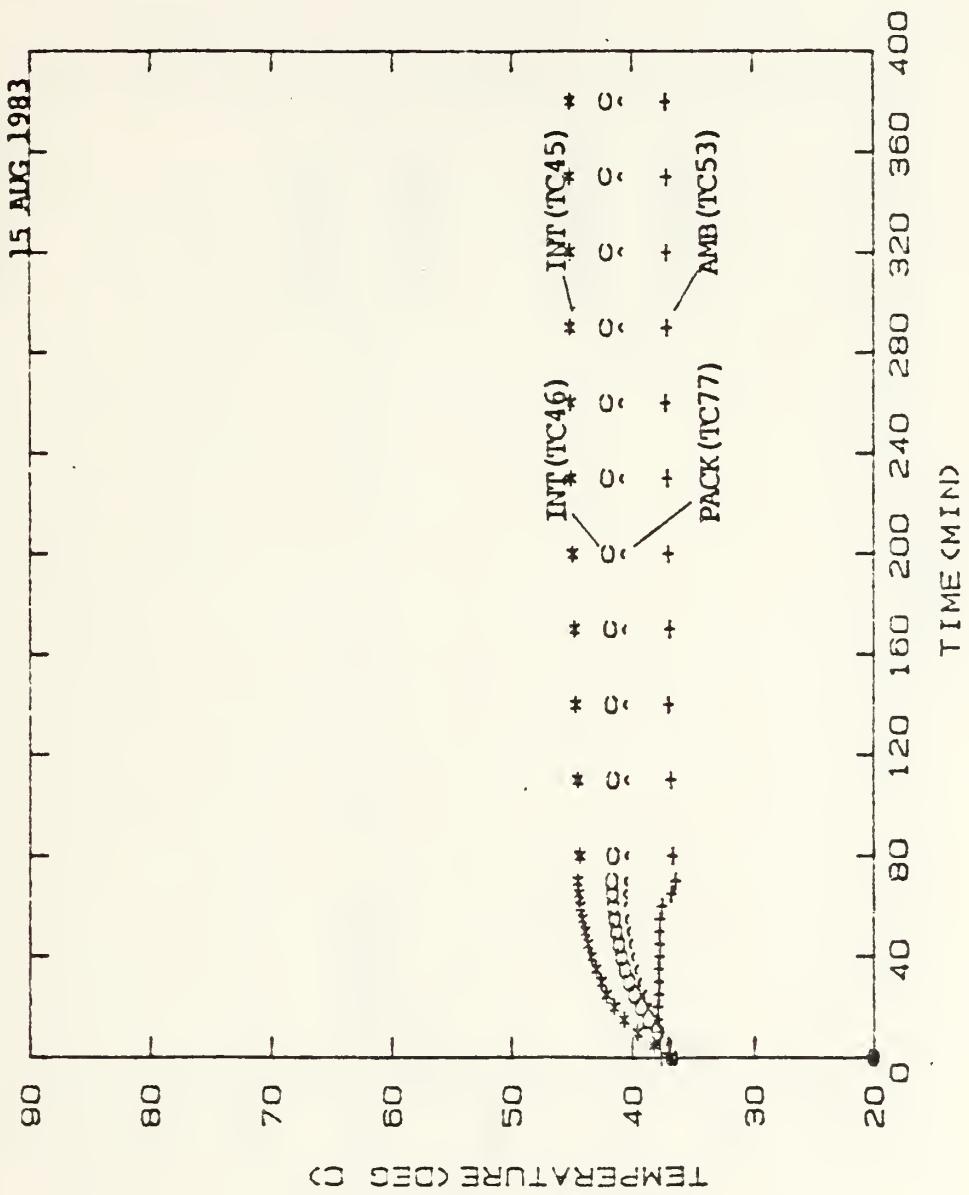


Figure 3.12 15 AUGUST 1983 (AMBIENT = 37.7°C) - graph 1.

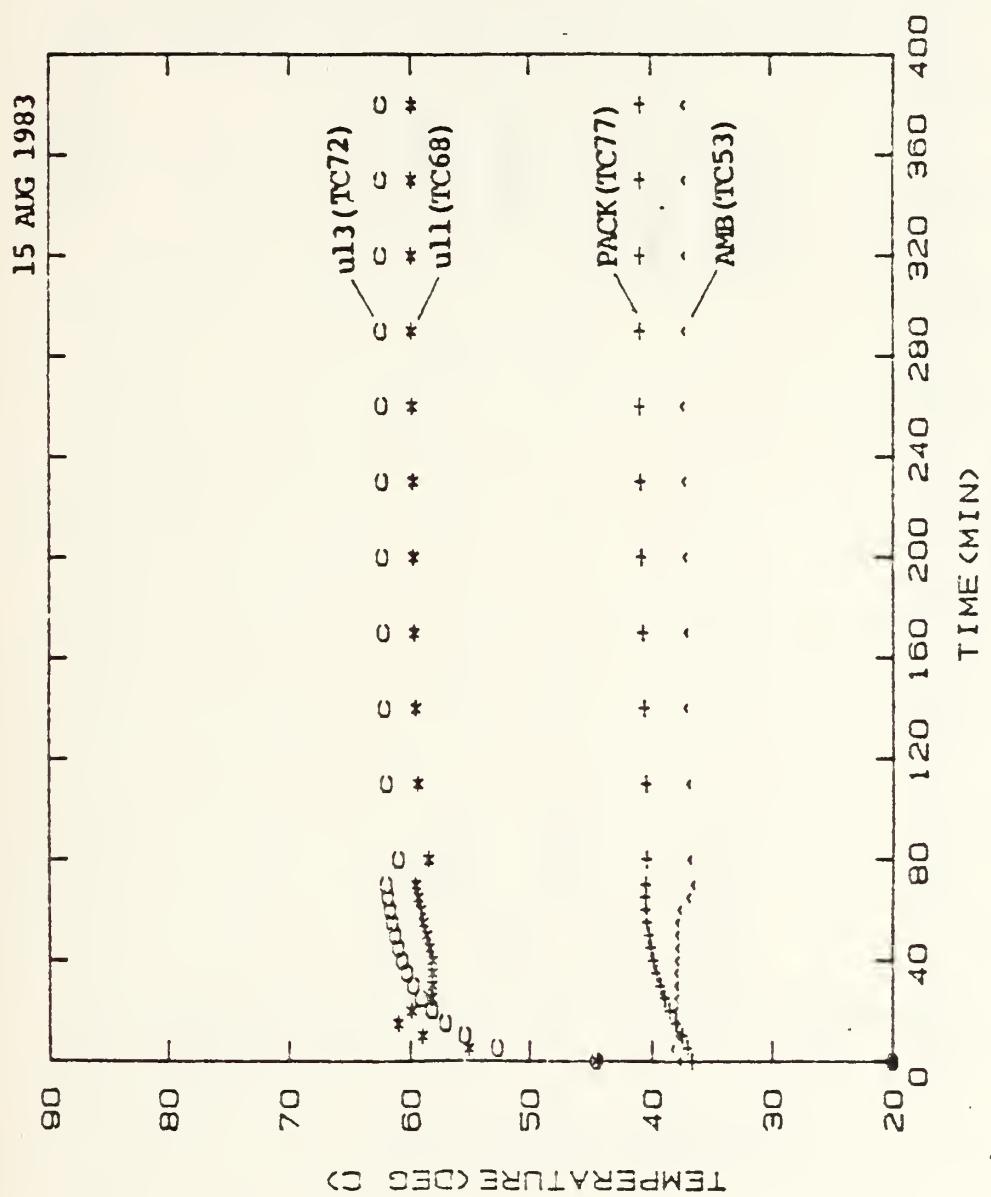


Figure 3.13 15 AUGUST 1983 (AMBIENT = 37.7°C) - graph 2.

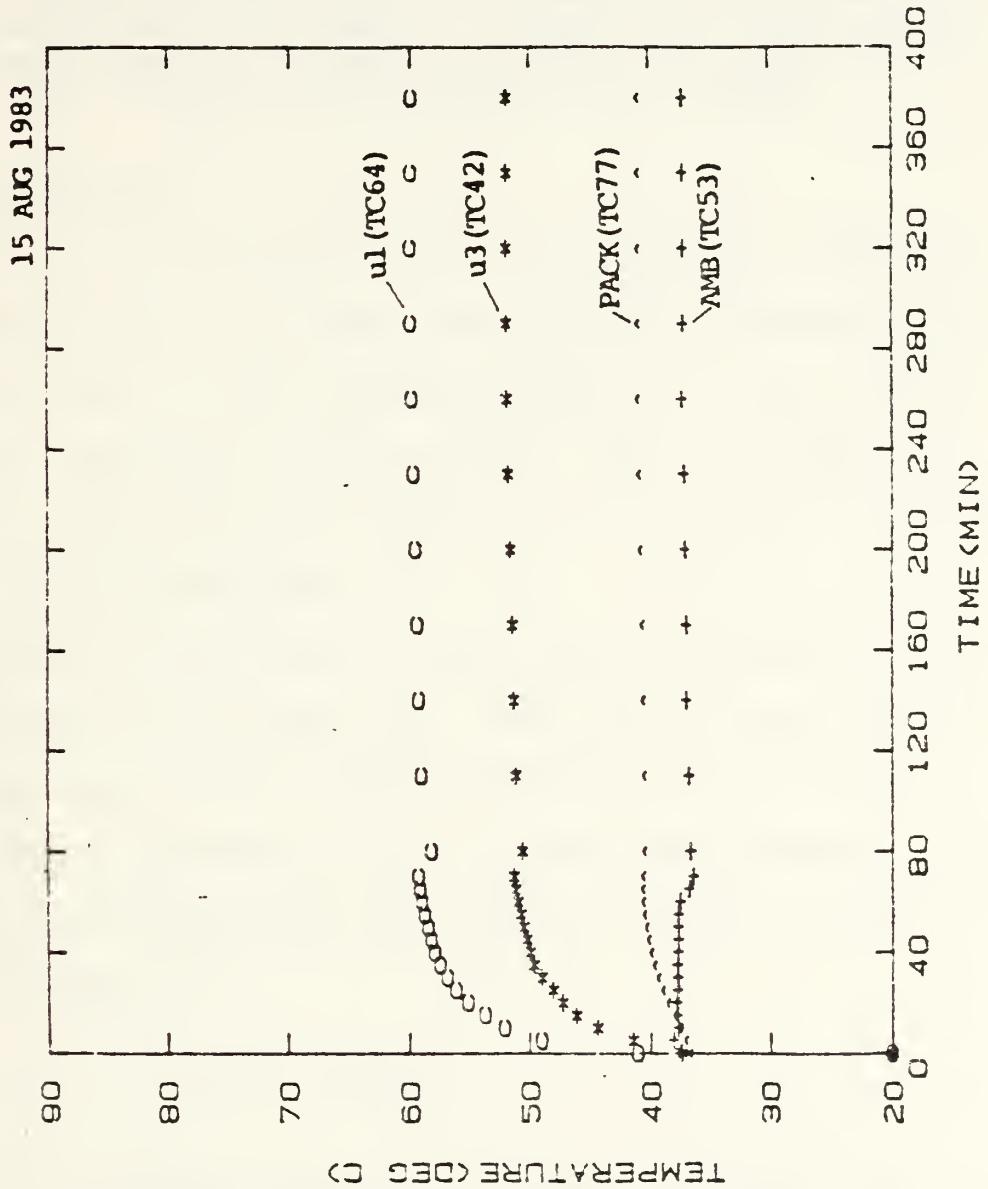


Figure 3.14 15 AUGUST 1983 (AMBIENT = 37.7°C) - graph 3.

- Unexpected temperature fluctuations occurred in all thermocouples between 50 and 80 minutes. It appears that all the fluctuations lag slightly behind that of the ambient air fluctuation. An actual change in ambient air temperature would have this type of delayed response. Since the environmental chamber was not monitored continuously, the door may have inadvertently been opened, or there may have been a short loss of power to the heating system of the chamber.

B. DISCUSSION

The ULM and backpack will be subjected to ambient environments ranging typically from 21C to 38C during the warm summer season. Solar loading--typical of a Ft. Hunter Liggett summer day--could add 22C higher environmental temperatures within the backpack resulting in a higher stress experienced by the ULM.

Energy in the form of heat will naturally flow from a hot element to a colder one. The rate of heat flow (Q) is proportional to the temperature difference (ΔT) and inversely proportional to the thermal resistance (θ) of the medium through which the heat is flowing. This relationship is:

$$Q = (\Delta T) / \theta$$

In the ULM--as in most electronic equipment--most of the energy used to power the equipment is converted to heat, causing the equipment temperature to rise. The temperature will continue to rise unless the heat can be removed. In the ULM, the power input to the module is the

total energy that must be dissipated. In the case of the ULM, the ultimate sink for thermal energy is the air outside the backpack. Both the air inside the backpack and the backpack itself, can be considered local sinks through which all energy leaving the ULM must flow [Ref. 4].

There are three modes of heat transfer at work in most systems:

- Conduction refers to heat transfer across a medium resulting from kinetic energy interchange between molecules or by electron drift [Ref. 5]. Conduction can occur in a solid, liquid, or gas and is the only mode of heat transfer occurring in an opaque solid [Ref. 4].
- Convection heat transfer occurs at the interface between a solid and a fluid at a different temperature when fluid motion is present. The fluid of this analysis is air. Motion caused by the density differences associated with the temperature variation within the fluid is called natural convection. Motion caused by external methods is forced convection. In this analysis the only forced convection is when wind is present [Ref. 5].
- Radiation heat transfer refers to the energy emitted by matter in the form of electromagnetic waves. Given two surfaces at different temperatures, each will be emitting and exchanging thermal radiation. However, the net radiation exchange is in the direction of hot to cold and will continue until both surfaces are the same temperature. At this point the net radiation will be zero [Ref. 6]. The net radiation occurring between two bodies with similar surface material, is a function of the intensity which varies with the viewing direction between the emitting surfaces. Thus the energy transferred from one surface to another is a function of the area of the receiving surface "seen" by the emitting surface [Ref. 5].

The primary heat flow paths of this system are:

- From each component to the ULM case via convection and conduction.

- From ULM case to backpack by convection through the air, by conduction through the backpack frame, and by radiation.
- From backpack to ambient air via forced and natural convection, and radiation.

Because of the geometric positioning of the components, radiation was not considered as playing a very significant role in the component to ULM case heat flow path. The dissipating elements are flat DIP devices whose sides make up a small proportion of emitting surface. The greatest surface area is the top of each component. When assembled, each of these surfaces is facing another dissipating surface. This would have an effect of heating the lower temperature device, but as both are power dissipators, the net effect in terms of energy dissipation would be negligible.

Natural convection and conduction would be the primary heat transfer modes of energy transfer from the component to the air. Since the ULM was hermetically sealed, the only fluid motion would be caused by natural convection. The dense packing of the components leaves little room for temperature gradients to occur between components on the same board. The space between the boards and the top surfaces of the components vary with the component. Some components would act as barriers to air flow resulting from adjacent components. Unfortunately, all high power dissipating components are clustered at one end of the ULM.

Additionally, the hot components of the I/O board directly face the hot components of the CPU board. Since the air is being heated from two directions, the cooling effect of the air on the surface of each component is reduced. Thus, due to the geometric configuration and high concentration of high power dissipators, it is postulated that much of the advantage in cooling achieved by natural convection is offset by the dual heating effect. This would leave conduction as the dominant heat transfer mode within the ULM.

Conduction within the ULM will occur from component to air to the case, and component to board to the case. Since the boards are separated from the case by electrically insulating gaskets, most of the conduction will take place from boards and components to the air--then to the case. With the available data, however, it is impossible to quantify how much heat is conducted by the boards to the case compared to conduction from the components to the case.

Ideally all thermal paths with their individual resistances would be calculated. However, the complexity of this device and amount of instrumentation required for this type of analysis made such a task impractical. It would have required calculating not only the path of the energy from each component to the ultimate sink, but also

the effect each of the other components would have at each temperature along the path. Even if the device could be instrumented to determine all of these temperatures, the individual power dissipating rates for each component of the actual ULM would have to be available. This data was not available. Unfortunately there is little correlation between the behavior and resistances of IC components and the resistors used to model the components. This is because power dissipation in the IC components is frequency dependent and not based solely on voltage supplied to and the resistance of the component. This is the case for the model, which is made of resistors having a fixed value. Thus little correlation existed between the actual component and its model, in terms of individual power dissipation. Knowing the total dissipation of the ULM enabled calculating an equivalent thermal resistance from the internal backpack air to the ambient air shown in Figure 3.15. These calculations are based on the following assumptions:

- The temperature measured inside the backpack is assumed to be representative of the average value of the air within the backpack.
- Heat dissipated by the backpack frame directly to the ambient air is assumed to be negligible compared to the heat dissipated by the internal backpack air through the canvas to the ambient air.

Using data from the environmental chamber on 13, 14, 15 August, 1983, and the relation:

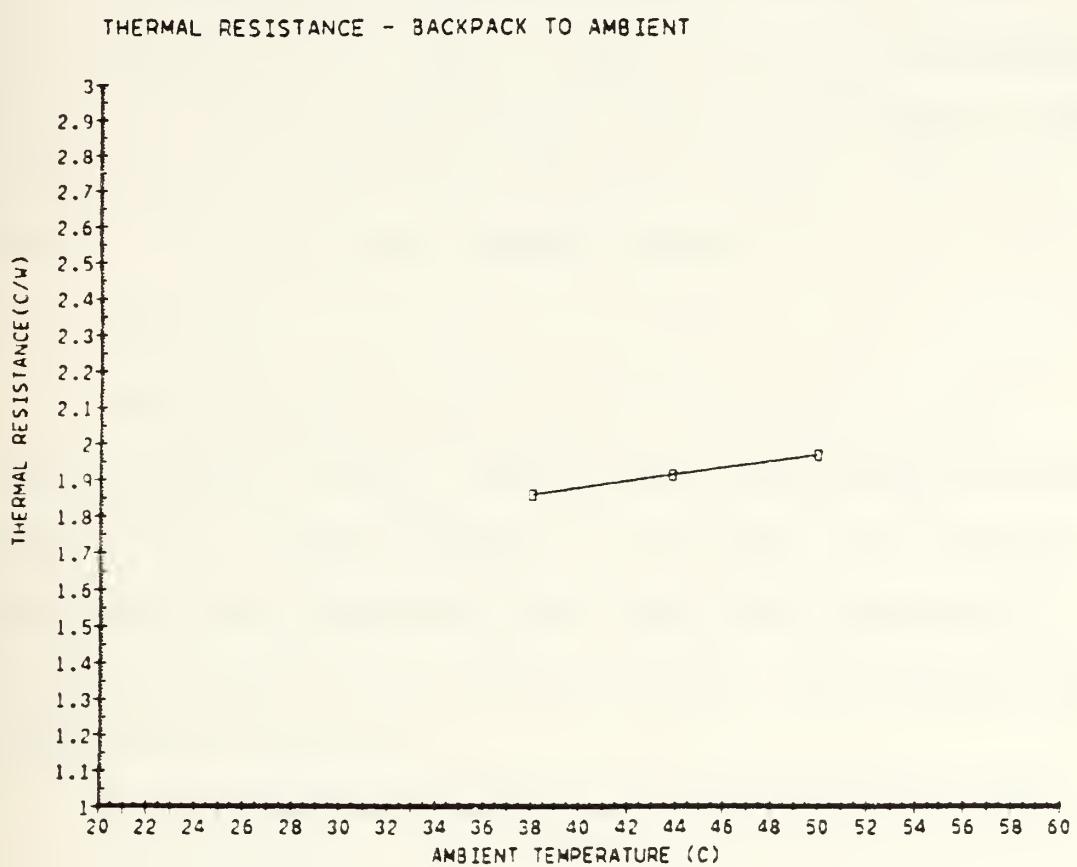


Figure 3.15 THERMAL RESISTANCE OF PACK AIR TO AMBIENT.

$$Q = \theta / \Delta T$$

Theta was calculated as 1.86 C/W for the test of 12 Aug 83. Therefore, since the total heat within the pack was the sum of the ULM load and the solar load, the solar load was calculated as 29.67 watts. This is as if in the absence of solar loading, the ULM--at 8 watts--was joined in the backpack by an additional unit of 30 watts. This is a very significant additional thermal stress.

C. CONCLUSION

Operating under typical power consumption rates (approximately 8 watts) under design environmental conditions of Ft. Hunter Liggett in the summer, all internal components were measured to be below their specified critical temperatures of 85C or higher. The design conditions meant here are:

- An environmental temperature range of 21C to 38C (70F to 100F)
- The ULM mounted in a backpack
- No additional internal heat sources
- The backpack in direct sunlight
- No wind.

However, operating under these conditions causes several of the components, whose critical temperatures are 85C, to be within 5 to 10C of that limit. Therefore, any slight increase in power over 8 watts, or increase in ambient

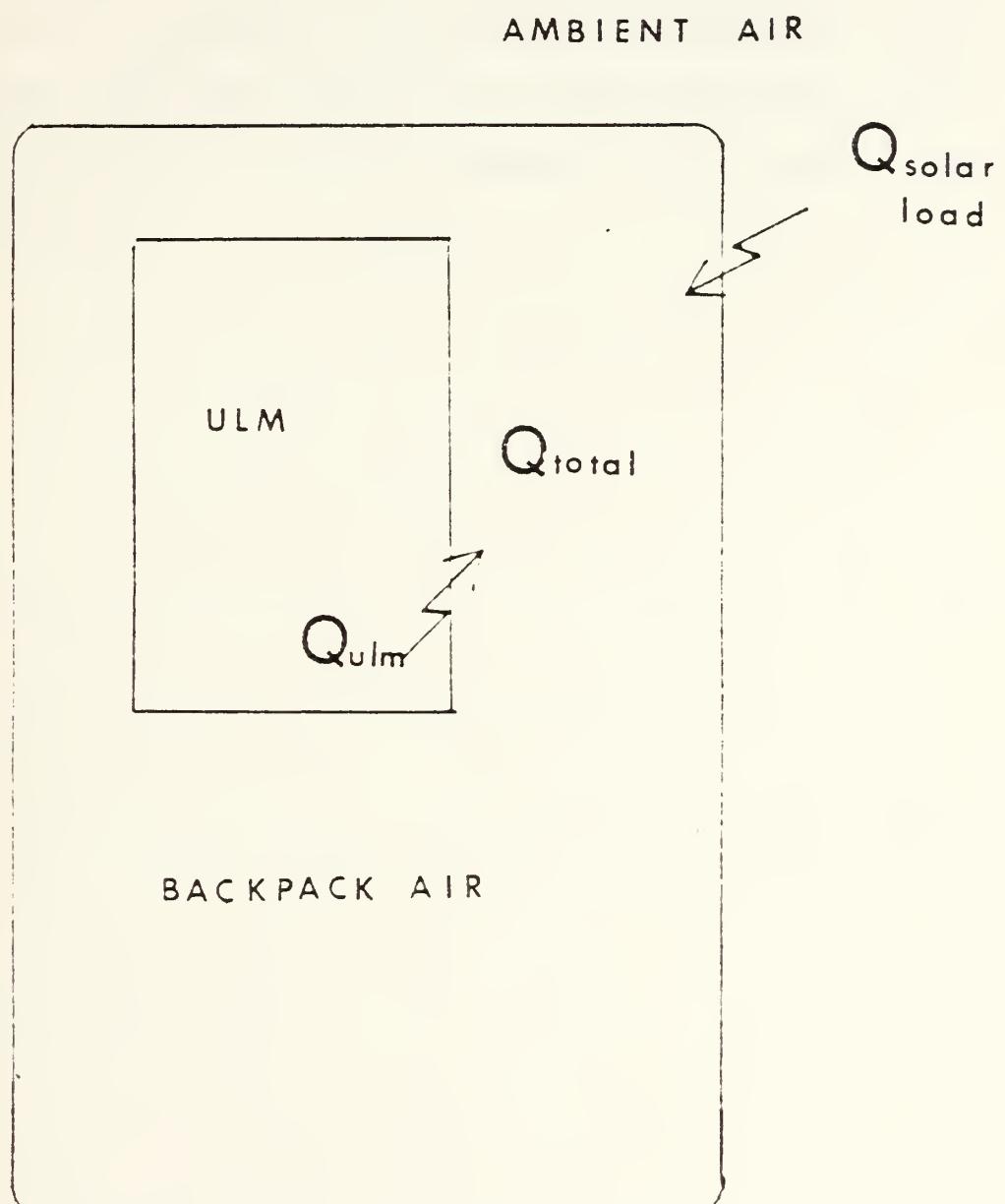


Figure 3.16 ENERGY BALANCE ON THE BACKPACK.

temperature above 38C, could cause one or more of the components to exceed specifications. Then reliability of the system could not be predicted, and would be substantially decreased. Conversely, the absence of direct sunlight and/or the addition of wind would have a beneficial effect on the ULM by decreasing the thermal stress on the unit.

APPENDIX A
EQUIPMENT LIST

The following is a list of the equipment used for this analysis:

- Thermocouples were made of copper-constantan, 30 gauge, teflon coated thermocouple wire.
- The HP3054A Automated Data Acquisition System was used for data acquisition which consists of:

 HP3497 Data Acquisition Control Unit

 HP3456 Digital Voltmeter for obtaining data from the thermocouples

- The HP9826 Desktop computer was used to control data acquisition, storage of data, computation and display of data.
- The Lambda 60 volt power supply was used to provide power to the ULM and model.
- A Controlled Acoustic Environmental Chamber manufactured by Industrial Acoustics Company Inc. was used for simulating ambient temperatures up to 48.8C (120F).

APPENDIX B
THERMOCOUPLE CALIBRATION

The following is a list of equipment used during the calibration of the thermocouples:

- Rosemount Engineering Model 920a Commutating Bridge
- Rosemount Model 162 Platinum Resistance Temperature Standard
- HP3054 Data Acquisition System
- HP9826 Desktop Computer

A computer program listed on page 62 was written for the HP9826 to:

- Read emf values from the thermocouples
- Store the emf values in a data file
- Convert the emf values to temperatures based on a reference relative to platinum at 0C.
- Compare these temperatures to temperatures obtained from the platinum resistance standard.

A second program was written to fit a second degree polynomial to the comparison above and for obtaining coefficients to apply to each thermocouple. This program is listed on page 63.

The thermocouples and the platinum resistance standard were placed in the calibration bath. The temperature of the bath was cycled from 10C to 100C and back to 10C. Temperature measurements were taken at 20 degree increments

ascending and descending the scale. Coefficients correcting the thermocouple temperatures to the standard temperatures were calculated and listed on pages 64-67.


```

100! FILE NAME: CAL
110! REVISED: May 20, 1982
120 COM /C17 C(7)
130 DIM Emf(39),T(39),Delta(29)
140 DATA 0.10086091,25727.94369,-767345.8295,78025595.81
150 DATA -9247486589,6.97688E+11,-2.66192E+13,3.94078E+14
160 READ C(*)
170 PRINTER IS 701
180 SLEEP
190 INPUT "ENTER MONTH, DATE AND TIME (MM:DD:HH:MM:SS)":Date$
200 OUTPUT 709;"TD";Date$
210 OUTPUT 709;"TD"
220 ENTER 709:Date$
230 PRINT USING "12X,***Month, date and time: ***,14A":Date$
240 BEEP
250 INPUT "GIVE A NAME FOR DATA FILE":D_file$
260 CREATE BDAT D_file$,30
270 ASSIGN #File TO D_file$
280 J=0
290 Repeat: !
300 J=J+1
310 BEEP
320 INPUT "ENTER BATH TEMPERATURE (DEG F)":T_bath
330 PRINT ""
340 PRINT USING "12X,***Data set number = ***,DD.":J
350 PRINT USING "12X,***Bath temperature = ***,.4D.DP,*** (Deg F)***":T_bath
360 OUTPUT 709;"AR AF40 AL79"
370 OUTPUT 722;"F1 R1 T1 Z1 FL1"
380 FOR I=0 TO 39
390 OUTPUT 709;"AS SA"
400 ENTER 722:Emf(I)
410 T(I)=FN1vsV(Emf(I))
411 Delta(I)=T_bath-T(I)
420 NEXT I
430 PRINT USING "(12X.5(5D,2D,2X),18X)":T(*)
431 PRINT ""
432 PRINT USING "***DELTAS=***"
433 PRINT USING "(12X.5(5D,2D,2X),18X)":Delta(*)
440 OUTPUT #File:T_bath,T(*)
450 BEEP
460 INPUT "ARE YOU TAKING MORE DATA (1=YES,0=NO)?":Go_on
470 IF Go_on=1 THEN Repeat
480 BEEP
490 PRINT ""
500 PRINT USING "***Duns were stored in file ***.DIA":I,D_file$
510 END
520 DEF FN1vsV(V)
530 COM /C17 C(7)
540 T=0.
550 FOR I=0 TO 7
560 T=T+C(I)*V I
570 NEXT I
580 RETURN T+1.8+32
590 FNEND

```



```

1 ! FILE NAME:COEF_CAL
2 !REVISED:18 MAY 1983
3 DIM Enf(39),T(39),Delta(39),Sx(39),Sy(39),Sx2(39),Sx3(39),Sx4(39),Sxy(39)
4 DIM Sx2y(39),Det(39),Det0(39),Det1(39),Det2(39),A0(39),A1(39),A2(39),D(39)
10 BEEP
20 INPUT "ENTER THE FILE NAME",D_file$ 
30 ASSIGN #File TO D_file$
31 CREATE BDAT "COE",20
32 ASSIGN #File2 TO "COE"
40 BEEP
50 INPUT "ENTER NUMBER OF RUNS STORED",Nrun
60 FOR I=0 TO 39
70 Sx(I)=0
80 Sx2(I)=0
90 Sx3(I)=0
100 Sx4(I)=0
110 Sy(I)=0
120 Sxy(I)=0
130 Sx2y(I)=0
140 NEXT I
150 FOR I=1 TO Nrun
160 ENTER #File:T_bath,T(*)
170 FOR J=0 TO 39
180 D(J)=T_bath-T(J)
190 Sx(J)=Sx(J)+T(J)
200 Sx2(J)=Sx2(J)+T(J)^2
210 Sx3(J)=Sx3(J)+T(J)^3
220 Sx4(J)=Sx4(J)+T(J)^4
230 Sy(J)=Sy(J)+D(J)
240 Sxy(J)=Sxy(J)+D(J)+T(J)
250 Sx2y(J)=Sx2y(J)+D(J)+T(J)^2
260 NEXT J
270 NEXT I
280 PRINT "          T/C      A0      A1      A2"
290 PRINT " "
300 FOR J=0 TO 39
310 Det(J)=40*Sx2(J)*Sx4(J)+Sx(J)*Sx3(J)*Sx2(J)+2-Sx2(J)^3-Sx(J)^2*Sx4(J)-40*S
x*(J)^2
320 Det(J)=Sx(J)*Sx2(J)*Sx4(J)+Sx(J)*Sx3(J)*Sx2y(J)+Sxy(J)*Sx3(J)*Sx2(J)
330 Det0(J)=Dd-Ds-Sx2(J)^2+Sx2y(J)-Sx(J)*Sxy(J)*Sx4(J)-Sy(J)*Sx3(J)^2
340 De=40*Sxy(J)*Sx4(J)+Sy(J)*Sx3(J)*Sx2(J)+Sx2(J)*Sx2y(J)-Sx2y(J)*Sx(J)
350 Det1(J)=De-Sx2(J)^2+Sxy(J)-Sx(J)*Sy(J)*Sx4(J)-40*Sx3(J)*Sx2y(J)
360 Df=40*Sx3(J)*Sx2y(J)+Sx(J)*Sxy(J)*Sx2(J)+Sx(J)*Sx3(J)*Sy(J)
370 Det2(J)=De-Sx2(J)^2+Sy(J)-Sx(J)^2+Sxy(J)-40*Sx3(J)*Sxy(J)
380 A0(J)=Det0(J)/Det(J)
390 A1(J)=Det1(J)/Det(J)
400 A2(J)=Det2(J)/Det(J)
410 PRINT USING "14X.00,4X,3(80,60,4X)":J+1,A0(J),A1(J),A2(J)
420 OUTPUT #File2:A0(J),A1(J),A2(J)
430 NEXT J
440 END

```


47

	EXONENT	COEFFICIENT	T/C=
0	-3.1930275E-01	0	-2.0144173E-01
1	1.0128575E+00	1	1.0087372E+00
2	-5.4818475E-05	2	-3.5634842E-05

48

	EXONENT	COEFFICIENT	T/C=
0	-2.2522528E-01	0	-2.8066019E-01
1	1.0107620E+00	1	1.0104503E+00
2	-4.5712065E-05	2	-4.4520679E-05

49

	EXONENT	COEFFICIENT	T/C=
0	-1.9938344E-01	0	-3.0628157E-01
1	1.0095769E+00	1	1.0108137E+00
2	-4.1260696E-05	2	-4.5446338E-05

50

	EXONENT	COEFFICIENT	T/C=
0	-2.4667796E-01	0	-2.7662537E-01
1	1.0108583E+00	1	1.0102160E+00
2	-4.6423785E-05	2	-4.2556286E-05

51

	EXONENT	COEFFICIENT	T/C=
0	-2.5058039E-01	0	-2.4360369E-01
1	1.0104461E+00	1	1.0102052E+00
2	-4.3850226E-05	2	-4.5606545E-05

52

	EXONENT	COEFFICIENT	T/C=
0	-1.4662748E-01	0	-2.7754513E-01
1	1.0081341E+00	1	1.0100960E+00
2	-3.3403832E-05	2	-4.4413257E-05

EXONENT	COEFFICIENT	T/C=	53	EXPONENT	COEFFICIENT
0	-3.5887496E-01			0	-3.9258228E-01
1	1.0114225E+00			1	1.0109995E+00
2	-4.7818694E-05			2	-4.6366880E-05
EXONENT	COEFFICIENT	T/C=	54	EXPONENT	COEFFICIENT
0	-3.2936623E-01			0	-2.9769225E-01
1	1.0102503E+00			1	1.0095916E+00
2	-4.3399839E-05			2	-4.1222481E-05
EXONENT	COEFFICIENT	T/C=	55	EXPONENT	COEFFICIENT
0	-3.5742917E-01			0	-2.7987174E-01
1	1.0111652E+00			1	1.0121568E+00
2	-4.7246171E-05			2	-4.9924368E-05
EXONENT	COEFFICIENT	T/C=	56	EXPONENT	COEFFICIENT
0	-4.1638880E-01			0	-1.9282761E-01
1	1.0117568E+00			1	1.0102605E+00
2	-4.8533907E-05			2	-4.2767110E-05
EXONENT	COEFFICIENT	T/C=	57	EXPONENT	COEFFICIENT
0	-3.6276984E-01			0	-2.1019688E-01
1	1.0105931E+00			1	1.0103867E+00
2	-4.4865618E-05			2	-4.4603609E-05
EXONENT	COEFFICIENT	T/C=	58	EXPONENT	COEFFICIENT
0	-3.3989581E-01			0	-2.4817587E-01
1	1.0102587E+00			1	1.0112909E+00
2	-4.4930951E-05			2	-4.8233817E-05

EXONENT	COEFFICIENT	T/C=	61	EXponent	T/C=
0	-3.2936623E-01			0	-2.7987174E-01
1	1.0102503E+00			1	1.0121568E+00
2	-4.3399839E-05			2	-4.9924368E-05
EXONENT	COEFFICIENT	T/C=	62	EXponent	T/C=
0	-4.1638880E-01			0	-1.9282761E-01
1	1.0117568E+00			1	1.0102605E+00
2	-4.8533907E-05			2	-4.2767110E-05
EXONENT	COEFFICIENT	T/C=	63	EXponent	T/C=
0	-3.6276984E-01			0	-2.1019688E-01
1	1.0105931E+00			1	1.0103867E+00
2	-4.4865618E-05			2	-4.4603609E-05
EXONENT	COEFFICIENT	T/C=	64	EXponent	T/C=
0	-3.3989581E-01			0	-2.4817587E-01
1	1.0102587E+00			1	1.0112909E+00
2	-4.4930951E-05			2	-4.8233817E-05

EXONENT	COEFFICIENT	T/C=	65	EXPONENT	COEFFICIENT	T/C=
0	-1.9101588E-01			0	-3.4055123E-01	
1	1.0104827E+00			1	1.0121429E+00	
2	-4.5500415E-05			2	-4.9454810E-05	
EXONENT	COEFFICIENT	T/C=	66	EXPONENT	COEFFICIENT	T/C=
0	-2.6448185E-01			0	-2.2716454E-01	
1	1.0116511E+00			1	1.0104838E+00	
2	-5.0080800E-05			2	-4.5364118E-05	
EXONENT	COEFFICIENT	T/C=	67	EXPONENT	COEFFICIENT	T/C=
0	-1.7570321E-01			0	-3.4035121E-01	
1	1.0100325E+00			1	1.0119056E+00	
2	-4.4527871E-05			2	-4.9277126E-05	
EXONENT	COEFFICIENT	T/C=	68	EXPONENT	COEFFICIENT	T/C=
0	-2.7670041E-01			0	-3.3760097E-01	
1	1.0119687E+00			1	1.0126166E+00	
2	-5.0293806E-05			2	-5.3815004E-05	
EXONENT	COEFFICIENT	T/C=	69	EXPONENT	COEFFICIENT	T/C=
0	-3.3189622E-01			0	-3.5448472E-01	
1	1.0129848E+00			1	1.0124541E+00	
2	-5.4476114E-05			2	-5.0742084E-05	
EXONENT	COEFFICIENT	T/C=	70	EXPONENT	COEFFICIENT	T/C=
0	-2.3237513E-01			0	-3.4015128E-01	
1	1.0108945E+00			1	1.0118546E+00	
2	-4.6776910E-05			2	-4.8928220E-05	

EXONENT	COEFFICIENT	T/C=	
0	-2.8240400E-01		77
1	1.0108175E+00		
2	-4.7151498E-05		
EXONENT	COEFFICIENT	T/C=	
0	-3.3900080E-01		78
1	1.0117118E+00		
2	-4.8660568E-05		
EXONENT	COEFFICIENT	T/C=	
0	-3.2247594E-01		79
1	1.0114324E+00		
2	-4.8182073E-05		
EXONENT	COEFFICIENT	T/C=	
0	-2.6107879E-01		80
1	1.0098416E+00		
2	-4.0564349E-05		

APPENDIX C

PROGRAM LISTING

```
10      JULY
11      VERSION 25 JULY 1983
12      !THIS IS A MODIFICATION OF A PROGRAM WRITTEN BY A. MANNIARACHCHI FOR GENER
13      AL USE ON THE HP3054
14      ! DATA ACQUISITION SYSTEM. MODIFICATIONS DONE BY H. KEEBLER FOR TESTING ON
15      THE
16      ! ULM
17      COM /Co, A(39),B(39),C(39),D(7)
18      DIM Emf(39),T(39),Emf1(39)
19      ASSIGN *Coef TO "COE"
20      FOR I=0 TO 39
21      ENTER *Coef;A(I),B(I),C(I)
22      NEXT I
23      DATA 0,10086091,25727,94369,-767345,8295,78025595,81
24      DATA -9247486589,6,37688E+11,-2.66192E+13,3.94078E+14
25      READ D(*)
26      BEEP
27      PRINTER IS 701
28      CLEAR 709
29      INPUT "ENTER RESISTOR VOLTAGE",RV
30      INPUT "ENTER LOAD VOLTAGE",LV
31      Amp=RV/2.0
32      Pow=Amp*LV
33      PRINT "RESISTOR VOLTAGE=",RV,"VOLTS"
34      PRINT "LOAD VOLTAGE=" " ,LV,"VOLTS"
35      PRINT "CURRENT=" " ,Amp,"AMPS"
36      PRINT "POWER=" " ,Pow,"WATTS"
37      INPUT "ENTER MONTH,DATE, AND TIME (MM:DD:HH:MM:SS)",Times
38      OUTPUT 709;"TD";Times
39      BEEP
40      INPUT "ENTER INPUT MODE(1=3054A-AUTO,2=FILE,3=MANUAL)",In
41      IF In=2 THEN
42      BEEP
43      INPUT "ENTER NAME OF EXISTING DATA FILE",Oldfiles
44      PRINT USING "10X,***THESE RESULTS ARE FROM DATA FILE***,10A";Oldfiles
45      ASSIGN *File TO Oldfiles
46      END IF
47      IF In=1 OR In=3 THEN
48      BEEP
49      INPUT "NEW DATA FILE NAME?",Newfiles
50      CREATE BDAT Newfiles,30
51      ASSIGN *File TO Newfiles
52      INPUT "Enter number of samples",It
53      INPUT "Enter wait time in SEC",I_time
54      END IF
55      BEEP
56      J=1
57      OUTPUT 709;"AR AF40 AL73"
58      OUTPUT 722;"F1 R1 T1 Z1 FL1"
59      J=J+1
60      IF In=1 OR In=3 THEN
61      !READ TEMP OF BOX WALL(INSIDE)
62      PRINT ""
63      PRINT "INSIDE BOX WALL TEMP"
64      FOR I=0 TO 9
65      OUTPUT 709;"AS SA"
66      ENTER 722;Emf(I)
67      IF I<4 THEN 400
68      IF I>5 THEN 400
69      IF Emf(I)<.00001 THEN 400
```



```

395 CALL Tvsy(Emf(I),Emf1(I))
396 Tt=Emf1(I)
397 T(I)=FNTem(Tt,I)
398 PRINT T(I),I+41,J
400 NEXT I
401 !PRINT "INTERNAL AIR TEMP"
402 !READ AIR TEMP MODEL
403 FOR I=10 TO 11
404 OUTPUT 709;"AS SA"
405 ENTER 722;Emf(I)
406 IF Emf(I)<.00001 THEN 450
407 CALL Tvsy(Emf(I),Emf1(I))
408 Tt=Emf1(I)
409 ! T(I)=FNTem(Tt,I)
410 ! PRINT T(I),I+41,J
411 NEXT I
412 PRINT ""
413 PRINT "ULM U1,U11,U13-EPROM/CHIP"
414 !FOR ACTUAL
415 FOR I=12 TO 19
416 OUTPUT 709;"AS SA"
417 ENTER 722;Emf(I)
418 IF Emf(I)<.00001 THEN 464
419 CALL Tvsy(Emf(I),Emf1(I))
420 Tt=Emf1(I)
421 T(I)=FNTem(Tt,I)
422 PRINT T(I),I+41,J
423 NEXT I
424 PRINT ""
425 ! PRINT "I/O MODEL U2,U1,U10,U11,U12,U13"
426 !READ I/O BOARD TEMP
427 FOR I=20 TO 31
428 OUTPUT 709;"AS SA"
429 ENTER 722;Emf(I)
430 IF Emf(I)<.00001 THEN 500
431 CALL Tvsy(Emf(I),Emf1(I))
432 Tt=Emf1(I)
433 ! T(I)=FNTem(Tt,I)
434 ! PRINT T(I),I+41,J
435 NEXT I
436 PRINT ""
437 PRINT " ULM U3. INTERNAL AIR,FRONT HALL"
438 !READ ACT BOARD TEMP
439 FOR I=32 TO 37
440 OUTPUT 709;"AS SA"
441 ENTER 722;Emf(I)
442 IF Emf(I)<.00001 THEN 550
443 CALL Tvsy(Emf(I),Emf1(I))
444 Tt=Emf1(I)
445 T(I)=FNTem(Tt,I)
446 PRINT T(I),I+41,J
447 NEXT I
448 PRINT ""
449 PRINT "EXTERNAL BOX TEMP"
450 !READ OUTSIDE BOX TEMP
451 FOR I=38 TO 39
452 OUTPUT 709;"AS SA"
453 ENTER 722;Emf(I)
454 IF Emf(I)<.00001 THEN 565
455 CALL Tvsy(Emf(I),Emf1(I))

```



```

10 !MODEL
11 !VERSION 13 AUG 1983
20 !THIS IS A MODIFICATION OF A PROGRAM WRITTEN BY A. WANNIARACHCHI FOR GENER
AL USE ON THE HP3054
30 ! DATA ACQUISITION SYSTEM. MODIFICATIONS DONE BY H. KEEBLER FOR TESTING ON
THE
40 ! ULM
50 COM /Co/ A(39),B(39),C(39),D(7)
60 DIM Emf(39),T(39),Emf1(39)
70 ASSIGN #Coe TO "COE"
80 FOR I=0 TO 39
90 ENTER #Coe;A(I),B(I),C(I)
100 NEXT I
110 BEEP
120 PRINTER IS 701
130 CLEAR 709
131 INPUT "ENTER RESISTOR VOLTAGE",Rv
132 INPUT "ENTER LOAD VOLTAGE",Lv
133 Amp=Rv/2.0
134 Pow=Amp*Lv
135 PRINT " MODEL OF ULM "
136 PRINT "RESISTOR VOLTAGE-",Rv,"VOLTS"
137 PRINT "LOAD VOLTAGE-",Lv,"VOLTS"
138 PRINT "CURRENT-",Amp,"AMPS"
139 PRINT "POWER-",Pow,"WATTS"
140 INPUT "ENTER MONTH,DATE, AND TIME (MM:DD:HH:MM:SS)",Time$ 
150 OUTPUT 709;"ID":Time$
160 BEEP
170 INPUT "ENTER INPUT MODE(1=3054A-AUTO,2=FILE,3=MANUAL)",Im
180 IF Im=2 THEN
190 BEEP
200 INPUT "ENTER NAME OF EXISTING DATA FILE",Oldfile$
210 PRINT USING "10X,***THESE RESULTS ARE FROM DATA FILE***",10A":Oldfile$
220 ASSIGN #File TO Oldfile$
230 END IF
240 IF Im=1 OR Im=3 THEN
250 BEEP
260 INPUT "NEW DATA FILE NAME?",Newfile$
270 CREATE BDAT Newfile$,40
280 ASSIGN #File TO Newfile$
281 INPUT "enter number of samples",It
282 INPUT "ENTER WAIT TIME IN SEC",I_time
290 END IF
300 BEEP
310 J=0
320 OUTPUT 709;"AR AF40 AL79"
330 OUTPUT 722;"F1 R1 T1 Z1 FL1"
340 J=J+1
350 IF Im=1 OR Im=3 THEN
360 !READ TEMP OF BOX WALL(INSIDE)
361 PRINT ""
364 PRINT "INSIDE BOX WALL TEMP(45.46)"
365 PRINT "CPU-U3,BOARD(B01/TOP)"
370 FOR I=0 TO 9
380 OUTPUT 709;"AS SA"
390 ENTER 722:Emf(I)

```



```

394 IF Emf(I)<.00001 THEN 402
395 CALL Tvsy(Emf(I),Emf1(I))
396 It=Emf1(I)
397 T(I)=FNTem(Tt,I)
398 IF I=5 THEN T(I)=0.
400 IF I=5 THEN 402
401 PRINT T(I),I+41,J
402 NEXT I
403 PRINT "INTERNAL AIR TEMP/AMBIENT(S3)"
410 !READ AIR TEMP MODEL
420 FOR I=10 TO 12
430 OUTPUT 709;"AS SA"
440 ENTER 722;Emf(I)
441 IF Emf(I)<.0001 THEN 450
442 CALL Tvsy(Emf(I),Emf1(I))
443 Tt=Emf1(I)
444 T(I)=FNTem(Tt,I)
445 PRINT T(I),I+41,J
450 NEXT I
451 PRINT "
452 ! PRINT "ULM U1,U11,U13-EPROM/CHIP"
454 !FOR ACTUAL
455 FOR I=13 TO 19
456 OUTPUT 709;"AS SA"
457 ENTER 722;Emf(I)
458 IF Emf(I)<.00001 THEN 464
459 CALL Tvsy(Emf(I),Emf1(I))
460 Tt=Emf1(I)
461 ! T(I)=FNTem(Tt,I)
462 ! PRINT T(I),I+41,J
464 NEXT I
465 PRINT "
466 PRINT "I/O MODEL U2,U1,U10,U11,U12,U13"
467 !READ I/O BOARD TEMP
470 FOR I=20 TO 31
480 OUTPUT 709;"AS SA"
490 ENTER 722;Emf(I)
491 IF Emf(I)<.00001 THEN 500
492 CALL Tvsy(Emf(I),Emf1(I))
493 Tt=Emf1(I)
494 T(I)=FNTem(Tt,I)
495 PRINT T(I),I+41,J
500 NEXT I
501 PRINT "
502 ! PRINT " ULM US. INTERNAL AIR"
510 !READ ACT BOARD TEMP
520 FOR I=32 TO 37
530 OUTPUT 709;"AS SA"
540 ENTER 722;Emf(I)
541 IF Emf(I)<.00001 THEN 550
542 CALL Tvsy(Emf(I),Emf1(I))
543 Tt=Emf1(I)
544 ! T(I)=FNTem(Tt,I)
545 ! PRINT T(I),I+41,J
550 NEXT I
551 Tt=Emf1(36)
552 T(36)=FNTem(Tt,36)
555 PRINT "EXTERNAL BOX TEMP"
556 !READ OUTSIDE BOX TEMP
557 FOR I=38 TO 39

```



```

561 Tt=Emf(I)
562 T(I)=FNTem(Tt,I)
563 PRINT T(I).I+41,J
565 NEXT I
566 OUTPUT #File:Emf(*)
570 ELSE
571 ENTER #File:Emf(*)
580 END IF
581 PRINT ""
582 PRINT "AMBIENT AIR= ",T(36),"77"
583 PRINT "SUMMARY"
584 Jmax=0
585 IF Im=1 OR Im=3 THEN
586 Tmax=0
587 FOR I=0 TO 39
588 !PRINT T(I).I+41,J
589 IF T(I)>Tmax THEN Tmax=T(I)
590 IF Tmax=T(I) THEN Jmax=I
591 NEXT I
592 PRINT "TMAX=",Tmax,Jmax+41
593 OUTPUT 709;"TD"
594 ENTER 709;Times
595 PRINT USING "10X,","Month, DATE, AND TIME:","",15A";Times$"
596 IF Im=3 THEN 705
597 IF (J+1)>It THEN 711
598 IF Tmax>250 THEN 711
599 WAIT 1_time
600 IF Tmax<250 THEN 350
601 END IF
602 INPUT "enter 1 for new data, 2 to end",Flag
603 IF Flag=1 THEN 350
604 OUTPUT 709;"TD"
605 ENTER 709;Times
606 PRINT USING "10X,DD,","Data runs are stored in file","",10A";J,Newfile$"
607 PRINT USING "10X,","Month, DATE, AND TIME:","",15A";Times$"
608 END
609 SUB Tvsy(V,T)
610 COM /Co/ A(39),B(39),C(39),D(7)
611 Sum=0
612 FOR I=0 TO 7
613 Sum=Sum+B(I)*V^I
614 NEXT I
615 T=(Sum*9/5)+32
616 SUBEND
617 !THIS FUNCTION USES CALIBRATION COEFICIENTS
618 !TO ADJUST THERMOCOUPLE READINGS
619 DEF FNTem(T,I)
620 COM /Co/ A(39),B(39),C(39),D(7)
621 Delta=A(I)+T*(B(I)+T*C(I))
622 T=T+Delta
623 RETURN T
624 FNEND

```


APPENDIX D

ULM DATA RUN 1 AUG 83

A. LOCATION: Root Hall, Room 107

B. CONDITIONS:

1. Backpack placed in the environmental chamber in a vertical position.
2. Initial temperature: 48.3C

C. CONDUCT OF RUN:

1. Part I - 8 samples were taken at 5 minute intervals.

Initial electrical readings were as follows:

resistor voltage = 3.053
load voltage = 5.3
current (amps) = 1.53
power (watts) = 8.09

2. Part II - 20 samples were taken at 30 minute intervals. Electrical readings (same as settings as part I) were as follows:

resistor voltage = 2.88
load voltage = 5.27
current (amps) = 1.44
power (watts) = 7.59

THIS DATA IS FROM

1 AUG 83 -ULM

TIME(MIN)	TC= 53	TC= 54	TC= 55
0	47.8441040866	47.9501080717	55.1470236239
5	50.0519163325	50.2542632526	60.6554476882
10	51.9587254154	52.1449375838	63.1962387995
15	53.3484079473	53.5005109174	64.8282906294
20	54.4157701349	54.5551780048	65.9791786115
25	55.2440257037	55.3733415172	66.8864085739
30	55.9340846794	56.0534698769	67.5875183775
35	56.5003721356	56.6169181363	68.1355276816
40	57.5479035191	57.5542438633	69.1523717308
70	58.7460233785	58.8443815125	70.3133928582
100	59.2656585865	59.3497301723	70.7842003465
130	59.8447832523	59.9421979306	71.7834172501
160	60.1145335545	60.2153244852	72.0611767063
190	60.2412953484	60.3291621641	72.1740524784
220	60.2574256552	60.3475825413	72.1943674633
250	60.289687906	60.3913285744	72.3275261539
280	60.2781662393	60.3775143962	72.3275261539
310	60.2620355165	60.3590949776	72.3049589994
340	60.2389908389	60.3222543706	72.2846478223
370	60.2666443408	60.3557925028	72.3139859547
400	60.356509004	60.4511861797	72.401991641
430	60.4417521965	60.5363574277	72.4899841954
460	60.5292960637	60.6284202823	72.5779636342
490	60.5799574572	60.6997588763	72.6298427935
520	60.6605618098	60.7595844337	72.7020149232
550	60.7112216046	60.8148025123	72.7606482799
580	60.7664817325	60.3539121117	72.7989823274
610	60.7825982673	60.8907187325	72.8260401571

TIME(MIN)	TC=	56	TC=	57	TC=	58
0		59.2646601061		54.2242673643		53.6747653638
5		64.7564593407		62.7103743992		61.9641898526
10		67.2689145278		65.4822041173		65.5953764639
15		68.860682052		68.5179772		67.5726553626
20		70.0040787045		69.8221577964		68.8558037418
25		70.8941117788		70.7684290911		69.7965093429
30		71.5884427722		71.4963408179		70.5050113685
35		72.1238975223		72.0541004269		71.0635158682
40		73.1031756465		73.0531389563		72.0368079486
70		74.2541184082		74.1944448031		73.181928885
100		74.6882367736		74.6418138627		73.636657536
130		75.8316159961		75.8315596382		74.7854319011
160		76.096367814		76.0940035074		75.0391563695
190		76.2130006293		76.2015983501		75.1514036921
220		76.2242141157		76.2352177546		75.1873151699
250		76.3879059042		76.4077675161		75.3421505479
280		76.3901489579		76.4077675161		75.3376709014
310		76.3632437549		76.3965645025		75.326451637
340		76.3363373328		76.3539911304		75.2838165017
370		76.3834227714		76.3920832381		75.326451637
400		76.4596484249		76.4727408437		75.3937640493
430		76.5403472793		76.5690675738		75.4947183871
460		76.6299998174		76.6317335916		75.5664977167
490		76.697230344		76.7056904318		75.627054791
520		76.744287187		76.7661529535		75.6898482112
550		76.8137452408		76.8288481513		75.7459081666
580		76.8518316951		76.8646710777		75.7929944487
610		76.8787147817		76.8937756215		75.8086890433

TIME(MIN)	TC=	59	TC=	50	TC=	73
0	52.9230399384		53.4915719066		60.4794926494	
5	59.1196971873		59.7441540964		67.0099174447	
10	62.0804306303		62.7087069186		69.5018270822	
15	63.8665340167		64.4664793469		70.9181138233	
20	65.064877772		65.6513549459		71.8927982524	
25	65.9551732579		66.5469785521		72.6650682604	
30	66.6595960994		67.2433880434		73.2572744412	
35	67.2038581594		67.7981037046		73.7359847625	
40	68.1977063118		68.7698677536		74.6250611021	
70	69.3373030142		69.9189303182		75.6789661844	
100	69.8020404161		70.3761201091		76.0650034914	
130	70.7756634596		71.3639819248		77.3313262464	
160	71.0289941213		71.6281873299		77.5753152956	
190	71.1488358459		71.7455741761		77.8670650798	
220	71.1759664375		71.7929732175		77.6693027025	
250	71.3138609717		71.9328935233		77.8818384775	
280	71.3002990053		71.9125846455		77.8684174123	
310	71.2980386472		71.9058149651		77.8438112394	
340	71.2709136744		71.3764782573		77.8236783407	
370	71.3002990053		71.9103230606		77.8728911343	
400	71.3771460232		71.995072254		77.9511758242	
430	71.4630220148		72.0772921688		78.0383952016	
460	71.5466250965		72.1539996624		78.1300735823	
490	71.6031086323		72.2148294371		78.201617628	
520	71.6753983867		72.2790381615		78.2552700173	
550	71.7296098897		72.3389252147		78.3200935364	
580	71.7725237971		72.3930417994		78.3670302982	
610	71.8064009931		72.4246075302		78.382675063	

TIME(MIN)	TC=	74	TC=	75	TC=	76
0	57.768527767		49.7411491201		49.4412288862	
5	64.2325309951		53.3177246146		51.9828399328	
10	66.7185211319		55.2661529747		53.5479774681	
15	68.1463249777		56.5582684882		54.6689145319	
20	69.1303059733		57.5323705708		55.5343046684	
25	69.8995147097		58.3150763113		56.2405204087	
30	70.5159637076		58.939540499		56.3153909276	
35	70.9937168594		59.4640231928		57.2981930797	
40	71.8960795617		60.3952719992		58.1919545693	
70	72.9459529556		61.501921446		59.2552500981	
100	73.3586139085		61.9526803176		59.5961529347	
130	74.5273724097		62.7616033272		60.3718762554	
160	74.7590464793		63.0095364267		60.616135668	
190	74.8557377972		63.12887254		60.7123891702	
220	74.8692283461		63.1426416153		60.7405209699	
250	75.0445773522		63.2160657903		60.7912013068	
280	75.0333385979		63.2229488273		60.7750730947	
310	75.0108604456		63.1977106246		60.7543498838	
340	74.9816375645		63.174765844		60.7313165182	
370	75.0288430361		63.2252431545		60.7912013068	
400	75.1187477508		63.2986568004		60.871805565	
430	75.1974031172		63.3995952891		60.9685157161	
460	75.2827884795		63.475270055		61.0421926934	
490	75.3524357926		63.5417727052		61.1056447856	
520	75.4063506383		63.6059748809		61.1756968478	
550	75.4669989426		63.674754993		61.2378365965	
580	75.5231492141		63.7137267481		61.2861628636	
610	75.5366244831		63.7320654862		61.2976685174	

TIME(MIN)	TC=	77	TC=	78	TC=	79
0	48.0603555101	47.8664507086	47.9508227469			
5	48.1074329693	48.7047198125	47.3861555411			
10	48.1309701872	49.5980955848	48.0356176345			
15	48.1262628242	50.3891718085	48.0685898893			
20	48.1427384183	51.0690168288	48.1133347846			
25	48.1333238536	51.6427208867	48.1415928412			
30	48.1709811454	52.1363353671	48.1627854302			
35	48.1497992361	52.5547465453	48.1886363736			
40	48.1351019649	53.3462988865	48.2287127039			
70	48.1968690376	54.2998119748	48.2828613361			
100	48.2156958303	54.7049725346	48.2875696603			
130	48.2815845303	55.1098415058	48.3652511988			
160	48.243904811	55.3261176971	48.3911425058			
190	48.1709811454	55.4144647374	48.3417124375			
220	48.1050791921	55.4214389142	48.261673376			
250	47.9449986902	55.4167894726	48.1486571284			
280	47.9661284931	55.4029409177	48.1439476137			
310	47.862586131	55.3795925595	48.059169447			
340	48.067417386	55.2633131383	48.1674947334			
370	48.2557006251	55.4260883175	48.3252348072			
400	48.3357014881	55.505122309	48.4264471085			
430	48.4580332572	55.5957653119	48.5088154701			
460	48.4627377824	55.5678044917	48.5441124227			
490	48.5074287663	55.7398344769	48.6217577521			
520	48.5850413291	55.8141783704	48.6923349143			
550	48.646182919	55.8722527257	48.7605509079			
580	48.6297223893	55.9140625655	48.7346768704			
610	48.6038548486	55.921030571	48.7135062993			

TIME(MIN)	TC=	80	TC=	72	TC=	71
0	47.7228550225		46.582655042		47.9567490852	
5	48.1535718775		48.1978434802		48.0439512688	
10	48.710888076		50.523359328		48.0628039734	
15	49.2746890375		45.551192061		48.0887253852	
20	49.8168080979		49.2346260592		48.076343077	
25	50.2576242103		49.8707785711		48.1122892429	
30	50.6676457146		57.869733629		48.0981510496	
35	51.0165128393		49.6572442648		48.1028638212	
40	51.6668387636		51.3458451162		48.1254270721	
70	52.4868587403		51.566748384		48.1617700526	
100	52.3462625708		53.4067982254		48.1711944632	
130	53.1751261926		49.7792739431		48.2324491907	
160	53.3662920665		46.7817531805		48.2348050053	
190	53.4245614679		57.2727323055		48.1429207461	
220	53.4315533919		50.3773002908		48.076343077	
250	53.4129080687		48.1884306327		47.9251071901	
280	53.3779464279		46.2482991922		47.9072497387	
310	53.3756155749		50.0255981512		47.8530311484	
340	53.3220032984		48.6800368189		48.0086007022	
370	53.4268921188		48.9503511218		48.2018226809	
400	53.5131194425		49.1171748001		48.2724966655	
430	53.5806938186		49.6009138075		48.366714505	
460	53.6552492579		46.935084015		48.4020420307	
490	53.7437710892		55.0502639902		48.4632710304	
520	53.8020015694		51.8590387435		48.5692281884	
550	53.8905004145		49.3943197559		48.5645194149	
580	53.8974865755		47.7858808248		48.5645194149	
610	53.8998152767		46.7416441893		48.5456839175	

APPENDIX E

ULM DATA RUN 12 AUG 83

A. LOCATION: Ft. Hunter Liggett Ca.

B. CONDITIONS:

1. The backpack was placed on a concrete slab outside in direct sunlight in an upright position.
2. Initial temperature: 23.8 deg C

C. CONDUCT OF RUN:

1. Part I - 10 samples were taken at 3 minute intervals. Initial electrical setting was at zero to check the effect of solar radiation on the internal temperature of the backpack.

resistor voltage = 0.0
load voltage = 0.0
current (amps) = 0.0
power (watts) = 0.0

2. Part II - 15 samples were taken at 5 minute intervals. Electrical readings were as follows:

resistor voltage = 3.05
load voltage = 5.21
current (amps) = 1.52
power (watts) = 7.93

3. Part III - 10 samples were taken at 15 minute intervals. Electrical readings (w/same setting as part II) were as follows:

resistor voltage = 2.86
load voltage = 5.29
current (amps) = 1.43
power (watts) = 7.56

4. Part IV - 8 samples were taken at 15 minute intervals. Orientation was changed to maintain the direct nature of the sun's rays. This caused the backpack to be moved to a position on dirt rather than the concrete slab. Electrical readings (w/same setting as part II) were as follows:

resistor voltage = 2.82
load voltage = 5.28
current (amps) = 1.41
power (watts) = 7.44

THIS DATA IS FROM

12 AUG 83 -ULM

TIME(MIN)	TC= 53	TC= 54	TC= 55
0	24.7605274812	24.8202072084	24.6303455133
3	25.7790354263	25.8572818349	25.6415094195
6	26.748846169	26.8382921855	26.640795652
9	27.6898374478	27.7684672344	27.5621850327
12	28.5606330198	28.6505370614	28.440311482
15	29.4055218448	29.4969452617	29.3023037891
18	30.253610772	30.3468059482	30.1530617023
21	31.0716138195	31.1539524516	30.9756439063
24	31.8540545667	31.9307137737	31.7556231203
27	32.5940819256	32.6772460615	32.5198663217
35	34.2594813034	34.5460880202	42.7965644442
40	37.5767123727	37.8922342882	48.5689895285
45	40.2809449799	40.5663570155	51.7636361939
50	42.4268528515	42.6760963648	54.0836065826
55	44.2062071733	44.4484611008	55.3183160569
60	45.7574688251	45.9789058732	57.520264379
65	47.1580921032	47.3684425915	58.9676349059
70	48.3974751948	48.5946398075	60.1924862001
75	49.4602709299	49.6562440617	61.2445498802
80	50.4084763949	50.5588885915	62.1339621686
85	51.2801450285	51.4226504075	63.0059528514
90	52.1831770563	52.3668129177	63.8766288228
95	53.0684136373	53.2511069131	64.702559547
100	53.9406017428	54.1014238887	65.5159005232
105	54.7276722225	54.8644527058	66.3030258487
115	55.4346313381	55.5498354081	66.9729547098
130	56.7363310748	56.8625274241	68.244613446
145	57.9321316908	58.0820541785	69.4091998323
160	58.7113641985	58.8397644029	70.1775128938
175	59.2448822574	59.3405040513	70.614481489
190	59.3295238592	59.4212275857	70.7140558236
205	59.2887425103	59.258956146	70.6439029337
220	59.4756879251	59.5526673324	70.8226631466
235	59.7271599796	59.8269796978	71.0918323662
250	60.3173389608	60.4143514669	71.6501356177
255	60.4187147462	60.5041319507	71.7088736111
280	61.0012779176	61.1023111812	72.2146817486
295	61.6637141195	61.7595926	72.7989823274
310	62.3047223465	62.4138329136	73.4300090525
325	63.3141847481	63.3926642218	74.3325585389
340	63.6098064631	63.7017874389	74.6361000839
355	63.7518344414	63.8093695124	74.7507308831
370	62.7431377907	62.789973052	73.824059039

TIME(MIN)	TC=	56	TC=	57	TC=	58
0	24.5605910362		24.0285427841		24.2108088404	
3	25.5649558789		25.0230727016		25.1399130174	
6	26.555008818		26.0232867812		26.1638656453	
9	27.4696027387		26.9698730576		27.0987489429	
12	28.3433960367		27.863321885		27.9843540028	
15	29.2010203296		28.730760649		28.8415560006	
18	30.0498741694		29.582034867		29.6924206795	
21	30.870540251		30.4052095981		30.5102563361	
24	31.6558704294		31.20270932061		31.3000588189	
27	32.415734676		31.9771319647		32.0571201915	
35	46.9613425262		41.5328910534		40.0261725465	
40	52.7393243739		50.2132710082		47.816438792	
45	55.8720955705		54.5686647556		51.7825307814	
50	58.1483921073		57.2607504905		54.3265697407	
55	59.9661207607		59.2276681289		56.22415111047	
60	61.5596694548		60.8589280992		57.8172037314	
65	62.9882591552		52.3124797597		59.2489944143	
70	64.1844472581		63.5399910209		60.4494067199	
75	65.2205181273		64.6153497107		61.4865093642	
80	66.0973201624		65.5038784151		62.3910117649	
85	66.9454827956		66.3568693677		63.2299679167	
90	67.8106023861		67.2154431938		64.1020181314	
95	68.6380954314		68.0454897158		64.9453548918	
100	69.448539572		68.8562080605		65.7487006509	
105	70.2012252456		69.6136832257		66.5213319504	
115	70.3482500307		70.2795385754		57.1837495035	
130	72.1103477099		71.5799253869		68.4427775275	
145	73.2564637567		72.7037799663		69.5654392969	
160	73.9795372186		73.4630912487		70.2877978669	
175	74.4723420531		73.9695089315		70.7967659641	
190	74.5892948029		74.0954835201		70.8894639336	
205	74.4993332002		74.0235013147		70.8713776634	
220	74.6679999923		74.1989426514		71.0431747865	
235	74.9310242378		74.4395278791		71.370806271	
250	75.4859146318		74.9945257862		71.9059246553	
265	75.4904055517		75.0955829892		72.090958075	
280	75.9640066691		75.5557375666		72.6006286803	
295	76.5201735935		76.1321122363		73.1539126433	
310	77.1541963483		76.716887639		73.7716582813	
325	78.0178882599		77.5918592326		74.6349363856	
340	78.3062522778		77.8713113646		74.8932261501	
355	78.435858843		78.0500921686		74.9942655032	
370	77.5459218565		77.2608187763		74.1652350334	

TIME(MIN)	TC=	59	TC=	60	TC=	72
0	24.	7344327394	24.	7532140491	20.	952029885
3	25.	7230713335	25.	7579964545	21.	651059098
6	26.	7048330707	26.	7166600571	21.	2942347573
9	27.	6112395902	27.	6392570616	22.	4480057124
12	28.	4769136194	28.	5040258563	21.	8457048697
15	29.	3362193143	29.	3600034395	22.	2090638144
18	30.	1818884473	30.	2023735929	23.	2979573619
21	31.	0018378659	31.	0214933695	22.	6606331492
24	31.	7694940684	31.	793228685	23.	2154861144
27	32.	5238793749	32.	5492761944	23.	2979578619
35	40.	4541879591	41.	0468732013	23.	5867025963
40	47.	0581615869	47.	7034452009	23.	595571918
45	50.	7180808049	51.	3701332824	24.	0355220136
50	53.	1936760802	53.	8525170453	24.	0281272251
55	55.	0751900976	55.	7210890994	24.	346002197
60	56.	6630691325	57.	3105749921	24.	7153553517
65	58.	0846708482	58.	7156449799	24.	8162752945
70	59.	2766356147	59.	9008056934	25.	5663066979
75	60.	3348463455	60.	9524935922	25.	1704201516
80	61.	2209496082	61.	8576559154	26.	6855445518
85	62.	0666522798	62.	5949533805	27.	359305983
90	62.	9478042509	63.	5676575119	28.	2839336511
95	63.	7909828599	64.	3910590595	29.	7846816149
100	64.	6009274806	65.	2087346753	28.	6332903734
105	65.	3777778635	65.	9910782131	29.	3580900537
115	66.	0441279566	66.	5631042233	29.	8139113057
130	67.	3176563855	67.	9094384337	29.	3337029859
145	68.	4748639558	69.	0193614452	31.	1254576308
160	69.	2125547522	69.	7536212215	29.	696348301
175	69.	7000563829	70.	2426210261	29.	899179773
190	69.	8020404161	70.	3331321688	31.	3927048183
205	69.	7680477052	70.	3105056219	33.	1433579313
220	69.	890412263	70.	4417272576	34.	0188688174
235	70.	1871538057	70.	7538271478	33.	1046263554
250	70.	7485144243	71.	2984768989	34.	0382003586
265	70.	7892375078	71.	2736292707	36.	3153942292
280	71.	3206418379	71.	8381128121	34.	7095231761
295	71.	8967306755	72.	4336260022	33.	7868338813
310	72.	5331630745	73.	0398043452	36.	8312797171
325	73.	4189646094	73.	9457906637	34.	9363206201
340	73.	7026815563	74.	2458157301	35.	9340186217
355	73.	7814677026	74.	3424609218	36.	3960718339
370	72.	8669031264	73.	4315759393	35.	9219805218

TIME(MIN)	TC=	56	TC=	57	TC=	58
0	24.5605910362		24.0285427841		24.2108088404	
3	25.5649558789		25.0330727016		25.1999130174	
6	26.555008818		26.0232867812		26.1698656453	
9	27.4696027387		26.9698790576		27.0987489423	
12	28.3433960367		27.863321385		27.9843540028	
15	29.2010203296		28.730760649		28.8415560005	
18	30.0498741694		29.5820834867		29.6924286795	
21	30.870540251		30.4052095931		30.5102563361	
24	31.6558704294		31.2027093061		31.3000588189	
27	32.415734676		31.9771319647		32.0571201915	
35	46.9613425262		41.5338910534		40.0261725465	
40	52.7393843739		50.2132710082		47.816438782	
45	55.8720955705		54.5686647556		51.7825807814	
50	58.1483921073		57.2607604905		54.3265697407	
55	59.9661207607		59.2276681289		56.2241511047	
60	61.5596694548		60.8589280992		57.8172037314	
65	62.3882531552		62.3134797597		59.2489994143	
70	64.1844472581		63.5399910209		60.4494067199	
75	65.2205181273		64.6153497107		61.4865093642	
80	66.0973301624		65.5038784161		62.3910117849	
85	66.9454827956		66.3568693677		63.2299679157	
90	67.8106023861		67.2154431938		64.1020181314	
95	68.6380954314		68.0454897163		64.9453548918	
100	69.448539572		68.8562080605		65.7487005509	
105	70.2012252456		69.6136832267		66.5213319504	
115	70.3482500307		70.2796365754		67.1837495035	
130	72.1103477099		71.5799253869		68.4427775275	
145	73.2564637567		72.7037799663		69.5654392869	
160	73.9795372136		73.4630912437		70.2877978669	
175	74.4723420531		73.9695089315		70.7967559641	
190	74.5892948029		74.0954825201		70.8894639336	
205	74.4993332002		74.0235013147		70.8713776694	
220	74.6679999923		74.1989426514		71.0431747865	
235	74.9310242878		74.4395278791		71.370806871	
250	75.4859146318		74.9945257862		71.9059246553	
265	75.4904055517		75.0955329892		72.090958075	
280	75.9640056691		75.5557375666		72.6006286803	
295	76.5201725935		76.1321122363		73.1639126433	
310	77.1541963483		76.716887639		73.7716582813	
325	78.0179382599		77.5918592326		74.6349363856	
340	78.3062522778		77.8713113646		74.8932261501	
355	78.435853843	-	78.0500921686		74.99426555032	
370	77.5459218565		77.2608187763		74.1652350334	

TIME(MIN)	TC=	73	TC=	74	TC=	75
0	24.6250659578		24.7165772347		25.0154785665	
3	25.6123548987		25.6992681737		25.9655621649	
6	26.5240237585		26.6259725203		26.3892765454	
9	27.4070610657		27.5141712424		27.7475735891	
12	28.2615240385		28.3714175948		28.5897188661	
15	29.092747886		29.2125341072		29.435333702	
18	29.9151838737		30.0278498242		30.2649018514	
21	30.6924585947		30.8199290628		31.0614679531	
24	31.4612498981		31.5937474589		31.820329895	
27	32.1948968269		32.3299678343		32.5586477286	
35	47.9507195608		45.2520117008		35.8921154521	
40	54.4096438967		51.2413975479		40.3556027987	
45	57.4341542255		54.1556445491		43.0243043999	
50	59.4784981967		56.1636046343		45.0758149457	
55	61.0852349557		57.7708437188		46.741688223	
60	62.5497300932		59.2210822152		48.2375778663	
65	63.8730740475		60.5315624385		49.5672366804	
70	65.0150855839		61.6575500748		50.750639311	
75	65.9859684171		62.641171838		51.7442451653	
80	66.8298877888		63.4740900139		52.6449218349	
85	67.6475494136		64.2974848087		53.4998025642	
90	68.489066469		65.1568885489		54.4698865945	
95	69.3180254888		65.988458253		55.3405997577	
100	70.0959510421		66.7800780556		56.1449277294	
105	70.8502101331		67.5136974998		56.9341923122	
115	71.4768893651		58.1440505746		57.5138319974	
130	72.6831188943		69.3641258377		58.7777082159	
145	73.7652668044		70.4570655856		60.0318609256	
160	74.4518523933		71.1498641806		60.7834923379	
175	74.3926475611		71.6044905187		51.3223986319	
190	74.9668307815		71.6429252965		61.4766075316	
205	74.9106322251		71.5909247		51.667584927	
220	75.2005595187		71.828281122		61.6537814648	
235	75.4656400542		72.0881325047		61.964279056	
250	76.0044212429		72.6142607899		62.4928884832	
265	76.0492975769		72.573632522		52.9314949349	
280	76.5158102749		73.0790283585		63.2986568004	
295	77.0469190087		73.6448255401		63.757280299	
310	77.660352151		74.2663486249		64.3781338901	
325	78.5346313863		75.1120053733		65.2247179206	
340	78.7356904388		75.3254765193		65.3413121429	
355	78.867458995		75.4085969831		65.2201451197	
370	78.0137961591		74.5611170282		64.3918721743	

TIME(MIN)	TC=	76	TC=	77	TC=	78
0	25.7860711488		33.0971990241		27.0383233603	
3	26.7341994544		34.0454006106		27.944780153	
6	27.6315314518		34.4850451503		28.7565181448	
9	28.4661194702		35.5873453505		29.5332372752	
12	29.301760646		36.3024687318		30.3670012366	
15	30.1335790441		36.9517317143		31.1677782789	
18	30.9275291893		37.6159918927		31.9041575953	
21	31.700801112		38.4228211708		32.6564507716	
24	32.4462130991		38.9856907805		33.3519449882	
27	33.1420830756		39.359009637		33.9908728446	
35	36.5039157022		40.1119192291		35.2542975133	
40	39.738976608		40.8472781213		36.8106246334	
45	42.016587993		42.2743069956		38.4486719898	
50	43.885855295		42.4550942719		40.0051259636	
55	45.4433815002		43.2488867892		41.3543635418	
60	46.8760562408		43.8992097708		42.8145400104	
65	48.162384112		44.8377124995		43.7720559119	
70	49.2719994654		46.0983428215		44.7849231288	
75	50.2279348011		46.0983428215		45.6279297576	
80	51.1002229128		47.0377790391		46.4625442952	
85	51.3664645639		48.5544679889		47.3949509532	
90	52.9131068114		49.1985014029		48.3657985949	
95	53.7788731727		50.5546259786		49.2338670194	
100	54.5827679883		51.163567351		49.9714742679	
105	55.3645882917		51.1354770477		50.7409197923	
115	55.9572109755		51.3414396707		51.1955167589	
130	57.1429131325		52.4378443283		52.3093478537	
145	58.3122616511		53.2336677434		53.4162938617	
160	58.9410939729		53.3549256257		53.9199997575	
175	59.4699778928		53.5017990786		54.4651713793	
190	59.4422756194		52.7693805071		54.2718590983	
205	59.4699772928		53.7931008433		54.4768145742	
220	59.6223163762		53.3339405621		54.5024287542	
235	60.07678225		54.5707531622		55.2586856396	
250	60.5884890656		54.9219240229		55.6817464966	
265	60.6046165292		56.5796358834		55.8141733704	
280	61.2332338847		57.3395372297		56.473552091	
295	61.8588644606		57.0060473596		57.0487153646	
310	62.6491293138		59.7561226945		58.1093811375	
325	63.4268485208		59.2137056532		58.5395673176	
340	63.6858554644		60.3989755099		58.8169343933	
355	63.5964768158		56.8600838818		58.4031456213	
370	62.6146927049		55.9997576023		57.4356942716	

THIS DATA IS FROM

12 AUG 83

TIME(MIN)	TC=	79	TC=	80	TC=	53
0	29.0684715174		27.5561125234		24.7605274812	
3	30.0003037018		28.4018094378		25.7790354263	
6	30.6749301303		29.1168549742		26.748846169	
9	31.5455030187		29.8576787529		27.6898374478	
12	32.43288454943		30.6873853398		28.5606330198	
15	33.1199412882		31.4089353196		29.4055218448	
18	33.8751191179		32.1246217311		30.263610772	
21	34.6122860716		32.8199450532		31.0716138195	
24	35.2567481767		33.4442105513		31.8540545667	
27	35.881136958		34.0218321636		32.5940819256	
35	36.8728338354		34.8496831764		34.2594819034	
40	38.2201648948		35.9121363991		37.5767123727	
45	39.7960779942		37.3134000161		40.2809449799	
50	41.0978184916		38.5241873884		42.4268528515	
55	42.5367017477		39.7510350909		44.2062071733	
60	43.7321869197		40.782539284		45.7574688251	
65	44.882312391		41.8331967479		47.1580921032	
70	45.78647002		42.703600134		48.3974751948	
75	46.589956369		43.4895734655		49.4602709299	
80	47.3403841089		44.238868737		50.4084753949	
85	48.4193863894		45.3348717653		51.2901450285	
90	49.2636770411		46.1548453568		52.1831770563	
95	50.247444461		47.063134144		53.0684136373	
100	50.9390261703		47.6922448844		53.9406017428	
105	51.5291136858		48.3911464647		54.7275722225	
115	51.7935213943		48.7367414745		55.4346313381	
130	52.9245899846		49.7816215808		56.7369310749	
145	54.0417258999		50.7332212436		57.9321316908	
160	54.4725923031		51.1779951073		58.7113641985	
175	54.735608604		51.6621623529		59.2448822574	
190	54.3817388722		51.3651526609		59.3395238592	
205	54.7612053463		51.8351456073		59.2887425103	
220	54.5517432363		52.0431218612		59.4756879251	
235	55.3356624137		52.3419093651		59.7271599796	
250	55.6517129481		53.1611359024		60.3173389608	
265	56.3134515373		49.0891677208		60.4187147462	
280	57.1783487929		49.1056088191		61.0012779176	
295	57.6855431044		48.8014532176		61.6637141195	
310	59.1074417409		52.8975872592		62.3047223465	
325	59.469862862		48.7390917237		63.3141847481	
340	60.1502240638		50.0724300939		63.6098064631	
355	58.8533789135		46.5867881865		63.7518344414	
370	57.8244214364		48.2265016493		62.7431377907	

APPENDIX F

MODEL DATA RUN 15 AUG 1983 (48.8C AMBIENT)

A. LOCATION: Root Hall, Room 107

B. CONDITIONS:

1. Backpack placed in the environmental chamber in a vertical position.
2. ambient temperature: 48.8C

C. CONDUCT OF RUN:

Part I - 8 samples were taken at 5 minute intervals.

Initial electrical readings were as follows:

resistor voltage = 3.06
load voltage = 5.17
current (amps) = 1.53
power (watts) = 7.91

Part II - 20 samples were taken at 15 minute intervals.

Electrical readings (same settings as part I) were:

resistor voltage = 3.1
load voltage = 5.40
current (amps) = 1.55
power (watts) = 7.97

THIS DATA IS FROM

15 AUG 83 -MODEL

TIME(MIN)	TC= 41	TC= 42	TC= 43
0	48.0423417034	48.2617698275	48.2409246372
5	52.6292596768	52.6408527849	50.7024765974
10	57.0951079766	55.3724462509	52.5467902645
15	57.7603061225	57.9745111823	53.8335178984
20	57.5954432734	59.2960903914	54.9244704346
25	59.5849958463	60.294489833	55.8115006264
30	60.4617159658	61.07953712	56.5071519243
35	61.8501562293	61.7210523301	57.0445403484
40	60.4017729355	62.0495808733	57.3454420579
55	61.4797830769	63.1051192634	58.2655806907
70	62.1881324611	63.7947669092	58.9121999061
85	62.659112528	64.2365346108	59.4588637927
100	57.2017779454	64.5871114141	59.7008905217
115	53.6942527515	64.6825387871	59.8644890337
130	56.7030381804	55.427402323	60.1515124957
145	55.2693082915	55.9751592211	60.5644422278
160	70.2584562837	55.9865653463	60.8083052039
175	54.2189880976	56.1725939502	60.9807875474
190	54.2725999077	56.2207621466	61.0635607785
205	64.8366645255	56.2762060938	60.9807875479
220	54.3611646605	56.3651220236	60.9853863719
235	64.9624809237	56.4107146747	61.012978547
250	64.9784919472	56.4357891136	61.107241859
265	65.0471055759	56.449465626	61.1831011782
280	54.5033050237	56.5474712487	61.240563723
295	54.5289330428	56.4312302049	61.3830461882
310	54.5242734904	56.4631418177	61.4083216637
325	54.5662080626	56.5406341814	61.5392769203

TIME(MIN)	TC=	53	TC=	79	TC=	80
0		47.9736664135		48.1086249672		47.9275638719
5		48.0207724131		48.1557213247		48.3017739222
10		48.1102626913		48.2216494457		48.9129825565
15		48.1550023663		48.2663818822		49.535253704
20		48.202092933		48.3158187624		50.1380755476
25		48.3480476591		48.3534819741		50.6582771539
30		48.3504014519		48.3770201717		51.121832644
35		48.4516050225		48.3934963108		51.4844493568
40		48.4257175081		48.414679193		51.7019068521
55		48.583377137		48.4805762779		52.4098137708
70		48.7480479624		48.5558775706		52.3232473506
85		48.7386395265		48.5982300209		53.242741038
100		48.8256614313		48.5982300209		53.475833567
115		48.8327166594		48.6264631777		53.6109831565
130		48.8938581881		48.645284478		53.7740515875
145		48.8585850567		48.664105135		53.9510442768
160		48.9220750629		48.680572682!		54.0721125647
175		48.9056153972		48.7040968953		54.1489309292
190		48.9526417274		48.7135062993		54.2117745645
205		48.9526417274		48.7346768704		54.260648125
220		48.9690999957		48.7511423076		54.286246873
235		48.9902599049		48.7746635071		54.3141714706
250		49.0372790199		48.8264066113		54.3327871007
265		49.1030990502		48.8663865913		54.4072435037
280		49.0866447786		48.8710899277		54.4235295374
295		49.0607870748		48.8734415808		54.4328356322
310		49.1125012708		48.8899029717		54.4281826039
325		49.1125012708		48.9087151737		54.4979740163

TIME(MIN)	TC=	44	TC=	45	TC=	46
0	48.2174113082		48.0725463971		42.7559080061	
5	51.0604488026		49.2928642121		57.9632095548	
10	53.0239893299		50.5597132385		57.7562021223	
15	54.3967095651		51.6623383837		56.4595724425	
20	55.3781652911		52.5456771229		61.6846302868	
25	56.1862359448		53.3040506485		58.4181527422	
30	56.8657011214		53.921560627		58.0163423746	
35	57.4239694089		54.4268980192		56.0077138922	
40	57.7040551246		54.7107500493		56.3344779918	
55	58.6682550178		55.6171913111		62.8358404643	
70	59.3147661036		56.2250206225		58.498942924	
85	59.7369125135		56.6265149274		63.1427530073	
100	60.0504372754		56.8975824914		66.9679768673	
115	60.2370874455		57.0969198821		63.9367732209	
130	60.6032992271		57.2253814439		64.9123821976	
145	60.9577703157		57.4581434781		62.4622025632	
160	61.0912161013		57.5575789409		63.483332829	
175	61.2108308129		57.7034699204		64.2930894737	
190	61.279827991		57.7728809574		69.1774016154	
205	61.3350197551		57.8075833603		62.4577046353	
220	61.3419133545		57.8399703663		64.5949728079	
235	61.4108997974		57.8839212213		61.1035775222	
250	61.4361909206		57.9139909096		66.0504524684	
265	61.4560789953		57.9533104204		60.5955430365	
280	61.5189540964		57.9787510141		55.2524368826	
295	61.4591818859		57.9880018581		60.7519086009	
310	61.5097587753		57.9810637392		62.5150136508	
325	61.5764215209		58.0481286921		63.1931262741	

TIME(MIN)	TC=	47	TC=	48	TC=	49
0	48.	2632210794	48.	0552507741	48.	4356028881
5	51.	7947963205	49.	7871985529	51.	6704553369
10	54.	0493006771	51.	3242510348	53.	7506223504
15	55.	5550834583	52.	5209835478	55.	1773009698
20	56.	6053847565	53.	3865453599	56.	3031683536
25	57.	4502566127	54.	136708721	57.	2260643112
30	58.	1622250615	54.	7789120299	57.	9389606853
35	58.	7210124047	55.	2972608187	58.	477670469
40	59.	0209642197	55.	6015403504	58.	8103530423
55	60.	0235193488	56.	5389016951	59.	7495984697
70	60.	6794265079	57.	1568103663	60.	4271143445
85	61.	1208834529	57.	5788608138	60.	9703929365
100	61.	4425679659	57.	8796083967	61.	2211408403
115	61.	6354933573	58.	0530445157	61.	3821140294
130	62.	0119731437	58.	7023838723	61.	7590751598
145	62.	3927967143	59.	0717852442	62.	2092666835
160	62.	5257969778	59.	1871743021	62.	4411161035
175	62.	6495975779	59.	2540293051	62.	5925714044
190	62.	7206564365	59.	3071542677	62.	672872505
205	62.	7596205279	59.	3532937188	62.	5742153003
220	62.	7825393676	59.	4201890251	62.	6086325171
235	62.	8444157446	59.	4386419115	62.	6361548148
250	62.	8742057374	59.	4709325083	62.	7279295638
265	62.	9062855698	59.	5193649934	62.	7852753079
280	62.	9635666055	59.	5631813257	62.	8334412489
295	62.	8764972124	59.	5332020949	62.	8861898195
310	62.	936072409	59.	5447327575	63.	01460101
325	63.	0116783378	59.	6093001844	63.	1406314071

TIME(MIN)	TC=	50	TC=	51	TC=	52
0	47.9678352179	48.6166056613	50.9866435953			
5	49.1459026629	52.2153654553	59.8222054394			
10	50.5534792299	54.9736633338	63.7923481024			
15	51.7845362736	56.8413476409	66.0260465546			
20	52.8379127414	57.5745988631	67.4763307196			
25	53.6773310447	58.5851502121	68.514591717			
30	54.3828742001	59.3674330637	69.3221190109			
35	54.9643431461	59.9943327911	69.8930695651			
40	55.2711180488	60.2960142215	70.1760737535			
55	56.2739505895	61.3655898649	71.198284123			
70	56.9253079635	62.0568799715	71.8531957522			
85	57.3745655402	62.5340981621	72.1736120337			
100	57.6892982934	62.8711251445	72.692228312			
115	57.8604771322	63.0682062731	72.487091012			
130	58.0593503321	63.5857971934	72.9896638416			
145	58.339043298	64.0388817713	73.491810644			
160	58.5007867745	64.1966916749	73.4287841701			
175	58.6416974338	64.3270239891	73.7033505415			
190	58.7225321714	64.4001301732	73.750591463			
205	58.7294603328	64.4253254809	73.7978439882			
220	58.7548622749	64.4298972379	73.8495840225			
235	58.8056645827	64.500754866	73.8968209836			
250	58.8218278186	64.5258958155	73.9350576744			
265	58.8813597052	64.5830302869	73.9283102021			
280	58.9280320357	64.6470142185	74.0070259391			
295	58.9511173031	64.4596127806	73.1270646653			
310	58.9580427034	64.626448724	73.869829895			
325	59.0226757464	64.7109910984	73.9380303832			

TIME(MIN)	TC=	61	TC=	62	TC=	63
0	55.0174069642	53.7116444363	58.9812601077			
5	67.3440189929	63.9949034532	71.6422990535			
10	72.4016978504	68.295687299	75.4900543497			
15	74.7433785399	70.3731891371	77.4437771323			
20	76.2686981403	71.7548913947	78.7084904925			
25	77.2617501624	72.702803531	79.6318732919			
30	78.040681905	73.4532973963	80.3913702581			
35	78.5281139215	73.9530837943	80.7985633027			
40	78.7359336315	74.1893277362	81.0231800183			
55	79.566487811	75.0480155134	81.9985096421			
70	79.816320521	75.3668983148	82.5086742204			
85	80.4627228022	75.9817259164	82.9500963488			
100	81.4866168171	76.8714310655	83.4131455444			
115	78.040681905	73.9598349234	83.3932129588			
130	81.0361716609	76.634007156	83.4617371816			
145	81.9112404202	77.3706096706	83.8891169854			
160	81.0928479468	76.7482511849	83.7917394501			
175	82.0290144837	77.4936614692	84.1280678938			
190	81.7367746937	77.3012420509	84.2121207017			
205	81.7912203444	77.325857288	84.2562543174			
220	81.7156397869	77.2542465134	84.2519311018			
235	82.2457243292	77.7039096253	84.3448118192			
250	82.2900402743	77.7396292051	84.3890257058			
265	81.568897304	77.155767701	84.3779800389			
280	82.2911451771	77.7799386657	84.4155684833			
295	80.6275547376	76.4211414047	82.4290172989			
310	82.4256093994	77.8760792061	84.3824023300			
325	81.8401203204	77.3952220544	84.4575763268			

TIME(MIN)	TC=	64	TC=	65	TC=	66
0		51.5913313513		65.1497556172		59.3194933536
5		61.626347329		73.7622221474		73.7077526758
10		65.4441932926		93.5245410075		77.5126090929
15		67.3821775578		85.5982975037		79.5118568475
20		68.6599964763		86.3437641446		76.4151910305
25		69.6131296277		87.7789311286		78.7576233918
30		70.3903730374		88.5392012584		73.1016545206
35		70.9381301108		88.8339694819		71.399442589
40		71.2140785881		89.0374732151		69.8033737788
55		72.2240310492		90.0152654948		77.8392027621
70		72.8490172386		90.5392635315		84.760547291
85		73.2300014417		91.0264765097		85.1561054332
100		73.7481053531		91.3260143221		85.4940016701
115		73.5386662521		91.5926317595		85.747850843
130		73.9304607073		91.8001527173		85.8824577381
145		74.3894754596		92.1560771475		86.2442022077
160		74.2860032401		92.1886367707		86.2916876563
175		74.6255942708		92.3197714929		86.4624669924
190		74.6885433789		92.424512754		86.5748755051
205		74.7267592142		92.461604292		86.6079328329
220		74.751485793		92.5619582905		86.5828560478
235		74.8548766614		92.5488695775		86.7026871009
250		74.897575317		92.5532325131		86.7203141546
265		74.8503817817		92.6154915636		86.7974264399
280		74.9402728936		92.6470280612		86.8084416735
295		74.1127592193		92.9955496381		84.7384413774
310		74.8953290434		92.5794094698		86.7533534877
325		74.9357786621		92.7059155496		86.8789343915

TIME(MIN)	TC=	67	TC=	68	TC=	69
0	48.	3495146664	54.	4364562752	48.	3548179333
5	48.	5141169617	60.	347352178	53.	3696458581
10	48.	6434128947	64.	2114387833	56.	7915614524
15	48.	7444777157	66.	6379196012	58.	9388036025
20	48.	8073275698	68.	1589996149	60.	4142149421
25	48.	8690205417	69.	1814452804	61.	4785657723
30	48.	918359934	70.	0094497922	62.	3134509937
35	48.	9559488953	70.	5872242751	62.	9520166669
40	48.	9606473357	70.	8770297527	63.	2893880241
55	49.	0569565642	71.	9060402033	64.	3506983565
70	49.	1555974068	72.	58125663094	65.	0281790731
85	72.	0762573091	72.	9851290334	65.	4649143057
100	49.	2072593494	73.	3887143381	65.	8396483511
115	49.	2236962945	73.	4292830404	66.	0337745749
130	49.	2589165682	75.	0699752309	66.	177614268
145	49.	2683082626	75.	5799338741	66.	5245087196
160	49.	3129166343	75.	5507410605	66.	602075049
175	49.	3316380309	75.	5507410505	66.	8050870797
190	49.	3575214108	75.	5775383242	66.	8871559874
205	49.	371606383	75.	6270884536	66.	9327559047
220	49.	3880383975	76.	0356041683	66.	9737927585
235	49.	4162064308	75.	8291369525	67.	0125471157
250	49.	4936611343	75.	302201143	67.	0467399822
265	49.	5288642369	75.	9054484465	67.	0900480473
280	49.	5312110308	76.	0266288302	67.	115119657
295	49.	3152643437	75.	0812125386	67.	0239449623
310	49.	3316380309	75.	8560715482	67.	0558577068
325	49.	3504787903	75.	972773944	67.	1675386056

TIME(MIN)	TC=	70	TC=	71	TC=	72
0	48.865428116	48.0368813376	55.103724146			
5	55.1354001523	48.0840124923	65.8104593379			
10	58.8636333767	48.1405645373	69.0250598208			
15	61.1179154116	48.1688383757	70.4368145135			
20	62.5676777787	48.1947547823	71.4634763419			
25	63.6612012726	48.2253816361	72.3530101173			
30	64.5034314515	48.2442281628	73.0392752851			
35	65.1365864779	48.2489396809	73.5384777989			
40	65.4677462765	48.2536511587	73.7748366401			
55	66.5444242903	48.2795635639	74.7418005976			
70	67.2368257798	48.3525829589	75.3840729649			
85	67.7032778864	48.3808457878	75.8193455099			
100	68.0625333614	48.3832009662	76.1153283566			
115	68.2148092481	48.3879112929	76.3170504844			
130	68.6691285621	48.4067521959	76.4514939445			
145	69.0822530269	48.413917368	76.7449234165			
160	69.1752793439	48.4208824493	76.8524033928			
175	69.3295343586	48.4467869706	76.9956798836			
190	69.4111823538	48.4491418665	77.0628288857			
205	69.4520020895	48.4703354762	77.112066681			
220	69.5313656678	48.4821993508	77.1389219465			
235	69.5495044059	48.5056563436	77.1836780347			
250	69.5767114542	48.54803839	77.2015795295			
265	69.619786725	48.5832542672	77.2329058523			
280	69.6809934991	48.5857085784	77.2754175157			
295	69.4338603355	48.6021884745	75.9494167117			
310	69.6084514366	48.6068959256	77.2575182373			
325	69.6945941376	48.6304385765	77.3492463615			

APPENDIX G

MODEL DATA RUN 15 AUG 1983 (37.7C AMBIENT)

A. LOCATION: Root Hall, Room 107

B. CONDITIONS:

1. Backpack placed in the environmental chamber in a vertical position.
2. ambient temperature: 48.8C

C. CONDUCT OF RUN:

Part I - 15 samples were taken at 5 minute intervals.

Initial electrical readings were as follows:

resistor voltage = 3.27
load voltage = 4.72
current (amps) = 1.64
power (watts) = 7.72

Part II - 24 samples were taken at 30 minute intervals.

Electrical readings (same settings as part I) were:

resistor voltage = 2.8
load voltage = 4.73
current (amps) = 1.40
power (watts) = 6.62

THIS DATA IS FROM

15 AUG 83 -MODEL 2

TIME(MIN)	TC=	41	TC=	42	TC=	43
0		37.0855553597		37.4556497504		37.0906383149
5		44.21953431		41.4458650994		39.3736976916
10		44.0841999571		44.3479901065		41.3922475246
15		51.6442112222		46.0993107425		43.0211119973
20		46.1745238767		47.2393783288		44.0756566808
25		51.7987542923		48.0522637493		44.8202363022
30		49.210309384		48.9791367002		45.5320804284
35		50.624549105		49.6415791671		45.8510452908
40		51.4708842904		49.9701570849		46.0210839623
45		55.8251100514		50.2446050618		46.2311977793
50		55.4926254515		50.5142294455		46.4577472658
55		56.2177925048		50.7860659036		46.667694055
60		49.7463632561		51.0249847819		46.7808905013
65		51.8900549133		51.2193235181		46.9836425541
70		52.032828261		51.3691287913		47.20516986
75		49.4760507102		50.703746645		46.8799192912
105		41.6852500496		51.3082752562		47.3088328858
135		43.057396597		51.5118744751		47.3135443781
165		43.4949793101		51.6382090233		47.3724346346
195		70.12245019		51.7434659646		47.4996151227
225		57.5425227602		51.8463646727		47.7727216891
255		50.578509482		51.9282023775		47.8221487708
285		52.3416545102		51.9772992448		47.8786314476
315		50.678509482		51.9843127307		47.7915515753
345		51.1357875932		51.9585951852		47.7209361903
375		51.215479362		51.9492444205		47.6903333846
405		52.0398489514		51.9422304943		47.6079327798
435		50.6222028818		51.9258643238		47.5961602603
465		51.7940718032		51.9094976738		47.6032298022
495		52.2246351181		51.9282023775		47.7515372994
525		52.0819712252		51.9305404215		47.695041619
555		50.5987401002		51.913850104		47.6456031544
585		50.612817889		51.8978069158		47.6079327798
615		51.0631174354		51.9024832483		47.6126417173
645		68.6515554292		51.9305404215		47.6691458328
675		42.2597697137		51.3749613966		47.9230490521
705		50.6714714716		51.988988339		47.798612617
735		42.2979114937		52.0404174483		47.7962589465
765		41.0718817606		44.9237079502		43.5147458379

TIME(MIN)	TC=	44	TC=	45	TC=	46
0		37.1365440714		36.8565915317		39.783042954
5		39.7179571843		38.2271578709		38.0019489225
10		41.5177356255		39.6037430532		41.0346370537
15		42.8481554484		40.7119949527		45.9510374214
20		43.8218684055		41.5321489804		48.6982223009
25		44.5403403535		42.2035506474		48.1273041075
30		45.2460290378		42.634044737		44.9211604513
35		45.8397081305		43.0855752052		45.7480487876
40		46.1752881958		43.4583974243		47.0378825369
45		46.456354959		43.7525742965		49.1442129982
50		46.7018748358		43.9946210093		49.8664332777
55		46.926051551		44.2127549281		51.1467922491
60		47.1194776839		44.3952561865		49.1535984541
65		47.2892589929		44.532684201		49.2615198841
70		47.4307032748		44.6274419054		45.098455357
75		47.0274908444		44.4473881446		46.8612091142
105		47.4118461441		44.5990163277		49.8523729347
135		47.553258833		44.7624431189		47.8475052429
165		47.6592944488		44.8476897905		51.254331505
195		47.7794434009		44.9660658067		49.9882748292
225		47.8548175713		45.0418129572		51.5057344401
255		47.9066313159		45.0820493479		45.8731552579
285		47.946665865		45.1317490234		51.5441178639
315		47.963149832		45.1388485071		50.8521230937
345		47.932536357		45.112816348		57.1771810129
375		47.9207614897		45.100993092		50.8404256934
405		47.9136964482		45.093883015		46.0005930308
435		47.8995660929		45.0867828456		46.0171106461
465		47.8901456542		45.0867828456		47.9486252549
495		47.9231154833		45.1104497174		48.014460974
525		47.93724E2333		45.1293824749		46.1232832063
555		47.9278254403		45.1199161784		45.1409976354
585		47.9042752517		45.1080830765		45.240250168
615		47.9113414142		45.1151829684		51.3992432879
645		47.9419560693		45.1435815115		48.5244242895
675		48.0009256156		45.1956419481		48.6958740396
705		48.0337898091		45.2145717472		49.5288877168
735		48.0455622565		45.2405991478		49.5030946236
765		43.3637297491		42.5555824957		38.3131715242

TIME<MIN>	TC=	47	TC=	48	TC=	49
0		37.2691617576		36.9170773633		37.3456732931
5		40.3667168968		38.8023725377		40.2460022045
10		42.4044476666		40.2967158988		42.5078518317
15		43.8234740536		41.5272968017		44.2175783358
20		44.8699544665		42.2723792338		45.2857901039
25		45.6098085387		42.8738810782		46.0259131943
30		46.341592568		43.6669331976		46.7933521186
35		46.968738196		44.1934094136		47.1519087021
40		47.3291431155		44.3711575562		47.2674460962
45		47.6092961504		44.6104331574		47.4819510751
50		47.856372625		44.8448684423		47.7081513287
55		48.0962846046		45.0460705894		47.9130649895
60		48.2914307475		45.2377354388		48.0321513343
65		48.4724087762		45.4269678119		48.254418379
70		48.6039922315		45.5452047079		48.4944152302
75		49.1197999154		45.2253696183		48.0255057058
105		48.6016427994		45.4506172415		48.5320534793
135		48.7496376811		45.5901280108		48.5602797316
165		48.8529758911		45.7366941286		48.6661153237
195		48.9703824416		45.8619533391		48.7977925131
225		49.0478572352		45.9375676393		49.0728056356
255		49.0995011244		45.9800960861		49.0963046
285		49.1487931082		46.0367955353		49.1902904747
315		49.1652228027		46.0486071804		49.091604687
345		49.1300157227		46.0131714794		49.0140538553
375		49.1088904092		46.0013590687		48.983500462
405		49.1159322691		46.0060840536		48.9153368061
435		49.0995011244		45.3848212548		48.8871286362
465		49.0901116817		45.9824586805		48.8777256729
495		49.1206267931		46.0178963722		49.0469556214
525		49.1323629304		46.0391578847		48.985850783
555		49.1182795361		45.3611949527		48.8683224895
585		49.0924590572		45.9493814287		48.8448138311
615		49.1112377057		46.0462448718		48.9317908721
645		49.1276685051		46.0745919016		48.999952499
675		49.1863459953		46.1360054258		49.2537219147
705		49.2074683691		46.1454530482		49.1245020393
735		49.2332835313		46.1832419064		49.1245020393
765		43.6670403434		42.8406139302		43.7004817102

TIME(MIN)	TC=	50	TC=	51	TC=	52
0		36.7228959512		37.6037868249		40.567320386
5		37.8081852892		40.8732221136		43.5519714776
10		39.1568847999		43.1288217897		52.5385167307
15		40.4329583555		44.7575358879		54.0861039647
20		41.4916487812		45.8288227088		55.1510928887
25		42.3199768365		46.5913926045		55.9056011338
30		42.9879004941		47.3246286292		56.2637270414
35		43.5434785325		47.9862928443		56.7193436125
40		43.9348902179		48.2709636963		57.1014697121
45		44.2241163214		48.5319786883		57.3977302553
50		44.4894999853		48.7834708101		57.6290756154
55		44.7026609948		49.0137038719		57.915315754
60		44.9039031793		49.213327455		58.1515738201
65		45.1287330665		49.5794988502		58.3410342359
70		45.2801452131		49.710885912		58.4934811333
75		45.1132634129		49.3166311142		57.4347519968
105		45.2422961125		49.6217338062		58.3964741787
135		45.3700263172		49.7601480242		58.6274160533
165		45.457527924		49.8586591078		58.7128409042
195		45.587571999		49.9899799829		58.7844032529
225		45.6868575629		50.0814172193		58.8835523353
255		45.7294030033		50.1212697583		58.9944216765
285		45.7979414781		50.1869029931		59.0336473441
315		45.7813984942		50.1939346648		59.0474910556
345		45.7459475559		50.1447110903		59.012881149
375		45.7317665419		50.1376787951		59.0013440485
405		45.7175851573		50.1095487206		58.9892067153
435		45.6939486994		50.0931388516		58.9828842938
465		45.6868575629		50.076728497		58.9598035606
495		45.7435840317		50.1353346767		58.9644237637
525		45.7530379298		50.1400229035		58.9851917159
555		45.7483110261		50.1189255706		58.9644237637
585		45.7199487469		50.090794545		58.9482703901
615		45.7199487469		50.1142371554		58.9182700578
645		45.7554013663		50.1400229035		58.9413473761
675		45.8546564846		50.2337791216		58.9874992208
705		45.8664713715		50.2290916869		58.9621161668
735		45.8782860034		50.2478411879		59.0474910556
765		43.2610122145		44.2317622515		44.9956272698

TIME(MIN)	TC=	53	TC=	77
0	37.6031270633		36.6560563395	
5	38.1743201914		37.0238223305	
10	37.763987873		37.4897590887	
15	37.8528003616		38.0056707581	
20	37.8984009473		38.5210671871	
25	37.792793567		38.9569630299	
30	37.8239979547		39.3374791663	
35	37.84800007		39.6483899336	
40	37.7735899464		39.9041567161	
45	37.7663884078		40.123369871	
50	37.7879927276		40.2911581254	
55	37.7711894445		40.4535192637	
60	37.583916511		40.5609369156	
65	36.8389653932		40.5871912671	
70	36.487750087		40.5513895573	
75	36.7379550141		40.4673428739	
105	36.8918678128		40.4964889222	
135	37.1130382293		40.6134442244	
165	37.0553506006		40.5893094992	
195	37.1490897739		40.8067224691	
225	37.194751504		40.8568201795	
255	37.3317128435		40.9092984476	
285	37.240409253		40.9307653419	
315	37.2452151061		40.9259949956	
345	37.2043639931		40.9069131838	
375	37.2500209102		40.8949867048	
405	37.228394445		40.9021426242	
435	37.228394445		40.3926013763	
465	37.3293103211		40.9212246057	
495	37.3245052434		40.9403059055	
525	37.2740492701		40.9546164335	
555	37.3509326253		40.9713115632	
585	37.3461277466		40.9498463005	
615	37.2235884427		40.947461218	
645	37.4422169828		40.9665415795	
675	37.3941745638		41.0261633116	
705	37.4398149662		41.0380868587	
735	37.5430917544		41.0786249264	
765	35.1239498263		40.0403560198	

TIME(MIN)	TC=	61	TC=	62	TC=	63
0	43.6225380124		42.4124141247		48.0212638353	
5	54.1928967898		51.2220991025		57.5944917117	
10	56.0962940121		52.925804213		60.3480844651	
15	59.1035004258		55.5030886086		62.4312823767	
20	61.8902991481		57.9623314662		63.8530990844	
25	62.8552555372		58.8821109267		64.8996696808	
30	63.6421049835		59.5828255612		65.5436612647	
35	64.2195151849		60.2774488057		66.1664225055	
40	64.3981204592		60.5146652416		66.6222363227	
45	64.3981204592		60.5515056303		66.9342636228	
50	64.9175938886		61.0210142761		67.2074354374	
55	65.585130393		61.6257489089		67.4691054383	
60	65.3318327953		61.8601144994		67.6874534497	
65	66.0030921946		62.036974539		67.8579812032	
70	66.124085032		62.1540860101		68.0102773627	
75	64.3179838944		60.7425773515		66.7930748251	
105	65.0182308301		61.2234294714		67.9398163958	
135	65.409176591		61.5682318577		68.1625339557	
165	65.9619945487		62.0553466178		68.282947732	
195	66.0761474908		62.1586781299		68.3624527098	
225	66.4777873806		62.5190459183		68.4146929705	
255	66.6853445983		62.700292718		68.5237011403	
285	66.7674346899		62.7713993963		68.5691152343	
315	66.7697148037		62.7828673985		68.5663446131	
345	66.7560339806		62.7576374942		68.5464086257	
375	66.7172693999		62.7255251185		68.5032636512	
405	66.6830641525		62.6934109636		68.507805377	
435	66.6488563922		62.6590009656		68.4873673342	
465	66.5918389837		62.6154120348		68.4828254502	
495	66.4960371416		62.5488752387		68.4750125583	
525	66.3294868157		62.3997132729		68.4669285794	
555	66.3408958953		62.3997132729		68.4533023472	
585	66.2678739095		62.3469236816		68.4396757985	
615	66.3112318213		62.383647385		68.401065525	
645	66.2701559856		62.3584000891		68.3987942533	
675	66.3157956237		62.4180737419		68.4487601995	
705	66.1583237093		62.2849471497		68.4305912569	
735	66.3819667238		62.4685620304		68.507805377	
765	45.3803356381		45.1715145013		45.0496088416	

TIME(MIN)	TC=	64	TC=	65	TC=	66
0		41.0135475522		53.6382928171		38.1781834585
5		48.9054496352		65.4465971159		39.7975778125
10		52.0194009048		69.1421598549		40.0175854015
15		53.625823893		70.9473178816		40.1084314425
20		55.0765144664		71.9415261839		40.2327213524
25		56.0709744136		72.7717619458		40.2566205147
30		56.7948060599		73.1143454515		40.2709591953
35		57.4227638153		73.5648112974		40.2948561348
40		57.8788224505		73.9844341814		40.2327213524
45		58.1795711796		74.1656497647		40.2685694421
50		58.4639794022		74.4197539239		40.2781283902
55		58.7528666423		74.626554835		40.2924664893
60		58.3815614293		74.8035699151		40.2781283902
65		59.1732247712		74.9770525559		39.6803625286
70		59.3140447066		75.1454876092		39.2950435537
75		58.2558897203		73.7944170088		41.3214090479
105		59.1893862048		75.1791688691		41.574152421
135		59.4317527972		75.3722379129		41.7433925484
165		59.5655873789		75.4620160999		41.7076441745
195		59.6532551023		75.5517807283		41.8530059748
225		59.7455223843		75.5607564456		41.8124992957
255		59.8516113441		75.6303136609		41.8601538952
285		59.9092501297		75.6662109754		41.8482406414
315		59.9092501297		75.6684544856		41.8339443861
345		59.8977308377		75.6415318045		41.8053507275
375		59.8608355405		75.6146079042		41.8124992957
405		59.8446930992		75.610120469		41.80295678536
435		59.8377747704		75.5989017327		41.7886703864
465		59.8262440355		75.5764636249		41.8553886255
495		59.8354686423		75.5607564456		41.836327219
525		59.8285502019		75.5809513142		41.8363271219
555		59.8147120699		75.540560891		41.8434752654
585		59.7870378009		75.524852763		41.8434752654
615		59.7824251258		75.5136324175		41.7338598827
645		59.7893441245		75.511388323		41.8696843069
675		59.8400808893		75.5472929188		41.8506233164
705		59.8239378618		75.5742197676		41.8530059748
735		59.8977308377		75.6073767386		41.9292455292
765		45.2414224891		44.9529418505		36.4021373882

TIME(MIN)	TC=	67	TC=	68	TC=	69
0		45.895808987		44.4571194186		37.5832768645
5		38.5487755192		55.1603900256		42.4533067157
10		42.6116859684		58.3972974901		45.9295164015
15		44.4883932526		60.9578708934		47.9281622434
20		41.5768290704		59.8815371362		49.1647801063
25		46.5143951283		58.2273570767		49.9970467153
30		49.4279425884		58.1625706069		50.2413142545
35		42.3977400956		58.1440588288		50.6896389327
40		43.1176862552		58.1486868299		51.0930543054
45		41.7363468357		58.3869779045		51.4493157574
50		51.255766117		58.6274811074		51.7046514711
55		51.8870784755		58.8863708173		51.9622103562
60		42.6306992646		59.1081825495		52.184551252
65		43.4405181672		59.3045062398		52.3717155562
70		41.0574520393		59.4739854353		52.5330959305
75		41.4029622002		58.4077947056		51.8192970436
105		44.1898842076		59.3068155276		52.5541419553
135		42.3168939534		59.5053792637		52.7294944796
165		41.1813847906		59.6484869608		52.8346794287
195		41.1861508615		59.747717983		52.9351708925
225		53.9025058917		59.8169387056		52.9912512526
255		34.4230072634		59.8976856011		53.0730249734
285		41.2314264179		59.9599682567		53.122083435
315		45.3879666218		59.383034192		53.1290914335
345		33.0162457769		59.946128254		53.1104032414
375		43.5188233024		59.934594662		53.084705952
405		44.6825728857		59.9207540439		53.0823697759
435		40.3191854586		59.8930718006		53.0730249734
465		41.0836709779		59.8930716006		53.0590074753
495		42.6901114887		59.8907648864		53.0823697759
525		44.9145502249		59.8884579629		53.0893782748
555		44.1045657188		59.8515459173		53.0823697759
585		34.6981107256		59.8215531218		53.0660162685
615		51.7351511108		59.8561500536		53.0543348974
645		45.3663852153		59.8700022386		53.0636800139
675		44.2657115933		59.9299811599		53.1267554468
705		45.7351453665		59.9207540439		53.1337633834
735		54.5541056072		59.3853407233		53.1851522431
765		38.7618763202		45.3908196379		44.9535067969

TIME(MIN)	TC=	70	TC=	71	TC=	72
0	38.1335143984		44.6161103723		44.5168859959	
5	44.2023628536		52.8400127074		52.6649677413	
10	47.9077250203		55.8341599238		55.4220559551	
15	50.0185803802		57.5674422551		57.024934074	
20	51.1342159709		58.8263734857		58.1542042328	
25	51.9133652164		59.7941342785		59.0296993545	
30	52.2546307083		60.3994410929		59.5664204213	
35	52.7427920422		60.9491419743		60.1734452814	
40	53.0998842824		61.4003581522		60.562523456	
45	53.4101129514		61.729355336		60.8756258977	
50	53.6968634817		62.0144784605		61.1355603905	
55	53.9508533708		62.24661137		61.358596362	
60	54.1721270911		62.4327096917		61.5470748575	
65	54.3537393785		62.5980799124		61.7194097401	
70	54.5352930578		62.751923433		61.8664280971	
75	54.7364841462		61.6557521969		60.8365105383	
105	54.5329658171		62.7978389082		61.8802091459	
135	54.7191146837		62.9699893542		62.0455560454	
165	54.8214703423		63.0517819009		62.1626480962	
195	54.9261330378		63.1673252621		62.2728006707	
225	55.0005480215		63.2109136216		62.3230239895	
255	55.0703031496		63.2682517068		62.369223174	
285	55.119126605		63.3141360696		62.4288866589	
315	55.1237762386		63.3141360696		62.4220027253	
345	55.1121520853		63.2866118838		62.401350432	
375	55.0865781047		63.256792546		62.3738128918	
405	55.0703031496		63.2453231571		62.369223174	
435	55.0656530762		63.2476170531		62.3554538019	
465	55.0610029644		63.2315595893		62.346274038	
495	55.0703031496		63.23385354		62.3646334198	
525	55.072628172		63.2384414142		62.3715180375	
555	55.072628172		63.23385354		62.3347991278	
585	55.0517026259		63.2246776822		62.3393891192	
615	55.0261259038		63.2017373987		62.3485689925	
645	55.0377518304		63.1925610297		62.3416841013	
675	55.0842531399		63.2590863964		62.401350432	
705	55.1051774783		63.2705555116		62.4288866589	
735	55.1446991108		63.2934930579		62.4449488515	
765	45.4552682996		44.5757934859		44.5737411014	

TIME(MIN)	TC=	78	TC=	79	TC=	80
0	36.7528874126		36.8704290819		36.6721180994	
5	37.5510209709		37.3631727522		37.1837654592	
10	38.5781529864		37.4472534414		37.8819757834	
15	39.5291045693		37.5577390023		38.6080009391	
20	40.3565032533		37.632183548		39.2206357361	
25	41.0346787071		37.6730034958		39.7680602736	
30	41.595193601		37.6922117853		40.2194424685	
35	42.0598559492		37.7066175415		40.5988820329	
40	42.421774955		37.5778056341		40.3755355025	
45	42.7097071126		37.6874097788		41.0948507795	
50	42.9451732407		37.6970137479		41.3164579607	
55	43.1591439328		37.7066175415		41.4784355469	
60	43.3350116964		37.5585968177		41.6046489894	
65	43.484691721		37.2958984942		41.6736966552	
70	43.5583285411		36.9714192126		41.7070268453	
75	43.4300514507		36.834356454		41.5975056222	
105	43.4989447937		36.8872621239		41.6356024863	
135	43.6438296506		37.0195029032		41.7665399129	
165	43.7506869841		37.0243110294		41.8569871923	
195	43.8646448244		37.1589206435		41.9831120139	
225	43.9216147256		37.1348857494		42.0211816372	
255	43.9762052423		37.1829544351		42.0830390472	
285	44.0212975961		37.178147765		42.1092073558	
315	44.0260439407		37.1637274901		42.0973128274	
345	44.0070583122		37.1348857494		42.10682284711	
375	43.9833253383		37.1444998394		42.0687548896	
405	43.9856986826		37.1541137529		42.0592485748	
435	43.9714584603		37.1541137529		42.04259462	
465	43.9833253383		37.2190030558		42.0877970159	
495	44.0094315523		37.2165998916		42.1258532553	
525	44.0212975961		37.2238093512		42.1282380562	
555	44.0070583122		37.2358248969		42.1187227899	
585	44.0094315523		37.257452135		42.1258592553	
615	44.0070583122		37.1901642577		42.1306163466	
645	44.0165512099		37.2766756921		42.1211016222	
675	44.0301155126		37.3127178679		42.2233814972	
705	44.1067254209		37.3103151333		42.2281382293	
735	44.130452976		37.3679777261		42.2566777417	
765	42.1551214834		36.0955224177		40.9422938119	

LIST OF REFERENCES

1. Azar, L., A Conceptual Design of the Upgraded Logic Module, a Preliminary design concept presented to the Cdr. U.S. Army Combat Developments Experimentation Command, Ft. Ord, California, 15 July 1981.
2. Commander, Instrumentation Command, U.S. Army Combat Developments Experimentation Command (CDEC), Letter to Chief of Staff, U.S. Army CDEC, subject: Request for Upgraded Logic Module, 12 December 1980.
3. BDM Scientific Support Laboratory Specification #28A600034, Development Specification for an IDFSS Upgraded Logic Module, 12 December 1980.
4. Rome Air Development Center, RADC-TR-82-172, RADC Thermal Guide for Reliability Engineers, by G. N. Morrison and Others, 23 January 1982.
5. Kraus, A. D. and Bar-Cohen, A., Thermal Analysis and Control of Electronic Equipment, Hemisphere Publishing Corporation, 1983.
6. Incropera, F. P. and Dewitt, D. P., Fundamentals of Heat Transfer, John Wiley and Sons, 1981.

INITIAL DISTRIBUTION LIST

No. Copies

1. Defense Technical Information Center 2
Cameron Station
Alexandria, Virginia 22314
2. Library, Code 0142 2
Naval Postgraduate School
Monterey, California 93943
3. Professor M. Kelleher, Code 69Kk 3
Department of Mechanical Engineering
Naval Postgraduate School
Monterey, California 93943
4. Chairman, Department of Mechanical Engineering 1
Code 69
Naval Postgraduate School
Monterey, California 93943
5. Cpt. Henry C. Keebler III 3
Headquarters, U.S. Army MICOM
Redstone Arsenal
Huntsville, Alabama 35898
6. Deputy Under Secretary of the Army 2
for Operations Research
Room 2E261, Pentagon
Washington, D.C. 20310
7. Commander 2
Instrumentation Command
Attn: ATEC-IC
Ft. Hunter Liggett
Jolon, California 93928
8. Commander 2
Instrumentation Command
Attn: ATEC-IC-E
Ft. Hunter Liggett
Jolon, California 93928
9. Commander 4
Instrumentation Command
Attn: Lt. Holiday
Ft. Hunter Liggett
Jolon, California 93928

246315

Thesis

K182 Keebler

c.1

Analysis and testing
of the thermal design
of the electronic pack-
age in the U.S. Army's
Upgraded Logic Module
(ULM).

246315

Thesis

K182 Keebler

c.1

Analysis and testing
of the thermal design
of the electronic pack-
age in the U.S. Army's
Upgraded Logic Module
(ULM).

Analysis and testing of the thermal desi



3 2768 002 11182 5

DUDLEY KNOX LIBRARY