IMECE2010-

The Entropy Analysis on NH3/CO2 Cascade Refrigeration Cycle

Yingbai XIE

School of Energy & Power Engineering North China Electric Power University, 62 Mailbox, 619 North Yonghua Street, Baoding 071003, Hebei, China Phone: 86-312-7522882. Fax: 86-312-7522440, E-mail: xieyb@ncepu.edu.cn

Luxiang ZONG

School of Energy & Power Engineering North China Electric Power University, 62 Mailbox, 619 North Yonghua Street, Baoding 071003, Hebei, China Phone: 86-312-7522882. Fax: 86-312-7522440, E-mail: zongluxiang@163.com

ABSTRACT

This paper introduces a cascade refrigeration cycle that uses natural refrigerants of $CO₂$ and NH₃ at low temperature. It introduces the character of $CO₂$ and NH₃, besides analyzes the cascade refrigeration cycle. The optimal intermediate temperature of $NH₃/CO₂$ cascade refrigeration cycle is determined by the entropy production minimization method. We analyze the four processes entropy production in both CO_2 cycle (LT side) and NH₃ cycle (HT side) and research how the total entropy production changes in the conditions of different T_0 , different T_{CL} and different $\triangle T$. We also find that in order to enhance the efficiency of $NH₃/CO₂$ cascade refrigeration cycle, it is necessary to reduce \triangle T. It can be concluded that NH₃/CO₂ cascade refrigeration cycle has a good future.

Kuikui CUI

School of Energy & Power Engineering North China Electric Power University,62 Mailbox, 619 North Yonghua Street, Baoding 071003, Hebei, China Phone: 86-312-7522882. Fax: 86-312-7522440, E-mail: wangyi16688@126.com

Zhichao WANG

School of Energy & Power Engineering North China Electric Power University, 62 Mailbox, 619 North Yonghua Street, Baoding 071003, Hebei, China Phone: 86-312-7522882. Fax: 86-312-7522440, E-mail: wzcmonkey@163.com

INTRODUCTION

Global environmental problems, such as global warming and depletion of the ozone layer, have become more and more severe by the use of synthetic refrigerants (CFC, HCFC and HFC). In order to keep sustainable development of environment, searching efficient, green and friendly refrigerants has become a common concern of the international community. Natural working fluid was regarded as the final plan to solve environmental problems by G**.** Lorentzen the former president of the International Institute of Refrigeration [1]. When the required T_{CL} is very low, we can use cascade refrigeration system. The cascade refrigeration system consisted by two single-stage compression refrigeration system usually uses R22 and R13 as refrigerant in most regions of the world. However R22 and

Nomenclature

R13 not only destroy atmospheric ozone layer, but also have serious greenhouse effect. Under the "Montreal Protocol", R13 has been forbidden currently, and R22 only can be used before 2030 in some countries.

Therefore, refrigerant friendly to environment is needed to meet the requirement of low-temperature refrigeration. W. R. Kitzmiller once promoted the program of $NH₃/CO₂$ cascade refrigeration cycle in 1932, high pressure level with $NH₃$ as refrigerant, low-level with $CO₂$ as refrigerant. $CO₂$ has good heat transfer performance, rather large cooling capacity by using latent heat and small viscosity at low temperature compared with other low-pressure refrigerant [2]. The research of Pettersen A**.** and Jakobsen shows that when using $CO₂$ instead of NH₃ at low-level, the size of compressor will reduce to the original $1 / 10$ compared with $NH₃/NH₃$ system, and T_{CL} can reach to - 50°C—- 45°C, even reach to - 80°C through the dry ice for powder effect. At present, Europe has established a few of cascade refrigeration system with low-temperature using $CO₂$ as refrigerant in the supermarkets. Operation conditions indicate that it is technically feasible. This system can also be applied to low-temperature freeze-drying process.

THE PHYSICAL PROPERTIES OF CO2 AND NH3

As a refrigerant, $CO₂$ has some special advantages.

Mainly in: (1) $CO₂$ is harmless to environment and a substance naturally existing in nature (ODP = 0 , GWP = 1). (2) $CO₂$ has excellent economy. (3) $CO₂$ has good security, and chemical stability. It is safe, non-toxic and non-combustible, adapting to mechanical parts materials using a variety of oil. Even at high temperature, it does not decompose to produce harmful gases. (4) $CO₂$ has good thermal physical properties, suiting to the refrigeration cycle and equipment. It has larger latent heat of evaporation and has greater cooling capacity(0 \degree C, the cooling capacity per unit volume of CO₂ is 1.58 times of NH3, 5.12 times of R22 and 8.25 times of R12) [3]. At the same time, its dynamic viscosity is low. 0° C, the dynamic viscosity of $CO₂$ saturated liquid is only 5.2% of NH₃ and 23.8% of R12. $CO₂$ has high thermal conductivity and small ratio of liquid density and vapor density; refrigerant between circuits is more easily distributed after throttling. $CO₂$ has excellent flow and heat transfer characteristics, so the size of the compressor and the system can be significantly reduced to make the whole system compact.

NH3 has been used for 120 years and still applies to large-scale industrial systems in many countries. The advantage is ODP=0, GWP=0, with excellent thermodynamic properties, cheap price and convenient leak detection. It is the most vital refrigerant used in standard refrigeration equipment with reciprocating or rotary compressor and cooling capacity higher than 25KW. And in the appropriate equipment, even more small-capacity NH₃ refrigerator has gradually appeared in the market. Most consideration about $NH₃$ is its safety, mainly about its toxicity and flammability, followed by pungent smell. In fact, its toxicity is only 1/10-1/50 of the toxicity of chlorine; its ignition limit is 15.5% (volume ratio), 3-7 times of the usual hydrocarbon and natural gas, while the heat of combustion is less than half of them. About 100 years historical experience shows that NH₃ has low accident rate. NH₃ has a strong pungent smell. Therefore, we can easily identify the leak. In addition, $NH₃$ is lighter than air, so it is easy to escape from the roof to outside. When $NH₃$ and water is contacted, NH₃ can be quickly absorbed by water. This performance can be used to eliminate the $NH₃$ vapor in the air, greatly reducing the accident.

THE ENTROPY ANALYSIS OF NH₃/CO₂ CASCADE **REFRIGERATION CYCLE**

Theoretical analysis

 $NH₃/CO₂$ cascade refrigeration cycle is composed of $NH₃$ high-temperature cycle and $CO₂$ low-temperature cycle [4]. Fig. 1 schematically depicts the cascade refrigeration cycle. Fig.2 is the corresponding temperature-entropy diagram. In Fig. 2, 1-2-3-4-5-1 is cycle of low-temperature part $(CO₂)$, and 6-7-8-9-10-6 is the cycle of the high temperature part (NH₃) .The evaporation of NH3 and the condensation of $CO₂$ complete in a "cascade condenser"; and this equipment insulates environment using insulation materials. Therefore, evaporation heat of NH3 is equal to the condensation heat of $CO₂$, and temperature difference in cascade condenser($\triangle T$) is 5-8℃.

Fig.1 Schematic diagram of CO₂/NH₃ cascade refrigeration cycle

Fig.2 The temperature-entropy diagram of $CO₂/NH₃$ cascade refrigeration cycle

Theoretical cycle is calculated as follows The relation of the mass flow between HT circuit and LT circuit:

If the mass flow of LT part of CO_2 is m_L and cooling capacity

is Q_0 , then

$$
m_L = \frac{Q_0}{h_1 - h_5} \tag{1}
$$

Heat transfer rate of cascade condenser is,

$$
Q_{KL} = Q_0 \frac{h_2 - h_4}{h_1 - h_5}
$$
 (2)

The mass flow of HT circuit is,

$$
m_{\rm H} = \frac{Q_{\rm KL}}{h_6 - h_{10}} = \frac{Q_0(h_2 - h_4)}{(h_6 - h_{10}) (h_1 - h_5)}
$$
(3)

The entropy production [5] of LT circuit:

The compression process:
$$
\Delta S_{\text{YL}} = m_{\text{L}}(s_{2} - s_{1})
$$
 (4)

The cooling process:
$$
\Delta S_{CL} = m_L (s_4 - s_2) + \frac{Q_{LZ}}{T_6}
$$
 (5)

Where,
$$
Q_{LZ} = m_L(h_2 - h_4)
$$

The through process:
$$
\Delta S_{JL} = m_L (s_5 - s_4)
$$
 (6)

The evaporation process:
$$
\Delta S_{ZL} = m_L (s_1 - s_5) - \frac{Q_0}{T_{CL}}
$$
 (7)

The entropy production of HT circuit:

The compression process:
$$
\Delta S_{\gamma H} = m_H(s_7 - s_6)
$$
 (8)

3 Copyright © 2010 by ASME

The cooling process: ΔS _{LH} = m_H^{(s}9^{-s}7) $\boldsymbol{0}$ \mathcal{Q}_{LH} *T* $\Delta S_{\text{H}} = m_{\text{H}} (s_o - s_a) + \frac{LH}{(9)}$

where, $Q_{LH} = m_H (h_7 - h_9)$,

The throt tling process:
$$
\Delta S_{JH} = m_H(s_{10} - s_9)
$$
 (10)

The evaporation process: $\Delta S_{ZH} = m_H (s_6 - s_{10})$ $\Delta S_{ZH} = m_H (s_6 - s_{10}) - \frac{Q_{LZ}}{T_3}$ (11)

where, $Q_{LZ} = m_H (h_6 - h_{10})$

Analysis of the calculating results

As the part of the HT cycle is cooled under ambient temperature conditions. So the condensing medium temperature(T_0) is 25°C. Condensing temperature can be taken as 40 ℃ .The temperature difference [7] in cascade condenser($\triangle T$) is 5°C. Evaporation temperature is -55°C, and cooling capacity(Q_0) is 3.5kw. The isentropic efficiency of compressing process is 0.8;the refrigerated space temperature(T_{CL}) is - 45 °C, and CO_2 condensing temperature(T_3) is a known constant.

Fig.3 The entropy productions of compressing process, condensing process, throttling process, evaporating process and total entropy production ($\triangle S_{\text{YL}}, \triangle S_{\text{CL}}, \triangle S_{\text{JL}}, \triangle S_{\text{ZL}},$ $\triangle S_{GL}$) in LT circuit change with T₃

Fig.3 shows how the entropy productions of compressing process, condensing process, throttling process, evaporating process and total entropy production in LT circuit change with T_3 . It can be seen from the figure that the entropy productions of compressing process, condensing process, throttling process increase as T_3 rising. The entropy production of condensing process is the largest, followed is the compressing process. And the change of evaporating process is very small.

Fig.4 The entropy production of compressing process, condensing process, throttling process, evaporating process and total entropy production ($\triangle S_{\text{YH}}$, $\triangle S_{\text{CH}}$, \triangle S_{JH} , $\triangle S_{ZH}$, $\triangle S_{GH}$) in HT circuit change with T₃

Fig.5 The sum of the entropy production in each circuit and total entropy production($\triangle S_{GL}$, $\triangle S_{GH}$, $\triangle S_G$) change with T₃

Fig.4 shows how the entropy productions of compressing process, condensing process, throttling process, evaporating process and total entropy production in HT circuit change with T_3 . It can be seen from the figure that the entropy production of condensing process, throttling process decrease as $T₃$ rising. The entropy production of condensing process is the largest, followed is the throttling process; the changes of compressing process and evaporating process are nearly constant.

Fig.5 shows how the sum of the entropy production in each circuit and total entropy production change with $T₃$. It can be seen from the figure that with the raise of T_3 , the sum of the entropy production in LT circuit increases, while the sum in HT circuit decreases and the total entropy production first decreases, then increases. So there exists a minimum entropy production. The corresponding temperature of minimum entropy production is called optimum intermediate temperature [6]. The optimum intermediate temperature of the calculating condition is -18℃.

Fig.6 The total entropy production($\triangle S_G$) changes with T₃ in different △T

Fig.7 The total entropy production($\triangle S_G$) changes with T₃ in different T₀

Fig.8 The total entropy production($\triangle S_G$) changes with T₃ in different T_{CL}

Figure 6, Figure 7, and Figure 8 separately shows how the total entropy production of $NH₃/CO₂$ cascade refrigeration cycle changes with T_3 under the conditions of different $\triangle T$, T_0 and T_{CL} . It can be seen from the three figures, with the increase of T_3 , the total entropy production decreases at first and then increases, so there exists a minimum entropy production. As for different $\triangle T$, the smaller the $\triangle T$ is, the smaller the corresponding total entropy production is. That is, the irreversible loss is smaller. So we should reduce $\triangle T$.

CONCLUSIONS

The total entropy production of $NH₃/CO₂$ cascade refrigeration cycle decreases at first and then increases with T_3 increasing, and there is a minimum entropy production. The minimum entropy production can determine the optimal intermediate temperature of $NH₃/CO₂$ cascade refrigeration cycle. In this paper, the optimal intermediate temperature is about -18℃.

(1) As T_3 increases, the sum of entropy production in LT circuit increases while the sum of entropy production in HT circuit decreases, and the entropy production of condensing process is maximum.

(2) The minimum entropy production increases with $\triangle T$ and T_{CL} increasing, and decreases with T_0 increasing. Among them, the minimum entropy production changes greatest with \triangle T. In order to reduce irreversible loss of NH₃/CO₂ cascade refrigeration cycle, we should first reduce $\triangle T$.

(3) This paper only analyzes the irreversible loss of $NH₃/CO₂$ cascade refrigeration system by using entropy, but we need to do further research to optimize the system performance (COP).

ACKNOWLEDGMENTS

This work was supported by the Fundamental Research Funds for the Central Universities (09MG32).

REFERENCES

- [1] Jinghong Ning, Shitong Cha, Huiyu LI, Miao Peng. Analysis the $R290/CO₂$ cascade refrigeration cycle by using the minimum entropy method. Energy Research Institute of Tianjin University. 2007 (1):85-88.
- [2] J. PettersenA., A. Jakobsen. A dry ice slurry system for low temperature refrigeration. International symposium on refrigeration in sea transport today and in the future. Gdansk, Poland Sep/Oct, 1994.
- [3] J. PettersenA., A. Jakobsen. A dry ice slurry system for low temperature refrigeration. International symposium on refrigeration in sea transport today and in the future. Gdansk, Poland Sep/Oct, 1994.
- [4] Bingming Wang, Huagen Wu, Jianfeng Li, Ziwen Xing, Experimental investigation on the performance of $NH₃/$ CO2 cascade refrigeration system with twin-screw compressor , international journal of refrigeration 32 (2009) 1358-1365.
- [5] Eric B. Ratts, J. Steven Brown. A generalized analysis for cascading single fluid vapor compression refrigeration cycles using an entropy generation minimization method [J]. International Journal of Refrigeration, 2000, 23:
- [6] Tzong-Shing Lee, Cheng-Hao Liu, Tung-Wei Chen. Thermodynamic analysis of optimal condensing temperature of cascade-condenser in $CO₂/NH₃$ cascade refrigeration systems. International Journal of Refrigeration 2006, (29):1100-1108.
- [7] J.Alberto Dopazo, Jose Fernandez-Seara , Jaime Sieres, Francisco J. Uhia, Theoretical analysis of a $CO₂/NH₃$ cascade refrigeration system for cooling applications at low temperatures, Applied Thermal Engineering 2009 (29):1577-1583.