1	COMPARING PENMAN-MONTEITH AND PRIESTLEY-TAYLOR APPROACHES
2	AS REFERENCE-EVAPOTRANSPIRATION INPUTS FOR MODELLING MAIZE
3	WATER-USE UNDER MEDITERRANEAN CONDITIONS
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# 22 ABSTRACT

23 A comparison between experimental and simulated data, considering the Priestley 24 and Taylor (PT) and Penman-Monteith (PM) Reference-Evapotranspiration (ET<sub>0</sub>) approaches was carried out. Experimental data, obtained from an irrigation 25 assessment, conducted during the 1995 and 1996 maize growth-seasons at 26 27 Zaragoza, Spain, was compared to the mechanistic-model SWAP simulation-results, considering each of the ET<sub>0</sub> calculation approaches in the model input. Soil hydraulic 28 29 properties, meteorological data, seeding and harvest dates, crop water management and other experimental data were used as SWAP input. As corresponding to the 30 windy and dry conditions found in many Mediterranean landplanes, PT ET<sub>0</sub> values 31 32 were significantly lower than PM ET<sub>0</sub> calculations. Furthermore, simulated actual evapotranspirations considering the PT approach (PT-ET<sub>c</sub>) were lower than those 33 found in the simulations that consider the PM approach (PM-ET<sub>c</sub>). Correspondingly, 34 35 simulated drainage flux and soil water contents were higher when the PT  $ET_0$ approach was used. The correlation coefficients between simulated and measured 36 37 actual maize evapotranspirations and soil water contents were statistically significant, but the same for both ET<sub>0</sub> calculation approaches. Mean and median differences 38 between actual and simulated maize water-use were not statistically different from 39 40 zero for both considered  $ET_0$  calculation approaches. Experimental data variability was significantly higher than simulated variability. The comparisons among the 41 42 evaluated irrigation options, made with the experimental water-use data, lead almost 43 to the same conclusions than those achieved from the simulated maize water-use. Considering PM-ET<sub>c</sub> rather than PT-ET<sub>c</sub> yields no statistical difference in the 44 modeling-based conclusions. According to the obtained results, the PT approach 45 could be used under Mediterranean conditions for comparative assessments aimed 46 47 to support irrigation decision-making.

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50 Keywords: crop water-use modeling, reference evapotranspiration calculation,

51 Mediterranean conditions, maize irrigation.

#### 52 INTRODUCTION

53 Maize is one of the most important crops in the Mediterranean landplanes of 54 Europe. Very cost-effective yields are frequently obtained, due to high radiation rates 55 in the summer, combined with modern management techniques. Since the Mediterranean climate is very dry in the summer, irrigation is an absolute need for 56 obtaining reliable yields. Water availability is a serious limitation for maize production 57 in these zones and hence the focus has been set in optimizing the yield-water 58 59 relationships, usually through the experimental evaluations of several irrigation options. However, the results of these experiments are constrained to the particular 60 climate conditions and to the zone where the experiments were carried out. 61

62 Crop modelling has successfully been used since the last decade as a 63 powerful tool for irrigation and agricultural decision-making (Hoogenboom, 2000). In general, models estimate a daily soil water-balance in order to evaluate the possible 64 65 crop-growth reduction from its optimal value, due to plant-water deficits (Leenhardt et al., 1995; Ritchie, 1998). The optimum daily growth is generally settled by the 66 evaporation demand of the atmosphere, under the assumption that water and 67 nutrients are adequately provided. Therefore, the reference evapotranspiration  $(ET_0)$ 68 69 is normally needed as model input.

Many approaches have been developed for  $ET_0$  estimations. Among all of them, the physically based Penman-Monteith (PM) approach is presently considered as the state-of-the art in such calculations (Allen et al., 1998; Smith, 2000). According to Allen et al. (1998), the Penman-Monteith reference evapotranspiration can be calculated from:

$$\lambda ET = \frac{\Delta(Rn - G)}{\Delta + \gamma \left(1 + \frac{r_s}{r_a}\right)} + \frac{\rho_a c_p \frac{(e_s - e_a)}{r_a}}{\Delta + \gamma \left(1 + \frac{r_s}{r_a}\right)}$$
[1.]

where  $\lambda$  is the latent heat of vaporization of water,  $R_n$  is the net radiation, G is the soil heat flux, ( $e_s - e_a$ ) is the vapour saturation deficit,  $\rho_a$  is the mean air density at constant pressure,  $c_p$  is the specific heat of the air,  $\Delta$  represents the slope of the

saturation vapour pressure temperature relationship,  $\gamma$  is the psychometric constant,

and  $r_s$  and  $r_a$  are the (bulk) surface and aerodynamic resistances, respectively.

The practical derivation of equation [1] for a hypothetical grass reference crop 80 requires the values of the following meteorological variables: wind speed at 2 m, 81 82 maximum and minimum air temperatures, net solar radiation and the actual vapour pressure (Allen et al., 1998). These two last meteorological variables can be 83 84 estimated from actual duration of bright sunshine and relative humidity, respectively 85 (Allen et al., 1998). The first term in equation [1] has been called the "radiation" term, whereas the second term, called "aerodynamic", depends directly on vapour deficit 86 87 (Allen et al., 1998; Mc Aneney and Itier, 1996; Van Dam et al., 1997).

Despite the sounder theoretical background of the combined PM approach, many crop models use empirical approaches to calculate the reference evapotranspiration, due to the frequent unavailability of the meteorological variables needed for PM calculations. Priestley and Taylor, (1972) proposed an empirical equation for calculating the reference evapotranspiration, which can be written as:

$$\lambda ET = \alpha \left[ \frac{\Delta(Rn - G)}{\Delta + \gamma} \right]$$
[2.]

93 where  $\alpha$  is an empirical constant with an average value of 1.26 (Priestley and Taylor, 1972; Mc Aneney and Itier, 1996). As can be seen from equation [2], the Priestley 94 and Taylor (PT) approach neglects the influence of vapour deficit on the reference 95 evapotranspiration, relying on the assumption that ET<sub>0</sub> depends only on solar 96 97 radiation and temperature. The PT data requirement does not include some hardly 98 available meteorological variables as wind speed or relative humidity. Hence this reference evapotranspiration can be computed in places where PM calculations can 99 100 not be performed due to data lacking.

Since wind speed and actual water vapour pressure are connected to the air temperature also, PT results, although empirically, could be statistically equivalent to PM values by considering a proportionality between evapotranspiration and the available energy. The  $ET_0$  values calculated from the PT approach have been found to be highly correlated to PM calculations (Jamieson, 1982; Pereira and Nova, 1992).

106 However, despite the success of the PT method, this approach could fail in 107 mimicking PM values under dry conditions or in zones where wind speed is relatively 108 high (Shouse et al., 1980; Jensen et al., 1990; McAneney and Itier, 1996). The Mediterranean landplane is one of these places where PT could underestimate the 109 110 evapotranspiration rates, compared to PM approach, due to the dryer and windy conditions usually found there. This has been already shown by Martínez-Cob (2002) 111 112 in a study conducted for Ebro Valley, northern Spain. Martínez-Cob (2002) compared 113 several methods against FAO 56 Penman-Monteith at three different locations 114 (Zaragoza, Ejea and Tamarite) and two time scales, daily and monthly. The PT 115 method clearly underestimated PM  $ET_0$  at the relatively windy locations of Zaragoza 116 and Ejea, while there was not underestimation or overestimation on average at the 117 non-windy location of Tamarite.

Previous sensitivity analysis have shown that the use of PT ET<sub>0</sub> as the model 118 119 input, rather than the PM method, could lead to notable differences in crop model results, particularly in those cases where PM is significantly underestimated by PT 120 121 (Dugas and Ainsworth, 1985; Benson et al., 1992). Nevertheless, actual data 122 variability is usually higher than simulated results and many uncontrolled factors can 123 lead to smaller differences between actual and simulated data than those predicted 124 by the theoretical sensitivity analyses. Hence, the correspondence between model 125 outputs and actual data could remain even after model-input changes (Clemente et al., 1994; Utset et al., 2000), although those changes should lead to significant 126 127 differences, according to the sensitivity analyses. Present paper goal is to assess the 128 differences between actual and simulated maize water-use in a Mediterranean landplane, considering the PT and the PM approaches as the reference 129 130 evapotranspiration inputs in the model simulations. The reliability of a modeling-131 based irrigation decision-making, considering both ET<sub>0</sub> calculation approaches, is 132 also evaluated.

# 133 MATERIALS AND METHODS

The data used in this study were obtained from experiments conducted in Zaragoza (41° 43' N, 0° 48' W, 225 m altitude), Aragón, Northern Spain, during the 136 1995 and 1996 maize cropping-seasons. The experiment goal was to assess the

differences among the evaluated irrigation options, according to the maize actualwater-use (Farré, 1998).

139 The climate in the experimental site was Mediterranean semiarid. Mean 140 annual evapotranspiration is 1150 mm, whereas mean annual precipitation is 350 mm. It yields a precipitation-evapotranspiration ratio of about 0.3, which corresponds 141 142 to a semiarid climate (FAO, 1977). However, this ratio is close to the arid climate cut-143 off ratio of 0.2 (FAO, 1977). The mean annual maximum and minimum daily air 144 temperatures are 21 and 8 °C, respectively, and the annual average wind speed at 2 m height is 2.4 m.s<sup>-1</sup> (Faci et al., 1994). An automatic meteorological station, located 145 146 about 2 km from the experimental site, but within the same experimental farm, recorded half-hour and daily values of precipitation, air temperature and relative 147 humidity, wind speed and incoming global solar radiation (Martínez-Cob, 2001). 148

149 Maize cv. Prisma (FAO 700) was planted on 17 May 1995 and 16 May 1996 Details of the original irrigation experiments were provided by Farré (1998) and 150 Cavero et al. (2000). Nine irrigation treatments were evaluated each year. Irrigation 151 152 was supplied either to meet the estimated maximum evapotranspiration of the crop ("fully irrigated" treatment, FI) or about one third of this amount ("deficit irrigation" 153 154 treatment, DI), by skipping some of the irrigation events or applying a lower depth. 155 Between the extreme FI and DI treatments, six different combinations were 156 evaluated, providing from 5 to 7 irrigation supplies at different stages of the maize 157 development. An additional treatment ("half fully irrigated" treatment, HFI), consisting 158 of half of the water used in the FI treatment, was included. Consequently, considering 159 both years, a total number of 18 maize water-management options were evaluated 160 (Table 1). Soil water-content measurements were taken with a neutron probe, 161 approximately every week and for every 0.2 m layer till 1.2 m soil-depth (Cavero et al., 2000). Seasonal crop evapotranspiration (ET<sub>c</sub>) in each treatment was estimated 162 through water balance. Soil water content was also determined gravimetrically each 163 0.2 m (1995) or 0.3 m (1996) layer down to a depth of 1.2 m at two occasions during 164 each-year crop season (Farré, 1998; Cavero et al., 2000). 165

166 The mechanistic model SWAP (Van Dam et al., 1997) was used in this study. 167 SWAP follows the same approach than WOFOST, SUCROS, ORYZA and other

Wageningen models for crop-growth simulations (Van Ittersum et al., 2003), but it is particularly addressed to simulate soil-water movement and crop water-use (Van Dam et al., 1997). The Richards equation is solved in SWAP by a numerical scheme (Belmans, 1983), including several practical options for the initial and boundary conditions. Partitioning of evapotranspiration rate into transpiration and evaporation rates is based on crop leaf-area index (Ritchie, 1972; Belmans, 1983).

174 The actual crop daily evapotranspiration rates are calculated in SWAP by 175 reducing the potential crop evapotranspiration rate  $(ET_c)$ , according to the simulated 176 root water-uptake and to the maximum soil evaporation flux, which depend on the 177 simulated soil water-contents (Van Dam et al., 1997). SWAP uses the Feddes et al. (1978) root water-uptake function, which has been found suitable for simulating a 178 179 wide rank of soil-water contents (Leenhardt et al., 1995; Utset et al., 2000). Rainfall interception and soil-evaporation restrictions are also considered in SWAP 180 181 simulations (Van Dam et al., 1997). Since SWAP follows a physically-based approach, it can account for all the soil water-balance components, including 182 183 capillary rising (Van Dam et al., 1997). Hence, SWAP water-use and soil water-184 content simulations can be more sensitive to changes in the reference 185 evapotranspiration inputs, than those models that simulate soil-water movement 186 through the "cascade approach" (Ritchie, 1998), or similar simplifications.

187 The soil hydraulic properties, required in SWAP inputs, were estimated from 188 the pedotransfer functions proposed by Rawls et al. (1982, 1998). Physical soil data 189 needed for these estimations, i.e. mechanical composition, soil density, and soil 190 organic matter content, were obtained from published data (Farré, 1998; Cavero et 191 al., 2000). Free drainage at the bottom of the 2-m simulated soil layer was 192 considered as the bottom boundary condition, taking into account the soil 193 characteristics of the experimental site (Farré, 1998; Cavero et al., 2000). The gravimetrically-measured soil water contents at each seeding date (Farré, 1998), 194 were considered as the initial conditions for the SWAP simulations. The provided 195 irrigations shown in Table 1, were considered in SWAP simulations as water 196 197 supplies. The maize crop function included in SWAP (Van Dam et al., 1997) was used for the crop water-uptake calculations. 198

Daily values of PM and PT reference evapotranspiration were computed through equations [1] and [2], following the parameterization recommended by Allen et al. (1998) and Priestley and Taylor (1972), using the meteorological data recorded at the weather station, i.e. maximum and minimum daily temperatures and solar radiation for PT calculations, as well as relative humidity and wind speed at 2 m height for PM estimates. These  $ET_0$  values were considered as the SWAP top boundary conditions for each simulated day.

206 SWAP simulations were conducted for all nine irrigation scenarios for both 207 1995 and 1996 years, using either the PM or the PT method for  $ET_0$  estimations. 208 Paired comparison tests for mean, median and variance were performed between actual ET<sub>c</sub>, as measured by the water-balance method and the simulated ET<sub>c</sub> 209 considering both the PT and PM approaches for ET<sub>0</sub> calculations. Same test 210 211 comparison was performed between gravimetrically-measured and simulated SWC 212 considering both ET<sub>0</sub> approaches. Analysis of regression between actual and 213 simulated ET<sub>c</sub> and SWC were included.

## 214 **RESULTS AND DISCUSSION**

215 The annual precipitation recorded in the experimental site, was 188 mm in 216 1995 and 468 mm in 1996. The precipitation distributions for both crop-seasons (from 217 May to October 1995 and 1996, respectively) are depicted in Fig. 1. The daily means 218 of several other meteorological variables during each crop season were: a) total global solar radiation, 20.4 MJ m<sup>-2</sup> (1995) and 20.9 MJ m<sup>-2</sup> (1996); b) wind speeds, 219 2.0 m s<sup>-1</sup> (1995) and 2.2 m s<sup>-1</sup> (1996); c) (¿no será más bien, humedad relativa 220 221 media?) minimum relative humidity, 65 % (1995) and 68 % (1996). The recorded 222 rainfall in the 1995 maize crop-season was 76 mm, 49% of the historical rainfall mean in those months. However, the precipitation during the 1996 maize crop 223 224 season was 232 mm, which means 149% of the historical rainfall in Zaragoza from 225 May to October (155 mm). According to these meteorological mean values, the 1995 226 crop season was dry, whereas that corresponding to 1996 was a wet crop-season. 227 There is a considerable inter-annual variability in rainfall behavior, comparing 1995 and 1996. Farré (1998) found statistical significant differences in maize grain yield 228 229 between the two years, particularly for those irrigation management options

comprising lesser water supplies. The differences were considered to be due to the
different rainfall distributions. Nevertheless, despite the different rainfall behavior in
1995 and 1996, radiation and wind speed records were similar in both years and
corresponded to the typical climate behavior.

234 The calculated daily PT and PM ET<sub>0</sub> estimates for both years, 1995 and 1996, 235 are shown in Figure 2. The mean of all PM ET<sub>0</sub> estimates was 2.9 mm day<sup>-1</sup>; whereas that of PT ET<sub>0</sub> estimates was 2.8 mm day<sup>-1</sup>. Furthermore, in some 236 237 instances, the PM values were much higher than the PT ones (Figure 2). Despite the similarity between the two means, the PM and PT ET<sub>0</sub> estimates were significantly 238 239 different ( $\alpha$  = 0.95), according to three conducted paired-comparison tests: t-Student's test of means, sign test of medians and signed rank test of medians. These 240 results agree with those of Martinez Cob (2002) for the same site. 241

### 242 Simulated data analysis

The simulated water-balance results for each crop season and each of the irrigation-management options are shown in Table 2. The shown results comprise the simulated drainage flux at the bottom of the 2-m layer, the simulated crop transpiration and soil evaporation and the simulated total actual evapotranspiration. Simulations indicated no runoff, as it was usually found (Farré, 1998).

248 As can be seen in Table 2, the average simulated maize evapotranspiration 249  $(ET_c)$ , considering PT calculations as  $ET_0$ , was 11.7 mm (1995) and 3.9 mm (1996) less than the corresponding ET<sub>c</sub> values considering PM calculations as ET<sub>0</sub> in the 250 model input. As expected, the ET differences considering both ET<sub>0</sub> approaches were 251 252 due mainly to the simulated crop transpiration. The average simulated soil evaporation in the 1995 crop season, considering PM calculations, was only 3 mm 253 254 higher than that obtained considering PT calculations. Furthermore, the average 255 simulated soil evaporation in 1996, considering the PT approach, was higher than that considering the PM approach. 256

The differences in the simulated crop  $ET_c$ , considering both  $ET_0$  calculation approaches, depended on the irrigation-management option. The highest difference between the simulated  $ET_c$  using both  $ET_0$  calculation approaches corresponded to the FI option in 1995 (more than 20 mm). The lowest difference corresponded to the

DI option in 1996. Again, those differences in the predicted ET<sub>c</sub> were due to the simulated crop transpiration rather than to the simulated soil evaporation. Besides, the simulated crop transpiration, considering the PM approach, showed higher variability among the irrigation management options than that found by considering the PT approach. This was particularly evident in 1995, the relative dry year, when irrigation was more important for water availability.

267 The average estimated drainage at the bottom of the 2-m depth soil layer was 268 higher in both years (0.9 mm higher in 1995 and 1 mm higher in 1996) for those simulations that consider the PT calculations as ET<sub>0</sub> than for those which consider 269 PM calculations. Moreover, the estimated bottom fluxes in both years, corresponding 270 to those simulations that consider PT as ET<sub>0</sub> input and the FI irrigation option were 271 1.9 mm higher than those simulations that consider the PM approach. The same 272 273 bottom flux differences, but considering the DI irrigation option, were 0.1 and 0.3 mm 274 in 1995 and 1996, respectively.

275 Since PT values underestimated ET<sub>0</sub> as compared to PM calculations, the 276 simulated water balance predicted higher drainage rates when the PT approach was used for ET<sub>0</sub> calculations. This is particularly evident for the cases of higher water 277 278 income from rainfall or irrigation. Likewise, total ET<sub>c</sub> in both simulations, considering 279 PT and PM, was higher in 1996 than in 1995. As was pointed out above, 1996 was a 280 wet year. Accordingly, the predicted drainage flux and soil evaporation in 1996 were higher than those predicted for the 1995 crop season, for both ET<sub>0</sub> calculation 281 282 approaches. Although the average crop transpiration corresponding to the PT 283 calculations was higher in 1996 than in 1995, the corresponding crop transpirations 284 considering the PM approach were almost equivalent.

#### 285 Comparison between simulated and actual data

Table 3 shows the mean and median differences and variance ratio between the measured maize actual-evapotranspiration (A-ET<sub>c</sub>) and those simulated actual evapotranspirations considering the PM (PM-ET<sub>c</sub>) and the PT (PT-ET<sub>c</sub>) approaches for ET<sub>0</sub> calculations. Kolmogorov Goodness-of-fit tests for normality, performed for A-ET<sub>c</sub>, PM-ET<sub>c</sub>, PT-ET<sub>c</sub>, as well as for actual and simulated SWC yield that all these variables can be considered normally distributed at the 95% confidence level.

292 According to a t-student test, the A-ET<sub>c</sub> mean was not statistically different at the 293 95% confidence level from the PM-ET<sub>c</sub> and PT-ET<sub>c</sub> means, respectively. The same 294 conclusion was obtained from a signed-rank comparison of medians. Nevertheless, 295 the A-ET<sub>c</sub> variances were significantly higher than the simulated actual-296 evapotranspiration variances, considering both  $ET_0$  calculation approaches. Despite that PM-ET<sub>c</sub> variability was closer to A-ET<sub>c</sub> variability than PT-ET<sub>c</sub>, both simulated-297 298 ET<sub>c</sub> variances were statistically different from A-ET<sub>c</sub>. As pointed out above, 299 experimental data usually involves more variability than simulations, because many 300 uncontrolled factors can be found during experiments and measurements. Hence, from a statistical point of view, PM-ET<sub>c</sub> and PT-ET<sub>c</sub> showed a similar behavior 301 302 regarding their average differences with A-ET<sub>c</sub>, due to A-ET<sub>c</sub> variability.

303 Figure 3 depicts the scatter plots and regressions between PM-ET<sub>c</sub> and A-ET<sub>c</sub>, as well as between PT-ET<sub>c</sub> and A-ET<sub>c</sub>. The regression statistical results are shown in 304 305 Table 4. The correlation coefficients between measured and simulated actual maize evapotranspiration were 0.96 for both considered ET<sub>0</sub> calculation approaches, 306 307 significant at the 95% confidence level. Furthermore, the PM-ET<sub>c</sub> - A-ET<sub>c</sub> regression 308 intercept was higher than that obtained for the PT-ET<sub>c</sub> - A-ET<sub>c</sub> regression. The slope 309 corresponding to the PM-ET<sub>c</sub> - A-ET<sub>c</sub> regression was also higher than that obtained 310 for the PT-ET<sub>c</sub> - A-ET<sub>c</sub> regression. The regression lines shown in Fig. 3 were almost 311 parallel, indicating that PM-ET<sub>c</sub> was higher than PT-ET<sub>c</sub> for the whole rank of actual 312 evapotranspirations considered.

313 On the other hand, as can be seen in Table 3, mean and medians of simulated 314 SWC as obtained from both  $ET_0$  calculation approaches were statistically different 315 from the corresponding measured SWC. Particularly, experimental SWC variability 316 was much higher than the found variability through both simulations. Figure 4 depicts the regression between simulated and measured soil water contents. Accordingly, 317 Table 4 shows the regression statistical results. The correlation coefficients obtained 318 from both ET<sub>0</sub> calculation approaches were the same (0.72) and both of them were 319 significant at the 95% confidence level. The regression corresponding to those SWC 320 321 estimated from considering PM as  $ET_0$  (SWC-PM) showed a higher slope and a lower intercept than the regression obtained from those simulations where PT was 322 323 considered as ET<sub>0</sub> (SWC-PT). Differences between SWC-PM and SWC-PT were

324 higher for lower SWC and hence the regression lines diverged as approaching to the 325 ordinate axis. The estimated maize transpiration considering the PT approach were 326 lower than those obtained considering the PM approach, hence SWC-PM were lower 327 than SWC-PT, because the estimated root water-uptake was higher in those cases. 328 This difference, however, was not observed for higher SWC because in these cases, 329 close to soil-water saturation, an important amount of water will drain. As pointed out 330 above, the obtained simulations considering PT for ET<sub>0</sub> calculations predicted higher 331 bottom flux rates than those obtained considering the PM approach. The maximum 332 amount of water retained in the soil pores depend only on the soil hydraulic 333 properties (Van Dam et al., 1997), thus both SWC-PM and SWC-PT simulations 334 agreed predicting the higher SWC.

335 The goal of the Farré (1998) experiment was to assess the differences 336 between each of the evaluated irrigation options. Therefore, the modeling practical 337 use in this case should be just the same, to point out the statistical significant 338 differences between those irrigation managements. Consequently, Table 5 shows the 339 differences between each of the evaluated irrigation options, according to the actual 340 evapotranspirations measured through the water balance method (A-ET<sub>c</sub>) and those simulated actual evapotranspirations, as obtained from both ET<sub>0</sub> calculation 341 342 approaches (PM-ET<sub>c</sub> and PT-ET<sub>c</sub>). The Fisher's least significant difference procedure 343 (LSD) was used to indicate the significant differences at the 95% confidence level. The both-years data was considered and only differences respecting to the DI, FI and 344 345 HFI irrigation options are shown.

346 According to the experimental data comparison, the maize water-use 347 corresponding to the FI option was equivalent to that obtained by applying the EO1 348 and EO2 irrigation supplies. The same conclusion can be achieved from the simulation results, considering both  $ET_0$  calculation approaches. Besides, simulations 349 and measured data indicated that the HFI option yielded different maize water uses 350 than the EO2 and the DI options. However, A-ET<sub>c</sub> mean for the EO1 option was not 351 different from the HFI option, whereas the corresponding PM-ET<sub>c</sub> and PT-ET<sub>c</sub> means 352 353 were statistically different. An identical situation was found for the DI-EO5 comparison, although in the rest of the DI option comparisons the results obtained 354 355 from measured and simulated actual-evapotranspirations agreed. The differences

356 between means according to A-ET<sub>c</sub> values were higher than those differences computed from the simulated data. The simulated ET<sub>c</sub> differences according to the 357 358 evaluated irrigation option, successfully agreed with the experimentally-measured  $ET_{c}$  differences in 19 cases of the 21 shown in Table 5 (90.5%). The  $ET_{c}$  differences 359 360 estimated from PM-ET<sub>c</sub> were closer to A-ET<sub>c</sub> differences than those estimated from 361 PT-ET<sub>c</sub>. However, from a statistical point of view, the simulations obtained from both 362  $ET_0$  calculation approaches gave rise to the same conclusions, while comparing the effects of each irrigation option on maize water-use. 363

## 364 CONCLUSIONS

365 Considering the PT approach as the reference-evapotranspiration input in a 366 crop model under Mediterranean conditions, lead to lesser simulated actual 367 transpiration and evapotranspiration values than those obtained considering the PM 368 approach. Correspondingly, the simulated drainage flux and soil water contents were 369 higher considering the empirical PT approach as the model  $ET_0$  input, than those 370 found considering the combined PM approach. The correlations between simulated 371 and actual data were significant in all the cases, but no disagreements were found 372 according to the ET<sub>0</sub> approach followed in simulations. Differences between actual 373 and simulated maize water-use and SWC keep the same statistical significance for 374 both  $ET_0$  approaches. Besides, simulations obtained considering both  $ET_0$  calculation 375 approaches gave the same successful conclusions, when using the model as a tool for irrigation decision-making support. Hence, despite that the PT approach 376 377 significantly underestimates the PM physically-based values under Mediterranean 378 conditions; this empirical approach still could be used for modeling-based comparative assessments, if meteorological information is not enough for computing 379 380 the PM ET<sub>0</sub>.

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# 457 **ACKNOWLEDGMENTS**

458 Special thanks are due to Miguel Izquierdo, Jesús Gaudó, Lola Naval and 459 Teresa Molina for the field work.

460

IWS (mm)											
1995	F	hase l	(b)	Ρ	hase I	(c)	P	hase I	<sup>(d)</sup>	Total IWS	NI
DAS	28	40	51	62	72	84	97	111	125		
FI	79.3	65.2	60.7	60.2	65.0	65.0	60.0	57.4	55.6	568.4	9
EO1	79.3	65.2	60.7	60.2			60.0	57.4	55.6	438.4	7
EO2	79.3	65.2	60.7		52.0		60.0	57.4	55.6	430.2	7
EO3		65.2		60.2	65.0	65.0	60.0	57.4	55.6	428.4	7
EO4	79.3	65.2	60.7		52.0			57.4		314.6	5
EO5		65.2			52.0		60.0	57.4	55.6	290.2	5
EO6		65.2		60.2	65.0	65.0		57.4		312.8	5
DI		65.2			52.0			57.4		174.6	3
HFI	79.3		60.7		65.0		60.0		55.6	320.6	5
1996		Phase	I	ļ	Phase			Phase		Total IWS	NI
DAS	22	43	55	67	81		92	106	120		
FI	63.3	58.4	69.7	70.7	66.0		55.2	59.7	62.4	505.3	8
EO1	63.3	58.4	69.7	70.7	66.0			59.7		387.8	6
EO2	63.3	58.4	69.7		32.0		55.2	59.7	62.4	400.6	7
EO3		58.4		70.7	66.0		55.2	59.7	62.4	372.2	6
EO4	63.3	58.4	69.7		32.0			59.7		283.1	5
EO5		58.4			32.0		55.2	59.7	62.4	267.5	5
EO6		58.4		70.7	66.0			59.7		254.7	4
DI		58.4			32.0			59.7		150.0	3
HFI	63.3		69.7		66.0			59.7		258.7	4

503 Table 1. Irrigation water supply at each irrigation event, maize phase and irrigation option<sup>(a)</sup>. DAS, days after seeding. NI, number of irrigations. 504

509 (d) Grain filling phase (from 90 to 150 days after seeding)

<sup>505</sup> (a) FI, fully irrigated; HFI, half fully irrigated; DI, deficit irrigated; EO1..EO6, 506 evaluated options between FI and DI.

<sup>(</sup>b) Vegetative phase (first 60 days after seeding) 507

<sup>(</sup>c) Flowering phase (from 60 to 90 days after seeding) 508

Table 2. Simulated drainage bottom-flux (BF), crop transpiration (CT), soil evaporation (SE) and actual evapotranspiration (ET) for each irrigationmanagement option (IMO) and crop season using the SWAP model with two different  $ET_0$  approaches, Penman-Monteith (PM) and Priestley-Taylor (PT).

Year	$ET_0$	IMO	BF (mm)	CT (mm)	SE (mm)	ET (mm)
		FI	42.2	350.7	244.1	594.8
		HFI	22.4	272.9	231.9	504.8
	PM	DI	19.3	179.3	204.5	383.8
		EO1	27.7	327.3	244.1	571.4
		EO3	24.1	328.7	210.4	539.1
		EO4	26.0	270.4	239.6	510.0
		EO5	19.4	248.5	209.0	457.5
		EO6	22.1	295.2	205.9	501.1
1005		Average	25.4	284.1	223.7	507.8
1995		FI	44.1	333.3	241.0	574.3
		HFI	22.6	267.9	228.5	496.4
		DI	19.4	178.7	201.9	380.6
		EO1	28.2	314.0	241.0	555.0
	PT	EO3	24.9	313.3	207.7	521.0
		EO4	26.2	267.7	236.5	504.2
		EO5	19.5	238.9	206.4	445.3
		EO6	22.4	288.8	203.2	492.0
		Average	25.9	275.3	220.8	496.1
		FI	47.6	337.5	251.8	589.3
		HFI	25.4	290.3	232.0	522.3
		DI	20.8	215.2	216.7	431.9
		EO1	37.3	333.0	250.1	583.1
	РM	EO2	31.0	329.8	251.8	581.6
		EO3	28.5	321.4	218.6	540.0
		EO4	27.8	294.0	250.1	544.1
		EO5	21.9	280.7	218.5	499.2
		EO6	22.6	275.3	222.4	497.7
1996		Average	29.2	297.5	234.7	532.1
1000		FI	49.5	330.1	254.8	584.9
		HFI	26.2	285.1	235.0	520.1
		DI	21.2	212.0	218.5	430.5
	PT	EO1	38.9	327.1	253.1	580.2
		EO2	32.1	321.4	254.8	576.2
		EO3	29.3	312.7	220.2	532.9
		EO4	28.7	289.3	253.1	542.4
		EO5	22.4	271.1	220.2	491.3
		EO6	23.3	270.8	224.2	495.0
		Average	30.2	291.1	237.1	528.2

Table 3. Mean (MD) and median (MND) differences and variance ratio (VR) between
 the experimentally-obtained maize actual-evapotranspiration (ET<sub>c</sub>) and soil water
 contents (SWC) and those simulated actual evapotranspirations considering the
 PM and the PT approaches for ET<sub>0</sub> calculations.

 Voor	Statiation	Experimental DM	Experimental DT
rear	Statistics	Experimental-PM	Experimental-P1
	MD	0.6	7.0
ETc	MN	10.4	0.2
	VR	3.01*	3.12*
	MD	0.06*	0.06*
SWC	MN	0.07*	0.07*
	VR	5.30 <sup>*</sup>	5.18 <sup>*</sup>

520 \* Statistically significant at the 95% confidence level.

Table 4. Correlation coefficients (CC), intercepts (INT) and slopes (SLP) of the
 regression analyses between simulated and measured actual evapotranspiration
 (ET) and soil water contents (SWC); for each of the evaluated ET<sub>0</sub> calculation
 approaches.

	ET <sub>0</sub> approach	CC	INT	SLP
FT (mm)	PM	0.96 <sup>1</sup>	235.7 <sup>2</sup>	0.548 <sup>3</sup>
	PT	0.96 <sup>1</sup>	231.6 <sup>2</sup>	0.541 <sup>3</sup>
SWC (cm <sup>3</sup> cm <sup>-3</sup> )	PM	0.72 <sup>1</sup>	0.522 <sup>2</sup>	0.036 <sup>3</sup>
	PT	0.72 <sup>1</sup>	0.540 <sup>2</sup>	0.034 <sup>3</sup>

Statistically significant at the 95% confidence level.
 Statistically different from 0 at the 95% confidence level.

3. Statistically different from 1 at the 95% confidence level.

Table 5. Differences between each of the evaluated irrigation management options (IMO) according to the measured actual evapotranspirations (A-ET<sub>c</sub>) and the simulated actual evapotranspirations, considering the PM (PM-ET<sub>c</sub>) and the PT (PT-ET<sub>c</sub>) ET<sub>0</sub> calculation approaches.

IMO	A-ET <sub>c</sub>	PM-ET <sub>c</sub>	PT-ET <sub>c</sub>
EO1 - FI	-68.8	-14.8	-12.0
EO2 - FI	-27.3	-10.5	-3.4
EO3 - FI	*-135.0	*-52.5	*-52.6
EO4 - FI	*-122.1	*-65.0	*-56.3
EO5 - FI	*-209.1	*-113.7	*-111.3
EO6 - FI	*-199.3	*-92.6	*-86.1
HFI - FI	*166.5	*78.5	*71.3
DI - FI	*-317.1	*-184.2	*-174.1
EO1 - HFI	97.7	*63.7	*59.3
EO2 - HFI	*139.2	*68.1	*67.9
EO3 - HFI	31.5	26.0	18.7
EO4 - HFI	44.4	13.5	15.1
EO5 - HFI	-42.7	-35.2	-40.0
EO6 - HFI	-32.9	-14.2	-14.8
DI - HFI	*-150.6	*-105.7	*-102.7
DI - EO1	*-248.3	*-169.4	*-162.1
DI - EO2	*-289.8	*-173.7	*-170.7
DI - EO3	*-182.1	*-131.7	*-121.4
DI - EO4	*-195.0	*-119.2	*-117.7
DI - EO5	-108.0	*-70.5	*-62.7
DI - EO6	*-117.8	*-91.5	*-87.9

533

\* Significantly different at the 95% confidence level.







568

Figure 3. Actual simulated evapotranspirations, as based on Penman-Monteith (PM) and Priestly and Taylor (PT) calculations vs. actual measured evapotranspiration, as estimated from the water-balance method. The black (E-PM) and the gray (E-PT) lines show the corresponding regressions.



Figure 4. Simulated soil water contents, as based on Penman-Monteith (PM) and Priestly and Taylor (PT) calculations *vs.* actual soil water contents. The black (SWC-PM) and the gray (SWC-PT) lines show the corresponding regressions.