GALCIT REPORT NO.________

GUGGENHEIM AERONAUTICAL LABORATORY

CALIFORNIA INSTITUTE OF TECHNOLOGY

STRESS DISTRIBUTION IN TWO INTERSECTING CYLINDERS UNDER PRESSURE

Thesis by

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PASADENA, CALIFORNIA

FORM AL-5 6M 2-49

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Thesis by

Lieutenant Commander Vernon E. Teig, U. S. Navy

In Partial Fulfillment of the Requirements

For the Degree of

Aeronautical Engineer

California Institute of Technology

Pasadena, California

1949

ACKNOWLEDGEMENT

The author is indebted to Dr. Ernest E. Sechler, Professor of Aeronautics, California Institute of Technology, for his valuable guidance in the formulation of this thesis, and to Mr. William H. Bowen, Superintendent, Guggenheim Aeronautical Laboratory, California Institute of Technology, for his able assistance and advice in the procurement and preparation of the test specimens and testing equipment. He also wishes to thank the other members of his supervising committee, Professors Housner and Fung for their comments and criticisms on the work.

Further indebtedness is acknowledged to Commander Leonard E. Harmon, U. S. Navy, who collaborated in conducting the experiments and in the preparation of all tables and graphs presented herein.

SUMMARY

The experimental studies presented here were undertaken in an effort to determine the stress distribution in two circular cylinders intersecting at right angles and under internal pressure. The investigation was limited to tests of two specimens in the thick-walled cylinder range.

The experimental analysis led to the following conclusions:

1. The highest stress concentrations are located at an angle of about 14.5 degrees from the crotch centerline, measured in the plane of the intersection.

2. The critical stress causing rupture is the tangential stress in the plane of the ellipse.

3. For the R/t ratios tested, the strength reduction as compared with a straight closed cylinder is approximately 50%.

4. It appears probable that bending effects for these thick-walled cylinders are of relatively minor importance.

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EXPLANATION OF SYMBOLS

E	Young's Modulus of Elasticity (assumed = 30×10^6 psi)
R	Strain gage reading
b	Strain gage constant (-200)
p	Internal pressure - lbs./sq.in.
ϵ_a	Axial strain - in./in.
ϵ_r	Radial strain - in./in.
ϵ_t	Tangential strain - in./in.
ϵ_1	Principal strain - in./in.
σ_a	Axial stress - lbs./sq.in.
σ_r	Radial stress - lbs./sq.in.
σ_t	Tangential stress - lbs./sq.in.
$\sigma_{1,2}$	Principal stresses - lbs./sq.in.
μ	Poisson's ratio - (assumed = 0.3)

INTRODUCTION

This investigation was prompted by certain problems which have arisen in systems employing high pressure piping. The construction of ducting for high speed wind tunnels involves cylindrical intersections of large diameter and similar problems, though on a smaller scale, may be found in various industrial applications. For piping which is highly stressed tangentially it has been the practice to furnish heavy ribs or other devices to take the bending stresses of the elliptical intersection. This procedure ignores bending stiffness of the pipe itself and some doubt has arisen as to the actual necessity for such ribs. Further, in some cases there was evidence that the reinforcing might in reality be harmful to the strength of the joint.

The tests presented here are steps toward a complete investigation of the problem. Some tests of this nature were made preliminary to the design and construction of the 20-inch supersonic wind tunnel of the Jet Propulsion Laboratory (CIT) (Ref. 1). The specimens tested in that project were of various shapes, materials, and Radius/thickness ratios. For the present approach to the problem it was decided to reduce the number of variable parameters to just one--the wall thickness. The steel to be used, the internal diameter, and other specifications were held constant. For this series it was originally planned to make tests on 90-degree elbows of at least four wall thicknesses, but difficulties in the manufacture of suitable specimens and time limitations forced a reduction in scope to only two specimens.

A search was made both in applicable textbooks and in the many engineering publications for previous work, either theoretical or experimental, on this subject. Considerable information was found on pipe bends, pipe elbows, and the like, but nothing on stresses to be found at or near a welded cylindrical intersection. This problem is of a type possessing mixed boundary conditions and as such is very difficult to solve from a purely theoretical approach.

The tests whose results are presented herein were conducted in the Structures Laboratory of the Guggenheim Graduate School of Aeronautics, California Institute of Technology.

EQUIPMENT AND PROCEDURE

The test specimens were made of eight-inch National Extra Strong welded steel pipe, ASTM Spec. 53-47. This steel has a yield point of 30,000 psi. and ultimate strength of 48,000 psi. The pipe was first machined inside and out to remove any eccentricity and to obtain a uniform wall thickness. Inside diameter was held constant for both specimens and was 7.68 inches. The wall thickness of the first specimen was 0.4 inch and the second was 0.3 inch.

After machining, the pipe was cut and welded so as to form a 90-degree elbow as shown in Fig. 6. Care was taken in machining off excess weld metal in the joint in order to have smooth fillets of small radius so that the finished product would approximate as closely as possible a cylindrical intersection machined from a single billet. Standard eight-inch pipe caps were welded on the ends and threaded studs welded in these caps. The studs were drilled and tapped to provide pressure connections and were threaded to receive lugs intended for use in applying either tension or compression across the ends by means of a turnbuckle. The turnbuckle was not used, however. Complete details of manufacture and assembly are shown in Figs. 5 and 6.

Pressure was applied by means of a Blackhawk hand-operated hydraulic pump. Pressure was measured by a standard high pressure gage. The variable resistance wire strain gages used were Baldwin-Southwark A-8 rectangular gages and AR-7 rectangular rosettes. The location and orientation of these gages is shown in Figs. 7, 8, and 9. Other equipment included a potentiometer and Wheatstone Bridge circuit, a switch panel, 6-volt battery, and the necessary wiring and plumbing. The specimen was placed on wooden block supports spaced approximately 6 and 16 inches from each end.

The same procedure was followed in both tests. Within the elastic limit the following procedure was observed:

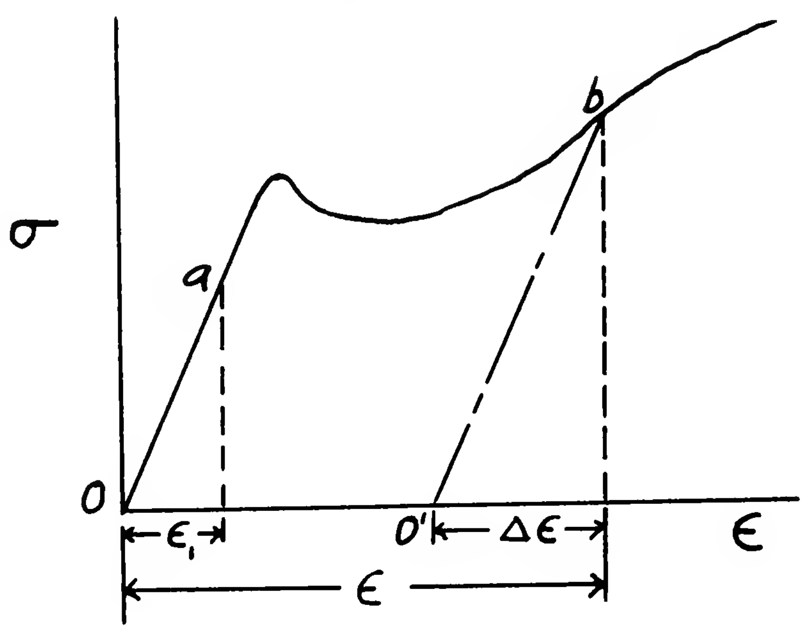
(1) Zero readings were taken on all gages.

(2) Load was applied and load readings taken.

(3) Load was removed and a second zero reading taken.

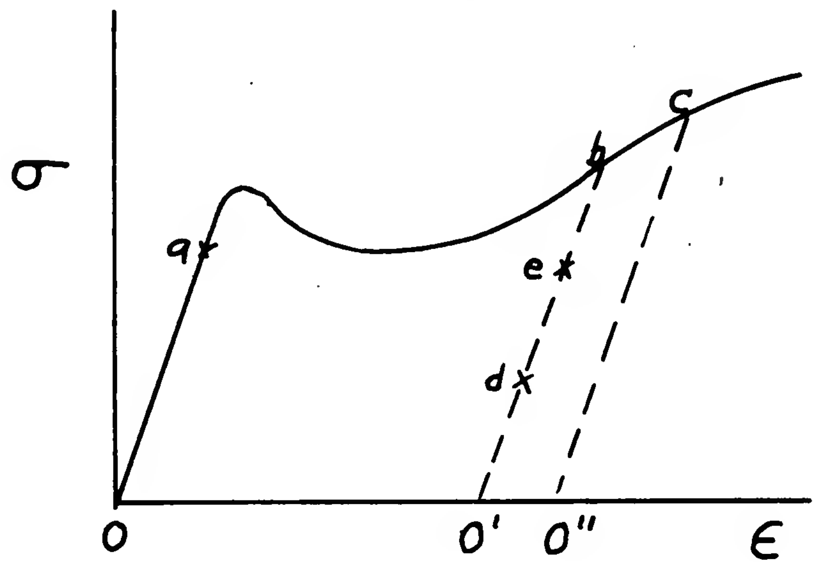
(4) Increased load was applied, readings taken, followed again by zero readings, etc.

After the elastic limit had been exceeded, zero readings were taken only after the load readings. The reason for this can be seen by considering the curve below.



Assume that under the applied load, the metal at some given position reaches point "a" on the stress-strain diagram. This is below the elastic limit and when the load is removed both the stress and the strain (ϵ_1) return to zero. Now if a sufficiently high load to cause yielding is applied, some point "b" on the curve will be reached. When the load is now removed, the line bo' will be followed ending at zero stress but with a permanent set o-o'. This permanent set can be computed by comparing strain gage readings at o and at o'. The strain at point "b" cannot now be referred directly to the zero strain at o but must be referred to the new "zero" at o'. Doing this gives the value of $\Delta\epsilon$ and adding this strain increment to the permanent set o-o' gives the total strain ϵ at point "b".

Theoretically the line bo' of the preceding diagram is parallel to oa. In order to check on the reliability of strain gage readings beyond the specimen elastic limit, this parallelism was utilized by taking readings at points d and e on the way up to point c,



the next higher load reading above b. Since stress was not measured directly, a stress versus strain curve could not be plotted. Points d and e were plotted on the load versus strain curves where the same reasoning as above applies. Therefore it was assumed that if points o', d, e, and b on the load-strain curves plotted a straight line parallel to oa, the strain gages were giving useful readings.

Punch marks were made in the stud in each end cap and a trammel bar and points used to measure the distance between the punch marks both in the unloaded condition and for each loading applied.

At the higher loadings where considerable yielding occurred it was necessary to maintain pressure constant for some time until a condition of equilibrium was reached and readings held substantially constant.

RESULTS AND DISCUSSION

The results of the two series of tests have been plotted on curves of loading versus tangential strain and axial strain for the several strain gage locations. The axial and tangential components were plotted since these were the strain components actually measured and also to facilitate comparison with the curves applying to a straight tube and the curves derived from previous tests on specimens having larger R/t ratios than those used in the present investigation. The principal strains and the principal axis orientation were computed within the elastic limit and are included in the tables. The maximum pressure held by the first specimen (0.4" wall) was 3350. psi. The maximum pressure held by the second specimen was 2950. psi.

The results of the two tests as shown in Tables I - XVIII and Figs. 22 and 27 show that the axial strains at position #5 are only very slightly smaller than the tangential strains at position #9 for all loadings under the elastic limit. Above the elastic limit, however, the tangential strains in the crotch increase much more rapidly than do those at any other point measured. For the locations investigated in these tests then, the critical strains occur in the crotch and are the tangential strains.

The type and location of ruptures obtained in the two tests were almost exactly identical as can be seen in Figs. 2, 4, and 50. In each case the failure was a crack perpendicular to the line of the weld at a distance of 1½" up from the crotch centerline. In both cases audible cracks and snaps were heard at irregular intervals as the internal pressure was increased. In the first test these noises started at a pressure of about 2600 psi and were accompanied by the appearance of fine, hair-line cracks in the weld and perpendicular to the line of the weld as shown in Fig. 50. In the second test no such cracks appeared, but roughened stress lines approximately parallel to the weld appeared in the parent metal near the weld.

In specimen #2, cracks between the parent metal and the weld metal started widening perceptibly at loads below the elastic limit. As in specimen #1, however, when rupture finally occurred, the break was in the weld and at right angles to both the line of the weld and the initial cracks. Since the two breaks were so exactly similar, it seems quite possible that a point of stress concentration existed between positions #6 and #9. This possibility should be investigated in any further tests of this nature. Further evidence of this high stress area was given by the extremely high strains measured at position #6. The tangential gage in the crotch failed fairly early, but up to the time of failure indicated strains even higher than those at position #6.

Rosettes 1, 2, and 4 all were located some distance from the weld. (Fig. 7) The test results from both specimens as plotted in Figs. 10 and 12 show that the tangential strains did not become large until high loadings were applied. When these strains did begin to increase, the magnitudes of the strains and the rates of increase at these three locations remained quite close to each other. The axial strains show no such uniformity but all remained relatively small as compared with the tangential strains. A comparison of strains at these three locations with the theoretical strains in a straight pipe follows: p = 1,000. psi.

I: $\epsilon_{a_{th}} = .0608 \times 10^{-3}$ $\epsilon_{a_1} = .0865 \times 10^{-3}$ $\epsilon_{a_2} = .0318 \times 10^{-3}$ $\epsilon_{a_4} = .0764 \times 10^{-3}$

$\epsilon_{t_{th}} = .2586 \times 10^{-3}$ $\epsilon_{t_1} = .1896 \times 10^{-3}$ $\epsilon_{t_2} = .2694 \times 10^{-3}$ $\epsilon_{t_4} = .3274 \times 10^{-4}$

II: $\epsilon_{a_{th}} = .0822 \times 10^{-3}$ $\epsilon_{a_1} = .1392 \times 10^{-3}$ $\epsilon_{a_2} = .0299 \times 10^{-3}$ $\epsilon_{a_4} = .0946 \times 10^{-3}$

$\epsilon_{t_{th}} = .3490 \times 10^{-3}$ $\epsilon_{t_1} = .3305 \times 10^{-3}$ $\epsilon_{t_2} = .3048 \times 10^{-3}$ $\epsilon_{t_4} = .4313 \times 10^{-3}$

Previous testing and experience had indicated an appreciable bending effect in this type of joint as evidenced by an opening of the original ninety-degree angle. For both specimens tested in this investigation no measurable amount of bending was found until the rupture point was reached. This would seem to indicate, at least for R/t ratios close to these, that the bending effects are much less important than had been believed and that for a properly welded joint there is sufficient inherent stiffness to eliminate the necessity for stiffening webs.

In making these tests it was desirable to get strain readings insofar as possible right up to the point of rupture. It was not known to what extent the strain gage readings would prove reliable once the yield point of the steel was passed. As a result of these tests it appears that the gage readings gave reliable qualitative results throughout the range of readings. Since the physical properties of the strain gages themselves are not known, it is impossible to state definitely at what total strain the gage accuracy underwent a change. Quantitatively, therefore, the results are of an unknown degree of accuracy. It is probable that the close agreement of the curves for the two test specimens at each location would not have been obtained if the gages had become unreliable at the high loadings. In order to check the gage action at the higher loads, intermediate readings were taken between the unloaded condition and the high loads as previously explained in "PROCEDURE". These points as plotted in Figs. 16, 19, 22, 23, 25, 27, 28, and 31 give a straight line parallel to that obtained within the elastic region and the gages were therefore assumed to be giving useful readings. At some locations gages were broken under high loadings. This fact was immediately apparent due to the inability to obtain a balance in the bridge circuit.

From the strain readings taken, stresses at the various locations were computed within the elastic region and recorded in Tables I-XVIII. Since the strain gages can measure only two-dimensional strains, stresses were computed using two-dimensional theory. The third-dimensional strains while known to be present could not be accounted for in these tests. When yielding first occurred anywhere in the specimen, the resultant permanent deformation imposed residual stresses throughout the specimen when the load was removed. This was shown by an apparent permanent set indicated by all gages at approximately the same loading even though local load stresses had not risen sufficiently to reach the yield stress of the metal. This is the reason why all the load-strain curves deviate from a linear relation at about the same loading. Above the elastic limit the strains measured cannot be transformed to other axes since the usual transformation equations are invalid outside the elastic range. Considerable work is now being done toward developing stress and strain relations for use in the plastic region (Ref. 2), but no attempt was made to apply any of those theories here.

The curves plotted from the results of the tests on the two specimens agree quite closely with three exceptions. The tangential strain curves at position #8 diverge, and the axial strain curves for positions 7 and 8 also diverge. The reason for this divergence is not known but may be due to the change in thickness ratio. Further tests on specimens of various R/t ratios would indicate whether the divergence is a trend established by the change in wall thickness.

For the wall thicknesses used in these tests it is believed that gravity effects were of very minor importance. In any further tests using thin-walled specimens of similar dimensions it would be better to provide supports which distribute the load uniformly along the length of the specimen rather than supporting it at four points as was done here.

Considering the fact that first yielding occurred at approximately 54% of maximum load in the first test and at about 42% of maximum load in the second test, use of the theory of limit design in actual construction is indicated. At the same time the large difference in yield loads observed compared with the theoretical yield load for a straight pipe should be considered.

Specimen I: $P_{yield-str.\,pipe} = 3288.\ psi.$

$P_{yield-actual} = 1800.\ psi.$

Specimen II: $P_{yield-str.\,pipe} = 2435.\ psi.$

$P_{yield-actual} = 1200.\ psi.$

This shows a reduction in strength of 45% for the first specimen, and 51% for the second.

A measurement of the intersection cross section shape was made after rupture in the tests described in Ref. 1. The original elliptical cross section was found to have been deformed into an egg shape with the greatest outward deviation located approximately midway between the crotch and the 90 degree point of the intersection. This contour is typical of deformations suffered by such intersections and was observed in the present tests.

Figs. 32 to 49 were plotted to show the measured strain distribution both along the cylinder axis and along the elliptical intersection. Examination of these figures (for instance Fig. 39 and Fig. 40) shows that axial strains are highest at position #5 and tangential strains are highest in the crotch. All strains are relatively low at the outside of the elbow for all loadings. There are relatively high tangential and axial strains in the region between positions 6 and 9 so that the principal strains will be highest in that region.

CONCLUSIONS

1. The results of this investigation indicate that the highest stress concentration in a right angle cylindrical intersection under internal pressure occurs at an angle of about 14.5 degrees from the crotch centerline measured in the plane of the ellipse.

2. The critical stress causing rupture is the tangential stress in the plane of the ellipse.

3. For the R/t ratios tested, the strength reduction as compared with a straight closed cylinder is approximately 50%.

4. It appears probable that bending effects for these thick walled cylinders are of relatively minor importance.

RECOMMENDATIONS

1. An analysis of the tangential stresses in the plane of the elliptical intersection should be made.

2. A study should be made of the variation of these tangential stresses through the wall thickness.

3. Analytical studies of bending effects and shearing stresses should be made.

4. In any further experimental work, the critical area as determined in this investigation should be thoroughly examined by strain gages or other means.

5. Further experimental work should check on the differing axial strains observed in the two specimens on the outside of the elbow.

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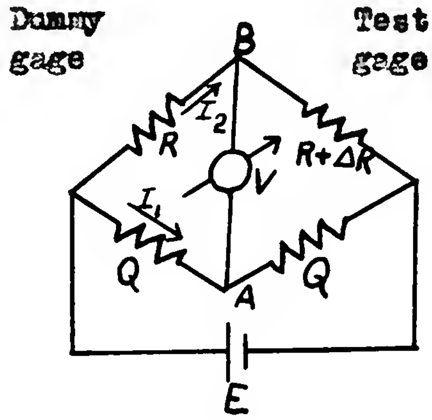
REDUCTION OF STRAIN GAGE DATA

The test gage mounted on the specimen and a dummy gage mounted on identical, unstrained material are included in a Wheatstone Bridge circuit. The opposite sides of the circuit are two precision resistances of magnitude Q.



Under load the potentiometer is varied so that no current flows between points A and B. We wish to determine the relation between the voltage V, across AB and the unit strain, ϵ, in the test specimen.

From the circuit diagram, we determine that

$$I_1(2Q) = E \qquad I_2\,(2R + \Delta R) = E \qquad V = I_1 Q - I_2 R$$

Hence

$$V = \frac{E}{2} - \frac{ER}{2R+\Delta R} = \frac{E}{4}\frac{\Delta R}{R}\left[1 + \frac{\Delta R}{2R}\right]^{-1} \approx \frac{E}{4}\,\frac{\Delta R}{R}$$

To eliminate the ratio $\Delta R/R$, the following relation for resistivity of a conductor is employed.

$$R = K\frac{L}{A}$$

where K is a resistivity constant, L the length of the conductor, and A its cross-sectional area. Then

$$\ln R = \ln K + \ln L - \ln A$$

Hence

$$\frac{\Delta R}{R} = \frac{\Delta L}{L} - \frac{\Delta A}{A}$$

For a cylindrical conductor

$$\frac{\Delta A}{A} = 2\frac{\Delta r}{r} = -2\nu\frac{\Delta L}{L} = -2\nu\epsilon$$ r is the radius of the cross section

Therefore

$$\frac{\Delta R}{R} = (1 + 2\nu)\epsilon$$

ν is the Poisson's ratio for the strain gage material.

Substituting directly into the equation for the voltage reading V,

Hence

$$v = \frac{E}{4}(1 + 2\nu)\epsilon$$

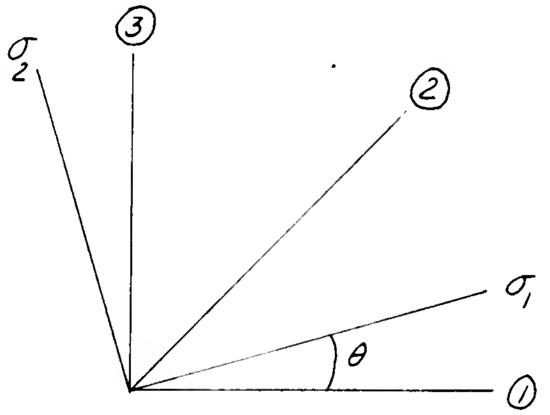
$$\epsilon = \frac{4v}{(1 + 2\nu)E}$$

This equation is usually employed in the form

$$\epsilon = \frac{4\ (\text{milli volts})}{(\text{gage factor})(\text{battery reading})}$$

where ϵ is obtained in inches per inch times 10^{-3}.

Within the elastic region the average of zero readings taken before and after loading was used in getting the gage readings. Application of gage factor and battery reading gave apparent strains in the case of the rosettes, so these readings were further corrected as follows:



$$\Delta\epsilon_1 = R_1 - \frac{1}{b}R_3$$

$$\Delta\epsilon_2 = 1.02\,R_2 - \frac{1}{b}(R_1+R_3)$$

$$\Delta\epsilon_3 = R_3 - \frac{1}{b}R_1$$

b = -200 where b is a factor furnished by the manufacturer for each gage lot.

Having the strains at a given point, the axial and tangential stresses were computed from the usual two-dimensional equations:

$$\sigma_a = \frac{E}{1-\mu^2}\left[\epsilon_a + \mu\epsilon_t\right] \qquad \sigma_t = \frac{E}{1-\mu^2}\left[\epsilon_t + \mu\epsilon_a\right]$$

These stresses could be computed only up to the load where yielding first occurred at any point in the specimen.

To compute principal stresses the following equations were used:

$$\sigma_{1,2} = \frac{E}{2(1-\mu)(1+b)}\left[(R_1+R_3) \pm \frac{(1-\mu)(1+b)}{(1+\mu)(1-b)}\cdot r\right]$$

where $r = \left|\dfrac{R_1+R_3-2R_2}{\sin 2\theta}\right|$

$$\tan 2\theta = -\frac{R_1+R_3-2R_2}{R_1-R_3}$$

Having the principal stresses, principal strains could then be computed.

$$\epsilon_1 = \frac{1}{E}(\sigma_1 - \mu\sigma_2)$$

Principal stresses and strains were computed only within the elastic region.

For test number one it was necessary to transform the measured strains at positions 5 and 7 to get the tangential strains due to the orientation of those two gages. (Fig. 8). This was done by using Mohr's circle. The transformation was performed only within the elastic region.

TABLE I

VARIATION OF TANGENTIAL AND AXIAL STRAINS WITH VARIATION OF INTERNAL PRESSURE

Test I — Position #1 — Gages 2,3

	← R →			← Δ ϵ →				← σ →			← ϵ →	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
500	.0430	.1133	-	.0436	.1135	-	-	-	2560	4170	.0436	.1135
750	.0645	.1416	-	.0652	.1419	-	-	-	3550	5320	.0652	.1419
1000	.0856	.1892	-	.0865	.1896	-	-	-	4725	7100	.0865	.1896
1250	.1068	.2381	-	.1080	.2386	-	-	-	5910	8930	.1080	.2386
1500	.1284	.2890	-	.1298	.2896	-	-	-	7140	10830	.1298	.2896
1600	.1325	.3003	-	.1340	.3010	-	-	-	7400	11240	.1340	.3010
1700	.1398	.3160	-	.1414	.3167	-	-	-	7800	11840	.1414	.3167
1800	.1468	.3335	-	.1485	.3342	-	-	-	-	-	.1460	.7388
1900	.1546	.3552	-	.1564	.3560	-	-	-	-	-	.1704	.7403
2000	.1627	.3856	-	.1646	.3864	-	-	-	-	-	.2075	.7209
2050	.1674	.3899	-	.1693	.3907	-	-	-	-	-	.2227	.7092
2150	.1809	.4807	-	.1833	.4816	-	-	-	-	-	.2449	.7873
750	.0616	.1480	-	.0623	.1483	-	-	-	-	-	.1239	.4540
1700	.1420	.3337	-	.1437	.3344	-	-	-	-	-	.2053	.6401
2200	.1850	.4263	-	.1871	.4356	-	-	-	-	-	.2581	.7481
2300	.1941	.4474	-	.1963	.4484	-	-	-	-	-	.2861	.7438
2400	.1993	.4922	-	.2018	.4932	-	-	-	-	-	.2938	.8333
2500	.2135	.4801	-	.2159	.4812	-	-	-	-	-	.2953	.9880
2600	.0804	.3915	-	.0824	.3955	-	-	-	-	-	.3602	2.2024
2800	.2096	.5993	-	.2126	.6003	-	-	-	-	-	.9139	4.1237
3000	.2146	.6726	-	.2161	.6937	-	-	-	-	-	1.1340	5.5106
3250	.2411	.7970	-	.2451	.7982	-	-	-	-	-	1.3111	6.8218

Pressures and stresses in lb./sq.in. Strains given in inches per inch x 10^3

TABLE II

Test I

Position #2

Gages 4,5,6

	R			ΔЄ				σ			Є	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
500	.0181	.1318	.0696	.0188	.1319	.1322	2-42	4540	1889	4530	.0188	.1319
750	.0234	.1908	.1052	.0244	.1909	.1909	0-39	6534	2690	6540	.0244	.1909
1000	.0305	.2693	.1489	.0318	.2694	.2690	0-15	9189	3707	9177	.0318	.2694
1250	.0474	.3300	.1780	.0480	.3302	.3306	2-10	11382	4855	11340	.0480	.3302
1500	.0576	.4050	.2194	.0596	.4053	.4058	1-58	13964	5973	13920	.0596	.4053
1600	.0522	.4300	.2360	.0543	.4303	.4302	0-47	14722	6045	14690	.0543	.4303
1700	.0531	.4600	.2510	.0554	.4603	.4601	0-47	15719	6380	15700	.0554	.4603
1800	.0580	.4807	.2619	.0604	.4810	-	-	-	-	-	.0546	.4994
1900	.0657	.4976	.2736	.0682	.4979	-	-	-	-	-	.0512	.5335
2000	.0644	.5211	.2866	.0670	.5214	-	-	-	-	-	.0448	.6029
2050	.0690	.5319	.2935	.0717	.5322	-	-	-	-	-	.0379	.6365
2150	.0608	.5297	.2921	.0634	.5300	-	-	-	-	-	.0191	.8161
750	.0197	.2410	.1035	.0209	.2411	-	-	-	-	-	-.0234	.5272
1700	.0528	.4400	.2409	.0550	.4403	-	-	-	-	-	.0107	.7264
2200	.0693	.5643	.3106	.0721	.5646	-	-	-	-	-	.0302	.8649
2300	.0718	.4518	.2357	.0741	.4522	-	-	-	-	-	.0188	1.5388
2400	.0754	.5411	.2932	.0781	.5415	-	-	-	-	-	.0171	2.1654
2500	.0878	.5583	.3058	.0906	.5587	-	-	-	-	-	.0362	2.7001
2600	.0955	.6440	.3646	.0987	.6445	-	-	-	-	-	-.0780	3.8779
2800	.1176	.6682	.3796	.1209	.6688	-	-	-	-	-	-.2543	5.5926
3000	.1336	.8351	.4486	.1378	.8358	-	-	-	-	-	-.4013	7.8630
3250	.1358	.9513	.5011	.1406	.9520	-	-	-	-	-	-.4910	9.4319

TABLE III

Test I | Position #3 | Gages 7,8,9

Press.	R Axial	R Tang.	R Diag.	Δε Axial	Δε Tang.	Princ.	θ	Princ.	σ Axial	σ Tang.	ε Axial	ε Tang.
500	-0.0127	0.1562	0.0623	-0.0119	0.1561	.1566	86-59	5041	1151	5025	-0.0119	0.1561
750	-0.0167	0.2350	0.0910	-0.0155	0.2349	.2362	85-54	7621	1813	7595	- .0155	0.2349
1000	-0.0161	0.3273	0.1320	- .0145	0.3272	.3289	86-06	10684	2760	10650	- .0145	0.3272
1250	-0.0273	0.4080	0.1487	- .0253	0.4079	.4117	87-17	13286	3200	13200	- .0253	0.4079
1500	-0.0368	0.4970	0.1875	-0.0343	0.4968	.5002	85-28	16118	3775	16050	- .0343	0.4968
1600	- .0397	0.5420	0.2098	-0.0370	0.5418	.5446	85-57	17561	4135	17500	- .0370	0.5418
1700	- .0487	0.5810	0.2221	-0.0458	0.5808	.5836	86-01	18760	4235	18700	- .0458	0.5808
1800	- .0421	0.6126	0.2367	- .0390	.6124	-	-	-	-	-	- .2812	.9485
1900	- .0007	0.5102	.2010	.0019	.5102	-	-	-	-	-	- .4396	1.2756
2000	- .0641	0.7296	.2511	- .0605	.7293	-	-	-	-	-	- .7452	3.1196
2050	- .0600	0.6597	.2101	- .0567	.6594	-	-	-	-	-	- .7604	3.2577
2150	- .0648	0.7677	.2941	- .0610	.7674	-	-	-	-	-	-1.0346	5.3378
750	- .0176	0.2486	.1007	- .0164	.2484	-	-	-	-	-	- .9900	4.8188
1700	- .0552	0.6031	.2356	- .0522	.6028	-	-	-	-	-	-1.0258	5.1732
2200	- .0888	0.8357	.3172	- .0846	.8353	-	-	-	-	-	-1.0363	5.3448
2300	- .0333	0.9655	.3673	- .0285	.9653	-	-	-	-	-	-1.3724	8.2622
2400	- .0485	0.9982	.3958	- .0435	.9980	-	-	-	-	-	-1.8190	10.7686
2500	- .0661	1.0539	.4339	- .0608	1.0536	-	-	-	-	-	-2.2653	12.7903
2600	- .0889	1.1337	.4893	- .0832	1.1333	-	-	-	-	-	-2.9376	15.1911
2800	- .0841	NG	.5448	-	-	-	-	-	-	-	-	-
3000	- .1180	NG	.6350	-	-	-	-	-	-	-	-	-
3250	- .1311	NG	NG	-	-	-	-	-	-	-	-	-

TABLE IV

Test I | Position #4 | Gages 10,11,12

Press.	R Axial	R Tang.	R Diag.	Δϵ Axial	Δϵ Tang.	Δϵ Princ.	θ	σ Princ.	σ Axial	σ Tang.	ϵ Axial	ϵ Tang.
500	.0369	.1582	.1411	.0377	.1584	.1723	-17-51	5916	2805	5,590	.0377	.1584
750	.0565	.2183	.2070	.0576	.2186	.2443	-20-22	8369	4060	7,840	.0576	.2186
1000	.0748	.3270	.2862	.0764	.3274	.3533	-17-03	12148	5750	11,530	.0764	.3274
1250	.0996	.3977	.3467	.1016	.3982	.4274	-16-40	14808	7290	14,120	.1016	.3982
1500	.1150	.4890	.4240	.1174	.4896	.5257	-16-34	18136	8720	17,280	.1174	.4896
1600	.1502	.5220	.4620	.1528	.5228	.5611	-17-04	19632	10190	18,710	.1528	.5228
1700	0.1549	0.5520	0.4820	.1577	.5528	.5905	-16-28	20655	10650	19,780	.1577	.5528
1800	.1429	.5841	.5168	.1458	.5848	-	-	-	-	-	.1562	.5833
1900	.1595	.6040	.5370	.1625	.6048	-	-	-	-	-	.1532	.6169
2000	.1650	.6164	.5539	.1681	.6172	-	-	-	-	-	.1345	.7743
2050	.1738	.6133	.5646	.1769	.6142	-	-	-	-	-	.1422	.8531
2150	.1893	.6289	.5878	.1924	.6298	-	-	-	-	-	.1570	1.3555
750	.0650	.2287	.2057	.0661	.2290	-	-	-	-	-	.0302	0.9547
1700	.1481	.5132	.4655	.1507	.5139	-	-	-	-	-	.1148	1.2396
2200	.1944	.6584	.5990	.1977	.6554	-	-	-	-	-	.1725	1.3850
2300	.1821	.5772	.5305	.1850	.5781	-	-	-	-	-	.4297	2.0265
2400	.2165	.6072	.5714	.2185	.6083	-	-	-	-	-	.7248	2.7650
2500	.2469	.6392	.6210	.2501	.6322	-	-	-	-	-	.9061	3.3265
2600	.2667	.7040	.6368	.2702	.7053	-	-	-	-	-	1.0969	3.9296
2800	.2931	.7206	.652	.2967	.7221	-	-	-	-	-	1.5359	5.2937
3000	.3268	.7730	.6833	.3307	.7746	-	-	-	-	-	2.1318	6.9961
3250	.3630	.8555	.6837	.3673	.8573	-	-	-	-	-	2.6431	8.6785

TABLE V

Test I — Position #5 — Gages 13,14,15

	R			ΔЄ				σ			Є	
Press.	Axial	Along Weld	Normal to Weld	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
500	0.2150	0.1288	0.2170	0.2210	0.1293	.2344	66-45	8847	8474	6420	0.2210	.1293
750	0.3265	0.1955	0.3286	0.3356	0.1970	.3555	67-01	13415	12816	9758	.3356	.1970
1000	0.4380	0.2633	0.4440	.4503	0.2655	.4783	66-31	18070	17306	13158	.4503	.2655
1250	0.5324	0.3163	0.5420	.5473	.3190	.5834	66-16	21996	21076	15892	.5473	.3190
1500	0.6515	0.3854	0.6590	0.6698	.3887	.7120	66-43	26814	25634	19350	.6698	.3887
1600	0.7020	0.415	0.7140	0.7216	.4185	.7694	66-19	28979	27748	20880	.7216	.4185
1700	0.7370	0.4330	0.7580	0.7576	.4343	.8128	65-32	30596	29381	21917	.7576	.4343
1800	0.7797	0.4558	0.7959	.8016	.4599	-	-	-	-	-	.8933	.4476
1900	0.8272	0.4849	0.8498	.8504	.4892	-	-	-	-	-	1.1027	.4711
2000	0.8738	0.5068	0.8907	.8983	.5115	-	-	-	-	-	1.3280	.4510
2050	0.8844	0.5203	0.9001	.9092	.5249	-	-	-	-	-	1.4455	.4866
2150	0.9243	0.5438	0.9376	.9502	.5486	-	-	-	-	-	1.8839	.6597
750	0.3123	0.1795	0.3096	.3209	.1811	-	-	-	-	-	1.2546	.2922
1700	0.7164	0.4150	0.7269	.7364	.4187	-	-	-	-	-	1.6701	.5298
2200	0.9250	0.5356	0.9381	.9509	.5404	-	-	-	-	-	1.9229	.6762
2300	0.9648	0.5649	1.0095	.9920	.5700	-	-	-	-	-	2.9586	1.1058
2400	1.0026	0.5841	1.0292	1.0307	.5615	-	-	-	-	-	3.6251	1.3387
2500	1.0108	0.5920	1.0229	1.0391	.7058	-	-	-	-	-	4.2130	1.7047
2600	1.0683	0.6175	1.0510	1.0980	.6229	-	-	-	-	-	5.0013	1.8820
2800	1.0585	0.6775	1.0585	1.0884	.6829	-	-	-	-	-	6.8464	2.4601
3000	1.0871	0.7703	1.0629	1.1180	.7770	-	-	-	-	-	8.9184	2.9686
3250	1.1626	0.9040	1.0636	1.1956	.9095	-	-	-	-	-	10.7605	3.5506

TABLE VI

Test I | Position #6 | Gages 16,17,18

	R			Δε				σ			ε	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
500	-.0101	.2050	.0429	-.0091	.2045	.2180	13-28	6970	1725	6650	-.0091	.2045
750	-.0127	.3055	.0408	-.0112	.3054	.3371	16-47	10691	2650	9950	-.0112	.3054
1000	-.0141	0.4170	0.0554	-.0120	.4169	.4615	17-04	14655	3730	13640	-.0120	.4169
1250	-.0126	0.5090	0.0717	-.0101	.5089	.5627	17-03	17920	4700	16690	-.0101	.5089
1500	-.0126	.6235	.0873	-.0095	.6234	.6907	17-14	22012	5850	20470	-.0095	.6234
1600	-.0093	0.6720	0.0959	-.0059	.6720	.7450	17-20	23780	6450	22100	-.0059	.6720
1700	-.0162	0.7100	0.0987	-.0126	.7099	.7862	17-11	25042	6610	23270	-.0126	.7099
1800	-.0126	0.7495	0.1074	-.0089	.7494	-	-	-	-	-	.0332	.6988
1900	-.0073	0.8001	0.1144	-.0033	.8001	-	-	-	-	-	.0883	.8339
2000	.0056	0.8535	0.1308	.0099	.8535	-	-	-	-	-	.2527	1.0209
2050	.0053	0.8551	0.1434	.0096	.8551	-	-	-	-	-	.2884	.8756
2150	.0260	0.9246	0.1562	.0306	.9247	-	-	-	-	-	.6063	1.8557
750	.0063	.2957	.0547	.0078	.2957	-	-	-	-	-	.5835	1.2267
1700	.0253	.8017	.1281	.0293	.8018	-	-	-	-	-	.6050	1.7328
2200	.0395	.9467	.1609	.0442	.9469	-	-	-	-	-	.5930	1.9099
2300	.0632	1.0085	.1958	.0682	1.0088	-	-	-	-	-	1.3146	3.8451
2400	.1191	1.1052	.2224	.1246	1.1058	-	-	-	-	-	1.8874	5.2142
2500	.1674	1.1740	.2418	.1733	1.1748	-	-	-	-	-	2.2353	6.2563
2600	.2271	1.2371	.2678	.2333	1.2382	-	-	-	-	-	2.5718	7.4738
2800	.3148	1.3137	.3051	.3214	1.3153	-	-	-	-	-	2.9714	9.8491
3000	.3834	1.3148	.3416	.3900	1.3167	-	-	-	-	-	2.7935	12.0549
3250	.3106	NG	.3779	.3106	-	-	-	-	-	-	-	-

TABLE VII

Test I Position #7 Gages 19,20,21

	R			Δ ε				σ			ε	
Press.	Axial	Along Weld	Normal to Weld	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
500	.0700	-.0385	.0868	.0716	-.0381	.1015	-63-06	2823	2479	-399	.0716	-.0381
750	.1045	-.0615	.1253	.1069	-.0608	.1451	-63-55	4090	3518	-770	.1069	-.0608
1000	.1340	-.0818	.1759	.1372	-.0809	.2019	-62-06	5594	4983	-931	.1372	-.0809
1250	.1732	-.1040	.2082	.1772	-.1029	.2488	-64-00	6779	5827	-1339	.1772	-.1029
1500	.2276	-.1344	.2633	.2328	-.1386	.3206	-64-42	8681	7469	-1917	.2328	-.1386
1600	.2382	-.1400	.2780	.2437	-.1442	.3368	-64-30	9144	7901	-1957	.2437	-.1442
1700	.2477	-.1452	.2900	.2534	-.1438	.3508	-64-30	9534	8113	-1881	.2534	-.1438
1800	.2549	-.1508	.3186	.2608	-.1492	-	-	-	-	-	.3051	-.1899
1900	.2690	-.1542	.3344	.2753	-.1525	-	-	-	-	-	.3469	-.2175
2000	.2753	-.1650	.3544	.2817	-.1633	-	-	-	-	-	.4062	-.3066
2050	.2941	-.1581	.3635	.3010	-.1500	-	-	-	-	-	.4235	-.3159
2150	.3064	-.1632	.3728	.3135	-.1614	-	-	-	-	-	.4603	-.4078
750	.1011	-.0599	.1220	.1034	-.0623	-	-	-	-	-	.2502	-.3087
1700	.2411	-.0599	.2942	.2471	-.0584	-	-	-	-	-	.3939	-.3048
2200	.3175	-.1641	.3826	.3249	-.1622	-	-	-	-	-	.4706	-.4109
2300	.3123	-.1560	.3890	.3197	-.1520	-	-	-	-	-	.4601	-.5308
2400	.3228	-.1614	.4048	.3304	-.1595	-	-	-	-	-	.4598	-.6319
2500	.3268	-.1598	.4109	.3346	-.1578	-	-	-	-	-	.4973	-.7219
2600	.3380	-.1544	.4311	.3462	-.1523	-	-	-	-	-	.5333	-.8354
2800	.3486	-.1458	.4686	.3572	-.1435	-	-	-	-	-	.6613	-1.0814
3000	.3630	-.1373	.5138	.3722	-.1344	-	-	-	-	-	.7355	-1.3375
3250	.4287	-.1021	.5800	.4397	-.0991	-	-	-	-	-	.8197	-1.4149

TABLE VIII

Test I | Position #8 | Gages 22&23

	R			$\Delta\epsilon$				σ			ϵ	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
500	.0058	-.0613	-	.0058	-.0613	.0058	0	-415	-415	-1965	.0058	-.0613
750	.0054	-.0875	-	.0054	-.0875	.0054	0	-686	-686	-2832	.0054	-.0875
1000	.0018	-.1263	-	.0018	-.1263	.0018	0	-1190	-1190	-4148	.0018	-.1263
1250	.0118	-.1675	-	.0118	-.1675	.0118	0	-1266	-1266	-5407	.0118	-.1675
1500	.0218	-.1956	-	.0218	-.1956	.0218	0	-1216	-1216	-6235	.0218	-.1956
1600	.0352	-.2100	-	.0352	-.2100	.0352	0	-916	-916	-6574	.0352	-.2100
1700	.0419	-.2280	-	.0419	-.2280	.0419	0	-874	-874	-7102	.0419	-.2280
1800	.0417	-.2425	-	.0417	-.2425	-	-	-	-	-	.1019	-.2680
1900	.0474	-.2563	-	.0474	-.2563	-	-	-	-	-	.1469	-.2941
2000	.0597	-.2696	-	.0597	-.2696	-	-	-	-	-	.2184	-.3303
2050	.0640	-.2696	-	.0640	-.2696	-	-	-	-	-	.2329	-.3382
2150	.0720	-.2891	-	.0720	-.2891	-	-	-	-	-	.3098	-.3850
750	-.0003	-.0825	-	-.0003	-.0825	-	-	-	-	-	.2375	-.1784
1700	.0283	-.2000	-	.0283	-.2000	-	-	-	-	-	.2661	-.2959
2200	.0646	-.2606	-	.0646	-.2606	-	-	-	-	-	.3148	-.3556
2300	.0789	-.2942	-	.0789	-.2942	-	-	-	-	-	.4184	-.4651
2400	.0903	-.3029	-	.0903	-.3092	-	-	-	-	-	.5437	-.6020
2500	.1060	-.3259	-	.1060	-.3259	-	-	-	-	-	.7146	-.8523
2600	.1161	-.3248	-	.1161	-.3248	-	-	-	-	-	.7247	-.8512
2800	.1401	-.3318	-	.1401	-.3318	-	-	-	-	-	.9385	-1.2150
3000	.1855	-.3549	-	.1855	-.3549	-	-	-	-	-	1.1440	-1.7719
3250	.2273	-.3218	-	.2273	-.3218	-	-	-	-	-	1.2880	-2.0626

TABLE IX

Test I **Position #9** **Gages 1-24**

	R			Δε				σ			ε	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
500	0.0468	0.2245	-	0.0468	0.2245	0.2245	090	7860	3762	7860	.0468	.2245
750	0.0646	0.3290	-	0.0646	0.3290	0.3290	090	11500	5385	11500	.0646	.3290
1000	0.0585	0.4560	-	0.0585	0.4560	0.4560	090	15600	6440	15600	.0585	.4560
1250	0.1178	0.5720	-	0.1178	0.5720	0.5720	090	20000	9535	20000	.1178	.5720
1500	0.1340	0.6980	-	0.1340	0.6980	0.6980	090	24300	11320	24300	.1340	.6980
1600	0.1235	0.7580	-	0.1235	0.7580	0.7580	090	26200	11560	26200	.1235	.7580
1700	0.1310	0.8120	-	0.1310	0.8120	0.8120	090	28050	12350	28050	.1310	.8120
1800	0.1441	0.8602	-	.1441	0.8602	-	-	-	-	-	.1246	1.0058
1900	0.1366	0.9786	-	.1366	0.9786	-	-	-	-	-	.1843	2.0139
2000	0.1198	1.0962	-	.1198	1.0962	-	-	-	-	-	.2643	3.7938
2050	0.1084	1.1037	-	.1084	1.1037	-	-	-	-	-	.3632	4.1425
2150	0.1140	1.1809	-	.1140	1.1809	-	-	-	-	-	.5995	6.6369
750	0.0346	.3310	-	.0346	.3310	-	-	-	-	-	.5201	5.7870
1700	.0958	.8170	-	.0958	.8170	-	-	-	-	-	.5813	6.2730
2200	.1198	1.0619	-	.1198	1.0619	-	-	-	-	-	.5911	6.3979
2300	.0827	NG	-	.0827	-	-	-	-	-	-	.9537	-
2400	.1373	NG	-	.1373	-	-	-	-	-	-	1.1431	-
2500	.1609	NG	-	.1609	-	-	-	-	-	-	1.1530	-
2600	.1669	NG	-	.1669	-	-	-	-	-	-	1.0149	-
2800	.1644	NG	-	.1644	-	-	-	-	-	-	.4478	-
3000	.1006	NG	-	.1006	-	-	-	-	-	-	-.2094	-
3250	.0175	NG	-	.0175	-	-	-	-	-	-	-.6431	-

TABLE NO. X

VARIATION OF TANGENTIAL AND AXIAL STRAINS WITH VARIATION OF INTERNAL PRESSURE

Test II — Position #1 — Gages 2,3

	R			$\Delta\epsilon$				σ			ϵ	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
400	.0600	.1385	-	.0670	.1388	-	-	-	3580	5239	.0670	.1388
600	.0815	.1970	-	.0825	.1974	-	-	-	4672	7326	.0825	.1974
800	.1142	.2680	-	.1155	.2686	-	-	-	6465	9996	.1155	.2686
1000	.1376	.3298	-	.1392	.3305	-	-	-	7860	12275	.1392	.3305
1100	.1535	.3677	-	.1553	.3685	-	-	-	8767	13686	.1553	.3685
1200	.1657	.4020	-	.1677	.4028	-	-	-	-	-	.1795	.3831
1250	.1724	.4182	-	.1745	.4191	-	-	-	-	-	.1905	.3906
1300	.1848	.4316	-	.1870	.4325	-	-	-	-	-	.2070	.3978
500	.0705	.1632	-	.0713	.1636	-	-	-	-	-	.0913	.1289
900	.1254	.3019	-	.1269	.3025	-	-	-	-	-	.1469	.2678
1400	.1940	.4794	-	.1964	.4804	-	-	-	-	-	.2531	.3806
1600	.2226	.5814	-	.2255	.5825	-	-	-	-	-	.3474	.3389
600	.0869	.2171	-	.0880	.2175	-	-	-	-	-	.2099	-.0261
1200	.1718	.4421	-	.1740	.4430	-	-	-	-	-	.2959	.1994
1800	.1989	.6038	-	.2019	.6048	-	-	-	-	-	.6174	1.7911
2000	.2622	.8185	-	.2663	.8198	-	-	-	-	-	1.1349	4.1168
2200	.2623	.9078	-	.2668	.9091	-	-	-	-	-	1.4475	6.6002
2400	.2727	1.0532	-	.2780	1.0546	-	-	-	-	-	1.7004	9.4359
2600	.2848	1.1135	-	.2904	1.1149	-	-	-	-	-	1.8471	12.5249
2800	.2852	NG	-	-	-	-	-	-	-	-	-	-

Pressures and stresses in lb./sq.in. Strains given in inches per inch x 10^3

TABLE XI

Test II | Position #2 | Gages 4,5,6

Press.	R Axial	R Tang.	R Diag.	ΔЄ Axial	ΔЄ Tang.	Princ.	θ	σ Princ.	σ Axial	σ Tang.	Є Axial	Є Tang.
400	.0112	.1296	.0739	.0118	.1297	.1296	-1-28	4401	1672	4392	.0118	.1297
600	.0172	.1824	.1164	.0181	.1825	.1841	-5-41	6234	2404	6195	.0181	.1825
800	.0228	.2475	.1564	.0240	.2476	.2497	-5-21	8450	3241	8401	.0240	.2476
1000	.0284	.3047	.1918	.0299	.3048	.3070	-5-11	10397	3999	10346	.0299	.3048
1100	.0307	.3374	.2152	.0324	.3376	.3408	-5-45	11524	4408	11450	.0324	.3376
1200	.0358	.3708	.2357	.0377	.3710	-	-	-	-	-	.0247	.3668
1250	.0375	.3804	.2408	.0394	.3806	-	-	-	-	-	.0246	.3797
1300	.0375	.3944	.2456	.0395	.3946	-	-	-	-	-	.0216	.3968
500	.0140	.1506	.0941	.0148	.1507	-	-	-	-	-	-.0031	.1529
900	.0253	.2773	.1742	.0267	.2774	-	-	-	-	-	.0088	.2796
1400	.0392	.4182	.2618	.0413	.4184	-	-	-	-	-	.0087	.4508
1600	.0443	.4806	.3925	.0467	.4808	-	-	-	-	-	-.0148	.6006
600	.0166	.1751	.1109	.0175	.1752	-	-	-	-	-	-.0440	.2950
1200	.0296	.3525	.2184	.0314	.3526	-	-	-	-	-	-.0301	.4724
1800	.0653	.5121	.3289	.0679	.5124	-	-	-	-	-	-.0584	.7023
2000	.0794	.6330	.4089	.0826	.6334	-	-	-	-	-	-.2413	4.3461
2200	.1129	.7303	.4958	.1166	.7309	-	-	-	-	-	-.5001	6.8078
2400	.1365	.8720	.5836	.1409	.8727	-	-	-	-	-	-.6110	9.2633
2600	.1419	.9022	.6138	.1464	.9029	-	-	-	-	-	-.6156	11.1987
2800	.1772	.9618	.6995	.1820	.9627	-	-	-	-	-	-.5345	12.4117

TABLE XII

Test II | Position #3 | Gages 7,8,9

	R			ΔЄ				σ			Є	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
400	-.0145	.1962	.0762	-.0135	.1961	.1972	+86-02	6356	1491	6334	-.0135	.1961
600	-.0211	.2798	.1095	-.0197	.2797	.2811	+86-14	9058	2117	9027	-.0197	.2797
800	-.0284	.3848	.1515	-.0265	.3847	.3863	+86-19	12459	2931	12420	-.0265	.3847
1000	-.0386	.4796	.1862	-.0362	.4794	.4819	+86-13	15504	3548	15446	-.0362	.4794
1100	-.0446	.5384	.2080	-.0419	.5382	.5410	+86-12	17394	3943	17329	-.0419	.5382
1200	-.0475	.6036	.2287	-.0445	.6034	-	-	-	-	-	-.1597	.8508
1250	-.0545	.6186	.2355	-.0514	.6183	-	-	-	-	-	-.2109	1.0195
1300	-.0588	.6543	.2466	-.0555	.6540	-	-	-	-	-	-.3137	1.3860
500	-.0186	.2354	.0948	-.0174	.2353	-	-	-	-	-	-.2756	.9673
900	-.0386	.4492	.1706	-.0364	.4490	-	-	-	-	-	-.2946	1.1810
1400	-.0652	.7153	.2831	-.0616	.7150	-	-	-	-	-	-.8225	3.1558
1600	-.1002	.9984	.3850	-.0952	.9979	-	-	-	-	-	-2.0917	8.4310
600	-.0303	.3196	.1352	-.0287	.3194	-	-	-	-	-	-2.0252	7.7525
1200	-.0583	.6458	.2583	-.0551	.6455	-	-	-	-	-	-2.0516	8.0786
1800	-.1563	NG	.4931	-	-	-	-	-	-	-	-	-
2000	-.1540	NG	.3516	-	-	-	-	-	-	-	-	-
2200	-.1809	NG	.7002	-	-	-	-	-	-	-	-	-
2400	-.2214	NG	.8117	-	-	-	-	-	-	-	-	-
2600	-.1979	NG	NG	-	-	-	-	-	-	-	-	-
2800	-.0874	NG	NG	-	-	-	-	-	-	-	-	-

TABLE XIII

Test II — Position #4 — Gages 10,11,12

	R			Δ ε				σ			ε	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
400	.0366	.1817	.1698	.0375	.1819	.2038	-19-57	6873	3036	6366	.0375	.1819
600	.0567	.2586	.2441	.0580	.2589	.2907	-20-18	9844	4474	9110	.0580	.2589
800	.0729	.3511	.3267	.0747	.3515	.3925	-19-46	13273	5938	12327	.0747	.3515
1000	.0924	.4308	.4087	.0946	.4313	.4860	-20-30	16418	7385	15156	.0946	.4313
1100	.1023	.4780	.4473	.1047	.4785	.5354	-19-58	18124	8186	16811	.1047	.4785
1200	.1162	.5226	.4847	.1188	.5232	-	-	-	-	-	.1022	.5148
1250	.1212	.5345	.4993	.1239	.5351	-	-	-	-	-	.1017	.5217
1300	.1259	.5470	.5117	.1286	.5476	-	-	-	-	-	.0998	.5286
500	.0462	.2125	.1975	.0473	.2127	-	-	-	-	-	.0185	.1937
900	.0864	.3890	.3411	.0883	.3894	-	-	-	-	-	.0595	.3704
1400	.1404	.5819	.5403	.1433	.5826	-	-	-	-	-	.0795	.5115
1600	.1927	.6107	.5701	.1958	.6117	-	-	-	-	-	-.0536	.5417
600	.0649	.2404	.2171	.0661	.2407	-	-	-	-	-	-.1833	.1707
1200	.1375	.4740	.4328	.1399	.4747	-	-	-	-	-	-.1095	.4047
1800	.2279	.6714	.5814	.2313	.6725	-	-	-	-	-	.6633	2.4305
2000	.3182	.7103	.5727	.3218	.7119	-	-	-	-	-	1.6984	4.8164
2200	.3792	.8006	.5930	.3832	.8025	-	-	-	-	-	2.5154	7.0360
2400	.4330	.9358	.6742	.4377	.9380	-	-	-	-	-	3.5395	9.9191
2600	.4897	1.0230	.6909	.4948	1.0254	-	-	-	-	-	4.8255	13.2397
2800	.5078	1.0089	.7735	.5128	1.0114	-	-	-	-	-	6.9492	18.8651

TABLE XIV

Test II | Position #5 | Gages 13,14,15

	← R →			← ΔE →				← σ →			← ε →	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
400	.2625	.1332	.2447	.2632	.1345	.2783	+72-02	10356	10010	7039	.2632	.1345
600	.3728	.1923	.3520	.3738	.1942	.3841	+71-32	14481	14246	10099	.3738	.1942
800	.5032	.2584	.4749	.5045	.2609	.5364	+71-13	19950	19215	13594	.5045	.2609
1000	.6292	.3195	.5919	.6308	.3226	.6625	+71-24	24900	23989	16874	.6308	.3226
1100	.6909	.3459	.6490	.6926	.3494	.7364	+71-26	27302	26290	18371	.6926	.3494
1200	.7570	.3778	.7105	.7589	.3816	-	-	-	-	-	.9014	.3298
1250	.7700	.3827	.7258	.7719	.3866	-	-	-	-	-	.9568	.3201
1300	.7945	.3898	.7434	.7964	.3938	-	-	-	-	-	1.0488	.3248
500	.3039	.1523	.2876	.3047	.1538	-	-	-	-	-	.5571	.0848
900	.5576	.2826	.5277	.5590	.2854	-	-	-	-	-	.8114	.2164
1400	.8687	.4258	.8154	.8708	.4301	-	-	-	-	-	1.4479	.3315
1600	.9385	.4719	.8862	.9409	.4766	-	-	-	-	-	3.0029	.5085
600	.3329	.1861	.3163	.3338	.1878	-	-	-	-	-	2.3958	.2197
1200	.6525	.3559	.6259	.6543	.3952	-	-	-	-	-	2.7163	.3911
1800	.9330	.5298	.8630	.9356	.5345	-	-	-	-	-	4.7072	.8899
2000	.9076	.5814	.8339	.9105	.5859	-	-	-	-	-	6.2507	1.0764
2200	.9146	.7028	.8174	.9181	.7074	-	-	-	-	-	8.7857	1.6676
2400	.9861	.8362	.8385	.9903	.8411	-	-	-	-	-	11.6937	2.8194
2600	1.0498	.9176	.9190	1.0544	.9228	-	-	-	-	-	14.6300	4.8068
2800	NG	.9635	.9618	-	-	-	-	-	-	-	-	-

TABLE XV

Test II | Position #6 | Geges 16,17,18

Press.	R Axial	R Tang.	R Diag.	ΔE Axial	ΔE Tang.	ΔE Princ.	θ	σ Princ.	σ Axial	σ Tang.	E Axial	E Tang.
400	-.0112	.2513	.0228	-.0099	.2512	.2833	+18-16	8924	2160	8183	-.0099	.2512
600	-.0327	.3616	.0356	-.0309	.3614	.3997	+16-35	12493	2555	11609	-.0309	.3614
800	-.0234	.4904	.0492	-.0209	.4903	.5494	+17-50	17320	4161	15957	-.0209	.4903
1000	-.0271	.6189	.0588	-.0240	.6188	.6962	+18-09	21949	5328	20164	-.0240	.6188
1100	-.0267	.6813	.0670	-.0233	.6812	.7663	+18-10	24192	5971	22228	-.0233	.6812
1200	-.0239	.7516	.0764	-.0201	.7515	-	-	-	-	-	.0675	.9130
1250	-.0236	.7700	.0807	-.0198	.7699	-	-	-	-	-	.1160	.9642
1300	-.0156	.8065	.0871	-.0116	.8064	-	-	-	-	-	.1944	1.0455
500	-.0123	.3002	.0269	-.0108	.3001	-	-	-	-	-	.1952	.5392
900	-.0200	.5619	.0592	-.0172	.5618	-	-	-	-	-	.1888	.8009
1400	..0063	.9046	.1094	.0108	.9046	-	-	-	-	-	.5171	1.5374
1600	.0998	1.1515	.1934	.1056	1.1520	-	-	-	-	-	2.1334	5.4698
600	.0223	0.3995	.0636	.0243	.3996	-	-	-	-	-	2.0521	4.7174
1200	.0383	0.7923	.1262	.0423	.7925	-	-	-	-	-	2.0701	5.1103
1800	.1779	1.3328	.2289	.1846	1.3337	-	-	-	-	-	2.6365	10.6465
2000	.2632	1.4870	.2820	.2706	1.4883	-	-	-	-	-	2.9129	16.1530
2200	.3718	NG	.3126	-	-	-	-	-	-	-	-	-
2400	.4696	NG	.3324	-	-	-	-	-	-	-	-	-
2600	.5635	NG	.2928	-	-	-	-	-	-	-	-	-
2800	.6793	NG	.1957	-	-	-	-	-	-	-	-	-

TABLE XVI

Test II | Position #7 | Gages 19.20.21

Press.	R Axial	R Tang.	R Diag.	ΔЄ Axial	ΔЄ Tang.	ΔЄ Princ.	θ	σ Princ.	σ Axial	σ Tang.	Є Axial	Є Tang.
400	-.0066	-.0336	.0425	-.0068	-.0336	.0435	+38-55	605	-557	-1174	-.0068	-.0336
600	-.0112	-.0475	.0614	-.0114	-.0476	.0626	+39-21	862	-847	-1681	-.0114	-.0476
800	-.0175	-.0640	.0822	-.0178	-.0641	.0836	+39-29	1118	-1220	-2288	-.0178	-.0641
1000	-.0224	-.0759	.1013	-.0228	-.0760	.1026	+39-58	1391	-1503	-2730	-.0228	-.0760
1100	-.0244	-.0838	.1132	-.0248	-.0839	.1147	+38-58	1570	-1648	-3010	-.0248	-.0839
1200	-.0242	-.0896	.1218	-.0246	-.0897	-	-	-	-	-	-.0298	-.1084
1250	-.0269	-.0860	.1236	-.0273	-.0861	-	-	-	-	-	-.0318	-.1169
1300	-.0276	-.0930	.1269	-.0281	-.0931	-	-	-	-	-	-.0316	-.1277
500	-.0103	-.0359	.0499	-.0105	-.0360	-	-	-	-	-	-.0140	-.0706
900	-.0203	-.0678	.0938	-.0206	-.0679	-	-	-	-	-	-.0241	-.1025
1400	-.0333	-.1031	.1334	-.0338	-.1033	-	-	-	-	-	-.0387	-.1686
1600	-.0493	-.0998	.1394	-.0493	-.1000	-	-	-	-	-	-.0634	-.2847
600	-.0156	-.0389	.0509	-.0158	-.0390	-	-	-	-	-	-.0294	-.2237
1200	-.0413	-.0802	.1015	-.0417	-.0804	-	-	-	-	-	-.0553	-.2651
1800	-.0743	-.1020	.1379	-.0748	-.1024	-	-	-	-	-	-.2306	-.4977
2000	-.1085	-.0854	.1229	-.1089	-.0859	-	-	-	-	-	-.4937	-.7576
2200	-.1139	-.0573	.1440	-.1142	-.0579	-	-	-	-	-	-.8624	-.9176
2400	-.1261	-.0255	.1821	-.1262	-.0261	-	-	-	-	-	-1.0256	-.8471
2600	-.1211	.0154	.2083	-.1210	.0148	-	-	-	-	-	-1.1384	-.6243
2800	-.0847	.0710	.2546	-.0843	.0706	-	-	-	-	-	-1.5323	-.1973

TABLE XVII

Test II | Position #8 | Gages 22 & 23

	R			ΔE				σ			ε	
Press.	Axial	Tang.	Diag.	Axial	Tang.	Princ.	θ	Princ.	Axial	Tang.	Axial	Tang.
400	-.0390	-.0307	-	-.0390	-.0307	-.0307	-	-	-1589	-1398	-.0390	-.0307
600	-.0579	-.0432	-	-.0579	-.0432	-.0432	-	-	-2338	-1998	-.0579	-.0432
800	-.0730	-.0597	-	-.0730	-.0597	-.0597	-	-	-2997	-2690	-.0730	-.0597
1000	-.0934	-.0741	-	-.0934	-.0741	-.0741	-	-	-3811	-3366	-.0934	-.0741
1100	-.1023	-.0801	-	-.1023	-.0801	-.0801	-	-	-4164	-3653	-.1023	-.0801
1200	-.1083	-.0856	-	-.1083	-.0856		-	-			-.1270	-.0846
1250	-.1145	-.0896	-	-.1145	-.0896	-	-	-	-	-	-.1355	-.0848
1300	-.1171	-.0918	-	-.1171	-.0918	-	-	-	-	-	-.1370	-.0833
500	-.0443	-.0353	-	-.0443	-.0353	-	-	-	-	-	-.0642	-.0268
900	-.0868	-.0674	-	-.0868	-.0674	-	-	-	-	-	-.1067	-.0588
1400	-.1255	-.0963	-	-.1255	-.0963	-	-	-	-	-	-.1465	-.0732
1600	-.1479	-.0923	-	-.1479	-.0923	-	-	-	-	-	-.2295	-.0248
600	-.0635	-.0361	-	-.0635	-.0361	-	-	-	-	-	-.1451	.0314
1200	-.1248	-.0754	-	-.1248	-.0754	-	-	-	-	-	-.2064	-.0079
1800	-.1697	-.0787	-	-.1697	-.0787	-	-	-	-	-	-.3453	.3800
2000	-.1945	-.0733	-	-.1945	-.0733	-	-	-	-	-	-.4368	-.0032
2200	-.1808	-.0610	-	-.1808	-.0610	-	-	-	-	-	-.6109	.0402
2400	-.1527	-.0502	-	-.1527	-.0502	-	-	-	-	-	-.7606	.1302
2600	-.1447	-.0276	-	-.1447	-.0276	-	-	-	-	-	-.9359	.2580
2800	-.1137	-.0113	-	-.1137	-.0113	-	-	-	-	-	-1.2371	.5097

TABLE XVIII

Test II — Position #9 — Gages 1 & 24

Press.	R Axial	R Tang.	R Diag.	$\Delta\epsilon$ Axial	$\Delta\epsilon$ Tang.	$\Delta\epsilon$ Princ.	θ	σ Princ.	σ Axial	σ Tang.	ϵ Axial	ϵ Tang.
400	.0379	.2609	-	.0379	.2609	.2609	-	-	3831	8978	.0379	.2609
600	.0586	.3790	-	.0586	.3790	.3790	-	-	5681	13076	.0586	.3790
800	.0790	.5128	-	.0790	.5128	.5128	-	-	7675	17688	.0790	.5128
1000	.1023	.6519	-	.1023	.6519	.6519	-	-	9822	22505	.1023	.6519
1100	.1174	.7238	-	.1174	.7238	.7238	-	-	11028	25024	.1174	.7238
1200	.0953	.8185	-	.0953	.8185	-	-	-	-	-	.2061	1.1963
1250	.0911	.8575	-	.0911	.8575	-	-	-	-	-	.2821	1.4422
1300	.0774	.9016	-	.0774	.9016	-	-	-	-	-	.4146	1.8942
500	.0483	.3181	-	.0483	.3181	-	-	-	-	-	.3855	1.3107
900	.0890	.6071	-	.0890	.6071	-	-	-	-	-	.4262	1.5997
1400	.1186	1.0540	-	.1186	1.0540	-	-	-	-	-	.8126	4.1393
1600	.1198	NG	-	.1198	-	-	-	-	-	-	1.3072	-
600	.0375	NG	-	.0375	-	-	-	-	-	-	1.2249	-
1200	.0563	NG	-	.0563	-	-	-	-	-	-	1.2437	-
1800	.1484	NG	-	.1484	-	-	-	-	-	-	1.4052	-
2000	.0664	NG	-	.0664	-	-	-	-	-	-	.7650	-
2200	.0468	NG	-	.0468	-	-	-	-	-	-	-.0689	-
2400	-.0429	NG	-	-.0429	-	-	-	-	-	-	-.7222	-
2600	-.0440	NG	-	-.0440	-	-	-	-	-	-	-.7927	-
2800	-.0856	NG	-	-.0856	-	-	-	-	-	-	-1.0672	-

TABLE NO. XIX

Relation of load to $p.\frac{R}{t}$

Test I: $\frac{R}{t} = \frac{3.84}{.4} = 9.6$

Test II: $\frac{R}{t} = \frac{3.84}{.3} = 12.8$

Test I		Test II	
P	$p.\frac{R}{t}$	P	$p.\frac{R}{t}$
500	4800	400	5120
750	7200	600	7680
1000	9600	800	10240
1250	12000	1000	12800
1500	14400	1100	14080
1600	15360	1200	15360
1700	16320	1250	16000
1800	17280	1300	16640
1900	18240	1400	17920
2000	19200	1600	20480
2050	19680	1800	23040
2150	20640	2000	25600
2200	21120	2200	28160
2300	22080	2400	30720
2400	23040	2600	33280
2500	24000	2800	35840
2600	24960		
2800	26880		
3000	28800		
3250	31200		

Fig. 1 First specimen and test setup.

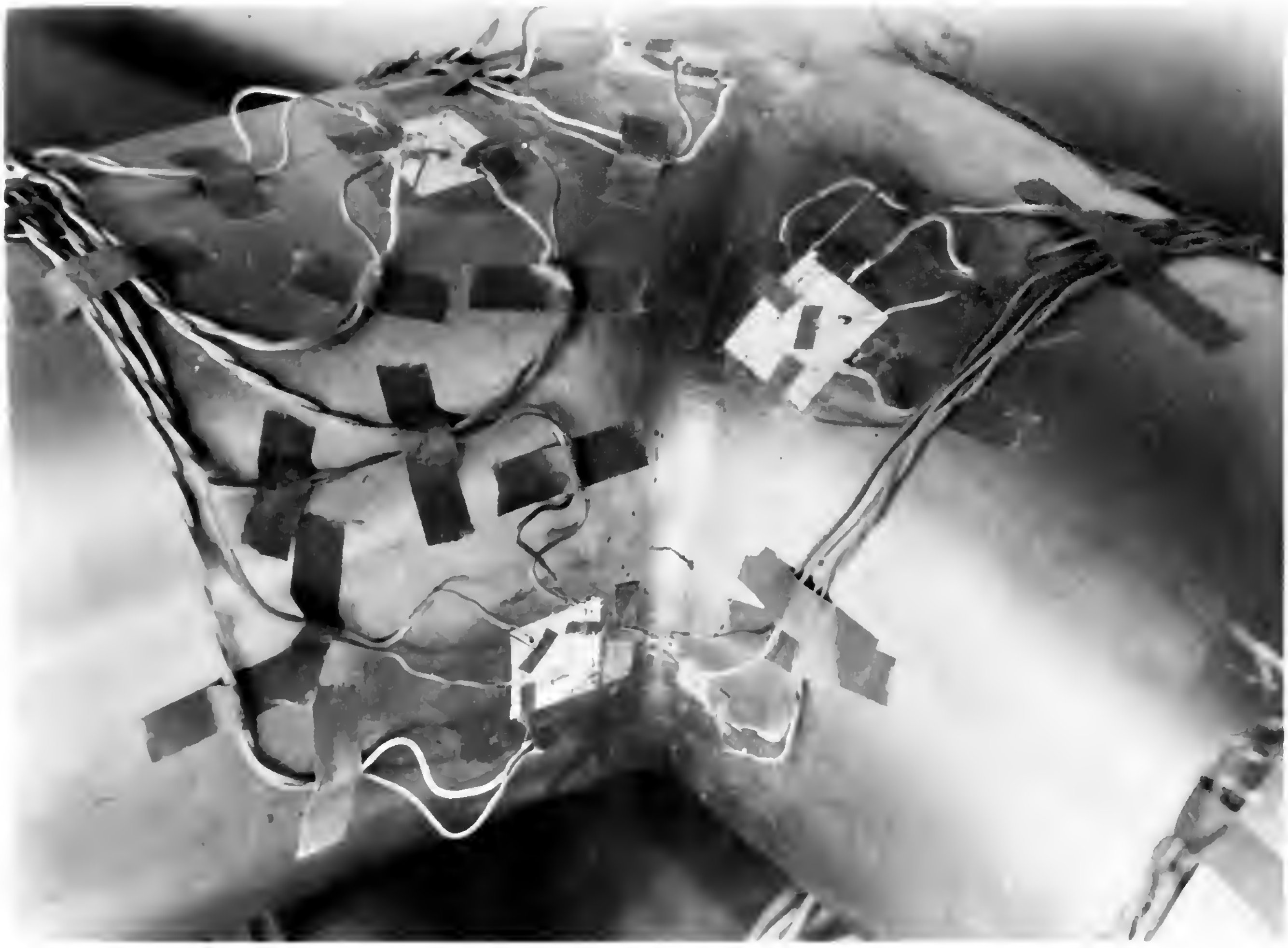


Fig. 2 Closeup view of first specimen showing rupture.

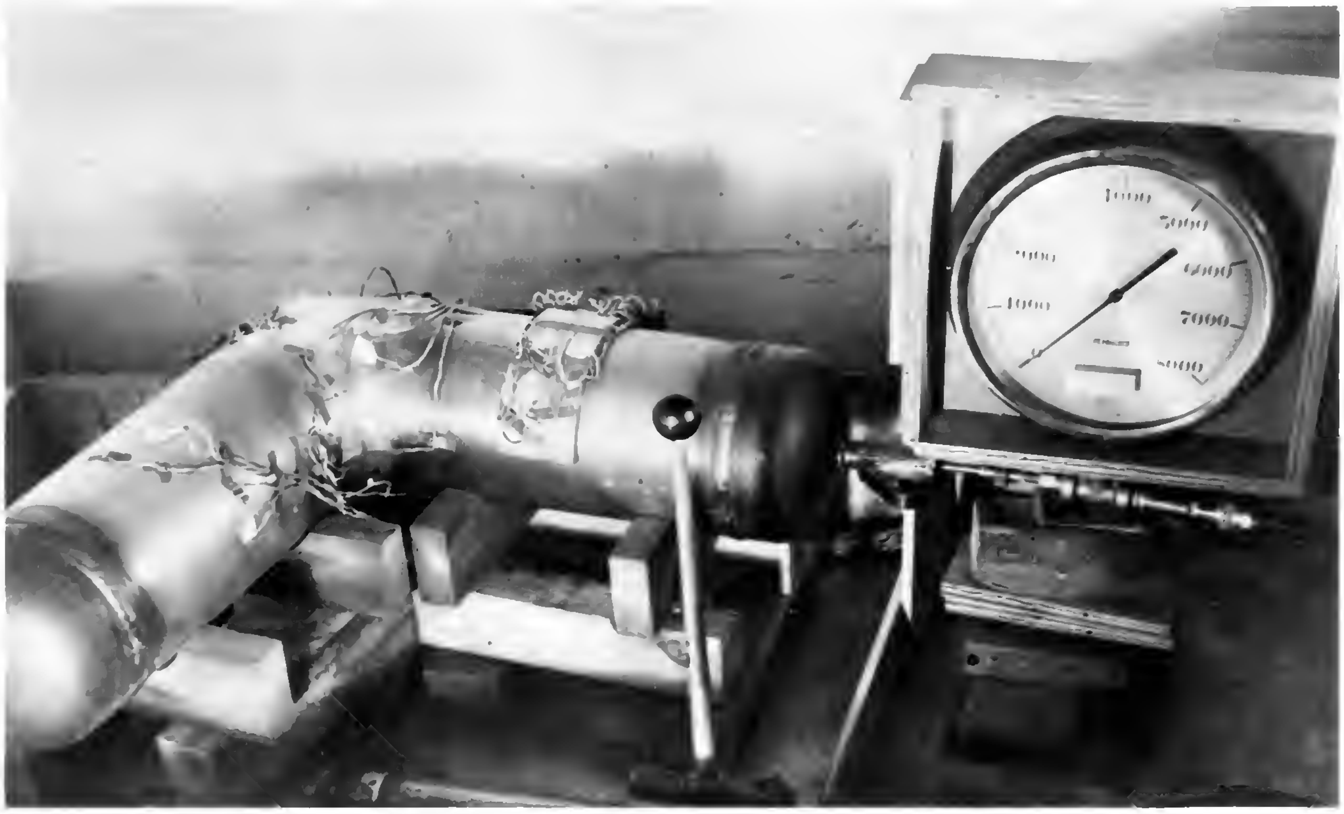


Fig. 3 Second specimen and test setup.

Fig. 4 Closeup view of second specimen showing rupture.

B-5

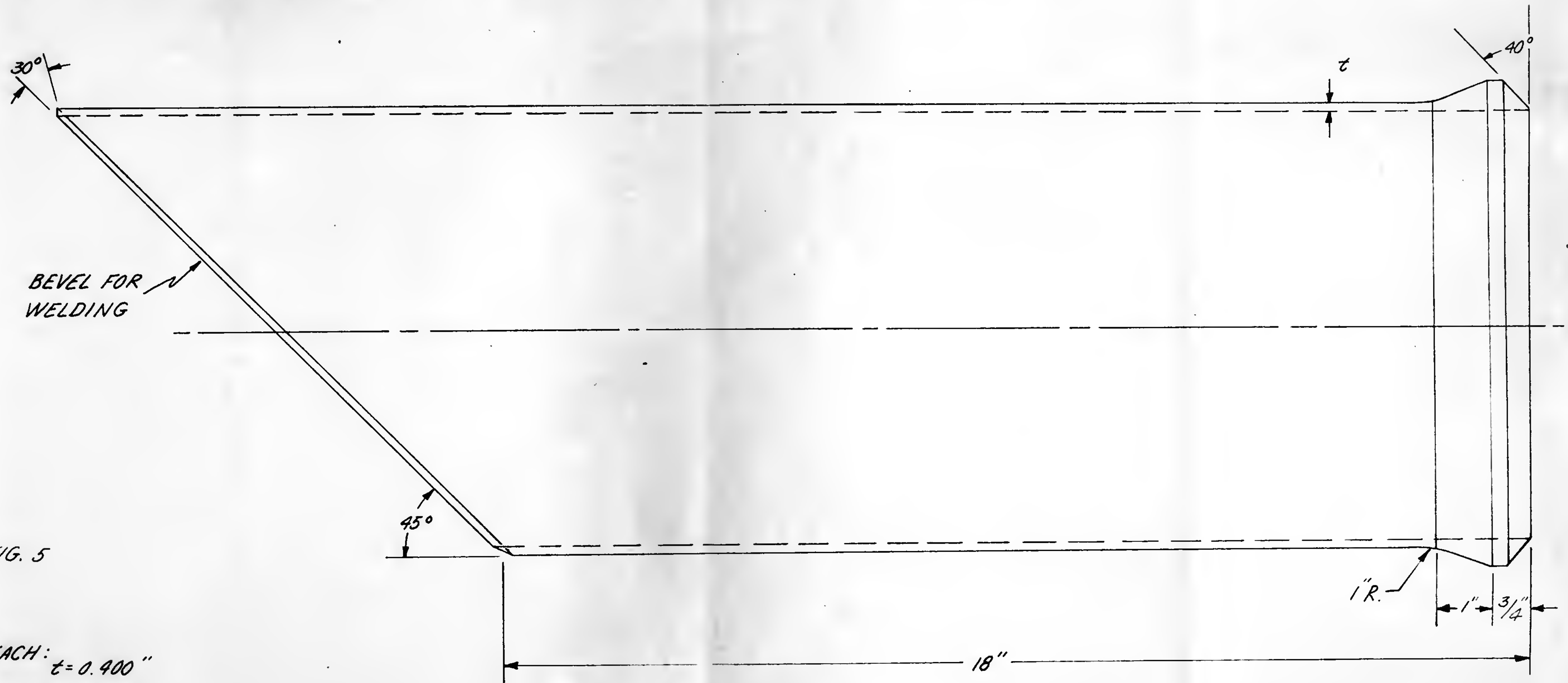


FIG. 5

NOTE:

2 EACH: t = 0.400"
t = 0.300"

MACHINE INSIDE AND OUT TO GIVE UNIFORM WALL THICKNESS WITH TOLERANCE ± .002"

MAINTAIN I.D. AS SMALL AS POSSIBLE

8" STEEL TUBING	MACHINE						TOLERANCES = .010 OR 1/64 UNLESS OTHERWISE NOTED
MATERIAL	FINISH	HEAT TREAT	DRAFTSMAN	CHECKED	APPROVED	ENGINEER	
GUGGENHEIM AERONAUTICAL LABORATORY CALIFORNIA INSTITUTE OF TECHNOLOGY			SPECIMENS FOR PRESSURE TESTS OF 90° CYLINDRICAL CORNER				
			NAME				DRAWING NO.

B-6

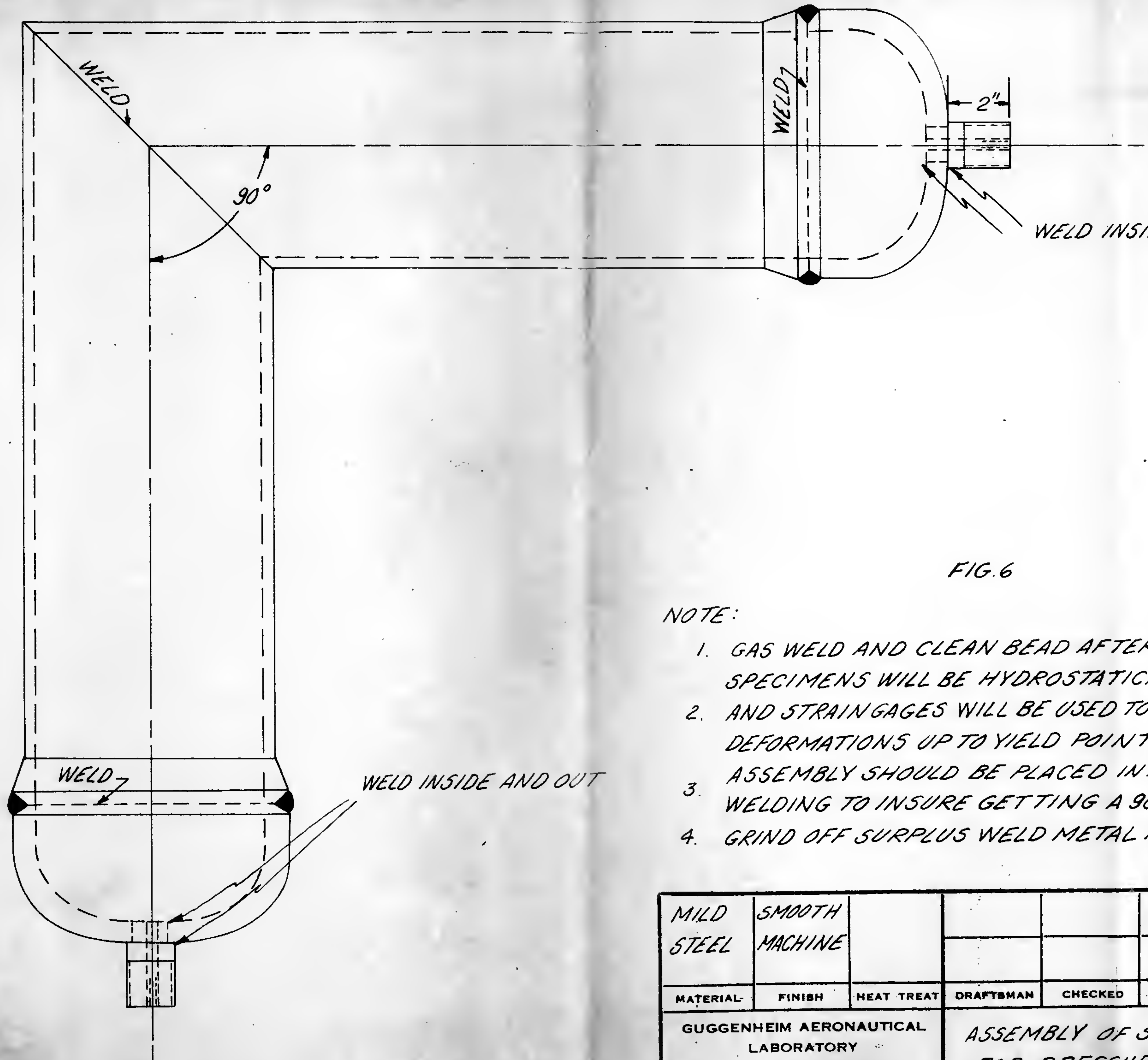


FIG. 6

NOTE:

1. GAS WELD AND CLEAN BEAD AFTER EACH PASS.
SPECIMENS WILL BE HYDROSTATICALLY LOADED
2. AND STRAINGAGES WILL BE USED TO MEASURE
DEFORMATIONS UP TO YIELD POINT.
3. ASSEMBLY SHOULD BE PLACED IN A JIG FOR
WELDING TO INSURE GETTING A 90° ANGLE.
4. GRIND OFF SURPLUS WELD METAL IN 90° JOINT.

MILD STEEL	SMOOTH MACHINE						TOLERANCES = .010 OR 1/64 UNLESS OTHERWISE NOTED SCALE: 1/4
MATERIAL	FINISH	HEAT TREAT	DRAFTSMAN	CHECKED	APPROVED	ENGINEER	
GUGGENHEIM AERONAUTICAL LABORATORY CALIFORNIA INSTITUTE OF TECHNOLOGY			ASSEMBLY OF SPECIMENS FOR PRESSURE TESTS NAME				DRAWING NO.

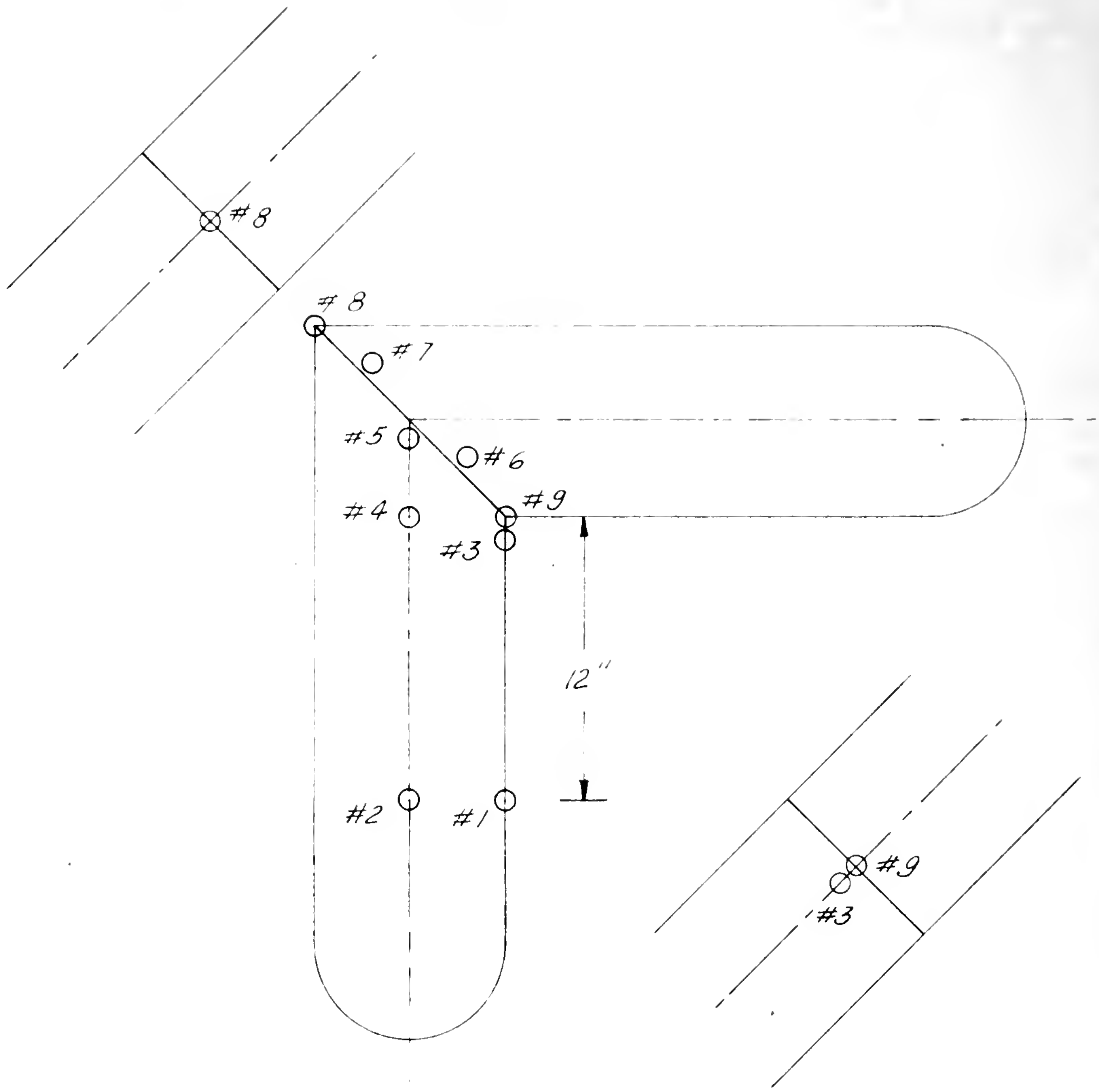


FIG. 7

LOCATION OF STRAIN GAGES
TESTS I AND II

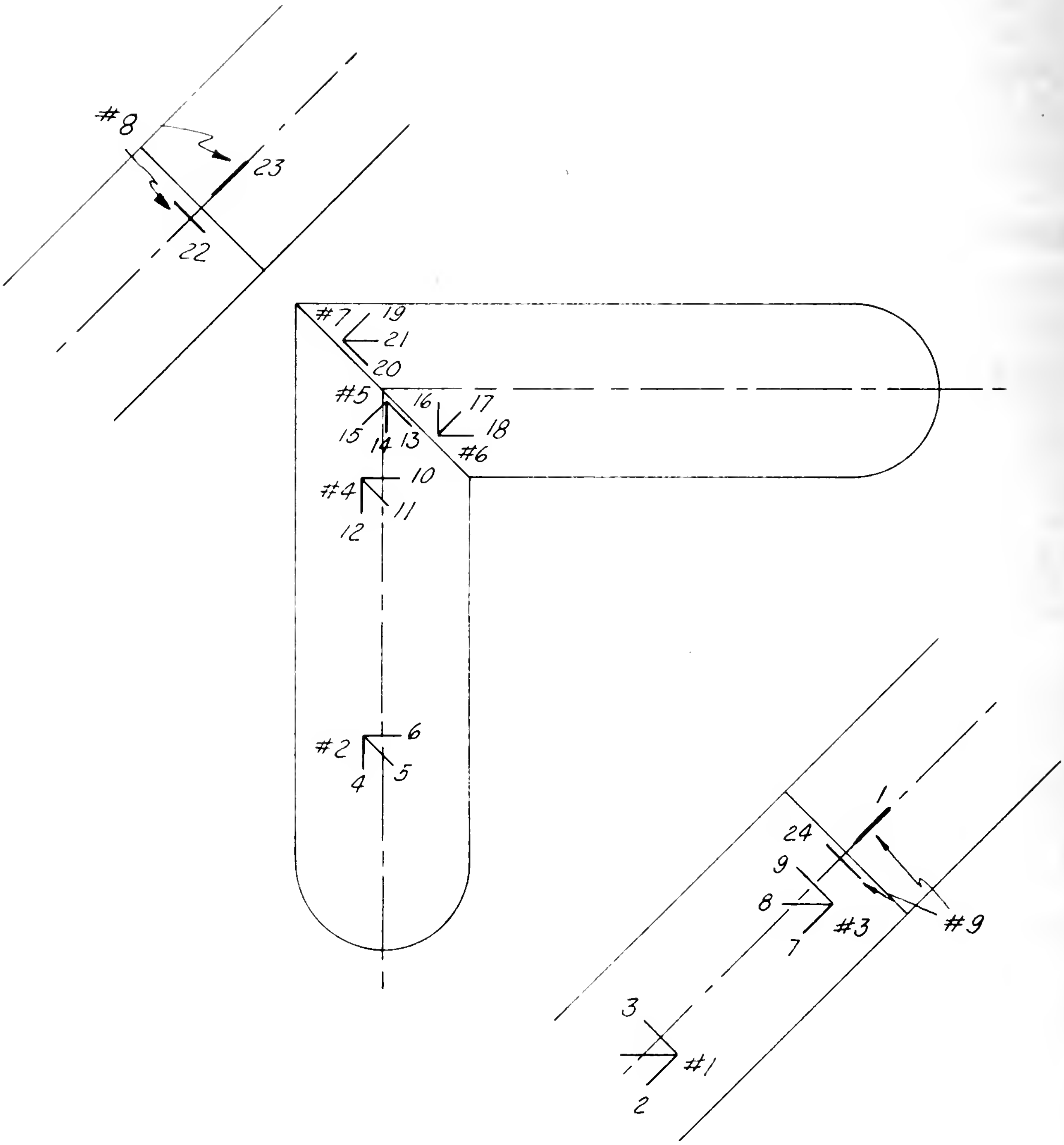


FIG. 8

ORIENTATION OF STRAIN GAGES, TEST I

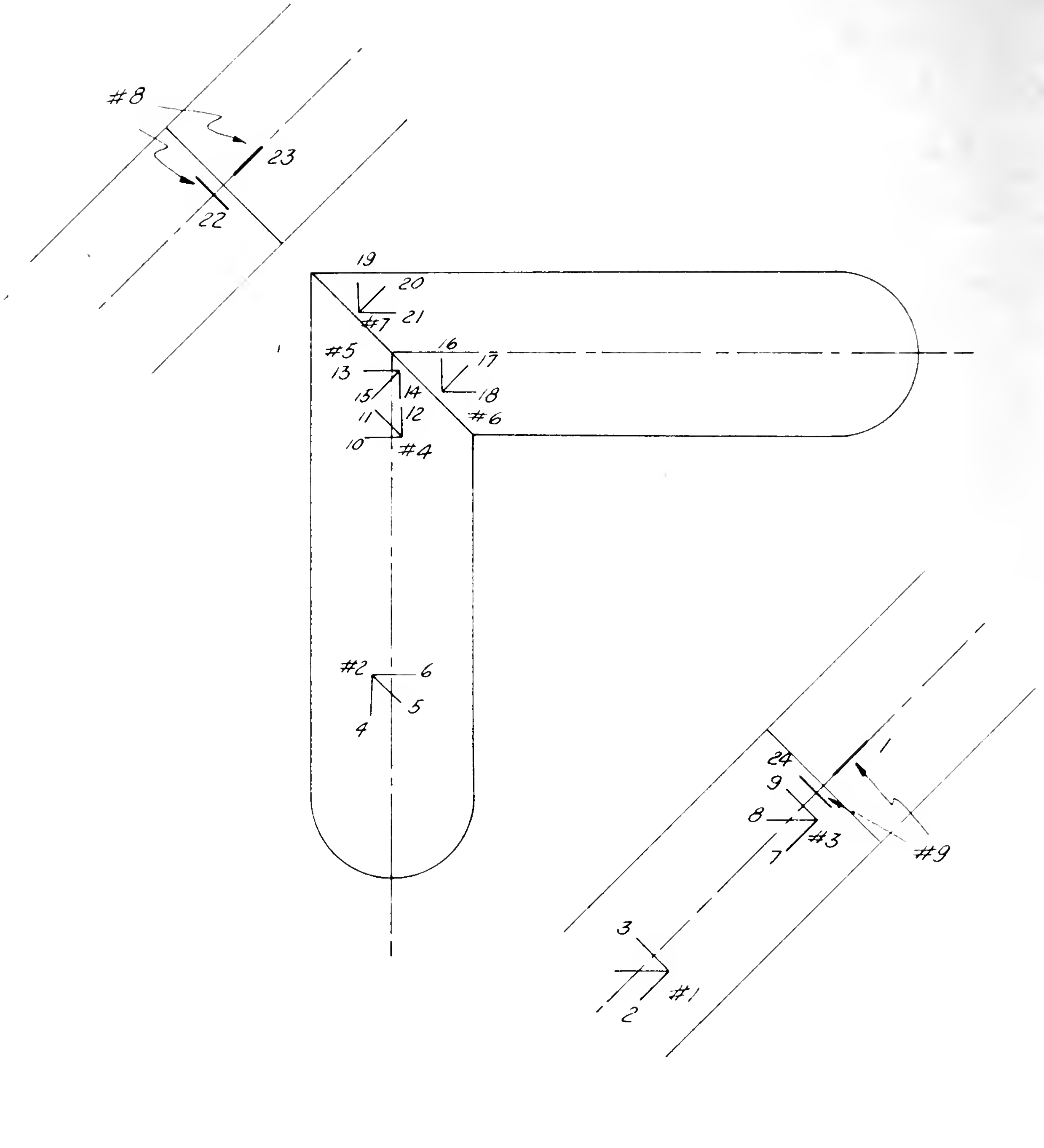


FIG. 9

ORIENTATION OF STRAIN GAGES, TEST II

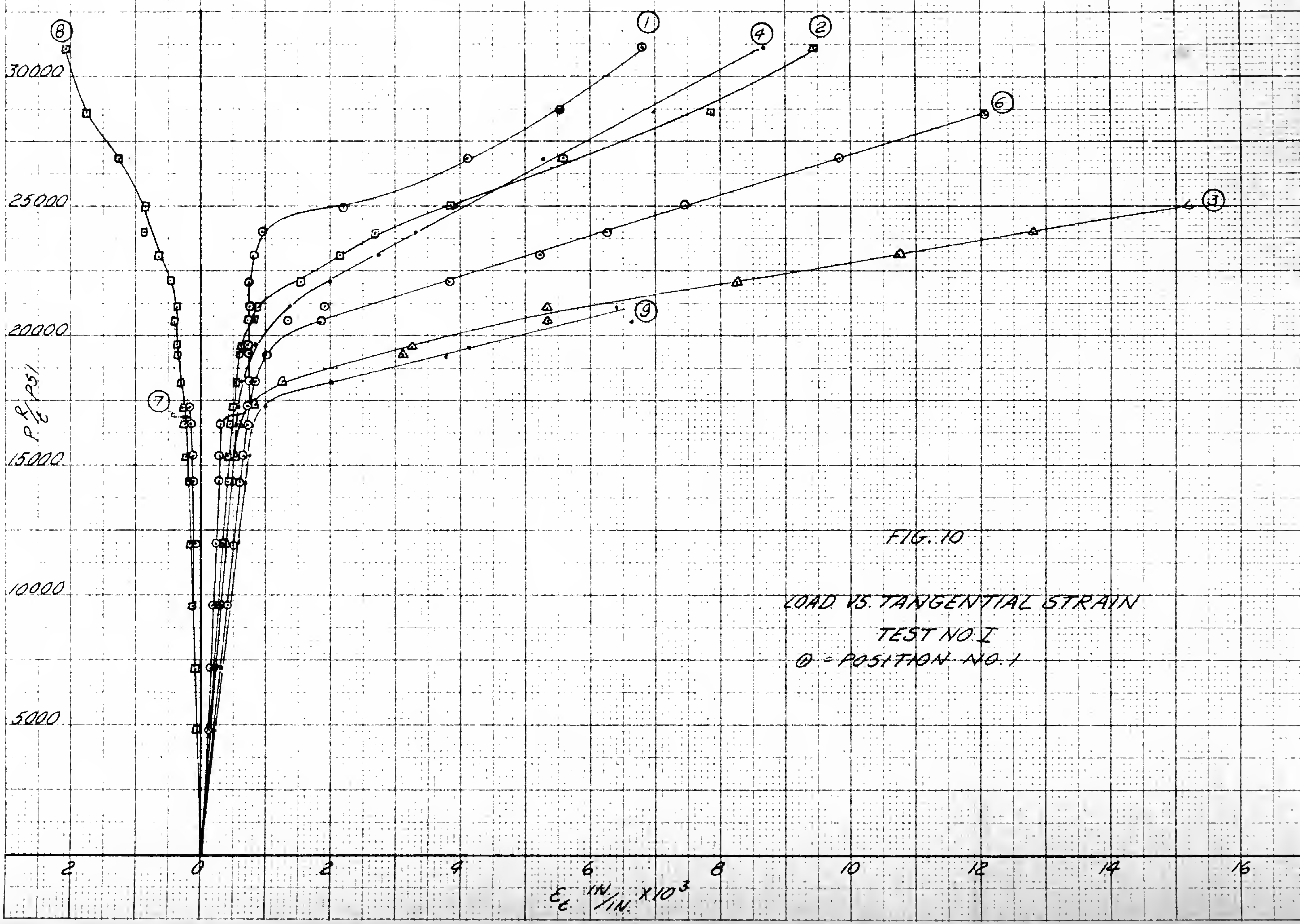


FIG. 10

LOAD VS. TANGENTIAL STRAIN

TEST NO. I

⊙ = POSITION NO. 1

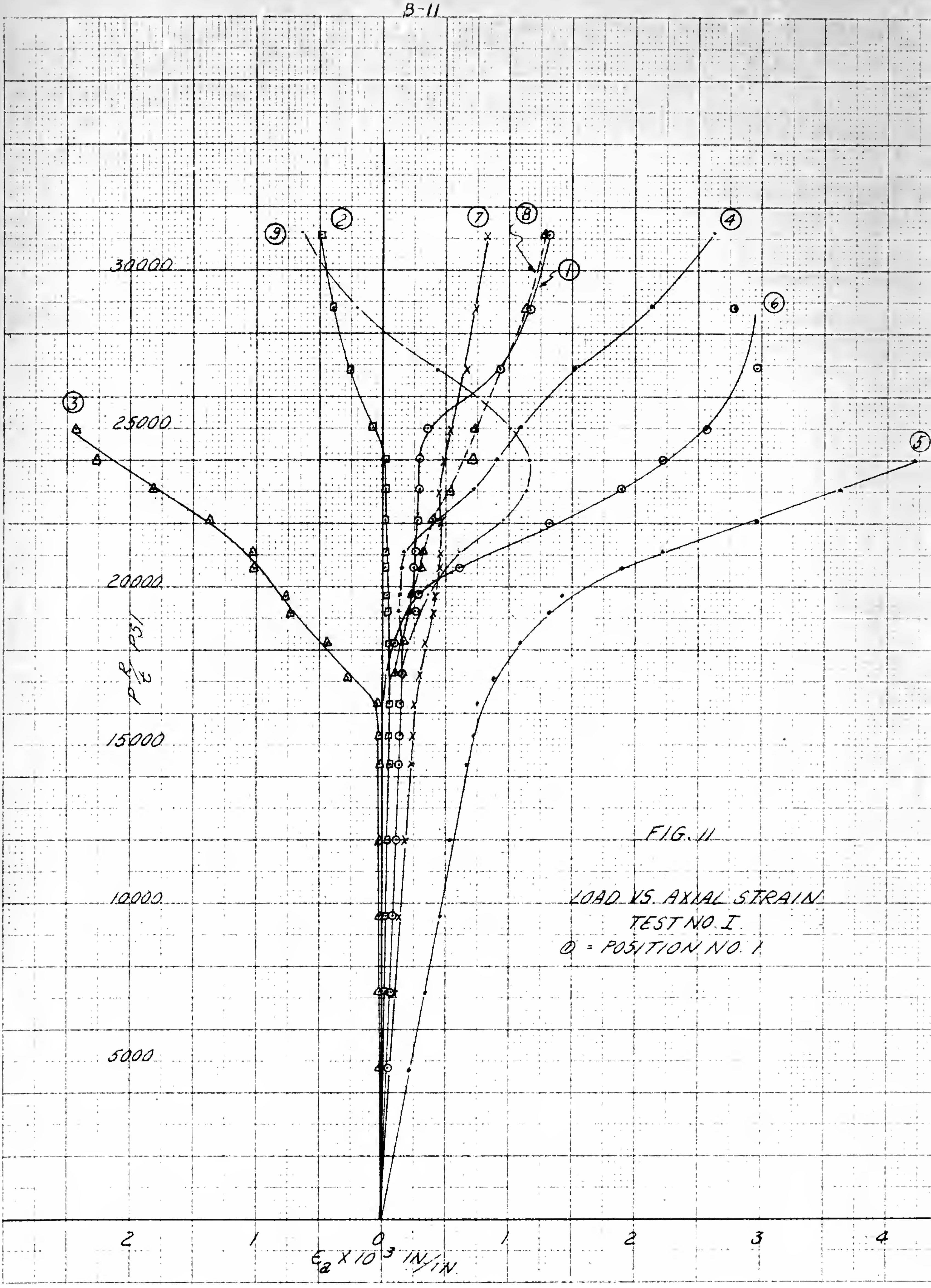


FIG. 11

LOAD VS. AXIAL STRAIN
TEST NO. I
① = POSITION NO. 1

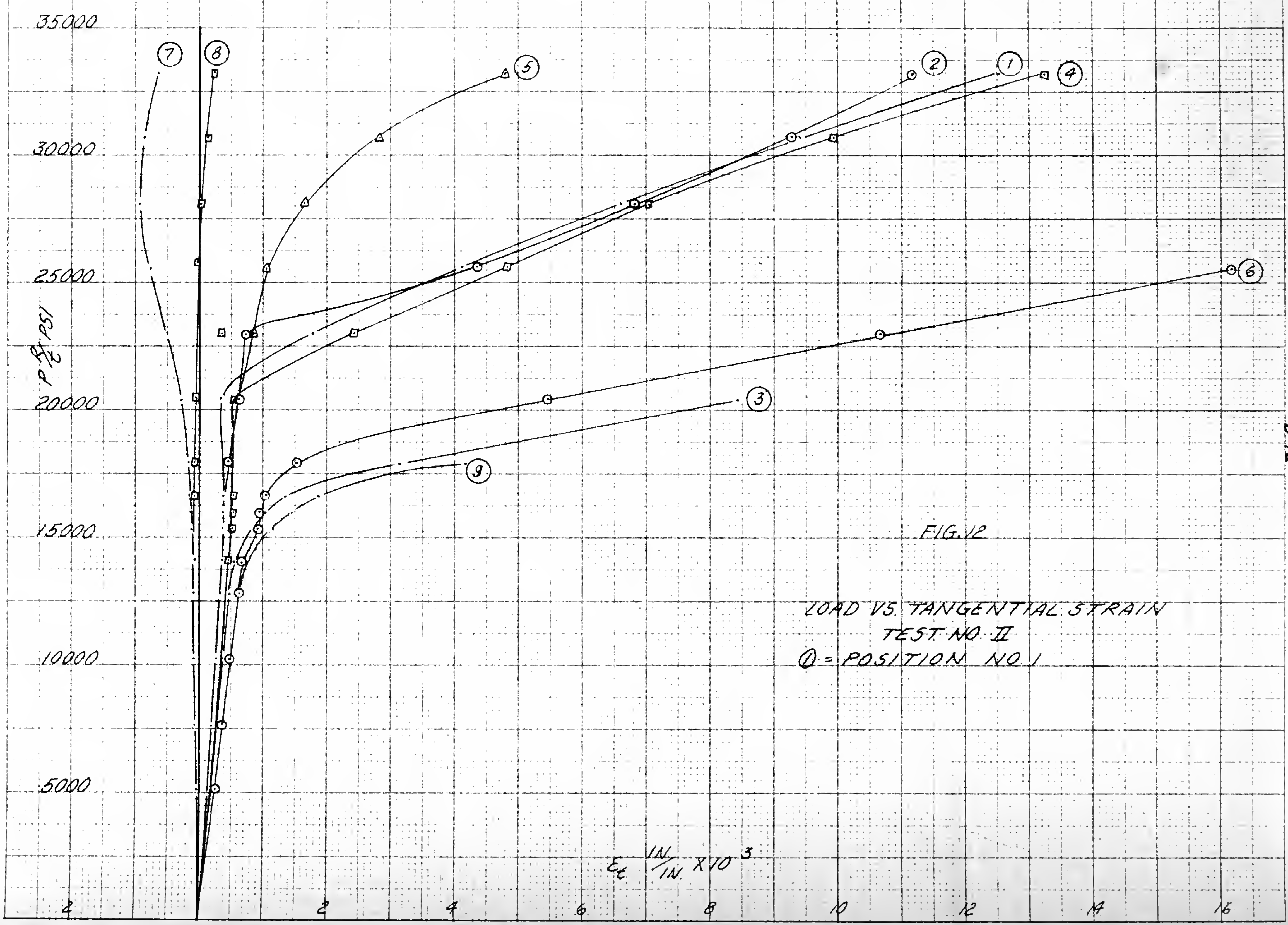


FIG. 12

LOAD VS. TANGENTIAL STRAIN
TEST NO. II
① = POSITION NO. 1

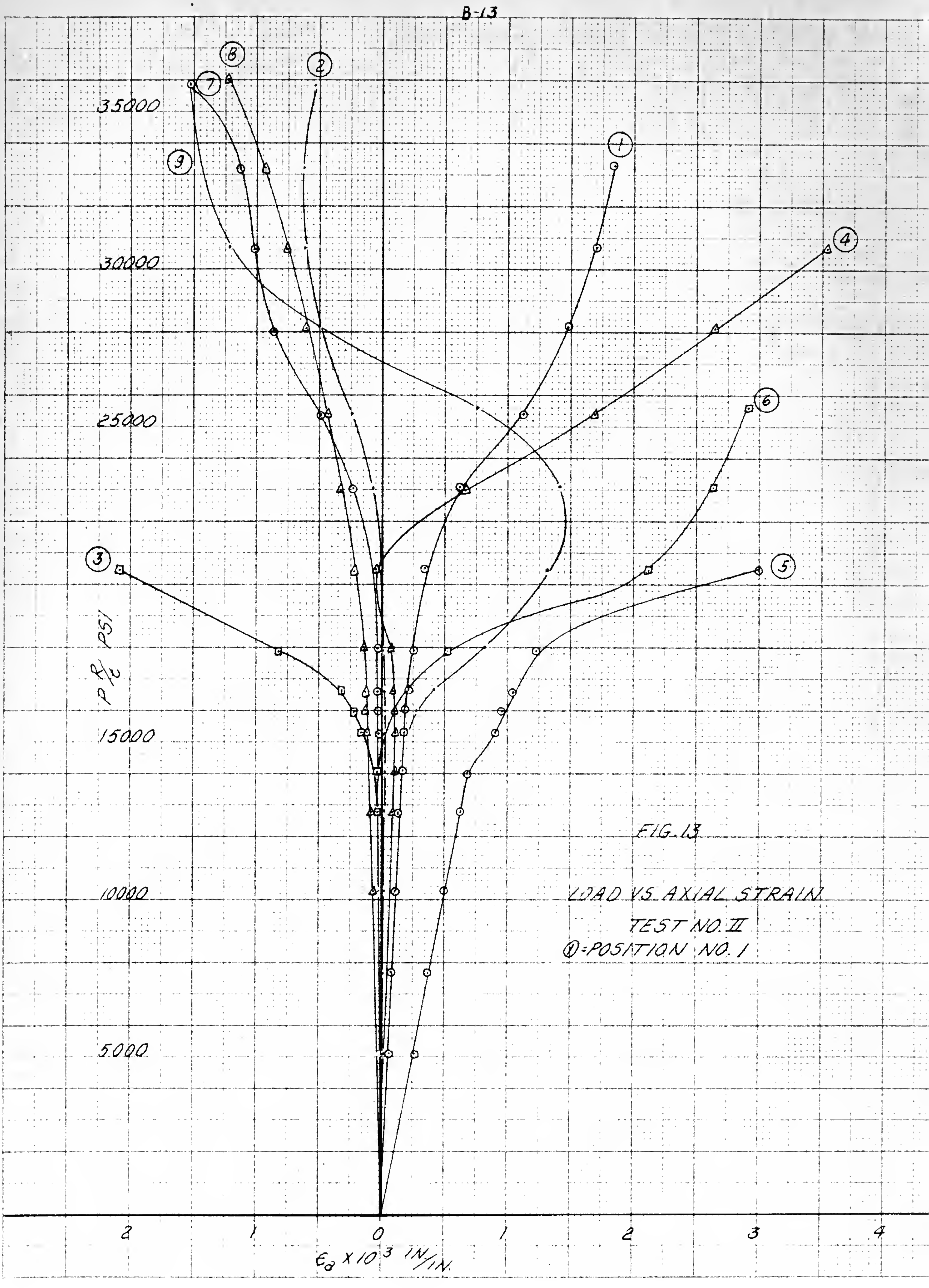


FIG. 13

LOAD VS. AXIAL STRAIN

TEST NO. II

① = POSITION NO. 1

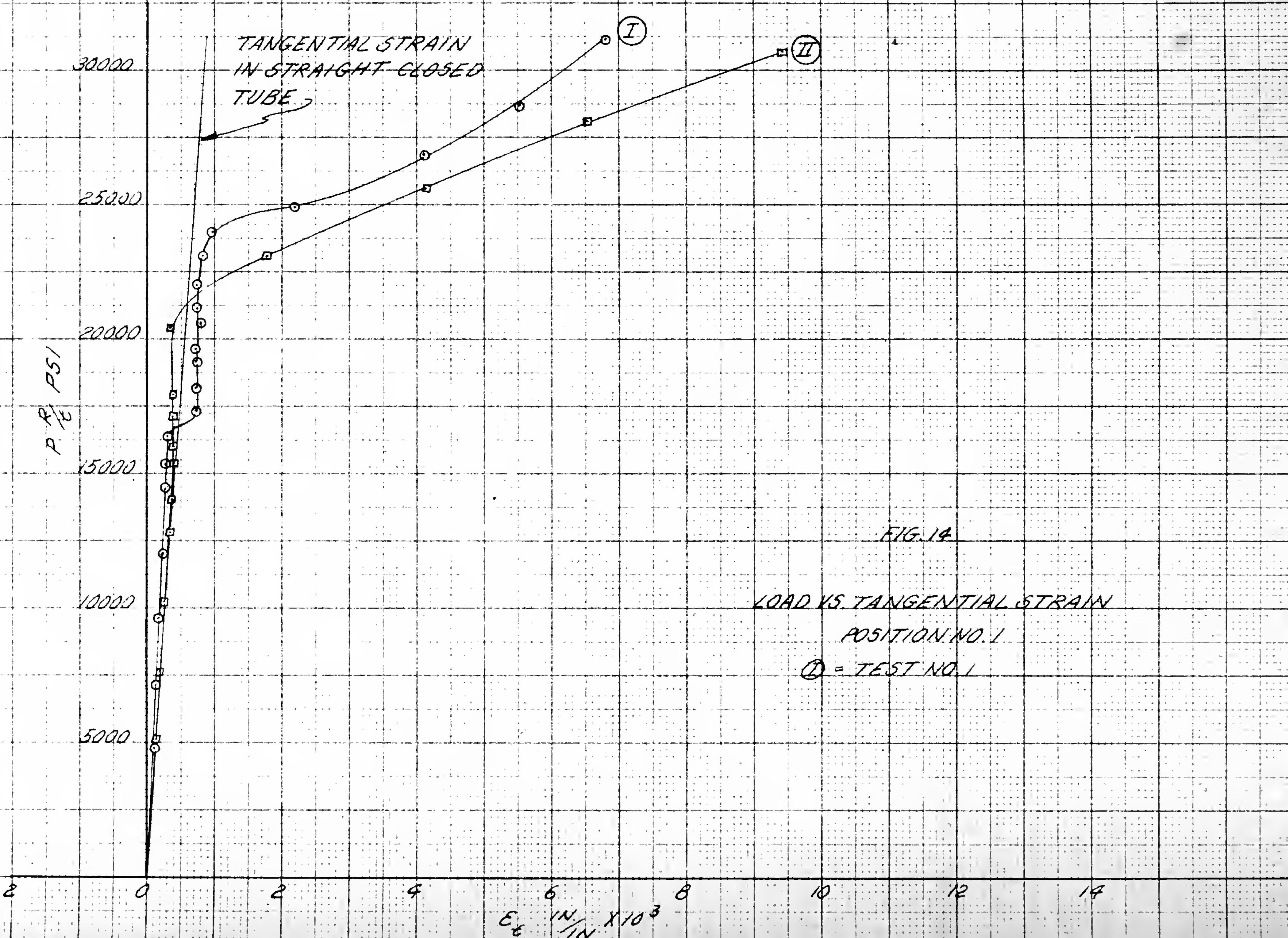

TANGENTIAL STRAIN
IN STRAIGHT CLOSED
TUBE
I
II
30000
25000
20000
15000
10000
5000
P R/t PSI
2
0
2
4
6
8
10
12
14
ε_t IN/IN X 10^3
LOAD VS. TANGENTIAL STRAIN
POSITION NO. 1
(I) = TEST NO. 1

FIG. 14

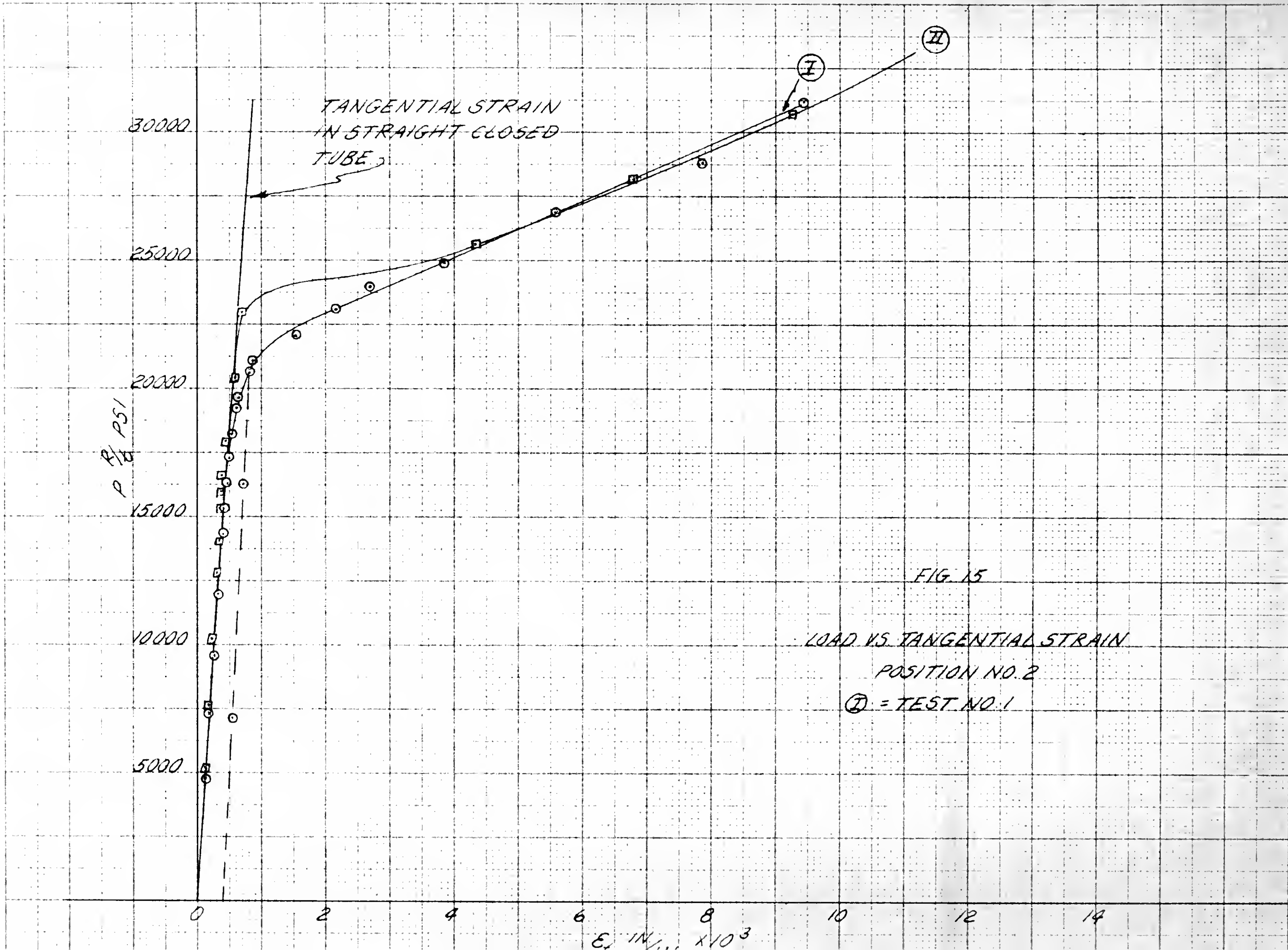


FIG. 15

LOAD VS. TANGENTIAL STRAIN

POSITION NO. 2

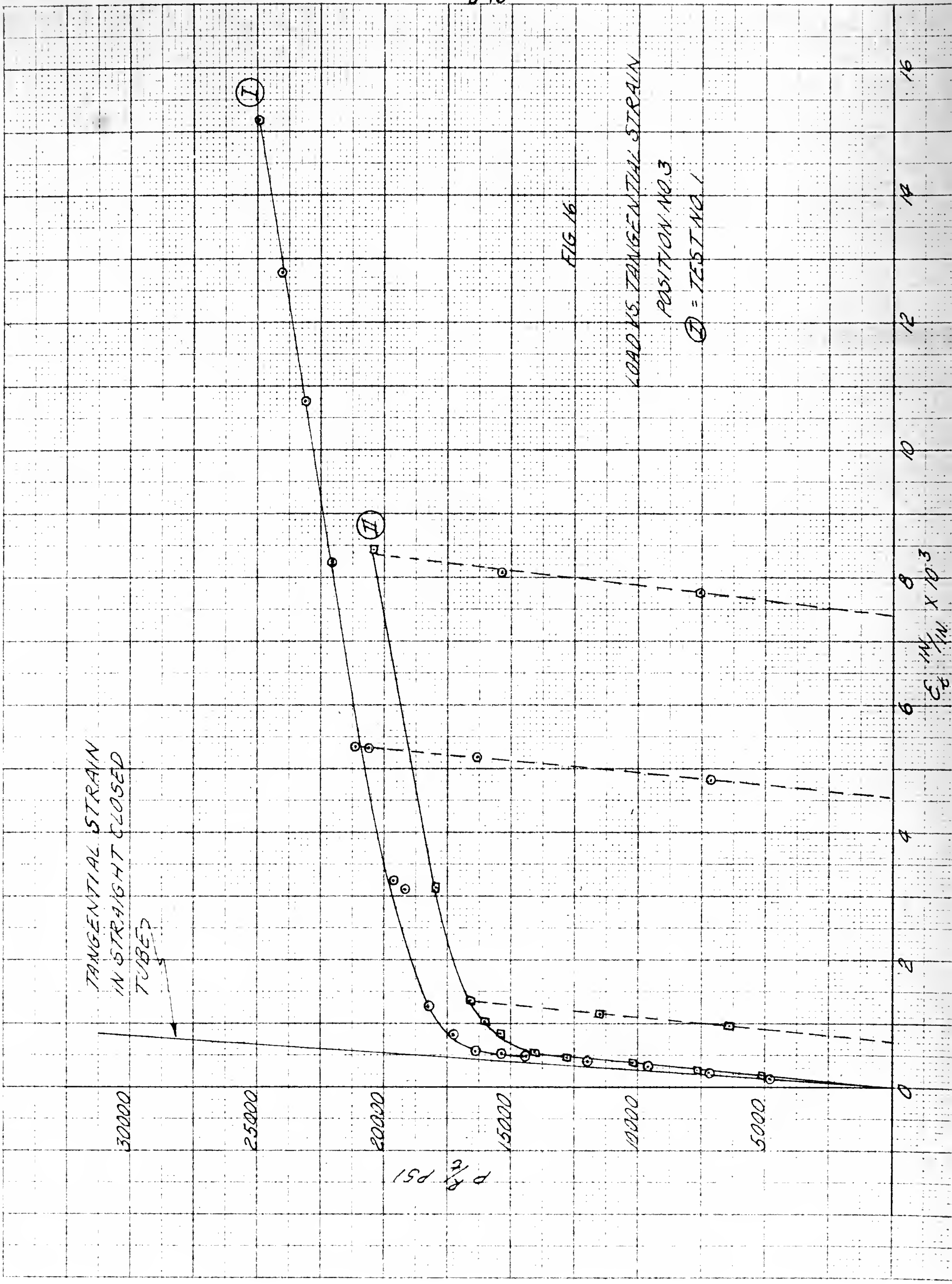


FIG. 16
LOAD VS. TANGENTIAL STRAIN
POSITION NO. 3
(I) = TEST NO. 1
I
II
TANGENTIAL STRAIN
IN STRAIGHT CLOSED
TUBES
P r/t PSI
30000
25000
20000
15000
10000
5000
ϵ_t IN/IN x 10^3
0
2
4
6
8
10
12
14
16

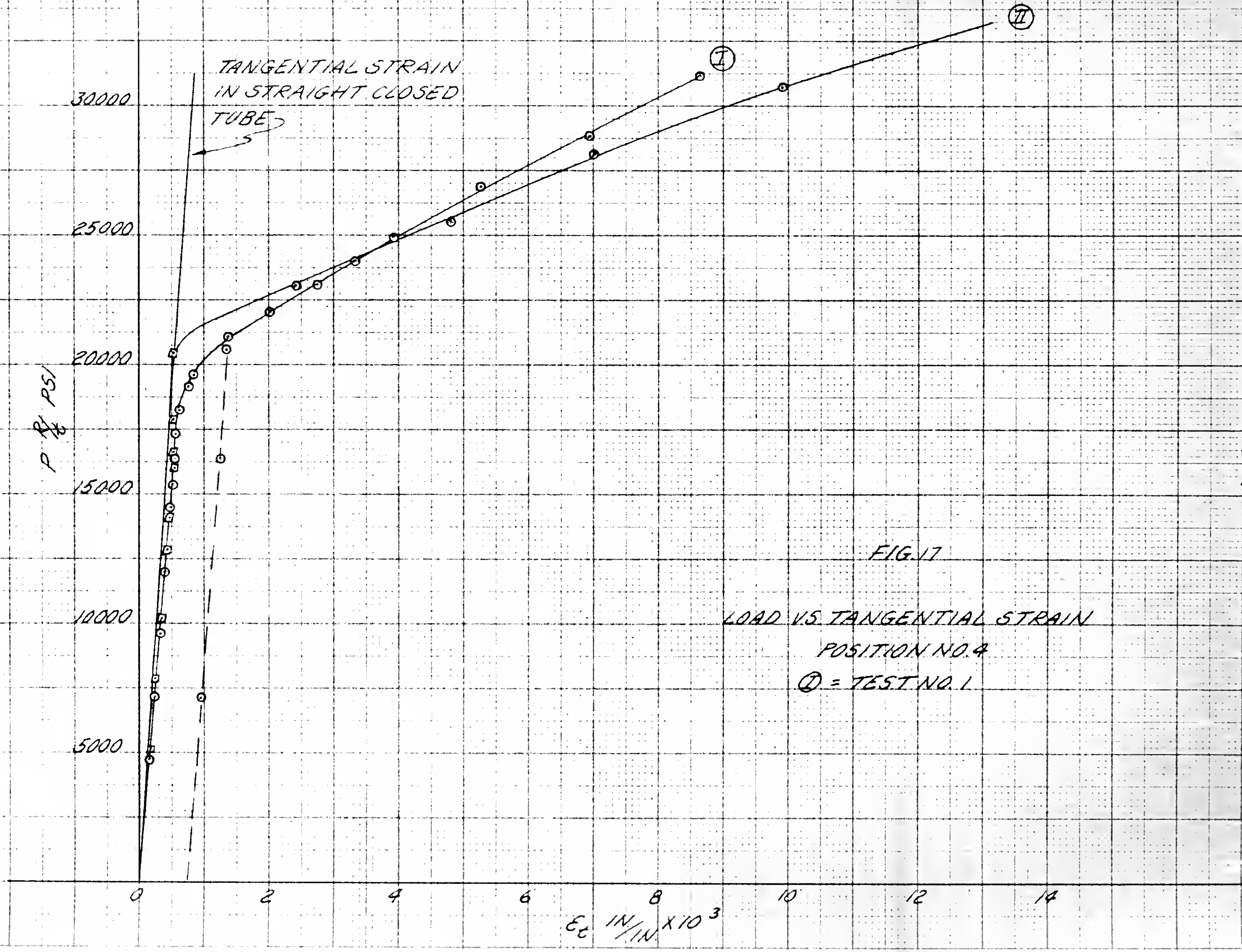


FIG.17

LOAD V.S. TANGENTIAL STRAIN

POSITION NO.4

Ⓘ = TEST NO.1

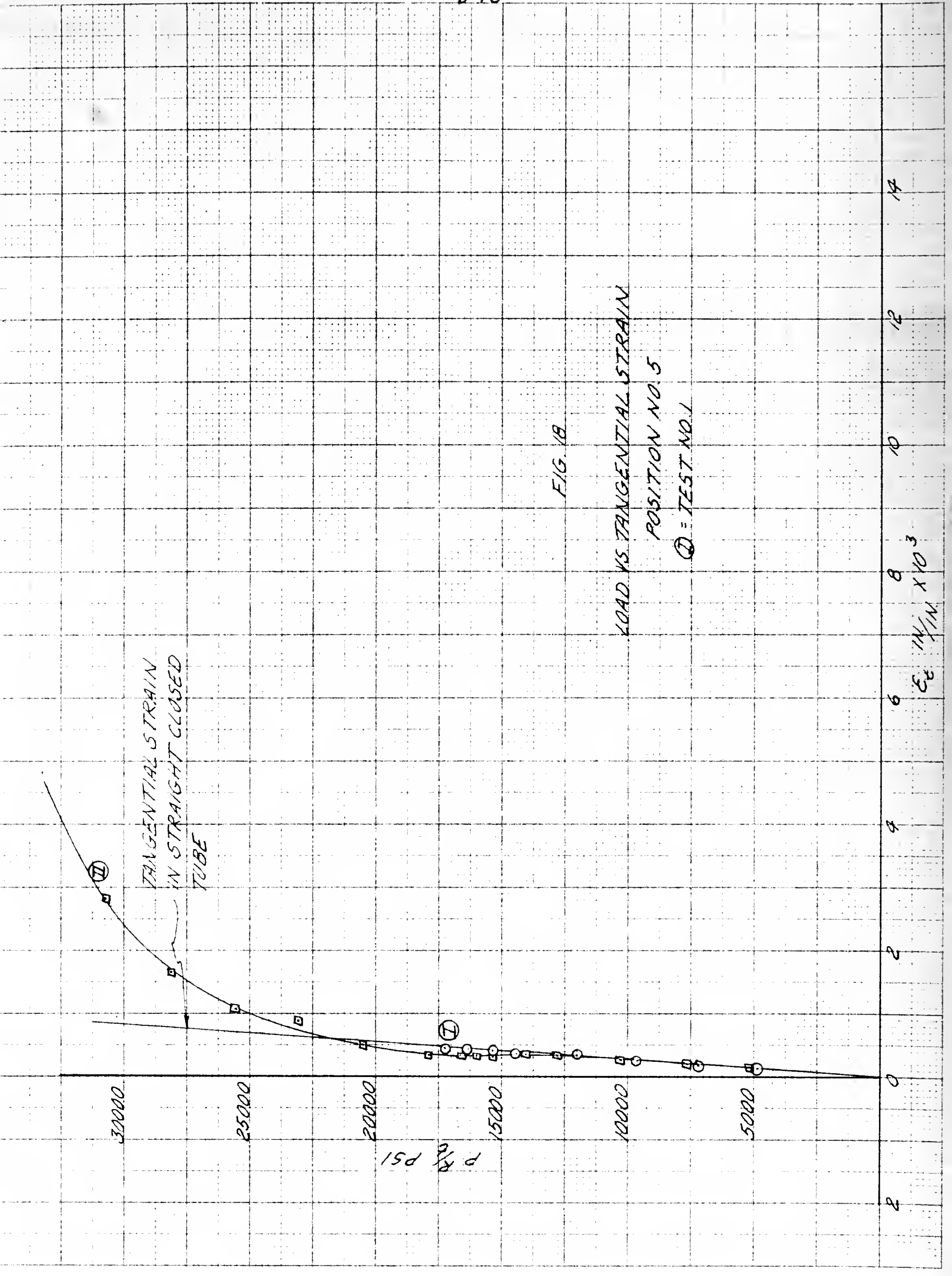


FIG. 18
LOAD VS. TANGENTIAL STRAIN
POSITION NO. 5
Ⓘ = TEST NO. I
TANGENTIAL STRAIN IN STRAIGHT CLOSED TUBE
Ⓘ
Ⓘ
ϵ_t IN/IN X10^3
0
2
4
6
8
10
12
14
2
5000
10000
15000
20000
25000
30000
p R/t PSI

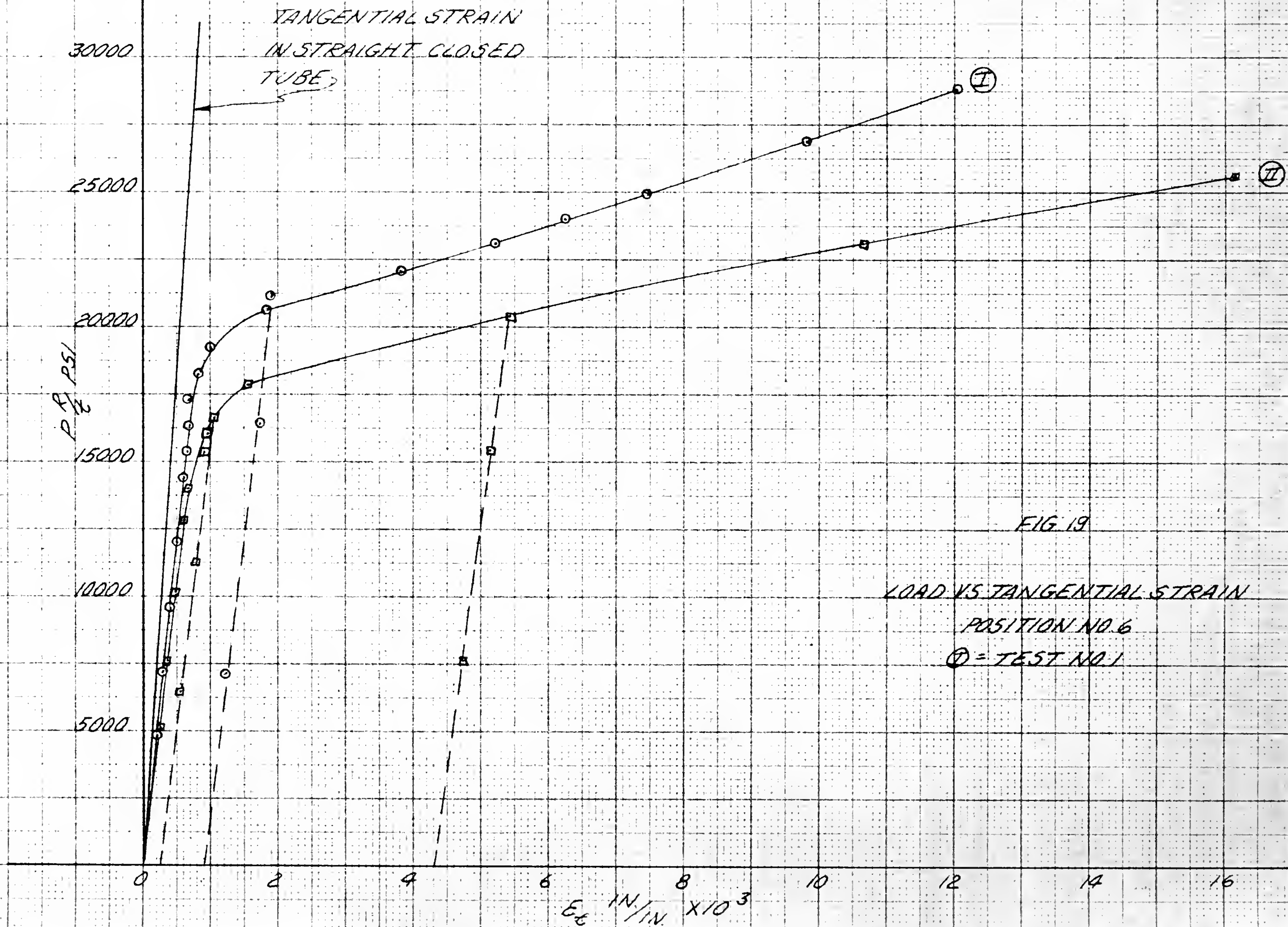


FIG. 19

LOAD VS TANGENTIAL STRAIN

POSITION NO. 6

Ⓘ = TEST NO. 1

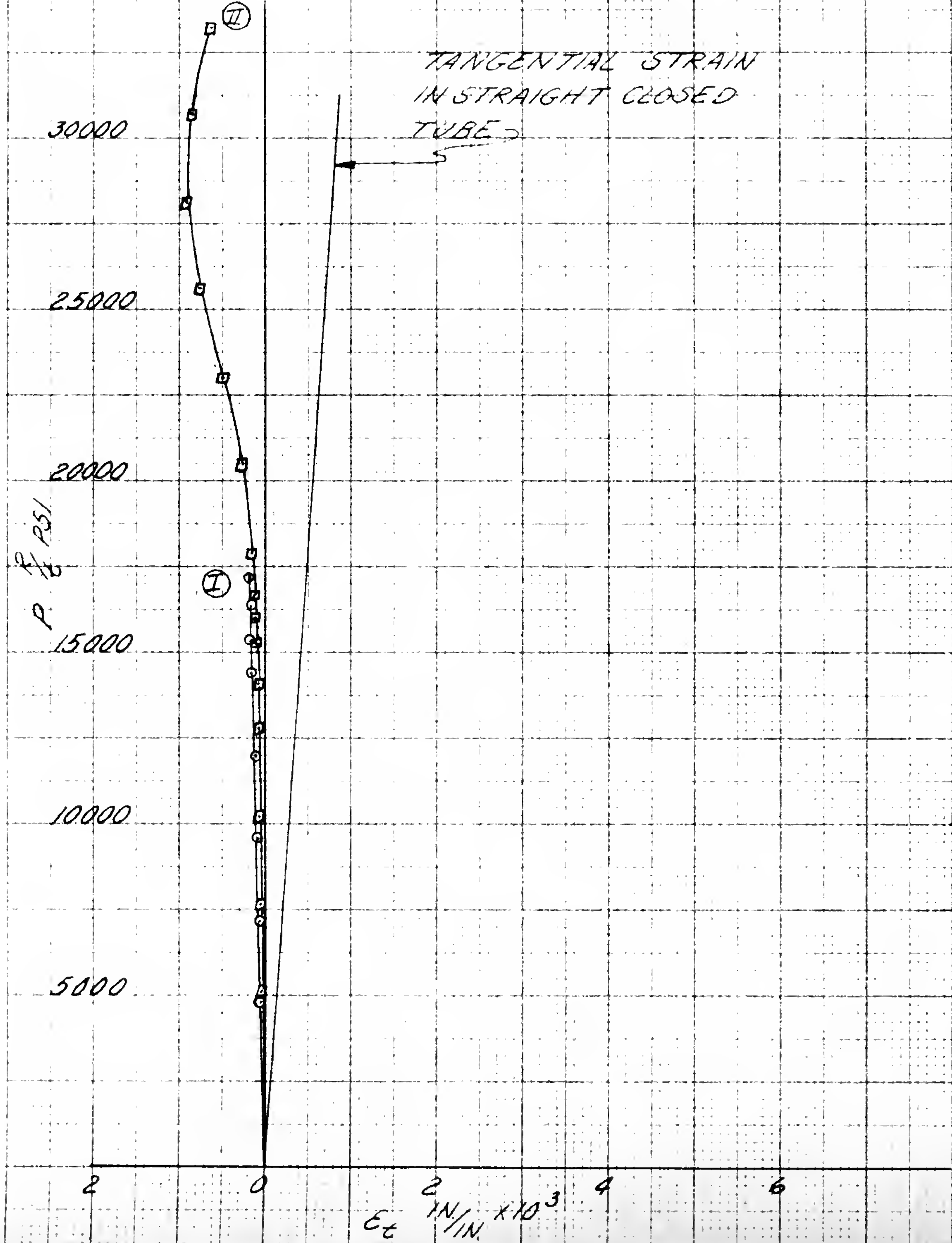


FIG. 20

LOAD VS. TANGENTIAL STRAIN

POSITION NO. 7

(I) = TEST NO. 1

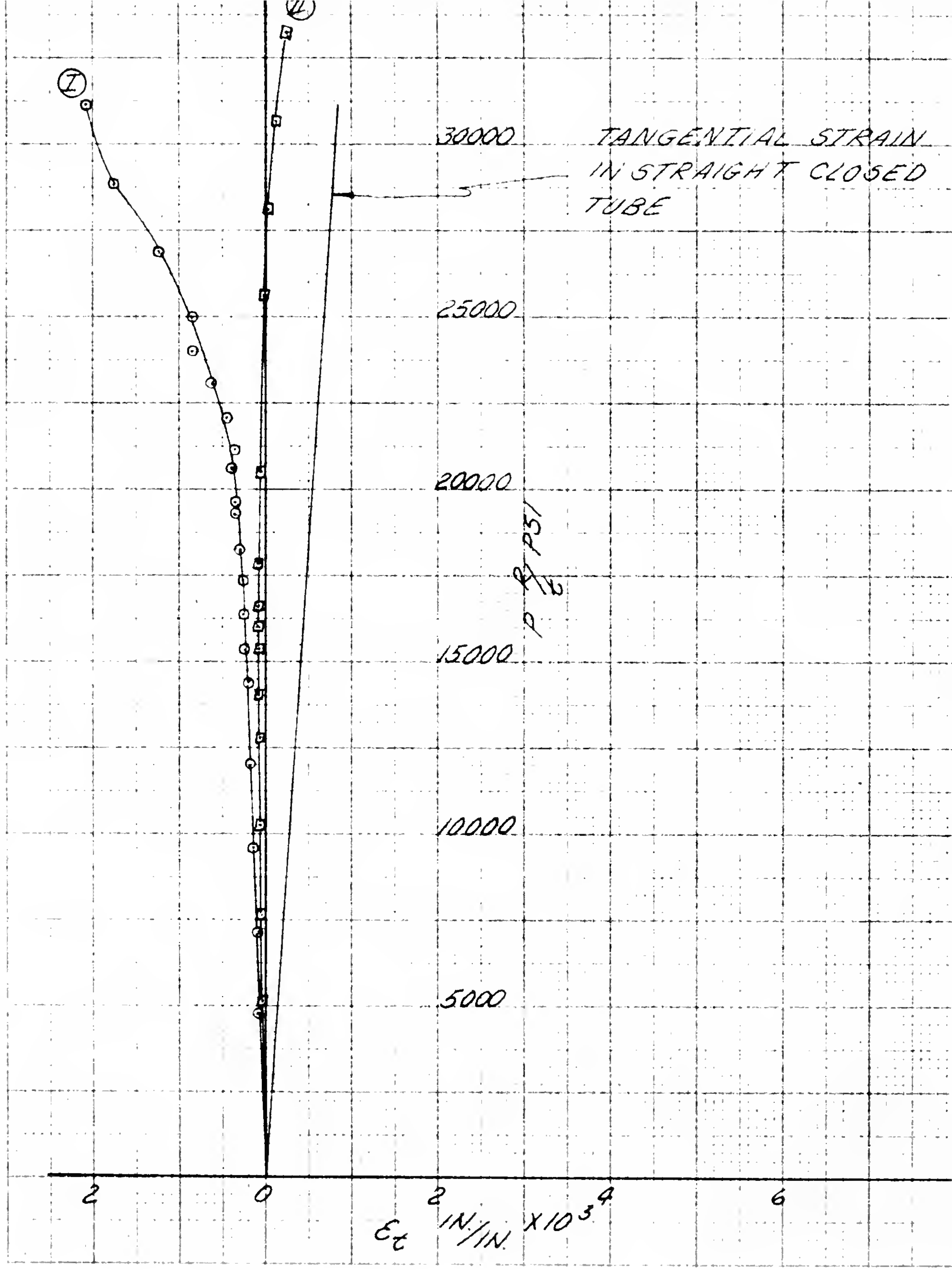


FIG 21

LOAD VS TANGENTIAL STRAIN

POSITION NO. 8

① = TEST NO. 1

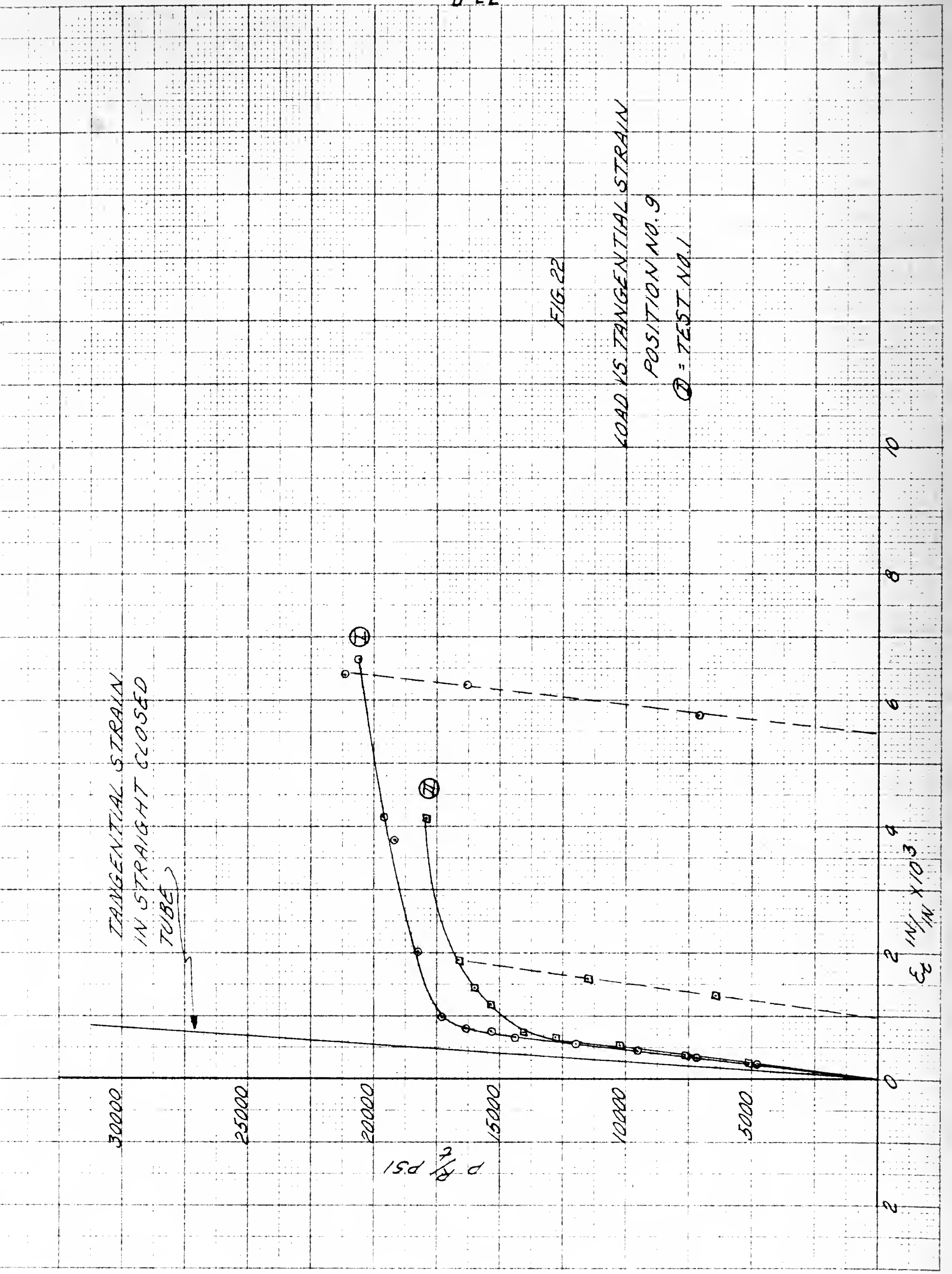


FIG. 22
LOAD VS. TANGENTIAL STRAIN
POSITION NO. 9
Ⓘ = TEST NO. 1
TANGENTIAL STRAIN
IN STRAIGHT CLOSED
TUBE
Ⅰ
Ⅱ
30000
25000
20000
15000
10000
5000
0
p r/t psi
2
4
6
8
10
ε_t IN/IN X10^3

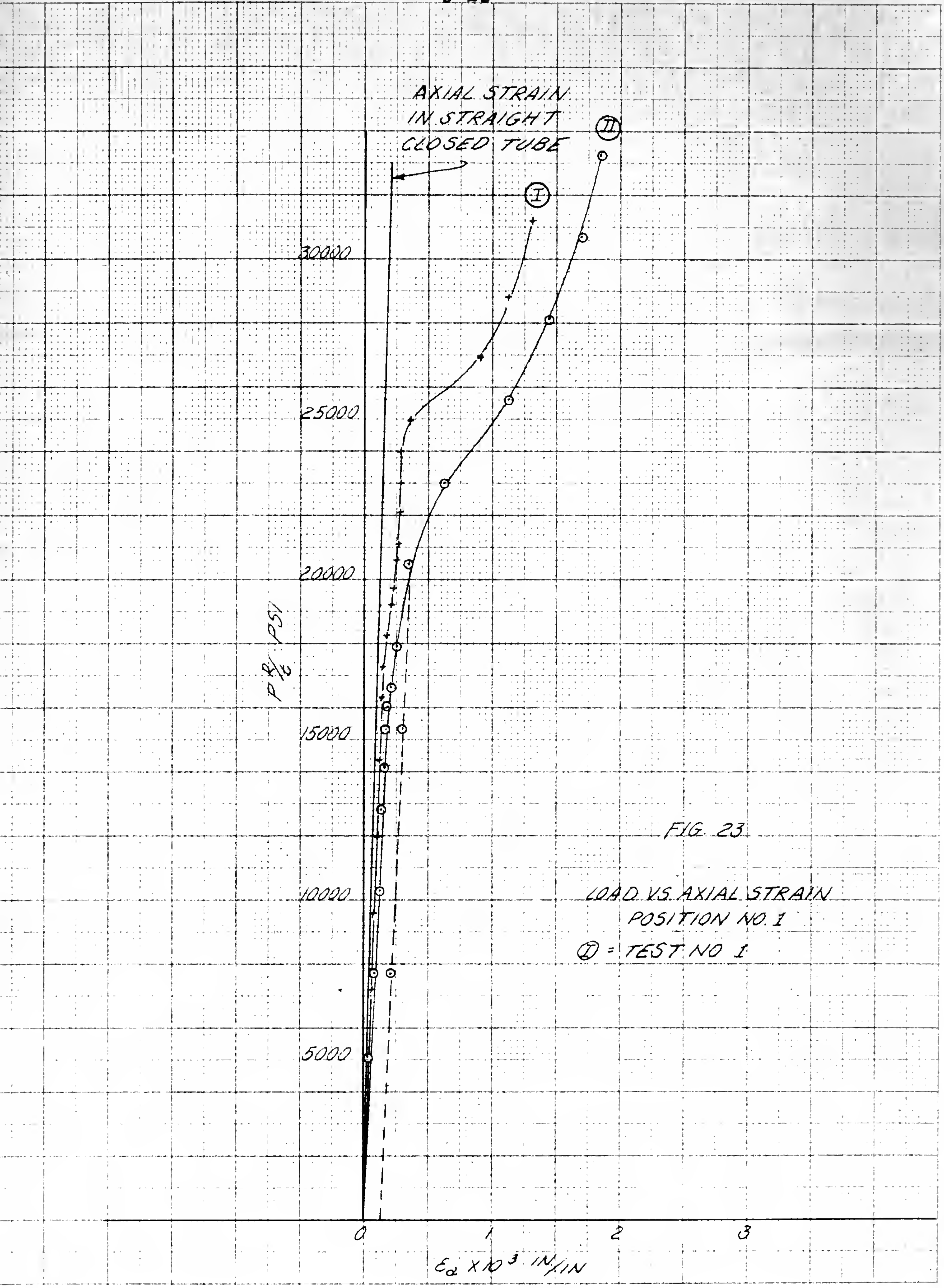
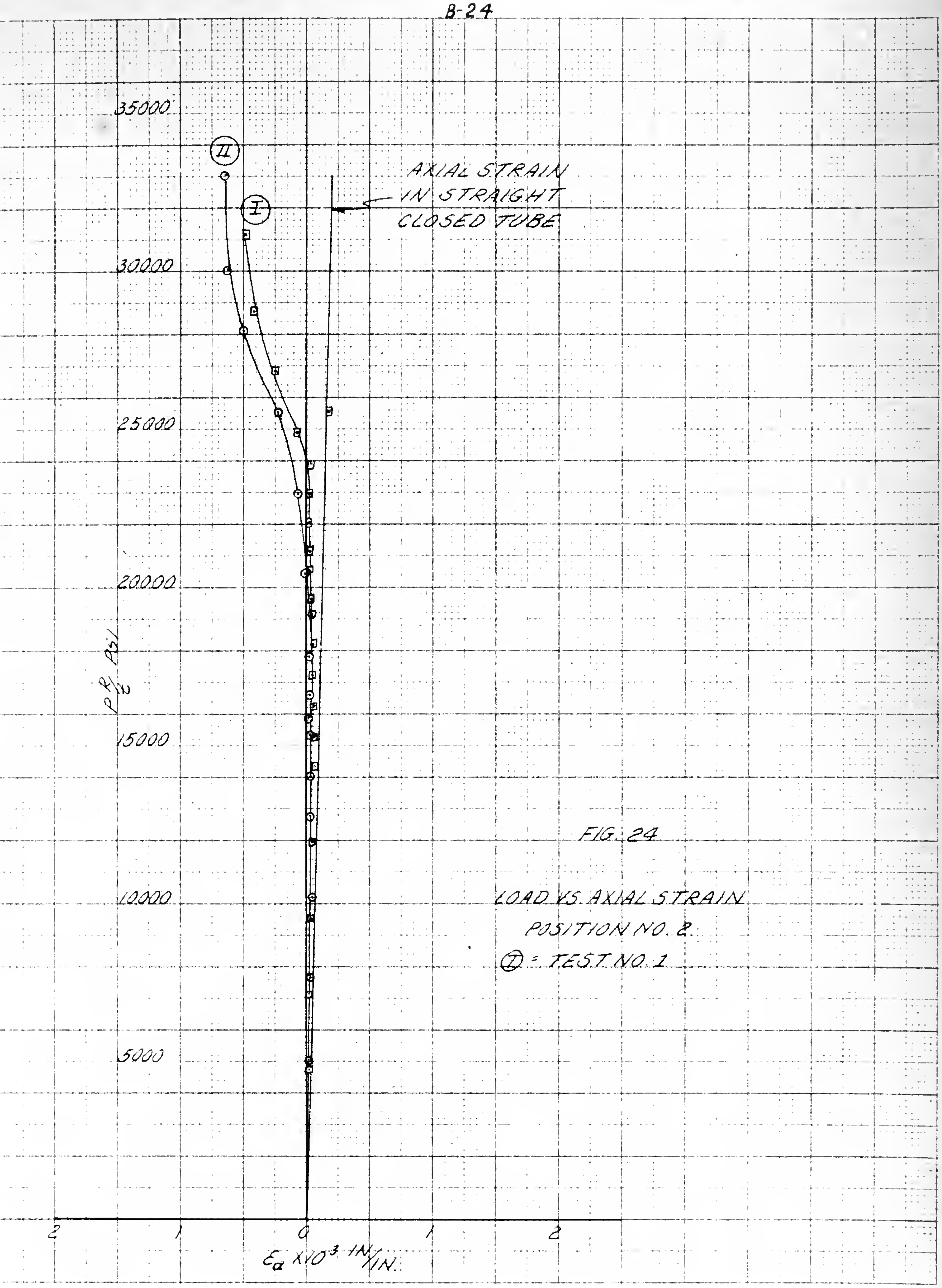


FIG. 23

LOAD VS. AXIAL STRAIN
POSITION NO. 1



35000
30000
25000
20000
15000
10000
5000
P R/t PSI
2
1
0
1
2
Ea X10^-3 IN/IN.
II
I
AXIAL STRAIN
IN STRAIGHT
CLOSED TUBE
FIG. 24
LOAD VS. AXIAL STRAIN
POSITION NO. 2
(I) = TEST NO. 1

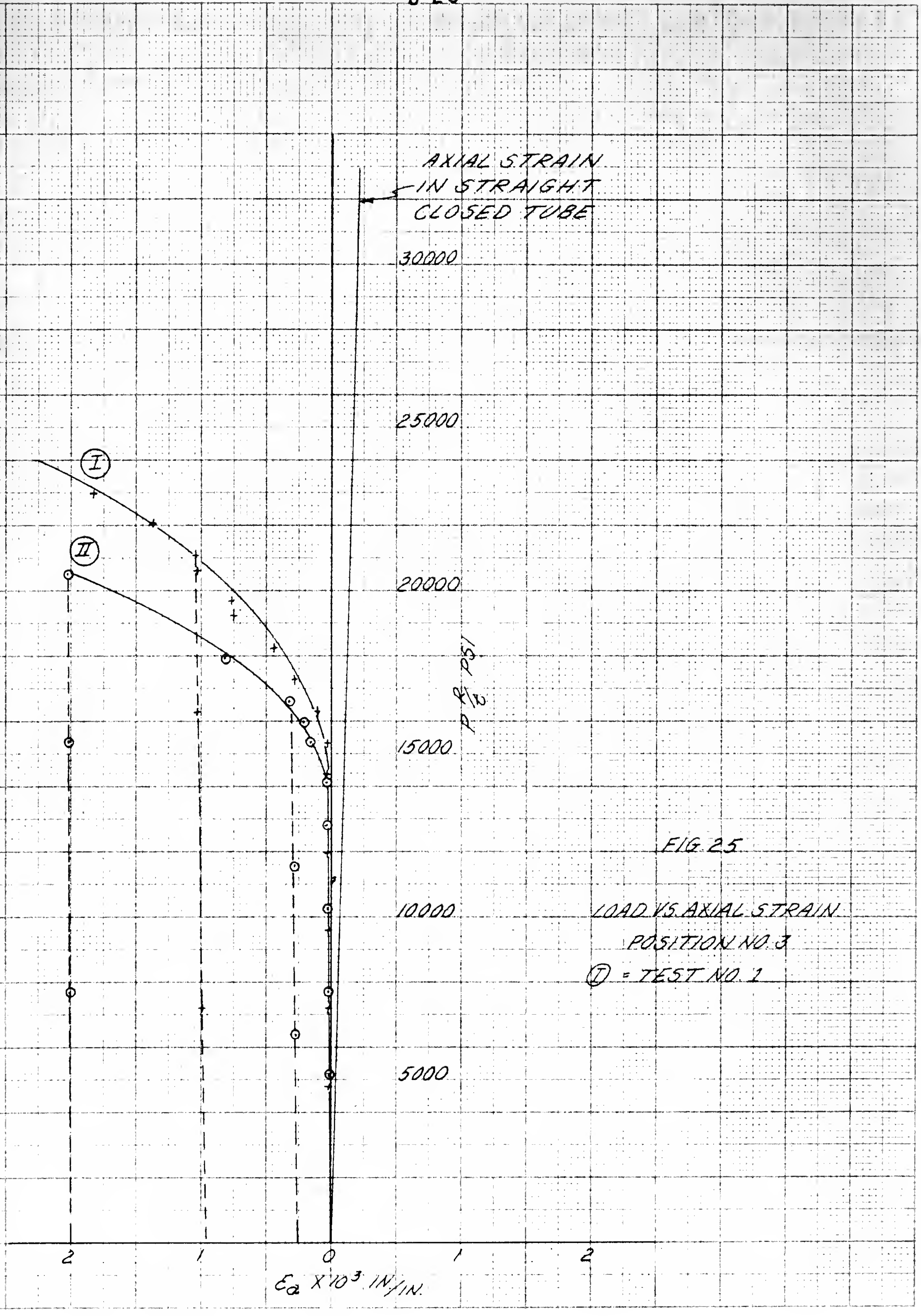
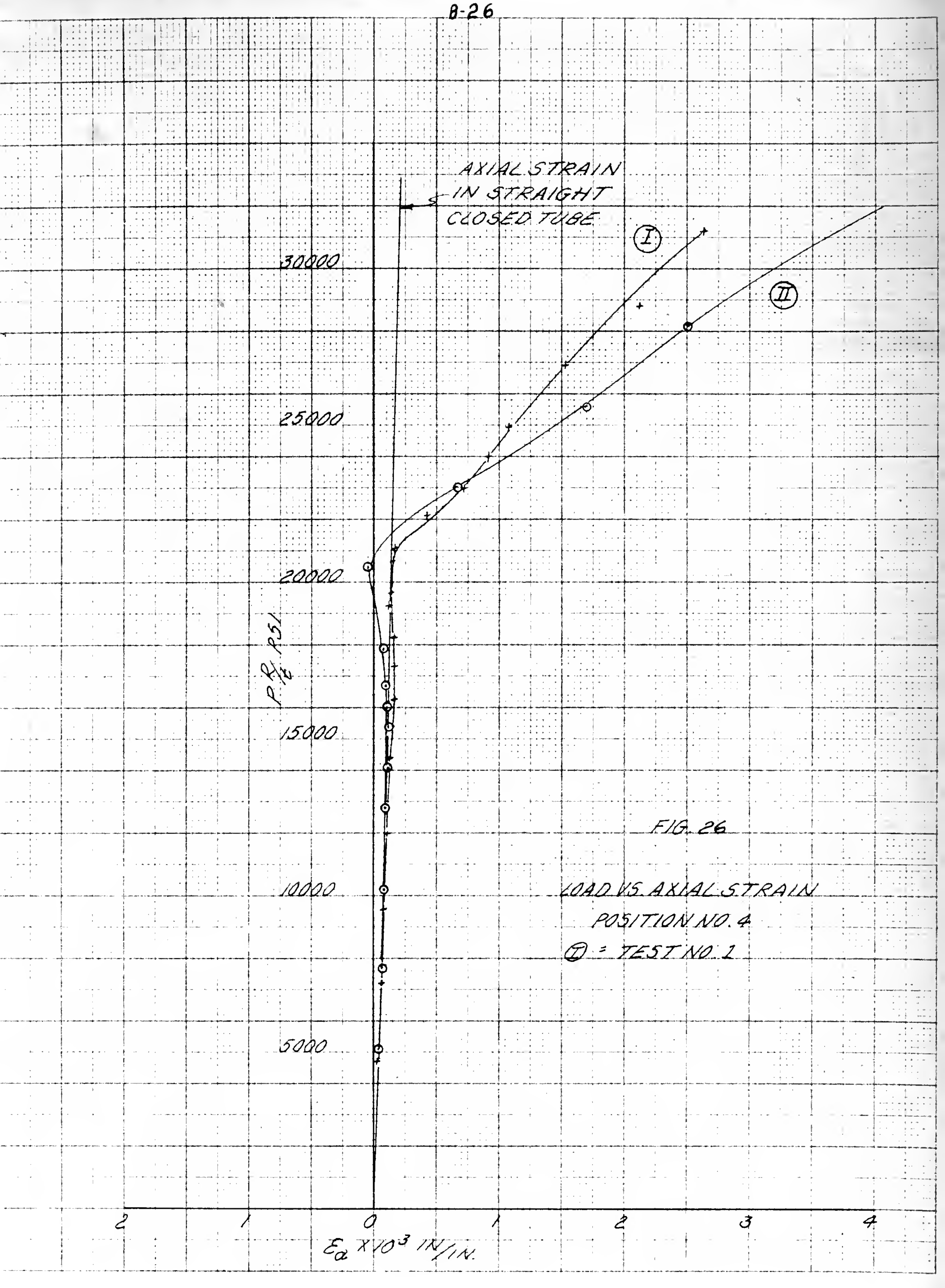


FIG. 25

LOAD VS. AXIAL STRAIN
POSITION NO. 3
(I) = TEST NO. 1


AXIAL STRAIN
IN STRAIGHT
CLOSED TUBE
I
II
30000
25000
20000
15000
10000
5000
P R/t PSI
2
1
0
1
2
3
4
$\varepsilon_a \times 10^3$ IN/IN.
FIG. 26
LOAD VS. AXIAL STRAIN
POSITION NO. 4
(I) = TEST NO. 1

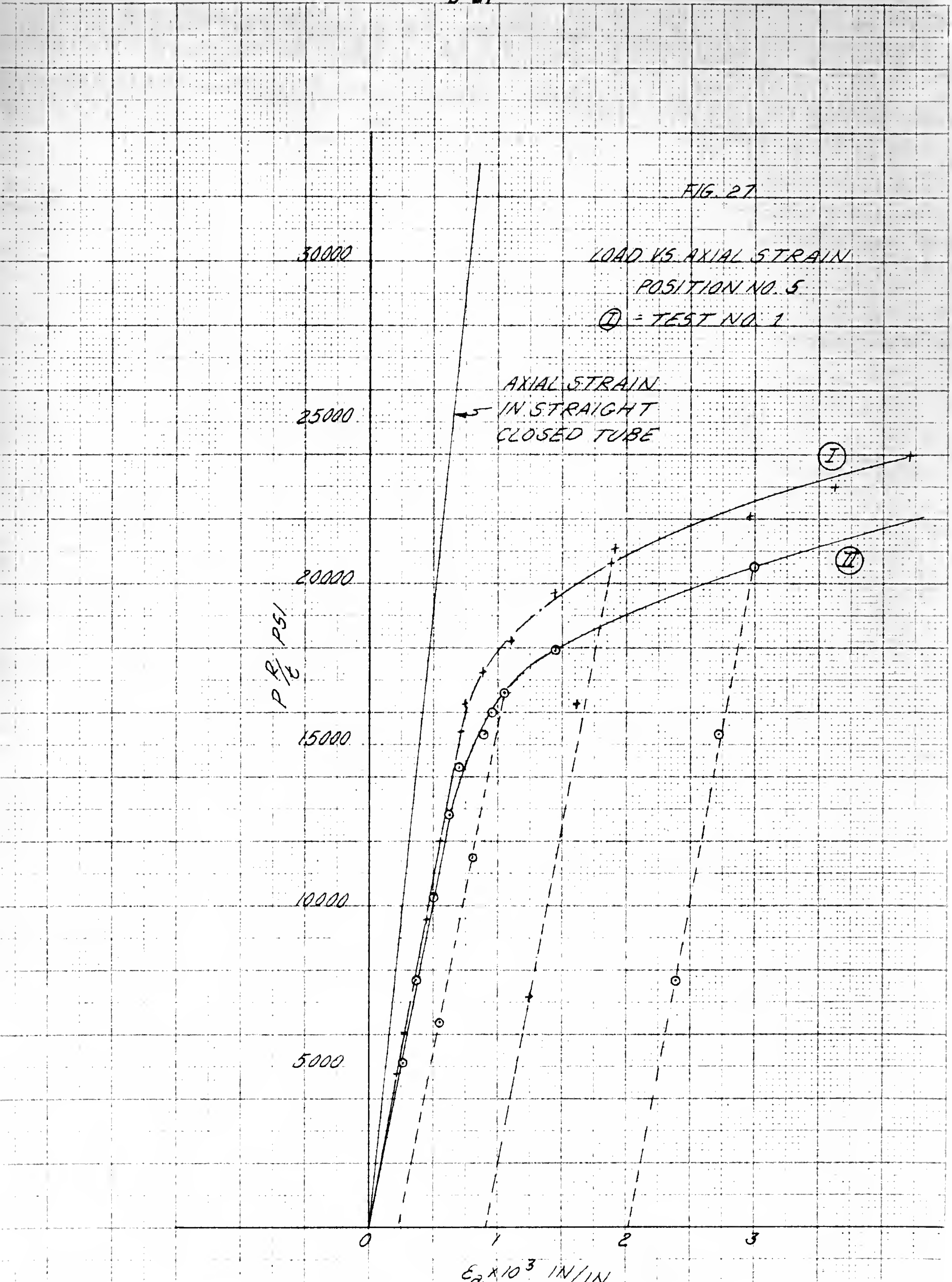


FIG. 27
LOAD VS. AXIAL STRAIN
POSITION NO. 5
(I) = TEST NO. 1
AXIAL STRAIN IN STRAIGHT CLOSED TUBE
I
II
30000
25000
20000
15000
10000
5000
P R/t PSI
0
1
2
3
εa x 10³ IN/IN

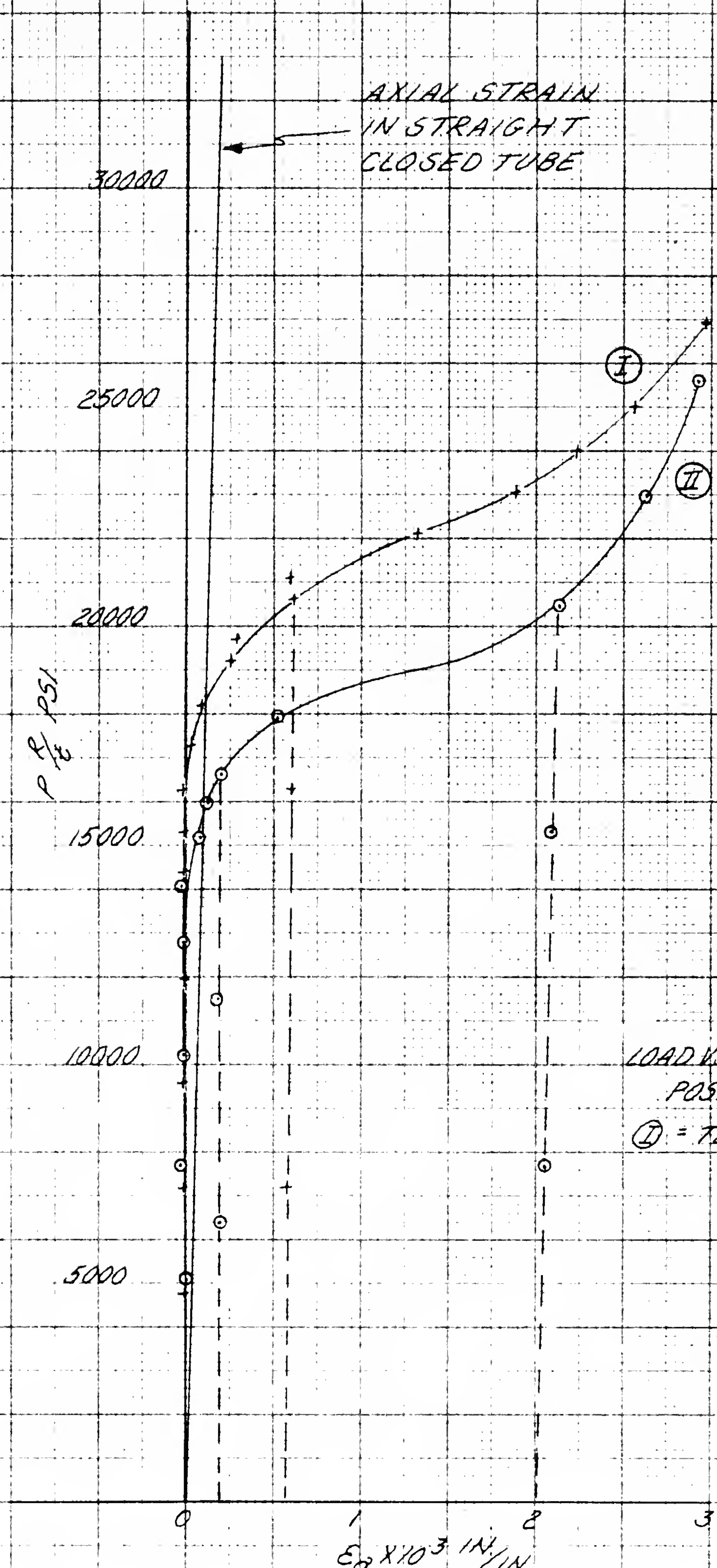


FIG. 28

LOAD VS AXIAL STRAIN
POSITION NO. 6
(I) = TEST NO. 1

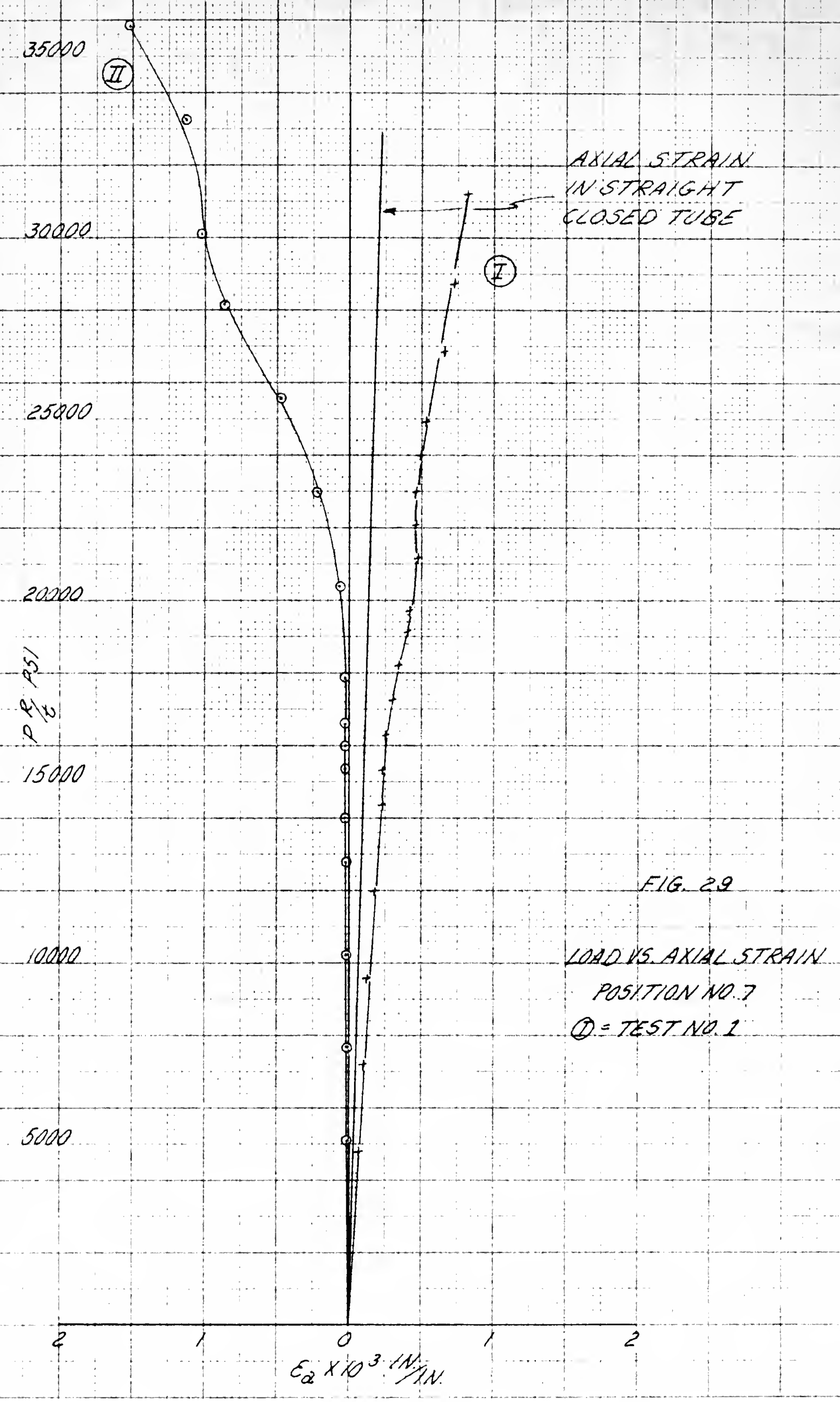


FIG. 29

LOAD VS. AXIAL STRAIN
POSITION NO. 7
① = TEST NO. 1

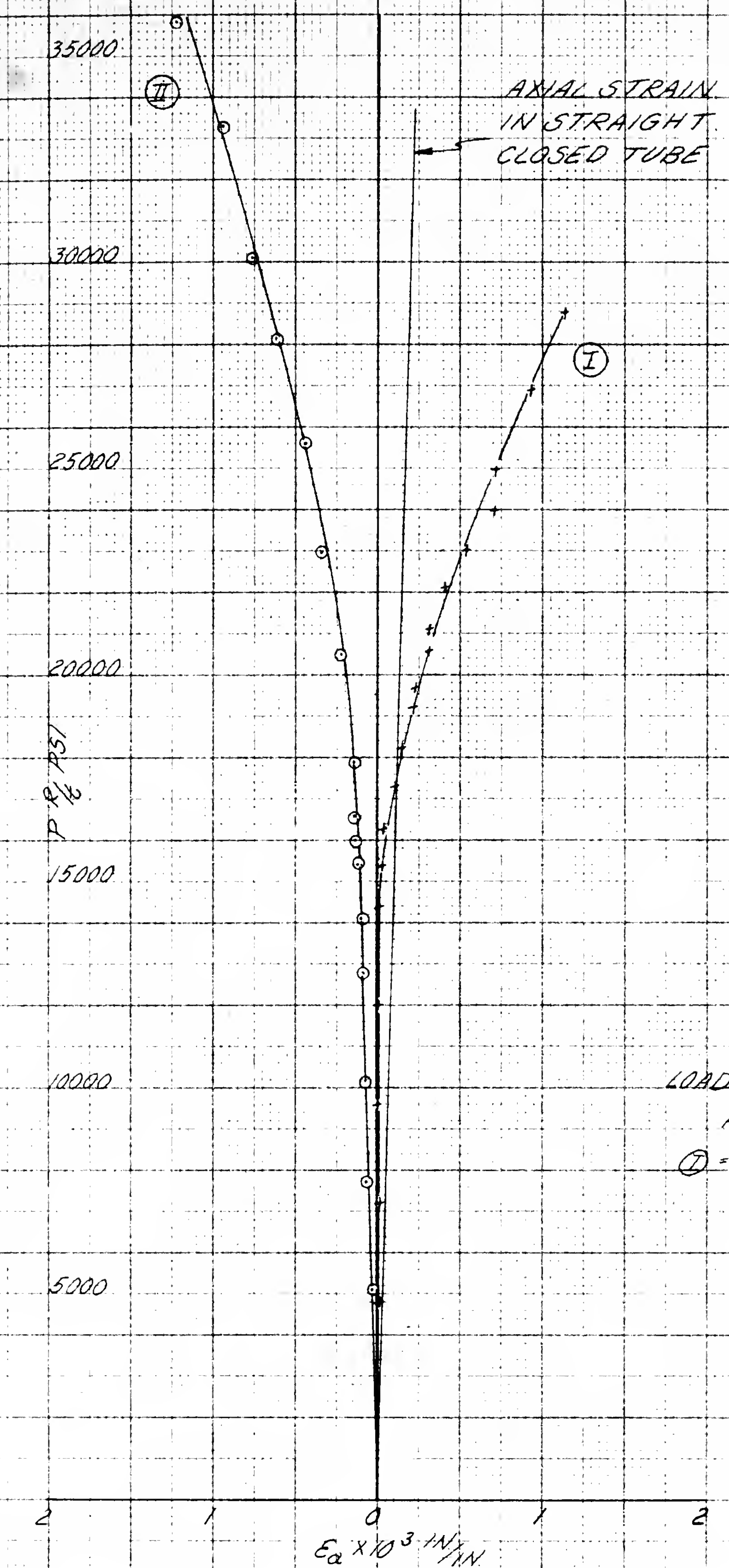


FIG. 30

LOAD VS. AXIAL STRAIN
POSITION NO. 8
(I) = TEST NO 1

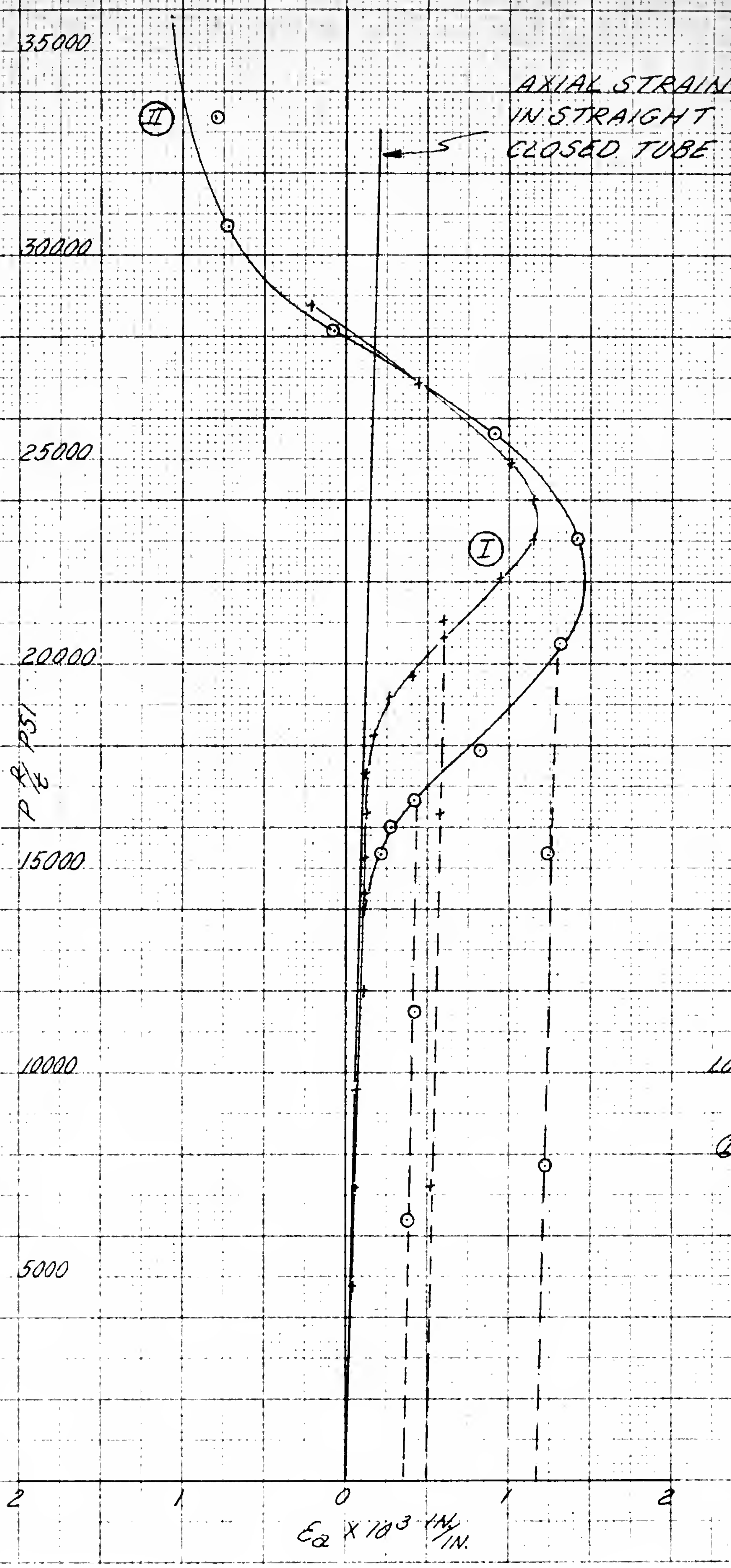


FIG. 31

LOAD VS. AXIAL STRAIN

POSITION NO. 9

① = TEST NO. 1

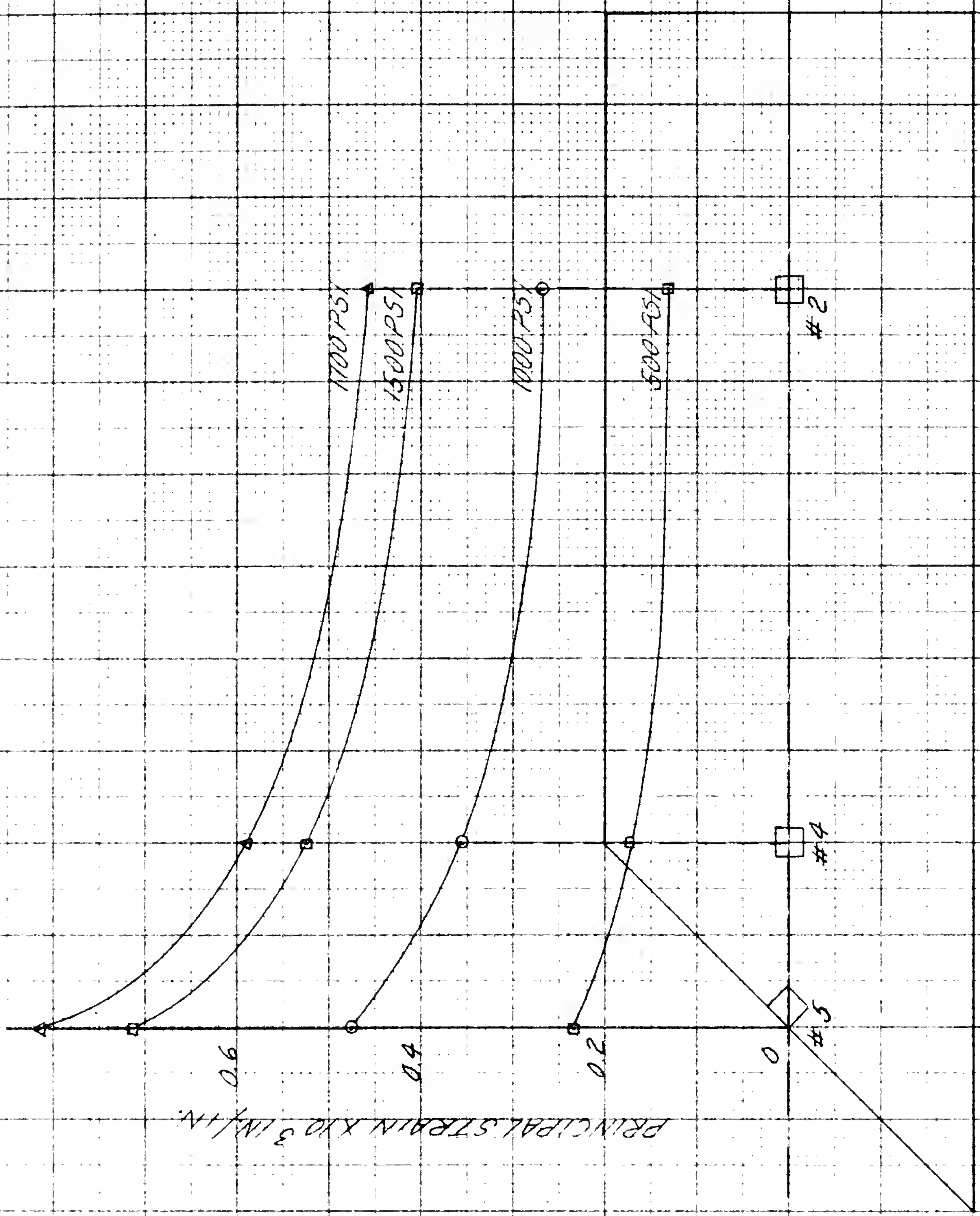


FIG. 32

PRINCIPAL STRAIN VS AXIAL POSITION

TEST NO. I

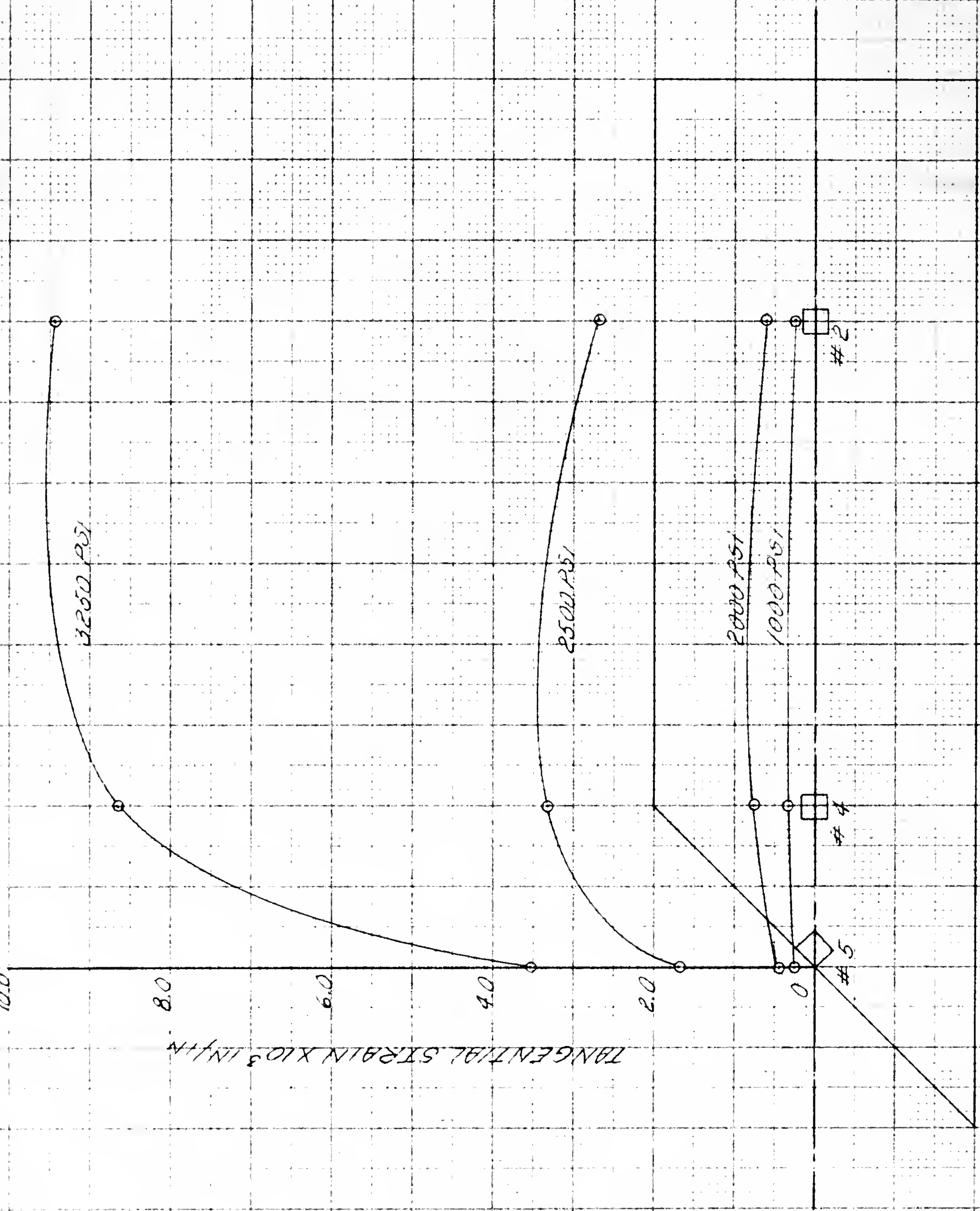


FIG. 33
TANGENTIAL STRAIN VS. AXIAL POSITION
TEST NO. I

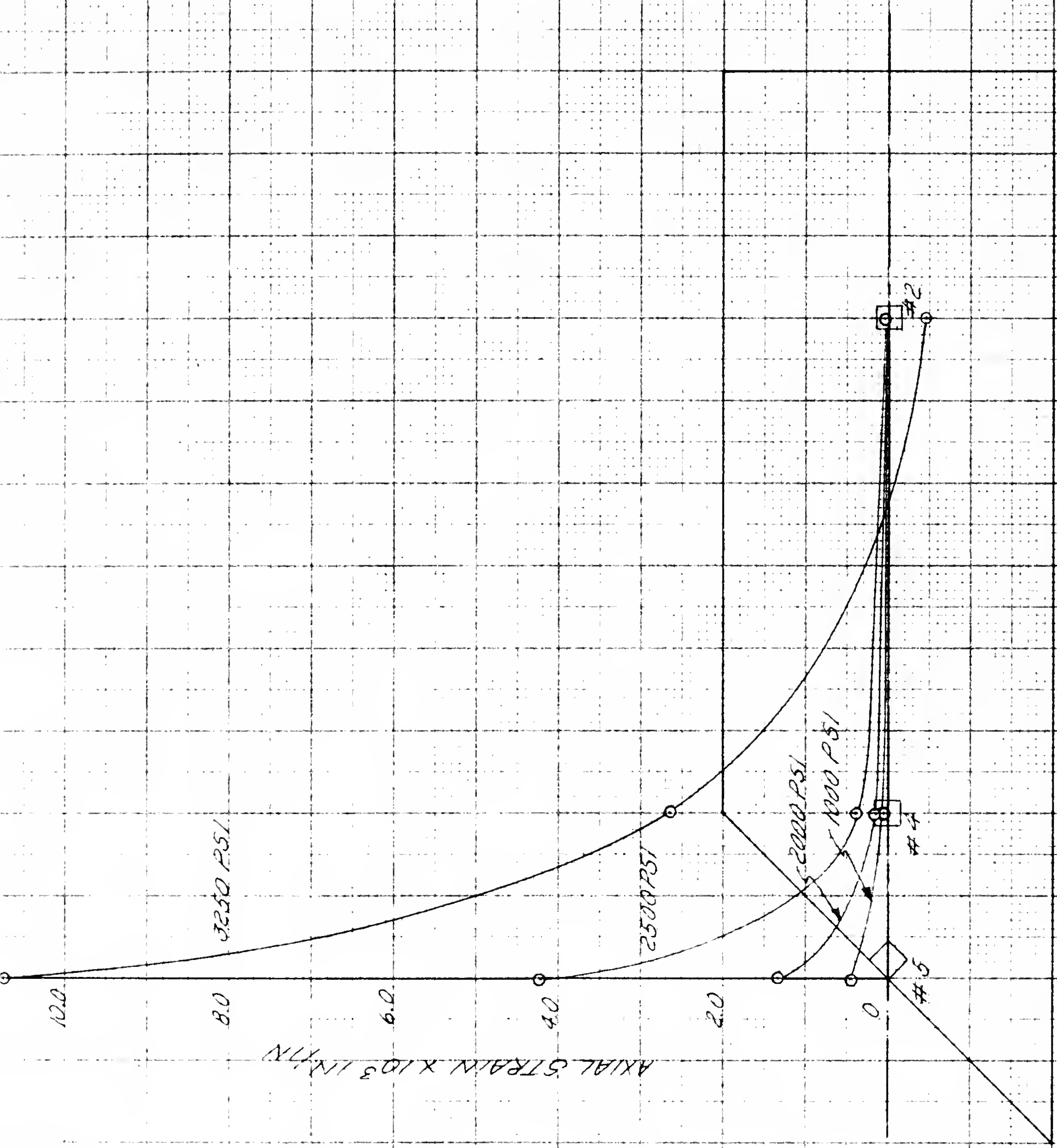


FIG. 34
AXIAL STRAIN VS AXIAL POSITION
TEST NO. I

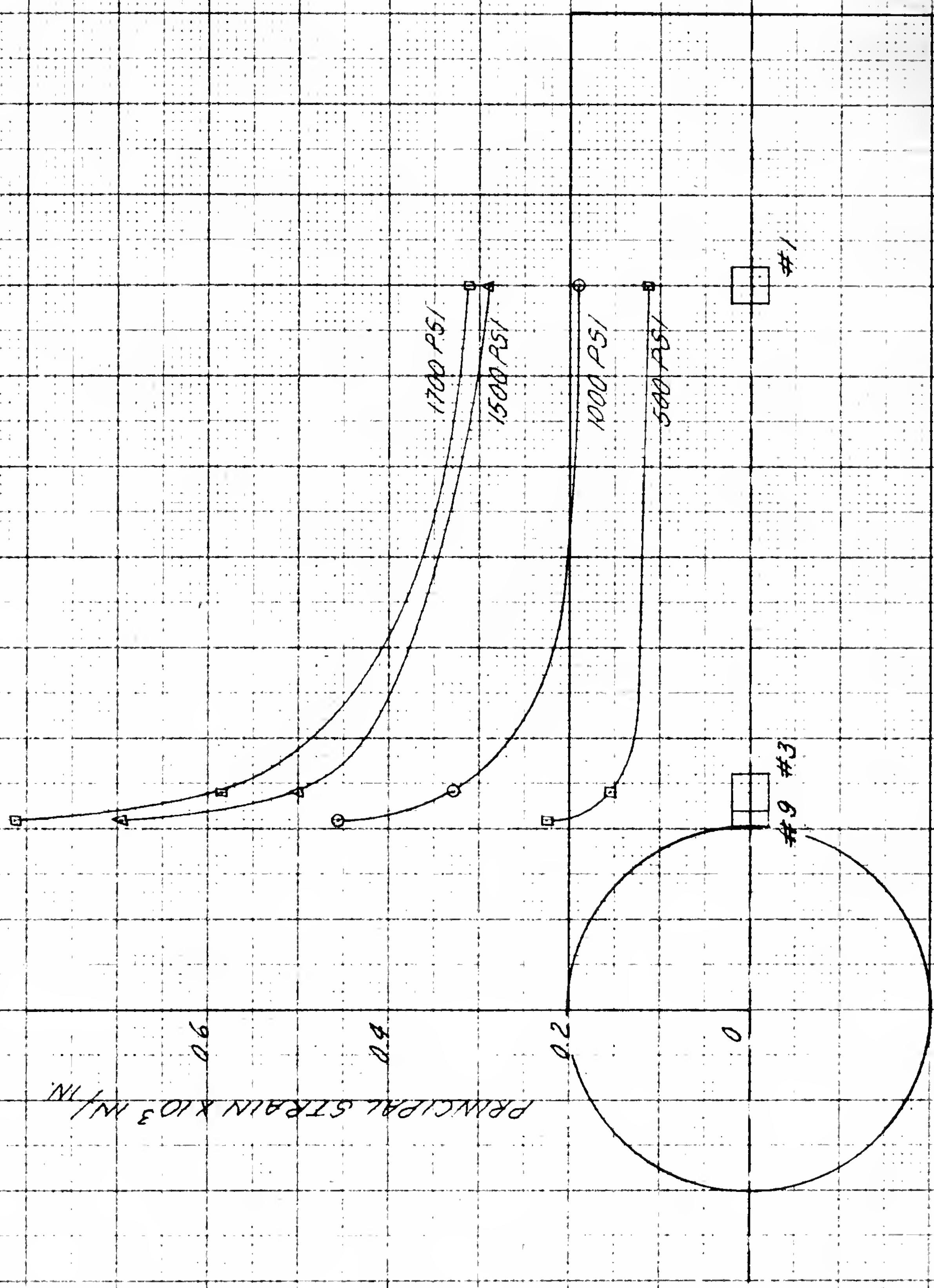


FIG. 35
PRINCIPAL STRAIN VS AXIAL POSITION
TEST NO. I

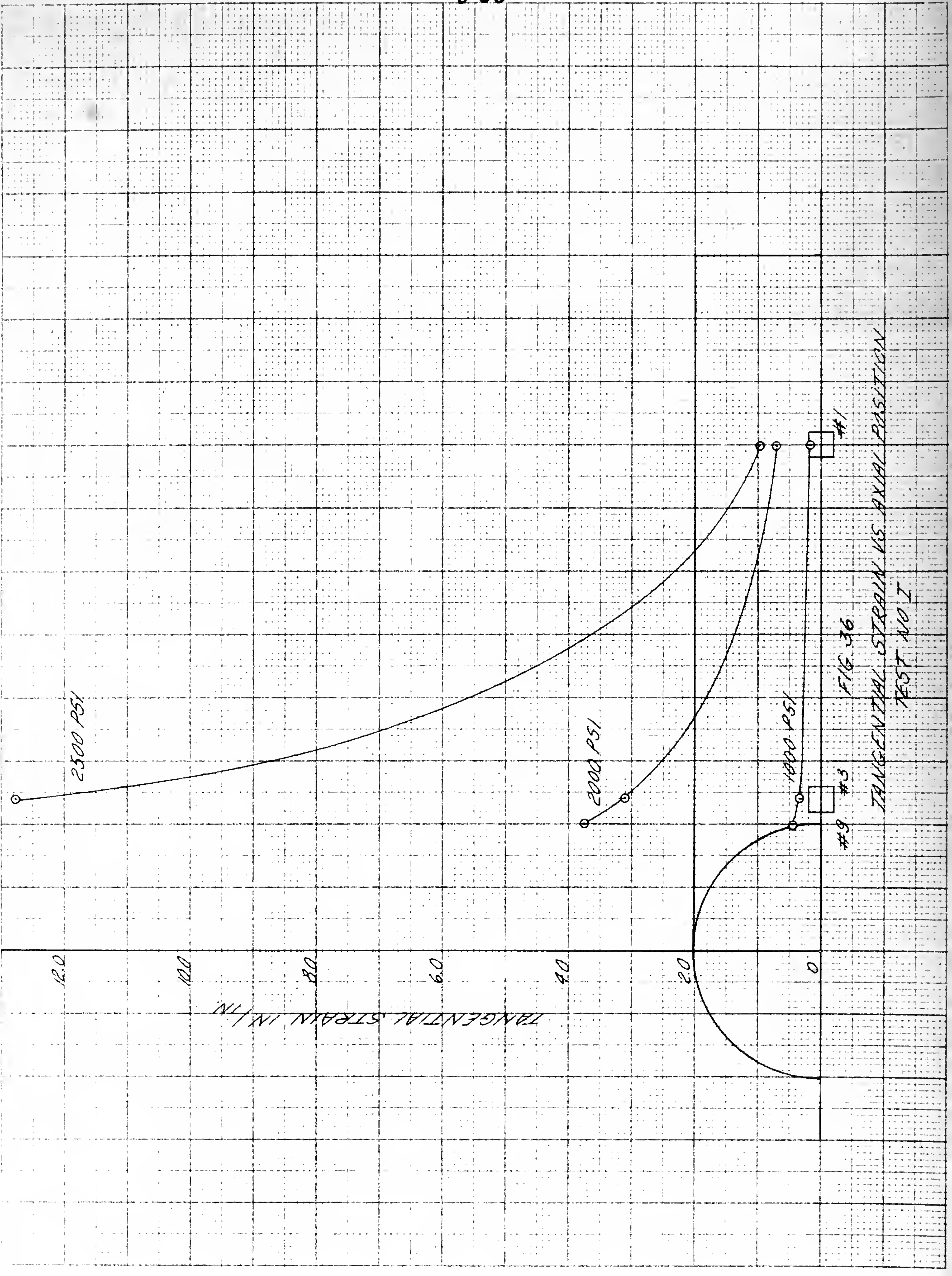


FIG. 36
TANGENTIAL STRAIN VS. AXIAL POSITION
TEST NO I

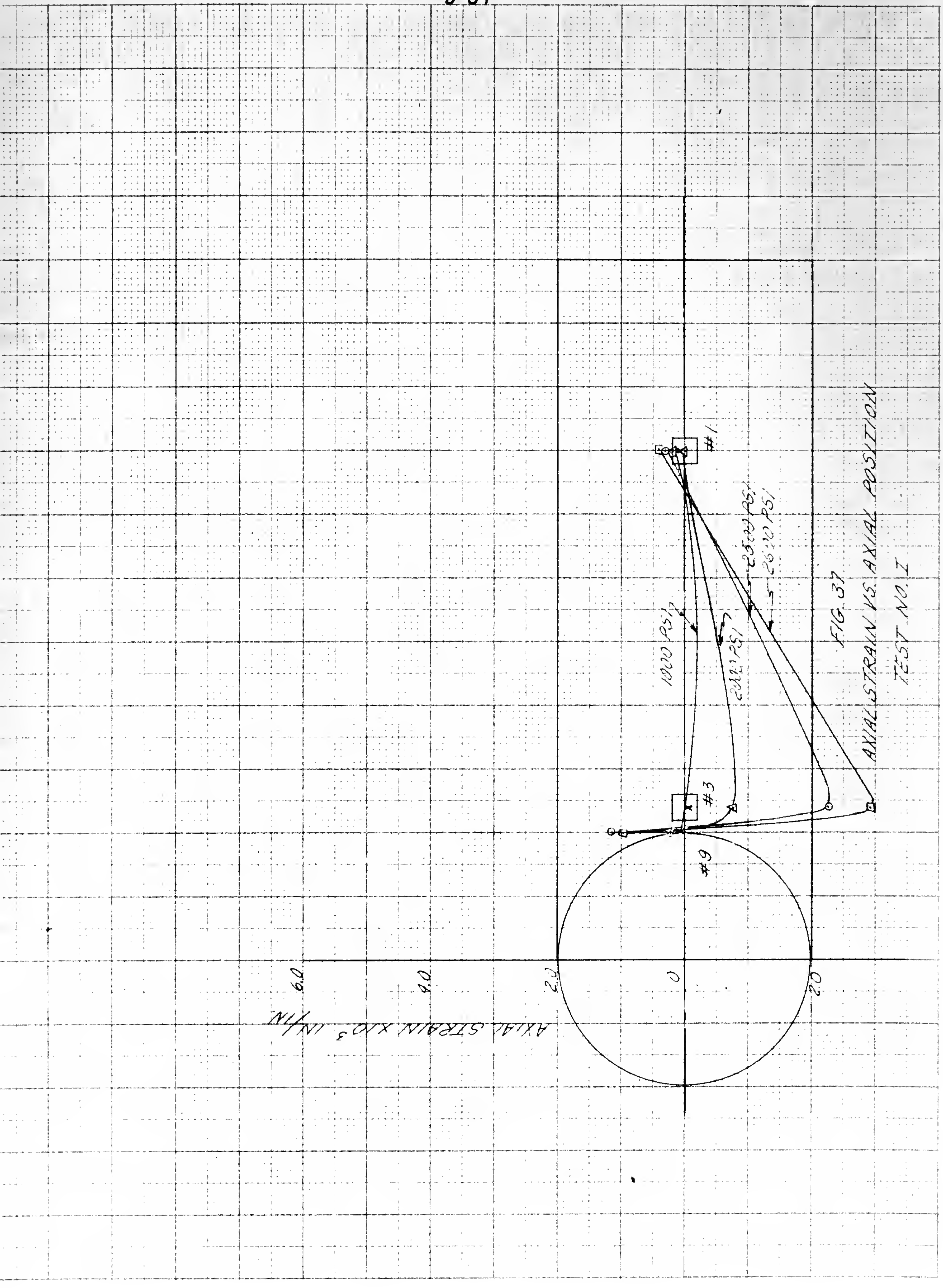


FIG. 37
AXIAL STRAIN VS AXIAL POSITION
TEST NO. I

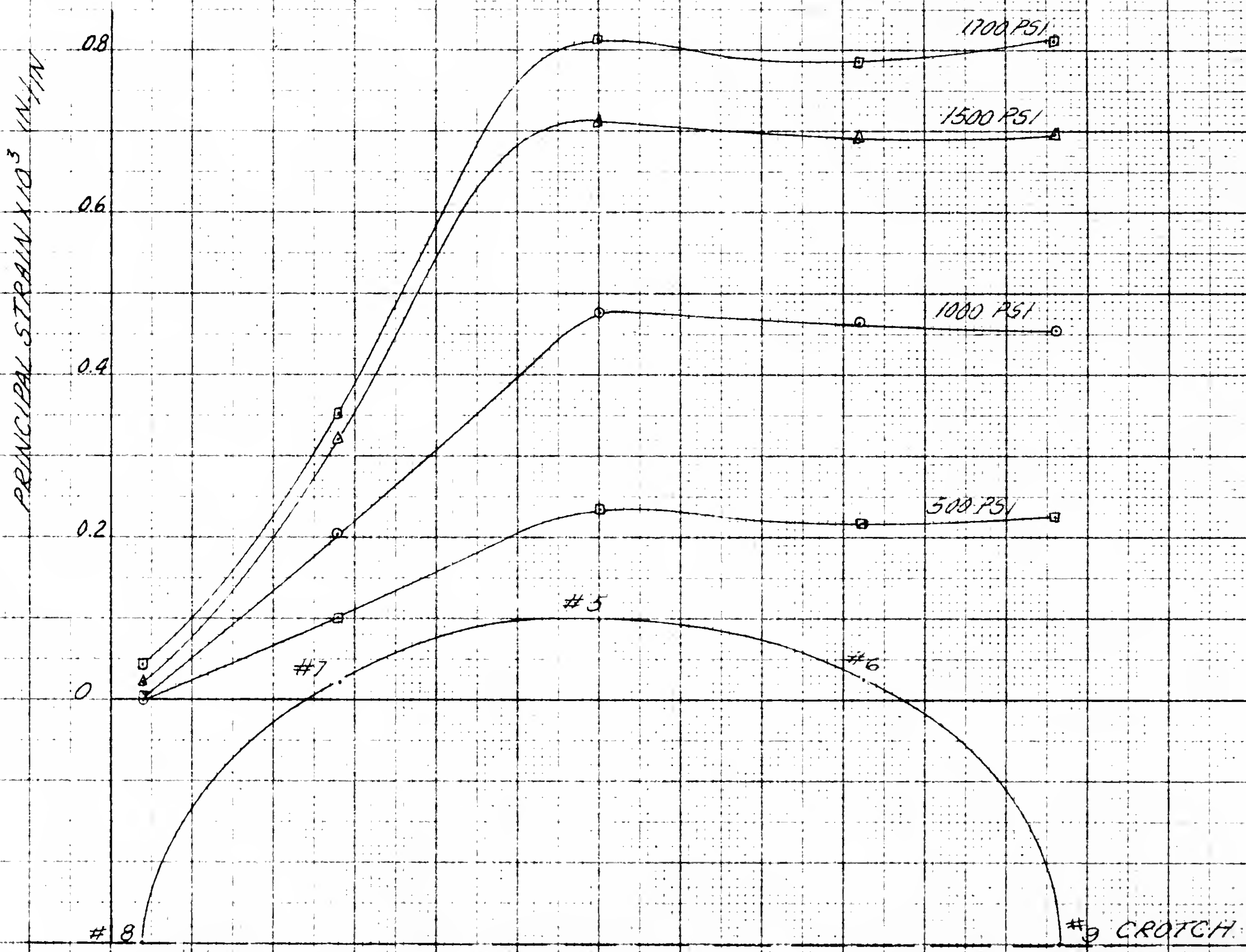


FIG. 38

PRINCIPAL STRAIN VS POSITION ON INTERSECTION

TEST NO. I

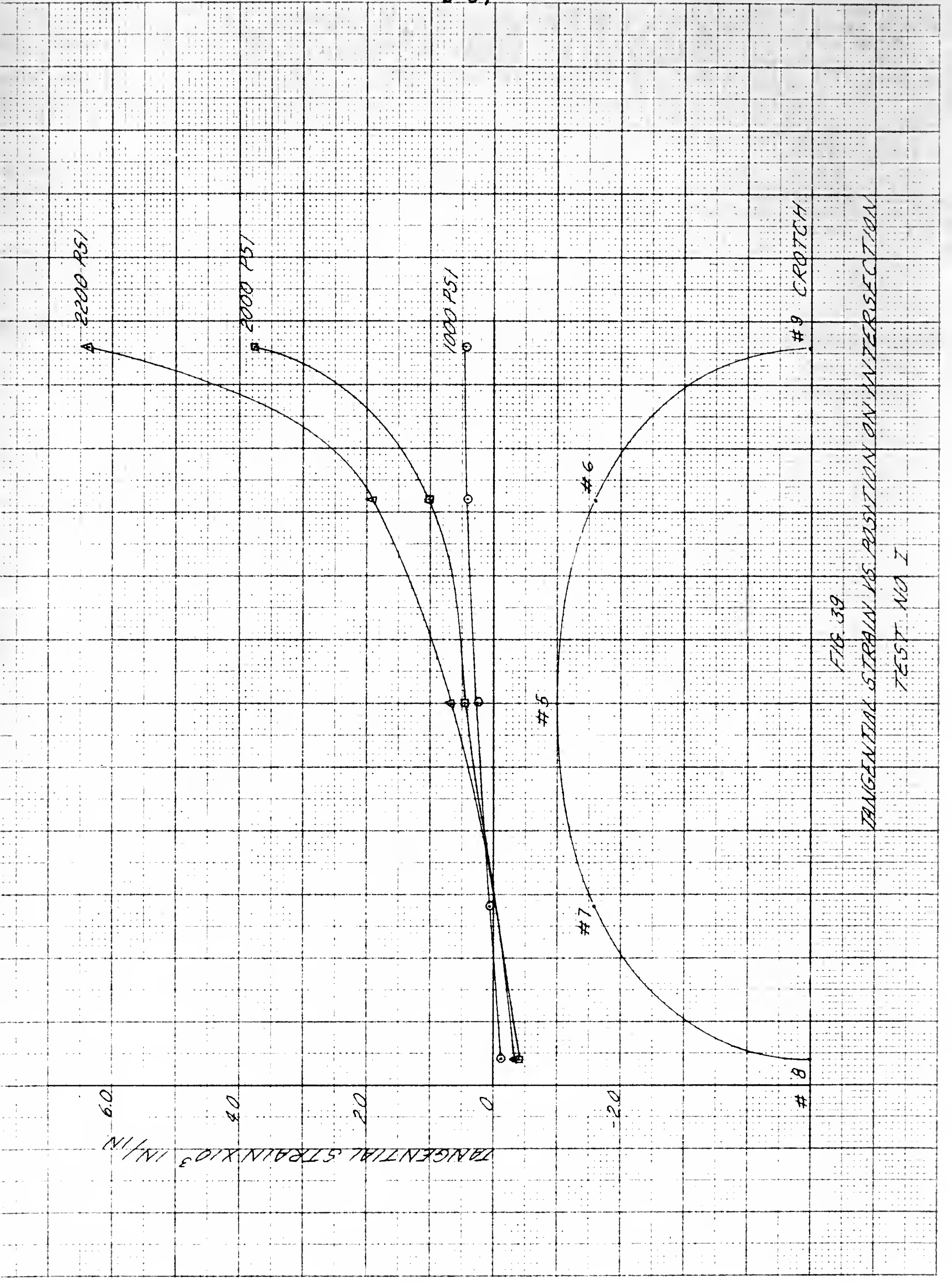


FIG 39
TANGENTIAL STRAIN VS POSITION ON INTERSECTION
TEST NO I

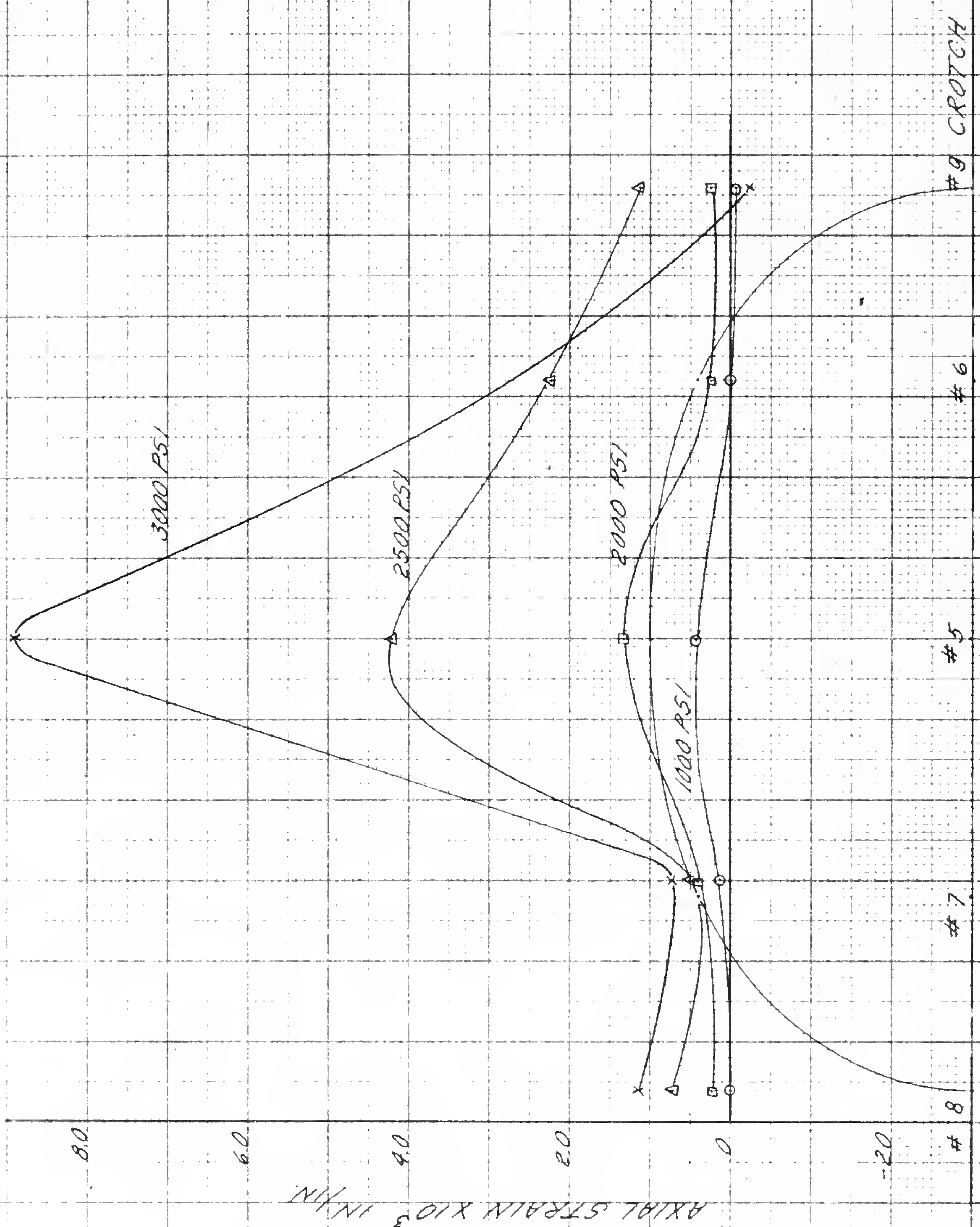


FIG 40
AXIAL STRAIN VS POSITION OF INTERSECTION
TEST NO I

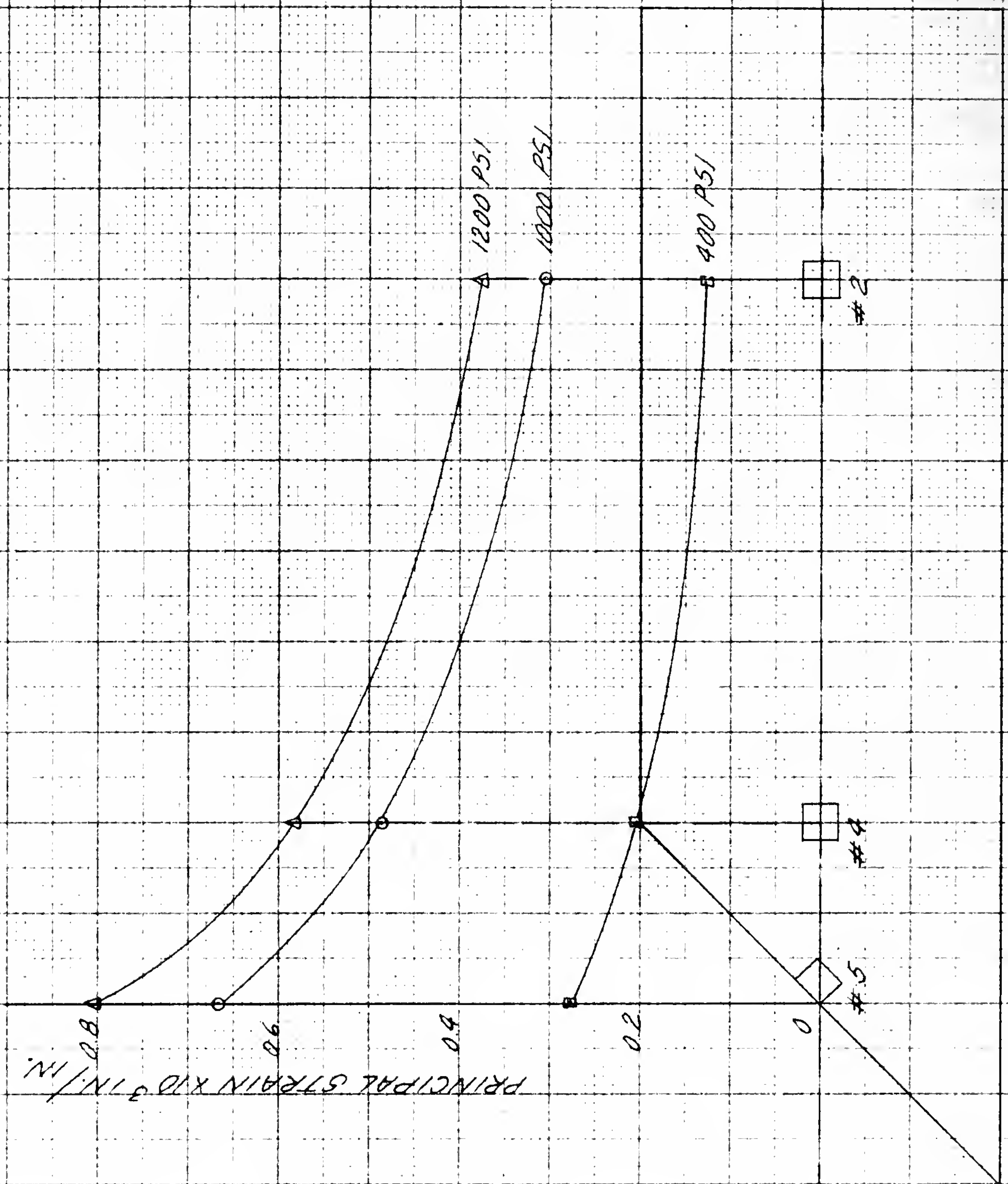


FIG. 41
PRINCIPAL STRAIN VS AXIAL POSITION
TEST NO. II

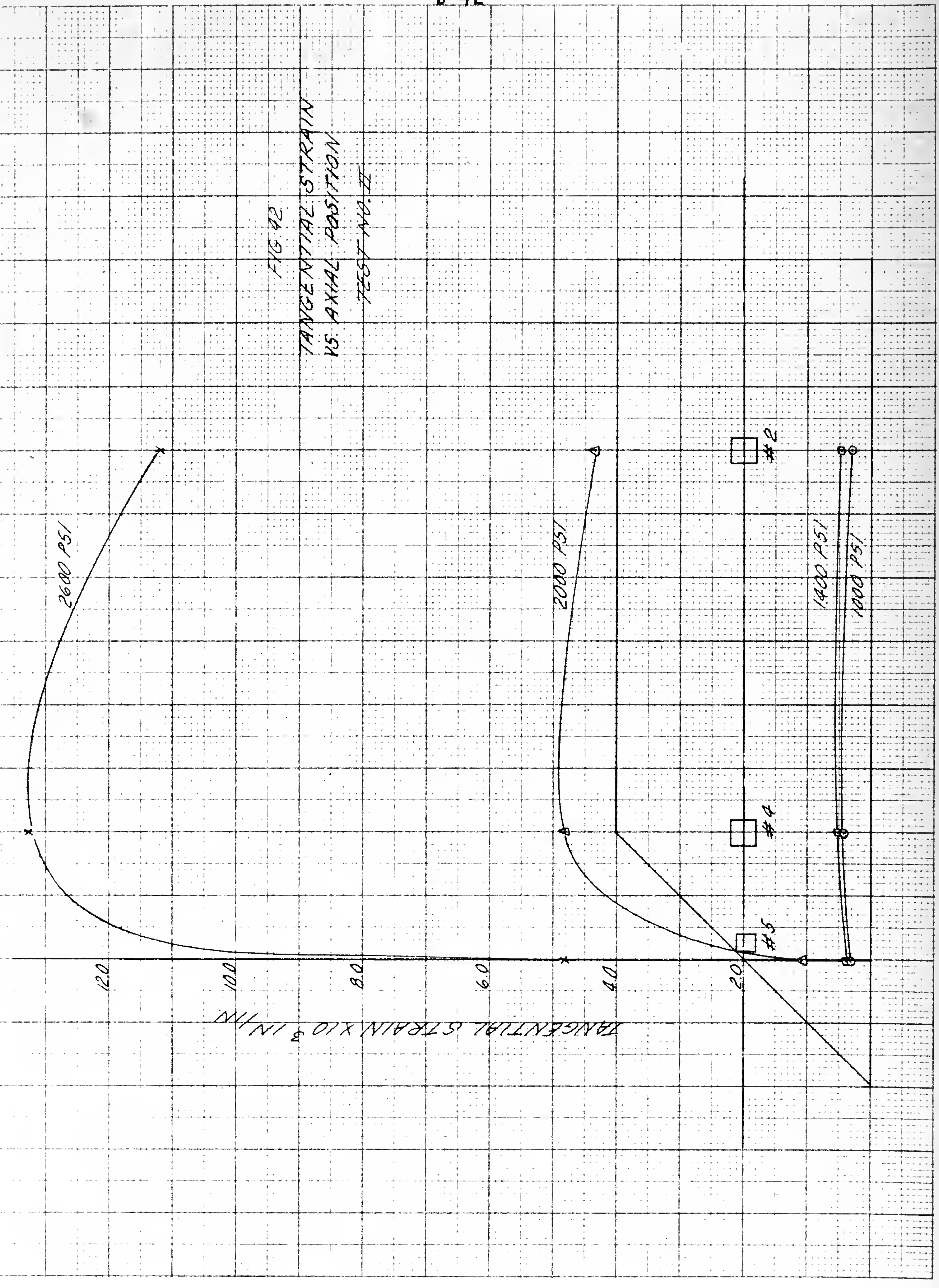


FIG. 42
TANGENTIAL STRAIN
VS. AXIAL POSITION
TEST NO. II
2600 PSI
2000 PSI
1400 PSI
1000 PSI
#2
#4
#5
12.0
10.0
8.0
6.0
4.0
2.0
TANGENTIAL STRAIN X10⁻³ IN/IN

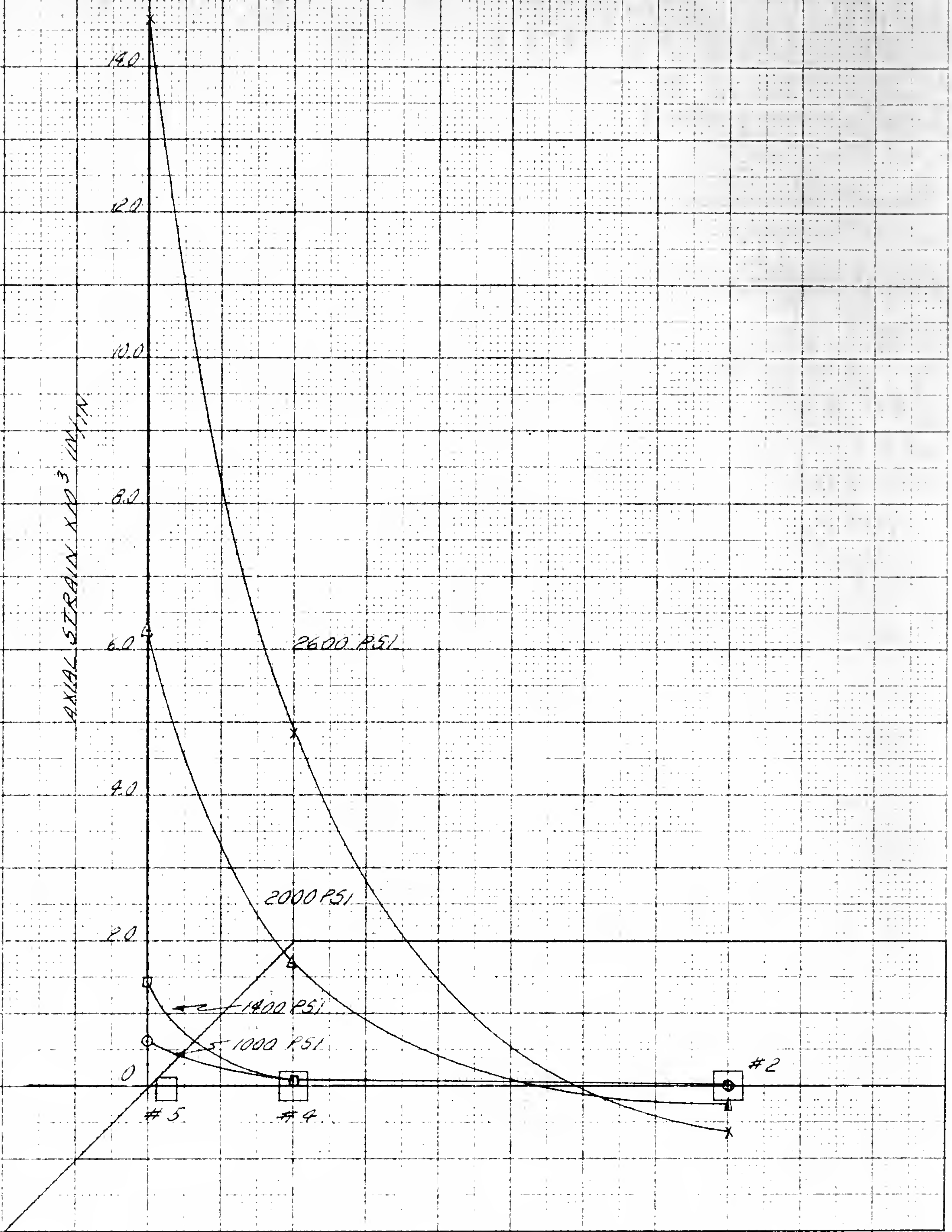


FIG. 4.3

AXIAL STRAIN V.S. AXIAL POSITION

TEST NO II

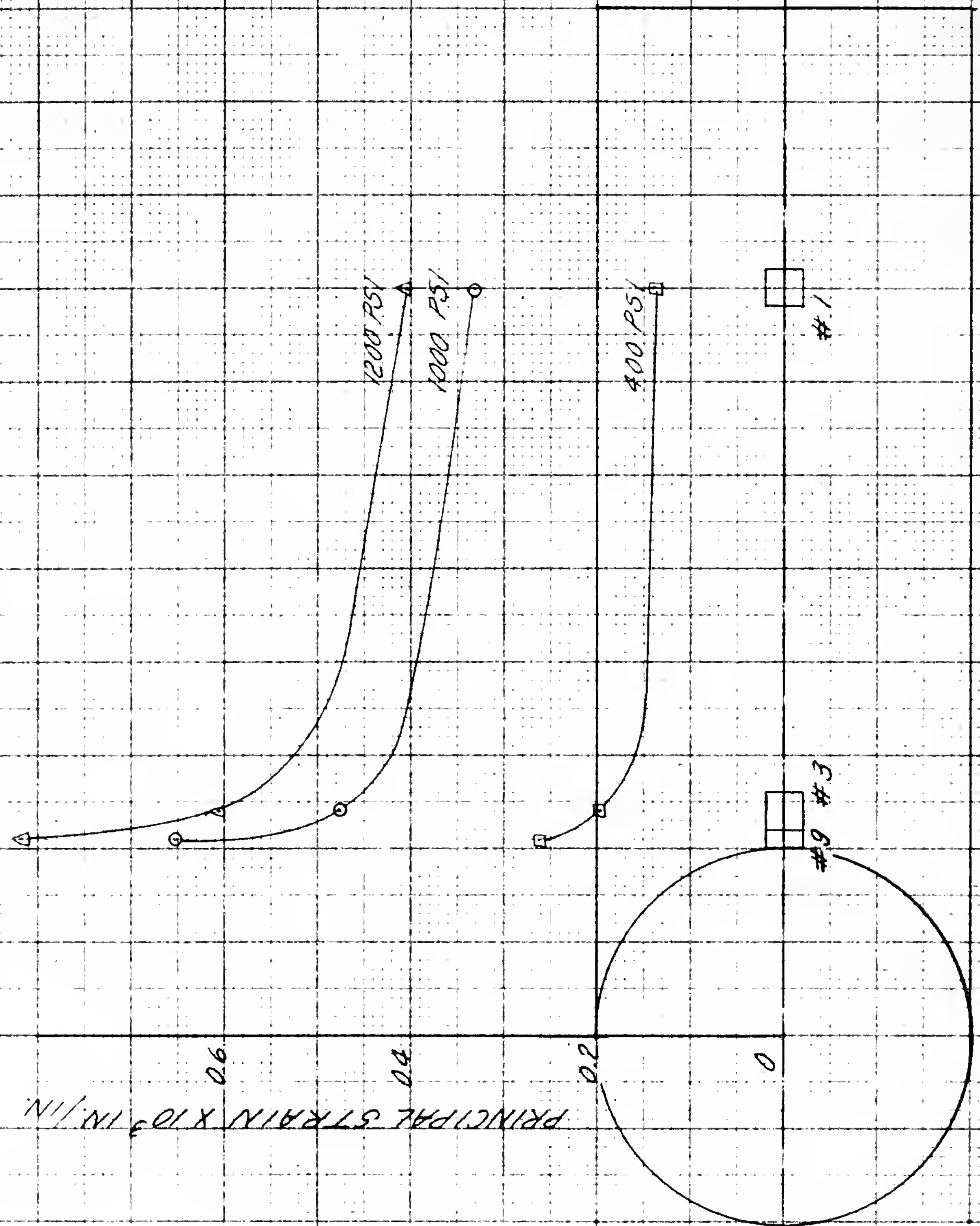


FIG 44
PRINCIPAL STRAIN VS AXIAL POSITION
TEST NO II

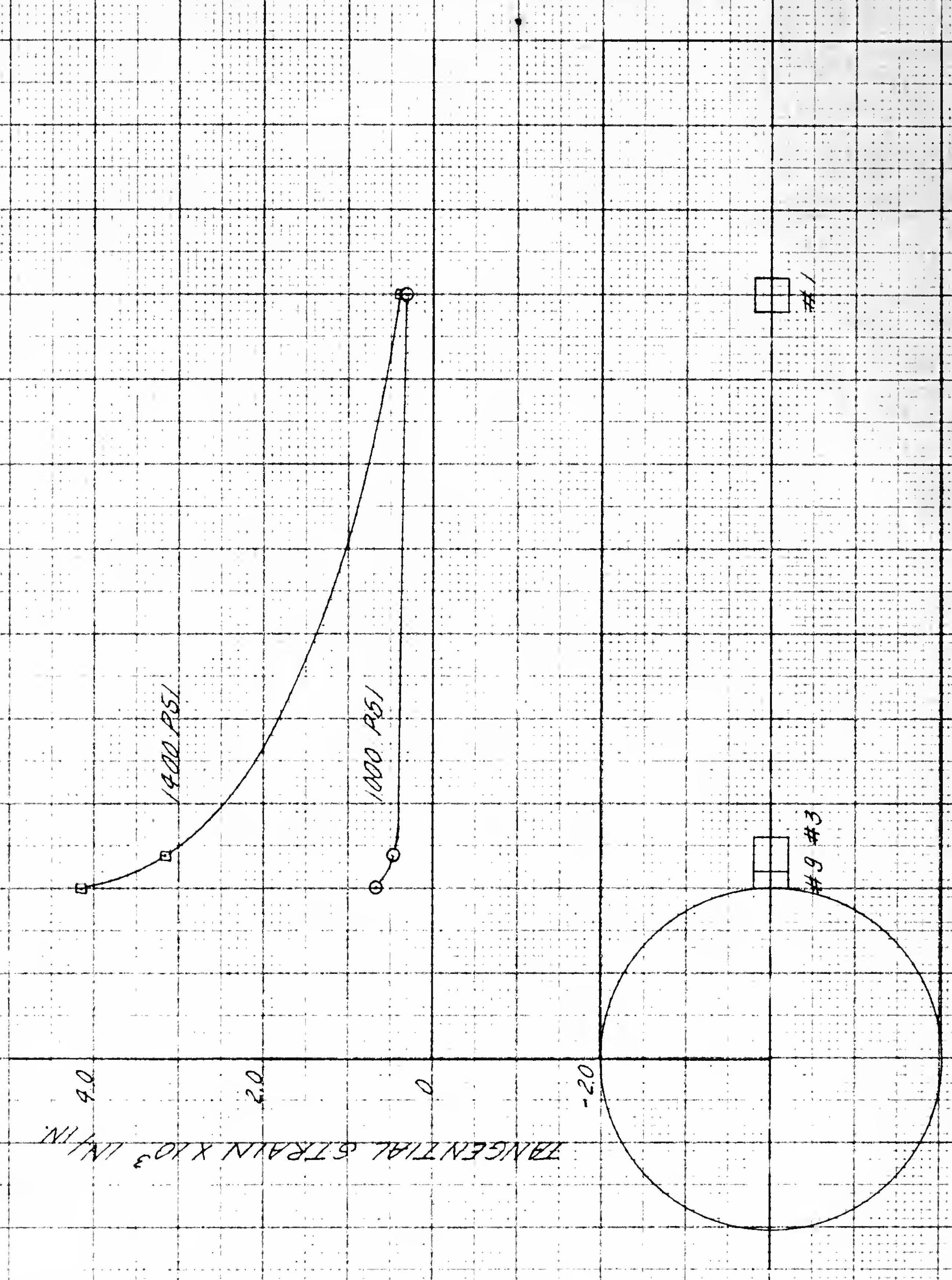


FIG 45
TANGENTIAL STRAIN VS AXIAL POSITION
TEST NO II

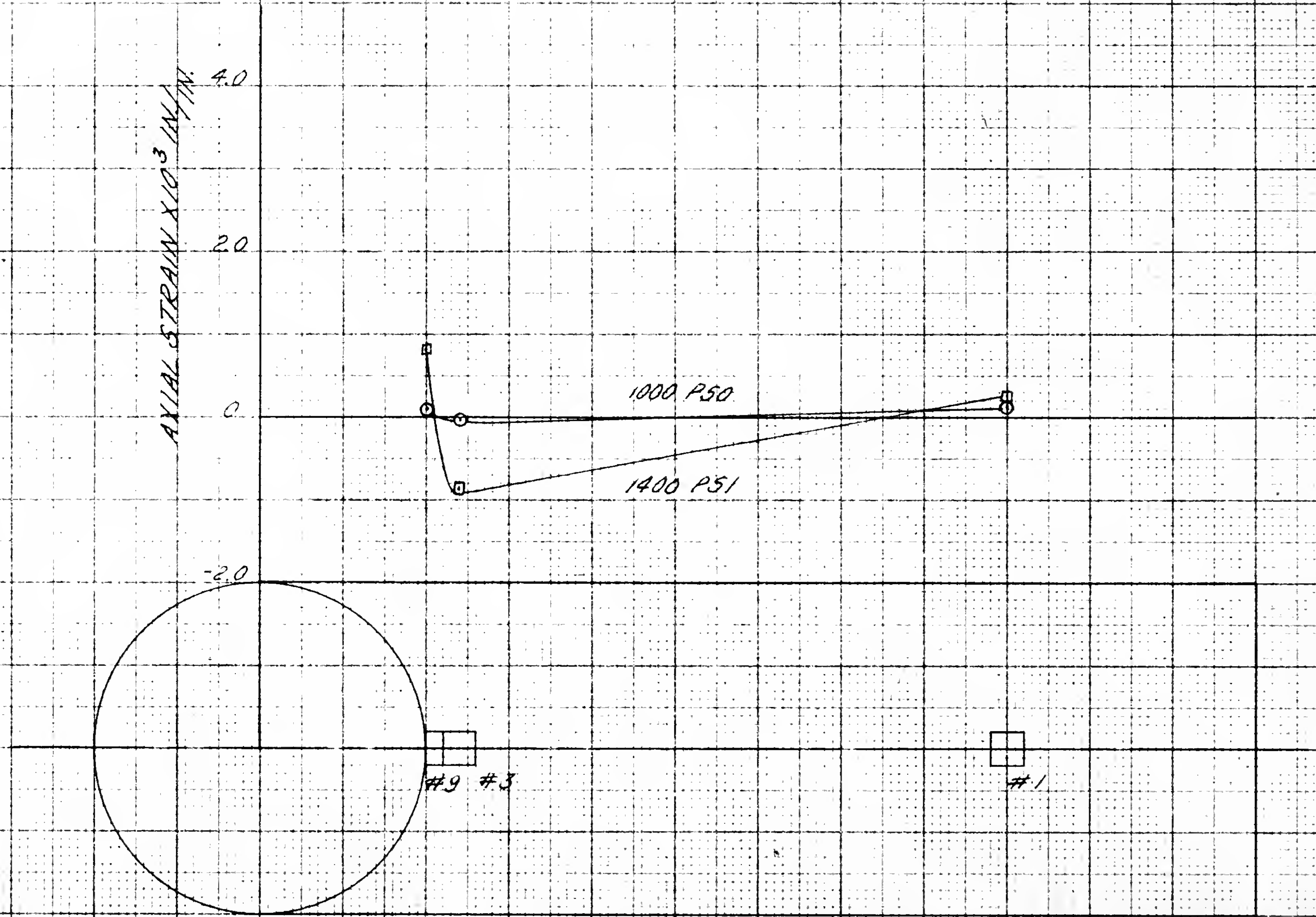


FIG. 46
AXIAL STRAIN VS AXIAL POSITION
TEST NO. II

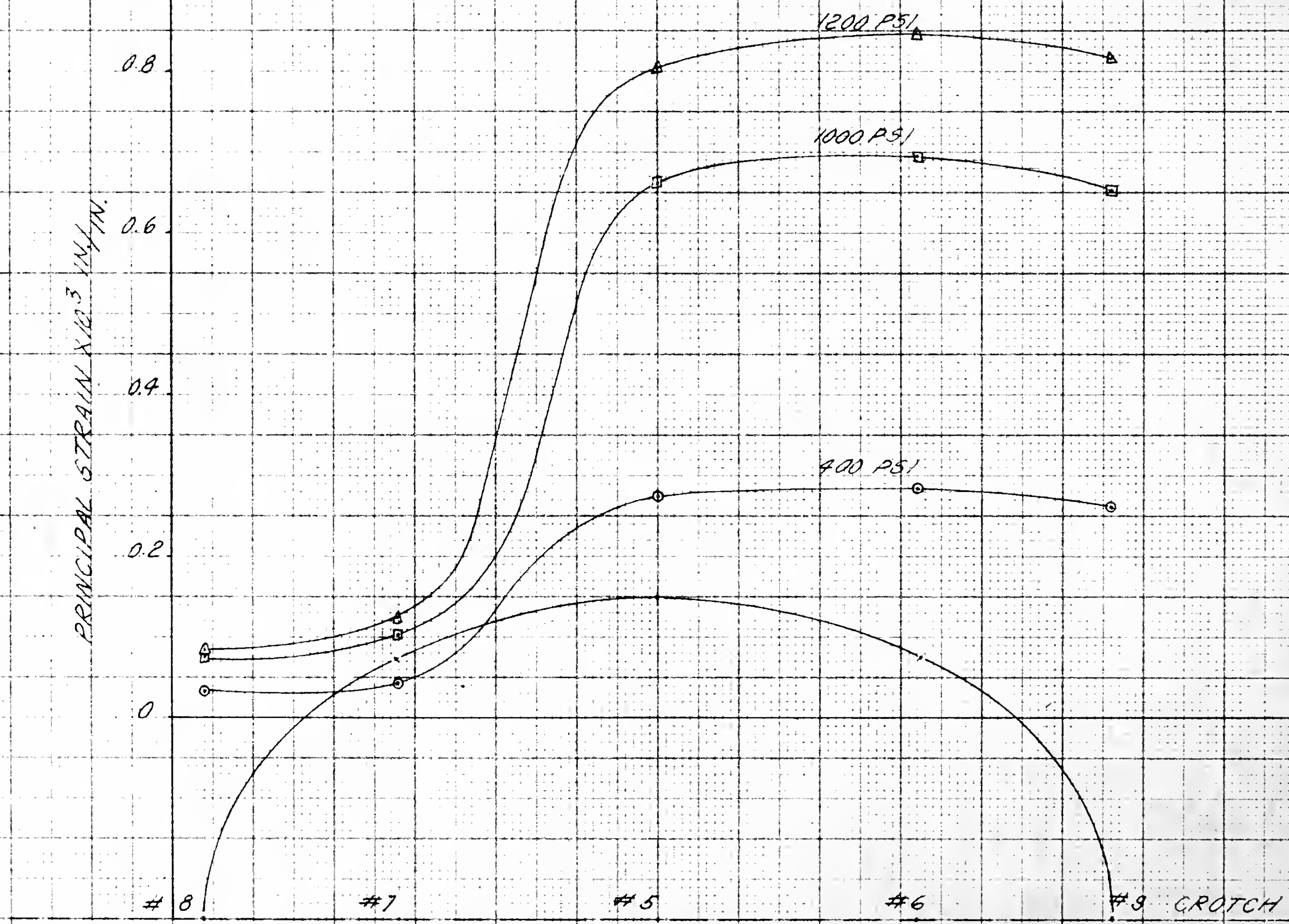


FIG. 47
PRINCIPAL STRAIN VS POSITION ON INTERSECTION
TEST NO. II

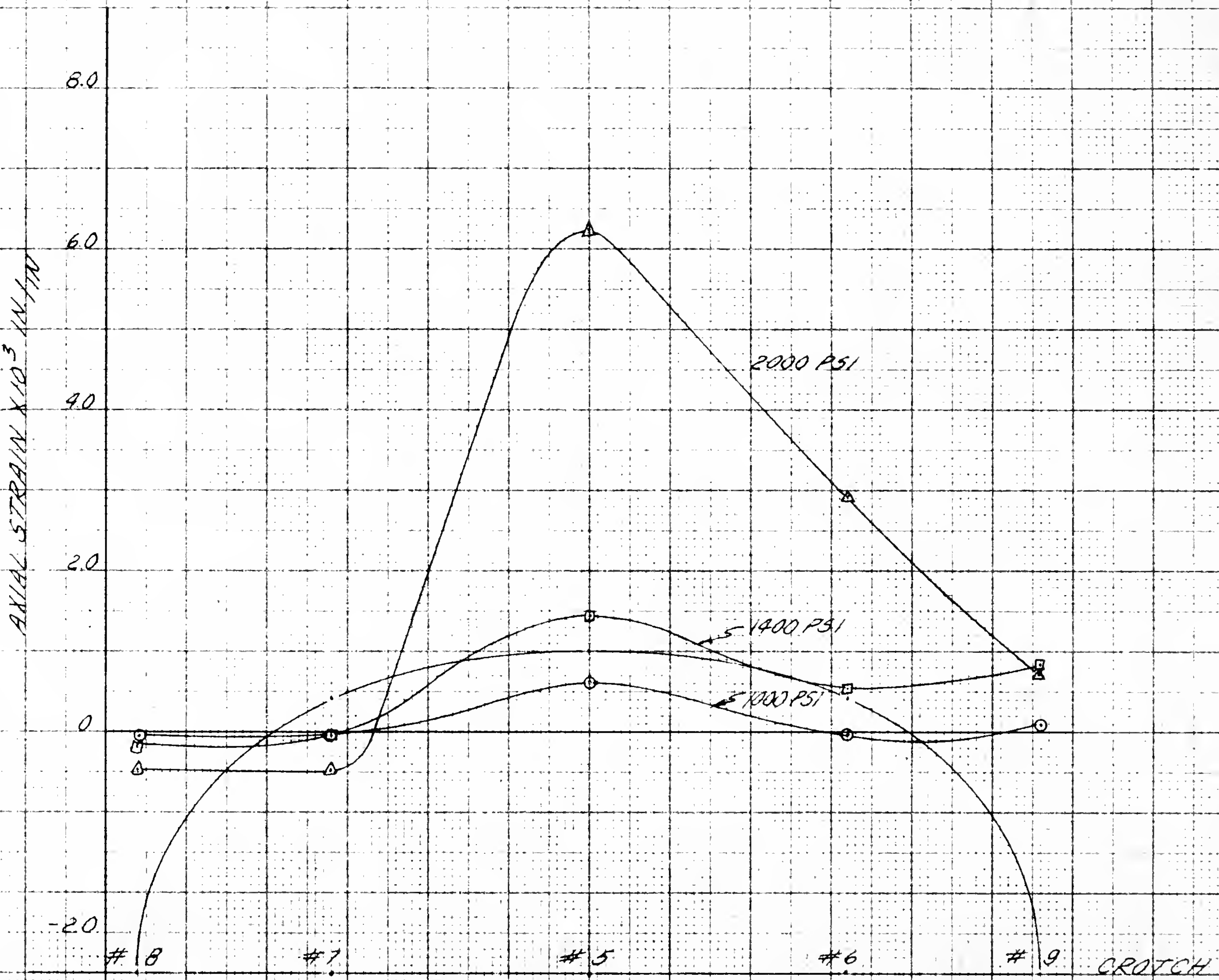


FIG. 48

AXIAL STRAIN VS POSITION ON INTERSECTION

TEST NO. II

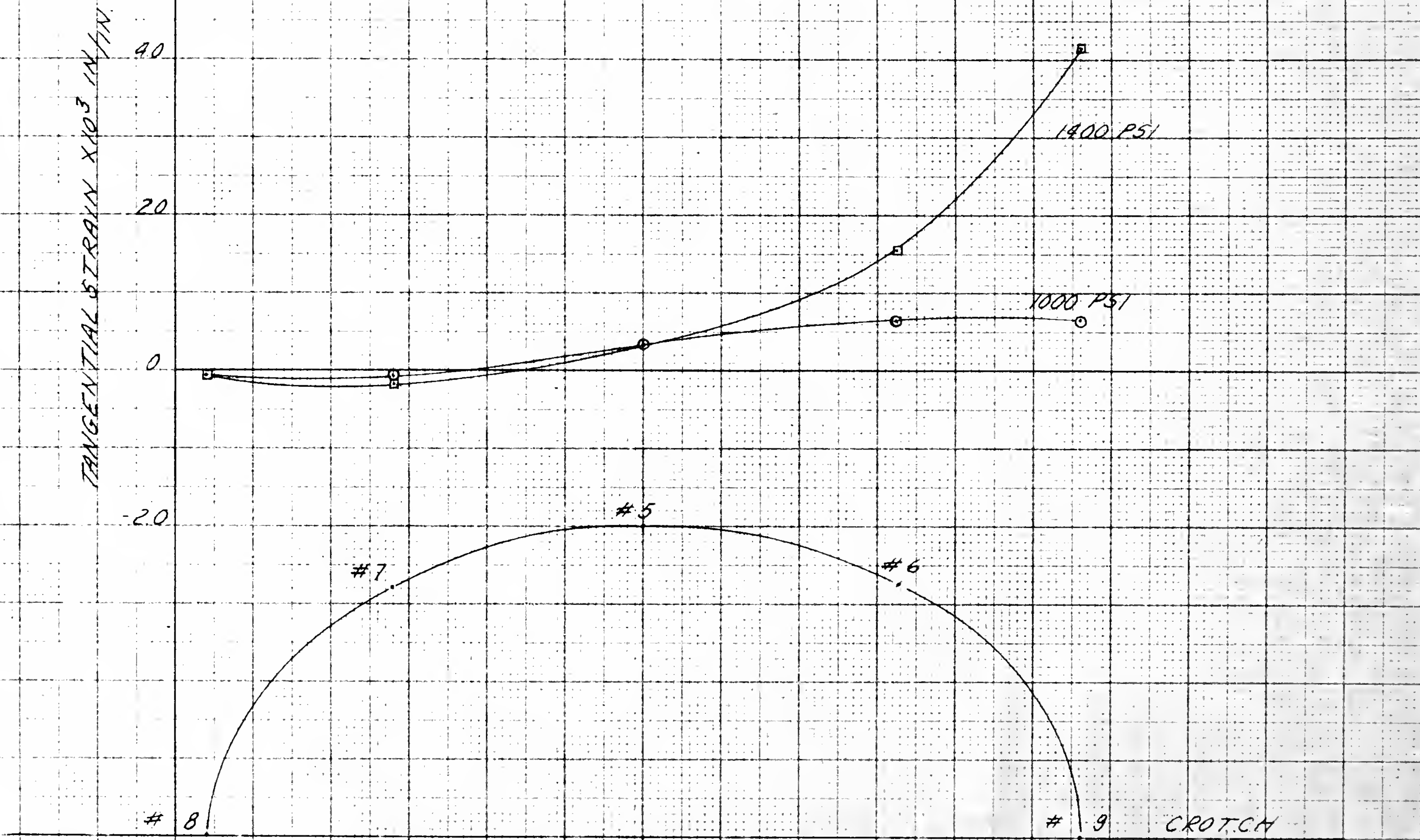


FIG. 49

TANGENTIAL STRAIN VS. POSITION ON INTERSECTION

TEST NO. II

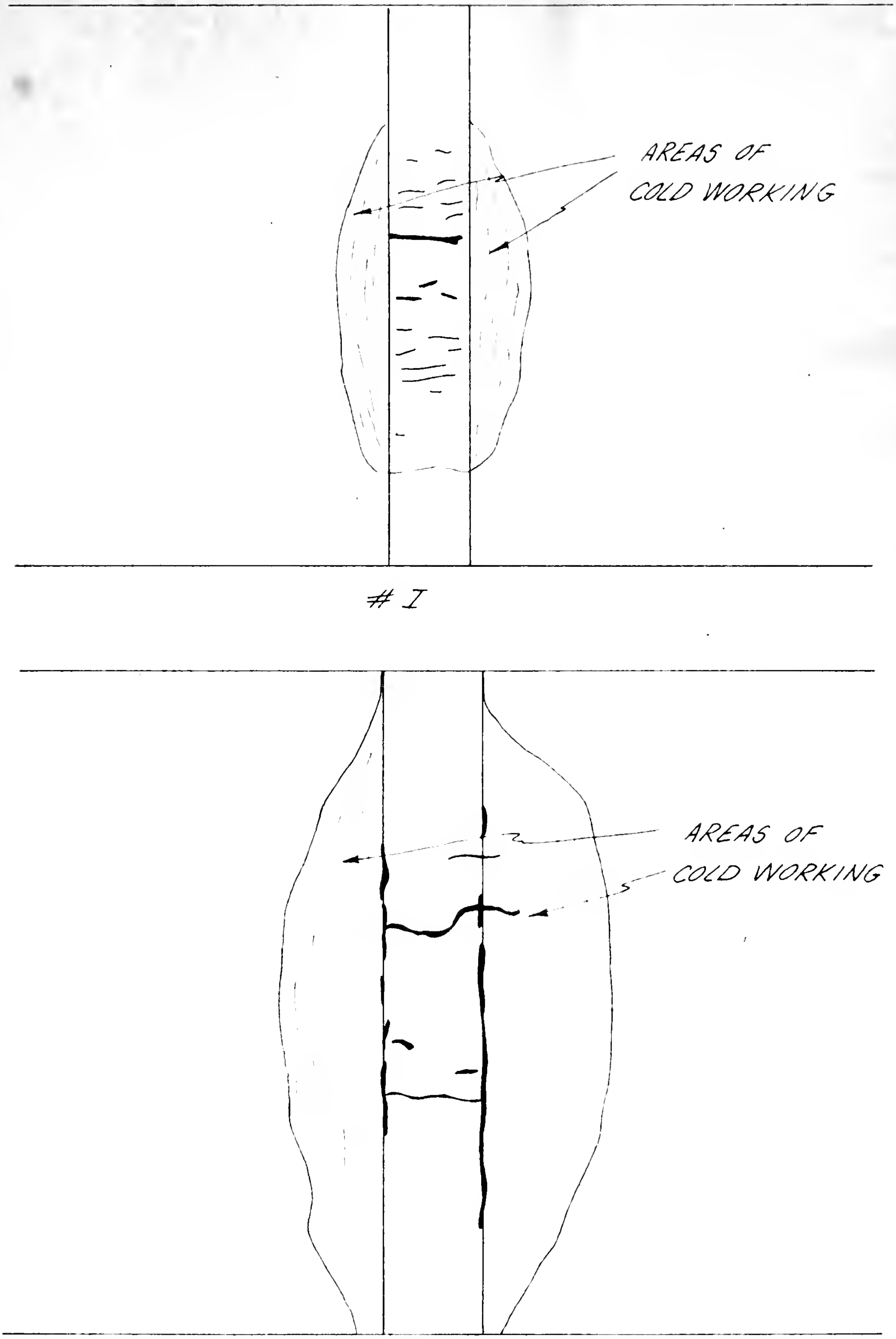


FIG. 50
SKETCHES OF BREAKS IN WELDS

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Stress distribution in two intersecting cylinders under pressure.