# Orientation relationships and interfaces in directionally solidified eutectics for

# solid oxide fuel cell anodes

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## Abstract

Orientation relationships (OR), interface planes and growth directions of the directionally solidified eutectics NiO-YSZ, CoO-YSZ, NiO-CeO<sub>2</sub>, NiO-GDC, CoO-CeO<sub>2</sub> and CoO-GDC have been determined by means of Electron Backscatter Diffraction (EBSD). The eutectics were prepared by the Laser Floating Zone technique at different growth rates (10-200 mm/h) to explore dissimilar lamellar spacing. The majority OR characterized single is by a plane and two  $(111)_{NiO/CoO} //(001)_{YSZ/GDC/CeO2}$  interface different growth directions: [011]<sub>NiO/CoO</sub>//[010]<sub>YSZ/GDC/CeO2</sub> and [110]<sub>NiO/CoO</sub>~//[110]<sub>YSZ/GDC/CeO2</sub>, the OR being the same for both cases. In addition, a cube-on-cube OR, where the crystallographic axes of the component phases are parallel, has also been observed. These experimental results are discussed in terms of the ionic charge balance and the lattice misfit at the interface. The coincidence of reciprocal lattice points model (CRLP) has also been applied to the NiO-YSZ case. The most favourable ORs predicted by the CRLP model are consistent with the experimental findings.

# Keywords: EBSD, CRLP, SOFC, DSE, Orientation imaging microscopy

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Instituto de Ciencia de Materiales de Aragón, CSIC-Universidad de Zaragoza. C/ María de Luna 3, E-50.018 Zaragoza, Spain Tel.: +34 876 555125 Fax: +34 976761957 e-mail:alarrea@unizar.es In recent decades, solid oxide fuel cells (SOFCs) have been deemed a clean alternative to convert chemical energy into electricity with high efficiency.<sup>1,2</sup> One of their most notable features is their ability to use a wide variety of fuels, which positioned them to be used in the current distribution network of natural gas and liquid fuels. The state-of-the-art SOFC materials are: a mixed conducting oxide as cathode, a YSZ (yttria-stabilized-zirconia) electrolyte and a porous cermet of Ni and YSZ as anode.<sup>3</sup> The anode has to provide electronic and ionic conductivity as well as permeation of the fuel gas. The electrochemical reactions take place at the Triple Phase Boundary (TPB) where metal, ionic conductor and pores meet, and thus, the TPB length should be as high as possible. These anodes have traditionally been fabricated by sintering a mixture of NiO and YSZ powders that subsequently undergoes reduction forming a porous ceramic-metal composite. There are still some unresolved issues regarding the anode performance, such as the low stability against redox cycling<sup>4</sup> and the coalescence of the metal particles during cell operation as a result of the low wettability with the ceramic phase.<sup>5</sup> This coarsening results in the degradation of the anode performance due to the loss of electronic conductivity, the obstruction of the pores and a less efficient catalysis.

Some other materials, such as cermets of Ni and gadolinium-doped ceria (GDC), have been proposed for SOFC anodes, mainly when GDC is used as an electrolyte. As GDC activation energy is lower than that of YSZ, SOFC using this type of electrolyte could work at lower temperatures, which, in return, would reduce costs of other cell components. Moreover CeO<sub>2</sub>-based anodes present higher resistance against redox cycling and better performance with hydrocarbon fuels<sup>6,7</sup> On the other hand, Co-based cermets such as Co-YSZ and Co-GDC have also been proposed for SOFC. Cobalt is more costly than nickel, but it is a better catalyzer and its sulphur tolerance is higher.<sup>8,9</sup>

The properties of the anode materials are highly dependent on the microstructure and on the metal-ceramic interface.<sup>10,11,12</sup> In general, when using conventional preparation methods, it is not possible to exert control on the metal-ceramic interfaces. Alternatively, a porous cermet obtained through reduction of a directionally solidified eutectic (DSE) of NiO-YSZ, CoO-YSZ or CoO-GDC has been proposed for anode.<sup>13</sup> Using this method it is possible to prepare aligned composite structures that, after reduction of the transition metal oxide, will result in a porous cermet. In a eutectic process the liquid solidifies simultaneously into two or more solid phases, producing a fine and homogeneous microstructure. In general DSE oxides present good mechanical properties in comparison with conventional ceramics, as well as better stability at high temperature operation.<sup>14</sup> Eutectic growth is ruled by minimization of the interfacial energy, which, for the compositions studied in this paper, results in the formation of a self-organized lamellar microstructure with low-energy interfaces. The constituent phases are well aligned along the solidification axis and the phase size can be tailored by choosing the solidification rate according to the Hunt-Jackson law.<sup>15</sup> The channeled microstructure of these cermets allows easy gas flow and electronic conduction through the metallic porous lamellae, whereas the ceramic scaffold provides an appropriate coefficient of thermal expansion (CTE) to get good thermomechanical integration with the electrolyte.<sup>16,17</sup> Moreover, the interfaces in this type of cermets are different to those found in conventional Ni-YSZ anodes, which give rise to improved anode properties and, specifically, better resistance against ageing.<sup>18,19</sup> For a good understanding of the metal-ceramic interfaces formed after reduction of the eutectic composite, prior understanding of both the oxide-oxide interfaces formed in the eutectic and of the parameters controlling its formation is essential.<sup>20,21,22</sup> This being the main objective of the paper.

Minford *et al.*<sup>23</sup> established in 1979 the two main factors that determine the interface plane and the orientation relationship in directionally solidified eutectics: the balance of charge at the interface and the minimization of the lattice misfit. Several models have been developed in order to predict or account for experimental orientation relationship between phases and interphase

configuration in different systems, based upon atomistic considerations (such as Density Functional Theory),<sup>24,25</sup> or geometrical considerations in 2D (Near Coincidence Site Lattice, NCSL)<sup>26,27</sup> or 3D (Coincidence of Reciprocal Lattice Points, CRLP).<sup>28</sup> The latter is based upon the hypothesis that most stable configurations correspond to relative orientations where the crystal lattices at the interphase suffer the minimum possible distortion in terms of interplanar spacing continuity. The CRLP model was developed to study heterophase interfaces and it has proved able to account for orientation relationships between phases in metal/ $\alpha$ -Al<sub>2</sub>O<sub>3</sub> systems,<sup>29</sup> as well as in Ni films deposited on YSZ by the pulsed laser deposition technique.<sup>30</sup>

In this paper, using Electron Backscattering Diffraction (EBSD), we have characterized the growth direction, interface plane and orientation relationship between the component phases of a family of eutectics. In recent years the EBSD technique has become a powerful microstructural characterization tool which is highly appropriate for studying relatively large surface samples displaying one or more orientation relationships.<sup>31</sup> The eutectics studied are formed by a transition metal oxide (NiO or CoO) and an ionic conductor (YSZ and GDC) that can be used as precursors for SOFC anodes. NiO-CeO<sub>2</sub> and CoO-CeO<sub>2</sub> have also been included in the paper for comparison with the doped ceria eutectics. The experimental results are discussed in terms of the balance of charge density at the interface and of the lattice misfit. To determine the orientation relationship that correspond to the optimum geometrical coherence between the constituent phases, the CRLP model has been applied.

# 2. Experimental details

#### 2.1 Preparation of the samples

Directionally solidified eutectic materials combining NiO or CoO, as precursor of the transition metal component of the cermet (TMO=NiO, CoO), and YSZ, GDC or CeO<sub>2</sub> as ionic conductors (IC=YSZ, GDC, CeO<sub>2</sub>) were prepared using the Laser Floating Zone method (LFZ). For this purpose, powders of NiO (99%, Alfa Aesar), Co<sub>3</sub>O<sub>4</sub> (99.7%, Alfa Aesar), YSZ (8 mol%

Y<sub>2</sub>O<sub>3</sub> stabilized ZrO<sub>2</sub>, 99.9%, Tosoh), GDC obtained from inorganic salt precursors following Pechini method<sup>32</sup> and CeO<sub>2</sub> (99.9%, Aldrich) were mixed, isostatically pressed under 200 MPa for 5 min and sintered at 1400 °C to obtain ceramic cylinders, 8 cm long and 2.5 mm in diameter. Then, these ceramic precursors underwent melting and subsequent solidification using the LFZ technique to obtain DSE rods with the compositions<sup>16,33,34,35</sup> and solidification rates indicated in Table 1. The laser used was a CO<sub>2</sub> continuous wave laser ( $\lambda = 10.6 \mu$ m; Blade600, Electronic Engineering, Firenze) and the eutectics were processed in two steps. In the first step, at 200 mm/h upwards, the ceramic precursor cylinder densifies and stretches, whereas the final step was performed downwards at the selected growth rate. The final diameter of the eutectic rod was 2 mm. The CoO eutectics were grown under inert atmosphere, assuring the reduction of Co<sub>3</sub>O<sub>4</sub> to CoO during the first processing step. X-ray analysis proved that the cobalt oxide in the resulting material was CoO.

#### 2.2 Electron Backscattering Diffraction experiments

Scanning Electron Microscopy (SEM) analysis and EBSD experiments were carried out in polished transverse and longitudinal cross-sections using a Merlin Field Emission SEM (Carl Zeiss, Germany), with an integrated EBSD system (HKL model from Oxford Instruments, United Kingdom).

The EBSD experiments were performed positioning the 70°-tilted sample at 14.5 mm from the pole piece and using 20 kV of accelerating voltage and 0.8 nA of probe current. The EBSD detector (model HKL EBSD system, Oxford Instruments) consists of a CCD camera that was set to 514 x 384 resolution using 4x4 binning. Each Kikuchi pattern was acquired twice (60 ms of acquisition time) and averaged out. The Channel5 software<sup>36</sup> was used to automatically detect 7 Kikuchi bands and index each pattern to determine the crystallographic orientation of the sample at that very spatial point and produce an orientation map for every experiment. This software also generates pole figures and calculates the lattice correlation boundary between phases. Typical

acquisition time of a map of a zone of about 50 x 9  $\mu$ m was about 2 hours, using 0.08  $\mu$ m size pixels. Depending on the interphase spacing of each sample the pixel size ranged from 0.05 to 0.3  $\mu$ m. Despite the relatively low number of bands used and the low camera resolution, it was possible to determine the spatial orientation with an angular accuracy better than 0.5° due to the high symmetry of the crystallographic phases involved. NiO and CoO are rock-salt structures whereas YSZ, GDC and CeO<sub>2</sub> are fluorite structures, all of them belonging to the F $m\bar{3}m$  space group.

Specimen preparation for EBSD was performed using a progressive lapping and polishing method to eliminate in each step the strains created during the previous one, which would blur the Kikuchi bands that form the EBSD patterns, also known as Kikuchi patterns. Special care has been taken to ensure that the sample surface is free of damage, because the EBSD patterns are generated from a very thin surface layer of about 40 nm.<sup>31</sup> Slices of the fibers were severed with a diamond saw, and then the cross-sections were ground in successive steps with SiC (15  $\mu$ m and 10  $\mu$ m of particle size using a polishing wheel rotating at 40 rpm), polished with diamond paste (**3**  $\mu$ m and **1**  $\mu$ m of particle size, 120 rpm) and finally colloidal silica (0.04  $\mu$ m of particle size, 100 rpm) for 15 min. Throughout the preparation process, the specimen was subjected to a 2.5 N load. Since colloidal silica might cause differential polishing between the phases, the duration of this treatment was chosen with the aim of obtaining a conveniently polished surface with only slight differential polishing. Differential polishing had to be kept to a minimum to avoid shadows in the orientation maps due to the tilted position of the sample. This shadowing effect is particularly important for eutectics grown at high rates because they display low interlamellar spacing.

# 2.3. Coincidence of Reciprocal Lattice Points (CRLP) calculation procedure

In order to determine the most favorable orientation relationship between the component phases of the eutectic we have used the CRLP method. <sup>28</sup> In order to apply this method we have

developed a Matlab code that calculates the overlapping of the reciprocal lattices of two phases of the eutectic. Each point P of the reciprocal lattice is associated with a family of the real lattice planes (hkl) as follows:  $OP_{hkl}=h\cdot a^*+k\cdot b^*+l\cdot c^*$ , where  $a^*$ ,  $b^*$  and  $c^*$  are the primitive vectors of the reciprocal lattice, the modulus of the  $OP_{hkl}$  vector being proportional to the inverse of the interplanar spacing.<sup>37</sup> The coincidence, or more precisely the near-coincidence of the reciprocal lattices, is calculated assuming that each point of the reciprocal lattice bas spherical shape with radius r\*. We have placed small spheres at the reciprocal lattice points and superpose both lattices according to a given orientation relationship. We have then calculated the intersection volume between all of the spheres for every possible orientation relationship. Those orientation relationships that yield the highest intersection volumes are the most favorable ones according to this model, since this means that there are several family planes with similar interspacing parallel to each other, that is to say, there is little discontinuity at the interface formed for that orientation relationship.

In the work presented in this paper, we took into account all reciprocal lattice points contained in a sphere of radius  $6 \cdot a^* (a^*=2\pi/a)$ , where *a* is the cell parameter of the TMO. The same volume considered for the IC phase included more points, since the cell parameters of the studied IC here are bigger than those of the TMO (NiO and CoO). The radius of the small spheres sited at the reciprocal lattice points was  $0.2 \cdot a^*$ . For the calculation of the overlapped volume as a function of the OR, the TMO lattice was set fixed and the IC phase was rotated in steps of 1° using the Euler angles. We used the ZXZ' convention for the Euler angle definition and reduced the Euler space to  $\alpha \in (0, 90^\circ)$ ,  $\beta \in (0, 90^\circ)$  and  $\gamma \in (0, 90^\circ)$  due to the cubic symmetry of the phases.<sup>38</sup>

#### **3. Experimental results**

# 3.1 Microstructure

Cylinders of NiO-YSZ, CoO-YSZ, NiO-GDC, NiO-CeO<sub>2</sub>, CoO-GDC and CoO-CeO<sub>2</sub> in their eutectic composition were grown following the process described above, and slices were cut

perpendicular to the solidification direction, i.e. perpendicular to the cylinder axis. Those transverse cross-sections were analyzed in a SEM. Lamellar microstructure, where NiO/CoO and YSZ/GDC/CeO<sub>2</sub> lamellae alternate, was found in all materials and for all solidification rates, while fibrillar microstructure was only found in the CoO eutectics solidified at low rate (10 mm/h), coexisting with the lamellar microstructure as described previously for the CoO-GDC case.<sup>21</sup> In those cases, CoO fibers were embedded in a YSZ/GDC/CeO<sub>2</sub> matrix. The interphase spacing ( $\lambda$ ) determined from the SEM experiments decreases with the solidification rate ( $\nu$ ), according to Hunt-Jackson law:  $\nu \cdot \lambda^2 = K$ , where *K* is a constant which depends on the material and the thermal gradient for each fabrication method.<sup>15</sup> The value of the interphase spacing obtained is indicated in Table 1.

# 3. 2. Orientation relationships, growth directions and interface planes

EBSD experiments were performed to determine the growth directions, interface planes and orientation relationships between phases. We analyzed the fibrillar and the lamellar areas in the central area of the transverse cross-sections as well as in peripheral zones. In these kinds of experiments, an Electron Backscattered Pattern (EBSP) is obtained from every point on the sample surface hit by the electron beam. The EBSP reflects the crystal symmetry of the point from which it has been taken as well as the spatial orientation, which can be determined from the position of the Kikuchi bands (an example of an EBSD pattern is shown in Fig. 1). In a typical orientation map, like the one shown in Fig. 2, a color or grey level is assigned to the crystallographic orientation according to a conventional scheme.<sup>3636</sup> As a consequence, all the pixels displaying the same grey level have the same crystallographic orientation and form a crystallographic grain if connected to each other. In Fig. 2, it can be seen that there are orientation deviations between eutectic grains (up to 20°), but within each grain, each phase behaves as a single crystal.

#### 3.2.1 Lamellar areas

The growth direction of each phase can be determined from the pole figures (Fig. 3). They appear as low Miller index crystal axes parallel to the cylinder axis, ergo, to the direction that is perpendicular to the sample transverse cross-section. They can be identified in the pole figures as poles close to the center of the stereogram. Thus, in the majority of areas with lamellar microstructure, experiments showed two possible combinations of growth directions (GD):

 TMO = NiO, CoO
 IC = YSZ, GDC, CeO<sub>2</sub>

 GD1:
  $\overline{(011)}$  //
 [010]

 GD2:
  $\overline{(110)}$  ~ 15° //
 [110]

where, between all the possible symmetry equivalent options, we have chosen a sign criteria that we will maintain throughout the paper. In both cases, the rock-salt structure phase (TMO = NiO, CoO) grows along the <110> crystal axis, while the fluorite structure phase (IC = YSZ, GDC, CeO<sub>2</sub>) may grow along the <100> axis as well as along the <110> axis. In the former case, growth directions  $[0\bar{1}1]_{TMO}$  and  $[010]_{IC}$  are fully parallel (growth direction GD1). In the latter,  $[1\bar{1}0]_{TMO}$  and  $[110]_{IC}$  are 15° misoriented (growth direction GD2).

Table 2 summarizes the growth directions found for each material studied at all solidification rates. Some authors suggested that the appearance of GD1 or GD2 could depend, among other factors, on the solidification rate.<sup>20</sup> However, the experimental results obtained in this work do not confirm this suggestion.

Interface planes were determined from the orientation maps and pole figures. The interface planes from both phases are parallel to each other and, as they are represented in the pole figure by their perpendicular axes, they can be identified as poles close to the stereogram periphery. We also verified that these planes correspond to the projection of the interface planes observed in the orientation map. Moreover, the EBSD Channel5 software<sup>36</sup> enables the calculation of the relative

orientation for any pair of axes or planes from the different phases, the so-called *lattice correlation boundary component*, and represents it in the orientation map. Thus, it is possible to calculate the misorientation for the given directions at every point of the interface drawn in the orientation maps. Moreover, quantitative data can be inferred from the misorientation histograms. This tool was used to verify the interface planes, namely,  $(111)_{TMO}/(001)_{IC}$  for GD1 and GD2 cases. Misorientation between these planes was calculated in all experiments, and in most cases it is lower than 1°, while the best angular resolution is 0.5° for this experimental setup, which confirms that  $(111)_{TMO}/(001)_{IC}$  are the actual interface planes.

In addition to the above-described OR, which is the most commonly found, we have observed the presence in some areas of a cube-on-cube OR, where the crystal axes of both phases are parallel. From the pole figures in this case the growth direction seems to be [111] or [110], depending on the zone analyzed. Fig. 4 shows an orientation map acquired over a longitudinal cross-section of a NiO-YSZ sample solidified at 10 mm/h where the cube-on-cube orientation relationship appears. With the aim of determining the interface plane for the zones with the minority OR, we performed additional EBSD experiments on transverse and longitudinal crosssections of NiO-YSZ solidified at 10 mm/h, since this was one of the materials and solidification rates in which the cube-on-cube OR appears more frequently. In the orientation maps the lines we observe representing the interface plane are produced by the intersection between the interface plane and the sample surface, and they correspond to vectors contained in the interface plane. As we can determine the crystallographic coordinates of these vectors form the orientation maps, the interface plane is obtained by doing the cross product of the intersection vectors obtained from transverse and longitudinal cross-sections. This procedure is not without its ambiguity, because the two vectors are obtained from different specimens. However, using vectors from different zones we have verified that the cross product results in a unique interface plane with coordinates of about (0.185, 0.188, 0.965), which forms ~15° with the (001) plane.

#### 3.2.2 Fibrillar areas

In the fibrillar zones, similar results were found in the case of the CoO-GDC, where the growth directions and lattice correlation boundary are the same as described for the majority orientation relationship in lamellar areas (Fig 5a). Nonetheless, CoO-CeO<sub>2</sub> and CoO-YSZ fibrillar areas showed different behavior. The orientation of the crystallographic axes varies throughout the same transverse cross-section, and there is no defined growth direction (Fig 5b). The orientation relationship between the phases also changes from one experiment to another. Furthermore, a cube-on-cube orientation relationship was found in CoO-CeO<sub>2</sub> and CoO-YSZ fibrillar areas, whereas it was not observed in fibrillar CoO-GDC.

# 4. Discussion

The particular properties of DSE materials are mostly due to their special interfaces, which are clean and strong, without interfacial precipitates. The nature of these interfaces stems from the thermodynamics ruling the eutectic growth, i.e., the minimization of the interfacial energy. Minford *et al.* were the first authors who reviewed the characteristic of the interfaces in DSE.<sup>23</sup> They pointed out that the orientation relationships in DSE result from two main factors: minimization of the lattice misfit between phases and the optimum matching between ionic charge densities of the polar planes involved. The interfaces are thought to be made up of a single plane of oxygen atoms, common to both crystal structures<sup>39</sup> and therefore, the non-directional ionic forces within each phase bond ions beyond the interface, strongly joining the phases in the DSE. These low-energy interfaces made up of polar planes may contribute to the exceptional microstructural stability of the studied materials. Hitherto, only one experimental direct observation of the interface being made up of a single plane of oxygen atoms has been reported: a HRTEM image combined with an EELS experiment carried out by E.C. Dickey *et al.*<sup>40</sup> However, to get these kinds of images the zone axes of both phases have to be perfectly parallel at the interface, and this is not the common situation in DSE. To determine the OR between the phases

and the interfacial planes we used mainly EBSD because it enables us to obtain this information throughout an extensive area of the sample surface.

#### 4.1. Growth directions, orientation relationship and interface planes

EBSD experiments showed that there are two possible growth directions:  $[110]_{TMO}$  fully parallel to  $[100]_{IC}$  (growth direction GD1), and  $[110]_{TMO}$  and  $[110]_{IC}$  15° misoriented (growth direction GD2). The interface planes are, in both cases,  $(111)_{TMO}$  and  $(001)_{IC}$ . These growth directions have been previously reported in samples grown at different rates and using different methods,<sup>20,21,41,42,43</sup> but it should be pointed out that they do correspond to the same orientation relationship between the interface planes.

The relative orientation of the interface plane atoms between the phases is shown in Fig. 6. The geometric configuration of these planes determines that whenever the axes  $[0\bar{1}1]_{TMO}$  and  $[010]_{IC}$  are parallel,  $[1\bar{1}0]_{TMO}$  and  $[110]_{IC}$  appear 15° systematically misoriented. Thus, it can be inferred that the relative orientation between TMO and IC phases is unique despite the growth direction. To represent the interfacial coincidence in a clear picture is not an easy task because the ions in the TMO phase are divalent whereas the ions in IC are either divalent, trivalent or tetravalent. As it is usually assumed that the interfacial plane is made up of a common oxygen plane, which maintains the anion-cation sequence of planes, we considered it was more coherent to show the coincidence between  $(001)_{IC}$  oxygen ions and  $(111)_{TMO}$  transition metal ions. Another valid criterion could be to represent the coincidence of oxygen ions from both phases. As a common oxygen plane forms the interface, it would have to be in a mixed configuration between that of the component phases, with a minimum distortion. In any case, as the (111) planes of anions and cations in the TMO rock salt structures are identical, the coincidence shown in Fig. 6 is the same with either criteria.

The growth direction is usually identified as a crystallographic axis of the material, which is oriented parallel to the solidification direction, i.e., to the cylinder axis. This axis can be identified in the pole figure as a pole close to the centre of the stereogram. A pole situated exactly at the centre of the pole figure is seldom found. Small deviations might be due to the solidification front curvature or any other small experimental deviation. However, since the interfacial planes are always  $(111)_{TMO}/(001)_{IC}$ , and the orientation relationship between these interface planes is the same for GD1 and GD2, the material might not be growing exactly along any preferred crystallographic axis, neither GD1 nor GD2. We believe that it is actually this preferred orientation relationship that is governing the spatial orientation of the phases during the solidification process. The fact that, in some cases, both GD1 and GD2 have been found over the same surface is consistent with this idea. Moreover, the component phases of these materials have relatively low entropy of melting. Their dimensionless entropy of melting usually ranges between 3 and 3.5.<sup>44</sup> The entropy of fusion criterion of Hunt and Jackson<sup>45</sup> was originally proposed in 1966 to classify eutectic morphologies. They used a nearest-neighbour broken model and thermodynamic arguments to show that the type of growth depends on the dimensionless molar entropy of melting  $\Delta S/R$ , where  $\Delta S$  is the entropy of melting and R is the ideal gases constant. Substances with low entropy of fusion, generally considered if  $S \leq 2$ , present independence of the growth kinetics with respect to the crystal direction. In these materials, the growth direction is mainly governed by the heat flow and not by the crystallography of the component phases.<sup>46,47</sup>

With respect to the cube-on-cube orientation relationship, it is not easy to quantify the presence of this minority OR. Crystal growth is a rather complex matter and the occurrence of different growth habits from the usual one is not surprising. However, it is important to point out that we have determined the presence of the cube-on-cube OR in the whole family of eutectics studied, mainly in the NiO-YSZ case grown at low rates. The cube-on-cube orientation relationship has previously been reported by Minford *et al.* for MgO-MgAl<sub>2</sub>O<sub>4</sub>, MgO-ZrO<sub>2</sub> and MgO-CaO DSE,<sup>23</sup> by Larrea *et al.* for CoO-YSZ DSE<sup>19</sup> and by Xing *et al.* for NiO-YSZ

fabricated by Pulsed Laser Deposition.<sup>48</sup> As we have previously mentioned, the interface plane seems to be near the (001), but this plane is not polar in the rock-salt structure of the TMO phases, which is contradictory to what has been reported about interfaces in DSE oxides.<sup>14</sup> Moreover the apparent interface plane is not perpendicular to one of the growth directions observed, [111]. Although this OR was first reported in 1979, there is still lack of understanding.

# 4.2. Ionic charge balance at the interface

As mentioned before, one of the requirements for the formation of DSE interfaces is the ionic charge density balance at the interface. The maintenance of the charge balance across the interface is a requirement of Pauling's second rule of ionic structures, because the ionic bonds extending from the interface plane must be compensated for on the polar plane of the other phase. <sup>49</sup> To check the fulfilment of this rule and to determine the possible pairs of planes with good balance, the ionic charge density was calculated for low Miller indices planes (see Table 3) in all materials, as well as the misfit between each possible combination of planes. It is known that there is some Ni diffusion (2 mol%) in the YSZ in the case of the NiO-YSZ eutectic, as well as some Co diffusion (5 mol%) in the YSZ in the case of the CoO-YSZ eutectic.<sup>16</sup> In the case of the CoO-GDC and CoO-CeO<sub>2</sub>, there is no detectable diffusion,<sup>21</sup> and in the case of the NiO-GDC and NiO-CeO<sub>2</sub>, it has not been determined. In addition to the diffusion of Ni and Co cations into the YSZ, it was assumed that the oxygen vacancies were homogenously distributed throughout the bulk, and that the NiO and CoO were stoichiometric. In spite of these assumptions, the lowest ionic charge density misfit, between high charge density polar planes, was found for  $(111)_{TMO}/(001)_{IC}$  for all the eutectics studied, which is the actual interface plane according to the EBSD experimental results (see Table 4). If we include in these calculations the polar planes with low charge density, we could obtain lower misfits, for instance in the  $(221)_{GDC}$  and  $(511)_{NiO}$  case. However, the stability of these interfaces between low-polarity planes would necessarily be lower.

We would like to point out that the three eutectics displaying the poorer misfit present deviations with respect to the most usual growth behaviour. CoO-YSZ (13.6 % misfit) and CoO-CeO<sub>2</sub> (6.7 % misfit) present fibrillar areas with neither clear growth directions nor well-defined interfacial planes. However, the CoO-GDC eutectic (4.3 % misfit) that also presents fibrillar microstructures always displays the majority OR and well defined (111)<sub>TMO</sub>//(001)<sub>IC</sub> interface plane. In addition, in the NiO-YSZ (9.9% misfit) and CoO-YSZ eutectics we have frequently observed the presence of the cube-on-cube orientation relationship.

#### 4.3. Lattice matching and CRLP calculations

In order to analyse the lattice matching of the component phases, the first approximation is to calculate within the interface plane,  $(111)_{TMO}$  and  $(001)_{IC}$ , the misfit of the oxygen sublattice for the close-packed direction,  $[011]_{TMO}/[010]_{IC}$ , and its perpendicular,  $[211]_{TMO}/[100]_{IC}$ . Tiller was the first author to propose that, as lattice strain energy is a major contribution to the interface energy, the interface planes with the minimum misfit would result in favoured low-energy interfaces.<sup>50</sup> This misfit is calculated as  $\delta = 2(l_1-l_2)/(l_1+l_2)$ , where  $l_1$  and  $l_2$  are the interface plane. According to the model and approximations used by Frank and Van der Merwe, coherent interfaces could be expected for misfits lower than about 9%.<sup>51</sup> The results are shown in Table 5, where it can be observed that the calculated lattice parameters misfit is quite high in at least one of the directions for all the materials in the family.

However, this approach could be considered only a first approximation to get an idea of the lattice matching. To get further insight into this matter, we have applied the CRLP model to the eutectic growth for the first time. The ionic charge balance at the interface would explain the formation of the  $(111)_{TMO}/(001)_{IC}$  interface in the whole family studied, as well as possibly indicating a potential origin of the deviations from this behaviour. However, we would like to investigate the reasons of the appearance of the well-defined majority OR and of its deviation, the

cube-on-cube OR. Considering, moreover, that in the last case we have not identified the interface plane.

The idea that a good matching between the lattices in the interface plane is one of the factors determining the orientation relationship between phases during eutectic growth may be extended to a good matching between the lattices in 3D by considering the CRLP model. This model takes into account not only atoms contained in the interface plane, but also all the low-index Miller planes from both phases. Thus, the most favourable orientation relationships between phases are those for which there are most planes with similar interspacing parallel to each other, i.e., those that give rise to a high intersection volume between the spheres located at the reciprocal lattices of both phases.

Although the CRLP model does not consider the interface plane in the calculations, it does determine the orientation relationship that maximizes the three-dimensional lattice continuity. Therefore, the favourable orientation relationship determined by the CRLP model corresponds to the state of better 3D geometrical coherence between the two adjacent crystals, which would probably correspond to the minimum elastic strain energy at the interface.<sup>29</sup> In addition, the ability of the CRLP method to predict not only the primary orientation relationship, but also secondary orientation relationships is significant.

The results of the CRLP calculations for the NiO-YSZ DSE are shown in Fig. 7. The extension of these calculations to the other eutectic systems will be presented in a future article. Fig. 7(a) is a representation of the 3D Euler space where the points marked in dark correspond to those combinations of Euler angles for which the calculated overlapped volume is the highest, above a certain threshold. It is easier to understand Fig. 7(b), where the horizontal axes correspond to the first two Euler angles,  $\alpha$  and  $\beta$ , and in the vertical axis we represent the overlapped volume for each pair of  $\alpha$  and  $\beta$  values and  $\gamma=0$ . It is possible to observe two main peaks for the values  $\alpha_1=45^\circ$ ,  $\beta_1=35.3^\circ$ ,  $\gamma_1=0^\circ$  and  $\alpha_2=45^\circ$ ,  $\beta_2=54.7^\circ$ ,  $\gamma_2=0^\circ$ , with the same height

that represent the two absolute maxima. Analysing the rotations produced by these Euler angles we obtained two symmetrically equivalent OR corresponding to the majority orientation relationship  $(111)_{TMO}/(001)_{IC}$  and  $[011]_{TMO}/[010]_{IC}$ . The minority cube-on-cube orientation relationship ( $\alpha$ =0,  $\beta$ =0,  $\gamma$ =0) may be distinguished in Fig. 7 (b) among other secondary relative maxima.

However, due to the large number of maxima that can be observed in Fig. 7 (a), a careful study of the symmetry equivalent ORs is essential. The triplet of Euler angles characterize the rotation that we have to apply to the IC phase to place it in the same orientation as the TMO phase. Due to the high symmetry of both phases we can obtain a large number of Euler triplets associated to symmetry equivalent variants of the same orientation relationship. The orientation of each phase with respect to a fixed reference system can be characterized by a rotation matrix (S<sub>IC</sub> and S<sub>TMO</sub>). In this way, an Euler rotation matrix  $G=G(\alpha,\beta,\gamma)$  for a particular inter-phase orientation relationship is defined by:

$$\mathbf{S}_{\mathrm{TMO}} = \mathbf{G}(\alpha, \beta, \gamma) \cdot \mathbf{S}_{\mathrm{IC}} \tag{1}$$

If we apply to each phase a rotation of its own point group ( $O_i$  and  $O_j$  for TMO and IC respectively) we obtain symmetry equivalent orientation relationships:

$$O_{i} \cdot S_{TMO} = G(\alpha, \beta, \gamma) \cdot O_{j} \cdot S_{IC}$$
<sup>(2)</sup>

As a consequence, for a given rotation matrix the set of symmetry equivalent matrices is given by:

$$G(\alpha',\beta',\gamma') = O_i \cdot G(\alpha,\beta,\gamma) \cdot O_j \quad \forall \ O_i \in R(TMO), \quad \forall \ O_j \in R(IC)$$
(3)

where R is the group formed by the rotations of the point groups of each phase. In our case the point groups of all the phases are the same,  $m\overline{3}m$  and this has 24 elements. So, in the full Euler space,  $\alpha \in (0, 360^\circ)$ ,  $\beta \in (0, 180^\circ)$  and  $\gamma \in (0, 360^\circ)$ , we have 24x24=576 Euler triplets. To

manage this large number of symmetry equivalent points we have implemented in our Matlab code an algorithm to identify all the maxima and a procedure to calculate the symmetry equivalent points for each maxima. Using these tools we have finally found that all the absolute maxima represented in Fig. 7(a) have the same overlapped volume and correspond to the same orientation relationship as the experimentally found  $(111)_{TMO}/(001)_{IC}$  and  $[0\bar{1}1]_{TMO}/[010]_{IC}$ . However, the cube-on-cube OR, corresponds to secondary maxima, which is less commonly found.

# **5.** Conclusions

NiO-YSZ, NiO-CeO<sub>2</sub>, NiO-GDC, CoO-YSZ, CoO-CeO<sub>2</sub> and CoO-GDC directionally solidified eutectic ceramics have been produced by the LFZ technique at rates varying from 10 to 200 mm/h. Two types of microstructure were found in this family of eutectic materials: lamellar and fibrillar (only for CoO eutectics solidified at low rate). Two orientation relationships were found in the lamellar areas. The most common one is given by the following parallelisms:  $(111)_{TMO}/(001)_{IC}$  and  $[OII]_{TMO}/[O10]_{IC}$ . Two different growth directions were found for this orientation relationship, and both give rise to the same interface plane:  $(111)_{TMO}/(001)_{IC}$ . The less common orientation relationship found in the lamellar areas is the so-called cube-on-cube, where the IC phase and the TMO phase grow parallel to each other. For this orientation, we determined that the interface plane is a crystal plane that forms about 15° with the (001) plane.

The calculations of the ionic charge balance at the interface show that, from the whole family of eutectics studied, the best possible matching is obtained for the experimentally found  $(111)_{TMO}/(001)_{IC}$  interface plane. Moreover, the eutectics that present poorer charge balance (CoO-YSZ, NiO-YSZ and CoO-CeO<sub>2</sub>) also present deviations from the usual growth behavior in the fibrillar areas when growth is at low rates.

The CRLP model has been applied to NiO-YSZ eutectic and predicts that the most common orientation relationship observed is the most favorable one, because it corresponds to the absolute maximum overlapping of reciprocal lattices calculated by the model. The less common cube-oncube orientation relationship corresponds to secondary maxima predicted by the model. Further calculations are in progress to apply this model to the other eutectic of the family studied in this paper.

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#### **FIGURE CAPTIONS**

Fig. 1. Kikuchi pattern acquired on a YSZ lamella of a CoO-YSZ specimen, (a) as acquired and (b) after indexation of the bands to determine the crystallographic orientation (round markers signal the main YSZ zone axes). The acceleration voltage was 20 kV and the probe current, 0.8 nA.

Fig. 2. EBSD orientation map of a CoO-YSZ sample solidified at 100 mm/h. Pixels with the same grey level correspond to surface areas with the same orientation. Within each eutectic grain, each phase behaves as a single crystal.

Fig. 3. Experimental pole figures for two different areas of the same transverse crosssection of a NiO-YSZ sample. In 3(a) the pole figures show growth direction GD1: <110> for NiO and <100> for YSZ (b). In 3(b) the pole figures show growth direction GD2: <110> for NiO and <110> for YSZ. In both cases, the interface plane is  $\{001\}_{YSZ}//\{111\}_{NiO}$ , highlighted by a square marker, while growth directions are signaled by round markers.

Fig. 4. (a) Forescatter image of a longitudinal cross-section of NiO-YSZ solidified at 10 mm/h. Surface relief due to differential polishing produces the contrast. (b) Orientation map of the same area. The absence of contrast indicates the presence of the cube-on-cube orientation relationship, where the two phases are parallel.

Fig. 5. (a) Orientation map of a CoO-GDC fibrillar area. The phases display a welldefined OR, the same as in the lamellar areas. (b) Orientation map of a CoO-YSZ fibrillar area. The different grey levels indicate different orientations of the fibres. Fig. 6. Coincidence of atoms at the  $(001)_{YSZ}$ //(111)<sub>NiO</sub> interface plane. Filled-in circles stand for  $(001)_{YSZ}$  oxygen anions while unfilled-in circles represent  $(111)_{NiO}$  nickel cations. Growth directions GD1 and GD2 are indicated in the figure.

Fig. 7. (a) High overlapping zones of the 3D Euler space, according to the CRLP model applied to NiO-YSZ. (b) Normalized overlapped volume as a function of the  $\alpha$  and  $\beta$  Euler angles ( $\gamma$ =0°).

# **TABLE CAPTIONS**

**Table 1:** Composition, solidification rates and interphase spacing of the studied DSE.

**Table 2:** Growth directions (GD1 or GD2, see main text) found for each material and solidification rate.

**Table 3:** Ionic charge density for some low-Miller-indices polar planes, calculated for

 the indicated cell parameter, a.

**Table 4:** Misfit between the ionic charge density of the  $(111)_{TMO}//(001)_{IC}$  polar planes calculated for each material.

**Table 5:** Misfit between lattice parameters along the close-packed directions of the interface planes,  $[0\bar{1}1]_{TMO}//[010]_{IC}$ , and along the crystallographic directions perpendicular to the close-packed ones,  $[2\bar{1}1]_{TMO}//[100]_{IC}$ , for each DSE.

Eutectic material	Composition (mol%)	Solidification rate	Interphase spacing $\lambda$ ( $\mu$ m) 0.2 - 3 0.5 - 3.4
		(mm/h)	spacing $\lambda$ (µm)
NiO – YSZ	77 % NiO, 23 % YSZ	10, 50, 100	0.2 - 3
CoO – YSZ	80 % CoO, 20 % YSZ	10, 50, 100	0.5 - 3.4
	72 % NO 27 % CDC	10 50 100	07.20
NIO – GDC	73 % NIO, 27 % GDC	10, 50, 100	0.7 - 3.8
NiO – CeO <sub>2</sub>	73 % NiO, 27 % CeO <sub>2</sub>	10, 50, 100	0.5 - 3
CoO – GDC	82 % CoO, 18 % GDC	10, 50, 100, 200	0.7 - 3.8
$CoO - CeO_2$	82 % CoO, 18 % CeO <sub>2</sub>	10, 50, 100, 200	0.5 - 3.4

**Table 1:** Composition, solidification rates and interphase spacing of the studied DSE.

Solidification rate	NiO-YSZ	CoO-YSZ	NiO-GDC	NiO-CeO <sub>2</sub>	CoO-GDC	CoO-CeO <sub>2</sub>
10 mm/h	GD1 GD2	GD1	GD1	GD2	GD1	GD2
50 mm/h	GD1	GD1	GD1	GD2	GD1	GD1
	GD2	001	021	022	021	GD2
100 mm/h	GD2	GD1	GD1	GD2	GD2	GD1
200 mm/h	-	-	-	-	GD1	GD2

Table 2: Growth directions (GD1 or GD2, see main text) found for each material and solidification rate.

	Ionic charge density $(e^{-}/Å^2)$				Ionic charge	density (e <sup>-</sup> /Å <sup>2</sup> )
	YSZ	GDC	CeO <sub>2</sub>		NiO	CoO
a (Å)	5.127	5.418	5.411	-	4.179	4.252
{111}	0.338	0.307	0.315	{111}	0.265	0.255
{100}	0.292	0.266	0.273	{311}	0.138	0.133
{311}	0.177	0.160	0.165	{331}	0.105	0.101
{331}	0.134	0.122	0.125	{511}	0.088	0.085
{102}	0.130	0.119	0.122	{531}	0.077	0.075
{221}	0.098	0.089	0.091	{551}	0.064	0.062
{308}	0.034	0.031	0.032	{771}	0.046	0.044

**Table 3:** Ionic charge density for some low-Miller-indices polar planes, calculated for

 the indicated cell parameters, *a*.

	NiO-YSZ	CoO-YSZ	NiO-GDC	NiO-CeO <sub>2</sub>	CoO-GDC	CoO-CeO <sub>2</sub>
Misfit (%)	9.9	13.6	0.5	2.9	4.3	6.7

**Table 4:** Misfit between the ionic charge density of the  $(111)_{TMO}//(001)_{IC}$  polar planes calculated for each material.

	Misfit along the close- packed directions	Misfit along the perpendicular to the close- packed directions
NiO -YSZ	14 %	0 %
CoO - YSZ	16 %	2 %
NiO - GDC	8 %	6 %
NiO - $CeO_2$	8 %	6 %
CoO - GDC	10 %	4 %
$CoO - CeO_2$	10 %	4 %

**Table 5:** Misfit between lattice parameters along the close-packed directions of the interface planes,  $[0\bar{1}1]_{TMO}/[010]_{IC}$ , and along the crystallographic directions perpendicular to the close-packed ones,  $[2\bar{1}1]_{TMO}/[100]_{IC}$ , for each DSE.





Figure 2 Click here to download high resolution image



Figure 3a Click here to download high resolution image





Figure 3b Click here to download high resolution image



















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