# A Critical Analysis of Fuzzy Logic Controller for Slip Control in Antilock Braking System (ABS) 

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#### Abstract

This project aims at proposing an innovative way to implement the concept of fuzzy logic to an ABS model. The implementation of this project was conducted using simulation of ABS which is a combination from vehicle speed, wheel speed and slip through MATLAB Simulink software. By implementing fuzzy logic to the ABS system, the fuzzy logic can facilitate in improving the ABS abilities. The ABS model is developed and fuzzy logic controller is implemented to the model. The performance of the Fuzzy ABS is analyzed. The result shows that the fuzzy logic controller can facilitates the performance of the ABS by reducing the stopping time and maintaining the slip value near to 0.2.


Keywords: Antilock Braking System (ABS); Fuzzy Logic Controller.

## 1. Introduction

Anti-lock braking system or anti-skid braking system (ABS) is one of an important safety technologies used in high end cars and trucks which became a mandatory feature for vehicles in the US and Europe [1]. ABS worked when driver brake very heavily, suddenly or in slippery conditions. The forces exerted by the brakes can be powerful enough to cause the tire to break traction with the road [3]. Other than that, according to [1], the wheels will stop spinning and lock up as the momentum of the vehicle will cause it to continue moving. Australian study by Accident Research Centre, Monash University in 2004 found that ABS reduced the risk of multiple vehicle crashes by $18 \%$. Other than that, ABS reduced the risk of run-off-road crashes by $35 \%$ [4].
An ABS contains a series of sensors that can monitor how fast each wheel is rotating. The system is automatically activated to prevent the wheels from locking up. This condition will happen if the system detect a wheel has suddenly stop from spinning. Normally, wheels can be locked up when the driver applied heavy pressure to the brake pedal. When tire triggered, ABS can releases and reapplies brake rapidly around 15 times a second. So, this can prevent the wheels from locking up, helping maintain grip and consequently control. If this happens, the brake pedal will vibrate or pulse rapidly under driver foot.
To design an ABS is a very challenging task considering the fact that it is time varying and highly non-linear system. There are two things in ABS that are highly non-linear and time varying between them, one of it is the contact between the tires and the road surface (slip) and the dynamics of the whole vehicle and the features of key components in ABS such as valves, brake chambers and brake pads. All of this are non-linear and time varying system that difficult to design. Even though a linear model can be derived through a simplification, it is less precise, thus the use of some advanced control strategy is needed. These two things in ABS will affect the time taken to stop and stopping distances of a vehicle.

## 2. Anti-Lock Braking System

A single hydraulic assembly is grouping from the master cylinder, hydraulic booster, and ABS hydraulic circuitry. All of these parts have their own functionality, for example; wheel speed sensor is to transmit a signal of impending wheel lockup to the logic control. It will provide signals to a modulator to decrease the brake line pressure. After that, it will make the wheel to be released and rotational speed to increase again [6]. Figure 1 shows the typical Antilock Braking System.


Fig. 1: Typical Antilock Braking System
The performance of an antilock braking system depends on an identification of the road surface type. At present, there is no available reasonable sensor that can accurately detect the road surface and make the information available to the ABS controller. However, according to [5], the road surface condition and type can be inferred from the deceleration rate comparisons, wheel slip measurements, and vehicle braking pressure. One of the main purposes of the ABS is to control the wheel slip so that the road grip coefficient is maximized $[7,8]$. With the other meaning, this
strategy leads to minimize the vehicle stopping distance. However, the desired slip range is strongly road surface dependent. It may be referred to that a locked-up wheel generates a decreased braking force, little over those top quality of the accessible bond between tires and road. A locked-up wheel will also lose the vast majority about its ability will support at any lateral force. This might bring about that reduction for vehicle stability and controllability.
The essential motivation behind routine an ABS is to prevent wheel from locking, while to keep those longitudinal slip in an operational reach toward cycling those braking pressure [9]. This will achieve a shorter stopping distance with good directional control and stability during moderate maneuvers.

## 3. ABS Modelling

The vehicle modeling is divided into 3 main parts which are vehicle dynamics, wheel dynamics and braking dynamics of the system. For vehicle dynamic, the equation of motion of the simplified vehicle can be expressed by using Newton's second law:
$m_{t} V=-F_{t}-F_{a}$
where $V=$ vehicle velocity, $F_{t}=$ road friction force, $F_{a}=$ aerodynamic force acting on the vehicle and $m_{t}=$ total mass of the quarter vehicle.
The road friction force is given by Coulomb's law:
$F_{t}=\mu N$
where $N=$ total normal load and $\mu=$ road adhesion coefficient. The total mass of the quarter vehicle can be written as
$m_{t}=m_{\text {tire }}+\frac{1}{4} m_{c}$
where $m_{c}=$ vehicle mass and $m_{\text {tire }}=$ tire mass.
Thus, the total normal load can be expressed by
$N=m_{t} g-F_{L}$
where $F_{L}=$ is the longitudinal weight transfer load due to braking and $g=$ center of gravity height.
The aerodynamic force acting ( $F_{a}$ ) on the vehicle is proportional to the square of the speed of the vehicle with respect to the air and depends on the vehicle shape and size.

$$
\begin{equation*}
F_{a}=\frac{1}{4}\left(\frac{\rho}{2} C_{d} A_{f} V^{2}\right) \tag{5}
\end{equation*}
$$

where ${ }^{\rho}=$ mass density of the air, $C_{d}=$ vehicle drag coefficient and $A_{f}=$ vehicle frontal area.
For wheel dynamic, the equation of motion at wheel level for the rotational wheel is given by $\omega$ :

$$
\begin{equation*}
J_{w} \omega=-T_{b}+F_{t} R_{w} \tag{6}
\end{equation*}
$$

where $J_{\omega}=$ wheel moment of inertia, $\omega=$ wheel speed, $R_{\omega}=$ wheel radius, $T_{b}=$ braking torque and $F_{t}=$ road friction force. Braking dynamics of the system is combination of all the speed that involve in each vehicle. The combination of wheel dynamic and speed dynamic will give the equations of the vehicle model that can be expressed as
$\left(m_{t}-\mu(s) m_{e}\right) V=-\mu(s) m_{t} g-\frac{1}{4}\left(\frac{\rho}{2} C_{d} A_{f} V^{2}\right)$
$J_{w} \omega=-T_{b}+\mu(s)\left(m_{t} g-m_{e} V\right) R_{w}$
(8)
where $m_{e}$ is the effective mass.
ABS is actually a closed loop feedback control system in which a sensor monitors the output that is the relative slip ratio and give feeds data to the controller. The controller will adjust to control the brake pressure modulator as necessary to maintain the desired system output either it match with the wheel slip ratio to the reference value or desired value of relative slip. The relative slip equation is expressed as
$s=1-\frac{\omega_{w}}{\omega_{v}}$
where $\omega_{w}=$ vehicle angular velocity, $\omega_{v}=$ vehicle speed.
The vehicle angular velocity is calculated
$\omega_{w}=\frac{T_{t}-B_{t}}{I}$
(10)
where $T_{t}=$ Tire Torque, $\mathrm{B}_{t}=$ Braking Torque and $I=$ Wheel rotational inertia.
The ABS model is developed based of the relative equation. Figure 2 shows the simulation block diagram of $A B S$ model used in the experiment.


Fig. 2: Simulation of ABS Model
Figure 3 shows the subsystem of the ABS model, which is brake pressure modulator. This is used to simulate braking torque. The hydraulic pressure from braking is multiply with piston area to get the braking torque.


Fig. 3: Brake Pressure Modulator
The parameter used in the model is listed in Table 1.

Table 1: Parameters used in the ABS model

| Parameters | Value |
| :---: | :---: |
| Proportional gain $\left(K_{p}\right)$ | 1200 |
| Force and Torque $\left(K_{f}\right)$ | 1 |
| Mass $(m)$ | 50 |
| Wheel radius $\left(R_{r}\right)$ | 1.25 |
| Gain $(g)$ | 32.18 |

Initial velocity $\left(V_{o}\right)$
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The weight of the vehicle for quarter part which is a quarter from the vehicle is calculated in (11), while wheel speed after it through the brake pressure is calculated in (12).
$K=\frac{(m * g)}{4}$
$\omega=\frac{V_{0}}{R r}$
where $V_{0}=$ Initial Velocity and $R r=$ Wheel radius.
Three value of initial velocity are used as a comparative study to the ABS model as shown in Table 2.

Table 1: Initial velocity

| Initial Condition $\left(V_{0}\right)$ | 1 st | 2nd | 3rd |
| :---: | :---: | :---: | :---: |
| Value (Rad/s) | 87.5 | 112.5 | 137.5 |

These 3 values indicate the low, medium and high initial velocity. The speed value is converted from ( $\mathrm{rad} / \mathrm{s}$ ) to $(\mathrm{km} / \mathrm{h})$ in (13).

$$
\begin{equation*}
v=r \omega \tag{13}
\end{equation*}
$$

where $v=$ Linear velocity (m/s), $r=\operatorname{Radius}(\mathrm{m})$ and $\omega=$ Angular Velocity ( $\mathrm{rad} / \mathrm{s}$ ).
The speeds of wheels are tabulated as shown in Table 3.
Table 3: Wheel speed used in the experiment
Table 3: Wheel speed used in the experiment

| Wheel Speed $(\mathrm{rad} / \mathrm{s})$ | 70 | 90 | 110 |
| :---: | :---: | :---: | :---: |
| Wheel Speed $(\mathrm{km} / \mathrm{h})$ | 80.64 | 103.6 | 126.72 |

## 4. Fuzzy Logic Controller

Fuzzy logic controller consists of three basic components which are input signal fuzzification, fuzzy inference mechanism and output defuzzification. Fuzzy inference mechanism handles rules where human experience may easily be injected through linguistic rules. The de-fuzzification block transforms the fuzzy control actions to continuous signals that can be used on physical plant. The knowledge base includes fuzzy sets that are defined on the period of the inputs and outputs of the FLC and rule base, which is constructed from fuzzy implication. The error and error changed for both position and time are scaled using appropriate scaling factors. These scaled input data then converted into linguistic variables which may be viewed as labels of fuzzy sets. Figure 4 shows the block diagram of fuzzy control system.


Fig. 1: Block diagram of fuzzy control system

### 4.1. Input Signal Fuzzification

For this project, the fuzzy controller use two inputs which are slip error and slip change rate. The slip error indicate the target error while slip change rate indicate the deceleration of the vehicle changes with respect to time. Fuzzy set uses a common function such as triangular, trapezoidal, Gaussian and many more that were called as membership function to support membership value of its element. In this project, triangular shape is being used for both input. $1^{\text {st }}, 2^{\text {nd }}$ and $3^{\text {rd }}$ parameters is used to mention the point
of the triangle. The rules used for comparison purpose are as follow.

| i. | $3 \times 3$ rules |
| ---: | :--- |
| ii. | $5 \times 5$ rules |
| iii. | $7 \times 7$ rules |

### 4.1.1. $3 \times 3$ Rule

In $3 \times 3$ rule, there is 3 membership function were namely as:

| Slip error: | Slip change rate: |
| :--- | :--- |
| $\mathrm{Z}=$ zero | $\mathrm{N}=$ negative |
| $\mathrm{PS}=$ positive small | $\mathrm{Z}=$ zero |
| $\mathrm{PB}=$ positive big | $\mathrm{P}=$ positive |

The range and parameter between the membership function has been adjusted as Table 4. The difference between each point of parameter is 0.75 and the range for parameter 1 st to parameter 3rd is from 0 to 3 .

Table 2: $3 \times 3$ slip error input

| Name | Parameters |  |  |
| :---: | :---: | :---: | :---: |
|  | 1 st | 2nd | 3rd |
| Z | 0 | 0.75 | 1.5 |
| PS | 0.75 | 1.5 | 2.25 |
| PB | 1.5 | 2.25 | 3 |

Table 5 shows the $3 \times 3$ rate of slip changes. The difference between each point of parameter is 0.75 and the range for parameter 1 st to parameter 3rd is from -1.5 to 1.5 .
Table 5: 3x3 rate of slip error changes

| Name | Parameters |  |  |
| :---: | :---: | :---: | :---: |
|  | 1 st | 2 nd | 3rd |
| N | -1.5 | -0.75 | 0 |
| Z | -0.75 | 0 | 0.75 |
| P | 0 | 0.75 | 1.5 |

### 4.1.2. $\quad$ 5x5 Rules

In $5 \times 5$ rule, there is 5 membership function were namely as:

$$
\begin{array}{lc}
\text { Slip error: } & \text { Slip change rate: } \\
\mathrm{Z}=\text { zero } & \mathrm{NS}=\text { negative small } \\
\mathrm{PS}=\text { positive small } & \mathrm{Z}=\text { zero } \\
\mathrm{PO}=\text { positive optimum } & \mathrm{PS}=\text { positive small } \\
\mathrm{PB}=\text { positive big } & \mathrm{PM}=\text { positive medium } \\
\mathrm{PTB}=\text { positive too big } & \mathrm{PB}=\text { positive big }
\end{array}
$$

The range and parameter between the membership function has been adjusted as Table 6. The difference between each point of parameter is 0.5 and the range for parameter 1st to parameter 3rd is from 0 to 3 .

Table 6: $5 \times 5$ slip error input

| Name | Parameters |  |  |
| :---: | :---: | :---: | :---: |
|  | 1 st | 2nd | 3rd |
| Z | 0 | 0.5 | 1 |
| PS | 0.5 | 1 | 1.5 |
| PO | 1.5 | 1.5 | 2 |
| PB | 1 | 2 | 2.5 |
| PTB | 2 | 2.5 | 3 |

Table 7 shows the $5 \times 5$ rate of slip changes. The difference between each point of parameter is 0.5 and the range for parameter 1 st to parameter 3 rd is from -1.5 to 0.5 .

Table 7: 5x5 rate of slip error changes

| Table 7: 5x5 rate of slip error changes |  |  |  |
| :---: | :---: | :---: | :---: |
|  | 1st | 2 nd | 3rd |
|  | -1.5 | -1 | -0.5 |
|  | -1 | -0.5 | 0 |
| PS | -0.5 | 0 | 0.5 |
| PM | 0 | 0.5 | 1 |


| PB | 0.5 | 1 | 1.5 |
| :---: | :---: | :---: | :---: |

### 4.1.3. 7x7 Rules

In 7 x 7 rule, there is 7 membership function were namely as:

| Slip error: | Slip change rate: |
| :--- | :--- |
| Z $=$ zero | NL $=$ negative large |
| VS $=$ very small | NS = negative small |
| TO = too small | $\mathrm{Z}=$ zero |
| STO = small than optimum | TS $=$ too small |
| $\mathrm{O}=$ optimum | $\mathrm{O}=$ optimum |
| TL $=$ too large | TL $=$ too large |
| VL $=$ very large | $\mathrm{VL}=$ very large |

The range and parameter between the membership function has been adjusted as Table 8 . Where the difference between each point of parameter is 0.375 and the range for parameter 1st to parameter 3rd is from 0 to 3 .

Table 3: 7x7 slip error input

| Table 3: 7x7 slip error input |  |  |  |
| :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd |
|  | 0 | 0.375 | 0.75 |
| Z | 0.375 | 1.75 | 1.125 |
| VS | 0.75 | 1.125 | 1.5 |
| TS | 1.125 | 1.5 | 1.875 |
| STO | 1.5 | 1.875 | 2.25 |
| O | 1.875 | 2.25 | 2.625 |
| TL | 2.25 | 2.625 | 3 |
| VL |  |  |  |

Table 9 shows the $7 \times 7$ rate of slip changes. The difference between each point of parameter is 0.375 and the range for parameter 1st to parameter 3rd is from -1.5 to 1.5 .

Table 9: 7x7 rate of slip error changes

| Name | Parameters |  |  |
| :---: | :---: | :---: | :---: |
|  | 1 st | 2nd | 3rd |
| NL | -1.5 | -1.125 | -0.75 |
| NS | -1.125 | -0.75 | -0.375 |
| Z | -0.75 | -0.375 | 0 |
| TS | -0.375 | 0 | 0.375 |
| O | 0 | 0.375 | 0.75 |
| TL | 0.375 | 0.75 | 1.125 |
| VL | 0.75 | 1.125 | 1.5 |

### 4.2. Fuzzy Inference Mechanism

Fuzzy inference is the process of formulating the mapping from a given input to an output using fuzzy logic. For this project, IFTHEN rules have been decided to diagnose between input and output of the variables. While, the connective between error slip and rate of change of slip has been decided by using OR that interpreted as interconnection operation.

### 4.2.1. 3X3 Rules

Rules for $3 \times 3$ have been created using the combination membership function that was developed between (Z, PS and PB) and ( N , Z and P ). Table 10 shows the fuzzy inference mapping for $3 \times 3$ rules:

Table 10: Fuzzy inference mapping for $3 \times 3$ rules

| Slip Error \Change of Error | N | Z | P |
| :---: | :---: | :---: | :---: |
| Z | P | P | Z |
| PS | P | P | P |
| PB | N | N | N |

### 4.2.2. $\quad 5 \mathrm{X} 5$ Rules

Rules for $5 \times 5$ has been created by using the combination membership function that was developed between (Z, PS, PO, PB and

PTB) and (NS, Z, PS, PM and PB). Table 11 shows the fuzzy inference mapping for $5 \times 5$ rules.

Table 11: Fuzzy inference mapping for $5 \times 5$ rules

| Slip Error \Change of Error | NS | Z | PS | PM | PB |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $Z$ | PB | PB | PB | PS | Z |
| PS | PB | PB | PS | PS | NS |
| PO | PS | Z | Z | NS | NB |
| PB | NS | NS | NS | NB | NB |
| PTB | NS | NS | Z | NB | NB |

### 4.2.3. 7X7 Rules

Rules for 7 x 7 has been created by using the combination membership function that was developed between (Z, VS, TS, STO, $\mathrm{O}, \mathrm{TL}$ and VL) and (NL, NS, Z, TS, O, TL and VL). Table 12 shows the fuzzy inference mapping for 7X7 rules.

Table 12: Fuzzy inference mapping for 7 x 7 rules

| Slip Error <br> Change of <br> Error | NL | NS | Z | TS | O | TL | VL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Z | PL | PL | PL | PL | PM | PS | Z |
| VS | PL | PL | PM | PM | PS | PS | NS |
| TS | PL | PM | PM | PS | PS | NS | NS |
| STO | PM | PS | NM | NL | NL | NL | NM |
| O | NS | NS | NM | NM | NL | NL |  |
| TL | NS | NS | Z | NM | NL | NL |  |
| VL | NS | NS | NS |  |  |  |  |

### 4.3. Output Defuzzification

Defuzzification is the process to produce a result or a crisp value in fuzzy logic. By given the membership functions and fuzzy sets, the defuzzification can process and associated between them. The result of the fuzzy sets that sense in an output will be sent to the plant of the system. The block diagram of ABS model with fuzzy logic controller is illustrated as Figure 5. The desired relative slip is selected to be 0.2 for the maximum friction force and minimum stopping distance. [10]


Fig. 5: ABS model with fuzzy logic controller

## 5. Results and Discussion

This project compared the skidding occurrence when without ABS, with standard ABS and with ABS and fuzzy logic controller. The braking without standard ABS and ABS standard model is being simulated and analyzed in term of wheel speed, time taken to stop and the relative slip. Number of ripple is also calculated to represent the drastic change of wheel speed when ABS activated. Then, the fuzzy logic controller is implemented to the
model and the simulation is being run again. The result is recorded and compared with the standard ABS model.

### 5.1. Breaking Without ABS and With ABS

Figure 6a-b show the result of braking without the ABS at vehicle speed $70(\mathrm{rad} / \mathrm{s})$.


Fig. 6a: Wheel spee Time (s) ABS at $70(\mathrm{rad} / \mathrm{s})$


Fig. 6b: Slip wit Time (s) $70(\mathrm{rad} / \mathrm{s})$
The data from Figure 6a-b are tabulated in Table 13:

Table 13: Breaking without ABS at 70 ( $\mathrm{rad} / \mathrm{s}$ )

| No. <br> Ripple | Wheel <br> Speed <br> $(\mathrm{rad} / \mathrm{s})$ | Wheel <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | Time (s) | Relative <br> Slip |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 70 | 80.64 | 0 | - |
| 1 | 45.52 | 52.78 | 5.32 | 0.16 |
| 2 | 0 | 0 | 16.82 | 1 |

Based on the graph of wheel speed without ABS at $70(\mathrm{rad} / \mathrm{s})$, the time taken to stop the vehicle was 16.82 s. The value of slip was 0.16 before the car stop. The slip value is already at 1 even before the car stop. It shows that the car is sliding on the road for 11s.
The wheel speed without ABS also simulated at $90(\mathrm{rad} / \mathrm{s})$ and $110(\mathrm{rad} / \mathrm{s})$. The result shows similar graphs as Figure 6a-b, but difference in value as shown in Table 14 and 15.

Table 14: Breaking without ABS $90(\mathrm{rad} / \mathrm{s})$

| No. <br> Ripple | Wheel <br> Speed <br> $(\mathrm{rad} / \mathrm{s})$ | Wheel <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | Time (s) | Relative <br> Slip |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 90 | 103.68 | 0 | - |
| 1 | 51.88 | 59.77 | 6.06 | 0.24 |
| 2 | 0 | 0 | 21.11 | 1 |

Table 15: Breaking without ABS 110 ( $\mathrm{rad} / \mathrm{s}$ )

| No. <br> Ripple | Wheel <br> Speed <br> $(\mathrm{rad} / \mathrm{s})$ | Wheel <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | Time (s) | Relative <br> Slip |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 110 | 126.72 | 0 | - |
| 1 | 68.34 | 78.73 | 6.11 | 0.23 |
| 2 | 0 | 0 | 25.00 | 1 |

For the $90(\mathrm{rad} / \mathrm{s})$, the stop time is 21.11 s with slip value 0.24 while for $110(\mathrm{rad} / \mathrm{s})$ the stop time is 25 s with slip value 0.23 . Similar to the result of wheel speed $70(\mathrm{rad} / \mathrm{s})$, the $90(\mathrm{rad} / \mathrm{s})$ and
$110(\mathrm{rad} / \mathrm{s})$ shows the car slide on the road for 13.8 s and 17.5 s . The high inertia of a sudden stopping will be taken by the passenger inside the car.
Figure 7a-b show the result of breaking with the ABS intact at vehicle speed $70(\mathrm{rad} / \mathrm{s})$.


Figure 7a: Wheel speed of standard ABS at $70(\mathrm{rad} / \mathrm{s})$


Figure 7b: Slip standard ABS at 70 (rad/s)
The data from Figure 7a-b are tabulated in Table 15:

| Cable 15: Breaking with standard ABS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| No. <br> Ripple | Wheel <br> Speed <br> $(\mathrm{rad} / \mathrm{s})$ | Wheel <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | Time (s) | Relative <br> Slip |  |
| 0 | 70 | 80.64 | 0 | - |  |
| 1 | 34.76 | 40.04 | 6.43 | 0.26 |  |
| 2 | 25.31 | 0 | 8.51 | 0.26 |  |
| 3 | 17.35 | 19.99 | 10.17 | 0.26 |  |
| 4 | 10.66 | 12.28 | 11.58 | 0.26 |  |
| 5 | 4.9 | 5.64 | 12.79 | 0.29 |  |
| 6 | 0 | 0 | 14.1 | 1 |  |

Based on the graph of wheel speed standard ABS at $70(\mathrm{rad} / \mathrm{s})$, the time taken to stop the vehicle was 14.01 s . The slip value before the car stop was 0.29 at ripple number 5 . The slip of 1 occurs at 13.7 s shows the car slide at about 0.31 s .
The wheel speed with ABS are also simulated at $90(\mathrm{rad} / \mathrm{s})$ and 110 (rad/s). The result shows similar graphs as Figure 7a-b, but difference in value and number of ripple as shown in Table 1718.

Table 17: Breaking with standard ABS at $90 \mathrm{rad} / \mathrm{s}$

| No. <br> Ripple | Wheel <br> Speed <br> $(\mathrm{rad} / \mathrm{s})$ | Wheel <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | Time (s) | Relative <br> Slip |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 90 | 103.68 | 0 | - |
| 1 | 48.52 | 55.66 | 6.68 | 0.26 |
| 2 | 37.37 | 43.06 | 9.06 | 0.26 |
| 3 | 27.66 | 31.86 | 11.15 | 0.26 |
| 4 | 19.33 | 22.27 | 12.90 | 0.26 |
| 5 | 12.32 | 14.19 | 14.37 | 0.26 |
| 6 | 6.27 | 7.22 | 15.67 | 0.28 |
| 7 | 0 | 0 | 17.21 | 1 |

Table 18: Breaking with standard ABS at $110 \mathrm{rad} / \mathrm{s}$

| No. <br> Ripple | Wheel <br> Speed <br> $(\mathrm{rad} / \mathrm{s})$ | Wheel <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | Time (s) | Relative <br> Slip |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 110 | 126.72 | 0 | - |
| 1 | 62.24 | 71.70 | 6.90 | 0.26 |
| 2 | 50.05 | 57.66 | 9.52 | 0.26 |
| 3 | 38.75 | 44.64 | 11.97 | 0.26 |
| 4 | 29.00 | 33.41 | 14.03 | 0.26 |
| 5 | 20.51 | 23.63 | 15.82 | 0.26 |
| 6 | 13.40 | 15.44 | 17.33 | 0.26 |
| 7 | 7.25 | 8.35 | 18.63 | 0.27 |
| 8 | 0 | 0 | 20.44 | 1 |

For wheel speed at $90(\mathrm{rad} / \mathrm{s})$, the stopping time is 17.21 s with mean slip 0.263 while for $110(\mathrm{rad} / \mathrm{s})$, the stopping time is 20.44 s with mean 0.261 . The sliding rate is at about 0.3 s for $90(\mathrm{rad} / \mathrm{s})$ and 0.6 s for $110(\mathrm{rad} / \mathrm{s})$.
As shown in Figure, the wheel speed and the vehicle speed decrease almost at the same speed of the vehicle. In comparison with the breaking without the ABS, it shows that the time taken to stop is reduced by 2 s for $70(\mathrm{rad} / \mathrm{s}), 3.9 \mathrm{~s}$ for $90(\mathrm{rad} / \mathrm{s})$ and 4.6 s for $110(\mathrm{rad} / \mathrm{s})$.

### 5.2. Breaking with ABS and fuzzy logic controller

The ABS is then implemented with $3 \times 3,5 \times 5$ and $7 x 7$ fuzzy logic controller. The wheel speed is set to $70(\mathrm{rad} / \mathrm{s}), 90(\mathrm{rad} / \mathrm{s})$ and 110 $(\mathrm{rad} / \mathrm{s})$. The result of all speed selected is represented by 70 $(\mathrm{rad} / \mathrm{s})$ for $3 \times 3,90(\mathrm{rad} / \mathrm{s})$ for $5 \times 5$ and $110(\mathrm{rad} / \mathrm{s})$ for 7 x 7 . These are due to the graphs result are similar.
The result for $3 \times 3$ fuzzy controller with ABS for $70(\mathrm{rad} / \mathrm{s})$ is shown in Figure 8a-b.


Fig. 8a: Wheel speed $3 \times 3 \mathrm{ABS}$ at $70(\mathrm{rad} / \mathrm{s})$


Fig. 8b: Slip $3 \times 3$ ABS at $70(\mathrm{rad} / \mathrm{s})$
Based on the graph of wheel speed $3 \times 3 \mathrm{ABS}$ at $70(\mathrm{rad} / \mathrm{s})$, the time taken to stop the vehicle was 12.32 s. Besides that, the slip that the vehicle take which is the contact between the tire and the road before it fully stop is 0.21 . The maximum value of the slip is 0.23 and the minimum value is 0.21 .

Figure 9a-b shows the result of ABS with $5 \times 5$ fuzzy at $90(\mathrm{rad} / \mathrm{s})$.


Fig. 9a: Wheel speed $5 \times 5 \mathrm{ABS}$ at $90(\mathrm{rad} / \mathrm{s})$


Fig. 9b: Slip $5 \times 5 \mathrm{ABS}$ at $90(\mathrm{rad} / \mathrm{s})$
From Figure 9a-b, the time taken to stop the vehicle takes 15.28 s . Besides that, the slip that the vehicle takes which is the contact between the tire and the road before it fully stops is 0.28 . The maximum value of the slip is 0.28 and the minimum value is 0.25 .

Figure 10a-b shows the result of ABS with $7 \times 7$ fuzzy at 110 ( $\mathrm{rad} / \mathrm{s}$ ) speeding.


Fig. 10a: Wheel speed $7 \times 7$ ABS at $110(\mathrm{rad} / \mathrm{s})$


Fig. 10b: Slip $7 \times 7 \mathrm{ABS}$ at $110(\mathrm{rad} / \mathrm{s})$
Based on the graph of wheel speed 7 x 7 ABS at $110(\mathrm{rad} / \mathrm{s})$, the time taken to stop the vehicle takes 18.43 s. Besides that, the slip
that the vehicle takes which is the contact between the tire and the road before it fully stops is 0.38 . The maximum value of the slip is 0.38 and the minimum value is 0.26 .

### 5.3. Summarize result of breaking with standard ABS and breaking with ABS fuzzy

Table 19 shows the summarize result of breaking with standard ABS and breaking with ABS fuzzy; $3 \times 3,5 \times 5$ and 7 x 7 rules.

Table 19: Summarize result of breaking with standard ABS and breaking with ABS fuzzy; $3 \mathrm{x} 3,5 \mathrm{x} 5$ and 7 x 7 rules

| Parameters | No. <br> Ripple | Max. <br> Slip | Min. <br> Slip | Mean <br> Slip | Stop <br> Time (s) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $70 \mathrm{rad} / \mathrm{s} / \mathrm{std}$. <br> ABS | 5 | 0.29 | 0.26 | 0.266 | 14.1 |
| $70 \mathrm{rad} / \mathrm{s} / 3 \times 3$ | 10 | 0.23 | 0.21 | 0.213 | 12.32 |
| $70 \mathrm{rad} / \mathrm{s} / 5 \times 5$ | 8 | 0.28 | 0.26 | 0.265 | 12.18 |
| $70 \mathrm{rad} / \mathrm{s} / 7 \mathrm{x} 7$ | 7 | 0.34 | 0.28 | 0.294 | 12.23 |
| $90 \mathrm{rad} / \mathrm{s} / \mathrm{std}$. <br> ABS | 6 | 0.28 | 0.26 | 0.263 | 17.21 |
| $90 \mathrm{rad} / \mathrm{s} / 3 \times 3$ | 12 | 0.23 | 0.21 | 0.216 | 15.42 |
| $90 \mathrm{rad} / \mathrm{s} / 5 \times 5$ | 10 | 0.28 | 0.25 | 0.26 | 15.28 |
| $90 \mathrm{rad} / \mathrm{s} / 7 \times 7$ | 9 | 0.36 | 0.28 | 0.293 | 15.29 |
| $110 \mathrm{rad} / \mathrm{s} /$ <br> $\mathrm{std} . \mathrm{ABS}$ | 7 | 0.26 | 0.27 | 0.261 | 20.44 |
| $110 \mathrm{rad} / \mathrm{s} /$ <br> 3 x 3 | 14 | 0.23 | 0.21 | 0.212 | 18.58 |
| $110 \mathrm{rad} / \mathrm{s} /$ <br> $5 \times 5$ | 13 | 0.30 | 0.24 | 0.254 | 18.36 |
| $110 \mathrm{rad} / \mathrm{s} /$ <br> 7 x 7 | 11 | 0.38 | 0.26 | 0.288 | 18.43 |

From Table 19, the best stopping time for $70(\mathrm{rad} / \mathrm{s})$ is $5 \times 5$ fuzzy rules which values 12.18 s . The same result also occur to 90 $(\mathrm{rad} / \mathrm{s})$ and also $110(\mathrm{rad} / \mathrm{s})$ where the best stopping time is 5 x 5 fuzzy.
For the slip value, the best slip value for $70(\mathrm{rad} / \mathrm{s})$ goes to $3 \times 3$ fuzzy rules which values 0.213 . The same result also happen to $90(\mathrm{rad} / \mathrm{s})$ and $110(\mathrm{rad} / \mathrm{s})$ where the best slip value goes to $3 \times 3$ fuzzy rules.
Figure 11a-c shows the overall result of fuzzy implementation to ABS.


Fig. 11a: The overall result of fuzzy implementation to ABS at 70 (rad/s)


Fig. 11b: The overall result of fuzzy implementation to ABS at $90(\mathrm{rad} / \mathrm{s})$


Fig. 11c: The overall result of fuzzy implementation to ABS at (110 $\mathrm{rad} / \mathrm{s}$ )

From the Figure 11a-c, the fuzzy logic controller clearly takes less time to stop the vehicle compare with standard ABS and without ABS. This is done by the controlling of relative slip at 0.2 . For vehicle speed at $70(\mathrm{rad} / \mathrm{s})$, the difference between fuzzy and standard ABS is 1.83 second while for $90(\mathrm{rad} / \mathrm{s})$ and 110 $(\mathrm{rad} / \mathrm{s})$ are 1.93 second and 2.08 second.
Figure 12 shows the mean slip comparison between fuzzy $3 x 3$, fuzzy 5 x 5 and fuzzy 7 x 7 .


Fig. 12: Mean slip comparison between fuzzy $3 x 3$, fuzzy $5 x 5$ and fuzzy 7x7

From Figure 12, it can be clearly seen that $3 \times 3$ fuzzy logic shows the best mean value slip. All of the $3 \times 3$ fuzzy result 0.21 in average. The lowest performance is from $7 \times 7$ fuzzy rules where the average value is 0.29 . The middle value is from $5 \times 5$ fuzzy rules.

## 6. Conclusion

Fuzzy logic controller is implemented to increase the performance of the ABS at wheel speed $70(\mathrm{rad} / \mathrm{s}), 90(\mathrm{rad} / \mathrm{s})$ and 110 $(\mathrm{rad} / \mathrm{s})$. Three fuzzy rules were designed which comprised of $3 \times 3$, 5 x 5 and 7 x 7 . The fuzzy controller result is compared with standard ABS and without ABS. From the comparisons, the best performance of ABS occurs when $3 \times 3$ fuzzy rules is implemented. The average means slip of $3 \times 3$ fuzzy rules at 0.21 and the stopping time 1.93 s less than the standard ABS. This demonstrated that fuzzy logic facilitates the performance of the ABS by reducing the stopping time and maintaining the slip value near to 0.2 . Thus, the ABS with fuzzy logic will help the driver to steer while braking heavily and prove to be lifesaving system. This research highlighted that automobile ABS fuzzy control system is worth to be further developed and has bright prospect. For future prospect, the fuzzy controller can be enhanced by implementing to the real ABS and analysis.

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