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# Empirical Mappings of the Frequency Response of an Electron Ratchet to the Characteristics of the Polymer Transport Layer

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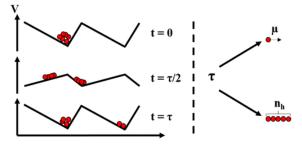
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Abstract



Flashing electron ratchets oscillate a periodic asymmetric potential to rectify nondirectional forces and thereby produce directional transport of electrons with zero source-drain bias. The relationship between the oscillation frequency of the potential and the ratchet (short-circuit) current reflects microscopic mechanisms of charge transport within the device. This paper describes experimental mappings of the "optimal frequency(ies)" of the ratchet  $f_{peak}$ —the oscillation frequencies that produce the largest ratchet current—to the carrier concentration,  $n_h$ , and to the linear field effect transistor mobility,  $\mu_h$ , for a poly(3-hexylthiophene-2,5-diyl) (P3HT) transport layer. Measurements on multiple devices, multiple P3HT films per device, and a range of annealing and photoexcitation conditions yield the empirical relationships  $f_{peak} \propto n_h$  and  $f_{peak} \propto \mu_h^{2/3}$ . Finite-element simulations suggest the sublinear relationship between mobility and peak frequency arises due to a combination of damped and inertial motion of the holes. This work also provides evidence that the frequency response of ratchets is sensitive to multiple length scales of asymmetry encoded within the periodic electrical potential. These multiple asymmetries cause changes in the polarity of the ratchet current at points within the frequency response, a long-mysterious characteristic of particle ratchets called "current inversion", by encouraging transport in opposite directions in different frequency regimes.

## Introduction

Particle ratchets are driven nonequilibrium systems that rectify nominally nondirectional (isotropic) forces to produce directional transport of particles, including electrons, by breaking both temporal symmetry and spatial inversion symmetry in the direction of transport. Molecular motors in biological systems—such as Na-K ATPase,(1) the myosin family,(2) and the kinesin family(3,4)—utilize a ratcheting mechanism; well-defined energetic landscapes defined by the structure and conformational states of the protein yield directional transport while hydrolyzing adenosine triphosphate (ATP). One class of synthetic ratchet, the flashing ratchet, utilizes a periodic array of asymmetric structural features, the "ratchet potential", which oscillates between two states of different symmetries to rectify the isotropic motion of a collection of particles (Figure 1).(5–8) The ratchet potential is typically electromagnetic and is used to drive the motion of various charged particles, including microspheres(9,10) and electrons.(11–13) Flashing electron ratchets produce current without application of a source-drain bias and can be used in applications such as rectifiers, digital logic, cryptography, and potentially (if the energy input is light) solar energy conversion. What is needed to move toward these

applications are experimental studies that map parameters of the electron ratchet to their electrical characteristics and performance and offer at least semiquantitative physical models for these mappings.

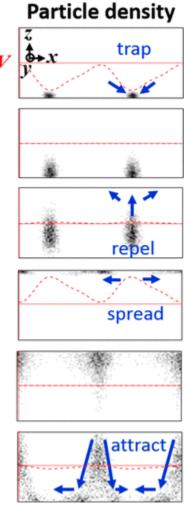


Figure 1. General mechanism of a 2D flashing particle ratchet: density plots displaying trajectories of likecharged nanoparticles in a medium of fixed dynamic viscosity ( $1 \times 10^{-4}$  Pa s) and dielectric constant (2.09) during application of a sinusoidal oscillating potential at the bottom boundary. Trajectories are calculated through finite element simulations. Darker areas indicate higher particle densities. The red dashed traces correspond to the potential applied, *V*. The *z*-axis indicates both the physical coordinate of the particles (spanning the thickness of the transport layer) and the electrostatic energy they experience, while the *x*-axis is the direction along which transport is recorded to determine particle current. The Supporting Information contains details of the simulation.

A major feature of any flashing particle ratchet, electron or otherwise, is a peaked dependence of the ratchet current or average particle velocity on the frequency of the oscillation of the ratchet potential. This peaked dependence is due to a change in the degree of coincidence between the time scale of oscillation and the inherent average time scale of motion of the traveling particles with changing oscillation frequency.(14–16) If the potential oscillation is too fast relative to particle motion, the particle experiences a time-averaged (spatially symmetric) potential, and there is no ratcheting. If the potential oscillation is too slow, the energy provided by the oscillation is dissipated as the particle relaxes to an equilibrium position at the bottom of a potential well, and there is no ratcheting. An examination of the frequency dependence of a flashing ratchet therefore offers insight into the time scale(s) of microscopic motion of the ratcheted particles, but so far there have been few

reports experimentally relating the peak frequency of an electron ratchet and electrical properties of the transport layer.(17,18)

A second major feature of a ratchet is the dependence of ratchet current on the density and interaction potential of ratchet particles. Theoretical studies of repulsively interacting particles (e.g., hard sphere(19–23) and Coulombic repulsion(24)) have revealed a strong dependence of the ratchet current on particle density, identifying regimes of cooperative transport and destructive particle jamming, but there have been no experimental studies of the relationship of the frequency response and the carrier density for a particular type of transport layer.

A third characteristic of ratchets is that the polarity of the ratchet current does, under some conditions, switch with a change in oscillation frequency of the potential. These so-called "current inversions" have been mysterious signatures of both experimental and theoretical ratchets for the lifetime of the field.

Here, we use extensive experimental characterization of a flashing electron ratchet with a poly(3-hexylthiophene-2,5-diyl) (P3HT) transport layer to propose mechanisms underlying all three of these ratchet characteristics. By varying the concentration and mobility of the majority carrier, holes, within P3HT through a combination of illumination and CS<sub>2</sub> vapor annealing, we show that the "optimal" frequency of the ratchet (the frequency at which the highest short-circuit current is achieved) scales linearly with the carrier concentration and as the 2/3 power of the linear field effect transistor mobility of the film. We also provide the first experimental evidence that the frequency response of the ratchet current depends on spatial asymmetries of multiple length scales within the ratchet potential, as opposed to only the spatial asymmetry of the fundamental repeating unit of the potential. The multiple asymmetries account for current inversions, since (i) asymmetries on different length scales in some cases encourage transport in opposite directions and (ii) asymmetries on longer length scales promote ratcheting at slower frequencies than asymmetries on shorter length scales.

## **Experimental Methods**

## **Device Architecture**

We fabricated ratchet devices with similar structures to those in our previous reports(14,15) (Figure 2A,B); the fabrication procedure and device characterization are described in detail in the Supporting Information. Within these devices, we used focused ion beam (FIB) assisted Pt deposition to form (unless otherwise noted) eight asymmetrically shaped finger electrodes (FEs) on Si/SiO<sub>2</sub> substrates and encapsulated them with a dielectric layer composed of plasma-enhanced chemical vapor-deposited (PECVD) SiO<sub>2</sub> and spin-on glass. On top of the dielectric layer, we deposited Ag source and drain electrodes using photolithography and spin-coated P3HT transport layers (~70 nm thick), which cover the 12  $\mu$ m channel between the source and drain electrodes. By applying a potential to the FEs (versus the source electrode), we generate an electric potential within the transport layer, *U*(*r*), which is determined by both the shape of the FEs (Figure 2C) and the dielectric response of the device. The time-dependent ratchet potential, *V*(*r*,*t*), experienced by the carriers within the transport channel is a product of *U*(*r*) and *F*(*t*), the time-dependent sinusoidal waveform that depends on the amplitude of the potential, *A*, and the flashing frequency, *f* (eq 1).

V(r,t) = U(r)F(t) (1a)

 $F(t) = A\sin(2\pi t f) \text{ (1b)}$ 

In this work, the amplitude of the potential, *A*, is 10 V. We measure the ratchet current (current at zero sourcedrain bias) at a range of flashing frequencies, *f*, for four devices denoted D1 through D4 with very similar FE shapes, as verified by atomic force microscopy (AFM) scans (Figure 2C and Figure S1).

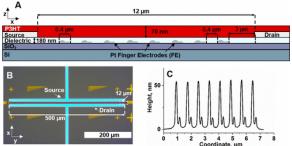


Figure 2. (A) Schematic diagram of a ratchet device where eight asymmetric Pt finger electrodes (FEs) encapsulated by a dielectric layer are used to generate an electric field within the transport layer (dimensions not to scale). (B) Optical microscopy image of the active area of one device, D1, prior to deposition of P3HT. The ratcheting transport channel is 12  $\mu$ m thick (between source and drain) and 50 nm high. (C) AFM line scan of the Pt FEs of device D1.

## Tuning the Electrical Properties of P3HT

We employed two methods for tuning the conductivity of our spin-coated P3HT films after the deposition: (i) illumination of the P3HT film with 532 nm light and (ii) annealing in CS<sub>2</sub> vapor. We measured the dc conductivity ( $\sigma$ ) of the P3HT films by recording source-drain current ( $I_{SD}$ ) as a function of source-drain bias ( $V_{SD}$ ). We estimated the FET mobility ( $\mu$ <sub>h</sub>) of the films from linear-regime field-effect transistor (FET) mobility sweeps, specifically by applying a dc potential to the FEs, which serve as a gate (see the Supporting Information for details). The carrier concentration,  $n_h$ , of our films is defined by eq 2

#### $\sigma = n_{ m h} e \mu_{ m h}$ (2)

where *e* is the fundamental charge of the electron. We assume that holes (rather than electrons) are responsible for the electrical response of the P3HT films as P3HT is known to be a p-type semiconductor,(25) and the mobility of electrons within our devices is more than a factor of 10 lower than that of the holes (see the Supporting Information). Illumination of the P3HT film and CS<sub>2</sub> vapor annealing each modifies both the mobility and carrier concentrations of P3HT (Figures S3 and S4); thus, to assess the *separate* contributions of carrier concentration and hole mobility to the ratchet response, we need data sets where one of these parameters is held constant while the other one varies. We produce such data sets by varying the intensity of illumination and duration of CS<sub>2</sub> annealing for a set of P3HT films on each of four devices and then compare the electrical characteristics of ratchets with either constant  $n_h$  (within ±25%) or constant  $\mu_h$  (within ±25%). This strategy is possible because we can dissolve the spin-coated P3HT films in CHCl<sub>3</sub> and redeposit on the same device (see the Supporting Information). Through a combination of absorbance, photoluminescence, and Raman spectroscopy measurements, we determined that CS<sub>2</sub> vapor annealing decreases the mobility of the P3HT films by disordering the packing structure of the spin-coated films (Figure S5). We assume, in our analysis, that the hole mobility of P3HT is spatially isotropic (see the Supporting Information for details).

## **Results and Discussion**

Effect of Carrier Mobility and Concentration on the Frequency Response of the Ratchet The y-axis of Figure 3A is the net charge transported per oscillation of the ratchet,  $q_{osc}$ ; this quantity scales the ratchet current by the frequency (f) of the applied sinusoidal potential and is therefore a measure of ratchet efficiency. A plot of  $q_{osc}$  vs f is the frequency response of the ratchet. Figure 3A shows the frequency responses for a series of transport layers on a single device D1 (analogous plots for other devices are in the Supporting Information). For all of these films, the carrier concentration is  $2.6 \times 10^{-3}$  C cm<sup>-3</sup> (±25%), and the hole mobility ranges from  $7.7 \times 10^{-5}$  to  $1.7 \times 10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>. There is no discernible trend in the magnitude of  $q_{osc}$  with  $\mu_h$  as a function of frequency.

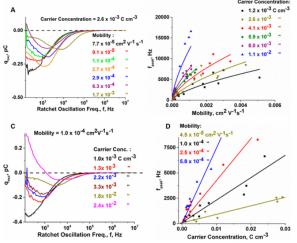


Figure 3. (A) Plots of source-drain charge as a function of ratcheting frequency for device D1 driven by 10 V sine waves with a fixed carrier concentration of  $2.6 \times 10^{-3} \pm 6.5 \times 10^{-4}$  C cm<sup>-3</sup>, with differing mobilities. (B) Plot of peak ratcheting frequency vs linear FET mobility for devices D1–D4 with varying carrier concentrations. Solid traces are power law fits described in the main text. (C) Plots of source-drain charge as a function of ratcheting frequency for device D1 driven by 10 V sine waves, with a fixed linear FET mobility of  $1.0 \times 10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> with differing carrier concentrations. The trend of decreased overall ratchet current with increasing carrier concentration. (D) Plot of peak ratcheting frequency vs carrier concentration for devices D1–D4 with mobilities of  $4.5 \times 10^{-5}$  (yellow),  $1 \times 10^{-4}$  (black),  $2.5 \times 10^{-4}$  (red), and  $5.8 \times 10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> (blue). Data for a mobility of  $5.8 \times 10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> are only plotted if the frequency response had a single discernible peak, as opposed to two peaks.

The most notable feature of these results is a maximum magnitude of  $q_f$  at a frequency that varies with mobility. We denote the oscillation frequency at which the absolute value of  $q_{osc}$  is maximized as  $f_{peak}$ . As the carrier mobility increases,  $f_{peak}$  shifts to higher values, as shown for a single carrier concentration in Figure 3A and summarized at a series of carrier concentrations ( $n_h$ ) in Figure 3B for four devices, D1–D4. In our case, the sign of  $q_{osc}$  is negative; however, we previously demonstrated that the direction of ratcheting is dependent upon the FE shape.(26) The relationship between  $f_{peak}$  and  $\mu_h$  is sublinear in this range of  $n_h$ . When we scale the traces in Figure 3B by  $n_h$  and plot versus  $\mu_h$ , the traces all overlay (Figure S8); this result indicates that  $f_{peak}$  is linearly proportional to  $n_h$ . Furthermore, plots of  $f_{peak}/n_h$  versus  $\mu_h$  are nonlinear. These two observations are summarized in eq 3

$$f_{\mathrm{peak}} pprox \mathcal{C}n_{\mathrm{h}}f(\mu_{\mathrm{h}})$$
 (3)

where  $f(\mu_h)$  is a sublinear function of mobility. Through a global fit of the data in Figure 3B to a power law function of the form  $f_{\text{peak}} = C_i n_{\text{h},i} \mu_h^x$ , where x is shared among all traces,  $n_{\text{h},i}$  is the fixed carrier concentration for trace *i*, and  $C_i$  is a free parameter for trace *i*, we empirically determine x to be 0.66 ± 0.06 (eq 4).

$$f_{\rm peak} pprox {{{\cal C}n_{\rm h}}{\mu_{\rm h}}^{2/3}}$$
 (4)

The proportionality constant *C* translates the mobility and carrier concentration into an average time scale of motion of the carriers and is primarily dictated by the drift velocity of the carriers during the ratcheting mechanism. The drift velocity, in turn, depends on the electric field experienced by the carriers; *C* is therefore different for different FE shapes and dielectric layers (Figure S6).

If we instead measure a series of P3HT ratchets with the same value of  $\mu_h$  (±25%), but a range of values of  $n_h$  (Figure 3C), we examine the frequency response of the ratchet as a function of carrier concentration and independently verify eq 4. At lower mobilities (here,  $\leq 2.5 \times 10^{-4} \text{ m}^2 \text{ V}^{-1} \text{ s}^{-1}$ ),  $f_{\text{peak}}$  indeed shifts linearly to higher values with increasing carrier concentration as defined by eq 4 (Figure 3D). Furthermore, with this independent data set, we observe a 2/3 power dependence of  $f_{\text{peak}}$  on carrier mobility, also consistent with eq 4 (Figure S8).

To understand the empirical relationship between  $f_{\text{peak}}$  and  $\mu_{\text{h}}$  in eq 4,  $(f_{\text{peak}} \propto {\mu_{\text{h}}}^{2/3})$  we refer to a previously published 1D analytical model for Brownian (overdamped) particles subject to an oscillating spatially asymmetric potential; (27) we have found this model useful in describing certain behaviors of our experimental flashing ratchets.(15) The 1D model predicts a linear relationship between the  $f_{\text{peak}}$  and  $\mu_h$  (Figure S10). If we expand the 1D model to 2D by allowing diffusion of particles in the spatially homogeneous y-dimension, we also observe a linear relationship between  $f_{\text{peak}}$  and  $\mu_h$  (see the Supporting Information). We therefore hypothesized that the observed sublinear dependence of  $f_{\text{peak}}$  on  $\mu_h$  arises from either (i) motion of carriers in the z-dimension (thickness) of our transport layer in response to oscillation of the potential between positive and negative or (ii) inertial effects as the carriers are not in a strictly overdamped transport regime. To distinguish between these mechanisms, we examine 2-dimensional (x, z) simulations of charged particles in solution experiencing an oscillating spatially asymmetric potential, where we vary the diffusivity/mobility of the particles by adjusting the dynamic viscosity of the solvent. For low simulated mobilities ( $\sim 7 \times 10^{-5}$  to 7  $\times 10^{-4}$  cm<sup>2</sup> V s<sup>-1</sup>), we observe a linear relationship between the peak ratcheting frequency and mobility (Figure S11A,B), indicating that our experimentally observed sublinear relationship does not arise from the motion of the carriers in the z-direction. At higher mobilities ( $\sim 7 \times 10^{-4}$  to  $1.2 \times 10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>), we observe a broad frequency response, where the peak frequency does not depend upon the mobility (Figure S11C). In this mobility regime, the particles no longer experience overdamped transport and—due to inertial effects—are less spatially confined by the ratcheting potential (Figure S12). Assuming the ratcheting current, I, scales as  $f^{-1}$  in the high-frequency limit(27) and f in the low-frequency limit, (28) we can use a simple ansatz to characterize the frequency dependence of the ratcheting current (eq 5)

$$I(f,\tau) \approx \frac{f\tau^{-1}}{f^2 + f\tau^{-1} + \tau^{-2}} \varphi$$
 (5)

where  $\tau$  corresponds to the time scale of transport of a particle across one spatial period, *L*, of the ratcheting potential and  $\phi$  is a proportionality constant with units of current. Qualitatively, eq 5 expresses the current in terms of  $\phi$  times the ratio of productive ratchet driven motion (the  $f\tau^{-1}$  term) to total motion, with the  $f^2$ term corresponding to unproductive motion in which the frequency term applies twice (first pushing one direction and then the reverse), and the  $\tau^{-2}$  term refers to motion not driven by the ratchet that could include both ballistic and diffusive components. At steady state the current *I* is proportional to the charge *q*, so to arrive at an expression for  $f_{peak}$ , the extrema of  $q_{osc}$ , we divide eq 5 by *f* and set the derivative (eq 6)

$$\frac{\partial}{\partial f} q_{\rm osc}(f,\tau) \approx \frac{\tau^{-2} + 2f\tau^{-1}}{\left(f^2 + \frac{f}{\tau} + \tau^{-2}\right)^2} \varphi \ (6)$$

equal to zero, yielding  $f_{peak} \approx \frac{\tau^{-1}}{2}$ . In the case of inertial/ballistic transport,  $\tau \propto \frac{L}{\sqrt{U}}$ , where *U* is the ratcheting potential experienced by the particle, whereas  $\tau \propto \frac{L^2}{D}$  in the overdamped limit, where *D* is the

diffusivity/mobility of the particle. Therefore, we would expect no dependence of  $f_{peak}$  upon the particle mobility and a linear dependence of  $f_{peak}$  upon the particle mobility in the case of underdamped/inertial and overdamped transport, respectively. The sublinear behavior in our experimental ratchets could be attributed to hole transport within the P3HT having mixed overdamped and inertial transport character.

Previous simulations of charged particle ratchets have shown that at low carrier concentrations carrier–carrier repulsion effects lead to a stronger potential experienced by the particles, increasing the peak frequency; at high carrier concentrations, the carrier–carrier repulsion begins to damp particle transport—so-called "jamming"– giving an overall peaked dependence of  $f_{peak}$  on  $n_h$ .(21,22) Our observed approximately linear relationship between  $f_{peak}$  and  $n_h$  at mobilities less than  $1.1 \times 10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> (eq 4) is reasonable if we are not achieving sufficient carrier densities to result in the jamming effects seen in simulations. Our hole densities are limited primarily by recombination of holes with less mobile electrons. The existence of electron—hole recombination in these films is supported by both (i) a sublinear relationship between carrier concentration and illumination intensity and (ii) a decrease in measured hole mobility upon illumination (see Figure S3B). Future experimental work can validate this hypothesis by comparing the effects of carriers introduced by chemical or electrochemical doping versus photogenerated carriers.

At higher mobilities (> $8.2 \times 10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>), the frequency response of the ratchet is more complex: we still observe a shift of the response to higher frequencies with increasing  $n_h$ , but the response also broadens and eventually splits into multiple discernible peaks (Figure 4A,B). We suspect these effects are due to the fact that when measuring the FET mobility, we preferentially measure holes with the highest mobility (a known problem in characterizing organic semiconductors(29)), but populations of holes with lower mobilities exist in the film. As we increase  $n_h$ , the holes sample a broad distribution of morphologies (amorphous and crystalline regions) within the heterogeneous P3HT film, and therefore have a set of distributions of time scales of motion. Each distribution gives rise to a peak in the frequency response of the ratchet.

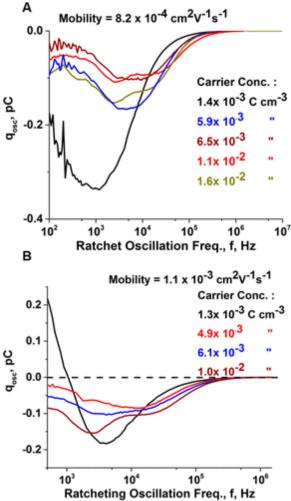


Figure 4. (A) Plots of source-drain charge as a function of ratcheting frequency for device D1 driven by 10 V sine waves, with a fixed linear FET mobility of  $8.2 \times 10^{-4}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> with differing carrier concentrations. (B) Plots of source-drain charge as a function of ratcheting frequency for device D1 driven by 10 V sine waves, with a fixed linear FET mobility of  $1.1 \times 10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> with differing carrier concentrations. All mobility values are within 25% of the specified value.

#### Sensitivity of Ratchets to Multiple Length Scales of Spatial Asymmetry: One Origin of

#### **Current Inversions**

In addition to the shape and peak position of the frequency response, the other major electrical characteristic of a flashing electron ratchet is the current inversion, where the directionality of particle transport is inverted(30,31) on going from one frequency region to another. Clear examples of such inversions are in Figure 3C (pink trace) and Figure 4B (black trace). We view the observed ratchet current as the small net current produced from the competition between the current in the source-to-drain direction and the current in the drain-to-source direction. While the asymmetry in the shape of each FE is the intentional, engineered source of asymmetry in the system, this asymmetry is very small once the field propagates into the transport layer (see Figure S15). Other asymmetries in the potential surface therefore may also contribute to ratchet current, and these asymmetries may drive the current in the opposite direction of that dictated by the shape of individual FEs. One such "incidental" asymmetry is caused by an underlying curvature of the ratchet potential surface in the *x*-direction (Figure 5A). Finite-element simulations of the electric potential generated by the FEs at the P3HT/SiO<sub>2</sub> interface predict this curvature and show that it is caused by the difference in the electrical

potential around FEs in the center of the array from FEs near the ends of the array. This curvature creates an additional unit of asymmetry associated with two or more adjacent FEs (termed a multi-FE mode). Since this unit of asymmetry has a longer period than the individual FE mode, holes moving in response to this asymmetry are resonant with a slower oscillation frequency than holes moving in response to the asymmetry of a single FE. If the multi-FE mode and the single-FE ratchet in opposite directions, the result is a current inversion.

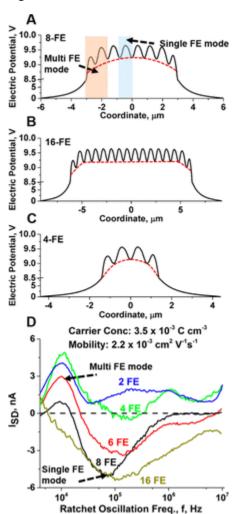


Figure 5

Figure 5. Plots of simulated electric fields versus *x* coordinate at the P3HT/SiO<sub>2</sub> interface for 8-FE (A), 16-FE (B), and 4-FE (C) devices. Red dashed lines highlight the longer length scale curvature of the potential surface. (D) Plots of source-drain current at zero applied source-drain bias as a function of ratcheting frequency for devices with 16 (yellow), 8 (black), 6 (red), 4 (green), and 2 (blue) FEs and driven by 10 V sine waves with fixed carrier concentration ( $3.5 \times 10^{-3}$  C cm<sup>-3</sup>) and mobility ( $2.2 \times 10^{-3}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>).

To confirm this hypothesis, we fabricated devices with 2, 4, 6, 8, or 16 FEs, where the devices all have very similar FE shapes, 400 nm separation between FEs, and 3  $\mu$ m separating the source (drain) electrode from the first (last) FE (see the Supporting Information for details). Increasing the number of FEs decreases the curvature of the underlying potential (e.g., compare Figures 5A–5C) and should decrease the contribution of the multi-FE mode to the overall frequency response of the ratchet.

Figure 5D shows the frequency responses of this set of devices, all of which we engineered to have a common  $n_h$  and  $\mu_h$  (±25%); here, we plot source-drain current,  $I_{sd}$ , rather than charge as we are primarily

interested in the different regimes of transport (rather than their efficiencies). All of the responses exhibit an artifactual peak at ~3 kHz that we attribute to capacitance of the FEs and source/drain electrodes; we subtracted this feature from the data sets (see the Supporting Information for details). When we decrease the number of FEs from 16 to 8 to 6 to 4, the magnitude of the negative higher frequency peak (~10<sup>5</sup> Hz) (which we tentatively attribute to the single-FE mode) decreases and appears to shift to higher frequencies, and the magnitude of the positive lower frequency peak (~10<sup>4</sup> Hz) (which we tentatively attribute to a multi-FE mode) increases. The frequency at which the current inversion occurs also increases with a decreasing number of FEs. One can interpret these trends as a competition between ratcheting in the negative current direction due to asymmetry of the single FEs and ratcheting in the positive current direction due to asymmetries on a longer length scale. As the curvature of the ratchet potential increases (on going from 16 to 4 FEs), the contribution of the lower frequency response increasingly dominates the contribution of the higher frequency response. In the "2 FE" device, the single FE mode completely disappears, and we observe two broad positive peaks.

We observe these trends across different mobilities and different carrier concentrations (see Figure S16).

## Conclusions

In summary, we examined the relationship between the ratcheting frequency and three microscopic properties in flashing electron ratchets with a P3HT transport layer: (i) carrier mobility, (ii) carrier concentration, and (iii) spatial asymmetry across multiple length scales. By varying the concentration and mobility of the holes within the film through a combination of illumination and CS<sub>2</sub> annealing, we observe that the peak ratcheting frequency, the frequency of oscillation that provides the biggest ratchet current, scales linearly with the carrier concentration and as the 2/3 power of the linear FET mobility. We provide evidence that increasing carrier concentration via photoexcitation increases the peak ratcheting frequency through repulsive carrier–carrier interactions. We also provide evidence that the sublinear relationship between the mobility and peak frequency arises from inertial effects, where carrier transport is no longer in an overdamped regime. Finally, we demonstrate that spatial asymmetries across multiple length scales (multi-FE modes) contribute to the ratcheting response and, in some cases, induce a current reversal in this response.

In our experimental system, we introduce free carriers through illumination—where the photogenerated holes are more mobile and primarily responsible for the ratcheting response. By using a transport layer with more ambipolar transport behavior (such as amorphous Si(32) or WSe<sub>2</sub>(33)), we would potentially increase the peak ratcheting efficiency by (i) finding an oscillation frequency that resonates with both electron and hole motion and (ii) decreasing electron—hole recombination events by spatially separating the two carriers. Additionally, by electrically doping the ratchet device through a top contact, we could avoid electron—hole recombination entirely and possibly introduce enough carriers to induce theoretically predicted jamming effects. While, in our system, the carrier mobility is isotropic (in-plane vs out-of-plane are not differentiable), portions of the racheting process consist of primarily horizontal or vertical transport (Figure 1). We could gain insight into the time scales of these substeps in the ratcheting process through the use of anisotropic transport layers, such as transition metal dichalcogenides (TMDCs)(34) or highly ordered semiconductor polymers.(35)

While the multi-FE modes arise in our system due to our devices' poorly approximating an infinite periodic array of FEs, one could imagine intentionally encoding multiple length scales of asymmetry within a ratchet device. In our devices, we observed a current inversion arising from the multi-FE mode; however, we could potentially encode ratchets with tunable frequency responses across a wide frequency range. When constructively interfering with the single-FE mode, the multi-FE modes generate a broadband frequency response. When destructively interfering with the single-FE mode, they give rise to a narrowed frequency response. By properly mapping the functional dependence of the frequency response versus the carrier mobility, carrier concentration, and spatial asymmetry within the field (including multiple length scales of asymmetry), we can

potentially fabricate ratchet information devices with tunable ratcheting efficiencies for a wide frequency range ( $\sim$ 100 Hz to 10 MHz) using our current device structure.

## Supporting Information

The Supporting Information is available free of charge on the <u>ACS Publications website</u> at DOI: <u>10.1021/acs.jpcc.9b06503</u>.

Device fabrication and characterization, methodology for electrical measurements, optical characterization of P3HT (absorption, photoluminescence, and Raman spectra), analytical simulations, and finite-element simulations (PDF)

The authors declare no competing financial interest.

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## Acknowledgments

This work was supported as part of the Center for Bio-Inspired Energy Science (CBES), an Energy Frontier Research Center funded by the U.S. Department of Energy (DOE), Office of Science, Basic Energy Sciences (BES), under Award # DE-SC0000989. This work made use of the Keck-II and EPIC facilities of the NU*ANCE* Center at Northwestern University, which has received support from the Soft and Hybrid Nanotechnology Experimental (SHyNE) Resource (NSF ECCS-1542205); the MRSEC program (NSF DMR-1720139); the International Institute for Nanotechnology (IIN); the Keck Foundation; and the State of Illinois, through the IIN. This work utilized Northwestern University Micro/Nano Fabrication Facility (NUFAB), which is partially supported by SHyNE, the Materials Research Science and Engineering Center, the State of Illinois, and Northwestern University. The authors thank Daniel Kwasnieski for useful discussions.

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