

# Improvement of microstructural properties of 3Y-TZP materials by conventional and non-conventional sintering techniques

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## Abstract

3 mol% Y<sub>2</sub>O<sub>3</sub>-stabilized zirconia nanopowders were fabricated using various sintering techniques; conventional sintering (CS) and non-conventional sintering such as microwave (MW) and **pulsed electric current-assisted-sintering (PECS)** at 1300 °C and 1400 °C. A considerable difference in the densification behaviour between conventional and non-conventional sintered specimens was observed. The MW materials attain a

1 bulk density 99.4% theoretical density (t.d.) at 1300 °C, while the CS materials attain  
2 only 92.5% t.d. and PECS 98.7% t.d. Detailed microstructural evaluation indicated that  
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4 a low temperature densification leading to finer grain sizes (135 nm) could be achieved  
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6 by PECS followed by MW with an average sintered grain size of 188 nm and CS 225  
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8 nm. It is believed that the high heating rate and effective particle packing are  
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10 responsible for the improvements in these properties.  
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17 **Keywords:** A. Sintering; B. Grain size; B. Microstructure; D. ZrO<sub>2</sub>  
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## 22 **1. Introduction**

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27 Recently, much effort has been focused on the synthesis and densification of  
28 ceramic nanoparticles. The reason for the interest in nanocrystalline ceramics lies in  
29 their unique properties resulting from the small grain size, and the growing significance  
30 of grain boundaries in the nanocrystalline structure [1]. Due to the excellent properties,  
31 such as low thermal conductivity, excellent biocompatibility, high fracture toughness  
32 and strength, high crack resistance and low wear rates, the Yttria-stabilized Tetragonal  
33 Zirconia Polycrystalline (Y-TZP) ceramic materials, are widely used for many  
34 applications [2].  
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46 Therefore, a variety of approaches in the field of sintering have arisen due to the  
47 widespread demand of ceramics in recent decades. Hence, understanding how the  
48 processing variables affect microstructural evolution is the key to initiating a proper  
49 sintering procedure. Various sintering methodologies based on diverse mechanisms are  
50 currently available to engineer the densification kinetics enabling the realization of  
51 above cited objectives. Applying a promising sintering procedure is, therefore, of a  
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1 great importance for the superior performance of zirconia bodies. Conventional  
2 sintering techniques (hot pressing, sinter forging, hot isostatic pressing, etc.) and non-  
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4 conventional sintering techniques (**Pulsed electric current-assisted sintering** and  
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6 microwave) represent an alternative approach to the densification of nanoparticles. In  
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8 ceramic materials, the high temperatures required to fully densify ceramic powders  
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10 result in large grain sizes due to Ostwald ripening when traditional sintering techniques  
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12 are used. This makes it extremely difficult to obtain dense materials with nanometric  
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14 and submicrometric grain sizes [3]. To overcome the problem of grain growth, non-  
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16 conventional sintering methods has been proposed in this work.  
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21 **Pulsed electric current-assisted sintering** simultaneously applies pulsed electrical  
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23 current and pressure directly on the sample leading to densification at relatively lower  
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25 temperatures and short retention times [4-6]. As both the die and sample are directly  
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27 heated by the Joule effect extremely high heating rates are possible due to which non-  
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29 densifying mechanisms like surface diffusion can be surpassed. This technique is  
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31 widely explored for the development of nanostructured ceramics. The mechanisms  
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33 responsible for high rate densification were identified as grain rotation and sliding,  
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35 aided by partial melting of the particle surface or plastic deformation in materials with  
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37 low yield stress [7,8].  
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43 Microwave radiation for sintering of ceramic components has recently appeared  
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45 as a newly focused scientific approach [9-16]. Microwave sintering has several  
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47 advantages such as rapid end volumetric heating, improved production rate,  
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49 enhancement in densification and grain growth prohibition of ceramics [17-19]. This  
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51 technique generally uses a frequency of 2.45 GHz resulting in relatively rapid heating  
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53 rates with uniform grained microstructures and has been employed for the sintering of a  
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55 wide variety of ceramics ranging from dielectric materials to transparent ceramics.  
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1 Microwave heating of these material results from the absorption by molecular vibration  
2 (rotating electric dipole/dipole reorientation) and ionic conduction of a portion of the  
3 energy transported by an oscillating electric field [11]. A genuine “microwave effect”,  
4 i.e. the acceleration of diffusion mechanisms by the oscillating electric field, was also  
5 proposed by some authors to explain the enhancement of the sintering process  
6 [11,16,20,21].  
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14 The objective of the present study is therefore a comparative evaluation of the  
15 densification, microstructure development and mechanical properties in yttria-stabilized  
16 zirconia ceramics by the different sintering methodologies: conventional sintering (CS),  
17 microwave sintering (MW) and **pulsed electric current-assisted sintering (PECS)**.  
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## 26 **2. Experimental procedure**

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31 The raw material used in this study was commercial ZrO<sub>2</sub> (3Y-TZP-B)  
32 nanopowders (Tosoh Corp., Japan) with average particle size of (50-60) nm. The MW  
33 and CS specimens were prepared by uniaxial pressing at 200 MPa of pressure in a steel  
34 cylindrical die (2.5 mm thick, 10 mm  $\phi$ ). The green density was approximately 2.9 g  
35 cm<sup>-3</sup>, i.e. 49% of theoretical density (6.08 g cm<sup>-3</sup>). Before MW sintering, the binder of  
36 the nanopowders was burnt out under air in an electric furnace by heating at 5 °C min<sup>-1</sup>  
37 up to 600 °C and by soaking for 3 h. The weight loss and shrinkage were about 0.5%  
38 and 20%, respectively. This preliminary debinding stage is necessary, since we  
39 observed cracks development during microwave heating for other specimens. After, all  
40 samples were sintered by different methods at 1300 °C and 1400 °C of final  
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Zirconia exhibit low dielectric losses at room temperature ( $\sim 0.04$ ) and increases markedly to  $\sim 1000$  around  $1000\text{ }^{\circ}\text{C}$ . This combined with low thermal conductivity  $\sim 2\text{ W m}^{-1}\text{ K}^{-1}$  and high thermal expansion ( $\alpha=10^{-6}\text{ K}^{-1}$ ) suggest that thermal stresses resulting from non uniform and/or fast heating may cause warpage/cracking. Therefore, SiC crucible with a high dielectric loss must be used as a susceptor in heating by microwave. Green samples were sintered in an experimental microwave oven with  $800\text{ W}$  of power and  $2.45\text{ GHz}$  of frequency in microwave mono-mode rectangular cavity (Figure 1). This resonant cavity is coupled by an iris which dimensions are optimized for this application. The method to tune and detune the cavity consists of a sliding short circuit that can be moved electronically, depending on the reflected and consumed power and on the material temperature. The temperature was measured with an optical pyrometer (Optris GmbH, Germany) through a circular hole located on the top of the cavity.

**(Figure 1)**

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The microwave sintered samples were heated with a heating rate of  $30\text{ }^{\circ}\text{C min}^{-1}$  and a holding time of 10 minutes. Other non-conventional technique is **pulsed electric current-assisted sintering**, where the powder was placed into a graphite die with an inner diameter of  $20\text{ mm}$  and cold uniaxially pressed at  $30\text{ MPa}$ . Then, they were introduced in a pulsed electric-current pressure sintering HP D 25/1 (FCT Systeme GmbH, Germany) under low vacuum ( $10^{-1}\text{ mbar}$ ). The holding time was to  $1\text{ min}$  at the maximum temperature under an applied pressure of  $80\text{ MPa}$  and a heating rate of  $100\text{ }^{\circ}\text{C min}^{-1}$ . The conventional heating process was carried out in an electrical furnace (Thermolyne type 46100) with  $5\text{ }^{\circ}\text{C min}^{-1}$  heating rate and  $1\text{ h}$  of holding time.

1 The density was measured by the Archimedes method (ISO-3369). In order to  
2 investigate sample microstructure, polished sections (Struers, model RotoPol-31) with  
3 diamond to 1  $\mu\text{m}$  roughness, were thermally etched between 30 min in an electrical  
4 furnace under air 100 °C below their maximum sintering temperature to reveal their  
5 microstructure. These sections have been observed using a field emission scanning  
6 electron microscope (FE-SEM, S4100 HITACHI). The grain size of the sintered  
7 samples was determined by multiplying the average linear intercept by 1.56 [22]. For  
8 each specimen, at least 15 lines were taken, and their average was reported.  
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### 22 **3. Results and Discussion**

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27 Table 1 shows the sintering parameters, relative densities and average grain size  
28 of 3Y-TZP powders densified using the sintering methodologies of CS, MW and PECS.  
29 It can be observed, a meaningful difference between the relative densities of the  
30 conventionally sintered samples and those prepared by MW and PECS.  
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43 (Table 1)

44 At 1300 °C, the density of the MW sample was significantly higher than that of  
45 the CS and PECS samples. At this temperature if we compare the samples sintered by  
46 MW with 10 min of dwelling time and CS with 1 h of dwelling time, the MW sample  
47 has a density enhancement up to 7% (from 92.5% to 99.4%) in a shorter time.  
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53 On increasing the temperature to 1400 °C a significant improvement in  
54 densification is observed in the CS samples. On the other hand, the MW method shows  
55 full dense samples compared to the pressed compacts sintered by PECS at equivalent  
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1 temperatures. Therefore, maximum densification was provided by MW, wherein  
2 samples could be sintered to >99.9% at a temperature of 1400 °C for 10 minutes.  
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4 According to previous reports [16,19], microwave heating has been recognized as a  
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6 promising method to improve the densification in the same ceramic systems.  
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9 During microwave heating energy is transferred to the material electro-  
10 magnetically and not as a thermal heat flux enabling the material to be heated at rapid  
11 rates. The higher oxygen vacancies associated with 3 mol% yttria-stabilized zirconia  
12 provides higher ionic conductance at elevated temperatures leading to high dielectric  
13 losses and enhanced absorption of microwaves. This mechanism could be one possible  
14 reason for the shorter sintering times in MW.  
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24 The rapid densification of samples by PECS is attributed to the enhanced  
25 densification rate due to mechanisms such as particle rearrangement and the breaking up  
26 of agglomerates aided by applied pressure and faster heating rates. By rearrangement of  
27 particles, the PECS process also impedes the pore size increasing which was generally  
28 observed in the first and intermediate stages of sintering. Further, applied electric field  
29 also promotes the diffusion of ions and vacancies which enhances the sintering rate.  
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39 But this method has a big problem with the sintering of zirconia materials. As  
40 can be observed in Figure 2a, the sample sintered by PECS at 1300 °C shows a full  
41 black colour. This is due to carbon diffusion within the zirconia sample by PECS  
42 processing, which is linked to the carbon rich atmosphere in which it is performed. As  
43 the sintering of the compact is taking place in a graphite die, the carbon diffuses into the  
44 sample from the die and this process is promoted by the applied pressure. Eliminating  
45 this contamination is possible (Figure 2b), but this implies high temperatures (>800 °C)  
46 and a long time inside a furnace (>2 h), resulting in high economic costs.  
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Figure 3 represents the FE-SEM microstructure of 3Y-TZP samples sintered by PECS, MW and CS at 1400 °C. All the sintered specimens exhibited equiaxed grain microstructures and the average grain size varied over a wide range from 135 nm to 256 nm.

**(Figure 3)**

Nanocrystalline 3Y-TZP ceramics with average grain size of 225 nm and a complete elimination of residual porosity were obtained at 1400 °C for 10 min by MW. The CS samples revealed a slight grain growth with an average grain size of 256 nm, and the PECS of 245 nm. These microstructures show similar values of grain size, but the MW micrograph (Figure 3b) shows a better homogeneous microstructure than the PECS and CS ones. Therefore, application of a heating microwave method has provided traces of improvement for grain growth suppression and densification compared to the other sintering techniques employed.

**4. Conclusions**

The microstructural evolution of the nanometric 3Y-TZP powder subjected to different sintering techniques (MW, PECS and CS), has been carried out in the current investigation. Comparison with conventional sintering shows that microwave sintering has a number of benefits in terms of microstructural design. Zirconia powders sintered by the microwave technique at the temperature of 1400 °C shows a full density of



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99.9% at an average grain size of 225 nm with a more homogeneous microstructure compared to the specimen conventionally sintered at the same temperature.

## **Acknowledgements**

This work has been carried out with programme to support research and development of the Polytechnic University of Valencia (U.P.V) under multidisciplinary projects PAID-05-09 and PAID-05-10. A. Borrell, acknowledges the Spanish Ministry of Science and Innovation for her FPI Ph.D. grant and the people from Institute Technological of Materials (ITM) of the U.P.V for helping us with the microwave experiments during a stay in 2010-2011. Felipe L. Peñaranda-Foix wants to thank the Generalitat Valenciana for the grant obtained in the frame of the Program BEST/2010, because some results of this paper have been possible with the help of.

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**Figure Captions:**

Figure 1. Microwave system setup.

Figure 2. (a) 3Y-TZP sample sintered by PECS and (b) 3Y-TZP sample sintered by PECS after heating treatment.

Figure 3. FE-SEM micrographs of near full dense specimens sintered by PECS at 1400°C/1min (a), MW at 1400°C/10min (b), and CS at 1400°C/60min (c).

Figure 1  
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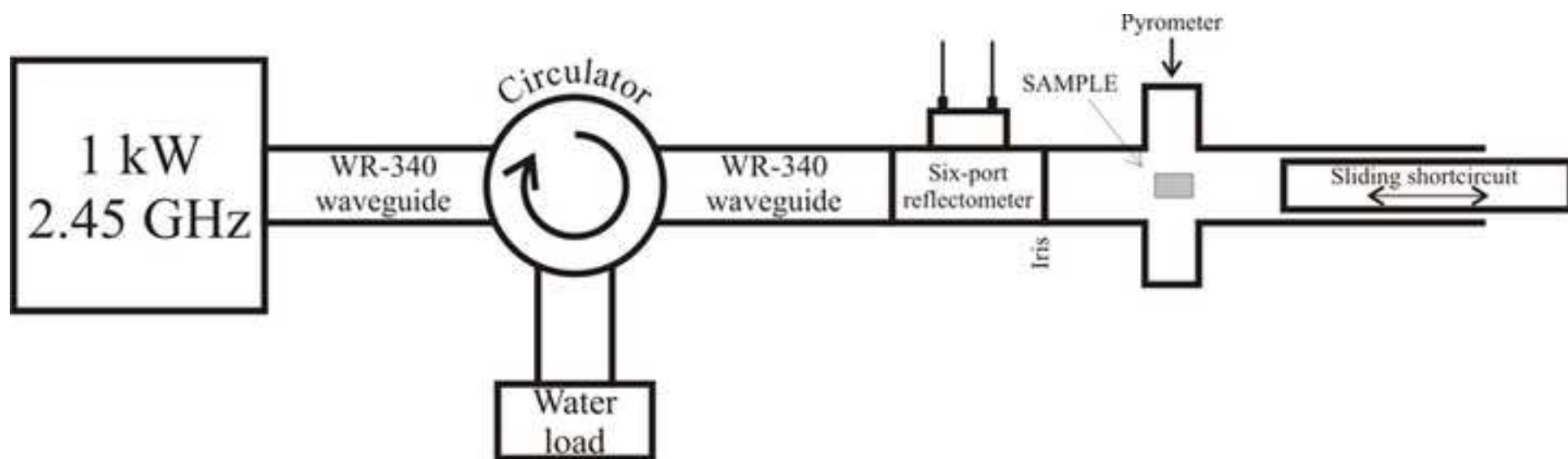
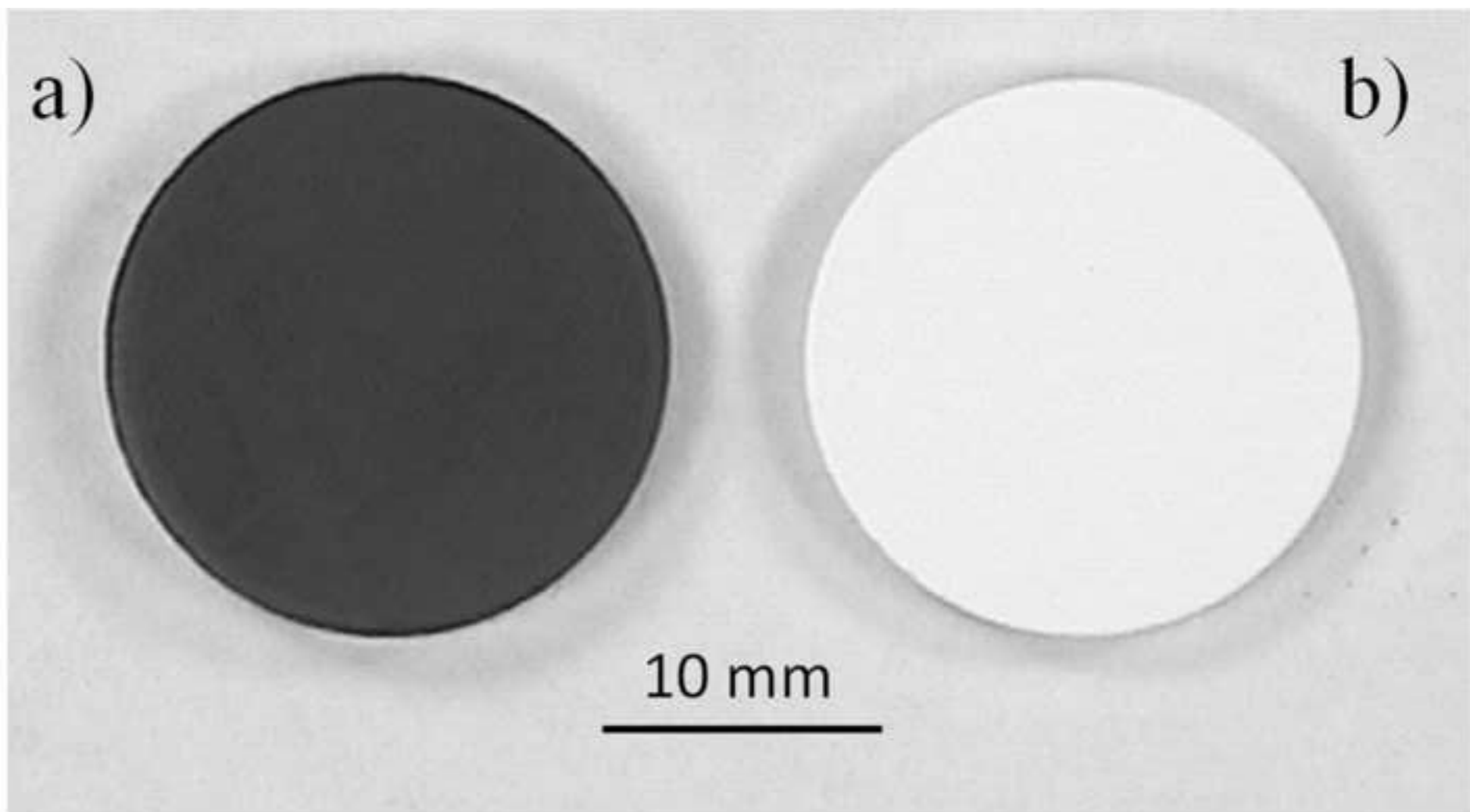
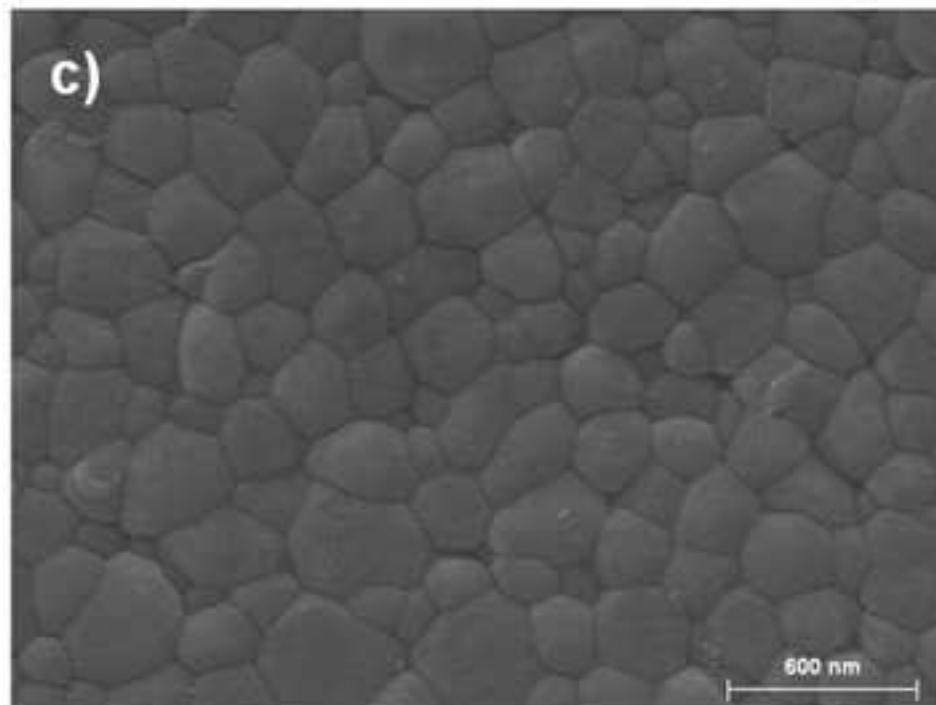
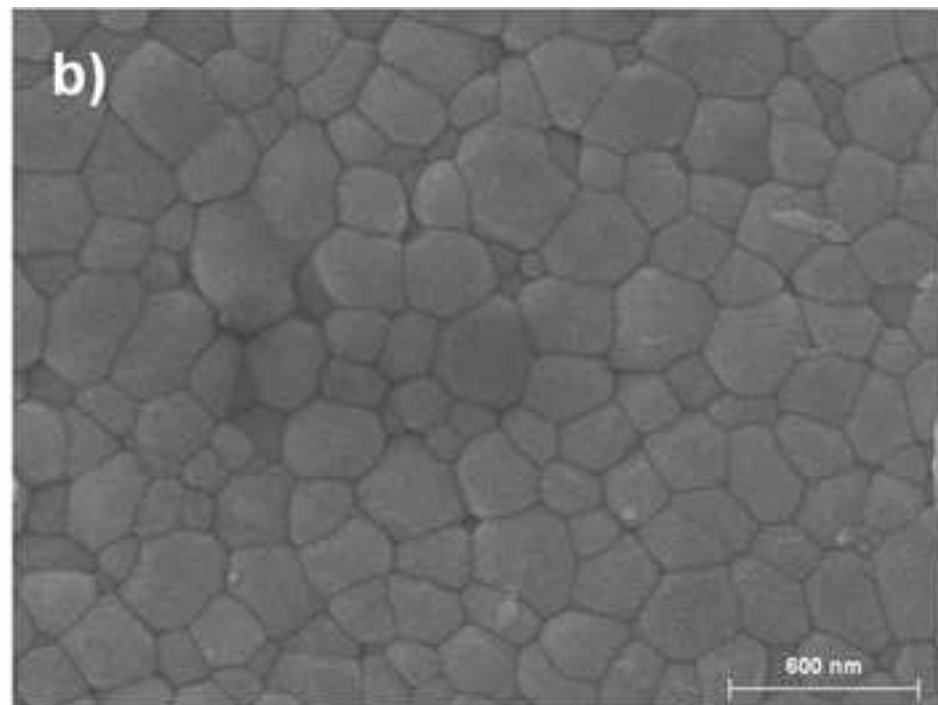
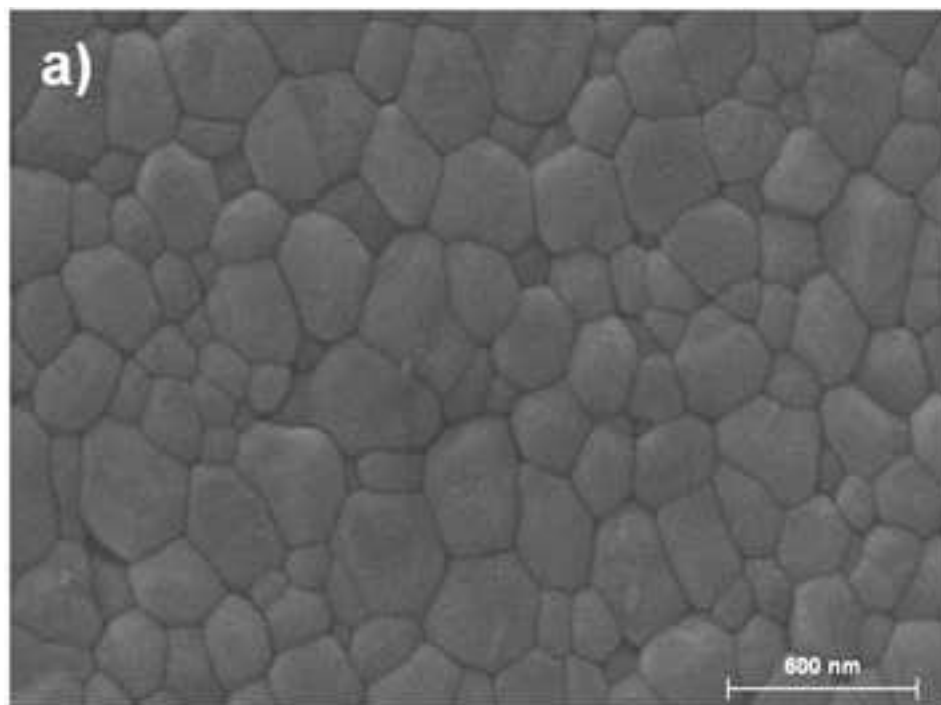


Figure 2  
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**Figure 3**  
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**Table 1**

Sintering technique	Final temperature (°C)	Dwell time (min)	Relative density (% t.d)	Average grain size (nm)
<b>CS</b>	1300	60	92.5 ± 0.5	165 ± 5
	1400	60	98.3 ± 0.5	256 ± 3
<b>MW</b>	1300	10	99.4 ± 0.5	188 ± 6
	1400	10	99.9 ± 0.5	225 ± 4
<b>PECS</b>	1300	1	98.7 ± 0.5	135 ± 6
	1400	1	99.0 ± 0.5	245 ± 5

Table 1. Sintering parameters, sintered densities and average grain size of the 3Y-TZP materials.