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# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



## THESIS

EFFECT OF BOUNDARY CONDITIONS ON THE DAMPING CHARACTERISTICS OF A RANDOMLY EXCITED CAST NICKEL-ALUMINUM BRONZE SPECIMEN AT LOW STRESS LEVELS

bу

Stephen T. Knouse

March 1984

Thesis Advisor:

Y. S. Shin

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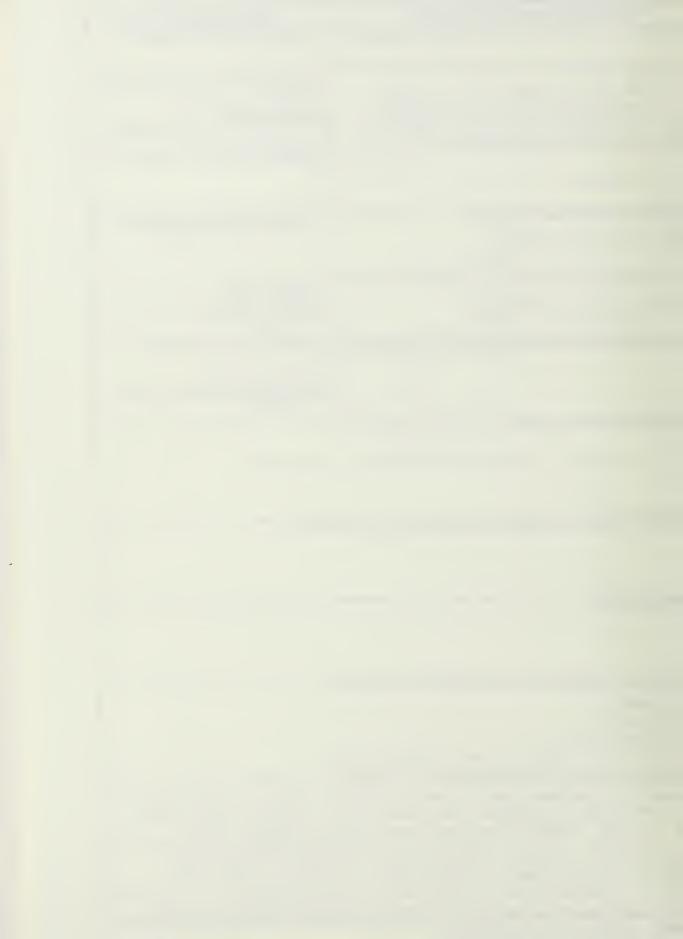
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This research examines how various specimen support arrangements affect a material's damping characteristics. The 74 lb. sample studied is cast nickel-aluminum bronze and measures 19.8 x 13.65 x 1 inches. Using previously documented Naval Postgraduate School research, desired random vibration analysis has been verified by impulse hammer techniques. Input excitation is provided by a combination piezoelectric-electromagnetic vibration generator system and response is recorded through the use of

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## 20. ABSTRACT (Continued)

piezoelectric accelerometers. The frequency range studied varies from 100 Hertz to 12,500 Hertz. The vibration generator is threaded into the specimen and the accelerometers are attached to the machined surface of the sample with a cyanoacrylate adhesive. Boundary support conditions include various: foam, bolted and shock-chord configurations.



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Effect of Boundary Conditions on the Damping Characteristics of a Randomly Excited Cast Nickel-Aluminum Bronze Specimen at Low Stress Levels

by

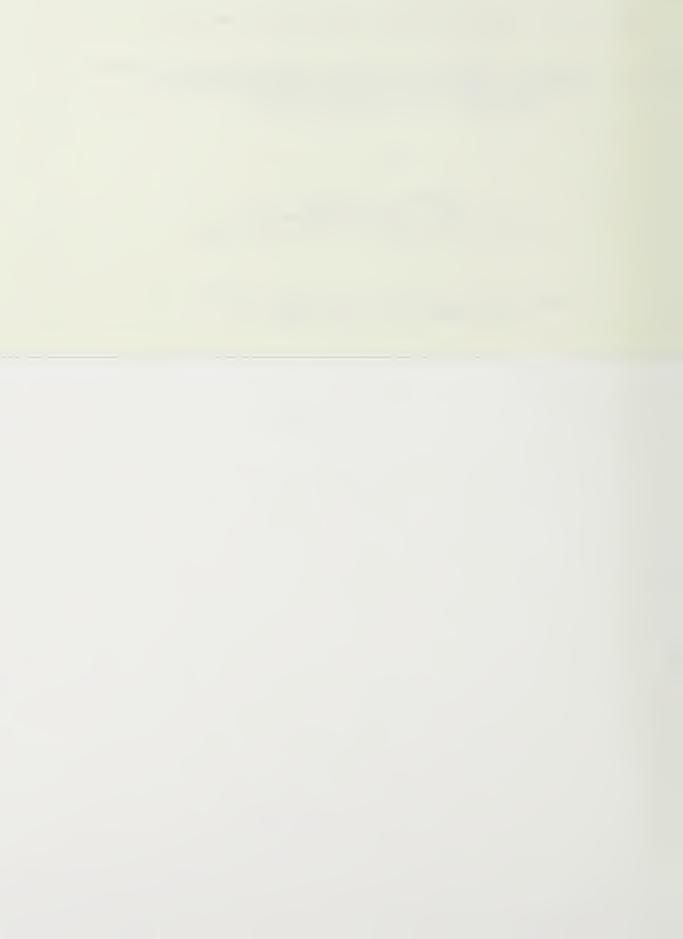
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This research examines how various specimen support arrangements affect a material's damping characteristics. The 74 lb. sample studied is cast nickel-aluminum bronze and measures 19.8 x 13.65 x 1 inches. Using previously documented Naval Postgraduate School research, desired random vibration analysis has been verified by impulse hammer techniques. Input excitation is provided by a combination piezoelectricelectromagnetic vibration generator system and response is recorded through the use of piezoelectric accelerometers. frequency range studied varies from 100 Hertz to 12,500 Hertz. The vibration generator is threaded into the specimen and the accelerometers are attached to the machined surface of the sample with a cyanoacrylate adhesive. Boundary support conditions include various: foam, bolted and shock-chord configurations.



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Y.S. Shin, Associate Professor, Naval Postgraduate School Ferman Milster, Lieutenant, United States Navy Ricky Heidgerken, Lieutenant, United States Navy



## I. INTRODUCTION

### A. NOTE TO THE READER

Please note that all tables and figures are chronologically grouped together in appendixes A and B respectively. The intent of this format is to facilitate location of the vital information contained therein for those readers using this document as reference material in the future. The casual and one-time reader may find it beneficial to review the contents of appendixes A and B prior to reading the remainder of this report.

# B. REVIEW OF PREVIOUS PERTINENT NAVAL POSTGRADUATE SCHOOL RESEARCH

This study follows the work initiated and performed by Lt. Ricky A. Heidgerken [Ref. 1]. There, a procedure for measuring the damping characteristics of relatively large metal plates at low stress levels has been designed and introduced. The testing environment is projected to be lab air or non-distilled water with medium (air/water) temperature control in the range of 30 to 90 degrees Fahrenheit. Samples are to be bolted into a support structure which can be immersed into a test chamber, specifically designed to allow for temperature control. His research has utilized the capabilities of a Hewlet-Packard 5451C Digital Fourier



Analysis system, combined with impulse hammer excitation, to determine desired damping characteristics in a frequency range between 100 Hertz and 12,500 Hertz. Maximum frequency is restricted to the frequency range of the available response accelerometers.

Lt. Heidgerken's work evolved to a point where he was able to take preliminary measurements on the test chamber itself, a cast nickel-aluminum bronze specimen bolted into a removable test chamber support structure and on the same specimen supported solely by a 3/4" thick foam pad. Conditions for these measurements are as follows: uncontrolled temperature (lab air), wax mounting for accelerometers, three or fewer measurement locations per test situation, impulse excitation and no specimen surface preparation other than mechanical cleaning. Future research, to include: random excitation, completion of the test chamber temperature control system and improvements to the established testing procedure, has been left for follow-on investigation.

## C. NATURE OF CURRENT RESEARCH

In a continuation of the broad scope of the research formalized in Ref. 1, this study centers on the effect of various boundary conditions on the damping characteristics of a 74 pound cast nickel-aluminum bronze specimen. The boundary support conditions include various foam, bolted and shock chord configurations. Random excitation is also



introduced (and validated) as the input energy source, replacing the impact hammer techniques utilized in the previous work with this specimen.

Various experimental considerations are explored to ascertain the optimal testing procedure to accomplish the goals set forth by the preceding research [Ref. 1]. Areas to investigate include: alternative accelerometer mounting techniques, specimen surface preparation, random excitation hardware mounting and the number of response pick-up locations desired.



# II. BACKGROUND

#### A. DAMPING

The capacity to remove from a structural vibration some of the energy associated with that vibration is termed structural damping [Ref. 2]. It increases the rate at which the free vibrations of a structure decay. Additionally, damping can lead to decreased sound transmission through a structure. Determination of material damping characteristics in the acoustic frequency range (100 Hertz to 20,000 Hertz), as they relate to structure silencing applications, is the overall objective of this ongoing research project.

Some commonly employed measures of damping are defined on the basis of viscous damping (i.e., damping that results from a retarding force that is proportional to the velocity). The ratio of the magnitude of that force to the velocity is called the viscous damping coefficient, "C." The smallest viscous damping coefficient for which nonoscillatory behavior is obtained is called the critical (viscous) damping coefficient, "C." Damping factor is defined as the percent of critical damping, i.e.,  $\text{C/C}_{\text{C}}$ . Loss factor equals twice the damping factor and is defined as the fraction of the system's energy that is dissipated per radian of the vibratory motion.

Theoretical discussion of pertinent vibration topics is covered in the preceding NPS thesis work [Ref. 1] and will not



be repeated here. For ease of location, the page numbers [Ref. 1] of important concepts are provided below.

Damping	. page	12
Measures of Damping	. page	17
Damping Mechanisms	. page	20
Theory of Frequency Response Function	. page	31
Display of Frequency Response	. page	38
Signal Processing	. page	44
Zoom Transform Analysis	. page	48
HP-5451C Fourier Transfer Function	. page	49
Modal Theory of Operation	. page	50
Identification of Modal Parameters	. page	57
Impulse Response of Complex Modes	. page	59
Modal Mass, Stiffness and Scaled Mode Shapes	. page	61
Measurement Implications of Modal Theory	. page	64

### B. AVAILABLE VIBRATION EXCITATION TYPES

Two types of input excitation are available to conduct damping measurements for this project. Impact testing was previously used [Ref. 1]. This form of input excitation testing does have some advantages. Namely, it is fast and requires no electro-mechanical shakers or noise sources. There are, however, some drawbacks. Variation between successive measurements can result from input force power spectrum fluctuations. Note: the input force is more easily controlled when using mechanical shakers (random excitation).



Poor signal-to-noise-ratios in impact measurements can result from a low excitation energy density. This is the result of the total energy, supplied by an impulse, being distributed over a broad frequency range. Inadequate frequency resolution can also be a problem. In order to obtain good frequency resolution for quantifying very lightly damped resonances, a large number of digital data points must be used to represent the signal. As the response signal decays to zero, its signal-to-noise ratio becomes smaller and smaller. If it has decayed to a small value before a data record is completely filled, the Fourier transform will be operating mostly on noise, causing uncertainties in the transfer function measurement. This can be reduced by using a force window on the input power spectrum. The problem becomes acute as higher frequency resolutions are needed and as more heavily damped structures are tested. Even with the above limitations, impact testing is a valuable tool for vibration analysis [Ref. 3].

Three types of random excitation can be used for making frequency response measurements. They are: (1) pure random, (2) pseudo random and (3) periodic random [Ref. 4]. Pure random is not periodic. Pseudo random is exactly periodic every "t" seconds. Periodic random is a combination of both; i.e., a pseudo random signal that is changed for every measurement. Both pseudo and periodic random signals are generated by the analyzer's (HP-5451C) processor and output



to the structure via a digital-to-analog (DAC) converter, whereas pure random must be generated by an external signal generator.

Pure random excitation is used for this research. The external signal generator output is passed through a by-pass filter in order to concentrate energy in the band of interest. Except for the filter roll-off, the signal spectrum will be flat and the overall level easily controlled. An Hewlett-Packard 3582A Spectrum Analyzer is used to provide bandlimited white noise for the damping measurements contained herein. White noise is defined to have a constant spectral density, S, at all frequencies (i.e., random data with energy distributed uniformly over all frequencies [Ref. 5]). With a pure random signal, each sampled record of data "t" seconds long is different from preceding and following records. As such, successive records of frequency domain data can be averaged together to remove nonlinear effects, noise and distortion from the measurement. As more and more averages are taken, all of the components of noise will average toward an expected value of zero in the frequency domain data. Thus, a much better measure of the response of the structure can be obtained. This is the single most important advantage of using a pure random signal for transfer function measurements.

A drawback of pure random excitation is that the measured input and response signals are not periodic in the measurement time window of the analyzer. A key assumption of digital



Fourier analysis is that the time waveforms be exactly periodic in the observation window. If this condition is not met, the corresponding frequency spectrum will contain so-called leakage due to the nature of the discrete Fourier transform; that is, energy from the non-periodic parts of the signal will leak into the periodic parts of the spectrum, thus giving a less accurate result.

To combat the effects of leakage, Band Selectable Fourier Analysis (BSFA), the so-called zoom transform, is used to collect data. Here, the Fourier transform is performed over a frequency band whose lower and upper limits are independently selectable. BSFA provides increased frequency resolution without increasing the number of spectral lines in the computer (the same number of data points are used, but now in a small frequency bandwidth). Zoom transforms also increase the dynamic range of the measurement to 90 dB or more in many cases. By using BSFA, leakage is no longer an important source of error. Coherence measurements taken during this research were unity in most cases, indicating the absence of any error due to leakage, and confirming the quality of the BSFA measurements taken.

Neither pseudo or periodic random excitation were used to take the 960 zoom transfer function measurements required by this research. However, 32 baseband measurements were taken using pseudo random excitation to assist in choosing



center frequencies for the boundary condition BSFA measurements.

### C. ACCELEROMETER MOUNTING CONSIDERATIONS

Three types of accelerometer mounting techniques are available for use in testing (wax, glue or screwed). Using BSFA, coherence measurements were conducted to ascertain the optimum accelerometer mounting technique to be used throughout the remainder of the research. The two accelerometers tested were a PCB #302A (fmax - 5,000 Hertz) and a PCB #303A (fmax = 10,000 Hertz). Center frequencies were chosen at 3,650 Hertz and 8,500 Hertz respectively. Bandwidths for each measurement were 1,000 Hertz. Figure 1 through 5 provide the results of these preliminary experiments. The specimen tested is the cast nickel-aluminum bronze plate previously studied [Ref. 1]. It is supported fully by a 3" foam pad. Figures 1, 2 and 3 are the coherence measurements for wax, screwed and glue mounting respectively. Notice that the coherence becomes progressively better, with the glue being optimum. Similar results were obtained with the PCB #303A accelerometer. The wax mounting (Figure 4) is degraded as compared to the glue mounting (Figure 5). From these measurements, glue accelerometer mounting is chosen to conduct the boundary condition measurements. Note: the glue utilized is a commercial "Super Glue" type cyanoacrylate adhesive.



## III. EXPERIMENTAL PROCEDURE

# A. EQUIPMENT DESCRIPTION

As noted in chapter II, zoom measurement techniques using random excitation provide excellent frequency resolution for data collection. Obtaining these BSFA measurements accurately is the essence of this study of boundary condition effects.

To clearly understand how these measurements are taken, a sequential description of the equipment utilized for a typical zoom measurement is provided below. Using a line diagram (Figure 6) as a guide, the order of equipment presented will be from the random noise source to the data reduction hardware. Other equipment used in: baseband determinations, the alternative accelerometer mounting investigation and impulse hammer vs. random comparisons will then be highlighted.

- (1) HEWLETT-PACKARD #3582 SPECTRUM ANALYZER: Supplies white noise to drive the vibration generator. Also allows monitoring of the Fourier analyzer's A & B input channels, thus serving as an independent check for transfer function measurements.
- (2) HEWLETT-PACKARD #467A POWER AMPLIFIER: Boosts random signal to the minimum required by the vibration generator system power amplifier.
- (3) HEWLETT-PACKARD #3400 RMS VOLTMETER: Allows monitoring of the H.P. amplifier output.



- (4) WILCOXIN RESEARCH #PA7C POWER AMPLIFIER: Provides
  100 watts of power per channel to vibration
  generator system.
- (5) WILCOXIN RESEARCH #N7C MATCHING NETWORK: Provides impedance matching for the reactive load of the F7 shaker and overload protection for the F4 shaker.
- (6) WILCOXIN RESEARCH #F7/F4 VIBRATION GENERATOR:

  Provides actual input excitation to test specimen.

  The shaker base contains a force sensing element to monitor the actual force applied to the sample

  (i.e., channel "A" input to the Fourier analyzer).
- (7a) PCB #302A QUARTZ ACCELEROMETER: Measures acceleration of vibration motion fmax = 5,000 Hertz.
- (7b) ENDEVCO #2250A PIEZOELECTRIC ACCELEROMETER: Measures acceleration of vibration motion, fmax = 15,000 Hertz.
- (8a) PCB #480D06 SIGNAL CONDITIONER: Supplies constantcurrent power to the accelerometer's transducer.
- (8b) ENDEVCO #4416A SIGNAL CONDITIONER: Supplies constantcurrent power to the accelerometer's transducer.
- (9) HEWLETT-PACKARD #54440A PROGRAMMABLE LOW PASS

  FILTERS: Automatically protects measurements from errors due to aliasing of out-of-band frequencies.
- (10) HEWLETT-PACKARD #54470A PRE-PROCESSOR: Allows fast and convenient Band Selectable Fourier Analysis.
- (11) HEWLETT-PACKARD #5451C FOURIER ANALYZER: Provides digital frequency domain analysis of complex time



signals. Its modal analysis application package operates on measured transfer function data to determine modal properties (i.e., natural frequencies, damping factors and mode shapes).

The remaining equipment used includes: (1) A PCB #086B03 impulse hammer, used as an excitation source in impact vs. random comparisons, (2) A PCB #303A accelerometer, used in preliminary testing of accelerometer mounting techniques, and (3) A Hewlett-Packard #54420A digital-to-analog converter, used to generate a pseudo random source signal for baseband measurements. Note: Figure 7 is a line drawing of the experimental baseband measurement set-up. The Naval Post-graduate School Modal Analysis Laboratory equipment room is shown in Figure 8.

Examples of the HP-5451C Fourier analyzer's graphical displays (either by CRT, terminal screen or printer) available to the user are shown in Figure 9 thru 16. They are representations of: coherence, log mag/polar/rectangular/complex (Nyquist) transfer functions, and input/output/cross power spectrum measurements respectively.

## B. SAMPLE PREPARATION

Various preliminary steps need to be taken to prepare the specimen for testing. To ensure reliable data acquisition, accelerometer mounting surfaces (i.e., entire plate) should be squared and machined flat. A 3/8" diameter mounting hole must be drilled and tapped into the specimen in order to accept the



vibration generator's threaded stud. A 1" by 1" square grid system, laid out on the specimen with a permanent marker, is recommended to enable documentation of response locations. Four samples (a cast magnesium bronze, an aluminum alloy (5086-H116), a steel plate (HY-130) and a cast nickel-aluminum bronze) in various stages of preparation are shown in Figure 17. A close-up of the cast nickel-aluminum bronze sample ready for testing is shown in Figure 18.

# C. MEASUREMENT TECHNIQUE

The basic procedural steps required to conduct data collection and reduction are as follows:

- (1) Conduct baseband measurements to determine location (frequency) of the vibration modes to be studied.
- (2) Take BSFA measurements centered on the frequencies chosen in step one above.
- (3) Manually store, via the 5451C's mass store commands, zoom transfer function measurements (in rectangular form) onto the removeable modal disk.
- (4) Perform modal analysis, using the Fourier analyzer's application package, on the stored zoom transfer function data to determine desired damping characteristics.

Four different boundary conditions are analyzed for their effect on the specimen's damping factor throughout a frequency range up to 12,500 Hertz. They are described in chapter IV and are designated boundary condition #1, #2, #3 and #4. For

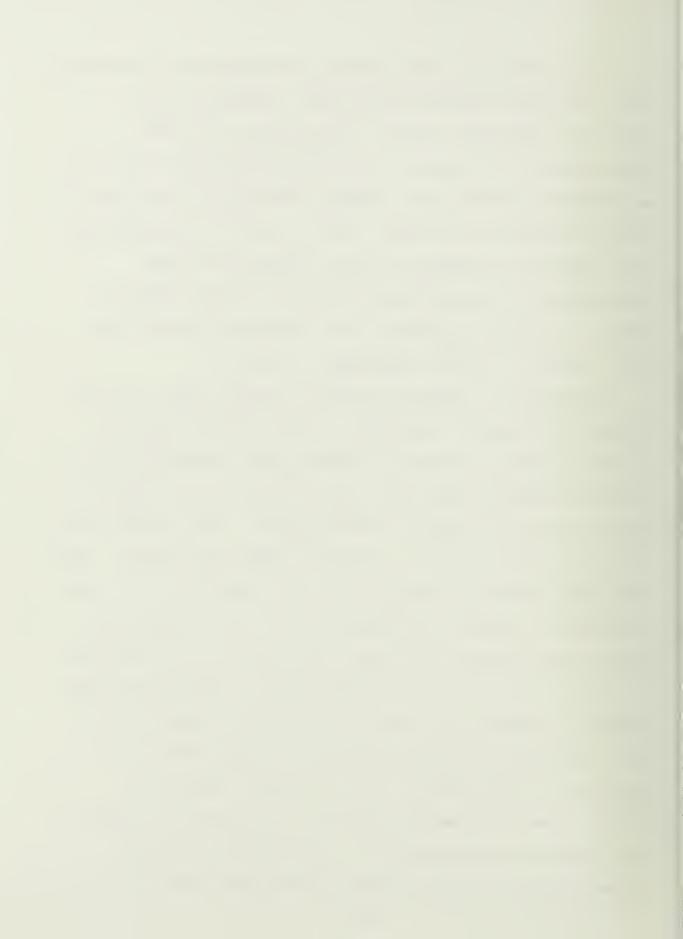


each boundary condition, grid locations 3, 6, 14 and 20 are used to record specimen response (via an attached accelerometer) to random excitation for baseband measurements, O Hertz to some fmax. For a given boundary condition, two separate baseband measurements (0 to 5,000 Hertz and 0 to 12,500 Hertz) are taken at each of the four designated baseband grid locations. This provides higher resolution in the frequencies below 5,000 Hertz, as compared against a single 0 to 12,500 Hertz baseband. Considering two basebands per grid location and four designated baseband grid locations per boundary condition, eight baseband measurements are required for each of the boundary conditions (32 total to completely document specimen baseband response for the four support configurations studied). These 32 baseband measurements are displayed in Figure 19 thru 50. They are arranged sequentially according to boundary condition number and accordingly by response grid location within the grouping for a particular boundary condition. The four lower frequency basebands are first, followed by the four higher frequency basebands. Note: Only a portion (5,000 Hertz to 12,500 Hertz) of the higher frequency baseband is plotted since a higher resolution baseband below 5,000 Hertz has already been The PCB #302A accelerometer is used in boundary produced. condition #1 to take the lower frequency baseband data. Endevco #2250A accelerometer is used to take the higher frequency baseband data for all boundary conditions, as well



as for the remaining lower frequency basebands for the second, third and fourth boundary conditions. Because of the frequency limitations (fmax = 5,000 Hertz) of the PCB accelerometer, the switch to the Endevco transducer for all measurements substantially reduces the actual elapsed time of the data acquisition process. This is due to the additional time expended in breaking free and cleaning the PCB accelerometer, then mounting the Endevco accelerometer to complete the data acquisition (for frequencies beyond the PCB's range) at a given measurement location.

Individually, compare the eight baseband plots for each of the four boundary conditions. Choose twelve peaks per boundary condition (from the plotted polar representations of baseband transfer functions) that span the entire frequency range studied, 100 Hertz to 12,500 Hertz. These peaks become the center frequencies for follow-on BSFA measurements. The number twelve is arbitrary and is a function of the time available to conduct the research more than anything else. Twice as many peaks could easily be identified and analyzed. It is felt that 12 is the minimum number of BSFA measurements needed to analyze the effect of a particular boundary condition, allowing an average separation between center frequencies of 1,000 Hertz. Vary the center frequencies chosen, from one boundary condition to the next, to obtain a more complete representation of the specimen's damping characteristics across the desired frequency spectrum.



Once center frequencies are identified for a particular boundary condition, take zoom transfer function measurements as desired and store them (in rectangular form) on the removeable modal disk via the analyzer's mass store commands. Check coherence measurements at each measurement to ensure correctness of the stored data. Beginning with boundary condition #2, temperatures of the sample for each measurement are recorded. This is accomplished using a thermocouple taped onto the bottom of the specimen during testing. All experimental data and disk storage locations are documented in Tables I thru IV. The following conditions are recorded for each of the 960 transfer function measurements taken:

- \*\*\* Disk label (i.e., "Steve's Modal One")
- \*\*\* Disk storage record number (e.g., 1 to 500)
- \*\*\* Grid location of response accelerometer (e.g., 1 to 20)
- \*\*\* Number of averages taken by the Analyzer per measurement (i.e., 10)
- \*\*\* Center frequency of the zoom measurement (Hertz)
- \*\*\* Bandwidth selected (i.e., 50 Hertz)
- \*\*\* Type of input excitation (e.g., Impact or Random)
- \*\*\* Temperature (measured in degrees Celsius)
- \*\*\* Computer set-up data number (e.g., 1 to 5)
- \*\*\* Boundary condition description (i.e., "FOAM (pad)")

Note: The computer set-up data number contains the following line items: number of measurements, disk storage location



(record number) of the first measurement, block size, polar transfer function display type (linear or log), input and response transducer scale factors and input and response amplifier gain values.

After all of the BSFA measurements are recorded for a certain boundary condition, the Fourier analyzer's modal analysis application package can be utilized to retrieve stored transfer function data from the removeable disk. Damping factors and natural frequencies for individual modes of vibration can now be determined through a number of interactive steps between user and computer [Ref. 6].

### D. USER DEVELOPED KEYBOARD PROGRAMS

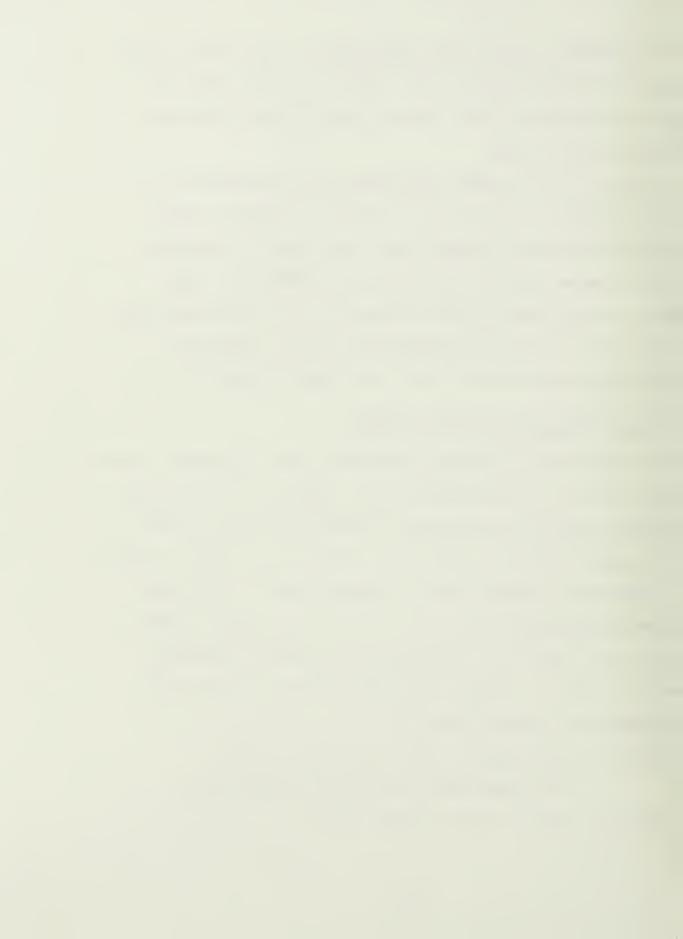
To facilitate the above procedure, and to automate certain capabilities of the HP-5451C Fourier analyzer, five locally developed interactive keyboard programs have been written.

Their actual program listings are provided in Figure 51 thru

55. They are invoked from the graphics mode of the modal analysis measurement step (No. 2) with the command "JUMP 0 (space) nn." Where "nn" represents the keyboard program numerical label. A brief description of what these five programs do is provided below:

LABEL "1"--Interactive impact testing procedure,
utilizing Hewlett-Packard pre-processor.

LABEL "5"--Partial plot of CRT display.



LABEL "10"--Interactive random testing procedure,
utilizing Hewlett-Packard pre-processor.

LABEL "15" -- Data transfer between removeable disks.

LABEL "16"--Plotting routine for stored animated mode shapes (to be used in follow-on research).

### E. IMPACT TESTING vs. RANDOM TESTING

To obtain correlation between impact and random testing, five zoom measurements were compared using similar test conditions for each method of excitation. The PCB #302A accelerometer was used for the impact response measurements, and the Endevco #2250A accelerometer utilized for random response data. Three different pick-up locations were used per center frequency tested. The almost identical results between the two methods are shown in Table V and displayed graphically in Figure 56. This close correlation was expected, but needed to be confirmed to lend credibility to the 960 BSFA transfer function measurements taken during this project to determine boundary condition effects.



# IV. BOUNDARY CONDITION TESTING

### A. DESCRIPTION OF BOUNDARY CONDITIONS TESTED

As previously indicated, four different support configurations for testing the cast nickel-aluminum bronze sample are investigated as to their possible effect on the material's damping factor. A brief description of each of the conditions analyzed follows:

- (#1) FOAM (pad): The specimen is laid on a large 3"
   thick foam pad. Testing is done on a 4 by 6 foot
   marble table to isolate possible extraneous
   excitations from the environment. Figure 57 shows
   the configuration.
- (#2) BOLTED (tank): The specimen is bolted at one end into the removeable test chamber support structure. Eight 3/4" diameter bolts (four on each side of the plate) are used to secure the sample in place. Two 1/8" thick metal strips are placed between the bolts and the specimen to distribute the bolt force along the edge of the sample. Figure 58 shows the configuration.
- (#3) CHORD (tank): The specimen is cradled in four 1/2" diameter shock chords. Hose clamps are used to secure the chords to the removeable test chamber



- support structure. Figure 59 and 60 show different aspects of this configuration.
- (#4) FOAM (ends): The specimen is supported at each end by a 2 inch square foam strip. When in place, the sample rests 3/8" above the marble testing table surface. Figure 61 shows the configuration.

### B. REFINED EXPERIMENTAL PROCEDURE

The following is a review of experimental techniques employed in the preceding vibration testing [Ref. 1] of this specimen:

- \*\*\* The sample was tested in the as received condition, with the exception of minor mechanical cleaning.
- \*\*\* Wax was used to mount accelerometers.
- \*\*\* Input excitation was provided by an impulse hammer.
- \*\*\* Three measurement points (hammer impact locations in the case of impulse testing) per center frequency were tested.
- \*\*\* BSFA measurements were limited to four or fewer averages and wider bandwidths (less zoom power) due to lengthy computer measurement times encountered without pre-processing hardware. Using 4 averages at a zoom power of 128, a twenty minute measurement time was common for one BSFA measurement.

Current research, with the addition of the necessary equipment, has allowed refinement and improvement of these procedural steps as follows:



- (1) The specimen is squared and machined flat prior to testing. A grid system is drawn onto the sample to accurately document response measurement locations.
- (2) Glue is used for accelerometer mounting.
- (3) White noise is used for input excitation.
- (4) Twenty measurement locations (accelerometer pickup locations in the case of random testing) are utilized.
- (5) Pre-processing equipment is incorporated to greatly reduce actual measurement times (thus allowing for more averages and smaller bandwidths). Note: The time required to complete one measurement has been reduced by as much as 95% in some cases and done with greater accuracy (resulting from the increased number of averages and a higher input spectral densities).

#### C. RESULTS AND OBSERVATIONS

Modal analysis was performed on the stored data for each boundary condition using the application package available with the HP-5451C Fourier analyzer. The results (damping factors and natural frequencies) are shown in tabular form in Table VI. Graphical results (damping & loss factors vs. frequency) for boundary conditions 1, 2, 3 and 4 are represesented in Figure 62 to 65 respectively. Note: Loss Factor = 2 times Damping Factor. A summary plot of all data collected for the four support arrangements is shown in Figure 66.

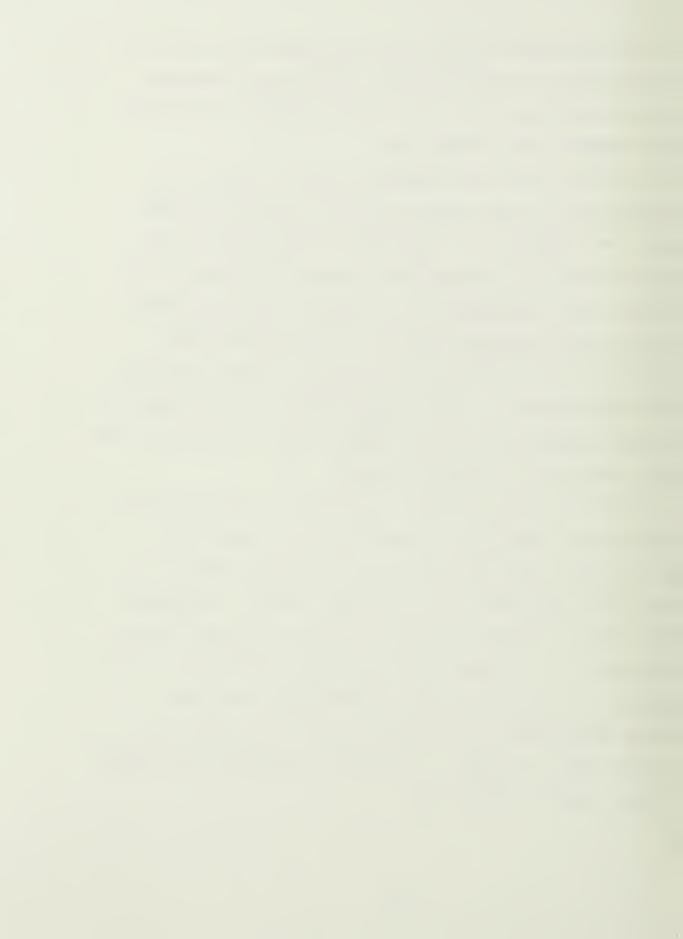


The curves through the data points of Figure 62 to 65 were produced using a rational spline interpolation technique.

A spline smoothing routine was used to generate the Experimental Summary curve (Figure 66).

All of the individual boundary condition curves show rapid decreases in the damping factor from zero to 1,000 Hertz. The summary plot indicates a leveling off of the damping factor to an average value between 0.05% and 0.15% throughout the remainder of the frequency spectrum studied. Relatively high damping factors are seen between 8,000 Hertz and 10,000 Hertz in all individual boundary condition plots except number 2. The damping factors for the FOAM (pad) boundary condition are notably higher than those for the FOAM (ends) condition at a given frequency.

One final note of interest regarding the bolted boundary condition was observed. In conducting the measurements, it is seen that many more modes are appearing during BSFA for the bolted case then show up for the other support arrangements under similar testing conditions. Figure 67 shows a Nyquist plot taken for the CHORD (tank) boundary condition at a center frequency of 8,221 Hertz over a bandwidth of 50 Hertz. A similar measurement (CF = 8,152, BW = 50) taken for the bolted boundary condition shows a significant increase in the number of modes excited (Figure 68).



## V. CONCLUSIONS

Although there is some scatter in the experimental results, boundary conditions do not appear to be a significant contributor to the material's damping characteristics. The order of magnitude of the resulting damping factors do not vary from one boundary condition to the next. Temperature fluctuations of as much as 8 degrees Celsius were encountered during some BSFA measurements (during the time required to complete the 20 measurements at a particular center frequency). This may be a significant factor in the observed scattering of resulting damping characteristics. Considering the extremely small values calculated for the damping factor, i.e., averaging 0.05% to 0.15% for frequencies above 1,000 Hz., this material can be expected to readily transmit energy in the acoustic frequency range.

Since increases in damping between 8,000 and 10,000 Hertz are noted in all of the boundary conditions (less notable for the bolted case), it is felt that this is more likely to be a material property of the metal rather than the result of a particular support configuration.

A possible cause for the relatively high damping observed in boundary condition #1, FOAM (pad), is coupling of the foam support to the metal plate. This interaction takes place on the entire bottom surface of the sample. The weight of the



specimen, 75 lbs., causes it to sink 1" into the 3" thick foam pad. The contact area between the foam and the metal plate equals 270 square inches. In contrast, the contact area between the sample and supporting foam in boundary condition #4, FOAM (ends), is only 20 square inches. Note: The damping factor for this end support configuration is lower throughout the frequency range studied as compared against the full pad support case.

The bolted boundary condition revealed increases in the number of modes excited to an extent that isolation of single modes of interest in BSFA was difficult. The contributing factor is attributed to transmission of the removeable test chamber support structure's own modes through the pressure bolts into the test specimen. This being the case, a switch to shock chord specimen support for the follow-on research is recommended.



## VI. RECOMMENDATIONS FOR FUTURE WORK

Having refined the testing procedure to accommodate random excitation, the most significant remaining original tasking is to take measurements at a constant temperature, initially in air. This is to be followed by varying temperature experiments in a water environment. The capability to test at a designated temperature will allow analysis as to the effect of the temperature on the damping characteristics of the specimen in question, i.e., in the same regard that this report studied boundary condition effects. Testing other available samples (aluminum, steel and magnesium bronze) will allow comparisons against a standard, the cast nickel-aluminum bronze specimen, under similar testing environments. Finally, a comparison of the HP-5451C's animated mode shapes against NASTRAN generated data may help to validate experimental procedures.



	Boundary Condition	POAM (pad)	FOAM (pad)	FOAM (pad)	POAM (pad)	FOAM (pad)	POAM (pad)	FOAM (pad)	POAM (pad)	FOAM (pad)												
(one) "	Setup Data No.	7	3	7	ਰ	#	3	7	J	ħ	ੜ	#	ħ	コ	ח	ੜ	ח	ੜ	#	J	т т	
	Temp.	1		!	-	;	:	-	;	;	:	;	:	;	:	;	:	;		:	-	
Steve's Modal	Input	Random	4 C C C C C C C C C C C C C C C C C C C																			
	Band Width	150	150	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	
Disk Label	Center Frequency	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	12206	
	Number	10	10	10	10	10	i	10	i	10	-	10	10	1	10	ĺ	10	10	10	10	10	
	Grid	1	2	3	3	5	9	7	8	6	10		12	13	14	15	16	17	18	19	2.0	,
	Disk	101	102	103	104	105	106	107	108	109	110		112	113	114	115	116	117	118	119	120	



		<del>,</del>			,		_			,		,	,				,	_			, ,
	Boundary Condition	POAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	POAM (pad)	FOAM (Fad)	POAM (pad)	FOAM (pad)								
ne) "	Setup Data No.	7	3	7	ħ	ħ	7	ħ	ħ	7	3	#	3	7	ħ	7	7	7	7	7	ħ
lal (or	Temp.	1	:	-	-	:	-		-	-	;	:	;	:	-	;	1	-	-	;	-
"Steve's Modal (one)"	Input	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random
.	Band Width	20	50	5.0	50	20	20	5.0	50	50	20	50	5.0	20	20	20	5.0	5.0	20	20	5.0
Disk Label	Center Frequency	11152	11152	11152	11152	11152	11152	11152	11152	11152	11152	11152	11152	11152	11152	111152	11152	11152	11152	11152	11152
	Number	15	15	15	15	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	7	5	9	7	60	6	10		12	13	74	15	16	17	18	19	2.0
	Disk	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140

Table I. (Continued)



Table I. (Continued)



•	Boundary	FOAM (pad)	POAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	POAM (pad)	FOAM (pad)												
ne) "	Setup Data No.	7	ħ	ħ	#	ħ	ੜ	7	7	J	3	ħ	7	77	ħ	3	7	7	7	ħ	7
Modal (one)"	Temp.		!	-		-		-	:	1	;	1	1	-	-	1		-	-	-	
Stevers	Input	Random																			
	Band Width	5.0	20	50	20	20	20	50	5.0	50	20	20	50	20	20	50	5.0	50	20	20	50
Disk Label	Center Frequency	1996	h996	1996	h996	h996	h996	h996	1996	1996	1996	1996	1996	1996	h996	1996		h996	h996	1996	9664
	Number	15	15	15	15	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	8	6	10		12	13	14	15	16	17	18	19	2.0
	Disk	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180

Table I. (Continued)



rable I. (Continued)



						,		,													
	Boundary Condition	POAM (pad)	FOAM (pad)	POAM (pad)	POAM (pad)	POAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)												
ne)"	Setup Data No.	3	J .	3	3	3	3	3	<b>3</b>	7	7	3	3	3	ħ	i i	ħ	3	3	T T	3
la 1 (or	Temp.	:	!	1	1	-	-	;	-	;	:	H		-	-	-	;	-	;	1	:
"Steve's Modal (one)"	Input	Random																			
	Eand Width	50	50	50	50	50	50	50	20	50	50	50	50	50	50	50	20	50	50	50	50
Disk Label	Center	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169	7169
	Number	15	15	15	15	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220

Table I. (Continued)



	<del></del>	_	_	_		_	_												-		
	Boundary	FOAM (pad)	POAM (pad)	POAM (pad)	POAM (pad)	FOAM (pad)	POAM (pad)	FOAM (pad)	FOAN (pad)	POAM (pad)											
ne) "	Setup Data No.	3	3	7	7	7	3	3	7	3	3	ħ	#	7	3	3	7	7	7	7	7
lal (or	Temp.	:	-		-	1	1	-	:	:	;	:		-	1	-	-	-	;	;	
"Steve's Modal (one)"	Input	Random																			
	Band	50	50	5.0	50	5.0	50	50	50	50	50	50	50	20	50	50	50	5.0	50	50	50
Disk Label	Center Frequency	6 0 95	6 0 95	6 0 95	6095	6 0 95	6 0 95	6095	6 0 95	6095	6 0 95	6095	6 0 95	6 0 95	6 0 95	6 0 95	6095	6 0 95	6 0 95	6 0 95	6 0 95
	Number	20	20	20	20	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	7	5	9	7	8	6	10		12	13	14	15	16	17	18	19	2.0
	D1sk Record	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240

Table I. (Continued)

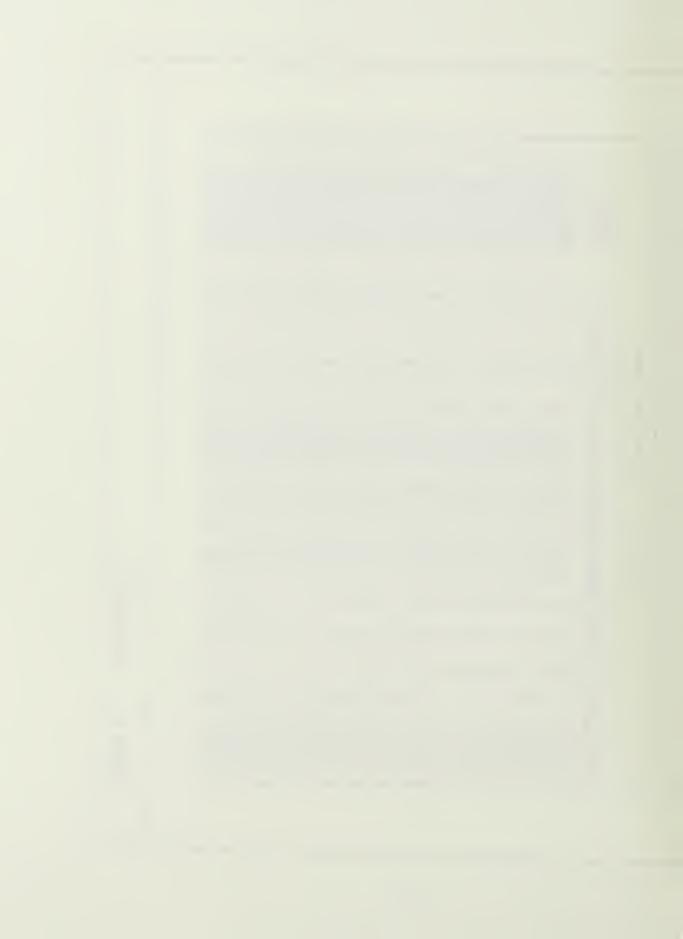


•	Bounda Fy Condition	FOAM (pad)	POAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	FOAM (pad)	POAM (pad)	FOAM (pad)												
1e) "	Setup Data No.	7	<b>3</b>	7	7	<b>=</b>	7	3	⇒	3	3	<b>¬</b>	7	3	7	3	3	3	3	⇒	3
lal (or	Temp.	;	;	-		;	-	;	1	1		:	;	-	;	;	-	:	;	-	;
"Steve's Modal (one)"	Input	Random																			
	Band Width	50	50	50	5.0	50	50	50	50	20	50	50	50	5.0	50	5.0	50	50	50	50	50
Disk Label	Center Frequency	4728	4728	4728	4728	4728	4728	4728	4728	4728	4728	4728	4728	47 28	4728	4728	4728	4728	4728	4728	4728
	Number	15	15	15	15	10	10	10	10	10	10	30	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	3	5	9	7	8	6	10	11	12	13	14	15	16	17	1.8	19	2.0
	Disk	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260

Table I. (Continued)



rable I. (Continued)



	Boundary	FOAM (pad)	FOAM (pad)	FOAM (Fad)	FOAM (pad)	FOAM (Fad)	FOAM (pad)														
ne)"	Setup Data No.	7	3	3	3	3	7	7	7	=	7	7	7	7	7	7	7	3	7	3	7
lal (or	Temp.	:	-	;	-	-	:	:	-	-	!	:		-	:	-	:	-		-	1
"Steve's Modal (one)"	Input	Random																			
	Eand	50	50	50	50	50	50	50	50	50	50	50	50	50	50	20	50	50	50	50	20
Disk Label	Center Frequency	2611	2611	2611	2611	26 11	2611	26 11	2611	26 11	2611	26 11	2611	26 11	2611	26 11	2611	26 11	2611	26 11	2611
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	-	2	3	7	5	9	7	8	6	10	11	12	13	7	15	16	17	18	19	2.0
	Disk	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300

Table I. (Continued)



	Boundary	FOAM (pad)																			
ne) "	Setup Data No.	7	7	<b>=</b>	7	<b>ə</b>	<b>=</b>	<b>コ</b>	7	<b>3</b>	<b></b>	7	<b>3</b>	7	<b>=</b>	3	3	<b>3</b>	<b>→</b>	7	7
la 1 (or	Temp.	:		-	-	8	-	-			-	-	-	-	1	:	1	-	-	-	
"Steve's Modal (one)"	Input	Random																			
	Pand	0.17	50	50	20	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	5.0
Disk Label	Center Frequency	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	7	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320

Table I. (Continued)



							,														
	Boundary Condition	FOAM (pad)																			
(one)"	Setup Data No.	3	3	ī	3	3	3	3	3	3	7	<b>寸</b>	3	3	3	3	7	す	#	3	3
Modal (o	Temp.			:	;	;	;	:	1	1	;	:	:	1		;	;	:	;	;	:
"Steve's Mod	Input	Random																			
	Pand Width	50	5.0	5.0	50	20	20	5.0	5.0	5.0	20	5.0	5.0	5.0	20	20	5.0	5.0	20	5.0	5.0
Disk Label	Canter Prequency	421	421	421	421	421	421	421	4 21	421	421	421	421	421	421	421	421	421	421	421	421
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	8	6	10	11	1.2	13	14	15	16	17	18	19	2.0
	Disk	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340

Table I. (Continu€d)



	Boun dary Condition	BOLTED (tank)	EOLTED (tank)	BOLTED (tank)																	
(two)"	Setup Data No.	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
Modal (t	Temp.	12	12	12	12	10	6	89	7	10	10	10	13	14	14	14	14	14	13	12	=
Steve's	Input	Random	Randem	Random	Random	Random															
11 : 11	Band Width	50	50	50	50	50	50	50	50	50	50	20	50	50	50	50	50	50	50	50	50
Disk Label	Center Frequency	278	278	278	2.78	278	2 78	278	278	2 78	278	278	2.78	278	2.78	2.78	2 78	278	2.78	278	278
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	3	5	9	7	8	6	10		12	13	14	15	16	17	18	19	2 0
	Disk	-	2	3	7	5	9	7	8	6	10	=	12	13	14	15	16	17	18	19	20

Experimental data - BOLTED (tank) Table II.



								,							,		,				,
•	Boundary Condition	BOLTED (tank)	BOLTED (tank)	, BOLTED (tank)	BOLTED (tank)																
#o}	Setup Data No.	3	ħ	3	Þ	=	3	3	7	3	7	3	7	3	3	3	7	=	7	3	7
Modal (two)"	Temp.	12	12	12	12	10	6	89	7	10	10	10	13	14	14	14	14	14	13	12	11
Steve's	Input	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random
. 19	Band Width	20	20	50	50	50	50	50	50	50	50	50	50	50	50	90	50	50	50	20	5.0
Disk Label	Center Fraguency	6 18	6 18	6 18	618	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18	6 18
	Number Averages	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	=	5	9	7	8	6	10		12	13	7	15	16	17	18	19	2.0
	Disk	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	017

Table II. (Continued)



				,						,							,				
	Boundary Condition	BOLTED (tank)																			
(two)"	Setup Data No.	3	3	3	3	3	3	7	3	3	3	3	7	3	3	7	3	7	3	7	7
Modal (t	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	14	14	14	13	12	=
"Steve's Mod	Input	Random																			
	Band Width	50	50	5.0	50	5.0	50	50	50	50	50	5.0	50	20	20	50	50	50	50	50	50
Disk Label	Center Fraquency	19.14	1914	1914	1914	1914	1914	19 14	1914	19.14	1914	1914	1914	19 14	19 14	1914	1914	1914	1914	1914	19 14
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	80	6	10	11	12	13	14	15	16	17	18	19	20
	Disk	4.1	42	43	777	45	917	47	87	611	50	51	52	53	カジ	55	95	57	58	- 29	09

Table II. (Continued)



•	Poundary Condition	BOLTED (+ank)	BOLTED (tank)	EOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	EOLTED (tank)	EOLTED (tank)	BOLTED (tank)	BOLTED (tank)									
(two)"	Setup Data No.	#	<b>=</b>	#	7	#	3	<b>=</b>	3	3	7	3	7	=	7	3	7	Ħ	<b>ə</b>	7	3
Bodal (t	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	14	14	14	13	12	11
Steve's	Input	Random																			
	Band Width	50	50	50	5.0	20	50	50	50	50	50	50	50	50	20	50	20	20	20	5.0	50
Disk Label	Center Frequency	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196	3196
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk	19	62	63	119	65	99	13	89	69	70_	71	72	73	74	75	76	11	78	79	80

Table II. (Continued)



		,													,						
	Boundary Condition	BOLTED (tank)																			
(tvo) <sup>H</sup>	Setup Data No.	7	<b>a</b>	7	#	7	3	7	3	7	3	7	3	7	đ	ī	3	7	3	7	3
Modal (t	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	14	14	14	13	12	11
Steve's	Input	Random																			
	Pand	50	5.0	50	5.0	50	50	5.0	50	50	50	50	50	50	50	50	50	50	50	5.0	50
Disk Label	Center Freguency	4 256	4 2 56	4 2 56	4 2 56	4 256	4 2 56	4 256	4 2 56	4 256		4 256	4 256	4 256	4 256	4 256	4 2 56	4 256	4 256	4 256	4 2 56
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	-	2	3	3	5	9	7	8	6	10	11	12	13	7	15	91	17	18	19	2.0
	Disk	81	82	83	94	982	98	18	88	- 68	06	91	92	93	16	95	96	- 6	96	66	100

Table II. (Continued)



		, .						,	, .	,			,								,
	Boundary Condition	BOLTED (tank)																			
(two)".	Setup Data No.	7	3	ā	3	コ	3	Þ	#	3	3	3	3	7	Ħ	<b>3</b>	Ħ	7	Þ	7	ħ
Modal (tı	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	ηl	14	ηį	14	13	12	=
Steve's	Input	Random																			
.1: "	Band Width	50	50	20	50	20	50	50	50	50	50	50	50	50	20	20	20	50	50	50	50
Disk Label	Center Frequency	56 16	56 16	56 16	5616	56 16	5616	56 16	5616	56 16	56 16	56 16	56 16	56 16	56 16	56 16	5616	56 16	56 16	56 16	56 16
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	8	6	10		12	13	10	15	16	17	18	19	2.0
	Disk	101	102	103	104	105	106	107	1 08	109	100	131	112	113	114	115	116	117	118	119	120

Table II. (Continued)



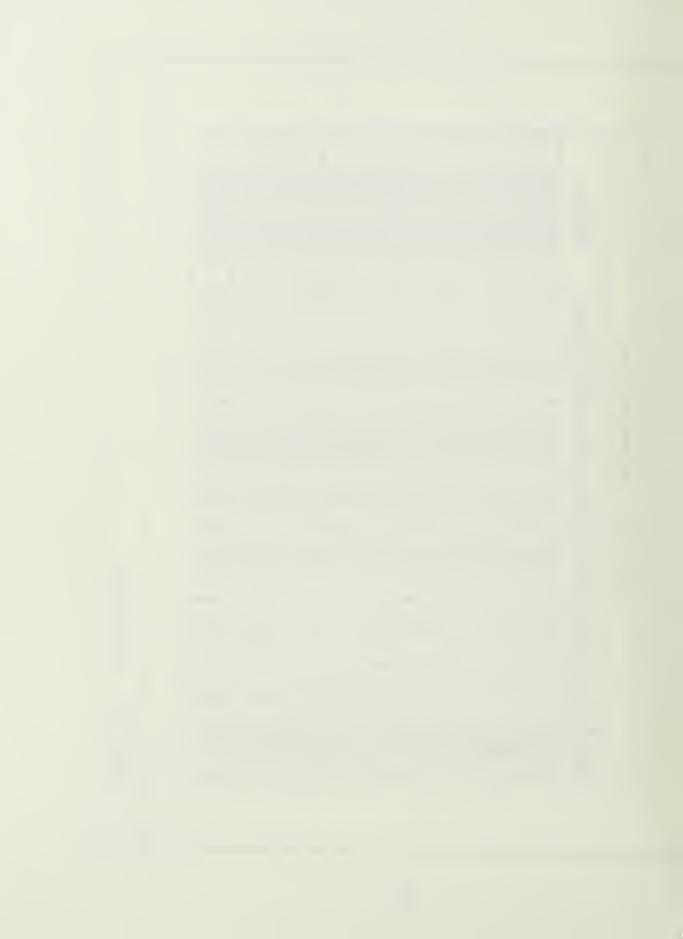
							,						,		,						
٠	Boundary Condition	BOLTED (tank)	EOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)															
(two)"	Setup Data No.	=	7	J	3	=	7	3	<b>3</b>	7	J	7	7	7	7	7	3	3	=	<b>=</b>	7
Modal (t	remp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	14	14	14	13	12	Ξ
"Steve's Mod	Input	Random																			
	Band Width	50	50	50	50	50	20	50	50	50	50	50	50	50	50	20	50	20	20	20	50
Disk Label	Center Prequency	6880	6880	6880	6880	6880	6880	6880	6880	6880	6880	6 8 80	6880	6880	6880	6880	6 8 80	6880	6880	6880	6880
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	-	2	3	3	5	9	7	80	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk Record	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	1361	137	138	139	140

. Table II. (Continued)



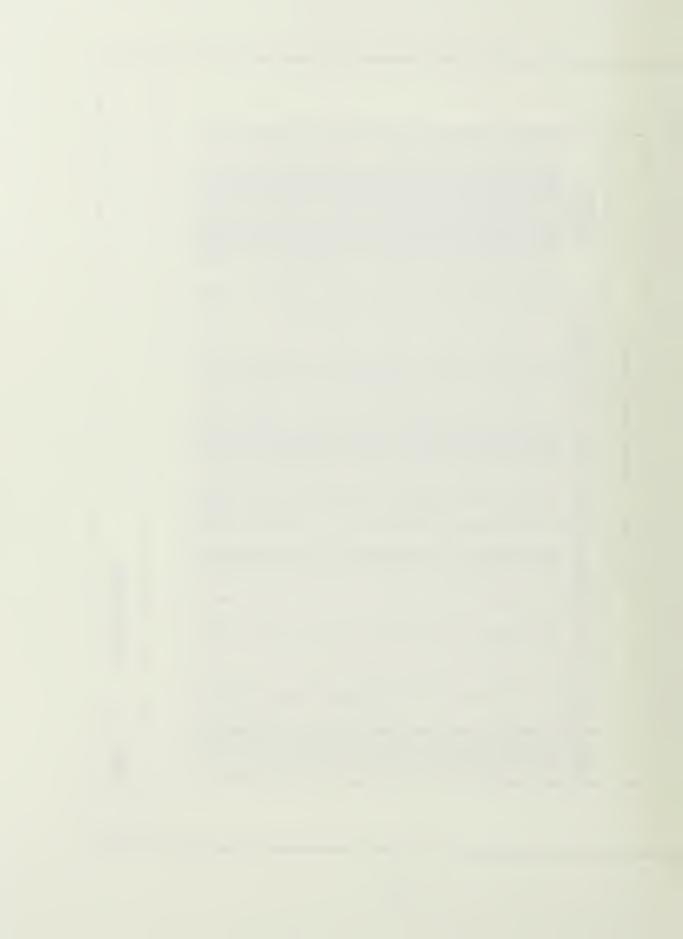
		<b>,</b>	,							,											
•	Boundary Condition	BOLTED (tank)	BOLTED (tank)	FOLTED (tank)	BOLTED (tank)																
(two)"	Setup Data No.	3	<b>=</b>	=	3	3	3	7	3	3	<b></b>	<b>=</b>	3	#	đ	Þ	3	ŧ	3	7	Þ
Modal (t	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	ħ1	71	14	14	13	12	=
Steve's	Input	Random																			
	Band Width	20	50	50	5.0	50	50	50	50	50	50	50	50	20	50	50	50	50	50	50	50
Disk Label	Center Fraguency	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152	8152
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	3	5	9	7	8	6	10	1-1	12	13	3.5	15	16	17	18	19	2.0
	Disk	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160

Table II. (Continued)



	Boundary Condition	BOLTED (tank)	BOLTED (tank)	BOLTED (+ank)	BOLTED (tank)	EOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	POLTED (tank)	BOLTED (tank)										
(two)"	Setup Data No.	3	#	3	7	3	3	7	3	3	#	7	3	7	Þ	3	7	<b>3</b>	3	3	Þ
Modal (t	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	14	70	14	13	12	1-
Steve's	Input	Random																			
	Band Width	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	20	50
Disk Label	Center Fraguency	0198	0198	0198	0198	0498	0198	0198	0198	0498	0498	0198	0198	0198	8640	0498	0 19 9 8	0198	0198	0198	8640
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	-	2	3	3	5	9	7	8	6	10	11	12	13	7	15	16	11	18	19	2.0
	Disk	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180

Table II. (Ccutinued)



													,	,						,	,
-	Boundary Condition	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLT ED (tank)	BOLTED (tank)														
"(0)	Setup Data No.	3	7	7	3	3	3	=	3	=	Þ	=	7	7	7	3	ti	Ū	3	3	3
Modal (two)"	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	14	14	14	13	12	-
"Steve's Mod	Input	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random
	Band Width	50	50	50	50	50	50	50	50	50	50	20	50	50	50	50	20	50	50	50	50
Disk Label	Center Freguency	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116	9116
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	7	5	9	7	8	6	10	11	12	13	74	15	16	17	18	19	20
	Disk	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200

Table II. (Continued)



		-													_				,		
,	Boundary Condition	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	EOLTED (tank)	BOLTED (tank)	BOLTED (tank)	EOLTED (tank)	EOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	EOLTED (tank)	BOLTED (tank)						
ro) "	Setup Data No.	3	7	3	<b>a</b>	7	<b>\$</b>	ħ	<b>=</b>	7	\$	7	3	7	⇉	7	3	3	3	3	3
Modal (two)"	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	17	14	14	13	12	=
Steve's	Input	Random																			
1 : "	Band Width	50	50	50	50	50	50	50	5.0	50	50	50	5.0	50	20	50	20	5.0	50	20	50
Disk Label	Center Frequency	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136	11136
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	7	5	9	7	8	6	10	-	12	13	7.	15	16	17	18	19	2.0
	Disk Record	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220

Table II. (Continued)



				-		_		_	_			-	_	-	_				_		
	Boundary	BOLTED (tank)	BOLTED (tank)	EOLTED (tank)	POLTED (tank)	EOLTED (tank)	BOLTED (tank)	FOLTED (tank)	BOLTED (tank)	FOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	BOLTED (tank)	FOLTED (tank)	EOLTED (tank)					
"(0)	Setup Data No.	<b>=</b>	3	7	7	7	3	3	3	<b>=</b>	7	7	3	3	3	#	3	3	7	3	3
lal (tı	Temp.	12	12	12	12	10	6	8	7	10	10	10	13	14	14	14	14	14	13	12	1-
"Steve's Hodal (two)"	Excitation	Random	Bandom	Random																	
	Pand Width	20	50	50	20	50	50	50	50	50	50	20	50	50	50	50	50	50	50	20	50
Disk Label	Center Frequency	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217	12217
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	3	5	9	7	8	6	10	1-1	12	13	14	15	16	17	18	19	2.0
	Disk Record	221	222	223	224	225	226	227	228	229	230	231	232	233	2.34	235	236	237	238	239	240

Table II. (Continued)



	Boundary Condition	CHORD (tank)	CHORD (tank)	CHORD (tank)	CHOBD (tank)	CHORD (tank)	CHORD (tank)	CHORD (tank)	CHOED (tank)	CHORD (tank)	CHORD (tank)	CHOED (tank)	CHORD (tank)	CHOED (tank)	CHORD (tank)	CHOED (tank)	CHORD (tank)				
10)11	Setup Data No.	7	7	7	=	Þ	7	#	7	7	3	7	#	7	3	#	<b>⇒</b>	ħ	3	7	Ħ
Modal (two)"	Temp.	13	14	14	13		7	9	5	3	11		12	12	12	12	12	10	8	9	=
"Steve's Mod	Input	Random																			
	Pand Width	50	50	50	5.0	50	50	50	5.0	50	50	50	50	50	50	5.0	50	50	50	50	50
Disk Label	Center Frequency	421	421	421	421	421	421	421	421	421	4.21	421	421	421	421	421	421	421	421	421	4 21
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	7	5	9	7	- 8	6	10	1-1-	12	13	71	15	16	17	18	19	2.0
	Disk	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	2 (8	269	270

Table III. Experimental data - CHOBE (tank)



		_																			
	Boundary Condition	CHORD (tank)																			
(two)"	Setup Data No.	7	#	7	3	オ	Ħ	#	3	3	3	7	3	7	<b>=</b>	3	3	7	3	#	7
Modal (t	Temp.	13	14	14	13	11	7	9	5	=	11	11	12	12	12	12	12	10	8	9	11
Steve's	Input	Random																			
1: "	Band Width	20	50	50	20	50	20	20	20	50	20	9.0	50	50	20	9.0	50	20	20	20	50
Disk Label	Center Frequency	8 50	8 50	8 50	8 50	8 50	8 50	850	8 50	8 50	8 50	850	8 50	8 50	8 50	8 50	8 50	8 50	8 50	850	8 50
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk	271	272	273	274	275	276	277	2.78	279	280	281	282	283	284	285	286	287	288	289	290

Table III. (Continued)



•	Boundary Condition	CHORD (tank)																			
(two)"	Setup Data No.	7	7	7	3	3	3	7	7	3	=	7	3	7	3	=	⇒	3	7	3	7
	Temp.	13	14	14	13	11	7	9	5	7		-	12	12	12	12	12	10	89	9	=
Steve's Modal	Input	Random																			
1 : "	Band Width	50	50	50	50	5.0	5.0	5.0	5.0	50	5.0	5.0	50	50	5.0	5.0	20	5.0	5.0	50	50
Disk Label	Center Frequency	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20	9 20
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	-	2	3	7	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20
	Disk	291	292	293	294	295	296	297	298	299	3 00	301	302	303	304	305	306	307	308	3 09	3 10

Table III. (Continued)



		1	_					-			_	-	1		_						
-	Boundary Condition	CHORD (tank)																			
,, (0)	Setup Data No.	3	7	ħ	7	7	7	ħ	7	7	7	3	7	7	7	7	3	7	ħ	7	3
lal (tw	Temp.	13	14	14	13	-	7	9	5	#		11	12	12	12	12	12	10	θ	9	=
Steve's Modal (two)"	Input	Random																			
.1: "	Pand	50	50	50	20	50	50	50	50	50	50	50	50	50	50	5.0	50	50	50	50	50
Disk Label	Center Frequency	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261	1261
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	7	5	9	7	8	6	10	1.1	12	13	14	15	16	17	18	19	2.0
	Disk Record	311	312	313	3.14	315	316	317	318	319	320	321	322	323	3.24	325	326	327	328	329	330

Table III. (Continued)



																					,
	Boundary Condition	CHORD (tank)																			
(two)"	Setup Data No.	7	Þ	7	<b>3</b>	ħ	ħ	3	<b>3</b>	ħ	₹	3	₹	7	ħ	ħ	#	⇉	ħ	7	<b>寸</b>
Modal (t	Temp.	13	14	14	13	11	7	9	5	ħ	11	11	12	12	12	12	12	10	8	9	=
"Steve's Mod	Input	Random																			
	Band	20	50	5.0	20	20	20	20	50	20	20	20	50	20	50	20	50	50	20	20	50
Disk Label	Center Frequency	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258	3258
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	80	6	10	1-	12	13	14	15	16	17	18	19	2.0
	Disk	331	332	333	334	335	336	337	338	339	340	34.1	342	343	344	345	346	347	348	349	350

Table III. (Continued)



			,											_							
	Boun dary Condition	CHORD (tank)	CHORD (tank)	CHORD (tank)	CHORD (tank)	CHOFD (tank)	CHORD (tank)	CHOBD (tank)	CHORD (tank)	CHOFD (tank)	CHORD (tank)										
(0)	Setup Data No.	3	コ	3	#	<b>3</b>	3	3	#	3	3	3	3	J	3	コ	3	3	#	ā	3
la 1 (t)	Temp.	13	14	14	13	=	7	9	5	<b>3</b>			12	12	12	12	12	10	8	9	=
"Steve's Modal (two)"	Input	Random	Random	Random	Handom	Random															
	Band Width	50	50	50	50	20	50	50	50	50	50	50	50	50	50	50	50	50	50	20	50
Disk Label	Center Prequency	5030	5030	5030	50 10	5030	50 30	50 30	5030	50 30	5030	5030	50 30	5030	5030	5030	50 30	50 10	50 30	5030	5030
	Nurber	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	3	5	19	7	80	6	0.	-	12	13	7	2.0	16	17	18	9	15
	Disk	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370

Table III. (Continued)



			,	,				,			,	,				,					,
	Boundary	CHORD (tank)																			
ro)"	Setup Data No.	3	7	3	7	ħ	Ť	ŧ	t	7	t	3	<b>3</b>	7	t	7	3	7	ħ	Ť	ħ
la 1 (tı	Temp.	13	14	14	13	11	7	9	5	7	11	11	12	12	12	12	12	10	8	9	=
"Steve's Hodal (two)"	Input	Random																			
	Band Width	50	50	50	50	20	20	50	20	50	20	50	20	50	50	50	50	50	50	50	50
Disk Label	Center Frequency	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100	7100
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	3	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	3 88	389	390

Table III. (Continued)



	Boundary Condition	CHORD (tank)																			
(two)"	Setup Data No.	7	3	3	3	3	3	3	3	3	3	7	3	<b>3</b>	3	3	3	3	3	3	3
Hodal (to	Temp.	13	14	14	13	-1	7	9	S	3	11	=	12	12	12	12	12	10	8	9	=
"Steve's Mod	Input	Random																			
	Band Width	50	5.0	5.0	50	50	50	5.0	50	50	50	50	50	50	20	50	50	50	20	50	50
Disk Label	Center Freguency	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221	8221
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10.	10	10	10	10	10	10	10
	Grid Location	-	2	3	7	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20
	Disk	391	392	393	3.94	395	396	397	398	399	00 1	401	4 02	4 03	10 th	4 05	90 h	407	4 0 B	60 h	4 10

Table III. (Continued)



		,				,							,	,		,			_		
	Boundary Condition	CHORD (tank) .	CHORD (tank)	CHOBD (tank)	CHORD (tank)																
"(0)	Setup Data No.	3	3	#	7	77	3	3	7	3	7	3	3	=	3	3	7	3	7	3	#
Hodal (two)"	Temp.	13	14	14	13	-1	7	9	5	3	11	=	12	12	12	12	12	10	8	9	=
Ste ve's	Input	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random						
1 : "	Band Width	50	50	50	50	50	5.0	50	50	50	5.0	50	50	50	50	50	50	50	50	50	50
Disk Label	Center Frequency	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447	8447
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	-	2	3	7	5	9	7	8	6	10	1.1	12	13	7.	15	16	17	18	19	2.0
	Disk	411	412	413	414	415	4 16	417	418	419	4 20	421	422	423	424	4 25	426	427	428	429	430

Table III. (Continued)



		,	,			1		_							,						
	Boundary	CHORD (tank)																			
(two)"	Setup Data No.	7	7	#	#	7	#	3	3	3	3	7	7	3	<b>=</b>	7	3	3	3	7	3
Hodal (t	Temp.	13	14	14	13		7	9	5	7	-	11	12	12	12	12	12	10	8	9	=
Steve's	Input	Random																			
1 : H	Band Width	20	20	20	20	50	20	50	20	50	5.0	20	20	50	50	20	20	20	5.0	50	50
Disk Label	Center Frequency	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065	9065
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	3	5	9	7	9	6	10		1.2	13	77	15	16	17	18	19	2.0
	Disk	431	432	433	434	435	436	437	438	4 39	044	441	442	6443	717	445	9111	L 11 11	8448	611	4 50

Table III. (Continued)



					,													,			
	Boundary Condition	CHORD (tank)	CHORD (tank)	CHOBD (tank)	CHORD (tank)	CHORD (tank)	CHORD (tank)	CHOBD (tank)	CHORD (tank)												
,, (o,	Setup Data No.	7	7	7	7	3	=	7	7	7	7	3	3	7	3	7	7	7	7	7	2
Hodal (two)"	remp.	13	14	14	13	11	7	9	5	7	11		12	12	12	12	12	10	8	9	=
Steve's	Input	Random																			
	Band	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
Disk Label	Center Preguency	8996	8996	9996	8996	8996	8996	9996	8996	8996	9996	9996	9996	9996	8996	8996	8996	9996	9668	8996	9996
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	7	5	9	7	8	6	10	11	12	13	77	15	16	17	18	19	2.0
	Disk	451	452	453	h5 h	4 55	4 56	457	4 58	459	03 17	194	4 62	463	464	465	99 17	467	4 68	6917	470_

Table III. (Continued)



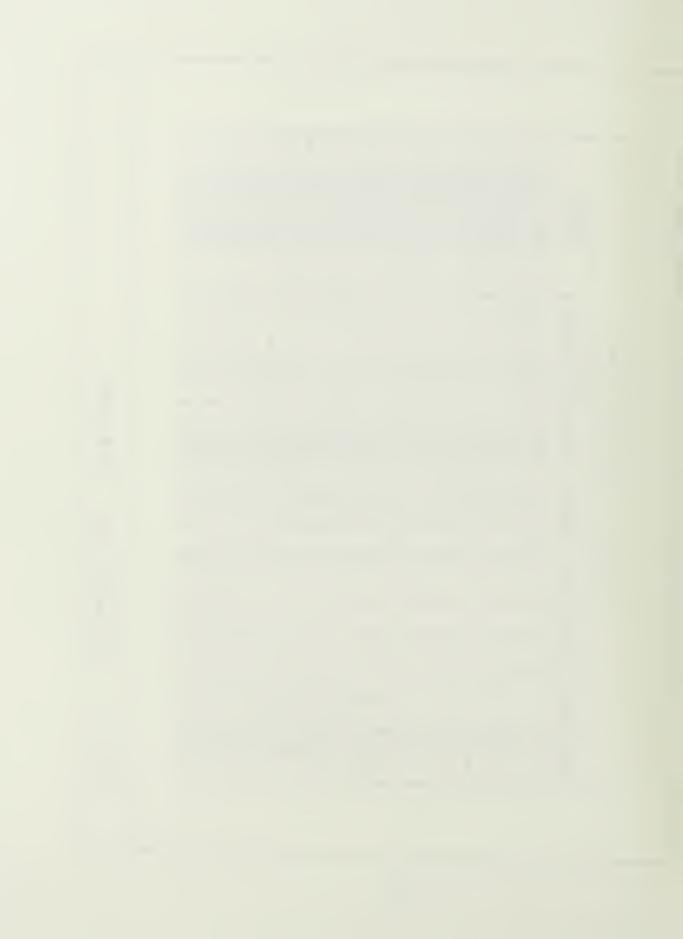
•	Boundary Condition	CHORD (tank)	CHOED (tank)	CHORD (tank)																	
" (0)	Setup Data No.	3	3	3	7	7	3	3	3	3	コ	3	Þ	<b>=</b>	3	<b>a</b>	#	3	<b>a</b>	3	<b>=</b>
Modal (two)"	Temp.	13	14	14	13	11	7	9	5	3	11	11	12	12	12	12	12	10	8	9	=
"Steve's Mod	Input	Random																			
••	Pand Width	50	50	50	50	50	5.0	50	20	50	20	50	20	50	5.0	50	50	5.0	20	50	50
Disk Label	Center Freguency	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512	11512
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	-	2	3	7	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20
	Disk	471	472	473	71.71	475	476	477	4 78	479	480	481	4 82	483	484	485	486	4 87	14 88	489	n 90

Table III. (Continued)



											,		,		,						
	Boundary Condition	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)	POAN (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)
(three) "	Setup Data No.	3	3	3	3	37	3	3	3	#	3	#	3	7	3	3	3	#	3	3	3
1	remp.	=	14	15	16	16	16	16	15	7	9	6	10	13	14	14	14	14	13	13	12
"Steve's Modal	Input	Random	Handom	Random																	
	Band Width	50	50	5.0	50	50	50	5.0	5.0	50	5.0	50	5.0	50	50	50	5.0	50	5.0	5.0	50
Disk Label	Center Frequency	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20	4 20
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	3	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2 0
	Disk	-	2	3	3	2	9	7	θ	6	10	=	12	13	14	15	16	17	18	19	20

Table IV. Experimental data - FOAB (ends)



	Boundary Condition	FOAM (ends)	POAM (ends)	FOAM (ends)																	
.ee) "	Setup Data No.	3	ħ	i d	ħ	ħ	ħ	7	3	Þ	3	Ţ,	7	7	7	3	Ŧ	3	ħ	7	7
(three)	Temp.	14	14	15	16	16	16	16	15	7	8	6	10	13	14	14	14	14	13	13	12
"Steve's Modal	Input	Random																			
	Band Width	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
Disk Label	Center Frequency	850	850	8 50	8 50	8 50	8 50	8 50	8 50	8 50	8 50	850	8 50	850	850	8 50	8 50	8 50	850	850	850
	Number Averages	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	7	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40

Table IV. (Continued)



				,	<b>,</b>									_							
	Boundary Condition	FOAM (ends)																			
(three)"	Setup Data No.	7	3	3	ŧ	3	3	3	3	3	3	3	7	3	Þ	<b>3</b>	3	3	Þ	3	7
	Temp.	=	14	15	16	16	16	16	15	7	8	6	10	13	14	=	14	10	13	13	12
"Steve's Modal	Input	Random																			
	Band Width	50	50	50	5.0	5.0	20	50	50	50	5.0	20	50	50	50	50	50	50	50	50	50
Disk Label	Center Frequency	1070	10 70	1070	10 70	10 70	10 70	1070	10 70	1070	10 70	1070	10 70		10 70	10 70	10 70	1070	1070	1070	10 70
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	7	5	9	7	8	6	10	1-1	12	13	77	15	16	17	18	19	2.0
	Disk	4.1	42	43	7.5	45	911	47	84	611	20	51	52	53	54	55	95	57	58	- 59	09

Table IV. (Continued)



	Boundary Condition	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)					
(three) "	Setup Data No.	Þ	Ħ	ħ	<b>3</b>	77	7	đ	#	ŧ	<b>3</b>	ħ	3	ħ	ħ	3	đ	7	7	ħ	ħ
1 (thr	Temp.	14	14	15	16	16	16	16	15	7	8	6	10	13	14	14	14	7	13	13	12
"Steve's Modal	Input	Random																			
	Band Width	50	50	50	50	20	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50
Disk Label	Center Frequency	36 70	36 70	36 70	3670	36 70	3670	36 70	36 70	36 70	3670	36 70	3670	36 70	3670	3670	3670	36 70	3670	36 70	3670
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	7	5	9	7	8	6	10		12	13	14	15	16	17	18	19	2.0
	Disk	61	62	63	64	65	99	19	68	69	70	71	72	73	74	75	76	77	78	79	80

Table IV. (Continued)



	Boundary Condition	FOAM (ends)	FOAM (ends)	FOAM (ends)	· POAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)													
ree) "	Setup Data No.	3	3	3	#	#	3	3	i i	3	Ħ	<b>3</b>	3	Ħ	র	3	3	3	3	3	3
1 (three)	Temp.	14	14	15	16	16	16	16	15	7	8	6	10	13	14	14	14	14	13	13	12
"Steve's Modal	Input Excitation	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random	Random
	Band Width	20	50	50	50	50	50	50	50	50	50	50	20	50	50	50	50	50	5.0	50	50
Disk Label	Center Frequency	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365	5365
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	80	6	10	11	12	13	77	15	16	17	18	19	2.0
	Disk	8.1	82	83	84	85	98	-87	-88	89	96	91	92	93	16	95	96	97	- 86	66	100

Table IV. (Continued)



																		_			,
	Boundary Condition	FOAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	POAN (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)									
" (əə:	Setup Data No.	7	7	ħ	ħ	ħ	ħ	7	7	7	ħ	ħ	מ	ז	ħ	ħ	=	3	7	ħ	#
l (thr	Temp.	14	14	15	16	16	16	16	15	7	8	6	10	13	14	14	7	7	13	13	12
"Steve's Modal (three)"	Input	Random																			
	Band Width	50	20	50	20	50	20	20	50	50	50	50	50	50	50	20	50	20	50	20	20
Disk Label	Center Prequency	7090	7090	7090	7090	7090	7 0 9 0	7090	7090	7090	7090	1090	7090	7090	7090	7090	7090	7 0 90	7090	7090	7090
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	1	2	3	3	5	9	7	8	6	10		12	13	14	15	16	17	18	19	2 0
	Disk	101	102	103	104	105	106	107	108	109	100	111	112	113	114	115	116	117	118	119	120

Table IV. (Continued)



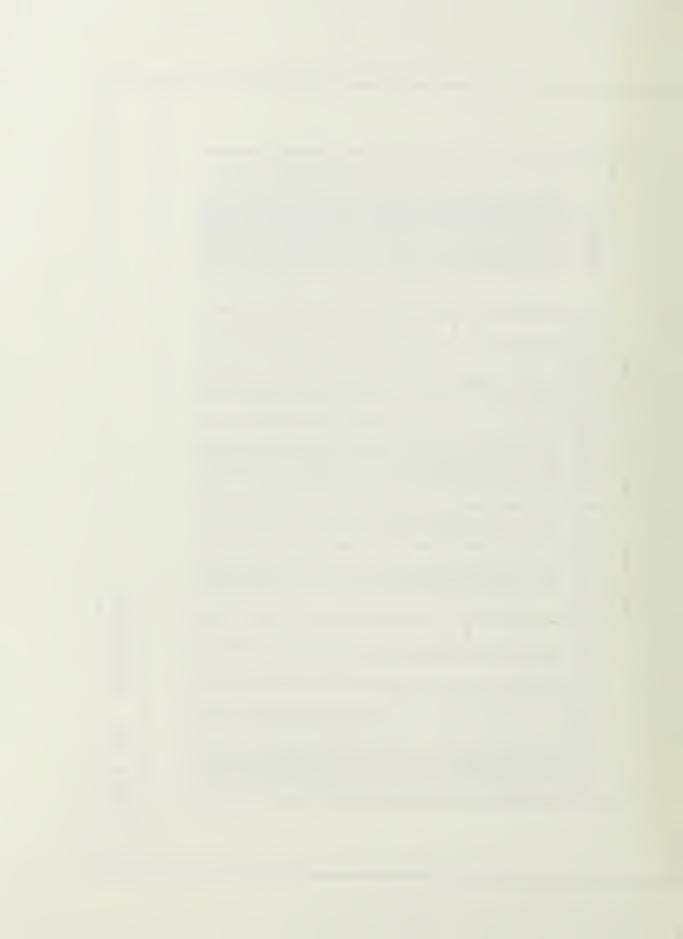
				_						_	-										
-	Boundary Condition	FOAM (ends)	POAM (ends)	FOAM (ends)	FOAM (ends)	FOAM (ends)	POAM (ends)	FOAM (ends)													
ree) "	Setup Data Ro.	7	7	ħ	7	7	3	=	3	3	3	3	7	<b>=</b>	7	7	7	27	3	3	3
Nodal (three)	Temp.	14	14	15	16	16	16	16	15	7	8	6	10	13	14	14	14	14	13	13	12
"Steve's Mod	Input	Random																			
	Band Width	50	5.0	50	50	50	50	50	50	50	50	50	50	50	50	5.0	50	50	50	50	50
Disk Label	Center Prequency	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8220	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8 2 20	8220	8 2 20	8 2 20
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid Location	-	2	3	7	5	9	7	8	6	10		12	13	14	15	16	17	18	19	2 0
	Disk	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140

Table IV. (Continued)



		,						,									,				
	Boundary Condition	FOAM (ends)																			
(three)"	Setup Data No.	7	7	7	7	7	7	7	7	7	ħ	7	3	3	7	3	7	#	7	3	3
i i	Temp.	14	14	15	16	16	16	16	15	7	8	6	10	13	14	14	14	14	13	13	12
"Steve's Modal	Input	Random																			
	Band Width	50	50	9.0	50	50	20	50	50	50	50	50	20	50	50	50	50	50	50	50	50
Disk Label	Center Freguency	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540	8540
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	3	5	9	7	8	6	10	11	12	13	14	15	16	17	18	19	2.0
	Disk	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160

Table IV. (Continued)



	la ry It ion	(ends)	(euds)	(en ds)																	
	Bounda: Condit	FOAM	FOAM	FOAM	FOAM	FOAM	FOAM	POAM	POAM	FOAM	FOAM	FOAM	FO AM	FOAM	POAM						
(three)"	Setup Data No.	3	7	ħ	Ħ	ħ	⇉	3	3	ħ	3	7	7	ব	7	ħ	ħ	#	3	ħ	ħ
į i	Temp.	14	14	15	16	16	16	16	15	7	8	6	10	13	14	14	14	14	13	13	12
teve's Hodal	Input	Random																			
1 : "S	Band Width	50	50	50	50	50	50	50	50	50	50	5.0	50	5.0	5.0	50	50	2.0	20	20	50
Disk Labe	Center Frequency	9065	9062	9065	9062	9062	9062	9062	10	9062	9065	9062	906	9065	9062	9062	9062	9065	9062	9062	9065
	Number	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10
	Grid	1	2	3	7	5	9	7	8	6	10	1-1	12	13	14	15	16	17	18	19	2.0
	Disk	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180

Table IV. (Continued)



Table IV. (Continued)



Table IV. (Continued)

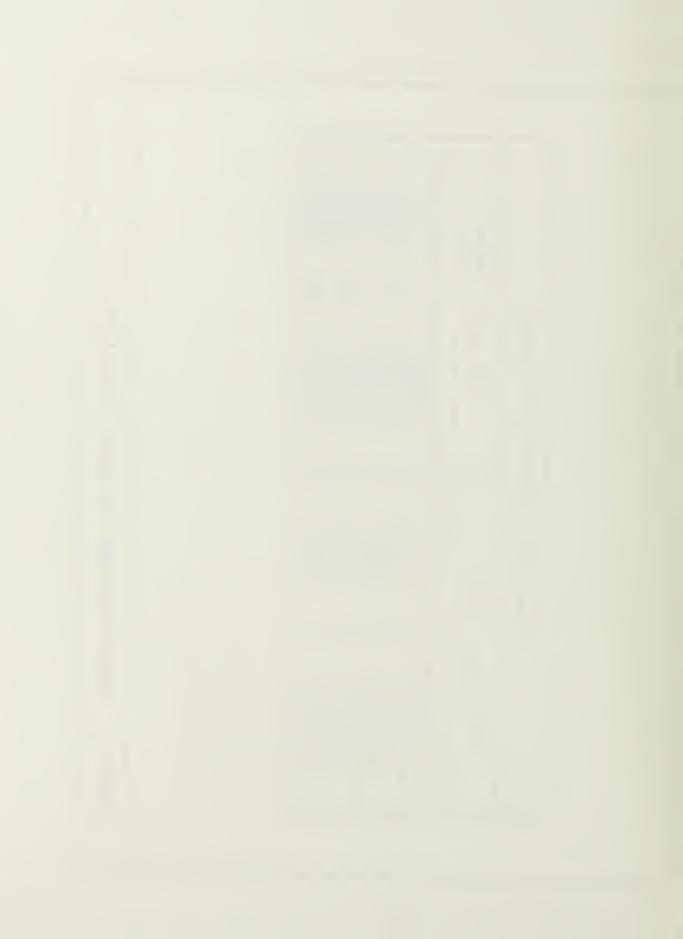


Table IV. (Continued)



V	VERAGE MODAL FRECI	AVERAGE MODAL FREÇUENCIES AND DAMPING	
FOAM (Fad) - Impact	- Impact	FOAM (pad) - Random	- Randon
Natural Freguency (Hertz)	Damfing Factor	Natural Frequency (Hertz)	Damping Factor
2276.8271	0.1068	2277.6323	0.1121
2396.0981	0.1021	2397.2002	0.1091
2629.7700	0.0920	2637.3799	0.0967
3253.0483	0.0954	3248.5352	0.0954
4569.0020	0.0740	4572.2363	0.0833
		T	

Rardem Cemparison Results of Impact vs. Table V.

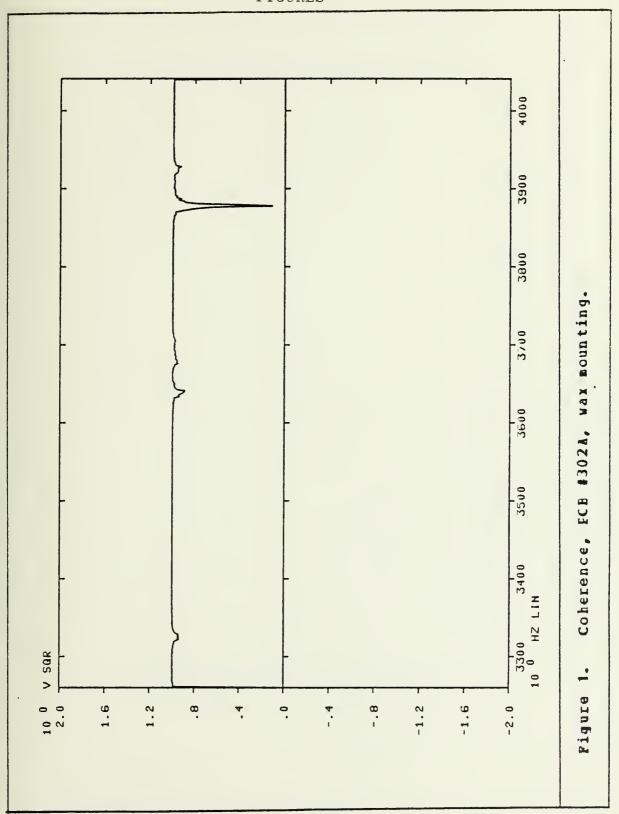


r			,											
	(spue)	Damping Factor	0.1873	0.0659	0.0793	0.0703	0.0477	0.0336	0.0542	0.1410	0.0938	0.0232	0.0361	0.0372
	FOAM	Natural Preguency (Hertz)	422.686	851.784	1072.964	3675.915	5366.419	7093.827	8218.264	8538.205	9062.781	9265.479	10655.359	12205.299
DAMPING	(tank)	Damping Factor (%)	0.3496	0.2027	0.1345	0.1221	0.1886	0.0360	0.0339	0.0377	0.1036	0.1697	0.0920	0.0155
FEEQUENCIES AND	CHORD (	Natural Frequency (Hertz)	422.641	851.768	918.969	1264.705	3257.515	5029.354	7098.269	8222.945	8446.225	9064.914	9669.775	11510.981
MODAL FEEQUE	(tank)	Damping Factor (%)	0.5045	0.2540	0.1224	0.0550	0.0405	0.1115	0.0836	0.0491	0.0603	0.0782	0.0591	0.0630
AVERAGE MC	BOLTED	Natural Freguency (Hertz)	277.590	621.142	1503.937	3188.707	4251.911	5613.253	6879.277	8159.321	8633.895	9099.016	11124.402	12212.816
	(pad)	Damping Factor (%)	0.3030	1	0.1284	0.1230	0.1156	0		- 2	0.1089	η//0.0	0	0.0697
	FOAM (	Natural Freguency (Hertz)	420.060	1262.487	2605.433	3669.019	4702.096	6093.651	7169.448	53.5	9659.422	10660.674	11150.273	12200.746

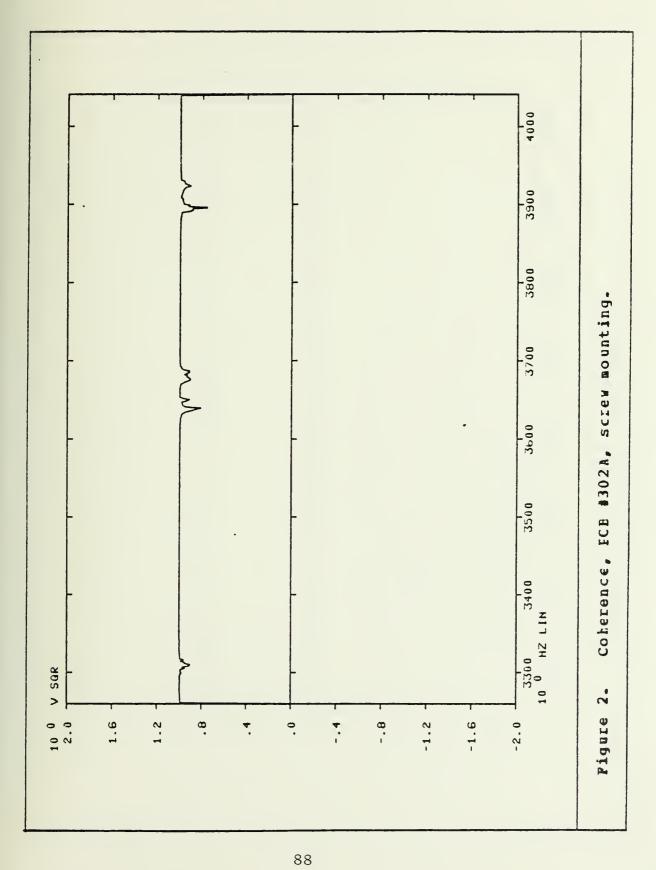
Experimental Summary of Camping Characteristics Table VI.



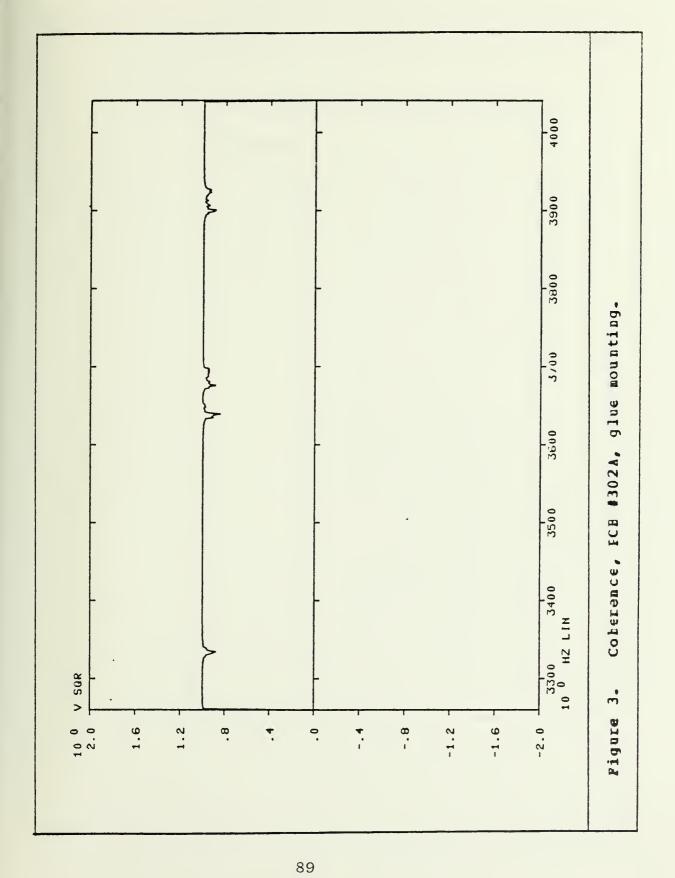
## FIGURES



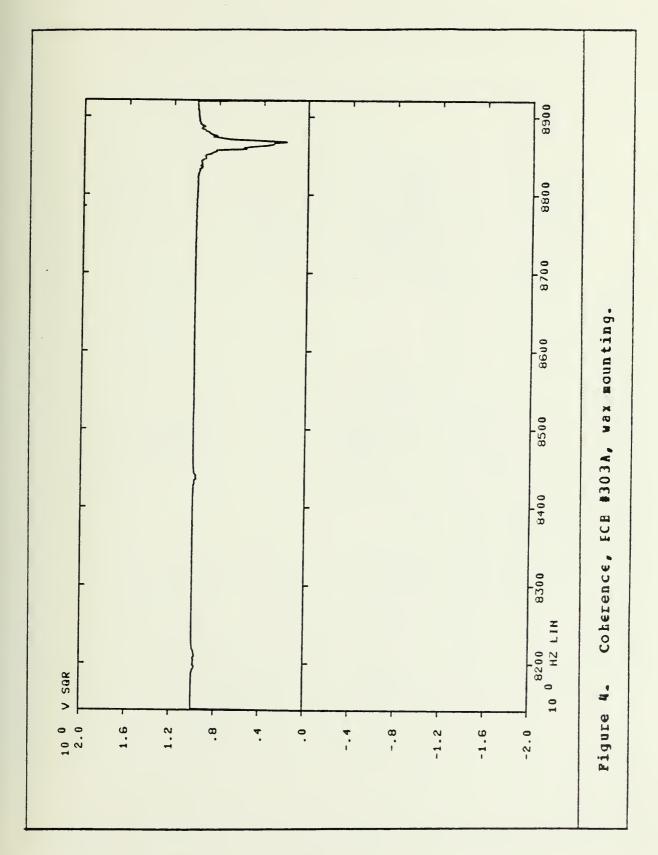




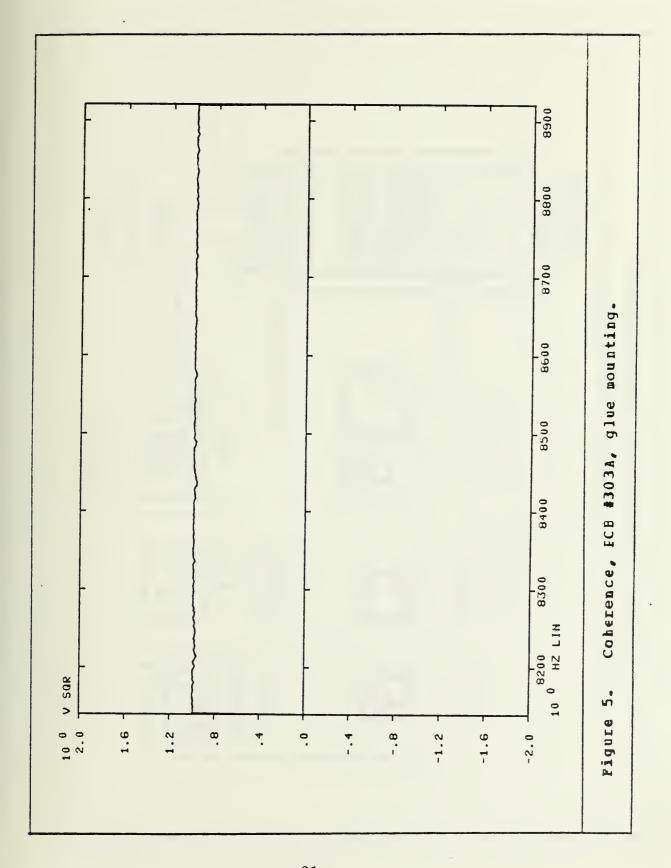




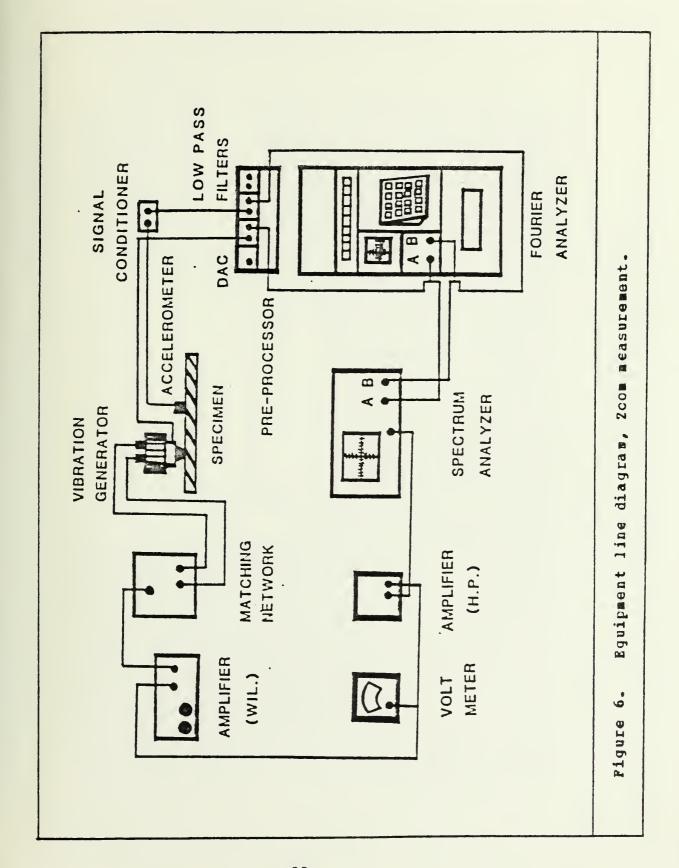




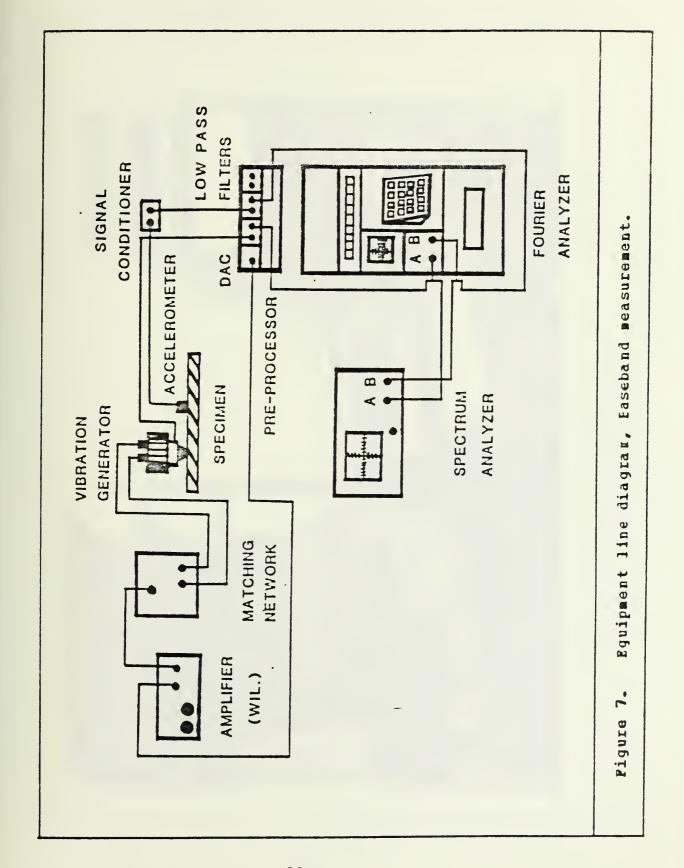








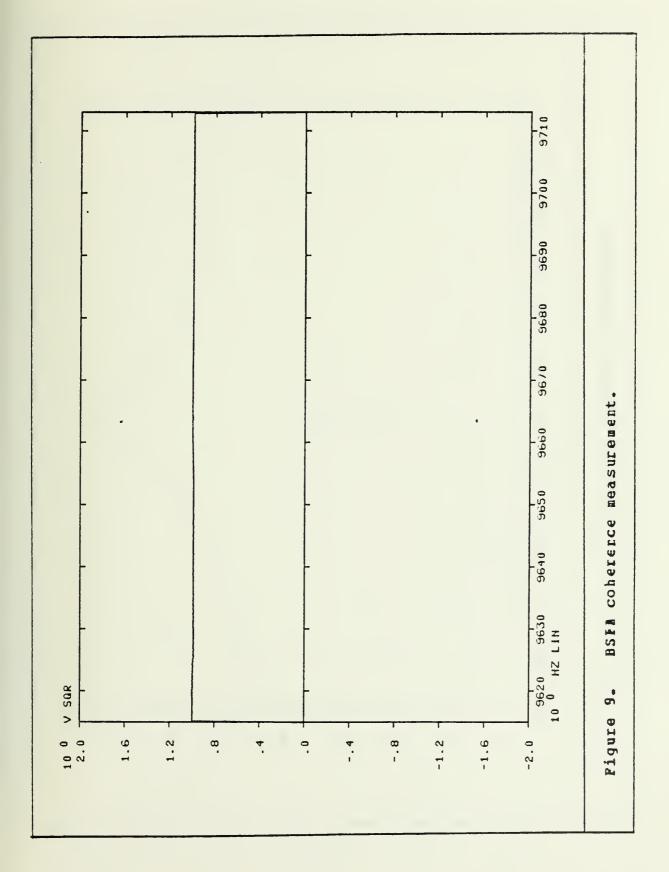




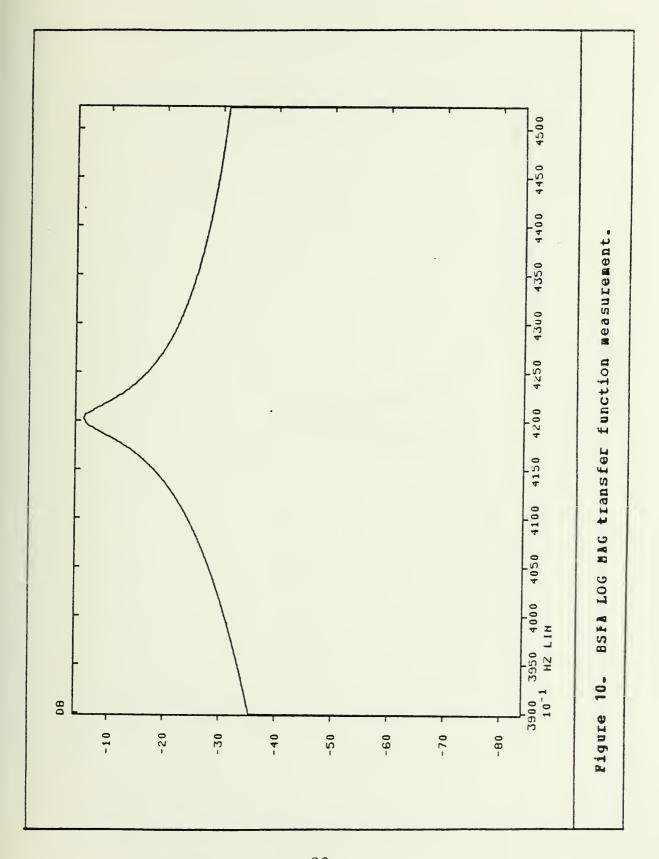


Pigure 8. NPS Modal Aralysis Laboratory.

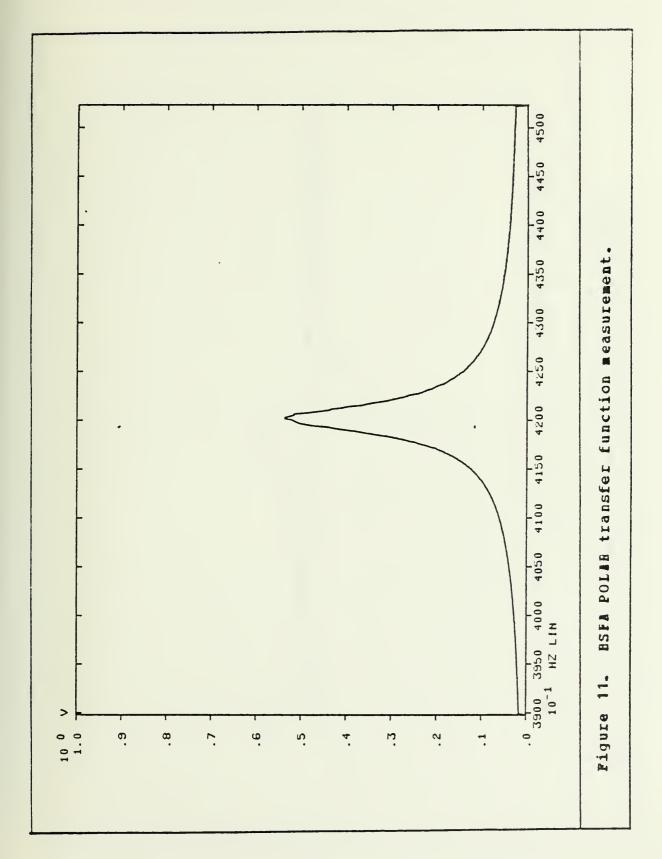




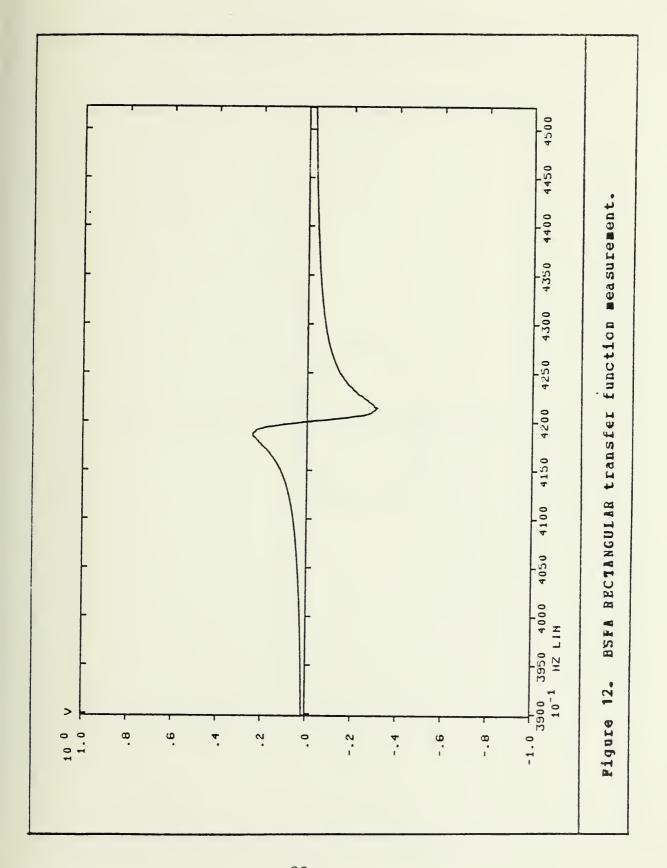




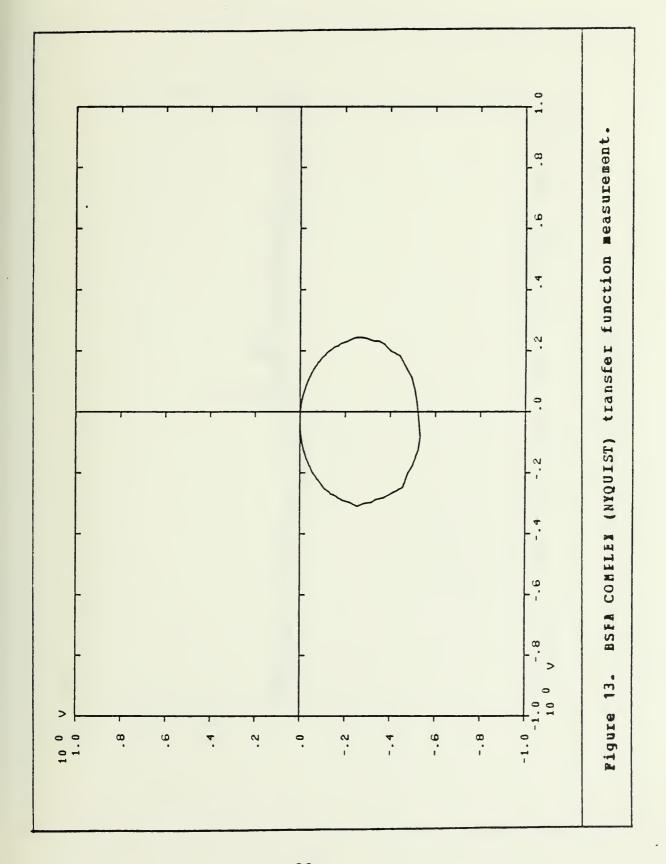




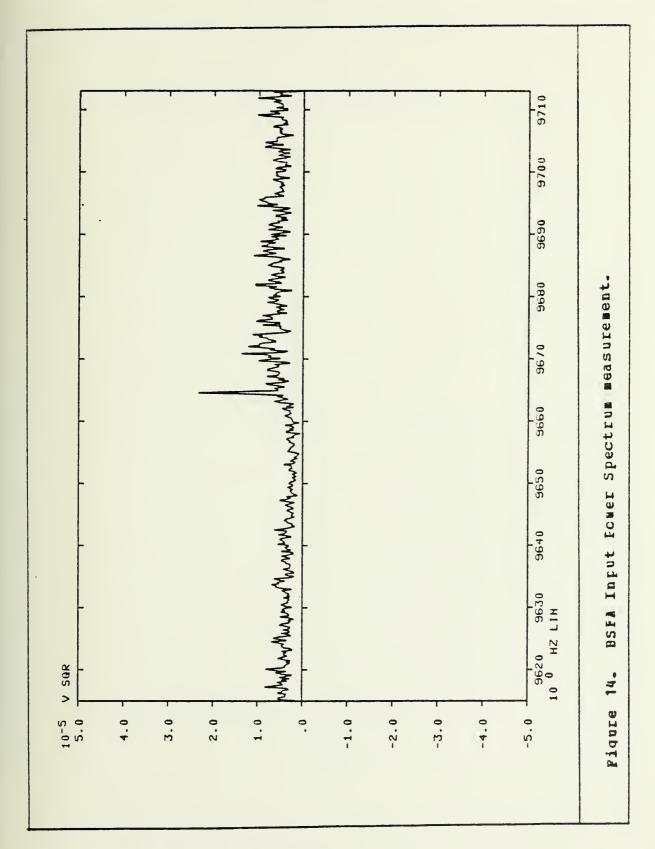


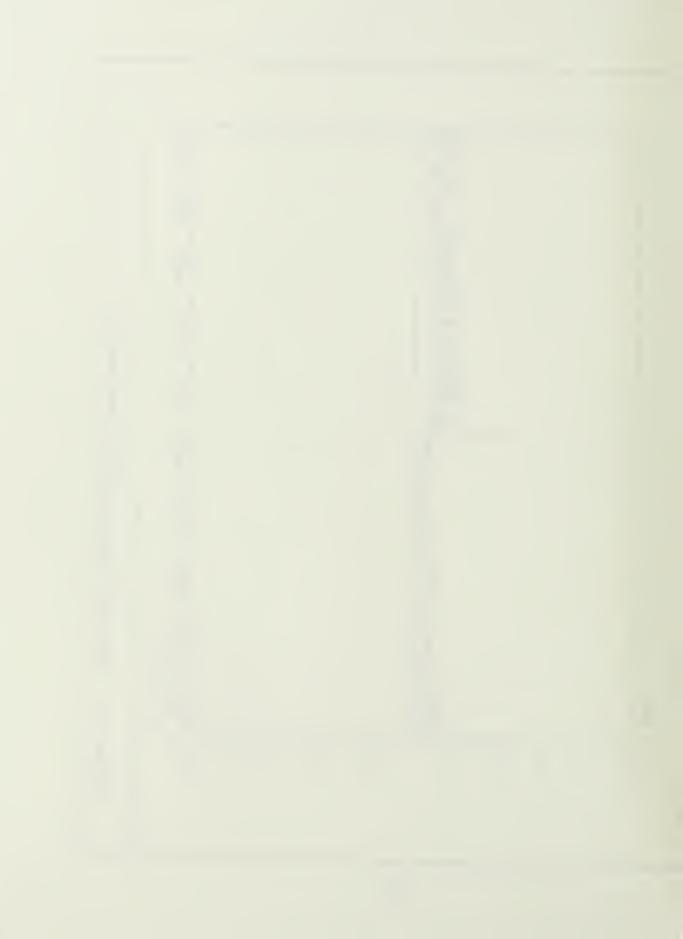


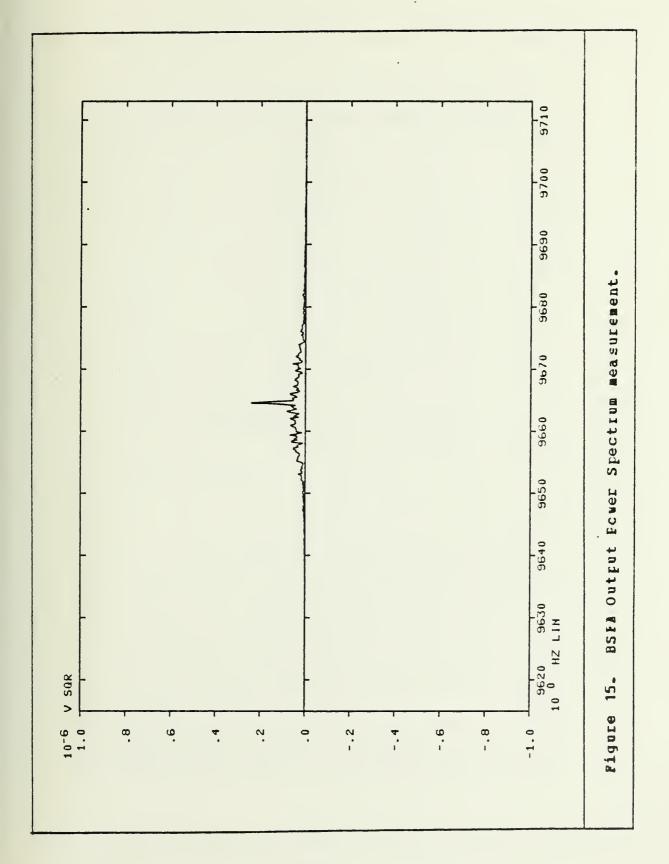




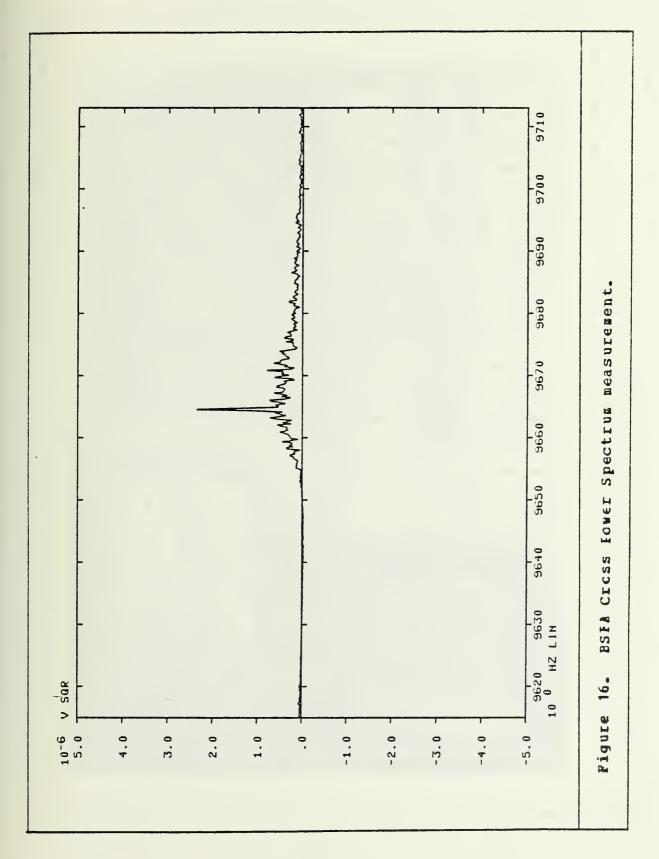




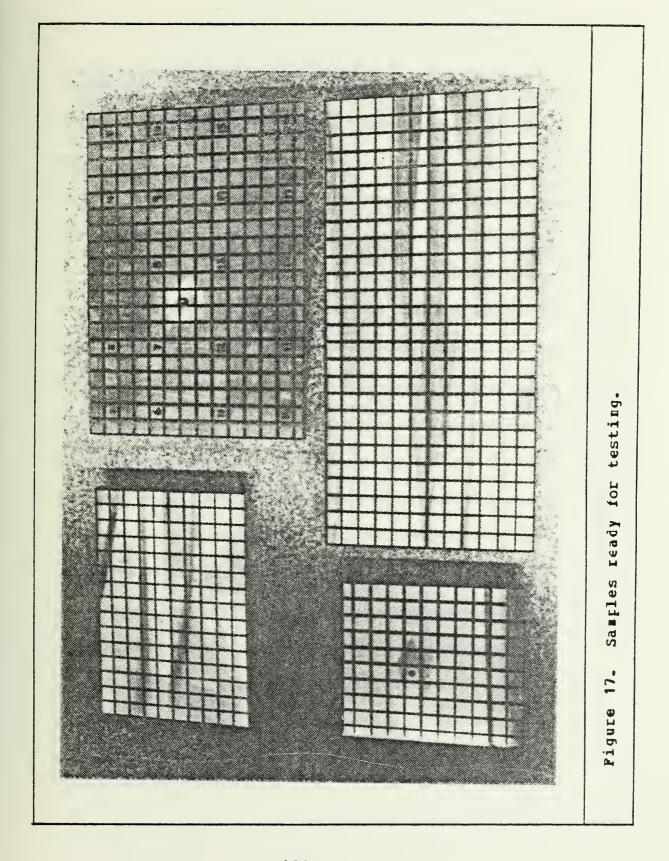




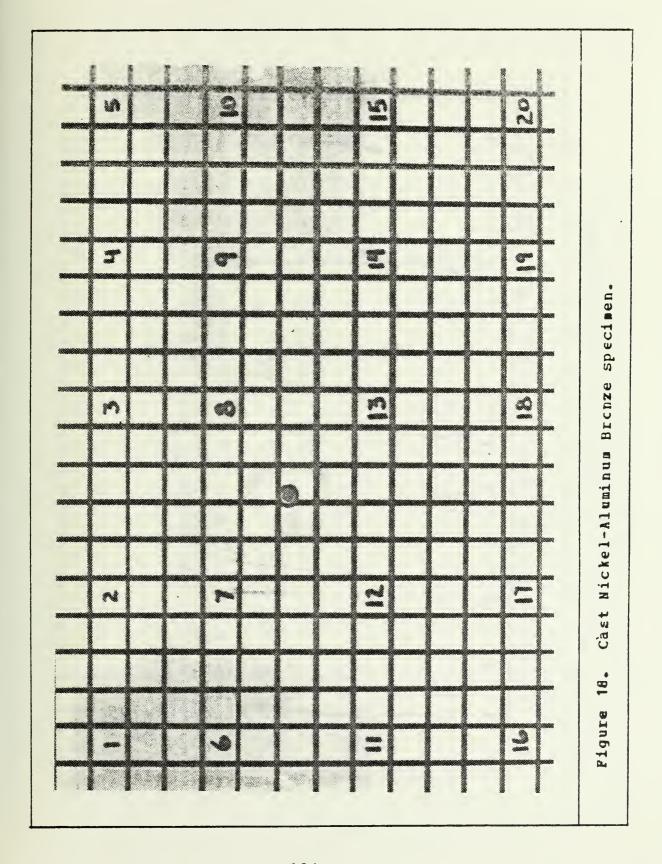




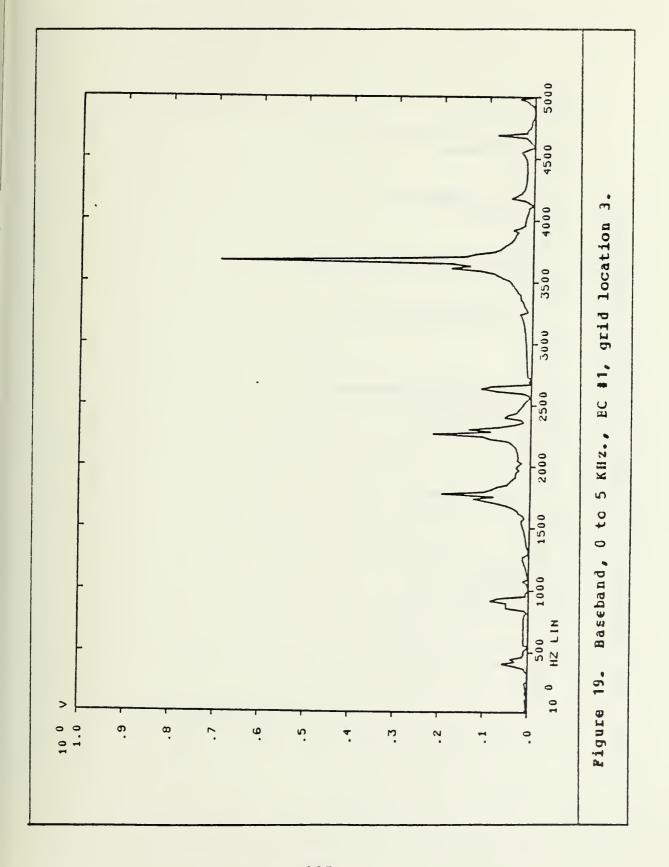


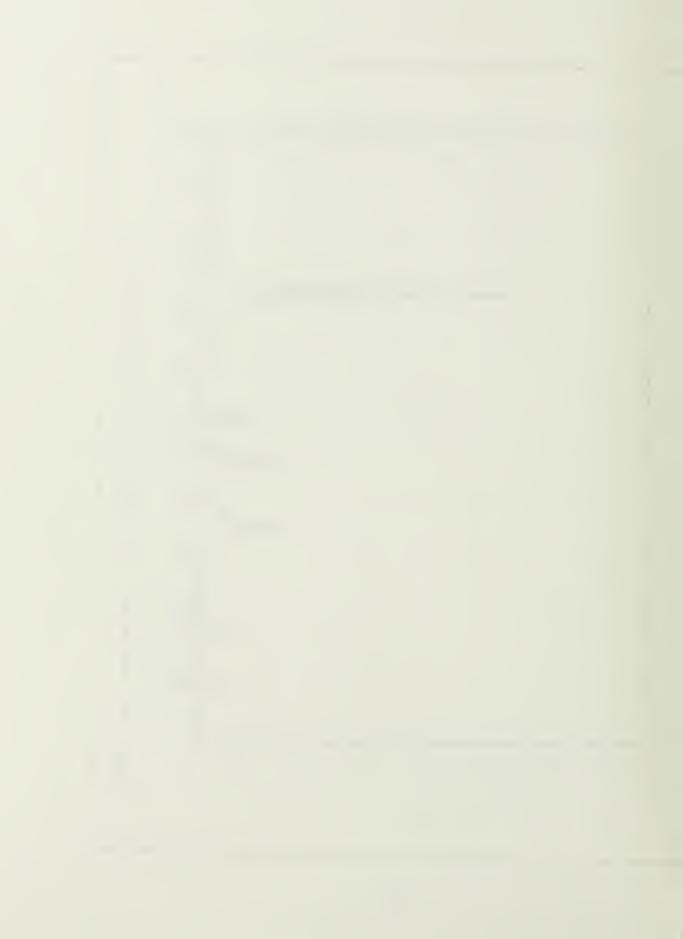


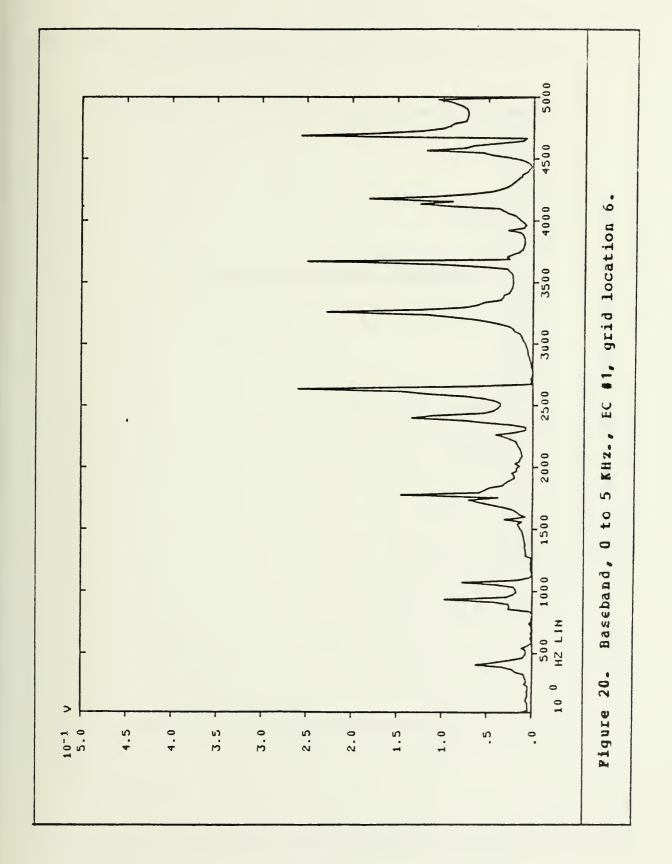




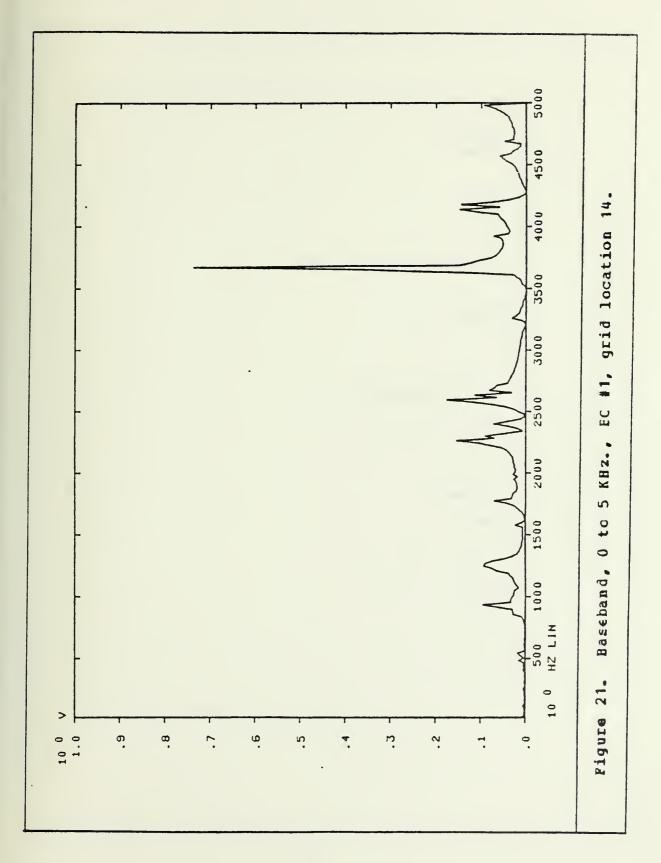




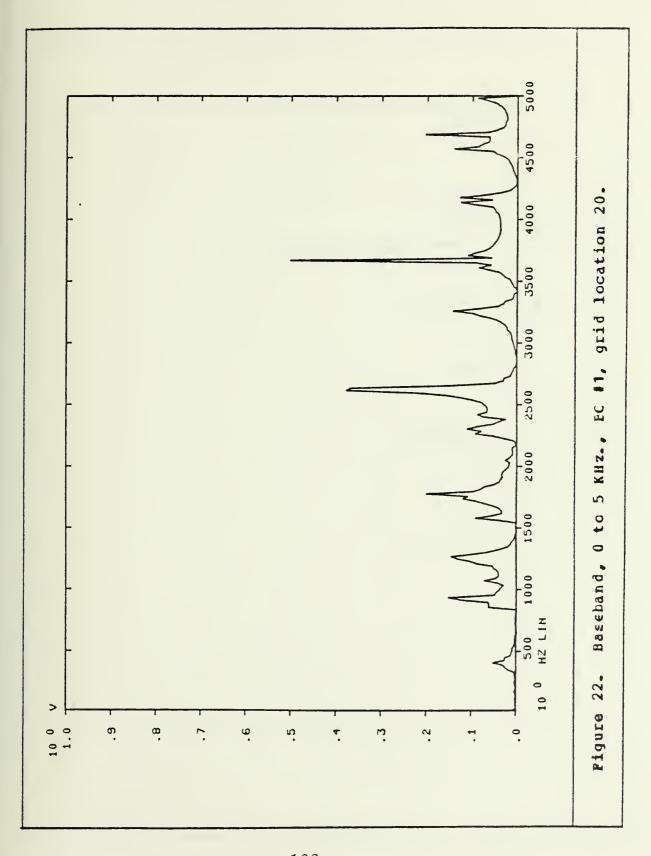




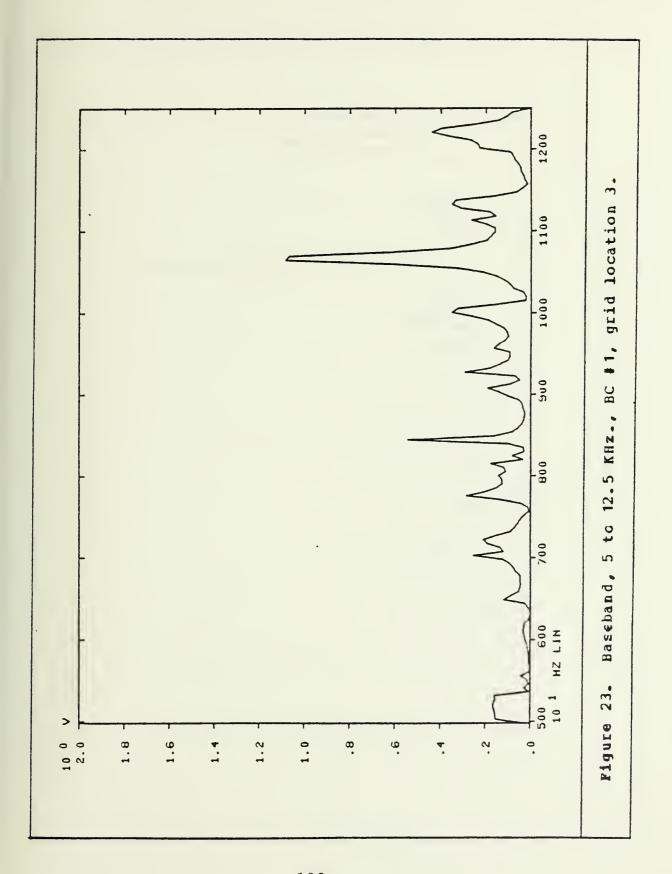




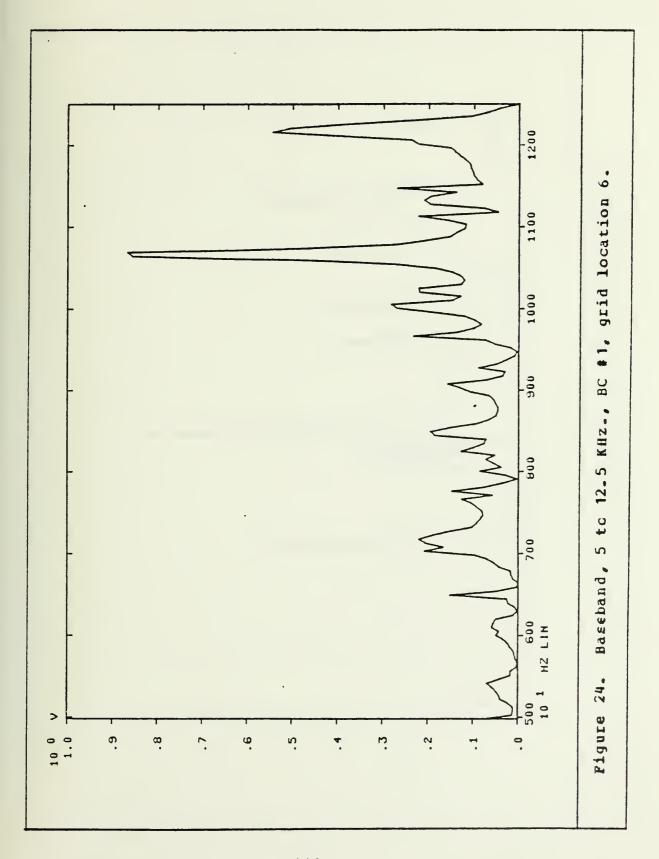




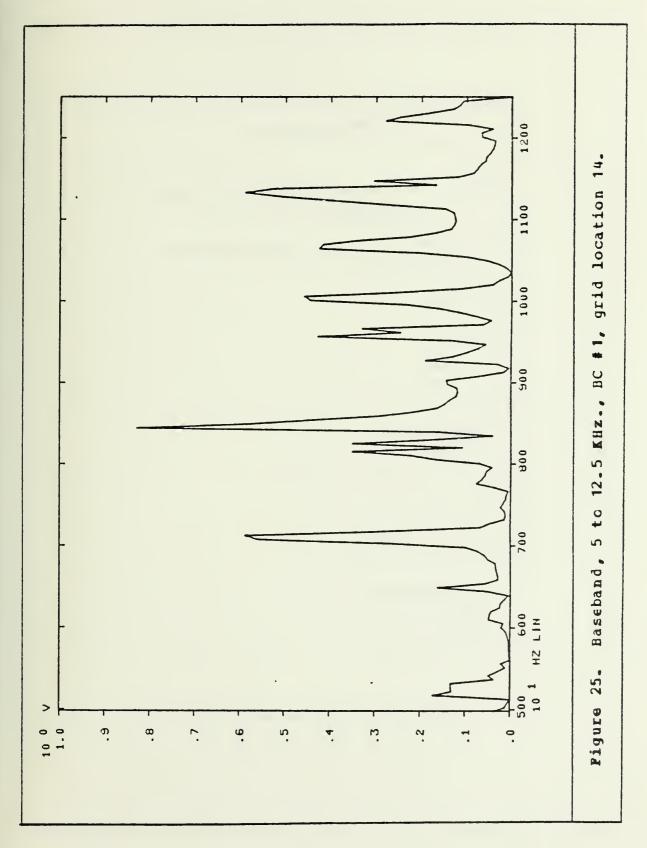


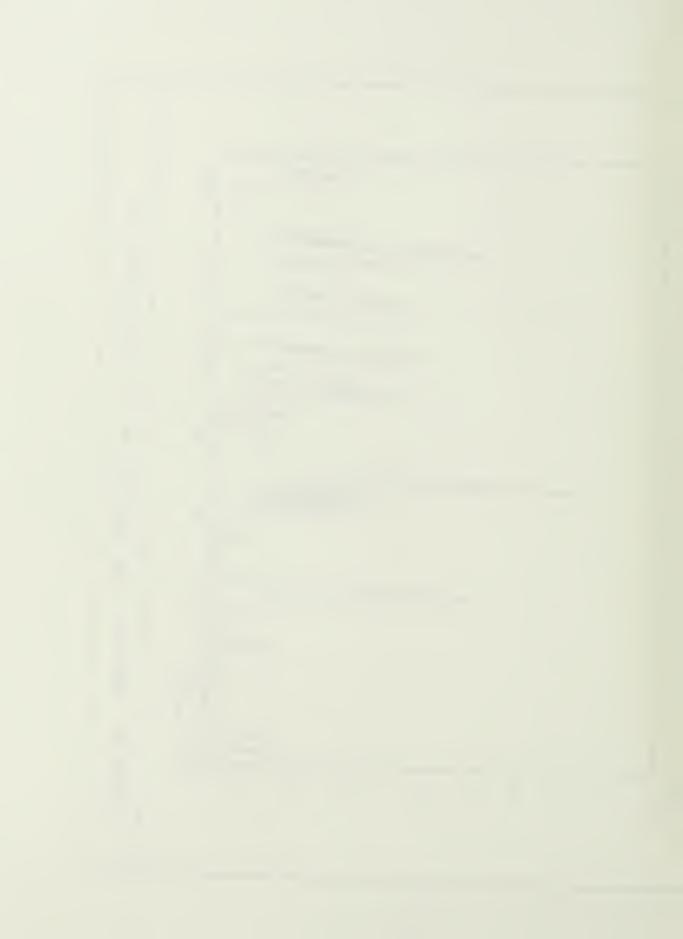


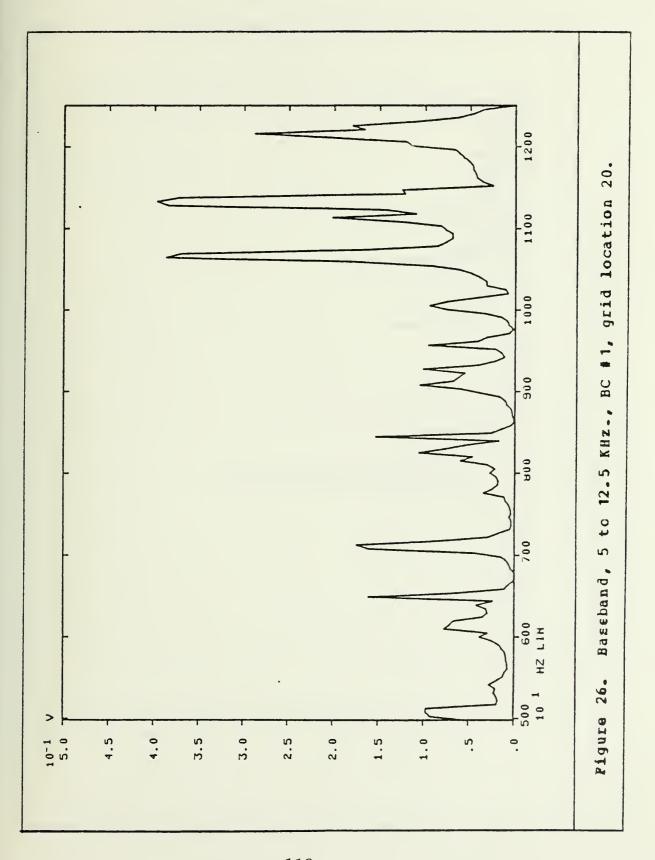


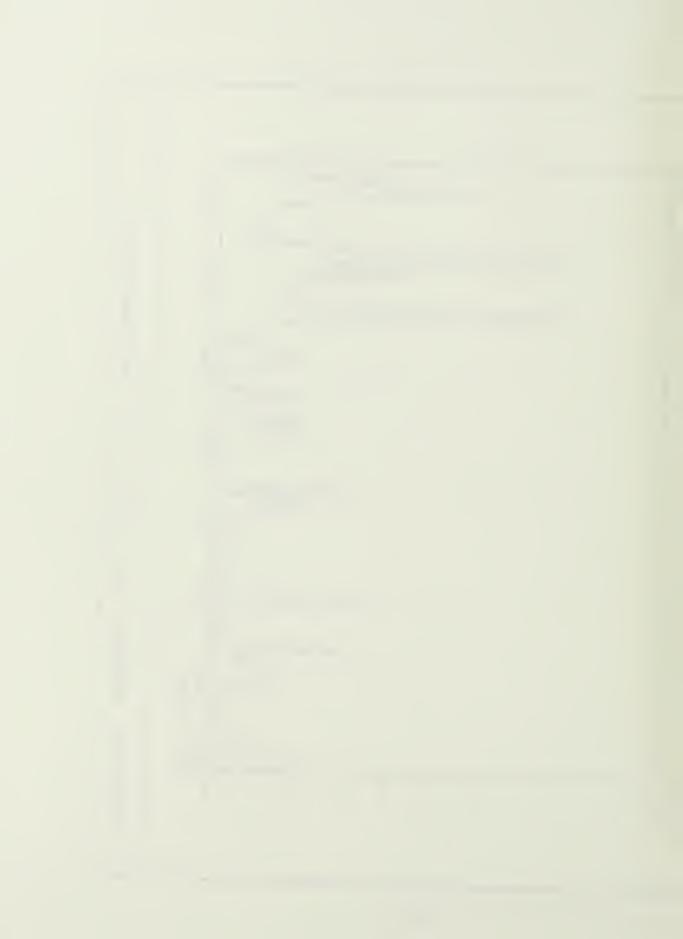


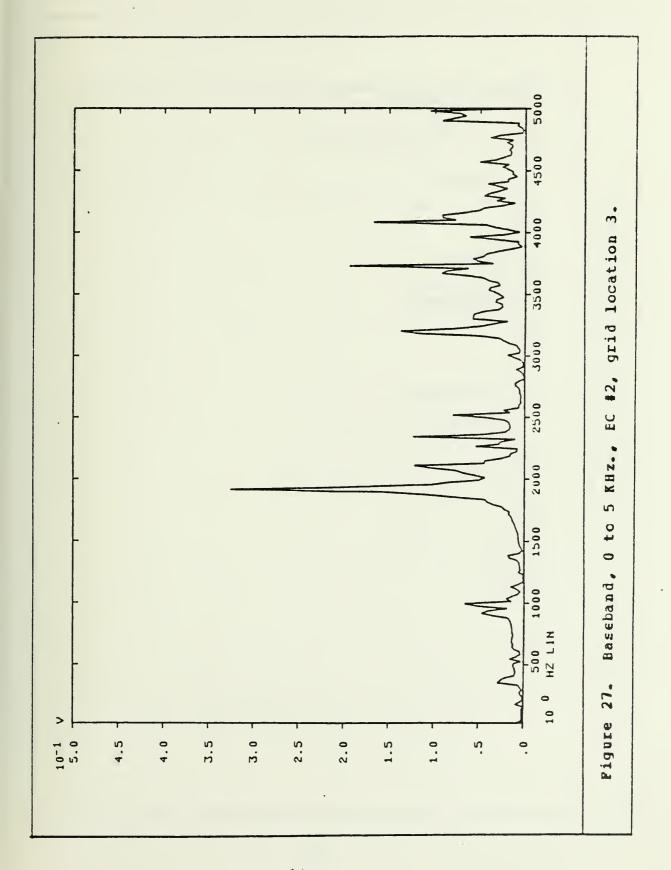


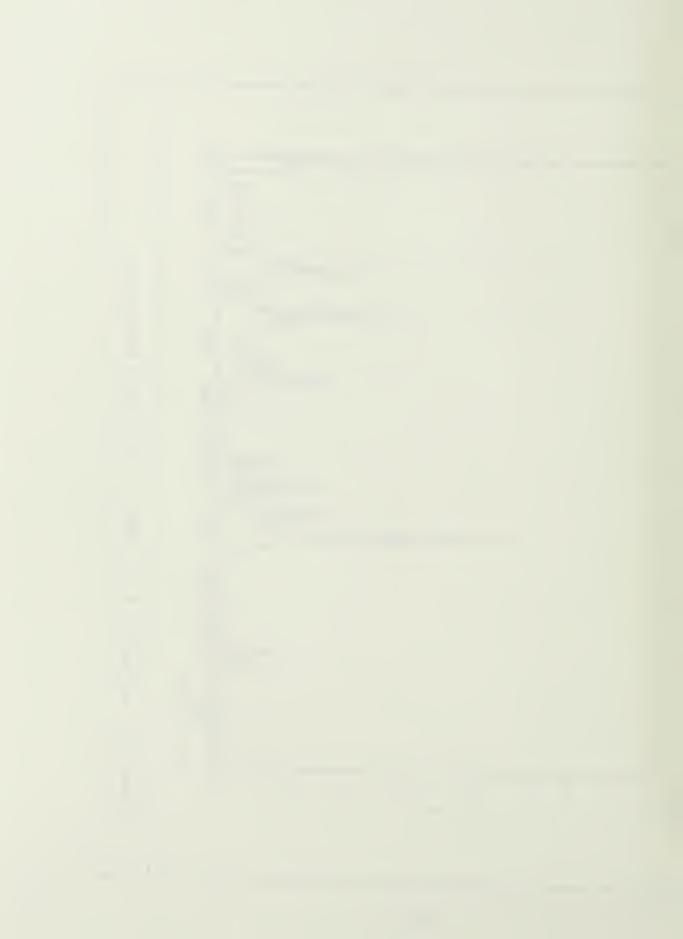


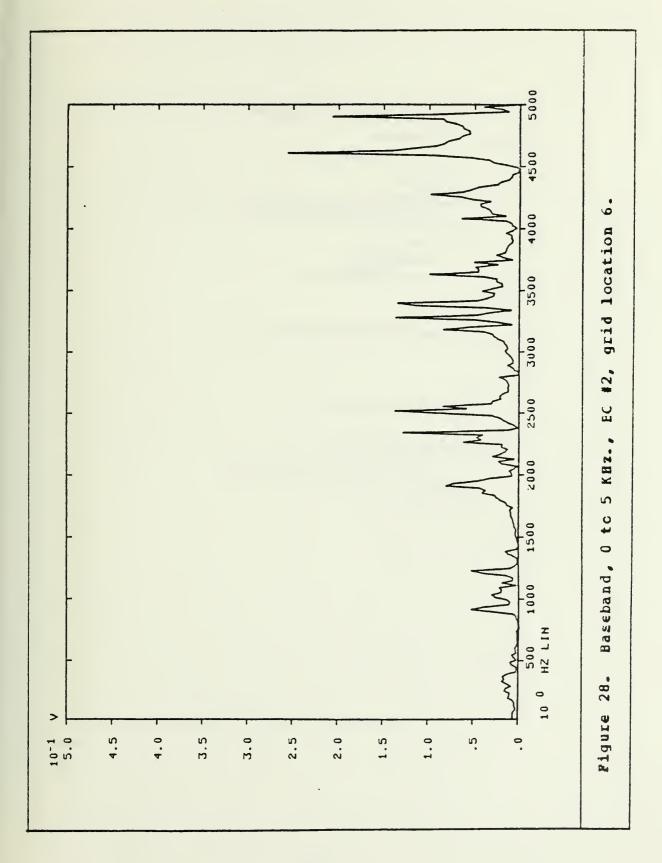




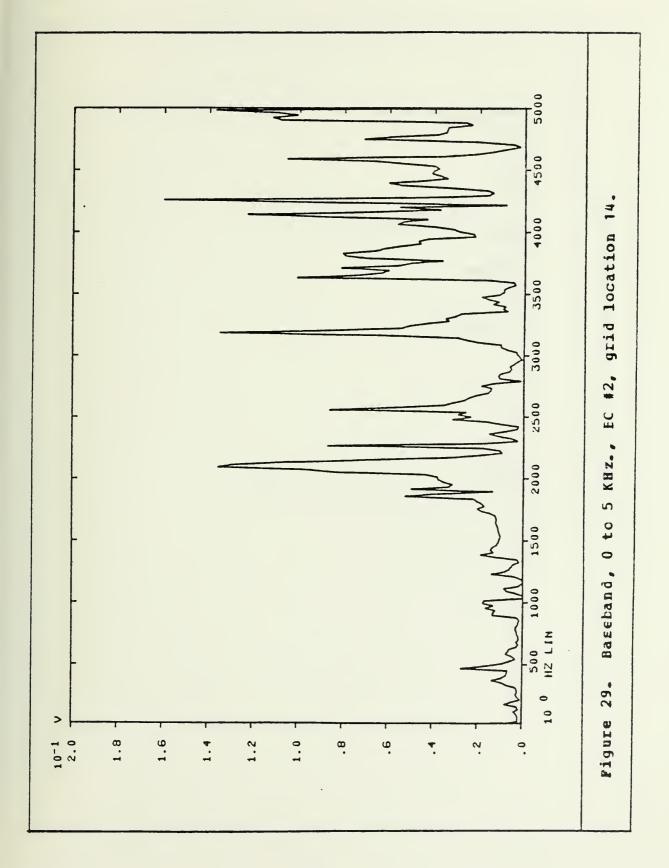




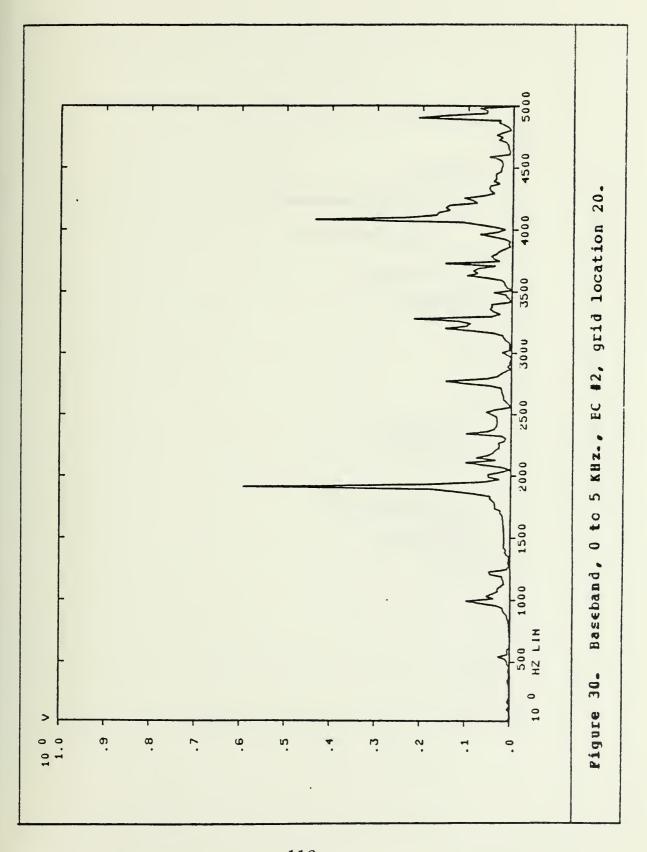




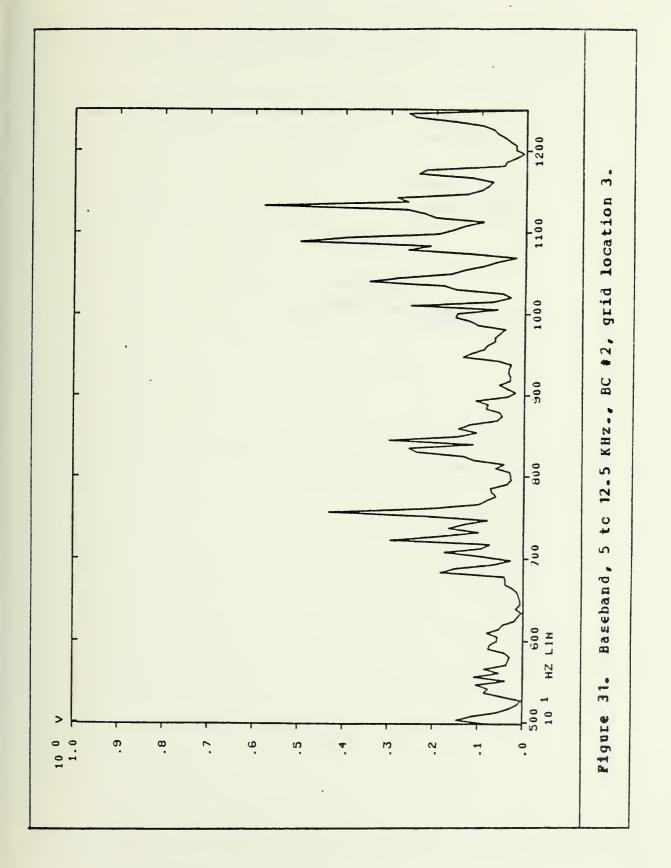




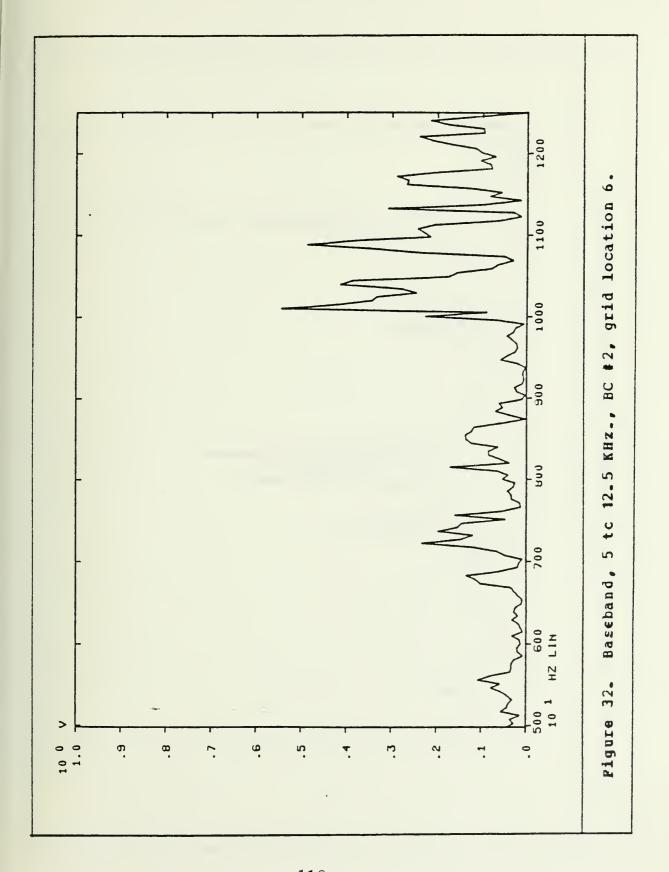




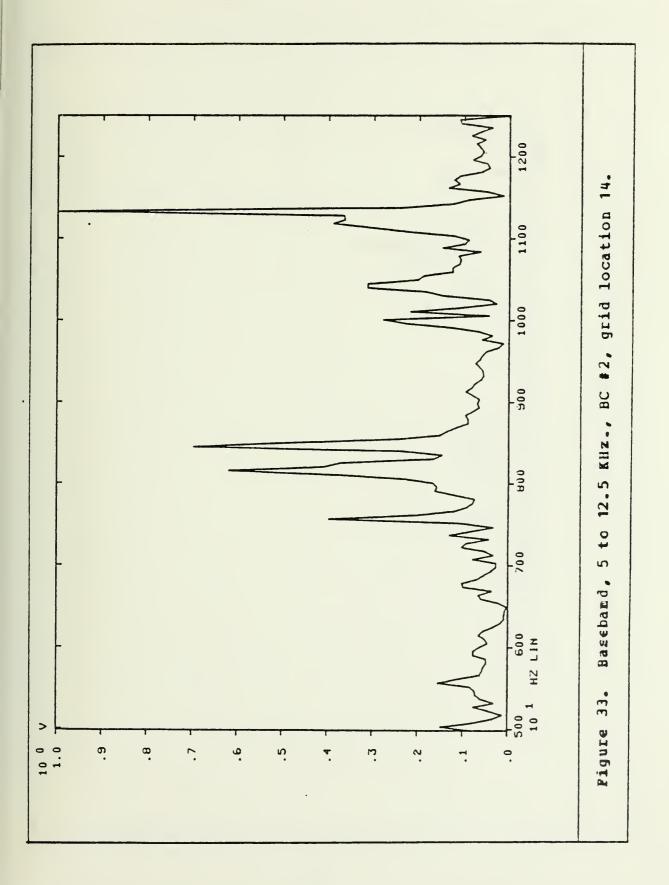




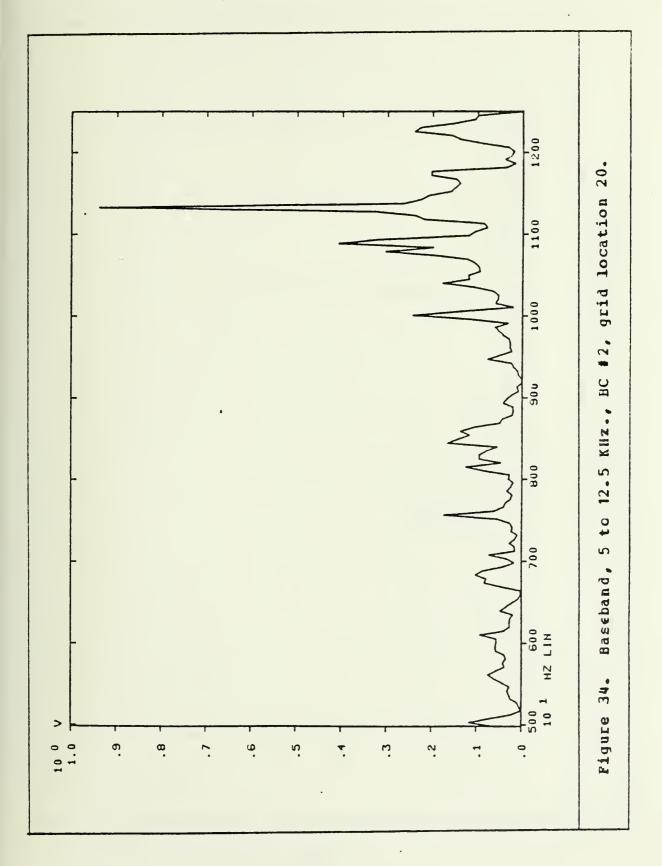


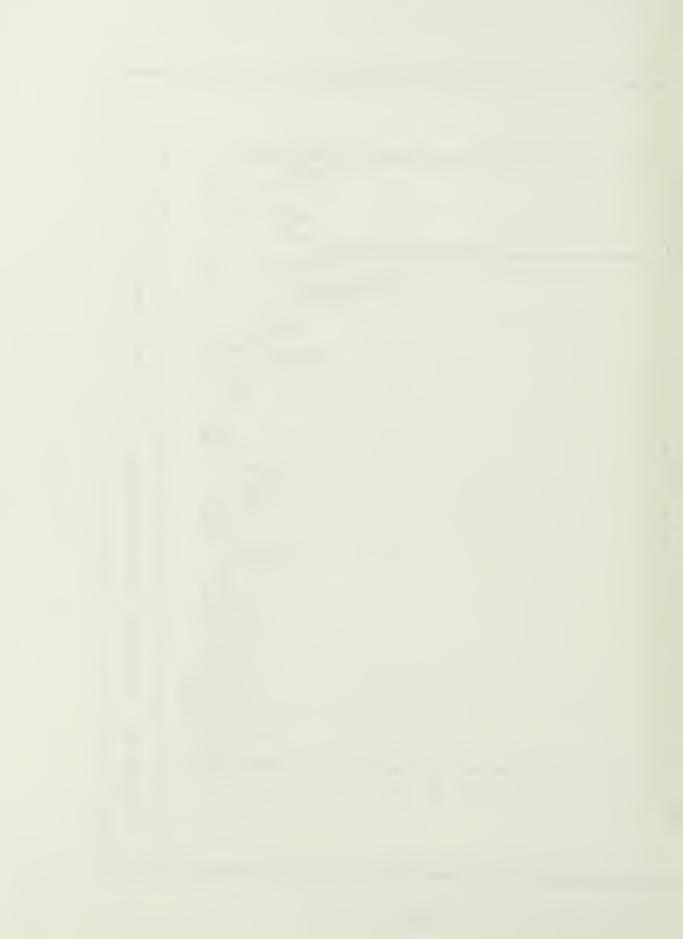


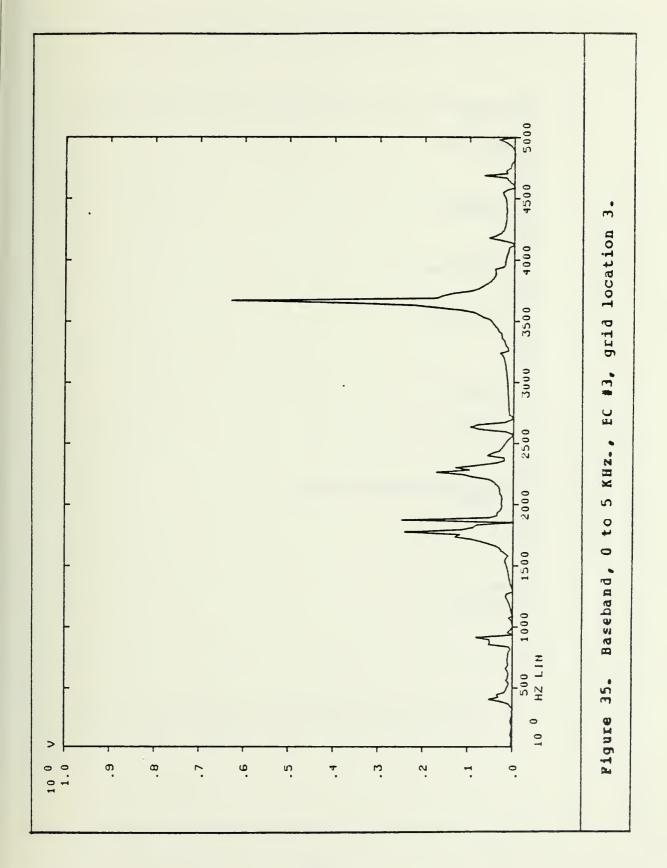




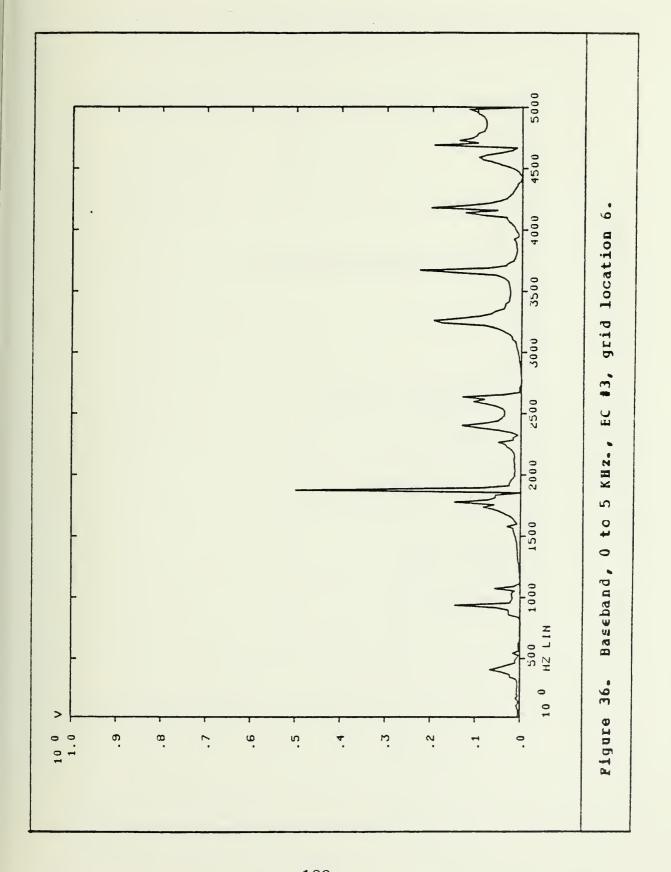


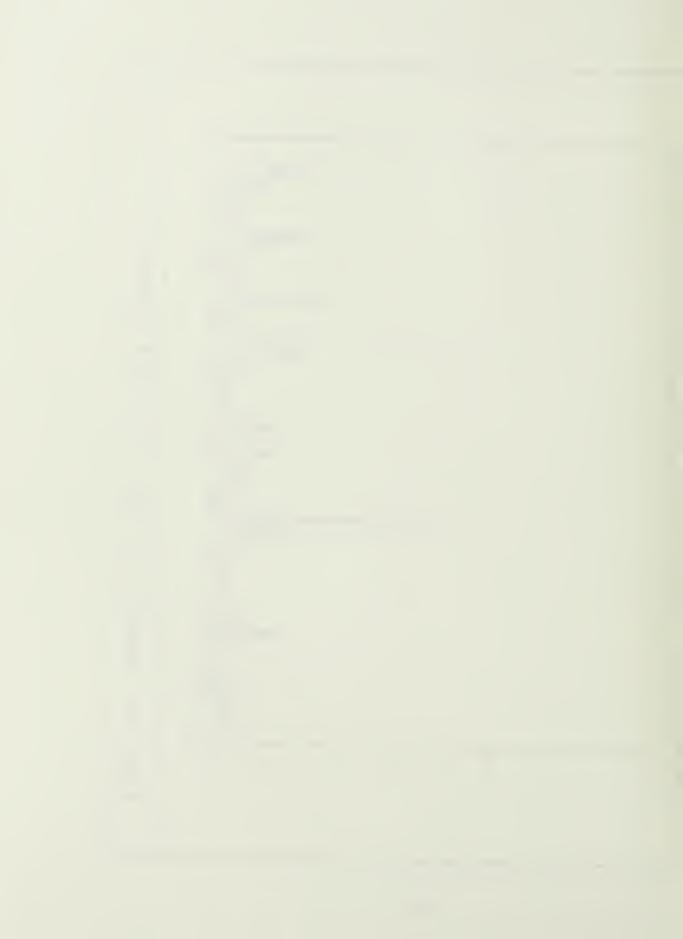


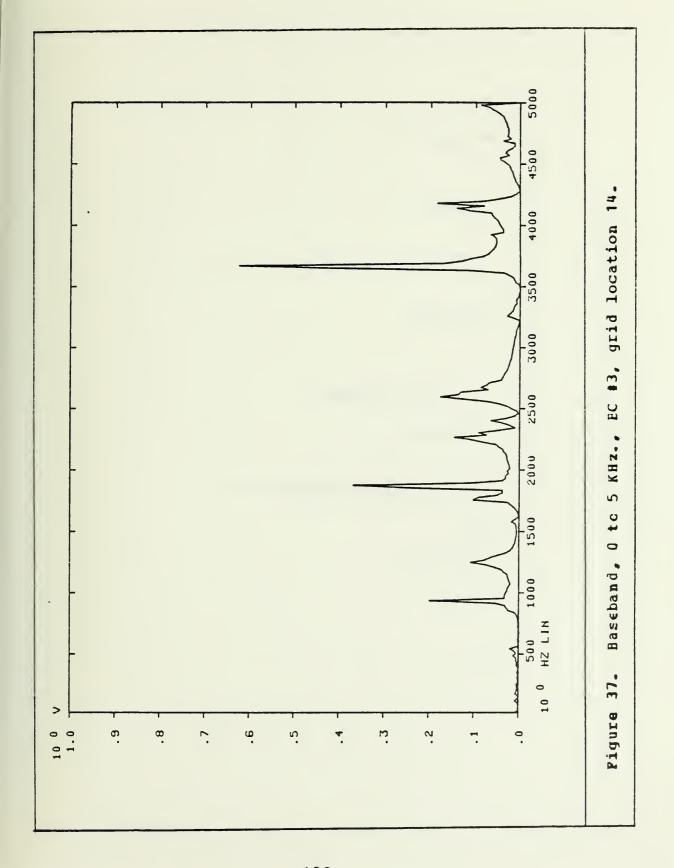




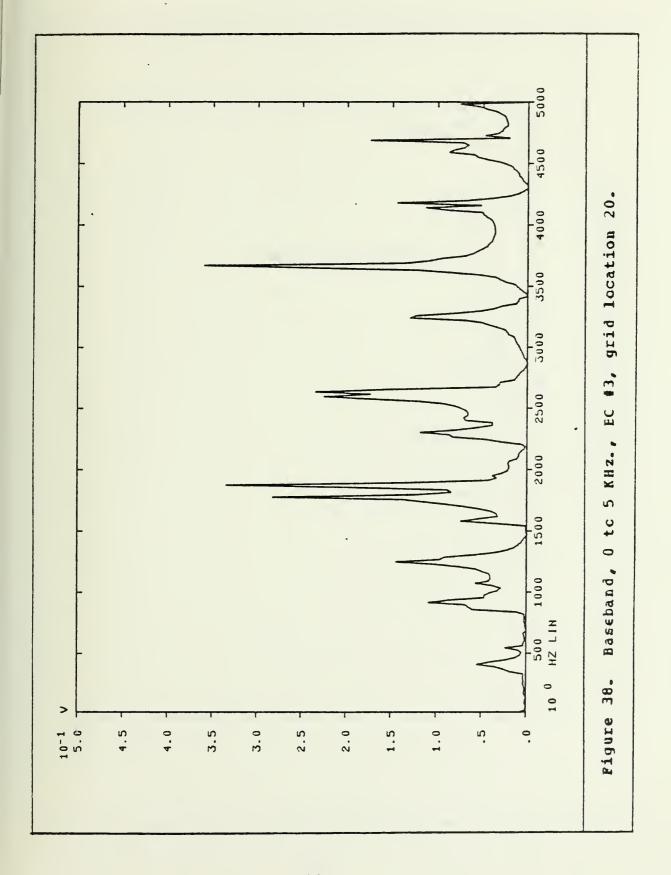




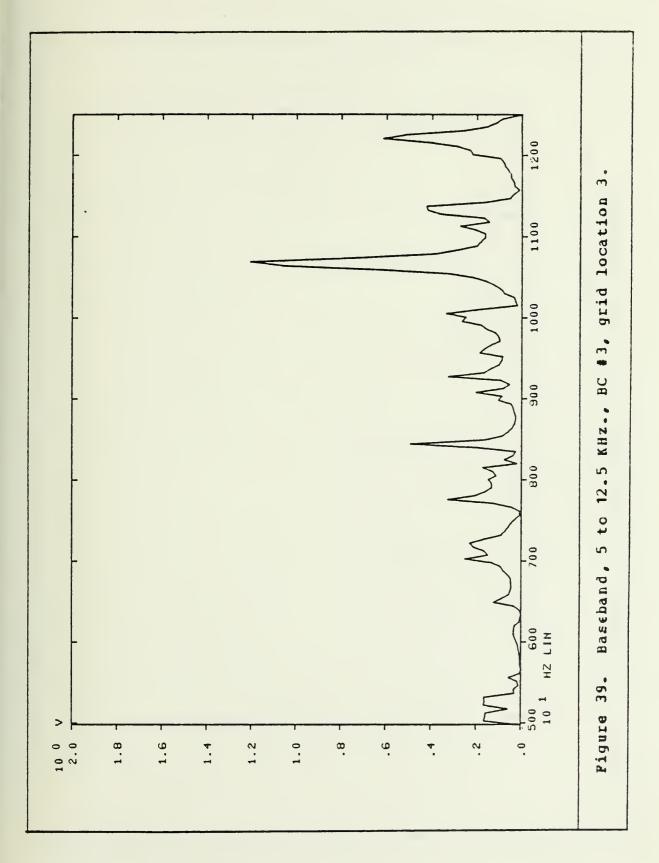




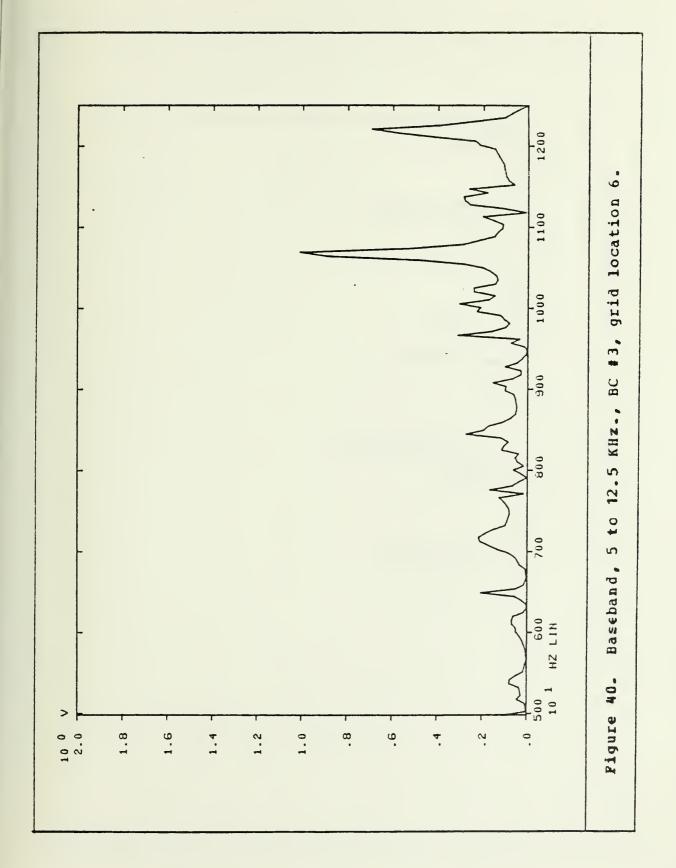




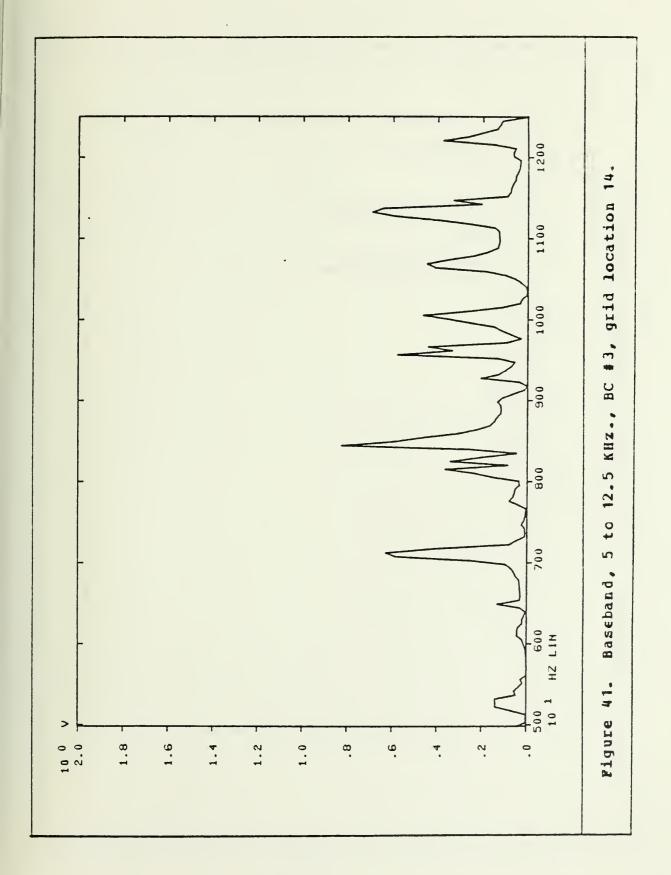




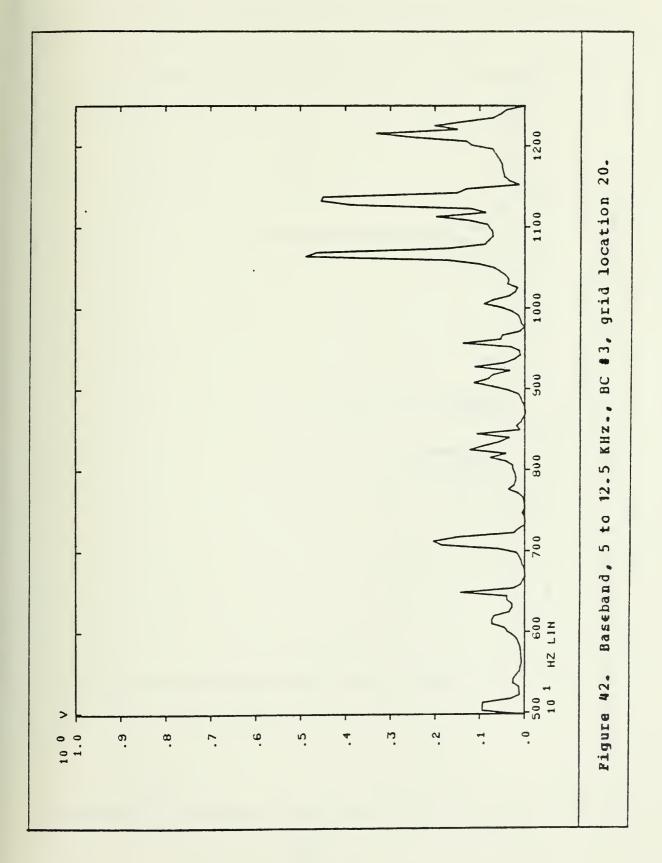


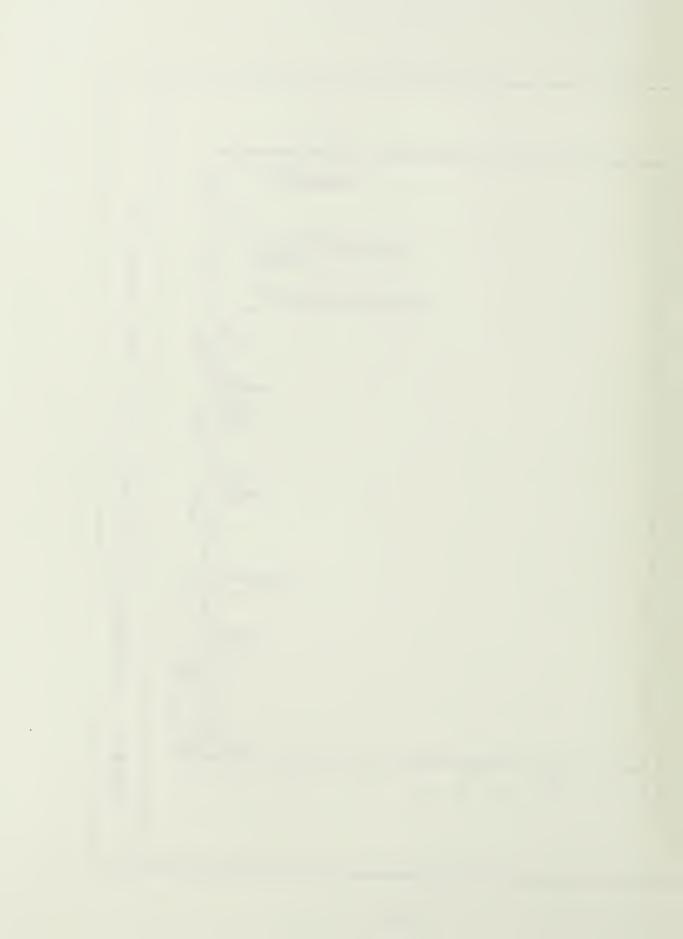


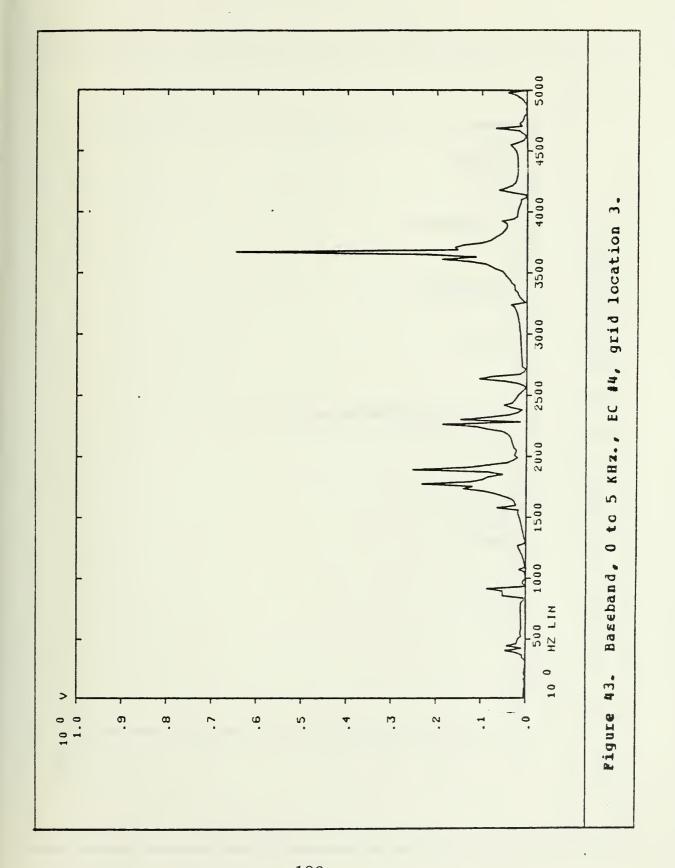


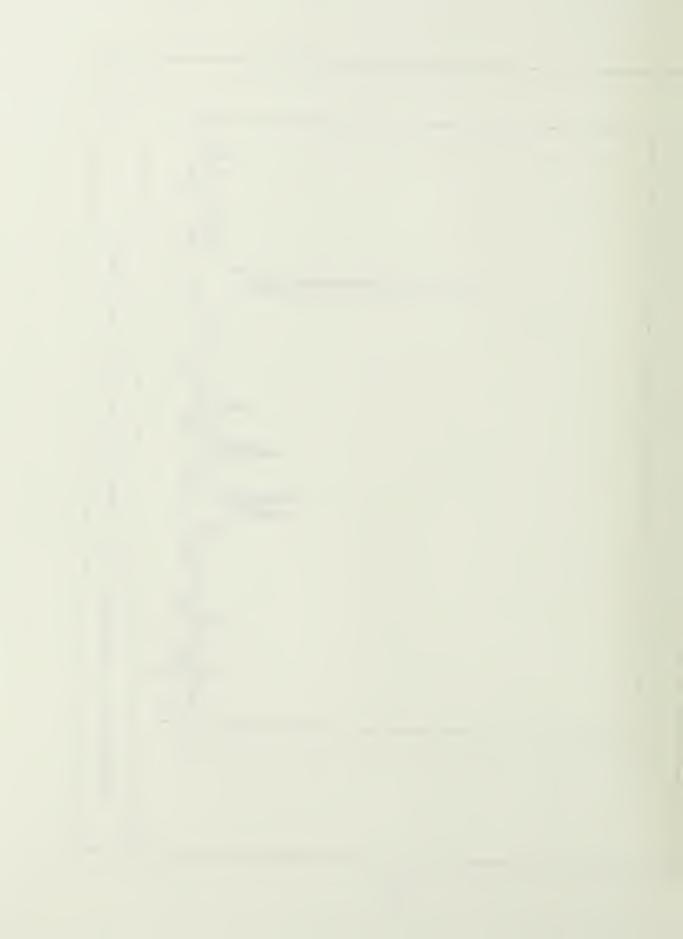


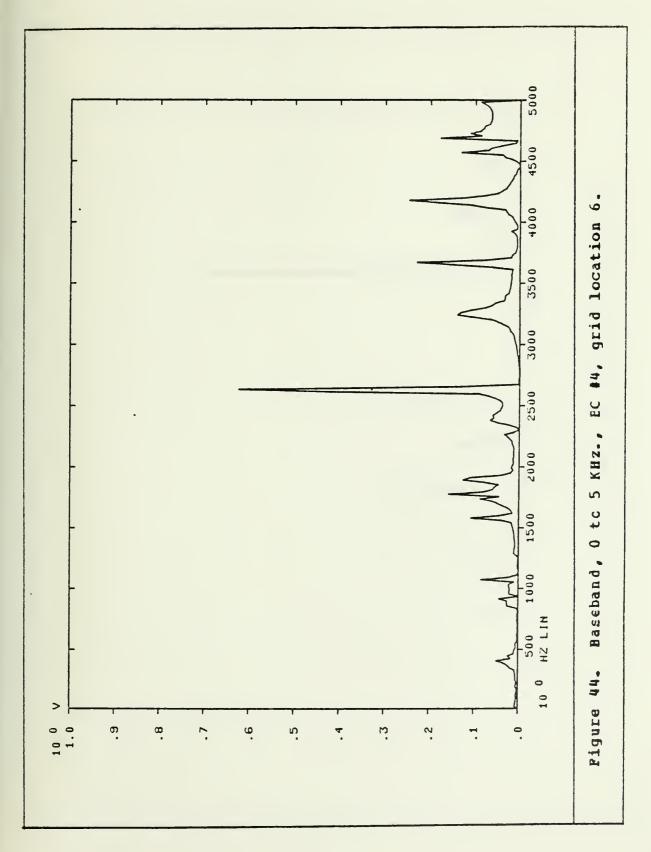




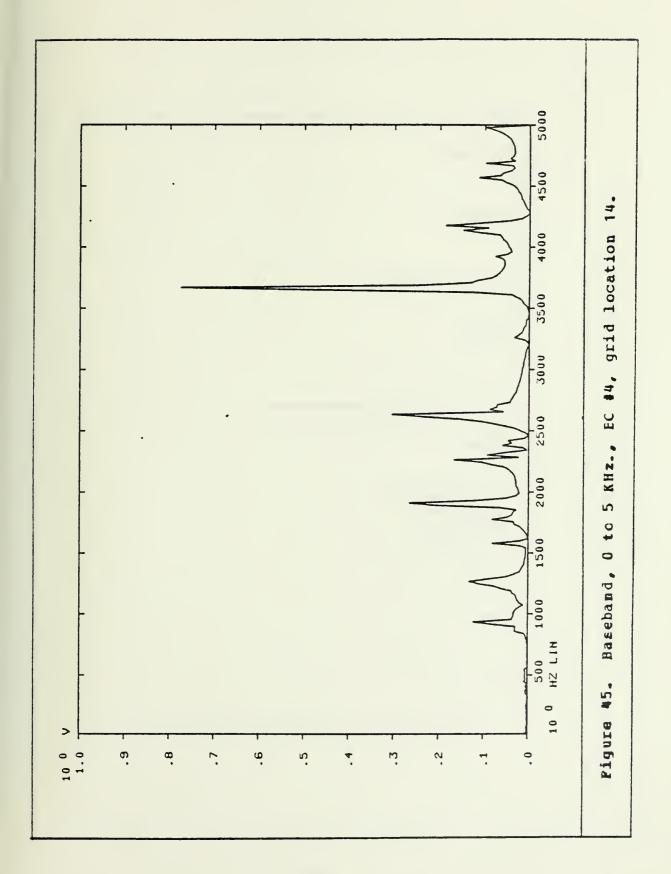




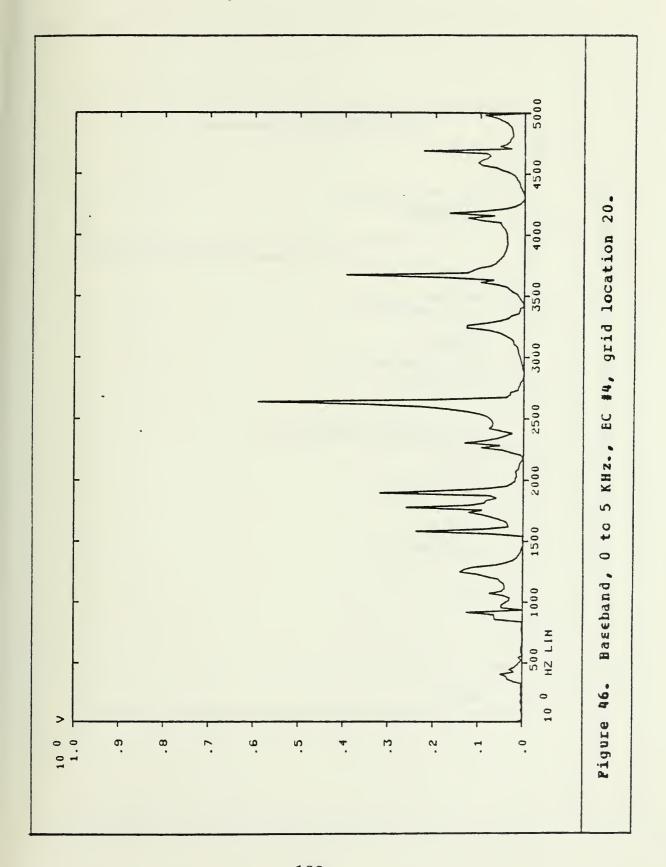


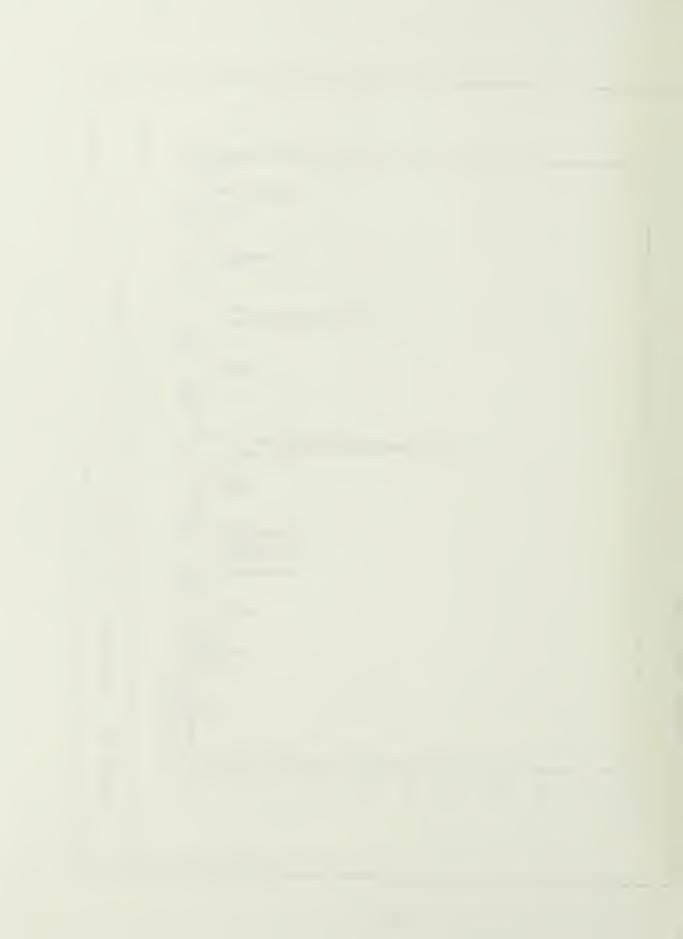


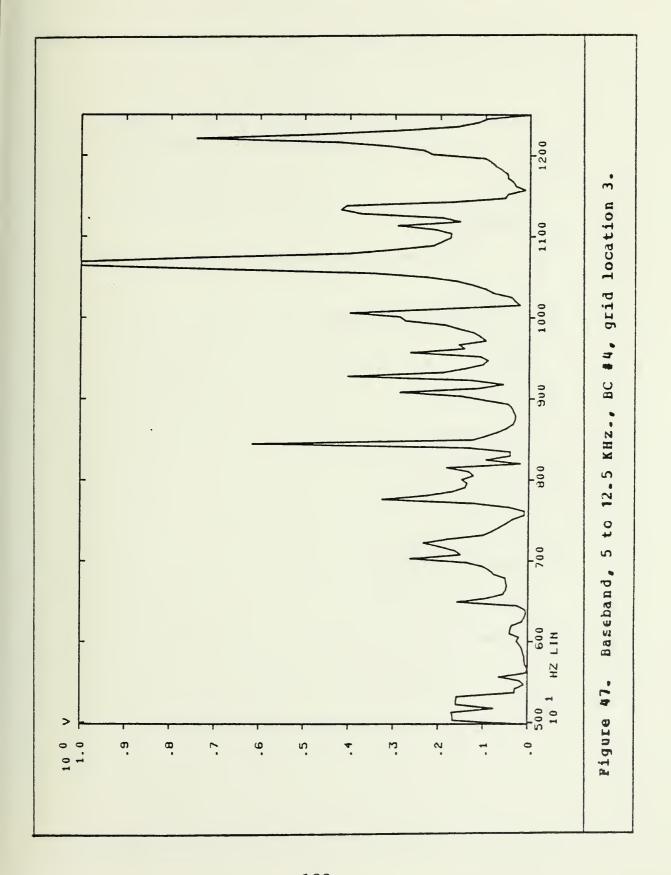


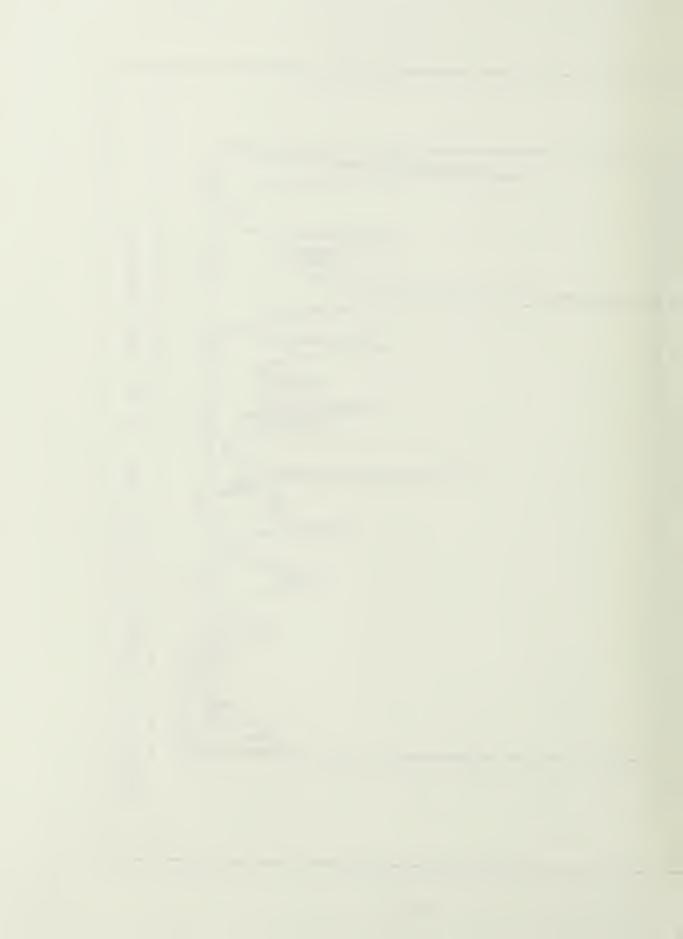


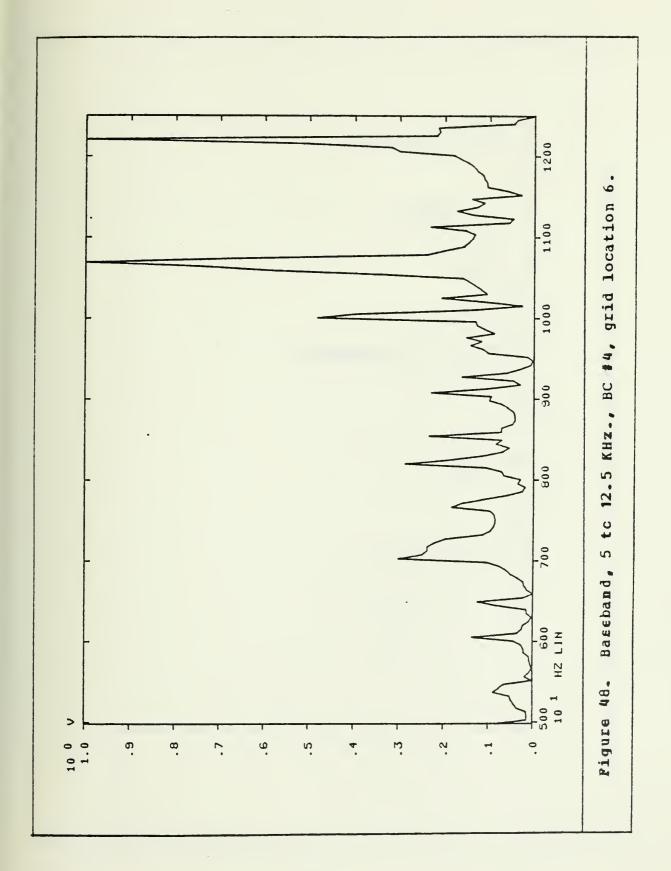


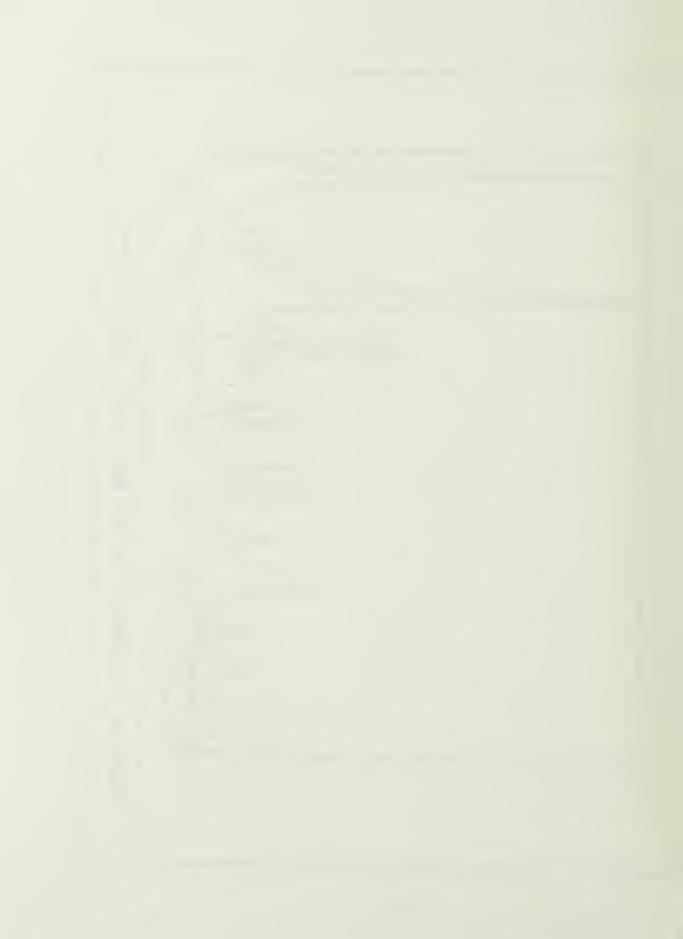


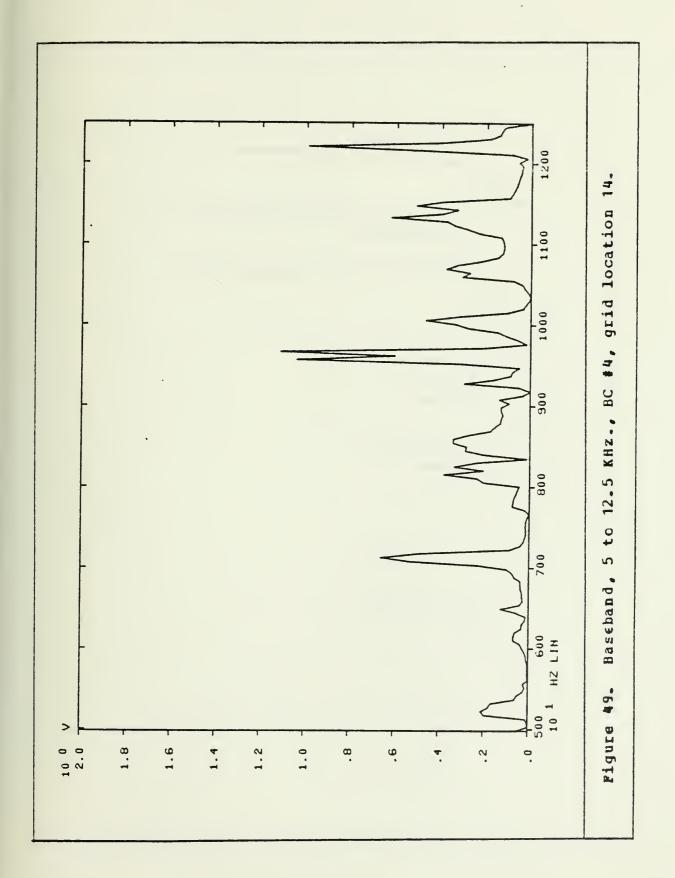


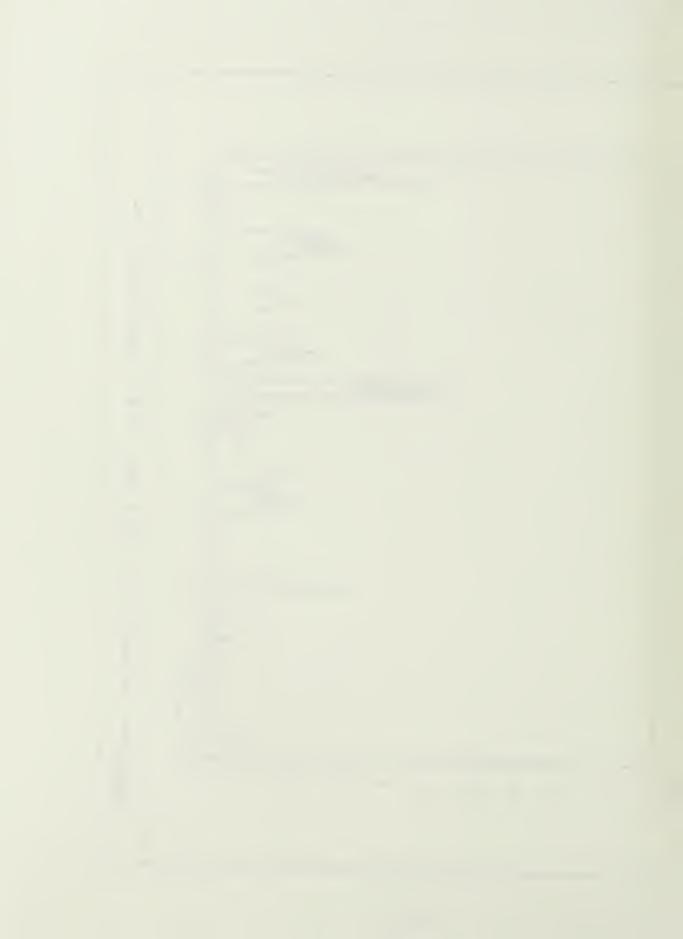


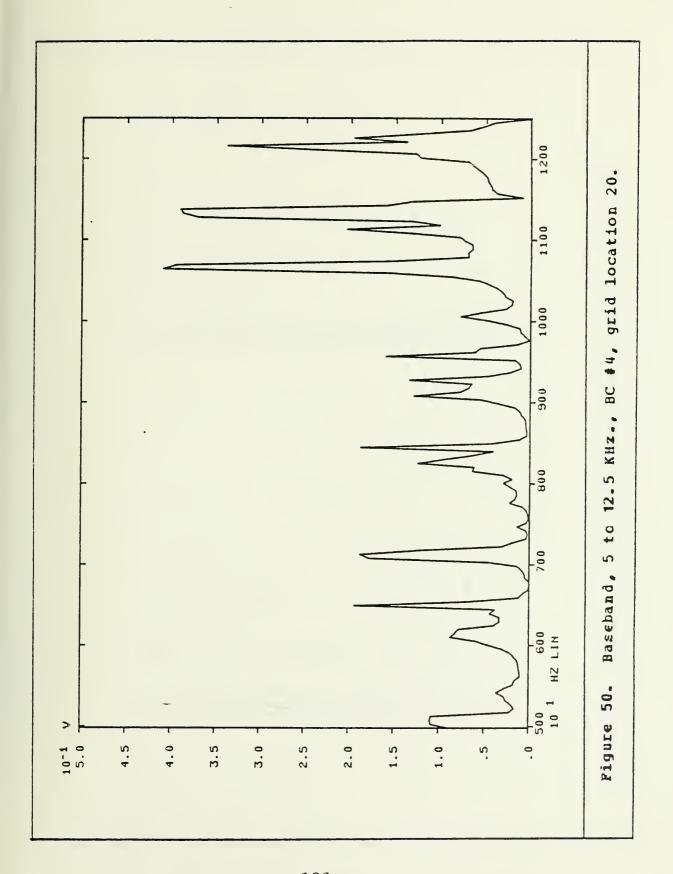














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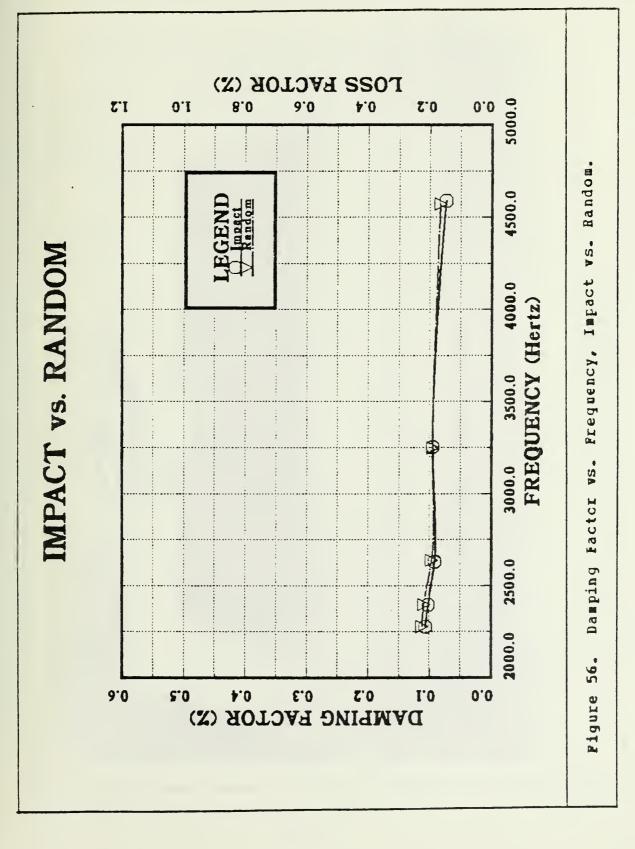
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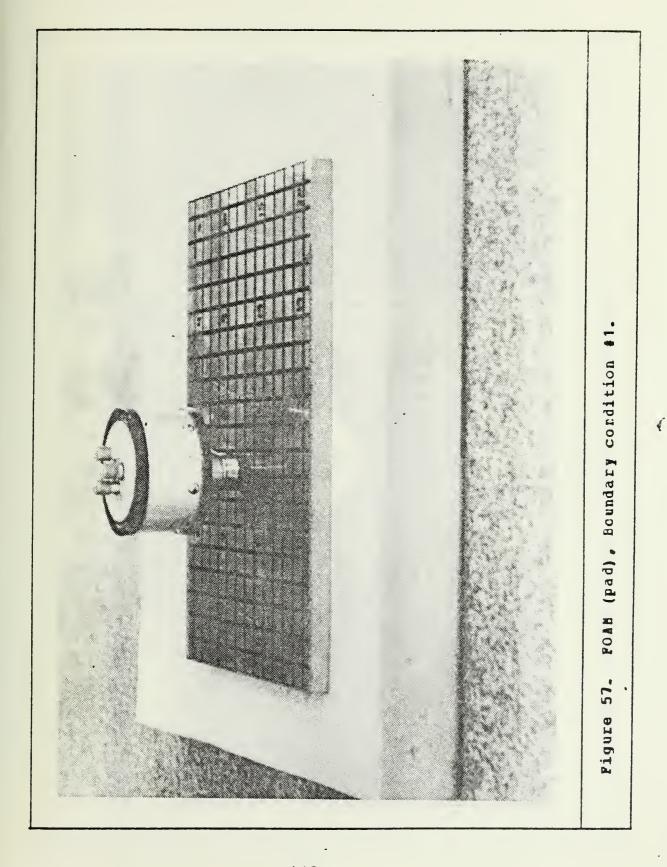


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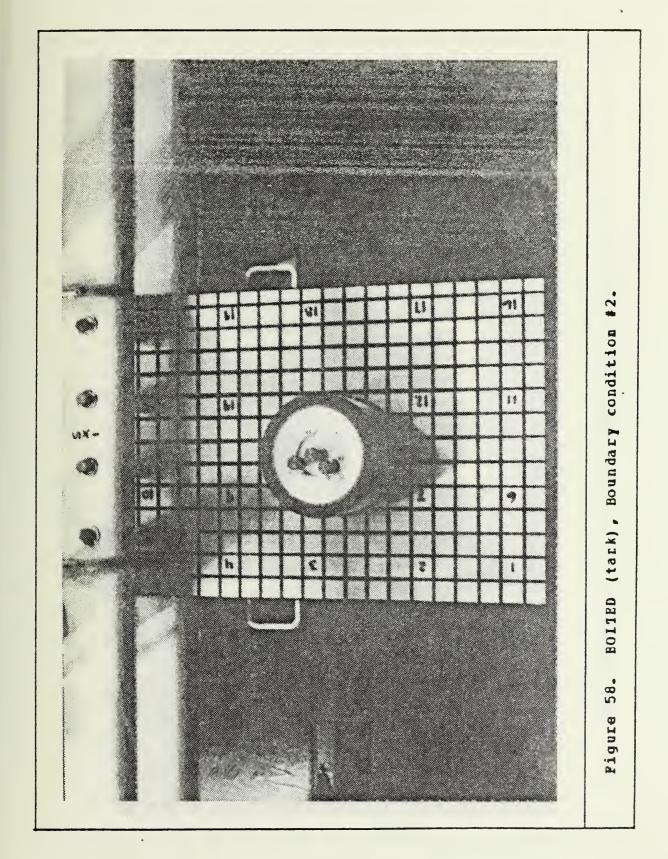




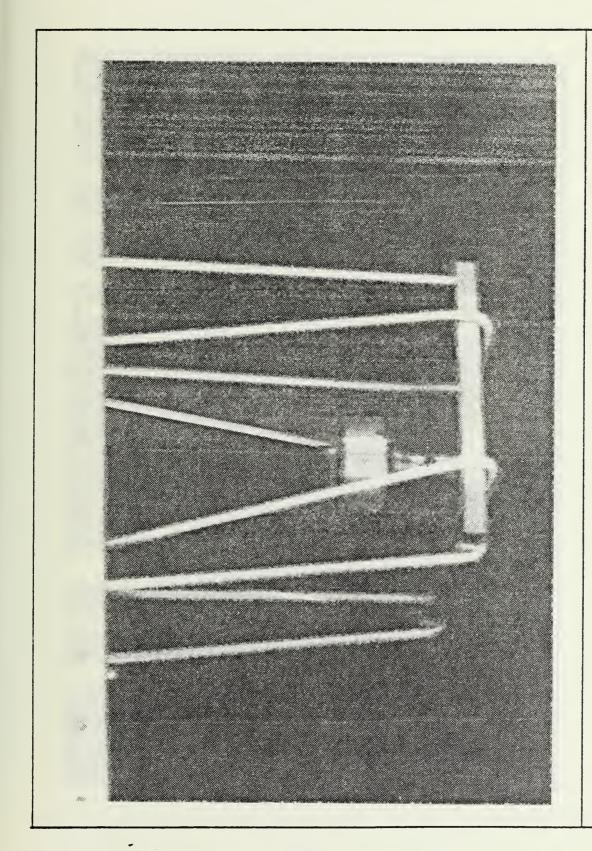






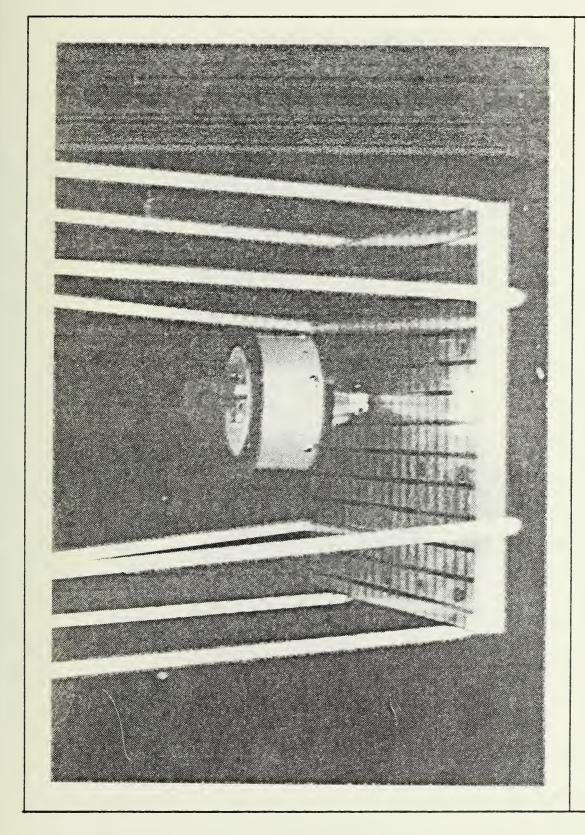






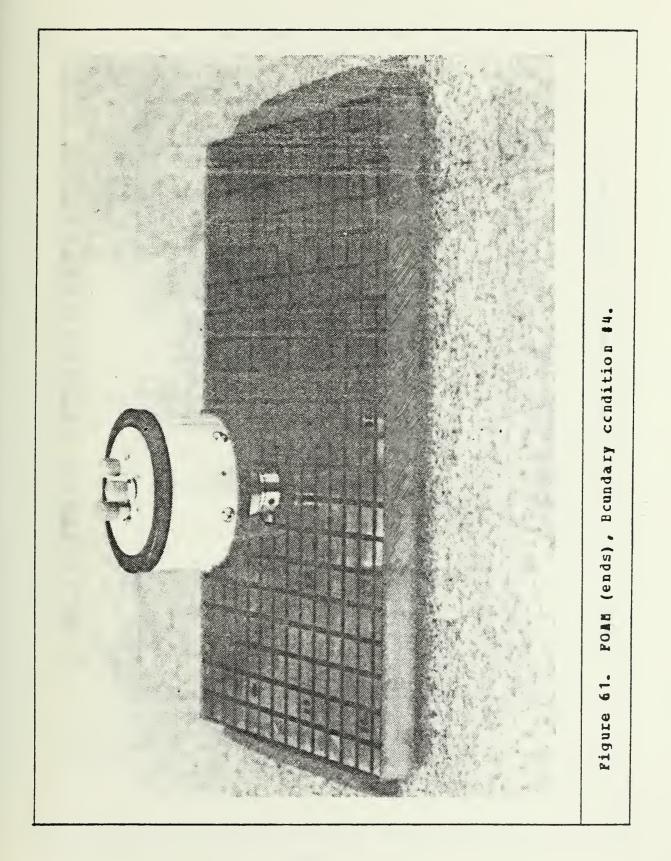
Eoundary condition 43, CHCED (tank), 59. Pigure



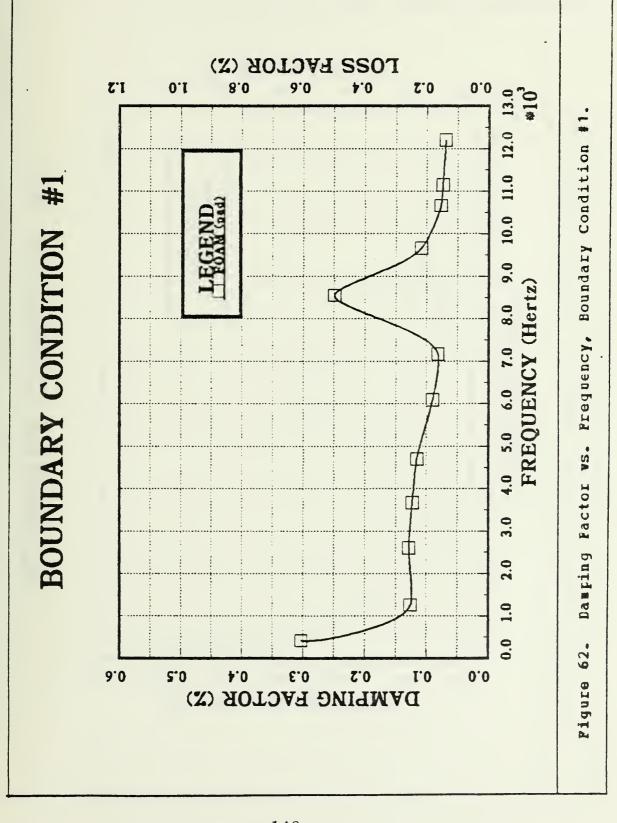


condition Boundary (tank), CHORD 09 Figure

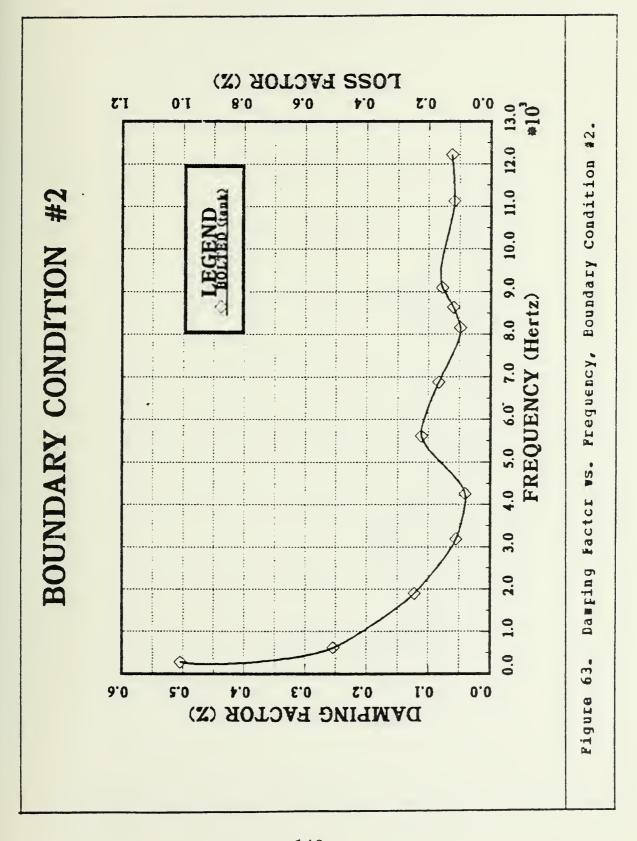




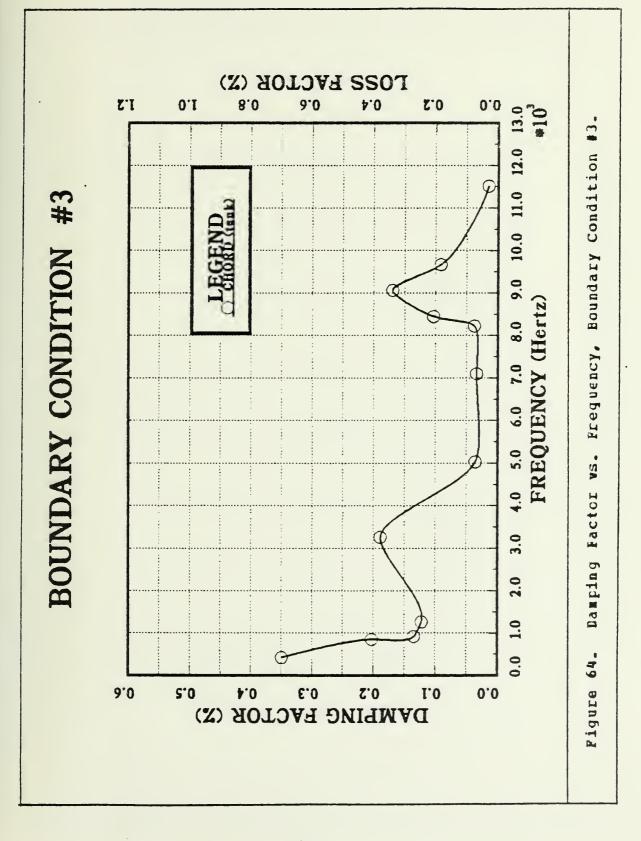




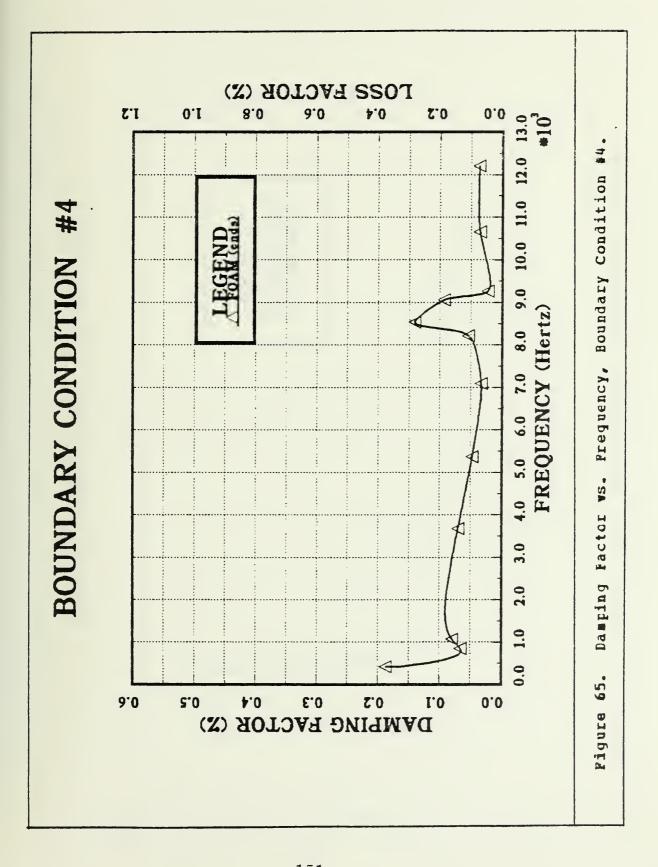




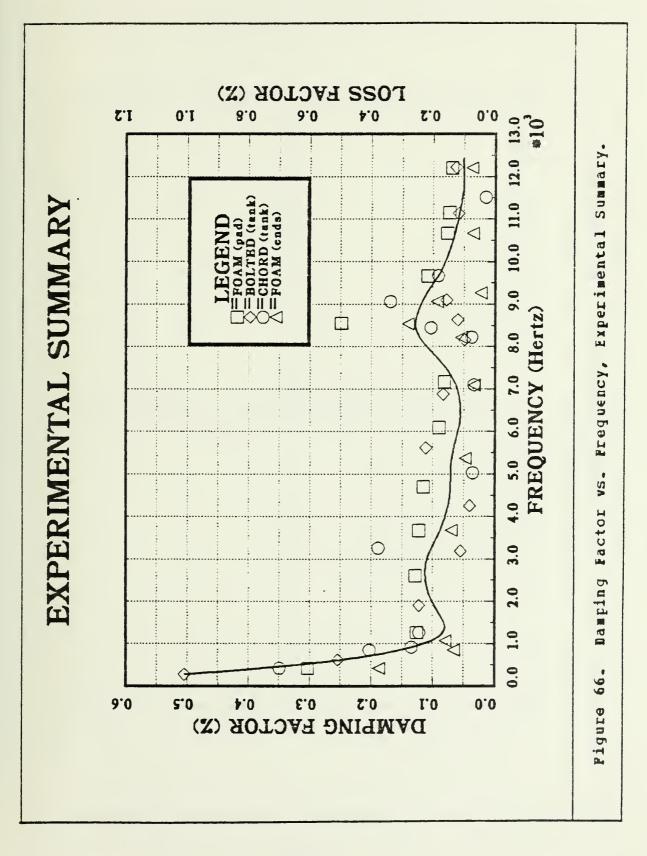




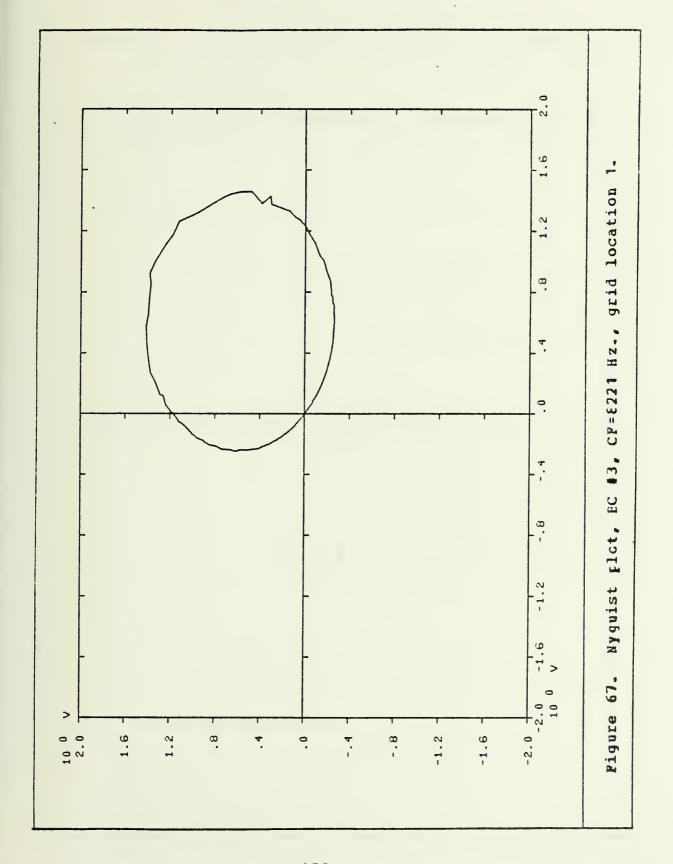




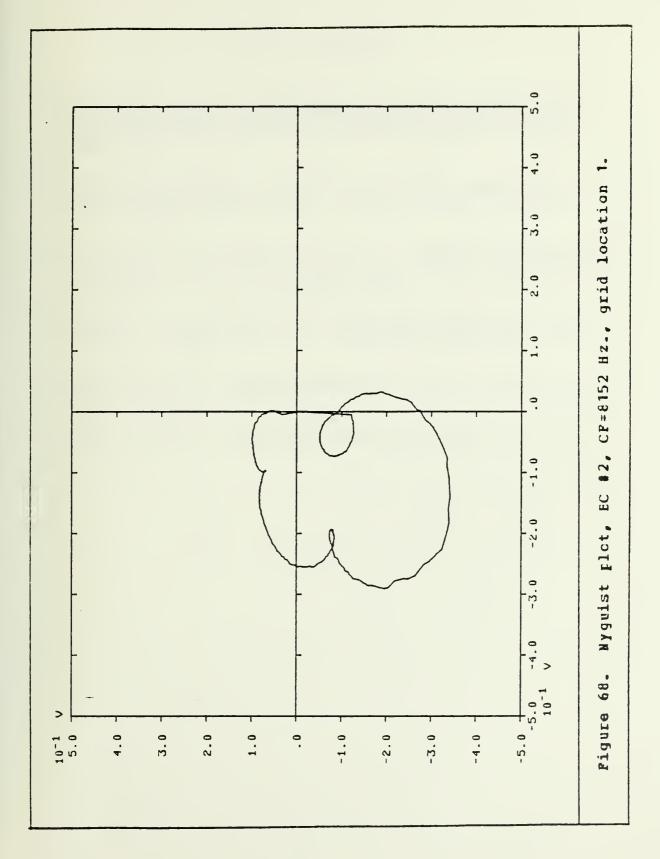












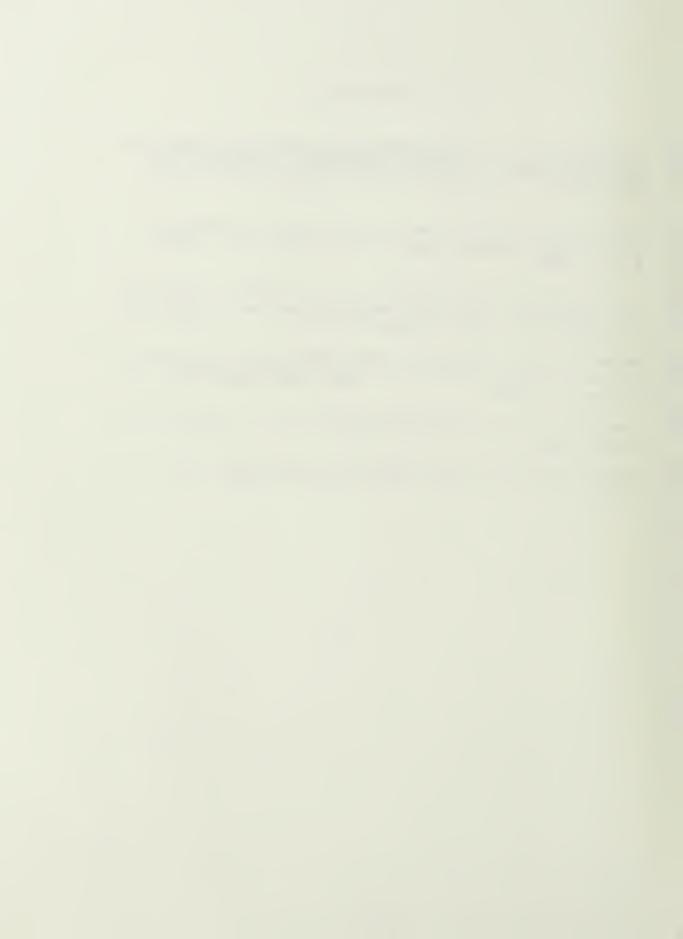


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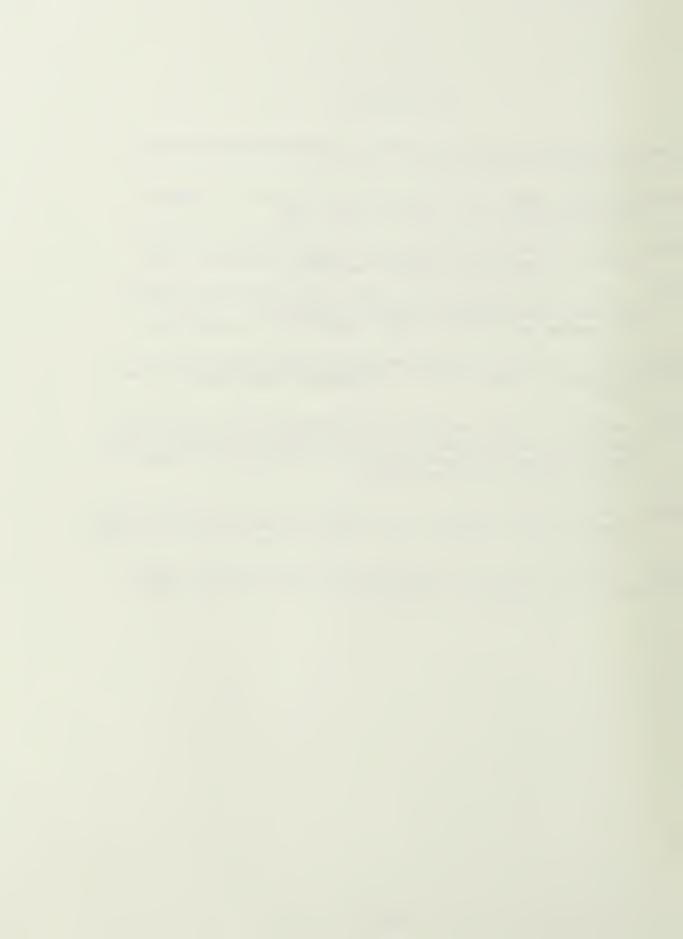
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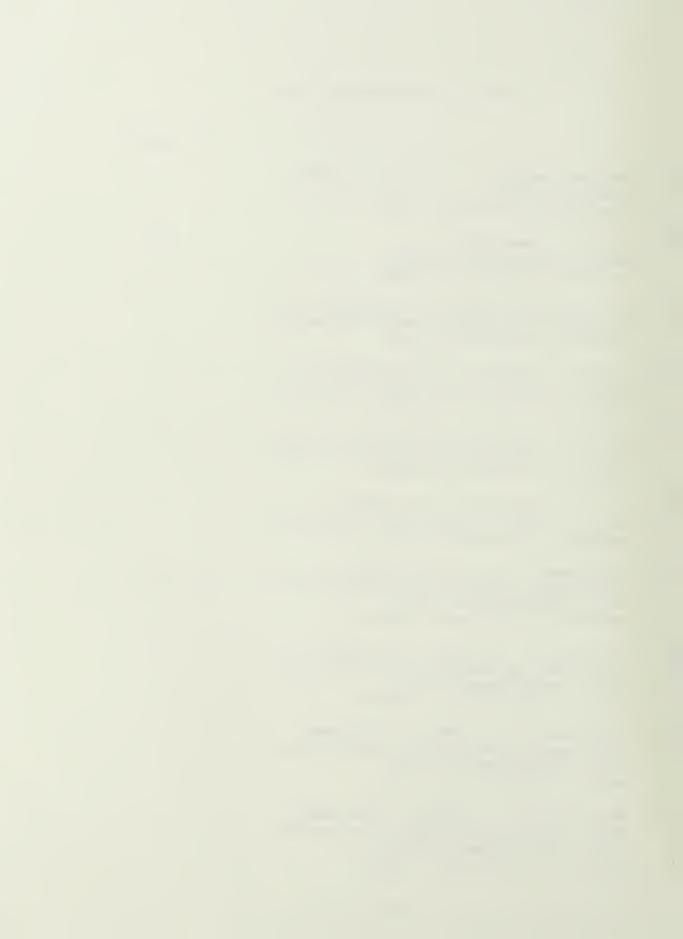
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Effect of boundary conditions on the damping characteristics of a randomly excited cast nickel-aluminum bronze specimen at low stress levels.

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