

Contents lists available at ScienceDirect

### Earth and Planetary Science Letters



journal homepage: www.elsevier.com/locate/epsl

# The oxidation state of Fe in MORB glasses and the oxygen fugacity of the upper mantle

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#### ARTICLE INFO

Article history: Accepted 9 March 2011 Available online 9 April 2011

Keywords: oxygen fugacity oxidation state MORB mantle iron XANES

#### ABSTRACT

Micro-analytical determination of  $Fe^{3+}/\Sigma$  Fe ratios in mid-ocean ridge basalt (MORB) glasses using micro X-ray absorption near edge structure (µ-XANES) spectroscopy reveals a substantially more oxidized upper mantle than determined by previous studies. Here, we show that global MORBs yield average Fe<sup>3+</sup>/ $\Sigma$ Fe ratios of  $0.16 \pm 0.01$  (n = 103), which trace back to primary MORB melts equilibrated at the conditions of the quartz-fayalite-magnetite (QFM) buffer. Our results necessitate an upward revision of the Fe $^{3+}/\Sigma$ Fe ratios of MORBs, mantle oxygen fugacity, and the ferric iron content of the mantle relative to previous wet chemical determinations. We show that only 0.01 (absolute, or <10%) of the difference between  $Fe^{3+}/$  $\sum$  Fe ratios determined by micro-colorimety and XANES can be attributed to the Mössbauer-based XANES calibration. The difference must instead derive from a bias between micro-colorimetry performed on experimental vs. natural basalts. Co-variations of  $Fe^{3+}/\sum$ Fe ratios in global MORB with indices of lowpressure fractional crystallization are consistent with Fe<sup>3+</sup> behaving incompatibly in shallow MORB magma chambers. MORB  $Fe^{3+}/\Sigma$  Fe ratios do not, however, vary with indices of the extent of mantle melting (e.g., Na<sub>2</sub>O(8)) or water concentration. We offer two hypotheses to explain these observations: The bulk partition coefficient of  $Fe^{3+}$  may be higher during peridotite melting than previously thought, and may vary with temperature, or redox exchange between sulfide and sulfate species could buffer mantle melting at ~QFM. Both explanations, in combination with the measured MORB  $Fe^{3+}/\Sigma$ Fe ratios, point to a fertile MORB source with greater than 0.3 wt.% Fe<sub>2</sub>O<sub>3</sub>.

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#### 1. Introduction

Oxygen fugacity  $(fO_2)$  is an intensive thermodynamic property that fundamentally regulates igneous processes by governing the likely speciation of multi-valent elements such as Fe. S. and V. thereby controlling their availability to participate in chemical reactions. Upper mantle processes critically affected by fO<sub>2</sub> include, but are not limited to, magmatic phase relations during melting and crystallization, trace element partitioning, the depth of melt initiation, and volcanic degassing (e.g., Ballhaus, 1993; Canil, 1999; Eggler and Baker, 1982; Eugster, 1959; Holloway and Blank, 1994). In multi-component systems, the relationship between iron oxidation state and oxygen fugacity is not always straightforward, and there is seldom consensus on which variable is dependent and which is independent (Canil et al., 1994; Frost, 1991; Herd, 2008; McCammon, 2005). The oxidation state of iron in basaltic glasses, on the other hand, directly relates to the  $fO_2$  of the solid mantle from which it derives because melts are free of crystal chemical constraints (Carmichael, 1991; Herd, 2008; Kress and Carmichael, 1991). The Fe<sup>3+</sup>/ $\sum$ Fe ratio [Fe<sup>3+</sup>/(Fe<sup>2+</sup> + Fe<sup>3+</sup>)] of basaltic glass can be quantified by comparing the X-ray absorption spectra of unknown basaltic glasses to the spectra of basaltic glasses of similar composition (Berry et al., 2003; Cottrell et al., 2009; Wilke et al., 2005). Synchrotron-facilitated micro X-ray Absorption Near Edge Structure ( $\mu$ XANES or XANES) spectroscopy affords non-destructive microanalytical determination of multi-valent element speciation at the same spatial scales as other micro-analytical techniques, allowing element oxidation state to be directly related to other geochemical proxies in microscopic glass samples.

The premise of this study is to re-assess the oxidation state of Fe in mid-ocean ridge basalts using  $\mu$ -XANES, a microbeam technique that samples glass only, and to explore global relationships between Fe<sup>3+</sup>/ $\sum$  Fe ratios and major element chemistry, magmatic water concentration, and trace elements. We report and compare new measurements of Fe<sup>3+</sup>/ $\sum$  Fe ratios of global mid-ocean ridge basalt glasses (hereafter referred to as 'MORB') using several methods, and show that MORBs are uniformly more oxidized than prior studies have indicated. These results place new constraints on the  $fO_2s$  relevant for MORB magmas and the Fe<sup>3+</sup> concentrations expected in mantle sources. We will examine the implications of these findings for the evolution of Fe<sup>3+</sup>/ $\sum$  Fe ratios in MORB magmatic systems during low-pressure crystal fractionation, for the Fe<sup>3+</sup>

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concentration of the MORB mantle, and for the mechanisms controlling  $fO_2$  of the MORB mantle during melting beneath mid-ocean ridges.

#### 2. Methods

#### 2.1. Samples and preparation

Natural samples analyzed in this study include pillow-rim basaltic glasses from a global distribution of mid-ocean ridges (Supplemental Fig. 1) with a particular emphasis on choosing glasses common to the studies of Christie et al. (1986) and/or Bezos and Humler (2005) (hereafter referred to as CCL86 and BH05, respectively). Two experiments were carried out to create glasses for wet chemical and XANES analysis for the present study at QFM-5.0 and QFM-1.0, using the All basalt starting material and experimental procedures detailed in Cottrell et al. (2009). We also prepared all of the experimental glasses (n = 6) from the original study of Kress and Carmichael (1991) provided by V. Kress.

For microbeam analysis, natural and experimental glass chips were hand-picked from the Smithsonian Sea Floor Glass Collection, from experimental run products, or from pre-picked splits sent from donors or other repositories. Samples were mounted in epoxy, double-side polished to a nominal thickness of 100  $\mu$ m, and photographed in reflected, plane-polarized, and cross-polarized light to ensure a crystal-free path for infrared and X-ray microbeams. In addition to glass wafers, chips and powders were prepared for Fe<sup>3+</sup>/ $\Sigma$ Fe determinations by wet chemistry (micro-colorimetry) and Mössbauer spectroscopy. In some cases, original glass powders from the micro-colorimetric study of CCL86 were available for reanalysis.

#### 2.2. Analytical methods

#### 2.2.1. μ-XANES

Glass wafers were analyzed by collecting three Fe K-edge XANES spectra per sample, each on an independent  $9 \times 5 \,\mu m$  spot, at station X26A (bending magnet) at the National Synchrotron Light Source (NSLS), Brookhaven National Laboratory (BNL). Spectral collection and fitting details are given in full in Cottrell et al. (2009), and an overview is provided in the electronic supplement. The Fe<sup>3+</sup>/ $\Sigma$ Fe ratios of MORB glasses were quantified by referencing the driftcorrected centroid (the area-weighted energy of the pre-edge  $1s \rightarrow 3d$ multiplet) to a calibration curve constructed from experimental basaltic glasses. The 13 calibration glasses were equilibrated at 1 atm over a range of oxygen fugacities, from 2 log units below to 4.5 log units above the Quartz-Favalite-Magnetite (QFM) buffer, and span a range of basalt compositions appropriate for MORB (average  $\sum d_i X_i = 0.18 \pm 0.01$ , defined in Table 2). The Fe<sup>3+</sup>/ $\sum$ Fe ratios of these reference glasses were determined with Mössbauer spectroscopy and range from 0.088 to 0.611. The 1  $\sigma$  uncertainty in Fe<sup>3+</sup>/ $\Sigma$ Fe ratio measured by XANES on unknowns for this range of oxidation states is  $\pm 0.0045$  (Cottrell et al., 2009).

#### 2.2.2. Electron microprobe analysis

Major element compositions of glasses new to this study were determined by electron microprobe at the Smithsonian Institution according to Melson et al. (2002). In all other cases we report the published values. The total iron concentrations, FeO\*, of glasses used for wet chemical determination of Fe<sup>3+</sup>/ $\Sigma$ Fe ratio for this study were all obtained on the Smithsonian microprobe. Additional details and analyses are provided in the electronic supplements.

#### 2.2.3. Mössbauer spectroscopy

Mössbauer spectra of two hand-picked MORB glasses were acquired and analyzed at the Geophysical Laboratory, Carnegie Institution of Washington, according to the procedures detailed in Cottrell et al. (2009) and Supplemental Fig. 3.

#### 2.2.4. Fourier transform infrared spectroscopy

Transmittance FTIR spectra were obtained at the Smithsonian Institution or at NSLS station U10B over the 700–6000 cm<sup>-1</sup> wavenumber range. We determined total water concentrations (molecular  $H_2O$  plus OH<sup>-</sup>) from the intensity of the broad 3530 cm<sup>-1</sup> absorption band, utilizing a molar absorptivity of 63 l/mol cm (Dixon et al., 1995) and a glass density of 2800 g/l. Thicknesses were determined using a piezoelectric digital micrometer and interference fringe patterns (Nichols and Wysoczanski, 2007). In all cases the absorption at this peak position was less than 0.8 above the baseline, and no systematic offset was observed between water concentrations derived from spectra collected at Smithsonian and the NSLS. Additional details are provided in the electronic supplement.

#### 2.2.5. Microcolorimetry (wet chemistry)

The FeO content of select natural MORB and experimental glasses was determined using the micro-colorimetric procedure of CCL86, modified from Wilson (1960). Analyses were carried out blind, in collaboration with Dr. Rebecca Lange at the University of Michigan. Four USGS powdered rock standards were run in each analytical session. Analyses of these USGS standards never deviated from the certified FeO content by more than 0.16 wt.% FeO, well within the established analytical precision of  $\pm 0.22$  (1  $\sigma$ , absolute). Additional details are provided in the electronic supplement.

#### 2.2.6. LA-ICPMS

Trace element concentrations of wafered MORB glasses were determined by Laser Ablation Inductively-Coupled Plasma Mass Spectrometry (LA-ICPMS) at the Graduate School of Oceanography, University of Rhode Island. Analytical methods are modified from the techniques of Kelley et al. (2003). On average, triplicate analyses of



Fig. 1. Plot of energy vs. intensity for edge-step normalized, baseline-subtracted Fe K-edge XANES fluorescence spectra. Reference glasses were equilibrated in 1/2 log unit steps ( $\Delta 0.02-0.03$  in Fe<sup>3+</sup>/ $\sum$ Fe). Baseline-subtracted, drift-corrected pre-edge peaks for calibration glasses are shown at 1 log unit steps (plus a glass at QFM = 0) in  $fO_2$ (solid lines) for clarity. All full raw spectra for these glasses, spanning the energy range from 7100 to 7200 eV and corrected only for instrumental energy drift, are presented in Cottrell et al. (2009). The area-weighted average energy of the pre-edge peaks is defined as the centroid, which shifts to higher energies as a function of iron oxidation state. As the percentage of  $Fe^{3+}$  increases above 10% of total Fe, the centroid shifts clearly to higher energies and the Fe<sup>3+</sup>/ $\Sigma$ Fe ratio is easily quantified. It is difficult to use the pre-edge centroid to quantify the  $Fe^{3+}/\Sigma Fe$  ratio when the ferric iron contribution falls below 9% of the total iron because octahedrally coordinated Fe<sup>2</sup> + has an electronic transition to a 3d-like electronic level that contributes to the spectra of reduced glasses near 7113 eV (referenced to glass LW\_0≡7113.3 eV). Also plotted is a typical baseline-subtracted pre-edge of a mid-ocean ridge basaltic glass (dashed line) that can clearly be seen to fall between calibration glasses equilibrated between QFM -0.5 and QFM (~14 and 16% of iron in the ferric state, respectively).

each sample agree within 3% rsd or less for all elements reported. Additional details are provided in the electronic supplement.

#### 3. Results

3.1. Accuracy of XANES for the assessment of  $Fe^{3+}/\sum Fe$  in MORB Part I: Range in  $Fe^{3+}/\sum Fe$  that can be accurately and precisely quantified with XANES

The  $\mu$ -XANES pre-edge centroid position can be used to determine Fe<sup>3+</sup>/ $\sum$ Fe ratios in basaltic glasses from ~0.09 (~QFM-2), to >0.60 (~QFM+4.5), with a precision of  $\pm$  0.0045 using the procedures of Cottrell et al. (2009). Representative baseline-subtracted pre-edge spectra for reference glasses are shown in Fig. 1. We also plot a typical baseline-subtracted spectrum of a MORB glass, which can clearly be seen to fall between basalts equilibrated at QFM and QFM-0.5 (Fe<sup>3+</sup>/ $\sum$ Fe  $\approx$  0.16 and 0.14, respectively).

Precise and accurate quantification of Fe<sup>3+</sup>/ $\Sigma$ Fe ratios greater than 0.60 may be achievable, but is beyond the range of our calibration. The shape of the calibration curve suggests that precise quantification of the Fe<sup>3+</sup>/ $\Sigma$ Fe ratio using the pre-edge centroid will be challenging when Fe<sup>3+</sup>/ $\Sigma$ Fe>0.80 (Cottrell et al., 2009; Wilke

Table 1

Wet-chemical results (micro-colorimetry) compared to Mössbauer/XANES results.

et al., 2005). Use of the pre-edge centroid to quantify  $Fe^{3+}/\sum Fe<0.09$  is prohibited by crystal field effects. The coordination of Fe in glasses is poorly constrained, but ranges from tetrahedral to octahedral (Mysen and Richet, 2005 and references therein). Both tetrahedrally and octahedrally coordinated  $Fe^{2+}$  have electronic transitions corresponding to 3d-like electronic levels that occur near 7113 eV, which overlap the energy range of the main contribution from  $Fe^{3+}$  (Galoisy et al., 2001; Westre et al., 1997). We observe that the centroid ceases to shift to lower energies as a function of ferric iron is essentially indistinguishable from a glass with 8% ferric iron (Fig. 1 and Supplemental Fig. 2).

To rigorously test this observation, experiment AII\_-50 was equilibrated at QFM-5 to ensure that 100% of the iron was in the ferrous state. Wet chemical analysis confirmed the absence of any ferric iron (Table 1 and Fig. 2). Relative to reference glass LW\_0 (QFM=0) with a centroid of 7112.300, the centroid of AII\_-50 is 7112.071  $\pm$  0.016, the same within error as glass equilibrated at QFM-3.0 (Cottrell et al., 2009). A shoulder is clearly visible in the baseline subtracted spectra in the region overlapping electronic transitions corresponding to ferric iron (Supplemental Fig. 2). The centroid of AII\_-50 would correspond to Fe<sup>3+</sup>/ $\Sigma$ Fe=0.082 if analyzed as an

		-										
	FeO (wt.%) wet chemistry				wt.%)	Fe <sup>3+</sup> /ΣFe we	Fe <sup>3+</sup> /ΣFe spectroscopy					
Sample	This study	Christie et al. (1986)	Bezos and Humler (2005)	SI	Christie et al. (1986)	This study SI FeO*	This study and Christie et al. (1986) FeO <sup>*a</sup>	Christie et al. (1986)	Bezos and Humler (2005)	Predicted/ reported K and C <sup>b</sup> (1991)	MÖSS	XANES <sup>h</sup>
Experimental hasalts <sup>c</sup>												
All -50	7.35			6.98		- 0.053				0.00	b.d	0.082
AII -50R <sup>d</sup>	7.25			6.98		- 0.039				0.00		
O62 <sup>e</sup>										0.63	n.a.	0.628
Q65 <sup>e</sup>	5.38			16.00		0.663				0.64	n.a.	0.620
Q66 <sup>e</sup>	5.62			15.47		0.637				0.62	n.a.	0.617
Q61 <sup>e,f</sup>										0.67 <sup>f</sup>	n.a.	0.647
Q51 <sup>e,f</sup>										0.75 <sup>f</sup>	n.a.	0.700
Q53 <sup>e,f</sup>										0.75 <sup>f</sup>	n.a.	0.709
LW_20 <sup>g</sup>	7.42			10.68		0.306				0.30	0.30	0.303
AII_15 <sup>g</sup>	7.47			9.33		0.200				0.26	0.25	0.247
AII10	8.55			9.40		0.090				0.10	n.a.	0.116
Natural basalts <sup>h</sup>												
IDF C6-1												0 165
IDF C6-1 (VG chip)	10.16	10.41	9.78	11.57	11.14	0.122	0.088	0.066	0.123			01100
IDF C6-1 (Carmichael pwd <sup>i</sup> )	10.42	10.41	9.78	11 57	11 14	0.099	0.065	0.066	0.123			
CH33-1	10112	10111	5110	11.07		0.000	01000	0.000	01125			0.153
CH33-1 (VG chip)	8.62	9.29	8.73	9.88	9.72	0.128	0.114	0.044	0.102			
CH33-1R <sup>d</sup> (VG chip)	9.13	9.29	8.73	9.88	9.72	0.076	0.060	0.044	0.102			
CH33-1_R <sup>d</sup> 3 (VG chip)	8.79	9.29	8.73	9.88	9.72	0.110	0.095	0.044	0.102			
CH33-4_R <sup>d</sup> 4 (VG chip)	9.00	9.29	8.73	9.88	9.72	0.089	0.074	0.044	0.102			
CH61-1												0.163
CH61-1 (Langmuir chip <sup>i</sup> )	8.28	9.14		10.05	9.93	0.177	0.167	0.072				
CH61-1 (Carmichael pwd)	8.60	9.14		10.05	9.93	0.144	0.134	0.072				
CH5-1 (VG chip)	9.60	10.16		11.16	11.13	0.140	0.138	0.087				0.166
VG3385, 523-2-1 (VG chip)	9.50	9.28	9.12	10.37	10.05	0.084	0.055	0.077	0.093		0.16	0.143
VG8488, 2πD47-1 (VG chip)	8.59		8.30	9.43		0.089	0.093		0.124		0.17	0.159
USNM 113716 (VG chip)	8.36			9.13		0.085						0.150
JDF C2-1 (Carmichael pwd)	11.95	11.76	12.03	14.31	13.78	0.165	0.133	0.146	0.127			0.160
975-5-1 (Langmuir chip)	9.35	9.59		10.68	10.34	0.125	0.096	0.072				0.165
CH6-1 (VG chip)	8.43	9.41		10.40	10.26	0.189	0.178	0.080				0.162
CH30-1 (Langmuir chip)	10.47	10.65		11.51	11.62	0.090	0.099	0.080				0.167

<sup>a</sup> The Fe<sup>3+</sup>/ $\sum$ Fe ratio calculated from the FeO measured in this study via micro-colorimetry combined with the FeO\* from Christie et al. (1986).

<sup>b</sup> Calculated from Kress and Carmichael (1991) equation (7) or measurements reported in that paper.

<sup>c</sup> Additional data plotted in Fig. 2 are from Cottrell et al. (2009).

<sup>d</sup> "R" = replicate analysis.

<sup>e</sup> Samples from Kress and Carmichael (1991). Provided by Victor Kress.

<sup>f</sup> These glasses fall outside of our XANES calibration range.

<sup>g</sup> From Cottrell et al. (2009).

<sup>h</sup> All XANES measurements taken on wafered glass chips.

<sup>1</sup> Wet chemistry performed on powder from the study of Christie et al. (1986), provided by Ian Carmichael, or on chips of glass provided by Charlie Langmuir.

unknown (Fig. 2). As the ferric iron content drops below 10% we observe that centroid values cease to decrease systematically in the calibration curves of Berry et al. (2008), Cottrell et al. (2009), Wilke et al. (2005), and calibration curves compiled from the literature shown in Cottrell et al. (2009).

The critical result is that the pre-edge centroid can only place an upper limit on the ferric iron content of samples with <8-9% of their iron in the ferric state. Caution should be exercised when centroid values fall near the lower end of the calibration range (Fe<sup>3+</sup>/ $\sum$ Fe  $\leq$  10%), such as for lunar glasses and Archean melt inclusions (Berry et al., 2008).

# 3.2. Accuracy of XANES for the assessment of $Fe^{3+}/\sum Fe$ in MORB Part II: Direct comparison with wet chemistry

The Fe<sup>3+</sup>/ $\Sigma$ Fe ratios of the calibration glasses used in this study were independently determined by Mössbauer spectroscopy and in Fig. 2 those determinations are compared to the Fe<sup>3+</sup>/ $\Sigma$ Fe ratios



expected from the composition-dependent empirical expression that relates fO<sub>2</sub> to iron oxidation state determined with micro-colorimetry (Kress and Carmichael, 1991). Kress and Carmichael (1991) and CCL86 employed the same wet chemical technique applied here. The  $Fe^{3+}/\Sigma$ Fe ratios of experimental glasses directly determined by micro-colorimetry in this study are also compared to the Mössbauerbased XANES calibration of Cottrell et al. (2009) in Fig. 2. The two determinations, by Mössbauer and by (or referenced to) wet chemistry, are strongly correlated ( $R^2 = 0.99$ ), but the XANES calibration is systematically offset to higher Fe oxidation state by 0.01 (absolute). Potential offsets between Mössbauer and wet chemical determinations of iron oxidation state have been debated in the literature (Dingwell, 1991; Dyar et al., 1987; Lange and Carmichael, 1989; Mysen et al., 1985; Ottonello et al., 2001). The practical result for the present study is that, if we reconstruct our XANES calibration using the Kress and Carmichael (1991) algorithm, the Fe<sup>3+</sup>/ $\Sigma$ Fe ratio of unknown basalts would shift to more reduced values by 0.01 (absolute), or <10% (relative).

The majority of the experimental glasses from the XANES calibration suite were pressed into pellets for Mössbauer analysis, rendering them unsuitable for wet chemical analysis. Two experiments, equilibrated at QFM+2 and QFM+1.5, had enough glass remaining to perform micro-colorimetric determination of Fe<sup>3+</sup>/ $\sum$ Fe. An additional experiment at QFM-1 was undertaken for micro-colorimetric analysis (AII\_-10, spectrum in Supplemental Fig. 2) and this experiment falls precisely on the XANES calibration curve at the expected Fe<sup>3+</sup>/ $\sum$ Fe ratio of 0.12. Two experiments provided by V. Kress from the original study of Kress and Carmichael (1991) were analyzed by XANES and reanalyzed by micro-colorimetry in R. Lange's lab at U. Michigan.

Glasses analyzed in this study by wet chemistry are tabulated in Table 1. The Fe<sup>3+</sup>/ $\sum$ Fe ratios of the five experimental basalts determined by micro-colorimetry in this study are consistent with the ratios predicted from the Kress and Carmichael (1991) algorithm, and the Mössbauer-based XANES calibration (Table 1; Fig. 2a). Micro-colorimetic and XANES results on glasses provided by V. Kress were identical within error. Given all of these tests, we are confident that micro-colorimetry and our Mössbauer-based XANES calibration return the same Fe<sup>3+</sup>/ $\sum$ Fe ratios on experimental glasses to within 0.01–0.02 absolute across our calibration range.

Twelve natural MORB glasses were selected for micro-colorimetric analysis in this study, ten of which are common to the studies of CCL86 and/or BH05, as indicated in Table 1. Replicate analyses were

Fig. 2. Comparison of  $Fe^{3+}/\Sigma$ Fe ratios in glasses determined by Mössbauer-based XANES relative to ratios determined by wet chemical techniques or algorithms based on wet chemical data. The solid line shows 1:1 correspondence. (a) The open circles are calibration glasses from Cottrell et al. (2009), which provide the XANES calibration. Their Mössbauer-derived  $Fe^{3+}/\Sigma Fe$  ratios are plotted against the  $Fe^{3+}/\Sigma Fe$  ratios predicted by the Kress and Carmichael (1991) algorithm, which is based on microcolorimetric wet chemical data, for the set of  $\sum d_i X_i$ -P-T- $fO_2$  under which they were equilibrated. The dashed line shows a linear regression through these data (y=0.9782 x-0.008, R<sup>2</sup>=0.99). The solid diamonds are experimental basaltic glasses analyzed directly by both XANES and micro-colorimetry. Two glasses (AII\_-50 and AII\_-10) were created for this study. Of the other experimental glasses, two are calibration glasses from Cottrell et al. (2009) and six are from the study of Kress and Carmichael (1991) and were provided by V. Kress. Two of the Kress and Carmichael glasses have analyses via XANES plotted against micro-colorimetry performed in this study (solid black diamonds) and all six against the original micro-colorimetry results reported by Kress and Carmichael (1991) (shaded triangles). XANES results for natural basalts are plotted against micro-colorimetric analyses carried out in this study (solid black circles), the study of Christie et al. (1986) (crosses) and the direct titration wet chemical study of Bezos and Humler (2005) (shaded squares). The large shaded area represents the range of  $Fe^{3+}/\Sigma Fe$  values that are poorly quantified by XANES. (b) Expanded view of the open boxed area of (a). Black horizontal bars compare XANES measurements to direct analysis of basalt glass powders by Mössbauer spectroscopy. Boxed cross is USNM 113716. Overlain open symbols indicate replicate analyses of the same basalt pillow (bull's-eye, CH 33; white cross, CH 61-1; white bar, JDF C6-1).

performed on three of the basalts and in some cases analyses were performed on original powders from the study of CCL86. Unlike the experiments, micro-colorimetric determination of the natural basalts fell on average to lower Fe<sup>3+</sup>/ $\Sigma$ Fe ratios relative to XANES (0.120  $\pm$ 0.035 vs.  $0.159 \pm 0.007$ ), and spanned a range from more reduced values to more oxidized values (Fig. 2). Replicate analyses of sample CH 33-1 varied in Fe<sup>3+</sup>/ $\sum$ Fe ratio by up to 0.05 (absolute), outside of analytical error. For the samples in common with CCL86, FeO values measured in this study are systematically offset to lower FeO contents by an average of 0.3 wt.% FeO, and CCL86 do not report analyses of standards to provide a baseline for comparison. We observe no offset between the wet chemical determinations made by BH05 and microcolorimetry in this study, despite the differences in analytical procedure. Relative to XANES determinations, however, the Fe<sup>3+</sup>/  $\sum$ Fe ratios measured by BH05 are systematically lower by 0.04 absolute (25%) than measured by XANES, and those measured by CCL86 are lower by 0.09 absolute on average (56%). In these calculations, we have used total iron concentrations obtained for the glass on the Smithsonian microprobe. The greatest accuracy would be achieved by using total iron obtained on the bulk sample, although using the bulk values reported for Fe<sub>2</sub>O<sub>3</sub>\* (converted to FeO\*) by CCL86 does not nullify the discrepancy. For the samples from CCL86 analyzed in this study by micro-colorimetry, the average  $Fe^{3+}$  $\Sigma$ Fe=0.124, whereas CCL86 report 0.069, and substituting the CCL86 bulk values for FeO<sup>\*</sup> lowers the average  $Fe^{3+}/\Sigma$ Fe ratio determined in this study to only 0.107 (also see discussion by BH05).

# 3.3. Accuracy of XANES for the assessment of $Fe^{3+}/\sum$ Fe in MORB Part III: Factors that could lead to an offset between XANES and wet chemistry

We investigated the possibility that iron coordination changes during the slower quench rate of natural basalts might lead to shifts in the XANES spectra relative to rapidly-quenched experimental glasses. Pillow basalts quench extremely rapidly at the outer margin, at rates of >400–1000 °C/s (Xu and Zhang, 1999; Zhou et al., 2000), and quite slowly, 2–3 °C/s maximum, deep within the spherulitic-rich margin that borders the fully crystalline interior (Fig. 3). Numerous studies have shown that slower quench rates affect only the coordination geometry and not the oxidation state of iron (Dyar and Birnie, 1984; Dyar et al., 1987; Wilke et al., 2002). Basaltic pillows therefore provide a natural laboratory in which to investigate the effect of quench rate and coordination changes on the oxidation states extracted from XANES pre-edge centroids. Fig. 3 shows a doubly-polished wafer through a MORB pillow from the Carlsberg Ridge. We acquired three XANES spectra at each of three locations: within 1 mm of the pillow rim, at 8.8 mm depth where quench crystals begin to form, and at 16.3 mm depth at the boundary with the fully crystalline pillow interior. The temperature and quench rate of these three locations as a function of time vary by over three orders of magnitude, yet all three locations recorded the same centroid position, and hence Fe oxidation state, within error. We conclude that guench rate does not influence the energy of the pre-edge centroid and this cannot be the cause of the offset between XANES and wet chemistry.



**Fig. 3.** Analytical and model profiles through the glassy rim of a MORB pillow. (a) Transmitted light image of a double-side polished wafer of a MORB pillow (VG 5291, NMNH catalog number 115296-3), from the crystalline interior through a spherulite-rich zone and into the glassy outer margin that was in contact with seawater. The wafer is 111  $\mu$ m thick. The locations of XANES and FTIR analyses are indicated. The centroid energy positions and the Fe<sup>3+</sup>/ $\sum$  Fe ratios calculated from them, remain constant at all depths analyzed within the pillow, even while cooling rates vary by orders of magnitude. No variations in the total water content of the glass are observed. (b) Temperature modeled as a function of time (Carslaw and Jaeger, 1959) at the depths of the three analysis locations, with t = 0 corresponding to the time of pillow emplacement and thermal diffusivity (K) equal to 0.5 mm/s<sup>2</sup> (Hofmeister et al., 2009). The glassy rim cools to the glass transition in only a tenth of a second, whereas the spherulitic material takes minutes to reach the same temperature. Using K = 0.7 mm/s<sup>2</sup> (Bagdasarov and Dingwell, 1994) does not change the conclusions. (c) Cooling rate as a function of time for each of the three analysis points. The cooling rate at the pillow margin is >2000 K/s in the first tenth of a second following emplacement. The analysis point at 8.8 mm depth reaches a maximum cooling rate of about 9 K/s after 26 s. The deepest regions of glass never cool faster than about 2.5 K/s.



**Fig. 4.** Histogram showing the distribution of  $\text{Fe}^{3+}/\Sigma$  Fe ratios of MORB glasses measured in each of three independent studies. The black bars show the XANES results of this study, grey bars indicate the wet chemical (direct titration) determinations of Bezos and Humler (2005), and the white bars indicate the wet chemical (micro-colorimetry) determinations of Christie et al. (1986). Average  $\text{Fe}^{3+}/\Sigma$  Fe ratios for MORB glasses reported by each study are provided in the legend.

As a second check on the application of our experimentally-based calibration to natural samples, we chose two natural MORB that were particularly aphyric, and meticulously hand-picked tiny, optically transparent shards of the glass for direct Mössbauer analysis (Supplemental Fig. 3). The Fe<sup>3+</sup>/ $\Sigma$ Fe ratio obtained in this fashion was the same within error as that obtained using XANES (Fig. 2), strengthening the case that no bias should exist between spectra collected on the calibration glasses and natural samples.

There is an additional key factor that could lead to the offset between XANES and wet chemistry observed for natural samples, but not experiments. XANES inherently measures something different than wet chemistry because with XANES one has total certainty that only glass is being analyzed. Even with careful hand-picking, clusters of spherulitic or micro-phenocryst material are ubiquitous within MORB pillow glass. The presence of micro-phenocrysts, even at the very edge of the pillow, is particularly obvious when each sample is wafered to a nominal thickness of 100 µm (Fig. 3 and Supplemental Fig. 4) as was done for this study. While the dissolution of relatively Fe-free minerals like plagioclase should only have the minor effect of diluting the solution (and no effect if total iron is obtained on the bulk sample), dissolution of olivine could radically lower the  $Fe^{3+}/\Sigma$ Fe ratio determined by wet chemistry. Four replicate analyses of sample CH 33-1, which deviate in FeO outside of analytical uncertainty, can be modeled by the addition of olivine to the wet chemical dissolutions (Supplemental Fig. 4). We show that our wet chemical analyses of CH 33-1 include 3-12 vol.% olivine, and the analysis from CCL86 must include 15 vol.% olivine (Fo<sub>86</sub>). We conclude that olivine dissolution is nearly unavoidable when performing wet chemistry on MORB glasses, and that this is the primary reason for the offset between XANES and wet chemistry in natural samples.

A second major source of uncertainty in wet chemical determinations of Fe<sup>3+</sup>/ $\Sigma$ Fe derives from the need to measure both Fe<sup>2+</sup> and total Fe. For example, we measured FeO\* = 10.68 wt.% by microprobe for MORB glass 975-5-1. The FeO\* determined for the bulk sample from CCL86 using direct current plasma (DCP) mass spectrometry is 10.34 wt.%. These values are within 3% of one another and are certainly equivalent in terms of both the accuracy and precision of the microprobe and DCP. Sample 975-5-1 was determined to have FeO = 9.75 wt.% by micro-colorimetry in this study, which translates to Fe<sup>3+</sup>/ $\Sigma$ Fe = 0.125 using the Smithsonian probe value and 0.096 for the CCL86 DCP value. Small errors and biases in the measurement of total iron can therefore propagate into large uncertainty in the assessment of mantle oxidation state using wet chemical determinations, whereas XANES allows direct determination of  $Fe^{3+}/\sum Fe$  ratio with a single measurement.

Finally, we cannot rule out the possibility that some other redox couple absent in our experiments (e.g. S) affects the wet-chemical determinations of natural basalts, but not experimentally created ones.

## 3.4. $Fe^{3+}/\sum$ Fe ratio of MORB and its behavior during low-pressure fractionation

Our results show that the average  $\text{Fe}^{3+}/\sum$  Fe ratio of MORB glass, as determined by  $\mu$ XANES measurements on 103 samples from six major spreading centers, is 0.16  $\pm$  0.01. This average is 25% higher than that proposed by BH05 and 56% higher than that of CCL86 (Fig. 4).

As crystal fractionation proceeds and magmatic MgO decreases, we observe an increase in the  $Fe^{3+}/\sum Fe$  ratio consistent with the incompatibility of  $Fe^{3+}$  during olivine fractionation ( $D_{Fe_2O_3}\!=\!0).$  The effect is subtle because, even after 14% olivine fractionation (e.g., decrease in MgO from 10 to 6 wt.%), the  $Fe^{3+}/\sum$  Fe ratio only increases by 0.025. The CHEPR suite from the East Pacific rise provides a wide enough range in MgO to test the global relationship on a regional scale. The trend of this regional suite is also consistent with  $olivine \pm$ plagioclase  $\pm$  clinopyroxene fractionation and with the trend of the global array on Fig. 5a.  $Fe^{3+}/\Sigma$  Fe ratios also increase with moderately incompatible minor and trace element concentrations, consistent with low pressure fractional crystallization (Fig. 5b-c). Both CCL86 and BH05 observed broad increases in the  $\text{Fe}^{3+}/\sum$  Fe ratio with decreasing MgO on global scales, but these were not consistent with olivine fractionation at either global or local scales. We attribute our observations to the increased precision and accuracy afforded by XANES and the certainty that XANES measures only glass.

#### 4. Discussion

#### 4.1. The relationship of MORB $Fe^{3+}/\sum Fe$ ratios to mantle $fO_2$

Having established a relationship between fractionation and  $Fe^{3+}/$  $\sum$  Fe, it becomes possible to make inferences about the fO<sub>2</sub> of the MORB source. Kress and Carmichael (1991) provide regression coefficients for the empirical expression of Sack et al. (1980), relating the  $Fe^{3+}/\Sigma Fe$ ratio of basalt to  $fO_2$  at a specified temperature and for a specific composition. In order to apply these regression coefficients, the technique used to measure  $Fe^{3+}/\Sigma Fe$  must be unbiased relative to the micro-colorimetric technique employed by Kress and Carmichael to determine  $Fe^{3+}/\Sigma$ Fe ratios of their experiments (n=46). It is unknown, for example, whether the direct titration procedure of BH05 would return the same  $Fe^{3+}/\Sigma$ Fe ratios as micro-colorimetry if applied to the experiments of Kress and Carmichael. Moreover, in this study we have shown that micro-colorimetry may not apply equally to experimental and natural samples, suggesting that  $fO_2$  calculated with the Kress and Carmichael algorithm from micro-colorimetry data on natural glasses may not be accurate. In the present case, we have determined that our Mössbauer-based XANES calibration is only slightly offset (0.01 absolute difference in  $Fe^{3+}/\Sigma Fe$  ratios measured on unknowns) from the micro-colorimetric technique, and we therefore apply the Kress and Carmichael algorithm to our XANES data with reasonable confidence.

Referenced to 1200 °C and 1 atm, the average MORB from this study reflects an  $fO_2$  of  $0.10 \pm 0.18$  log units above the QFM buffer. At fixed oxygen content, the equilibrium  $fO_2$  of a decompressing silicate melt roughly parallels the QFM buffer (Kress and Carmichael, 1991; O'Neill et al., 2006), such that the Fe<sup>3+</sup>/ $\sum$  Fe ratio of MORB provides an accurate approximation for the  $fO_2$  of the MORB source. Selecting the most primitive glasses, for which we can reasonably assume that olivine is the only crystallizing phase (glasses with >8.5 wt.% MgO), we reconstruct primary mantle melts by incrementally adding equilibrium olivine (D<sup>olv</sup><sub>Fe<sup>3+</sup></sub> = 0) until the melts reach equilibrium



**Fig. 5.** (a) Plot of  $Fe^{3+}/\sum Fe$  ratios in MORB as a function of MgO concentration for all samples (white circles) and those from the CHEPR cruise, 8–14°N on the East Pacific rise (black circles). The  $Fe^{3+}/\sum Fe$  ratio is modeled to increase from ~0.15 to ~0.18 as MgO falls from ~10 to ~5 wt.% due to the exclusion of  $Fe^{3+}$  during closed system olivine-only (solid line) or olivine  $\pm$  plagioclase  $\pm$  clinopyroxene fractionation (dashed line, liquid line of descent modeled using Petrolog3 (Danyushevsky and Plechov, in press), using the mineral-melt model of Langmuir et al. (1992) and  $Fe^{3+}$  mineral/melt partition coefficients  $D_{olv} = 0$ ,  $D_{plg} = 0$ ,  $D_{cpx} = 0.45$  (Mallmann and O'Neill, 2009)). Also shown are plots of  $Fe^{3+}/\sum Fe$  ratios in MORB as a function of (b) TiO<sub>2</sub> and (c) Sc concentrations, with symbols as in (a). (d) Plot of  $Fe^{3+}/\sum Fe$  ratios in MORBs as a function of otal H<sub>2</sub>O concentration determined by FTIR on the same glass wafers. The solid black path shows the predicted effect of H<sub>2</sub> loss at 1 bar and QFM during degassing from a single MORB magma, assuming an initial melt H<sub>2</sub>O concentration of 0.5 wt.%, an initial  $Fe^{3+}/\sum Fe$  ratio of 0.157, and XH<sub>2</sub> (fluid) = 0.001 (see discussion in text). The dashed curve shows the predicted trend if a suite of MORB magmas with initially uniform  $Fe^{3+}/\sum Fe$  ratios of 0.157, but variable water concentrations, were to lose 1% of their dissolved H has H<sub>2</sub> gas. Such a high mole fraction of H<sub>2</sub> would require conditions significantly more reducing than QFM, so this curve represents an extreme upper limit (at QFM the trend would have a slope near zero and overlap the modeled degassing pathway).

with mantle olivine at Fo<sub>90</sub> (Supplemental Table 2). The Fe<sup>3+</sup>/ $\sum$  Fe ratios of regionally averaged primary melts average  $0.14 \pm 0.01$ , or  $\Delta$ QFM = -0.19  $\pm$  0.16 at 1 atm and 1200 °C. The primary melts can also be referenced to mantle source conditions at the pressure and temperature of last equilibration using the thermobarometer of Lee et al. (2009). At average pressures of just over 1 GPa and average temperatures just above 1300 °C, the *f*O<sub>2</sub> of the MORB source is 0.07  $\pm$  0.14 log units above QFM (Fig. 6).

The V/Sc ratio has also been developed as a proxy for oxygen fugacity, based on the observation that vanadium oxidation state, and therefore the crystal/melt partition coefficients for V, depends on  $fO_2$  under the range of conditions expected for Earth's interior (Canil, 1997). Variations in source  $fO_2$  may therefore be discernable using the V/Sc proxy because subsequent processes, such as crystallization, degassing, and mixing, are modeled to have only moderate effects on the V/Sc ratios of MORB magmas after they leave the mantle source (Lee et al., 2005). The V/Sc ratio of MORB in this study ranges from ~5 to 12, mirroring the global range represented in PetDB (Lehnert et al., 2000). Lee et al. (2005) modeled the expected V/Sc ratio for 10% melting of a peridotitic MORB source, such that a V/Sc ratio sof MORB from this study (>8 wt% MgO) are consistent with the global compilation of Lee et al. (2005), and Fe<sup>3+</sup>/ $\sum$ Fe ratios are positively correlated with V/Sc ratio

(Fig. 6) indicating a general fidelity between these two proxies for relatively anhydrous, low melt fraction conditions. The predicted  $fO_2$  from the V/Sc model (QFM - 1 to QFM + 0.25; Fig. 6b), however, is about a half log unit more reduced on average than the  $fO_2$  we model for primary MORB melts using Fe<sup>3+</sup>/ $\Sigma$ Fe ratios (QFM - 0.25 to QFM + 0.50; Fig. 6a). This discrepancy is subtle, representing a shift in Fe<sup>3+</sup>/ $\Sigma$ Fe of only 0.02 (absolute). As we discuss below, other explanations, such as modification of the Fe<sup>3+</sup>/ $\Sigma$ Fe ratio due to crystallization and degassing, do not apply to these primitive, minimally degassed samples.

#### 4.2. Do $Fe^{3+}/\sum$ Fe ratios reflect source $fO_2$ ?

The  $fO_2$  we calculate for the MORB source is within the high end of the range of  $fO_2$  recorded by abyssal spinel peridotites, which spans three orders of magnitude (Ballhaus, 1993; Bryndzia and Wood, 1990), and is within the range of  $fO_2$  inferred from whole rock wet chemical analyses of MORB pillows (Carmichael and Ghiorso, 1986). Our data, therefore, do not require an ascent or post-eruptive process to modify the Fe<sup>3+</sup>/ $\Sigma$ Fe ratio of MORB glass from the Fe<sup>3+</sup>/ $\Sigma$ Fe ratio of the primary magma. CCL86 observed glassy pillow rinds to be more reduced than pillow cores and this led them to postulate that dissociation of H<sub>2</sub>O and subsequent H<sub>2</sub> loss during degassing could lead to the oxidation of pillow interiors. To investigate this possibility, we analyzed a depth profile through a pillow, from the natural surface in contact with seawater to 16.3 mm depth in the pillow, acquiring both XANES and FTIR analyses at the same points. Neither the dissolved H<sub>2</sub>O concentration nor the oxidation state of iron in the glass changes as a function of distance from the pillow rim (Fig. 3). The homogeneity of the pillow glass on the scale of centimeters argues against a redox front passing through the cooling melt/glass, and the constancy of the dissolved H<sub>2</sub>O concentration argues against the loss and outward diffusion of hydrogen as the glass cools.

The potential for the dissociation of  $H_2O$ , or degassing in general, to drive oxidation in terrestrial magmatic systems is often overstated. One can write a reaction whereby a melt that precipitates magnetite



in the presence of molecular water becomes reduced by the outward migration of  $H_2$  gas, leaving an oxidized, magnetite-rich whole rock behind (Holloway, 2004):

$$BFe^{2+}O_{(melt)} + H_2O_{(melt)} = H_{2(fluid)} + Fe^{2+}O \cdot Fe_2^{3+}O_{3(magnetite)}$$
(1)

The system will be oxidized by this reaction if H<sub>2</sub> gas escapes the system completely. While striking examples of this phenomena have been shown for cases of low-temperature disequilibria (Castro et al., 2009), the occurrence of reaction (1) must be limited to low pressures in the presence of a strong redox gradient (e.g., lavas at the surface, Sato and Wright, 1966) because it requires the preferential migration of H<sub>2</sub>. The MORB glasses presented here erupted under hydrostatic pressure that was greater than the pressure of H<sub>2</sub>O saturation (Table 2), greatly limiting the possibility that degassing has driven oxidation by this process. Moreover, H speciation depends on  $fO_2$ . The H<sub>2</sub>/H<sub>2</sub>O ratio in the equilibrium fluid phase would be extremely low at the  $fO_2$ s relevant for MORB. For example, at 12 kb X<sub>H2</sub><0.0001 in a fluid at QFM and is << 0.001 even at 1 bar, limiting H<sub>2</sub>O dissociation to 0.01-0.1% (Frost and Ballhaus, 1998). Furthermore, this process is self-limiting because increasing  $fO_2$  will drive  $X_{H2}$  in the fluid progressively downwards. Even if H<sub>2</sub> comprised 1% of a degassing H<sub>2</sub>-H<sub>2</sub>O phase, dissociation of the 0.1-0.2 wt.% H<sub>2</sub>O in MORB would result in H<sub>2</sub> losses much less than 0.001 wt.%, which is insufficient to explain the dichotomy between pillow cores and rims observed by CCL86 (note: not observed in this study). Finally, as elegantly described by Carmichael (1991), the potential for H<sub>2</sub> loss to oxidize mantle-derived basaltic magmas must be very low, because nearly all the water in MORB is speciated as hydroxyl groups (OH<sup>-</sup>; Dixon et al., 1995; Stolper, 1982). Molecular water is therefore largely unavailable to participate in reaction (1).

Kelley and Cottrell (2009) observed that the Fe<sup>3+</sup>/ $\sum$ Fe ratios of basalts increases with dissolved H<sub>2</sub>O concentration, but were careful to note that H<sub>2</sub>O was unlikely to be the agent of oxidation in these magmas. Rather, the H<sub>2</sub>O content of magmas serves as a proxy for the proximity of magmatism to subduction zones, and traces the influence of slab-derived mass fluxes on the mantle sources of subduction-related magmas. The absence of a global correlation between dissolved H<sub>2</sub>O concentration and Fe<sup>3+</sup>/ $\sum$ Fe among MORB (Fig. 5d) is consistent with the thesis of Kelley and Cottrell (2009) that proximity to subduction, and not H<sub>2</sub>O itself, leads to oxidation of the mantle source.

We also rule out the possibility that  $CO_2$  outgassing can oxidize magmas (e.g., Mathez, 1984). At these  $fO_2$ s, carbon predominantly speciates as carbonate ( $CO_2^{3-}$ ) when dissolved in basaltic melts and as carbon dioxide ( $CO_2$ ) when partitioned into the vapor (Dixon et al.,

Fig. 6. (a) Histogram showing the distribution of modeled oxygen fugacities relative to the QFM buffer (Kress and Carmichael, 1991). Samples from the same region/segment/ dredge have been averaged. Grey bars relate the measured  $Fe^{3+}/\Sigma Fe$  ratios and compositions of MORB glasses at 1200 °C and 1 atm to oxygen fugacity. White bars relate modeled primary melt compositions (samples with measured MgO concentrations higher than 8.5 wt.% that are assumed to have only olivine on the liquidus, see text for details) to fO2 at 1 atm and 1200 °C. The addition of olivine shifts the primary melt  $fO_2$  downward by ~0.25 log units relative to the raw data. Black bars relate those same modeled primary melts to fO2 at the pressure and temperature of the accumulated aggregate melt, according to the thermobarometer of Lee et al. (2009), which shifts fO<sub>2</sub> to more oxidized values by about 0.25 log units because the average pressure of equilibration is estimated to be about 1 GPa. We estimate the fO<sub>2</sub> of the MORB mantle to be near the QFM buffer. (b) The Fe<sup>3+</sup>/ $\Sigma$ Fe ratios of MORB glasses plotted as a function of the vanadium to scandium ratio (V/Sc) measured on the same glass chips using LA-ICPMS. Symbols are as in Fig. 5, and samples with >8 wt.% MgO are indicated with a triangle. (c) The oxygen fugacity of the MORB source region inferred from V/Sc ratios at 10% melt fraction. The distribution of MORB lavas with 8-12 wt.% MgO is taken from Fig. 10 of Lee et al. (2005). The range of source fO<sub>2</sub> inferred from V/Sc ratios on samples with>8 wt.% MgO is similar to the range inferred from the  $Fe^{3+}/\Sigma$  Fe ratios of modeled primary melts.

### Table 2

Physical and analytical data for samples in this study.

$ \begin{array}{c} \mbox{Figs}(R) & \mbox{Figs}(R) $	Sample name	VG #	NMNH catalog number	Latitude (°N)	Longitude (°E)	Depth (mbsl)	FeO* (wt.%)	MgO (wt.%)	Na <sub>2</sub> O (wt.%)	$H_2O^a$	$Fe^{3+}/$ $\sum Fe$	$\sum d_i X_i^{\mathbf{b}}$	∆QFM	Sc (ppm)	V (ppm)
15584         -         -         2283         -         0.812         1073         7.37         2.41         0.14         0.16         0.12         1.15           C117-4         1182         117328-10         1228         -         10.86         252         2.00         1.07         0.16         0.15         0.23         -0.07         0.16         0.16         0.23         -0.07         0.16         0.12         -0.05         0.11         0.15         0.23         -0.07         0.16         0.12         -0.05         0.16         0.16         0.12         -0.05         0.11         0.16         0.12         -0.05         0.11         0.16         0.12         -0.05         0.11         0.16         0.12         -0.01         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11         0.11	Fast Pacific Rise														
D12-5         T/72         11732-100         22.55         -108.42         2800         4.00         8.03         2.42         0.12         0.13         0.23         0.06         34         200           CH 19-3         1137         11732-83         12.22         -103.00         2630         3.16         0.38         0.23         0.06         34         430           CH 21-1         -         -         12.08         -103.82         2680         1.15         7.24         7.03         0.04         0.16         0.03         2.44         0.17         0.15         0.23         3.44         451           CH 31-1         -         -         3.03         -103.87         2.05         1.02         7.04         2.76         0.24         0.10         2.3         3.04         0.11         0.13         0.10         0.23         0.04         1.03         3.04         0.11         0.10         0.23         0.04         1.03         3.04         0.11         0.10         0.23         0.04         1.03         0.01         0.01         0.02         0.01         0.23         0.01         0.01         0.02         0.01         0.02         0.01         0.02         0.01	T558-R1	_	_	22.83	-108.12	3129	10.73	7.37	2.41	0.14	0.160	0.19	0.17		
H142       11732       11732       1228       -10336       827       8.07       8.07       2.00       1.17       0.18       0.23       -0.05       4.4         C113-1       -       -       1278       -10334       2620       8.91       8.81       2.83       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.16       0.15       0.15       0.15       0.16       0.15       0.15       0.16       0.15       0.15       0.16       0.15       0.15       0.15       0.16       0.15       0.15       0.16       0.15       0.15       0.15       0.16       0.15       0.15	D12-5	7172	117328-100	22.55	-108.42	2800	9.40	8.53	2.42	0.12	0.163	0.22	0.16	36	315
CH 19-3       1187       1172       1288       12.82       -103.80       263       8.82       2.88       0.26       0.15       0.21       -0.05         CH 30-1       -       -       12.00       -103.82       2088       11.51       7.24       20.7       0.24       0.16       0.17       0.19       0.28       38       443         CH 30-1       -       -       12.00       -103.82       2088       11.51       7.24       20.7       0.24       0.01       0.02       0.20       0.01       0.01       0.20       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01       0.01	CH 17-4	11182	117328-53	12.86	-103.96	2632	8.76	8.07	2.60	0.17	0.150	0.23	-0.07		
CH 21-1       -       -       12.78       -103.49       202       8.73       8.82       2.38       0.26       0.16       0.10       0.21       9.84       445         CH 3-1       -       -       13.75       -104.16       260       11.16       6.33       330       0.44       0.166       0.22       0.24       44       330         CH 3-1       -       -       13.75       -104.09       271       10.05       6.11       273       0.10       0.16       0.23       0.34       0.16       0.22       0.34       0.16       0.23       0.34       0.16       0.22       0.24       44       330         CH 15-2       -       -       -       4.35       0.26       2.38       0.24       0.10       0.172       0.33       0.19       0.06       2.90       0.11       1373       1.11       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14	CH 19-3	1187	117328-58	12.82	-103.90	2630	9.14	8.93	2.58	0.15	0.158	0.23	0.06	34	290
H 30-1       -       -       12.00       -103.82       268       11.51       7.24       2.67       0.24       0.167       0.19       0.28       38       444         CH 6-1       11141       11728-19       13.65       -104.17       2710       10.62       0.20       0.44       0.166       0.22       0.01       4.33       314         CH 6+1       -       -       3.33       -104.22       280       10.72       7.64       2.76       0.30       0.16       0.23       0.10       0.25       0.10       0.23       0.10       45       344         CH 6+1       -       -       3.33       -104.22       280       10.70       7.64       2.76       0.23       0.16       0.23       0.10       45       344         CH 314       -       -       -       -       3.33       -104.18       1.55       2.56       0.21       0.30       1.75       1.80       1.50       0.27       0.30       0.16       0.30       0.30       1.75       1.65       0.26       0.16       0.22       0.16       0.21       0.21       0.21       0.21       0.21       0.21       0.15       0.24       1.16       1.16	CH 21-1	-	-	12.78	-103.94	2623	8.93	8.82	2.38	0.26	0.150	0.21	-0.05		
CH 5-1       -       -       -       13.75       -104.16       2560       11.16       6.32       3.39       0.44       0.166       0.22       0.02       4.4       330         CH 61-1       -       -       3.35       -102.89       271       10.05       8.18       273       0.17       0.18       0.22       0.18       0.23       0.04       0.16       0.22       0.04       4.3       314         CH 61-1       -       -       3.35       -102.89       273       10.05       8.13       273       0.07       0.18       0.23       0.02       0.18       0.03       0.04       0.05       9.9       280         CH 131       -       -       -       -       -       -       1.13       1.13       1.13       1.14       1.13       1.13       1.14       1.13       1.13       1.14       1.13       1.13       1.14       1.13       1.13       1.14       1.13       1.13       1.14       1.13       1.13       1.14       1.13       1.13       1.14       1.13       1.14       1.13       1.14       1.13       1.14       1.14       1.15       1.14       1.14       1.15       1.15       1.1	CH 30-1	-	-	12.09	-103.82	2685	11.51	7.24	2.67	0.24	0.167	0.19	0.28	38	445
CH-6-1       11141       11725-19       12.65       -104.17       2710       10.42       6.99       30.2       0.24       0.16       0.24       0.12       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.16       0.24       0.17       0.17       0.16       0.24       0.16       0.27       0.16       0.24       0.05       0.27       0.16       0.27       0.20       0.16       0.21       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.20       0.21       0.21       0.21       0.21       0.21       0.21       0.21       0.21       0.21       0.21       0.21       0.21       0.21 <th0.21< th=""> <th0.21< th="">       0.21&lt;</th0.21<></th0.21<>	CH 5-1	-	-	13.75	-104.16	2660	11.16	6.32	3.39	0.44	0.166	0.22	0.20	44	330
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	CH 6-1	11141	117328-19	13.65	-104.17	2710	10.42	6.99	3.02	0.34	0.162	0.22	0.14	43	314
C1 84-2       -       -       9.32       -10.422       2.88       10.72       7.74       2.76       2.0       0.100       0.23       0.10       45       304         C1 15-2       -       -       -       0.23       1.8       1.28       -10.88       2.00       9.81       7.56       2.38       0.13       0.13       0.15       0.16       0.23       0.20       3.9       2.90         SN11 13D-1       -       -       -       2.48       -11.42       2448       8.15       3.54       0.14       0.15       0.66       0.10       0.27       0.06       0.17       0.27       0.28       0.10       0.44       1.40       0.15       0.44       1.40       0.15       0.44       1.40       0.15       0.27       0.20       0.10       0.14       0.15       0.20       0.14       0.15       0.20       0.14       0.15       0.20       0.15       0.21       0.13       0.16       0.24       2.00       0.15       0.21       0.13       0.16       0.24       0.20       0.10       0.14       0.15       0.21       0.13       0.15       0.21       0.13       0.13       0.15       0.21       0.13       0.13 </td <td>CH 61-1</td> <td>-</td> <td>-</td> <td>8.36</td> <td>- 102.89</td> <td>2715</td> <td>10.05</td> <td>8.13</td> <td>2.73</td> <td>0.17</td> <td>0.163</td> <td>0.24</td> <td>0.12</td> <td>40</td> <td>318</td>	CH 61-1	-	-	8.36	- 102.89	2715	10.05	8.13	2.73	0.17	0.163	0.24	0.12	40	318
Li 15-2 L2.85 - 10.387 2.440 9.51 8.05 2.52 0.19 0.172 0.23 0.22 0.3 C1 33: 1 17328-11 17328-11 17378 - 11037 210 0.68 7.28 5.29 0.22 0.135 0.20 0.41 3.40 RAT 02-0120 9483 117361-11 14.59 - 10.433 2797 6.18 2.75 0.22 0.175 0.166 0.19 0.27 42 316 RAT 02-0120 9485 117361-11 14.70 - 10.433 2797 6.18 2.75 0.23 0.172 0.18 0.38 RSE 5-D0 44.61 115180-3 13.83 - 10.418 1458 1.06 6.28 2.85 0.33 0.172 0.18 0.38 Signatris Fracture Zare RAT 02 12-1 730 116999-1 8.38 - 10.418 1458 1.06 6.28 2.85 0.33 0.172 0.18 0.38 Signatris Fracture Zare RAT 02 12-1 730 116999-1 8.38 - 10.418 1458 1.06 6.28 2.85 0.33 0.172 0.18 0.38 Signatris Fracture Zare RAT 02 12-1 730 116999-1 8.38 - 10.418 1458 1.06 6.28 2.85 0.33 0.172 0.18 0.38 Signatris Fracture Zare RAT 02 12-1 730 116999-1 8.38 - 10.465 3020 8.90 8.70 2.78 0.20 0.195 0.20 0.14 Signatris Fracture Zare RAT 02 12-1 730 116999-1 2.26 6 - 55.49 2.370 8.54 8.99 2.35 0.22 0.149 0.20 -0.02 38 144 K 10-34 4056 115197-4 2.43 -95.55 2.750 9.118 7.08 2.33 0.40 0.166 10.36 38 305 KK73-D17-4 4056 115197-14 2.43 -95.55 2.750 9.19 9.00 2.10 1.14 0.146 0.16 0.36 38 305 KK73-D17-4 4056 115197-14 2.43 -95.55 2.750 9.19 9.00 2.21 0.15 0.00 0.154 0.16 0.36 38 305 KK73-D17-4 4056 115197-28 2.44 -94.97 7.50 9.28 9.92 2.16 0.12 0.16 0.16 0.16 34 38 305 KK73-D17-4 4056 115197-28 2.43 -95.55 2.750 9.24 9.72 2.15 0.13 0.144 0.18 -0.07 KK73-D17-3 4045 115197-28 2.44 -94.97 7.50 9.28 9.94 2.27 0.15 0.15 0.18 0.11 Main Oven 11300 1130 9.32 1.40 0.180 0.15 0.25 0.16 0.10 1.02 0.22 0.05 KK73-D17-4 4056 115197-28 2.43 -95.55 2.750 9.24 9.92 2.15 0.13 0.144 0.19 -0.16 54 1197 KK73-D17-4 4056 115197-28 2.44 -94.97 7.50 9.28 9.94 2.27 0.15 0.15 0.18 0.11 Main Oven 113 9.30 1.44 0.19 -0.16 54 1197 KK73-D17-4 52.55 115291-4 0.33 57.65 3066 7.73 8.96 1.69 0.150 0.22 -0.05 KK73-D17-2 4.555 115291-4 9.83 57.96 3066 7.73 8.95 1.73 0.154 0.15 0.18 0.11 Main Oven 11.55 0.13 0.144 0.19 -0.16 54 1197 KK73-D17-1 52.55 115291-4 9.83 57.96 3066 7.73 8.95 1.70 0.154 0.15 0.22 -0.05 KK73-D17-1 5	CH 84-2	-	-	9.32	- 104.22	2588	10.72	7.64	2.76	0.20	0.160	0.23	0.10	45	304
H 33 1       1103       11/2 24-116       -11/7       -00.34       2000       32.8       2.56       2.51       0.14       0.15       0.29       113       0.00       33       2.50         SN115 13D-1       -       -       -       -       12.47       2340       0.163       2.55       0.14       0.15       0.29       10.35       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16       0.16	CH 15-2	-	-	12.85	- 103.89	2640	9.51	8.06	2.56	0.19	0.172	0.23	0.28	20	200
Ants 1:02-1       -       -       -       -       -       -       11240       2:040       6:03       2:02       2:05       0:030       110       0:150       0:50       -       0:000       41       340         NATT 02-D122       9485       117361-114       14:59       -       10:033       3777       12:07       7:287       7:38       2:25       0:33       0.176       0:15       0:50       10:05       0:32       42       316         Siguitos Fracture Zone       -       -       13:33       -       -       10:34       3618       11:96       0:20       0:15       0:15       0:20       0:14       338       -       0:03:44       316       9:00       8:70       2:88       10:7       0:16       0:15       0:20       0:14       0:17       0:17       0:17       0:17       0:13       0:15       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17       0:17 <td>CH 33-1 EN112 12D 1</td> <td>11303</td> <td>11/328-110</td> <td>24.96</td> <td>- 103.80</td> <td>2900</td> <td>9.88</td> <td>7.00</td> <td>2.38</td> <td>0.22</td> <td>0.155</td> <td>0.19</td> <td>0.06</td> <td>39</td> <td>290</td>	CH 33-1 EN112 12D 1	11303	11/328-110	24.96	- 103.80	2900	9.88	7.00	2.38	0.22	0.155	0.19	0.06	39	290
Display         1/18         1/18         1/18         1/18         1/18         2/18         2/18         2/18         2/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18         0/18 <th0 18<="" th="">         0/18         0/18         &lt;</th0>	075 5 1	-	-	-24.00	- 112.45	2946	0.70	0.15	2.24	0.14	0.155	0.20	-0.05	41	240
RATE 02.0122         9485         117361-116         1470         -10433         5850         10.18         7.54         2.23         0.00         0.166         0.19         0.27         42         316           RKE 02.030         4451         115180-3         11838         -104.16         1458         1156         6.28         2.85         0.33         0.172         0.18         0.33         0.172         0.18         0.33         0.172         0.18         0.20         0.14         0.07         10.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.07         0.08         0.159         0.21         0.016         0.02         0.02         0.02         0.02         0.02         0.02         0.03         0.16         0.32         38         444           K18-3         417         11594-3         2.25         5.25         1159         0.18         0.016         0.03         38	RAIT 02-D120	9483	117361_114	14 59	-103.07 -104.33	2797	12.00	6.18	2.52	0.32	0.105	0.21	0.20	41	J40
RSE 3-D30         4451         115180-3         13.83         -104.18         1458         11.96         6.28         2.85         0.33         0.172         0.18         0.38         m         m           Signetinos Fracture Zone RATT 02 D1-1         7370         117361-8         8.36         -104.65         3020         8.80         8.70         2.78         0.20         0.159         0.21         0.07           VV74-D7-1         5211         115076-11         8.84         -103.84         3618         9.06         8.75         1.96         0.06         0.159         0.21         0.017           VV74-D7-1         5211         115199-2         8.40         -103.94         3618         9.06         8.75         1.96         0.06         0.159         0.21         0.017         0.02         0.14         0.19         0.02         0.157         0.22         0.15         0.13         0.44         0.19         0.02         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.16         0.15         0.18         0.15         0.18	RAIT 02-D120	9485	117361-114	14.55	-104.33	2850	10.18	7 54	2.63	0.52	0.176	0.15	0.30	42	316
Signicitors Francture Zone RAT 02 D 12-1         9377         117361-8         8.36         -10465         3020         8.00         8.70         2.78         197         0.05         0.20         0.114           SQD 3-1         7330         116699-2         8.40         -103.94         618         9.10         8.72         2.78         9.51         2.30         0.08         0.157         0.21         0.013           SQD 3-3         7331         116999-2         8.40         -103.94         3618         9.06         8.75         1.96         0.06         0.162         0.22         0.13           SQD 3-3         7331         115191-32         2.66         -95.49         2370         8.54         8.99         2.30         0.48         0.167         0.18         0.22         0.167         0.18         0.23         38         444           K18-21         4550         115197-14         2.43         -95.55         2750         9.19         9.90         2.12         0.14         0.16         0.33         395           KK78-D17-3         4965         115197-18         2.43         -95.55         2750         9.24         9.70         2.15         0.13         0.14         0.11 <td>RISE 3-D30</td> <td>4451</td> <td>115180-3</td> <td>13.83</td> <td>-104.18</td> <td>1458</td> <td>11.96</td> <td>6.28</td> <td>2.85</td> <td>0.33</td> <td>0.172</td> <td>0.18</td> <td>0.38</td> <td></td> <td>510</td>	RISE 3-D30	4451	115180-3	13.83	-104.18	1458	11.96	6.28	2.85	0.33	0.172	0.18	0.38		510
Signature Zone           Signature Zone           NATT 02 10-11         7330         116999-1         8.40         -103.64         3618         9.10         8.70         2.7         2.8         0.20         0.115         0.20         0.115         0.21         0.007           Signating Center           K           K10-34         3618         9.06         8.75         1.96         0.06         0.162         0.22         0.15           Colspan="6">Colspan="6">K           K10-34         4517         115194-3         2.75         -95.24         2700         8.54         8.99         2.35         0.20         0.16         0.35         38         385           KK75-D17.14         4956         115197.14         2.43         -9555         2.750         9.19         9.02         2.12         0.14         0.16         0.35         38         955           KK76-D17.14         4965         115197.74         2.43         -9555         2.750         9.19         9.02         2.12         0.14         0.16         0.36         38         956         3.750         9.28         9.90 </td <td></td>															
RAT 02 D 12-1       9377       117361-8       8.36       -104.65       3020       8.90       8.78       2.78       0.20       0.15       0.20       0.14         SQD 3-1       731       116099-2       8.40       -103.94       3618       9.06       8.75       1.96       0.06       0.157       0.21       0.07         TV74-D7-1       5211       115076-11       8.38       -103.68       3474       7.98       9.51       2.30       0.08       0.159       0.21       0.015         Calapages Spreading Center       -       -       5.42       2.70       8.54       8.99       2.35       0.22       0.149       0.02       -0.02       38       184         K 14-3       4151       15198-21       2.66       -95.43       3200       11.18       7.08       0.14       0.16       0.36       38       395         KK78-D17-4       4966       15197-74       2.43       -95.55       2.750       9.94       9.21       0.14       0.16       0.16       0.36       8.3       395         KK78-D17-3       4945       15197-3       2.43       -95.55       2.750       9.24       2.16       0.12       0.14       0.19	Siqueiros Fracture Zone														
SiQ D3-1       730       116999-1       8.40       -103.94       3618       9.10       8.78       1.97       0.06       0.157       0.21       0.077         SiQ D3-3       731       116999-2       8.40       -103.84       3618       9.06       8.75       1.29       0.06       0.159       0.21       0.13         Calogages Spreading Center       K       4.795       115194-3       2.75       -95.24       2700       8.54       8.99       2.35       0.22       0.149       0.20       -0.02       38       184         K 14-34       4517       115194-31       2.75       -95.52       2700       9.18       0.12       0.14       0.16       0.06       38       395         KK7R-D17-14       4966       115197-74       2.43       -95.55       2750       9.19       902       2.12       0.14       0.16       0.06       34       395       KK7R-D17-3       4465       115197-3       2.43       -95.55       2750       9.29       9.21       2.16       0.13       0.144       0.18       0.011         Indim Ocean       V       33-73       11520-2       1.64       -94.97       2750       9.58       9.04       2.27	RAIT 02 D 12-1	9377	117361-8	8.36	-104.65	3020	8.90	8.70	2.78	0.20	0.159	0.20	0.14		
TVY-4D7-1       5211       115076-11       8.38       -103.88       3474       7.98       9.51       2.30       0.08       0.159       0.21       0.13         Galapages Spreading Centr       K       103.34       3618       9.06       8.75       1.96       0.06       0.162       0.22       0.15         K       10-34       4795       115191-32       2.66       -9544       2370       8.54       8.99       2.35       0.22       0.168       0.16       0.36       38       395         K       14-3       4550       115198-21       2.60       -9543       3220       11.18       70.8       0.168       0.168       0.16       0.36       38       395         K       115197-14       2.43       -95.55       2750       9.19       9.90       2.12       0.141       0.168       0.16       0.13       0.144       0.18       -0.07         K       107-23       4945       115197-3       2.43       -95.55       2750       9.28       9.90       2.12       0.14       0.18       0.27       -0.16       34       922       2.15       0.13       0.144       0.18       -0.07       K       K       0.72	SIQ D3-1	7330	116999-1	8.40	-103.94	3618	9.10	8.78	1.97	0.06	0.157	0.21	0.07		
SIQ D3-3       731       116999-2       8.40       -103.94       3618       9.06       8.75       1.96       0.06       0.162       0.22       0.15         Calagages Spreading Center       K       10.34       4795       115191-32       2.66       -95.44       2370       8.54       8.99       2.35       0.22       0.149       0.20       -0.02       38       144         K 14-3       4517       115189-12       2.66       -95.44       2700       115       0.49       0.168       0.166       0.16       0.36       38       395         KK78-D17-14       4966       115197-14       2.43       -95.55       2750       9.19       9.90       2.12       0.14       0.14       0.16       0.90       6.56       384       0.45       0.12       0.141       0.19       -0.05       KK78-D17-3       4945       115197-3       2.43       -95.55       2750       9.28       9.04       2.27       0.140       0.18       0.101         Indian Ocean	TW74-D7-1	5211	115076-11	8.38	-103.68	3474	7.98	9.51	2.30	0.08	0.159	0.21	0.13		
Galapago Spreading Center         K         Viol         A         4795         115191-32         2.66         -95.49         2370         8.54         8.99         2.35         0.22         0.149         0.02         38         184           K 14-3         4550         115198-21         2.60         -95.43         3220         11.18         70.8         0.149         0.068         0.166         0.16         0.02         38         444           K 18-21         4550         115197.4         2.43         -9555         2750         919         9.02         2.12         0.14         0.168         0.169         0.02           KK78-D17-4         4966         115197-4         2.43         -9555         2750         9.24         9.76         2.16         0.12         0.14         0.18         -0.07           KK78-D17-3         4945         115200-2         1.64         -94.97         2750         9.28         9.92         2.16         0.12         0.141         0.19         -0.16           KK78-D17-3         4945         115200-2         1.64         -94.97         2750         9.28         9.92         2.16         0.12         0.141         0.19         -0.16         3	SIQ D3-3	7331	116999-2	8.40	-103.94	3618	9.06	8.75	1.96	0.06	0.162	0.22	0.15		
Galogogs Spreading Center K 10-34 4795 115191-32 2.66 -95.49 2370 8.54 8.99 2.35 0.22 0.149 0.20 -002 38 184 K 14-3 4517 115194-3 2.75 -95.24 2780 11.59 6.19 2.50 0.48 0.167 0.18 0.32 38 444 K 18-21 4550 115197-14 2.43 -95.55 2750 9.19 9.72 2.18 0.12 0.151 0.19 0.02 KK78-D17-14 4956 115197-4 2.43 -95.55 2750 9.19 9.90 2.21 0.14 0.146 0.19 -0.05 KK78-D17-3 4949 115197-3 2.43 -95.55 2750 9.28 9.92 2.16 0.12 0.144 0.18 -0.07 KK78-D17-3 4949 115197-3 2.43 -95.55 2750 9.28 9.92 2.16 0.12 0.144 0.18 -0.07 KK78-D17-3 4949 115197-3 2.43 -95.55 2750 9.28 9.92 2.16 0.12 0.144 0.18 -0.07 KK78-D17-3 4949 115197-3 2.43 -95.55 2750 9.28 9.92 2.10 0.154 0.18 0.11 <i>Indian Ocean</i> <i>V</i> 33-7.3 6647 117350-61 -49.03 124.00 2180 8.70 6.56 3.84 0.45 0.155 0.25 -0.04 34 222 V33-8.7, 6658 117350-72 -49.27 121.03 1930 7.72 7.39 3.21 0.33 0.144 0.19 -0.11 <i>S</i> 873-D2-244 523 11520-9 3.25 7.94 3146 7.71 9.65 1.76 0.151 0.22 -0.04 34 222 V33-8.77 6.58 117251-1 9.83 57.96 3066 7.64 9.67 1.69 0.150 0.22 -0.06 4 <i>S</i> 8779-D3-1 5253 115291-1 9.83 57.96 3066 7.78 9.72 1.68 0.159 0.22 -0.05 <i>S</i> 878-D3-12 5255 115291-2 9.83 57.96 3066 7.78 9.72 1.68 0.150 0.22 -0.05 <i>S</i> 878-D3-12 5255 115291-3 9.83 57.96 3066 7.78 9.93 1.76 0.150 0.22 -0.04 <i>S</i> 8779-D3-14 5254 115291-4 9.83 57.96 3066 7.78 9.93 1.76 0.150 0.22 -0.04 <i>S</i> 8779-D3-12 5255 115291-4 9.83 57.96 3066 7.78 9.85 1.73 0.156 0.21 0.006 <i>S</i> 878-D3-17 5256 115291-4 9.83 57.96 3066 7.78 9.85 1.73 0.156 0.21 0.006 <i>S</i> 878-D3-17 5256 115291-4 9.83 57.96 3066 7.78 9.85 1.73 0.156 0.21 0.006 <i>S</i> 878-D3-27 0.526 115291-4 9.83 57.96 3066 7.78 9.85 1.73 0.156 0.22 0.03 <i>S</i> 878-D3-16 528 115291-4 9.83 57.96 3066 7.78 9.85 1.73 0.156 0.21 0.006 <i>S</i> 878-D3-17 5256 115291-4 9.83 57.96 3066 7.78 9.85 1.73 0.156 0.21 0.006 <i>S</i> 878-D3-27 0.260 528 115291-4 9.83 57.96 3066 7.75 9.93 1.76 0.188 0.22 0.03 <i>S</i> 878-D3-260 528 115291-4 9.83 57.96 3066 7.75 9.93 1.76 0.158 0.22 0.03 <i>S</i> 878-D3-16 0.528 115291-4 9.83 57.96 3066 7.75 9.95 1.73 0.156 0.21 0.004 <i>S</i> 878-D3-17 5256 1.5271 4.93 5.50 5.62 6.75 3															
k 10-34       4/49       115191-32       2.26       -95.49       2.37       0.22       0.149       0.20       -0.00       38       184         K 14-3       4517       115194-3       2.75       -95.24       2780       11.59       6.19       2.50       0.48       0.168       0.16       0.32       38       444         K 18-21       4550       115198-21       2.60       -95.43       3220       11.18       7.08       2.33       0.49       0.168       0.16       0.32       38       444         K 18-21       4550       115197-3       2.43       -95.55       2750       9.19       9.92       2.12       0.14       0.16       0.16       0.07         K (78-D17-3       4945       115197-3       2.43       -95.55       2750       9.28       9.92       2.16       0.12       0.141       0.19       -0.01         K (78-D17-3       4945       115197-3       2.43       -95.55       2750       9.28       9.92       2.16       0.12       0.141       0.19       -0.01         K (78-D17-3       4945       115197-3       2.43       -95.5       2750       9.28       9.92       2.16       0.150       0.21	Galapagos Spreading Center					~~~~									
k 14-3       4917       11519-3       2.75       -95.24       2.80       11.59       6.19       2.30       0.48       0.168       0.16       0.18       0.23       38       395         KK78-D17-14       4956       115197-14       2.43       -95.55       2750       9.19       9.20       2.18       0.12       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.168       0.167       0.173       0.161       0.173       0.161       0.173       0.161       0.173       0.161       0.173       0.161       0.11       0.161       0.11       0.161       0.11       0.161       0.11       0.161       0.11       0.11       0.173       0.144       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11       0.11	K 10-34	4795	115191-32	2.66	- 95.49	2370	8.54	8.99	2.35	0.22	0.149	0.20	-0.02	38	184
N 16-21       4350       115189-21       2.00       -93.43       3.220       11.18       7.08       2.33       0.499       0.108       0.10       0.36       36       393         KK78-D17-14       4956       115197-14       2.43       -95.55       2750       9.19       9.72       2.18       0.12       0.144       0.18       -0.05         KK78-D17-3       49465       115197-3       2.43       -95.55       2750       9.24       9.76       2.15       0.13       0.144       0.18       -0.07         KK78-D17-3       49455       115197-3       2.43       -95.55       2750       9.28       9.92       2.16       0.12       0.144       0.18       -0.07         KK78-D17-3       49451       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.15       0.23       -0.04       34       222         V33-73       6667       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-73       0.151       0.19       0.21       0.045       0.22       0.04	K 14-3	4517	115194-3	2.75	- 95.24	2780	11.59	6.19	2.50	0.48	0.167	0.18	0.32	38	444
KN7a-D17-14       4930       115197-14       243       -95.33       2730       51.2       2.12       0.11       0.19       0.02         KK7a-D17-3       4966       115197-3       2.43       -95.55       2750       9.24       9.76       2.15       0.13       0.144       0.18       -0.07         KK7a-D17-3       4969       115197-3       2.43       -95.55       2750       9.28       9.92       2.12       0.14       0.19       -0.16         KK7a-D17-3       4945       115197-3       2.43       -95.55       2750       9.28       9.92       2.12       0.14       0.18       0.11         Indian Ocean       -       -       45.37       6667       11750-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-73       6667       11750-72       -49.27       121.03       1930       7.72       7.39       3.21       0.33       0.144       0.19       -0.16       34       197         RSR79-D3-1       5253       115291-3       9.82       57.96       3066       7.68       9.67       1.69       0.150 <t< td=""><td>K 18-21 VV79 D17 14</td><td>4550</td><td>115198-21</td><td>2.00</td><td>- 95.43</td><td>3220</td><td>0.10</td><td>7.08</td><td>2.33</td><td>0.49</td><td>0.108</td><td>0.10</td><td>0.30</td><td>38</td><td>395</td></t<>	K 18-21 VV79 D17 14	4550	115198-21	2.00	- 95.43	3220	0.10	7.08	2.33	0.49	0.108	0.10	0.30	38	395
NOTE 17-32       4969       115197-28       243       -95.55       2750       9.24       9.76       2.15       0.13       0.144       0.18       -0.07         KK78-D17-3       4969       115197-28       2.43       -95.55       2750       9.28       9.92       2.16       0.12       0.144       0.19       -0.16         KK78-D17-3       4964       115197-3       2.43       -95.55       2750       9.28       9.92       2.16       0.12       0.144       0.19       -0.16         KK78-D17-3       6647       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-73       66647       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-8-8.7       6658       115197-4       2.43       -9.85       1.69       0.150       0.22       -0.04       34       222         V33-92-14       5252       115291-3       9.83       57.96       3066       7.78       9.27       1.68       0.150       0.21	KK78-D17-14 KK78-D17-4	4950	115197-14	2.45	- 95.55	2750	9.19	9.72	2.10	0.12	0.131	0.19	_0.02		
KK78-D17-3       4945       115197-3       2.43       -95.55       2750       9.28       9.92       2.16       0.12       0.141       0.19       -0.16         KK78-D21-2       4523       115200-2       1.64       -94.97       2750       9.28       9.92       2.16       0.12       0.141       0.19       -0.16         Main Ocean       V33-7-3       6647       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-88.7       6658       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-88.7       6647       15291-2       9.82       57.96       3066       7.78       9.72       1.68       0.150       0.22       -0.04         RSR79-D3-1       5255       115291-3       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.22       0.00         RSR79-D3-12       5255       115291-3       9.83       57.96       3066       7.78       9.86       1.71       0.156	KK78-D17-32	4969	115197-28	2.43	- 95 55	2750	9.15	9.50	2.12	0.14	0.140	0.15	-0.03		
KK78-D21-2       4523       11520-2       1.64       -94.97       2750       9.58       9.04       2.27       0.15       0.154       0.18       0.11         Indian Ocean       V33-7-3       6647       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-8-8,7       6658       117350-72       -49.27       121.03       1930       7.72       7.73       3.21       0.33       0.144       0.19       -0.16       34       197         RSR1979-011-005       5291       115291-3       9.82       57.94       3146       7.71       9.65       1.76       0.151       0.22       -0.04         RSR79-D3-1       5253       115291-1       9.83       57.96       3066       7.78       9.72       1.68       0.150       0.21       -0.03         RSR79-D3-12       5255       115291-4       9.83       57.96       3066       7.78       9.71       0.156       0.22       0.00         RSR79-D3-60       5258       115291-5       9.83       57.96       3066       7.75       9.93       1.76       0.158       0.22	KK78-D17-3	4945	115197-3	2.43	- 95.55	2750	9.28	9.92	2.16	0.12	0.141	0.19	-0.16		
Indian Ocean V33-7-3 6647 117350-61 -49.03 124.00 2180 8.70 6.56 3.84 0.45 0.155 0.25 -0.04 34 222 V33-8-8,7 6658 117350-72 -49.27 121.03 1930 7.72 7.39 3.21 0.33 0.144 0.19 -0.11 RSR79-D2.44 5252 115290- 9.82 57.94 3146 7.71 9.65 1.76 0.151 0.22 -0.04 RSR79-D3-1 5253 115291-1 9.83 57.96 3066 7.78 9.72 1.68 0.159 0.22 -0.05 RSR79-D3-4 5254 115291-2 9.83 57.96 3066 7.78 9.86 1.69 0.150 0.21 -0.03 RSR79-D3-4 5254 115291-3 9.83 57.96 3066 7.78 9.86 1.69 0.150 0.21 -0.03 RSR79-D3-17 5256 115291-4 9.83 57.96 3066 7.78 9.86 1.69 0.150 0.21 -0.03 RSR79-D3-17 5256 115291-4 9.83 57.96 3066 7.78 9.86 1.71 0.156 0.21 0.06 RSR79-D3-27 5257 115291-5 9.83 57.96 3066 7.78 9.85 1.73 0.155 0.22 0.03 RSR79-D3-60 5258 115291-6 9.83 57.96 3066 7.78 9.93 1.76 0.158 0.22 0.09 RSR79-D3-60 5259 115291-7 9.83 57.96 3066 7.75 9.93 1.76 0.158 0.22 0.09 RSR79-D3-60 5259 115291-7 9.83 57.96 3066 7.75 9.93 1.76 0.158 0.22 0.09 RSR79-D3-60 5259 113716 -24.98 66.193 5150 8.42 7.37 4.18 0.160 0.23 0.08 ANTP111-1 591728.86 61.93 5150 8.42 7.37 4.18 0.160 0.23 0.08 ANTP111-1 591826.62 67.53 4990 9.07 7.08 3.95 0.162 0.22 0.13 ANTP111-1 6940 - 2.662 67.53 4990 9.07 7.08 3.95 0.154 0.23 0.006 CIRCE110-14 647 11698-128.86 61.93 5150 8.42 7.37 4.18 0.160 0.23 0.08 ANTP111-10 6770 11696-1 -28.86 61.93 5150 8.42 7.37 4.18 0.160 0.23 0.08 CIRCE110-12 6487 11698-1- 2.456 61.93 5150 8.42 7.37 4.18 0.160 0.23 0.08 CIRCE110-12 6487 11698-1 -2.662 67.53 4990 9.07 7.08 3.95 0.162 0.22 0.13 AII 93-5-6-12 6857 11698-1-2 -26.62 67.53 4990 9.07 7.58 3.81 0.151 0.24 -0.08 CIRCE110-12 647 11698-1 -2.82.66 1.93 5150 8.44 7.52 8.26 3.74 0.151 0.24 -0.08 CIRCE110-12 6487 11698-1 -2.82.66 1.93 5150 8.44 7.52 8.26 3.74 0.151 0.24 -0.08 CIRCE110-12 647 11698-1 -2.82.66 1.753 4990 9.07 7.58 3.81 0.159 0.22 0.01 ANTP111-10 6770 11696-1 -2.82.86 1.93 5150 8.41 7.52 7.55 3.87 0.159 0.25 0.03 KN162 D36-57 12399 11737-324 -52.749 11.711 4017 8.37 7.59 3.87 0.159 0.25 0.03 KN162 D36-57 12404 117373-237 -52.749 11.711 4017 8.57 7.19 3.91 0.	KK78-D21-2	4523	115200-2	1.64	-94.97	2750	9.58	9.04	2.27	0.15	0.154	0.18	0.11		
Indian Ocean         V33-7-3         6647         117350-61         -49.03         124.00         2180         8.70         6.56         3.84         0.45         0.155         0.25         -0.04         34         222           V33-8-8,7         6658         117350-72         -49.27         121.03         1930         7.72         7.39         3.21         0.33         0.144         0.19         -0.11         34         197           RSR197-011-005         5291         115290-3         -5.36         68.62         3566         1.058         6.83         3.10         0.33         0.144         0.19         -0.01           RSR79-D3-1         5253         115291-2         9.83         57.96         3066         7.78         9.72         1.68         0.159         0.22         -0.05           RSR79-D3-12         5255         115291-4         9.83         57.96         3066         7.78         9.85         1.71         0.156         0.21         -0.03           RSR79-D3-60         5258         115291-5         9.83         57.96         3066         7.73         9.31         1.76         0.158         0.22         0.09           RSR79-D3-60         5258         115291-															
V33-3       6647       117350-61       -49.03       124.00       2180       8.70       6.56       3.84       0.45       0.155       0.25       -0.04       34       222         V33-8-8.7       6658       117350-72       -49.27       121.03       1930       7.72       7.39       3.21       0.33       0.147       0.25       -0.16       34       197         RSR1979-011-005       5221       115290-       9.82       57.94       3146       7.71       9.65       1.76       0.151       0.22       -0.04         RSR79-D3-4       5254       115291-1       9.83       57.96       3066       7.78       9.72       1.68       0.150       0.22       -0.05         RSR79-D3-4       5254       115291-3       9.83       57.96       3066       7.78       9.72       1.68       0.150       0.21       -0.03         RSR79-D3-12       5255       115291-4       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.21       0.06         RSR79-D3-60       5258       115291-5       9.83       57.96       3066       7.68       9.85       1.73       0.151       0.22       0.04       36	Indian Ocean														
V33-8-8.7       6658       117350-72       -49.27       121.03       1930       7.72       7.39       3.21       0.33       0.147       0.25       -0.16       34       197         RSR1979-011-005       5291       115296-3       -5.36       68.62       3566       10.58       68.3       3.10       0.33       0.144       0.19       -0.11         RSR79-D2-44       5252       115291-1       9.83       57.96       3066       7.78       9.72       1.68       0.150       0.22       -0.04         RSR79-D3-1       5255       115291-3       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.21       -0.03         RSR79-D3-12       5255       115291-3       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.21       -0.03         RSR79-D3-60       5258       115291-5       9.83       57.96       3066       7.78       9.85       1.73       0.151       0.22       -0.04         SI Indian Ocean probe std.       3095       11521-7       9.83       57.96       3066       7.75       9.33       1.73       0.151       0.22       -0.04         SI Ind	V33-7-3	6647	117350-61	-49.03	124.00	2180	8.70	6.56	3.84	0.45	0.155	0.25	-0.04	34	222
RSR1979-011-005       5291       115296-3       -5.36       68.62       35.66       10.58       6.83       3.10       0.33       0.144       0.19      0.11         RSR79-D 2-44       5252       115290-       9.82       57.94       3146       7.71       9.65       1.76       0.151       0.22       -0.04         RSR79-D3-1       5233       115291-1       9.83       57.96       3066       7.78       9.72       1.68       0.150       0.22       -0.05         RSR79-D3-12       5255       115291-3       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.21       -0.03         RSR79-D3-17       5256       115291-5       9.83       57.96       3066       7.78       9.86       1.71       0.155       0.22       0.03         RSR79-D3-60       5258       115291-6       9.83       57.96       3066       7.63       9.73       1.73       0.151       0.22       -0.04         SI Indian Ocean probe std.       3095       113716       -24.98       69.99       3522       9.13       7.74       2.51       0.13       0.158       0.19       0.33       0.06         CIRCE110-1 <t< td=""><td>V33-8-8,7</td><td>6658</td><td>117350-72</td><td>-49.27</td><td>121.03</td><td>1930</td><td>7.72</td><td>7.39</td><td>3.21</td><td>0.33</td><td>0.147</td><td>0.25</td><td>-0.16</td><td>34</td><td>197</td></t<>	V33-8-8,7	6658	117350-72	-49.27	121.03	1930	7.72	7.39	3.21	0.33	0.147	0.25	-0.16	34	197
RSR79-D 2-44       522       115290-       9.82       57.94       3146       7.71       9.65       1.76       0.151       0.22       -0.04         RSR79-D3-1       5253       115291-1       9.83       57.96       3066       7.78       9.67       1.69       0.150       0.22       -0.05         RSR79-D3-4       5254       115291-2       9.83       57.96       3066       7.78       9.86       1.69       0.150       0.21       -0.03         RSR79-D3-12       5255       115291-4       9.83       57.96       3066       7.78       9.86       1.71       0.155       0.22       0.00         RSR79-D3-60       5258       115291-5       9.83       57.96       3066       7.75       9.93       1.76       0.158       0.22       0.00         RSR79-D3-60       5258       115291-7       9.83       57.96       3066       7.73       9.73       1.73       0.151       0.22       0.00         RSR79-D3-60       5259       115291-7       9.83       57.96       3066       7.73       9.74       2.51       0.13       0.158       0.22       0.00         RSR79-D3-60       5259       115291-7       9.83	RSR1979-011-005	5291	115296-3	- 5.36	68.62	3566	10.58	6.83	3.10	0.33	0.144	0.19	-0.11		
RSR79-D3-1       5253       115291-1       9.83       57.96       3066       7.64       9.67       1.69       0.150       0.22       -0.05         RSR79-D3-12       5254       115291-2       9.83       57.96       3066       7.78       9.72       1.68       0.159       0.22       0.10         RSR79-D3-12       5255       115291-3       9.83       57.96       3066       7.78       9.86       1.69       0.150       0.21       -0.03         RSR79-D3-17       5256       115291-5       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.21       0.06         RSR79-D3-60       5258       115291-5       9.83       57.96       3066       7.63       9.73       1.73       0.151       0.22       -0.04         SI Indian Ocean probe std.       3095       113716       -24.98       69.99       3522       9.13       7.74       2.51       0.13       0.158       0.22       -0.04         ANTP111-3       5917       -       -28.86       61.93       5150       8.42       7.37       4.18       0.160       0.23       0.06         CIRCE110-1       5940       -       -26.62	RSR79-D 2-44	5252	115290-	9.82	57.94	3146	7.71	9.65	1.76		0.151	0.22	-0.04		
KK79-D3-4       524       115291-2       9.83       57.96       3066       7.78       9.22       1.68       0.199       0.22       0.10         RSR79-D3-12       5255       115291-3       9.83       57.96       3066       7.73       9.86       1.69       0.150       0.21       -0.03         RSR79-D3-17       5256       115291-5       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.21       -0.03         RSR79-D3-60       5258       115291-6       9.83       57.96       3066       7.63       9.73       1.73       0.151       0.22       -0.04         SR79-D3-60       5259       115291-7       9.83       57.96       3066       7.63       9.73       1.73       0.151       0.22       -0.04         SI Indian Ocean probe std.       3095       113716       -24.98       69.99       3522       9.13       7.74       2.51       0.13       0.158       0.19       0.15       36       272         ANTP111-1       5917       -       -28.86       61.93       5150       8.41       7.27       4.18       0.160       0.23       0.06         CIRCE110-1       5940	RSR79-D3-1	5253	115291-1	9.83	57.96	3066	7.64	9.67	1.69		0.150	0.22	-0.05		
KN/9-D3-12       5255       115291-3       9.83       57.96       3066       7.73       9.86       1.69       0.150       0.21       -0.03         RSR79-D3-17       5256       115291-4       9.83       57.96       3066       7.78       9.86       1.71       0.156       0.21       0.00         RSR79-D3-27       5257       115291-5       9.83       57.96       3066       7.78       9.85       1.73       0.155       0.22       0.09         RSR79-D3-60       5258       115291-7       9.83       57.96       3066       7.63       9.73       1.73       0.151       0.22       -0.04         SI Indian Ocean probe std.       3097       115291-7       9.83       57.96       3066       7.63       9.73       1.73       0.151       0.22       -0.04         ANTP111-1       5917       -       -28.86       61.93       5150       8.64       7.33       4.25       0.159       0.23       0.06         CIRCE110-1       5918       -       -26.62       67.53       4990       9.07       7.08       3.95       0.162       0.22       0.13         CIRCE110-14       6847       116981-5       -26.62       67.53	RSR/9-D3-4	5254	115291-2	9.83	57.96	3066	7.78	9.72	1.68		0.159	0.22	0.10		
KKY2-D3-17       5256       115291-4       9.33       57.96       3066       7.78       9.86       1.71       0.156       0.21       0.006         KSR79-D3-60       5258       115291-5       9.83       57.96       3066       7.75       9.93       1.76       0.158       0.22       0.09         RSR79-D3-60       5259       115291-7       9.83       57.96       3066       7.68       9.85       1.73       0.151       0.22       -0.04         SI Indian Ocean probe std.       3095       113716       -24.98       69.99       3522       9.13       7.74       2.51       0.13       0.158       0.19       0.15       36       272         ANTP111-1       5917       -       -28.86       61.93       5150       8.42       7.37       4.18       0.160       0.23       0.08         CIRCE110-1       5940       -       -26.62       67.53       4990       8.65       7.54       3.77       0.154       0.23       -0.02         ANTP111-10       6770       116966-1       -28.86       61.93       5150       8.41       7.27       4.34       0.177       0.24       0.03         CIRCE110-14       6847       11	RSR/9-D3-12	5255	115291-3	9.83	57.96	3066	7.73	9.86	1.69		0.150	0.21	-0.03		
RSR79-D3-60       5237       112291-3       533       57.96       3066       7.75       9.93       1.75       0.135       0.122       0.035         RSR79-D 3-60       5259       115291-7       9.83       57.96       3066       7.63       9.73       1.73       0.151       0.22       -0.04         SI Indian Ocean probe std.       3095       113716       -24.98       69.99       3522       9.13       7.74       2.51       0.13       0.158       0.19       0.15       36       272         ANTP111-1       5917       -       -28.86       61.93       5150       8.42       7.37       4.18       0.160       0.23       0.08         ANTP111-3       5918       -       -26.62       67.53       4990       8.65       7.54       3.77       0.154       0.23       -0.02         ANTP111-10       6770       116966-1       -28.86       61.93       5150       8.41       7.27       4.34       0.177       0.24       0.33         CIRCE110-1       5940       -       -26.62       67.53       4990       8.53       7.45       3.81       0.159       0.24       0.05         CIRCE110-12B       6873       116981	KSK/9-D3-17	5256	115291-4	9.83	57.96	3066	7.78	9.86	1./1		0.156	0.21	0.06		
RSRP5D3-60       5259       112251-0       5.35       57.96       3060       7.13       3.35       1.73       0.151       0.22       -0.03         RSR7-0.0       5259       113716       -24.98       69.99       3522       9.13       7.74       2.51       0.13       0.158       0.19       0.15       36       272         ANTP111-1       5917       -       -28.86       61.93       5150       8.42       7.37       4.18       0.160       0.23       0.08         ANTP111-3       5918       -       -28.86       61.93       5150       8.64       7.33       4.25       0.159       0.23       0.06         CIRCE110-1       5940       -       -26.62       67.53       4990       8.65       7.54       3.77       0.154       0.23       -0.02         ANTP111-10       6770       116966-1       -28.86       61.93       5150       8.41       7.27       4.34       0.177       0.24       0.33         CIRCE110-14       6847       116981-5       -26.62       67.53       4990       8.53       7.45       3.81       0.159       0.24       0.05         CIRCE110-128       6873       116981-14	RSR79-D3-27 RSR79-D3-60	5257 5258	115291-5	9.83	57.96	3066	7.08	9.85	1.73		0.155	0.22	0.03		
SI Indian Ocean probe std.       3095       113716       -24.98       69.99       3522       9.13       7.74       2.51       0.13       0.158       0.12       0.081         ANTP111-1       5917       -       -28.86       61.93       5150       8.42       7.37       4.18       0.160       0.23       0.08         ANTP111-3       5918       -       -28.86       61.93       5150       8.64       7.33       4.25       0.159       0.23       0.06         CIRCE110-1       5940       -       -26.62       67.53       4990       8.65       7.54       3.77       0.154       0.23       -0.02         ANTP111-10       6770       116966-1       -28.86       61.93       5150       8.41       7.77       4.34       0.177       0.24       0.33         CIRCE110-14       6847       116981-5       -26.62       67.53       4990       9.07       7.08       3.95       0.151       0.24       -0.02         AII 93-5-6-12       6857       116981-12       -26.62       67.53       4990       8.53       7.45       3.81       0.159       0.24       0.05         CIRCE110-12B       6873       116981-14       -26.62	RSR79-D 3-60	5259	115291-0	9.83	57.96	3066	7.63	9.55	1.70		0.150	0.22	-0.03		
ANTP111-1       5917       -       -28.86       61.93       5150       8.42       7.37       4.18       0.160       0.23       0.08         ANTP111-3       5918       -       -28.86       61.93       5150       8.64       7.33       4.25       0.159       0.23       0.06         CIRCE110-1       5940       -       -26.62       67.53       4990       8.65       7.54       3.77       0.154       0.23       -0.02         ANTP111-10       6770       116966-1       -28.86       61.93       5150       8.41       7.27       4.34       0.177       0.24       0.33         CIRCE110-14       6847       116981-5       -26.62       67.53       4990       9.07       7.08       3.95       0.162       0.22       0.13         AII 93-5-6-12       6857       116981-12       -26.62       67.53       4990       8.59       7.48       3.80       0.153       0.22       -0.02         AII 93-5-6-20G       6878       116984-13       -27.60       65.84       4850       7.90       8.46       3.60       0.153       0.22       -0.01         KN162 D36-5       12399       117373-234       -52.749       11.711	SI Indian Ocean probe std.	3095	113716	-24.98	69.99	3522	9.13	7.74	2.51	0.13	0.158	0.19	0.15	36	272
ANTP111-3       5918       -       -28.86       61.93       5150       8.64       7.33       4.25       0.159       0.23       0.06         CIRCE110-1       5940       -       -26.62       67.53       4990       8.65       7.54       3.77       0.154       0.23       -0.02         ANTP111-10       6770       116966-1       -28.86       61.93       5150       8.41       7.27       4.34       0.177       0.24       0.33         CIRCE110-14       6847       116981-5       -26.62       67.53       4990       9.07       7.08       3.95       0.162       0.22       0.13         AII 93-5-6-12       6857       116981-12       -26.62       67.53       4990       8.59       7.48       3.81       0.159       0.24       -0.05         CIRCE110-12B       6873       116981-14       -26.62       67.53       4990       8.59       7.48       3.80       0.153       0.23       -0.02         AII 93-5-6-20G       6878       116984-13       -27.60       65.84       4850       7.90       8.46       3.60       0.153       0.22       -0.01         KN162 D36-5       12399       117373-237       -52.749       11.71	ANTP111-1	5917	_	-28.86	61.93	5150	8.42	7.37	4.18		0.160	0.23	0.08		
CIRCE110-1594026.6267.5349908.657.543.770.1540.23-0.02ANTP111-106770116966-1-28.8661.9351508.417.274.340.1770.240.33CIRCE110-146847116981-5-26.6267.5349909.077.083.950.1620.220.13All 93-5-6-126857116984-2-27.6065.8448507.528.263.740.1510.24-0.08CIRCE110-12B6873116981-14-26.6267.5349908.537.453.810.1590.240.05CIRCE110-12E6876116981-14-26.6267.5349908.597.483.800.1530.22-0.02All 93-5-6-20G6878116984-13-27.6065.8448507.908.463.600.1530.22-0.01KN162 D36-512399117373-234-52.74911.71140178.257.353.870.1590.250.03KN162 D36-2712404117373-237-52.74911.71140178.577.193.910.1620.250.08KN162 D49-512427117373-262-52.47912.86141937.947.164.270.1640.280.05KN162 D49-1612430117373-265-52.47912.86141938.157.114.190.1630.270.04	ANTP111-3	5918	-	-28.86	61.93	5150	8.64	7.33	4.25		0.159	0.23	0.06		
ANTP111-10       6770       116966-1       -28.86       61.93       5150       8.41       7.27       4.34       0.177       0.24       0.33         CIRCE110-14       6847       116981-5       -26.62       67.53       4990       9.07       7.08       3.95       0.162       0.22       0.13         AII 93-5-6-12       6857       116984-2       -27.60       65.84       4850       7.52       8.26       3.74       0.151       0.24       -0.08         CIRCE110-12B       6873       116981-12       -26.62       67.53       4990       8.53       7.45       3.81       0.159       0.24       0.05         CIRCE110-12E       6876       116981-14       -26.62       67.53       4990       8.59       7.48       3.80       0.153       0.22       -0.02         AII 93-5-6-20G       6878       116984-13       -27.60       65.84       4850       7.90       8.46       3.60       0.153       0.22       -0.01         KN162 D36-5       12399       117373-234       -52.749       11.711       4017       8.33       7.08       3.91       0.170       0.26       0.20         KN162 D36-27       12404       117373-237       -52.7	CIRCE110-1	5940	-	-26.62	67.53	4990	8.65	7.54	3.77		0.154	0.23	-0.02		
CIRCE110-14       6847       116981-5       -26.62       67.53       4990       9.07       7.08       3.95       0.162       0.22       0.13         AII 93-5-6-12       6857       116984-2       -27.60       65.84       4850       7.52       8.26       3.74       0.151       0.24       -0.08         CIRCE110-12B       6873       116981-12       -26.62       67.53       4990       8.53       7.45       3.81       0.159       0.24       0.05         CIRCE110-12E       6876       116981-14       -26.62       67.53       4990       8.59       7.48       3.80       0.153       0.23       -0.02         AII 93-5-6-20C       6878       116984-13       -27.60       65.84       4850       7.90       8.46       3.60       0.153       0.22       -0.01         KN162 D36-5       12399       117373-234       -52.749       11.711       4017       8.25       7.35       3.87       0.159       0.25       0.03         KN162 D36-17       12402       117373-237       -52.749       11.711       4017       8.37       7.19       3.91       0.162       0.25       0.08         KN162 D36-27       12404       117373-262 <t< td=""><td>ANTP111-10</td><td>6770</td><td>116966-1</td><td>-28.86</td><td>61.93</td><td>5150</td><td>8.41</td><td>7.27</td><td>4.34</td><td></td><td>0.177</td><td>0.24</td><td>0.33</td><td></td><td></td></t<>	ANTP111-10	6770	116966-1	-28.86	61.93	5150	8.41	7.27	4.34		0.177	0.24	0.33		
All 93-5-6-12       6857       116984-2       -27.60       65.84       4850       7.52       8.26       3.74       0.151       0.24       -0.08         CIRCE110-12B       6873       116981-12       -26.62       67.53       4990       8.53       7.45       3.81       0.159       0.24       0.05         CIRCE110-12E       6876       116981-14       -26.62       67.53       4990       8.59       7.48       3.80       0.153       0.23       -0.02         All 93-5-6-20G       6878       116984-13       -27.60       65.84       4850       7.90       8.46       3.60       0.153       0.22       -0.01         KN162 D36-5       12399       117373-234       -52.749       11.711       4017       8.25       7.35       3.87       0.159       0.25       0.03         KN162 D36-17       12402       117373-237       -52.749       11.711       4017       8.33       7.08       3.91       0.170       0.26       0.20         KN162 D36-27       12404       117373-239       -52.749       11.711       4017       8.57       7.19       3.91       0.162       0.25       0.08         KN162 D49-5       12427       117373-262	CIRCE110-14	6847	116981-5	-26.62	67.53	4990	9.07	7.08	3.95		0.162	0.22	0.13		
CIRCE110-12B       6873       116981-12       -26.62       67.53       4990       8.53       7.45       3.81       0.159       0.24       0.05         CIRCE110-12E       6876       116981-14       -26.62       67.53       4990       8.59       7.48       3.80       0.153       0.23       -0.02         AII 93-5-6-20G       6878       116984-13       -27.60       65.84       4850       7.90       8.46       3.60       0.153       0.22       -0.01         KN162 D36-5       12399       117373-234       -52.749       11.711       4017       8.25       7.35       3.87       0.159       0.25       0.03         KN162 D36-17       12402       117373-237       -52.749       11.711       4017       8.33       7.08       3.91       0.170       0.26       0.20         KN162 D36-27       12404       117373-239       -52.749       11.711       4017       8.57       7.19       3.91       0.162       0.25       0.08         KN162 D49-5       12427       117373-262       -52.479       12.861       4193       7.94       7.16       4.27       0.164       0.28       0.05         KN162 D49-16       12430       117373-265	AII 93-5-6-12	6857	116984-2	-27.60	65.84	4850	7.52	8.26	3.74		0.151	0.24	-0.08		
CIRCE110-12E $6876$ $116981-14$ $-26.62$ $67.53$ $4990$ $8.59$ $7.48$ $3.80$ $0.153$ $0.23$ $-0.02$ All 93-5-6-20G $6878$ $116984+13$ $-27.60$ $65.84$ $4850$ $7.90$ $8.46$ $3.60$ $0.153$ $0.22$ $-0.01$ KN162 D36-5 $12399$ $117373-234$ $-52.749$ $11.711$ $4017$ $8.25$ $7.35$ $3.87$ $0.159$ $0.25$ $0.03$ KN162 D36-17 $12402$ $117373-237$ $-52.749$ $11.711$ $4017$ $8.33$ $7.08$ $3.91$ $0.170$ $0.26$ $0.20$ KN162 D36-27 $12404$ $117373-239$ $-52.749$ $11.711$ $4017$ $8.57$ $7.19$ $3.91$ $0.162$ $0.25$ $0.08$ KN162 D49-5 $12427$ $117373-262$ $-52.479$ $12.861$ $4193$ $7.94$ $7.16$ $4.27$ $0.164$ $0.28$ $0.05$ KN162 D49-16 $12430$ $117373-265$ $-52.479$ $12.861$ $4193$ $8.15$ $7.11$ $4.19$ $0.163$ $0.27$ $0.04$	CIRCE110-12B	6873	116981-12	-26.62	67.53	4990	8.53	7.45	3.81		0.159	0.24	0.05		
All 93-5-6-20G       6878       116984-13       -27.60       65.84       4850       7.90       8.46       3.60       0.153       0.22       -0.01         KN162 D36-5       12399       117373-234       -52.749       11.711       4017       8.25       7.35       3.87       0.159       0.25       0.03         KN162 D36-17       12402       117373-237       -52.749       11.711       4017       8.33       7.08       3.91       0.170       0.26       0.20         KN162 D36-27       12404       117373-239       -52.749       11.711       4017       8.57       7.19       3.91       0.162       0.25       0.08         KN162 D36-27       12404       117373-262       -52.749       12.861       4193       7.94       7.16       4.27       0.164       0.28       0.05         KN162 D49-5       12427       117373-265       -52.479       12.861       4193       8.15       7.11       4.19       0.163       0.27       0.04         Juan de Fuca       14404       117373-265       -52.479       12.861       4193       8.15       7.11       4.19       0.163       0.27       0.04	CIRCE110-12E	6876	116981-14	-26.62	67.53	4990	8.59	7.48	3.80		0.153	0.23	-0.02		
KN162 D36-5       12399       11/3/3-234       -52.749       11.711       4017       8.25       7.35       3.87       0.159       0.25       0.03         KN162 D36-17       12402       117373-237       -52.749       11.711       4017       8.33       7.08       3.91       0.170       0.26       0.20         KN162 D36-27       12404       117373-239       -52.749       11.711       4017       8.57       7.19       3.91       0.162       0.25       0.08         KN162 D36-27       12404       117373-262       -52.749       11.861       4193       7.94       7.16       4.27       0.164       0.28       0.05         KN162 D49-5       12427       117373-265       -52.479       12.861       4193       8.15       7.11       4.19       0.163       0.27       0.04         Juan de Fuca       J	All 93-5-6-20G	6878	116984-13	-27.60	65.84	4850	7.90	8.46	3.60		0.153	0.22	-0.01		
KN162 D36-17       12402       11/373-237       -52.749       11.711       4017       8.33       7.08       3.91       0.170       0.26       0.20         KN162 D36-27       12404       117373-239       -52.749       11.711       4017       8.57       7.19       3.91       0.162       0.25       0.08         KN162 D49-5       12427       117373-262       -52.479       12.861       4193       7.94       7.16       4.27       0.164       0.28       0.05         KN162 D49-16       12430       117373-265       -52.479       12.861       4193       8.15       7.11       4.19       0.163       0.27       0.04         Juan de Fuca	KN162 D36-5	12399	117373-234	- 52.749	11.711	4017	8.25	7.35	3.87		0.159	0.25	0.03		
KN162 D36-27       12404       117373-239       - 52.749       11.711       4017       8.57       7.19       3.91       0.162       0.23       0.08         KN162 D49-5       12427       117373-262       - 52.479       12.861       4193       7.94       7.16       4.27       0.164       0.28       0.05         KN162 D49-16       12430       117373-265       - 52.479       12.861       4193       8.15       7.11       4.19       0.163       0.27       0.04         Juan de Fuca       Juan       Lasse	KN162 D36-17	12402	117373-237	- 52.749	11./11	4017	8.33	7.08	3.91		0.170	0.26	0.20		
KN162 D49-5       12427       117375-262 $-32.479$ 12.801       4193       7.94       7.16 $4.27$ $0.164$ $0.28$ $0.05$ KN162 D49-16       12430       117373-265 $-52.479$ 12.861       4193 $8.15$ $7.11$ $4.19$ $0.163$ $0.27$ $0.04$ Juan de Fuca	KN162 D30-27	12404	117272 262	- 52.749	11./11	4017	8.37 7.04	7.19	3.91		0.164	0.25	0.08		
Juan de Fuca	KN162 D49-5 KN162 D40 16	12427	117272 265	- 52,479	12.001	4195	7.94 0.15	7.10	4.27		0.104	0.28	0.05		
Juan de Fuca	KN102 D45-10	12430	117575-205	- 32.479	12.001	4155	0.15	7.11	4.19		0.105	0.27	0.04		
	luan de Fuca														
VG-2 6196 111240-1 44.67 - 130.33 2220 11.84 6.71 2.62 0.02 0.164 0.18 0.26 41 340	VG-2	6196	111240-1	44.67	- 130.33	2220	11.84	6.71	2,62	0.02	0.164	0.18	0.26	41	340
T469-24 47.95 - 129.10 2207 11.08 6.27 3.00 0.52 0.166 0.21 0.22 43 329	T469-24	-	-	47.95	- 129.10	2207	11.08	6.27	3.00	0.52	0.166	0.21	0.22	43	329
T464-03 48.00 - 129.07 2154 9.92 7.05 2.69 0.44 0.171 0.21 0.30 43 301	T464-03	_	-	48.00	- 129.07	2154	9.92	7.05	2.69	0.44	0.171	0.21	0.30	43	301
T471-08 47.92 - 129.11 2262 10.00 6.99 2.73 0.44 0.171 0.23 0.26 45 307	T471-08	-	-	47.92	- 129.11	2262	10.00	6.99	2.73	0.44	0.171	0.23	0.26	45	307
T469-22 – – 47.95 – 129.10 2197 9.90 7.13 2.71 0.43 0.167 0.24 0.19 45 312	T469-22	-	-	47.95	- 129.10	2197	9.90	7.13	2.71	0.43	0.167	0.24	0.19	45	312
T465-01 – – 47.97 – 129.06 2330 10.45 6.68 2.76 0.40 0.162 0.19 0.21 42 326	T465-01	-	-	47.97	-129.06	2330	10.45	6.68	2.76	0.40	0.162	0.19	0.21	42	326
T471-14         -         -         47.93         -         129.10         2227         10.07         7.12         2.76         0.40         0.165         0.23         0.17         44         306	T471-14	-	-	47.93	- 129.10	2227	10.07	7.12	2.76	0.40	0.165	0.23	0.17	44	306
T469-10         -         -         47.95         -         129.10         2206         10.53         6.90         2.82         0.39         0.167         0.22         0.23         45         318	T469-10	-	-	47.95	-129.10	2206	10.53	6.90	2.82	0.39	0.167	0.22	0.23	45	318
T471-23         -         -         47.93         -         129.10         2227         9.63         7.15         2.97         0.37         0.173         0.25         0.25         45         295	T471-23	-	-	47.93	-129.10	2227	9.63	7.15	2.97	0.37	0.173	0.25	0.25	45	295
<u>1463-04</u> – – <u>48.00</u> – <u>129.07</u> 2141 9.09 7.58 2.46 0.37 0.167 0.23 0.20 42 277	1463-04	-	-	48.00	- 129.07	2141	9.09	7.58	2.46	0.37	0.167	0.23	0.20	42	277

Sample name	VG #	NMNH catalog	Latitude (°N)	Longitude	Depth (mbsl)	FeO*	MgO (wt %)	Na <sub>2</sub> O (wt %)	$H_2O^a$	$Fe^{3+}/\Sigma$ Fe	$\sum d_i X_i^{\mathbf{b}}$	ΔQFM	Sc (ppm)	V (ppm)
		number	(11)	( 1)	(111051)	(******)	(******)	(******)					(PPiii)	(Ppiii)
Juan de Fuca														
JDF C2-1	7455	117354-40	44.73	- 130.35	2200	14.31	4.76	3.15	0.160	0.13	0.30			
JDF C6-1	7456	117354-41	44.64	-130.37	2240	11.57	7.22	2.33	0.22	0.163	0.17	0.27	38	404
JDF D11-2	7454	117354-68	44.98	- 130.33	1550	10.26	7.60	2.80	0.22	0.167	0.24	0.19	47	255
JDF D5-2	7440	117354-54	44.82	- 130.29	2260	10.79	7.34	2.23	0.20	0.159	0.20	0.15	43	311
JDFD2	7432	117354-46	44.61	- 130.41	2240	12.22	6.50	2.62	0.45	0.167	0.17	0.34	43	339
Mid-Atlantic Ridge														
MAPCO CH98 DR12	5494	115388-2	30.25	-41.70	4200	10.61	8.16	2.86		0.152	0.19	0.05	38	265
AII 92-29-1F	P24	113707-2	23.03	-45.03	2889	10.06	7.26	3.14		0.163	0.21	0.18	36	296
2πD47-1	8488		15.90	-46.60	3760	9.48	7.87	3.07	0.33	0.159	0.22	0.11	37	274
523-1	3384	113762	36.83	- 33.25	2726	9.30	8.45	2.29		0.152	0.22	-0.03	36	228
523-2-1	3385	113763	36.83	- 33 25	2743	9.84	8 50	2.64	0.50	0 143	0.20	-0.14	38	268
ALV 527 1-1	3403	113811-	36.81	- 33 26	2707	9.01	9.48	2.00	0.14	0 128	0.19	-0.41	36	213
TR138 11D-1	9966	116932-7	52.01	- 29.95	3800	9.93	7 37	2.00	0.23	0.120	0.15	0.05	36	321
TR138 2D-2	9277	116926-2	47.05	-27.35	2975	8 21	915	2.02	0.25	0.133	0.20	-0.15	32	203
TR138 9D-4	9960	-	51 56	- 29.92	3710	10.06	7.01	2.57	0.25	0.145	0.20	-0.15	40	301
TK 2-10	-	_	26.27	- 44 73	3950	9.25	9.27	2.60	0.25	0.169	0.15	0.13	35	297
TK 3-1			26.27	- 44.85	3600	9.23	7.57	2.02		0.100	0.15	0.10	37	237
FN026 10D-3g			71.80	_ 1 30	2000	0.68	7.50	2.55	0.76	0.155	0.22	0.10	57	275
TP110 6D 1	7029	116020 1	25.94	24.19	2300	0.76	7.55	2.44	0.70	0.150	0.22	0.06		
TR110 CD 4	7030	116020-1	25.04	- 34.18	2450	10.49	7.56	2.15	0.29	0.150	0.22	- 0.00	20	205
ENI25 2D 4	7059	110920-2	53.64	- 54.10	2450	10.40	7.05	2.24	0.54	0.159	0.20	0.15	20 41	200
EN25 2D-4	6925	-	54.70	- 55.22	2075	11.25	7.40	2.10	0.14	0.105	0.17	0.29	41	250
EN25 0D-3	0400	-	57.14	- 33.42	760	12.20	0.91	2.07	0.30	0.155	0.15	0.19	45	300
211D43	8482	-	13.50	-45.00	3770	9.96	7.71	2.89	0.54	0.140	0.23	-0.13	32	280
MAPCO CH98 DRTT	5490	115387-2	30.70	-41.83	3640	10.30	8.67	2.53	0.23	0.154	0.19	0.09	37	298
AII107-D20-1	/298	-	- 33.72	- 14.25	1489	7.47	9.96	1.65		0.143	0.20	-0.13		
AII107-D20-2	7299	-	-33.72	- 14.25	1489	7.55	9.84	1.66		0.154	0.21	0.03		
AII107-D20-3	7300	-	-33.72	- 14.25	1489	7.48	10.07	1.64		0.146	0.20	-0.09		
AII107-D20-6	7301	-	-33.72	-14.25	1489	7.61	9.89	1.64		0.150	0.20	-0.02		
LYN73-D7	962	113181-	70.17	15.28	1097	10.03	8.00	1.72		0.156	0.20	0.16		
LYN73-D7-001	G65	-	70.17	-15.28	1097	9.97	7.94	1.72		0.161	0.21	-0.10		
LYN73-D7-002	G66	-	70.17	-15.28	1097	10.07	7.96	1.68		0.160	0.20	0.02		
LYN73-D30-012	G76	-	70.57	-14.69	1070	9.26	8.58	1.70		0.149	0.23	0.08		
LYN73-D30-014	G78	-	70.57	- 14.69	1070	9.05	8.47	1.70		0.157	0.24	0.14		
American-Antarctic ridge														
VLC5-39-10	5842	115462-5	- 58.65	- 16.21	3822	8.89	7.72	3.44		0.156	0.23	0.02		
VLC5-39-12	5844	115462-7	- 58.65	- 16.21	3822	8.93	7.77	3.42		0.157	0.23	0.04		
VLC5-39-13	5845	115462-8	- 58.65	- 16.21	3822	9.39	6.94	3.70		0.161	0.23	0.10		
VLC5-39-17	5846	115462-9	- 58.65	- 16.21	3822	9.03	6.96	3.54		0.162	0.25	0.07		
VLC5-39-20	5848	115462-11	- 58.65	- 16.21	3822	8,93	6.84	3.54		0.144	0.25	-0.23		
VLC5-39-28	5851	115462-13	- 58.65	- 16.21	3822	8.95	7.63	3.42		0.162	0.23	0.12		
												2		

Additional major element data and published data sources are available in the electronic supplement.

<sup>a</sup> H<sub>2</sub>O data and major elements on the 10 samples from Endeavor provided by P. Michael and J. Gill (pers. comm). Major element data for T558-R1 from D. Clague (pers. comm.) <sup>b</sup>  $\sum d_i X_i$  parameterizes basalt composition (sum of coefficients (*di*) multiplied by oxide mole fractions (*Xi*), as defined in Kress and Carmichael, 1991).

1995; Stolper and Holloway, 1988). Carbon dioxide degassing is therefore redox-neutral because the degassing reaction

$$CO_3^{2-}(melt) \rightarrow CO_{2(vapor)} + O_{(melt)}^{2-}$$
(2)

does not change the charge balance in the melt. More extensive discussion of the difficulty of changing magmatic redox through C-O-H degassing can be found in Ballhaus (1993), Candela (1986), and Frost and Ballhaus (1998). Sulfur does have a demonstrable theoretical and empirical capability to reduce or oxidize magmas through SO<sub>2</sub> degassing (Anderson and Wright, 1972; Gerlach, 1993; Sakai et al., 1982). Mid-ocean ridge basalts, however, are usually sulfide saturated and rarely reach saturation with SO<sub>2</sub> vapor (Mathez, 1976) and the complexities of S degassing are thus inconsequential to normal MORB systems.

#### 4.3. The ferric iron content of the mantle

The Fe<sup>3+</sup>/ $\sum$ Fe ratios of basalt glasses measured in this study can be converted to Fe<sub>2</sub>O<sub>3</sub> and FeO using electron microprobe measurements of total iron (FeO\*, Table 2). It would be inappropriate to use FeO\* values from bulk rocks because, unlike in the case of wet chemistry, our  $Fe^{3+}/\sum Fe$  ratios are measured directly on the glass. The average Fe<sub>2</sub>O<sub>3</sub> of our MORB samples is 1.67 wt.%, which decreases to 1.38 wt.% for modeled MORB primary melts. For partial melts of the mantle, there is a range of Fe<sup>3+</sup> bulk partition coefficients and mantle  $Fe_2O_3$  contents ( $C_0$ ) that would satisfy this liquid concentration (Fig. 7). Based on Mössbauer analyses of mineral separates from continental xenoliths, Canil et al. (1994) inferred the Fe<sub>2</sub>O<sub>3</sub> content of the primitive mantle to be 0.3 wt.%, and suggested that depleted oceanic peridotite might have <0.1 wt.%. The Fe<sub>2</sub>O<sub>3</sub> contents for MORB proposed in this study (and BH05), however, are consistent with 0.2-0.3 wt.% Fe<sub>2</sub>O<sub>3</sub> in the MORB mantle for a typically quoted bulk  $D_{Fe_2O_3} = 0.1$ . Yet, recent, experimental determinations of crystal/melt partitioning of Fe<sup>3+</sup> indicate that bulk mantle/melt Ds for Fe<sup>3+</sup> may be significantly higher. If we apply the experimentally determined partition coefficients of Mallmann and O'Neill (2009) to a fertile mantle mode with 55% olivine, 25% orthopyroxene, 18% clinopyroxene, and 2% spinel, we calculate a bulk  $D_{Fe_2O_3} = 0.22$ . With this higher bulk D, the inferred Fe<sub>2</sub>O<sub>3</sub> content of the MORB mantle shifts even higher, to 0.35-0.4 wt.% Fe<sub>2</sub>O<sub>3</sub> (Fig. 8). Below we consider the possibility that the construct of a single partition coefficient for Fe<sup>3+</sup> may be inappropriate because Fe<sup>3+</sup> cannot be treated strictly as a conserved incompatible element during melting. Regardless, a



**Fig. 7.** Plot of Fe<sub>2</sub>O<sub>3</sub> concentrations of MORB glasses, calculated from Fe<sup>3+</sup>/ $\sum$ Fe ratios measured in this study using determinations of FeO<sup>\*</sup> (total iron) from microprobe, as a function of the modeled Fe<sub>2</sub>O<sub>3</sub> concentration in the MORB source (peridotite) using a fractional melting model. The bold dashed line assumes a bulk ferric iron partition coefficient (D<sup>Fe3+</sup>) of 0.1 (Canil et al., 1994) and 10% melt fraction (F). Lighter dashed lines delineate the envelope of melt fractions estimated for global MORBs, from F = 8–20% (Klein and Langmuir, 1987). The solid bold line assumes D<sup>Fe<sup>3+</sup></sup> = 0.22 (calculated from Mallmann and O'Neill, 2009; see text for details) and F = 10%, with lighter solid lines indicating the melt fraction envelope for F = 8–20%. Primary melts modeled in this study indicate that the Fe<sub>2</sub>O<sub>3</sub> content of peridotite appropriate for the MORB source is between 0.2 and 0.35 wt.%, depending on the bulk partition coefficient of ferric iron.

relatively high ferric iron content for the MORB mantle is an inescapable consequence of these data.

#### 4.4. Controls on mantle fO<sub>2</sub>

The behavior of ferric iron and the evolution of mantle fO<sub>2</sub> during mantle melting are nuanced. Crystal chemistry exerts considerable control on the ferric iron contents of minerals, such that significant ferric iron can be incorporated in minerals even under reducing conditions (Frost et al., 2004; McCanta et al., 2004). Upon melting, the input of Fe<sup>3+</sup> and Fe<sup>2+</sup> to the melt will be governed by crystal/melt partitioning; however, the subsequent ratio of oxidized to reduced iron in the melt will reflect the prevailing system fO<sub>2</sub>, which is itself controlled by the solid phase assemblage. For example, the ferric iron content of spinels partially defines the intrinsic  $fO_2$  of the system and is used to record the  $fO_2$  of the system, but is also likely to decouple from the fO<sub>2</sub> of the system during melting due to crystal chemical effects commensurate with Fe<sup>3+</sup> extraction (Canil and O'Neill, 1996; Canil et al., 1994; Frost and McCammon, 2008; Woodland et al., 2006). Likewise, carbon present in the mantle has the potential to buffer melting through the reaction  $C + O_2 \leftrightarrow CO_2$ , and therefore define the  $fO_2$ , but the stability of graphite is itself controlled by  $fO_2$  (Ballhaus, 1993; Blundy et al., 1991; Dasgupta and Hirschmann, 2010). It is therefore difficult to deconvolve the factors controlling  $fO_2$  from those responding to it.

If Fe<sup>3+</sup> behaves incompatibly during peridotite melting and mantle  $fO_2$  is not buffered, we would expect to find a positive correlation between the Fe<sub>2</sub>O<sub>3</sub>(8) and other incompatible elements such as Na<sub>2</sub>O(8), a canonical proxy for the extent of melting (where the (8) denotes concentrations corrected for fractional crystallization to 8 wt.% MgO, Klein and Langmuir, 1987). Fe<sub>2</sub>O<sub>3</sub>(8), however, shows a very weak negative association, if any, with Na<sub>2</sub>O(8) consistent with the results of BH05. This observation holds on the global scale when samples from the same dredge or segment are locally averaged to prevent sampling bias (R<sup>2</sup> = 0.18) and when calculated primary melts are considered (R<sup>2</sup> = 0.03) (Fig. 8). We offer two potential explanations for this observation: either the bulk partition coefficient of ferric iron is higher than previously assumed, and potentially variable with



**Fig. 8.** Plot of  $Fe_2O_3(8)$  as a function of  $Na_2O(8)$ . Oxide concentrations of MORB glasses were corrected for fractionation to 8 wt% MgO ( $Na_2O(8)$ , Klein and Langmuir (1987);  $Fe_2O_3(8) = Fe_2O_3 - 0.2074 \cdot (8 - MgO)$ ). Samples with measured MgO>8.5 wt% first had olivine subtracted to 8.5 wt% MgO and were then corrected for olivine and plagioclase fractionation to 8.0 wt% MgO. A very weak negative correlation is present whether looking at (a) all samples or (b) regional and dredge averages. No correlation is observed among the modeled primary melts (b, inset). The expected correlations for incompatible behavior during melting are shown for an array of model assumptions about the partition coefficient of ferric iron, the extent of melting, and the initial ferric iron content of the mantle.

mantle temperature, or mantle melting is buffered at nearly constant  $fO_2$ .

The slope of the expected correlation depends on the relative difference between the bulk partition coefficient of Na (0.02-0.04, Langmuir et al., 1992) and that of  $Fe^{3+}$ . If  $D_{Fe_2O_2} = 0.1$ , as suggested by Canil et al. (1994) (based in part on the MORB  $Fe^{3+}/\Sigma Fe$  ratios of CCL86), the modeled slope should be observable within the error of our measurements. The modeled slope would be close to zero, however, if D<sub>Fe2O3</sub> = 0.22 (Mallmann and O'Neill, 2009). In combination with a slightly heterogeneous source ( $Fe_2O_3 = 0.2-0.4$  wt.%), this would be consistent with these data (Fig. 8). If the partition coefficient of Fe<sup>3+</sup> additionally varies by a factor of 1.5 to 2 over a reasonable range of mantle potential temperatures, similar to other cations (e.g. Pertermann and Hirschmann, 2003; Tuff and Gibson, 2007), then we would expect Fe<sup>3+</sup> concentrations to vary as a function of mantle potential temperature, resulting in a negative trend on Fig. 8. The partition coefficient of Na is much lower than that of Fe<sup>3+</sup>, and responds much more strongly to pressure than temperature (e.g. Blundy et al., 1995), such that variations in the bulk partition coefficient of Na will not affect the trends on Fig. 8. At low  $Na_2O(8)$ ,

where we expect high melt fractions from relatively hot mantle,  $Fe_2O_3$ (8) would be elevated due to melting with a lower bulk  $Fe^{3+}$  partition coefficient. At high Na<sub>2</sub>O(8) (low melt fractions, relatively cold mantle),  $Fe_2O_3(8)$  would be depressed due to melting with a higher bulk  $Fe^{3+}$  partition coefficient. Melting curves on Fig. 8 depict this variable partition coefficient model and match the data reasonably well. To fully test this hypothesis, we require greater knowledge of the mantle/melt partition coefficient for  $Fe^{3+}$  and more regional sample suites with well-defined liquid lines of descent that offer greater accuracy in determination of Na<sub>2</sub>O(8) and  $Fe_2O_3(8)$ .

The other possibility is that  $fO_2$  is buffered by a reaction during melting such that incompatible ferric iron entering the melt is reduced to ferrous iron commensurate with the oxidation of some other phase. BH05 proposed that graphite could serve as the reductant; however, the proportions of ferric iron measured in both this study and the study of Bezos and Humler are far too oxidized for graphite to be stable in the MORB source (see Fig. 12 in Ballhaus (1993), for example). The carbon–carbon dioxide buffer cannot buffer melting to produce MORB.

Sulfur, by contrast, could serve as a reductant up to QFM + 1.5 (Jugo et al., 2010) via the reaction

$$S^{2-} + 8Fe^{3+} \leftrightarrow S^{6+} + 8Fe^{2+}$$
 (3)

In this scenario, sulfide in the mantle would be consumed during melting while reducing ferric iron in the melt. Critically, this reaction would prevent  $fO_2$  recorded by the Fe<sup>3+</sup>/ $\Sigma$ Fe ratios of basalts from exceeding ~QFM + 1 (see Fig. 10 in Jugo et al., 2010) even as melting preferentially extracts ferric iron from the residue. Sulfide is commonly observed in MOR basalts (Mathez, 1976) and the mantle source of MORBs is likely to contain sulfide (Herzberg, 2010; Mavrogenes and O'Neill, 1999). The sulfur concentration of the mantle (250 ppm, McDonough, 2003) exceeds that necessary to reduce all the ferric iron produced during MORB melting from F = 1-10% if  $D_{Fe_2O_3} = 0.22$ , half that needed if  $D_{Fe_2O_3} = 0.1$ , and enough in either case to reduce enough  $Fe^{3+}$  to maintain the observed  $Fe^{3+}$  $\sum$ Fe ratios. This is because 1 mol of sulfide can reduce 8 mol of iron. Given the  $Fe^{3+}/\Sigma$ Fe ratios of basalts measured in this study, sulfur becomes a viable candidate to buffer mantle melting, although a greater understanding of the behavior of S in the mantle source as a function of  $fO_2$ , and investigation of the speciation and concentration of S in MORB glasses, are required to fully test this hypothesis. This scenario masks, but does not lessen, the relatively high ferric iron content of >0.3 wt.% that we propose for the MORB source.

#### 5. Conclusions

We show that  $\mu$ -XANES is a highly accurate and precise technique for the determination of Fe<sup>3+</sup>/ $\Sigma$ Fe ratios in naturally quenched basaltic glass for values ranging from 0.08 to 0.61. New  $\mu$ -XANES measurements of Fe<sup>3+</sup>/ $\Sigma$ Fe ratios in global MORB pillow glasses yield an average of Fe<sup>3+</sup>/ $\Sigma$ Fe = 0.16 ± 0.01, which is 25% higher than that proposed by Bezos and Humler (2005) and 56% higher than that of Christie et al. (1986). XANES determinations of Fe<sup>3+</sup>/ $\Sigma$ Fe ratios in experimental glasses are offset to more oxidized values by only 0.01 (absolute) from wet chemical determinations using micro-colorimetry. The larger interlaboratory–intertechnique offsets observed in natural samples must therefore be attributed to processes specific to the dissolution of natural lavas during wet chemical procedures.

Fe<sup>3+</sup> behaves incompatibly during low-pressure fractionation but not during mantle melting. The latter may be attributed to Fe<sup>3+</sup> having a higher (and potentially more variable) bulk partition coefficient than previously assumed, or melting under buffered conditions. Translation of Fe<sup>3+</sup>/ $\sum$  Fe ratios to solid buffers indicates that primary mantle melts form at QFM. At this oxygen fugacity, oxidation of small amounts of sulfide to sulfate would buffer the melt and prevent magmatic  $Fe^{3+}/\sum Fe$  ratios from increasing during melting. Under any model, our data indicate that the concentration of  $Fe_2O_3$  in the fertile MORB mantle source is greater than or equal to 0.3 wt.%.

Supplementary materials related to this article can be found online at doi:10.1016/j.epsl.2011.03.014.

#### Acknowledgments

This work would not have been possible without the generosity of Becky Lange at the University of Michigan, Bjorn Mysen at the Geophysical Laboratory, and Tony Lanzirotti at the University of Chicago and NSLS. Discussions with Becky Lange, Charlie Langmuir, and Marc Hirschmann were invaluable during preparation of the manuscript and we benefited greatly from reviews by Dante Canil and Claude Herzberg. We gratefully acknowledge the following individuals and institutions that provided samples: The Division of Petrology and Volcanology at the Smithsonian Institution, The Graduate School of Oceanography at URI, Victor Kress, Charlie Langmuir, Peter Michael, lim Gill, Ian Carmichael, David Christie, and David Clague. NSF Award OCE-0644625 provided curatorial support for marine geological samples at the University of Rhode Island. We thank the students, staff and volunteers at the Smithsonian and URI who contributed to this work. Use of the National Synchrotron Light Source, Brookhaven National Laboratory, was supported by the U.S. Department of Energy, Office of Science, Office of Basic Energy Sciences, under Contract No. DE-AC02-98CH10886. We acknowledge support from Smithsonian's Scholarly Studies Program (EC), a URI ADVANCE fellowship (KK) and NSF awards EAR-0841108 (KK) and EAR-0841006 (EC).

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