

Ultimate lateral load resistance of laterally loaded pile

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ABSTRACT: Several methods are available for predicting ultimate lateral load resistance of laterally loaded pile. These methods often produce significantly different ultimate lateral resistance. This makes it difficult to select an appropriate method in designing/predicting ultimate lateral resistance of pile. This paper presents a review of two different methods; Meyerhof and Patra & Pise for predicting lateral resistance of pile. Then, the predicted ultimate lateral resistances by these two methods are compared with the experimental results. It is found that Meyerhof's method gives better prediction for single pile with smaller L/d ratio whereas Patra & Pise method gives better predictions for pile groups with higher L/d . Thus, none of these methods can be applicable universally for all possible conditions. Also the parametric study on ultimate lateral resistance revealed that length to diameter ratio, pile spacing, pile configuration in a pile group are important parameters for prediction of lateral load resistance.

1 INTRODUCTION

There are several approaches available in the literature to estimate lateral load resistance of pile in sand and clay (Broms 1964; Meyerhof et al. 1981; Meyerhof and Ranjan 1972; Meyerhof and Sastry 1985; Meyerhof and Yalcin 1984; Sastry 1977; Sastry and Meyerhof 1986; Zhang et al. 2005). Also some simplified methods are proposed by Meyerhof et al. (1988) and Patra & Pise (2001) for cohesionless soil. However, these methods often produce significantly different ultimate lateral load resistance value (Zhang et al. 2005). This makes it difficult to select appropriate method when designing laterally loaded pile in cohesionless soil. A comparative study has been made in this paper between Meyerhof and Patra & Pise methods and experimental results with the intention that it could add some value on the understanding of practicing engineers. Also a parametric study is done on ultimate lateral load resistance. They are discussed in coming sections.

2 ULTIMATE LATERAL LOAD RESISTANCE

The simplified methods proposed by Meyerhof et al. (1988) and Patra & Pise (2001) has been briefly reviewed in this section. These methods are approximate with considerable assumptions. They are discussed in coming subsections.

2.1 Meyerhof's method

The ultimate lateral resistance of rigid pile, Q_{ur} is expressed by Meyerhof et al. (1981) as

$$Q_{ur} = 0.12\gamma dL^2 K_b \quad (1)$$

Where γ is average unit weight of sand; d is the diameter of pile; L is embedded length of pile; K_b is coefficient of net passive earth pressure on pile using an average angle of skin friction $\delta = \phi/3$. Where ϕ is the angle of internal friction. However the ultimate lateral load resistance of flexible pile was presented by Meyerhof et al. (1988) as

$$Q_{ur} = 0.12\gamma dL_e^2 K_b \quad (2)$$

Where L_e is the effective embedded length of flexible pile. Meyerhof and Yalcin (1984) suggested that if relative stiffness ratio K_{rs} is less than 10^{-1} to 10^{-2} then the pile can be considered as flexible pile. However, the relative stiffness, K_{rs} can be presented as

$$K_{rs} = E_p I_p / E_h L^4 \quad (3)$$

Where E_p is modulus of elasticity of pile; I_p is moment of inertia of pile; E_h is horizontal soil modulus at pile tip; L is embedded length of pile. Meyerhof et al. (1988) reported that L_e/L has an approximate functional relationship with relative stiffness K_{rs} and it can be presented as

$$L_e/L = 1.8K_{rs}^{0.12} \quad (4)$$

However, Rahman et al. (2003) reported that L_e/L can be represent by following relation as

$$L_e/L = 1.65K_{rs}^{0.12} \quad (5)$$

2.2 Patra & Pise method

Patra & Pise (2001) modified the Meyerhof's equation by multiplying a constant shape factor of 3 with the line of Broms (1964)

$$Q_{ur} = 3 \times 0.12 \gamma L_e^2 K_b \quad (6)$$

2.3 Pile group

Patra & Pise (2001) reported that the ultimate resistance of the pile group can be represented by

$$Q_{Lg} = 2F + P_p \quad (7)$$

Where, Q_{Lg} is ultimate lateral resistance of the pile group, F is frictional resistance on the vertical plane along the side of the pile group of width equal to centre to centre distance between external piles and embedded length L and P_p passive earth pressure for the front pile as shown in Figure 1.

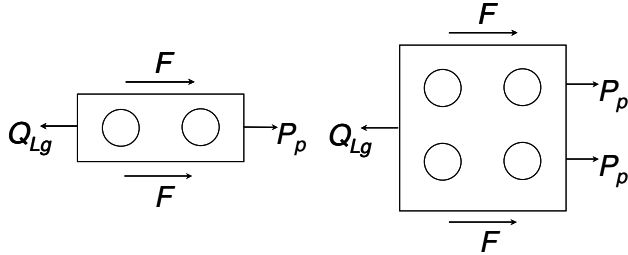


Figure 1. Free body diagram of laterally loaded pile group

The frictional resistance along the side of the pile group could be approximately found as

$$F = \frac{1}{2} \gamma L^2 \times K_s S \quad (8)$$

Where, K_s is coefficient of earth pressure along the side of the piles group governing frictional resistance $[(1 - \sin \phi) \tan \delta]$. Thus, ultimate lateral resistance of pile group, 2x1 is

$$Q_{Lg} = \gamma L^2 [K_s S + 0.36 d K_b] \quad (9)$$

And the ultimate resistance of pile group, 2x2 can be expressed as

$$Q_{Lg} = \gamma L^2 [K_s S + 0.72 d K_b] \quad (10)$$

2.4 Group efficiency

The efficiency of ultimate lateral resistance of pile group can be expressed as

$$\eta = \frac{Q_{Lg}}{n_1 n_2 Q_{Ls}} \quad (11)$$

Where Q_{Lg} is the ultimate lateral capacity of pile group; Q_{Ls} is the ultimate lateral capacity of single pile; n_1 is the number of rows in the pile group and n_2 is the number of columns in the pile group.

3 EXPERIMENTATION

An experimental program was designed for the verification and comparison of the above mention methods. The details of the experimental program and material properties such as sand, pile, pile cap etc. are given in following subsections.

3.1 Foundation

Rajshahi sand (available in north-west region in Bangladesh) is used as foundation medium. All model pile tests were done on a concrete tank of one meter in height, one meter in width and one meter in depth. Sand had a placement density of 95 lb/ft³ or 15kN/m³ and the angle of internal friction was 37.9°. Specific gravity of the sand used in the model tank was 1.82.

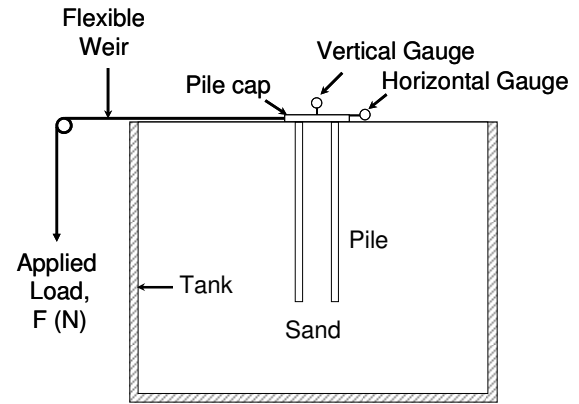


Figure 2. Experimental arrangement for laterally loaded pile

3.2 Pile and pile cap

Aluminum alloy tube of 19mm outer diameter and 0.81mm wall thickness were used as model pile. To increase the pile wall friction angle, sand was added around the pile by adhesives. The average outside diameter of the rough piles were 20mm. The embedment length-to-diameter ratios, L/d were 20, 30, and 35. Steel plate of 0.64cm thickness was used as pile cap. The piles were attached with the pile cap by screw. The details of sand and piles properties can

be found in (Rahman et al. 2003). The pile groups used in this study had configurations of 2x1 and 2x2.

3.3 Experimental procedure

The arrangement of test program is shown in Figure 2. The Loading arrangement was made in such a way that it acted laterally to pile or pile cap. However, it was not possible to apply continuous loading but load is applied by stepping. To maintain a uniform density all through the tank depth, sand was placed in the tank from a constant height of about 0.5m. After filling the tank, the upper surface of sand was leveled and then the pile was pushed into sand. Pile cap was then fixed on the pile top with screw connections. A 24 hours of rest period was allowed before applying any load on pile setup. The lateral load was applied to the pile cap through a pulley arrangement with flexible weir. The other end of the weir was attached to the loading apron. Load was applied by dead weight over the loading pan starting from the smallest with gradual increase in steps. To measure the lateral and vertical deflection dial gauges with a sensitivity of 0.01 mm were used. When step by step lateral loads were applied on the pile or pile group, they were deflected in the direction of the lateral load and the dial gauge readings and the corresponding loadings were recorded.

4 RESULTS

The ultimate lateral load resistance of the pile was worked out by plotting the recorded data, thus load Vs deflection curve was obtain which was non-linear in nature. Ultimate lateral resistance of the pile was obtained from the curve by double tangent method (DTM) or the point where the curve show a greater deflection without further increase in any load. The detail can be found in (Rahman et al. 2003). The curves presented in this paper are only showing the general trends. The ultimate load resistance behaviours of single pile and the pile group are presented in coming subsections.

4.1 Single pile

The ultimate lateral load resistance of single pile increases with increase in L/d ratio as shown in Figure 3. The ultimate load resistance of a single pile for L/d=20 is about 107N whereas 115.2N predicted by Meyerhof's method and 72N by Patra & Pise method. Thus, Patra & Pise method doesn't predict well for single pile and the prediction by Meyerhof's method is very closed to the experimental observation. However, in higher L/d, Patra & Pise method gives better prediction. The ultimate lateral load resistance of L/d=35 is about 225N and Patra & Pise method predicted 221.7N whereas Meyerhof's prediction deviate by 50N in higher side.

4.2 Pile group, 2x1

The ultimate lateral load resistance of pile group, 2x1 increases with increasing L/d as shown in Figure 4. It is about 117.2N for L/d=20 and 160N, 250N for L/d=30, L/d=35 respectively.

However, when the observed ultimate lateral resistance is compared with Meyerhof and Patra & Pise methods, it is found that the ultimate lateral load resistance predicted by Patra & Pise method gives a better prediction for pile group. Table 1. shows the detailed results for L/d=20.

Table 1. Comparison of lateral load resistance of pile group, 2x1 with Patra & Pise method and observed value.

L/d ratio	Spacing (d)	Observed resistance (N)	Theoretical resistance (N)
20	3.0	117.2	115.6
20	4.5	147.0	137.2
20	6.0	166.0	158.8

4.3 Pile group, 2x2

The load deflection curve for pile group, 2x2 is shown in Figure 5. This figure only shows two different L/ds and it clearly shows that ultimate lateral load resistance of pile increases with its L/d ratio. The ultimate lateral load resistances are 200N and 300N for L/d=20 and L/d=30 respectively. However, the ultimate lateral load resistances predicted by Patra-Pise methods are 190N and 280N respectively. Again, it indicates that this method could better and conservative prediction.

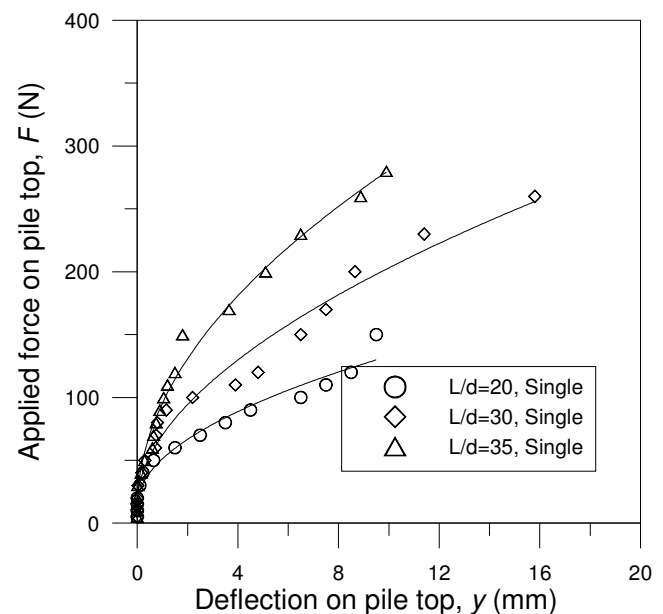


Figure 3. Load deflection curve for single piles for different L/d ratios.

4.4 Effect of pile spacing in group

Figure 6 shows that the centre to centre distance of piles in a group has strong influence on the ultimate lateral resistance of pile; it increases with increasing in piles c/c distance. However, the variation with c/c distance of piles is not linear. Figure 7 shows that the increment of lateral resistance for 3.0d to 4.5d is higher than the increment for 4.5d to 6.0d.

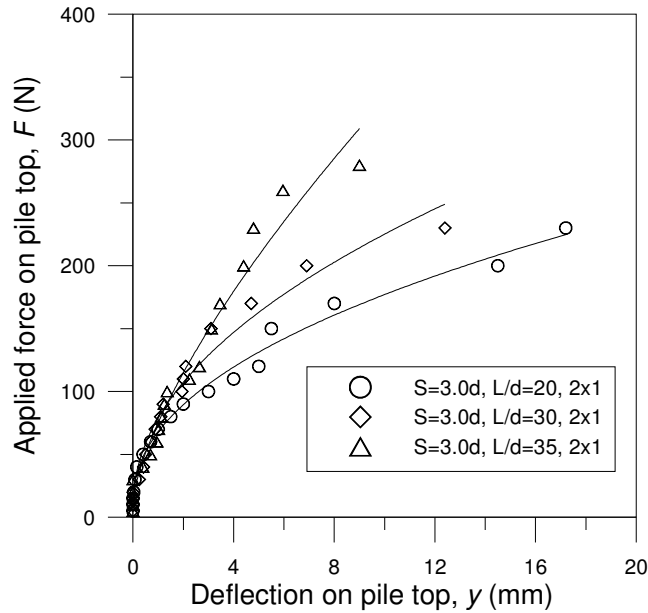


Figure 4. Load-deflection curve for pile group, 2x1

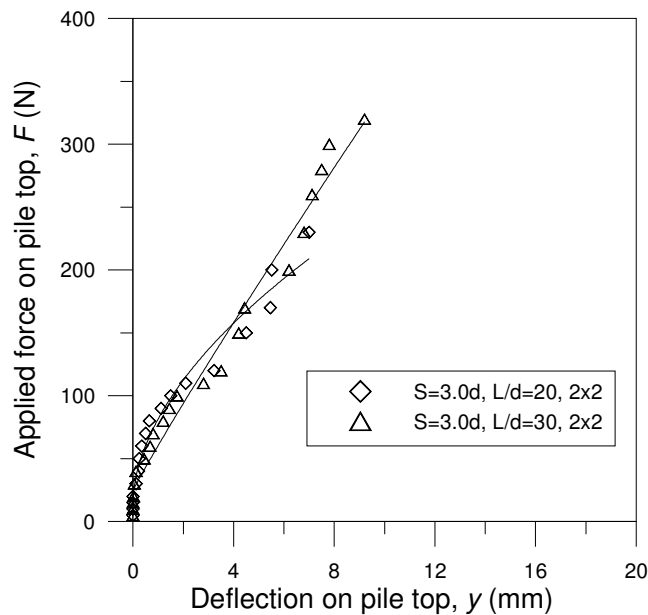


Figure 5. Load-deflection curve for pile group, 2x2

4.5 Group efficiency

The efficiency of lateral load resistance for pile group is calculated by the Equation 11 and they are presented in Figure 7. It shows that the increment of group efficiency for 3.0d to 4.5 is maximum and it reduces from 4.5d to 6.0d. This trend is seen in both groups of 2x1 and 2x2. However, it is interesting to

note that group efficiency for the group of 2x2 is less than for the group of 2x1. Thus, it indicates that pile spacing also very important for ultimate lateral resistance of pile.

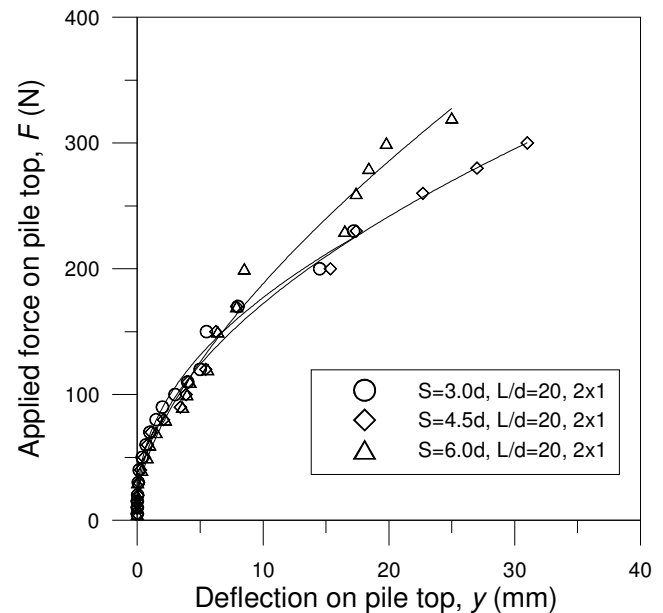


Figure 6. The effect of centre to centre distance between piles in group, 2x1.

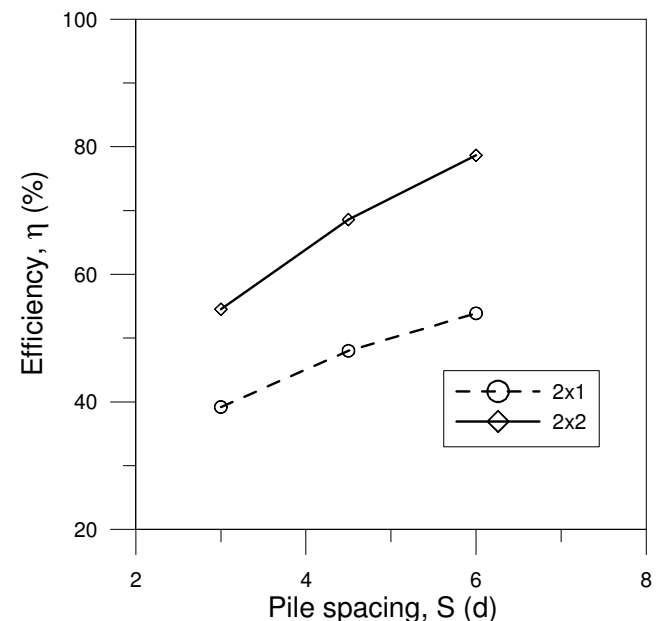


Figure 7. Variation of pile group efficiency with pile spacing between group, 2x1 and group, 2x2.

5 CONCLUSIONS

The following conclusions are drawn from the present study:

- The ultimate lateral load resistance of pile group depends on the length to diameter ratio of pile, pile friction angle, pile group geometry, spacing of piles in a group and sand placement density. The quantitative and

qualitative influence of those parameters has been investigated.

- The ultimate resistance of pile group increases with an increase in pile spacing. It has been found that resistance at 3d spacing is less than that of 4.5d spacing. Again resistance at 4.5d spacing also less than that of 6d spacing.
- Group efficiency of pile increases with an increase in pile spacing. It has also been found that the efficiency at 3d spacing is less than that of 4.5d and 6d spacing.
- Finally, the prediction by Patra & Pise method can give better prediction for pile groups whereas Meyerhof's method gives better prediction for single pile. Thus, none of these can be universally used for the prediction of lateral load resistances of pile or pile group.

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