LNG Vapor Barrier and Obstacle Evaluation: Wind-tunnel Simulation of 1987 Falcon Spill Series, Data Report

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Measurements of the behavior of simulated liquefied natural gas clouds dispersing over small-scale model placed in meteorological wind tunnels permits evaluations of the fluid physics of dense cloud movement and dispersion in a controlled environments. A large data base on the interaction of simulated LNG plumes with the Falcon test configuration of vapor barrier fences and vortex generators was obtained.

The purpose of the reported test program is to provide post-field-spill wind-tunnel experiments to augment the LNG Vapor Fence Field Program data obtained during the Falcon Test Series in 1987. The goal of the program is to determine the probable response of a dense LNG Vapor cloud to vortex inducer obstacles and fences, examine the sensitivity of results to various scaling arguments which might augment limit, or extend the value of the field and wind-tunnel tests, and identify important details of the spill behavior which were not predicted during the pretest planning phase.

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RESEARCH SUMMARY

Title	LNG Vapor Barrier and Obstacle Evaluation: Wind-Tunnel Simulation of 1987 Falcon Spill Series, Data Report Accession Code: GRI-??????
Contractor	Civil Engineering Department Colorado State University Fort Collins, Colorado 80526
Principal Investigator	Robert N. Meroney
Report Period	July 1987 - July 1989 Final Report
Objective	The purpose of the reported test program is to provide post-field-spill wind-tunnel experiments to augment the LNG Vapor Fence Field Program data obtained during the Falcon Test Series in 1987. The goal of the program is to determine the probable response of a dense LNG vapor cloud to vortex inducer obstacles and fences, examine the sensitivity of results to various scaling arguments which might augment, limit, or extend the value of the field and wind-tunnel tests, and identify important details of the spill behavior which were not predicted during the pretest planning phase.
Technical Perspective	A liquefied natural gas (LNG) spill would result in a cold LNG vapor plume, remaining negatively buoyant for a long period of time. The LNG plume could be diluted utilizing passive systems such as a vapor barrier fence or a vortex generator at or near the LNG spill location. Measurements of the behavior of simulated liquefied natural gas clouds dispersing over small-scale models placed in meteorological wind tunnels permits evaluations of the fluid physics of dense cloud movement and dispersion in a controlled environment. An evaluation of scaling arguments and limitations to laboratory testing may be obtained by pre- and post-simulation of a documented field scale spill of LNG such as the 1987 Falcon LNG Spill Tests.
Results	A large data base on the interaction of simulated LNG plumes with the Falcon test configuration of vapor barrier fences and vortex generators was obtained. The wind-tunnel experiments included replication of Falcon Tests 2 through 5 at simulated scales of 1:50, 1:100, 1:150 and 1:250. In addition some tests were performed with exaggerated density for the simulation gases, additional wind approach angles, and source release conditions.

Technical Approach

Wind-tunnel tests were performed in the Environmental Wind Tunnel at Colorado State University to simulate the micrometeorological and source conditions determined to occur at the Nevada test site during Falcon Tests 2, 3, 4, and 5. Approach wind flow conditions were carefully adjusted to simulate the characteristic surface roughness and consequent wind and turbulence profiles observed at the Nevada test site. The fences and vortex generator of various sizes were constructed from sheet metal, the model source-spider and spill-pond-plenum were designed to reproduce concentration time histories measured within the vapor fence. Each release was replicated up to five times per task while concentration time series were measured over a distributed grid within and outside the vapor barrier fence. Flow visualization was also used to document model spill behavior on TV tape. This report summarizes the sets of data obtained during the laboratory experiments. A subsequent report will present the results of field/model data comparisons.

Project Implications

(to be provided by project manager)

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LIST OF SYMBOLS

Dimension are given in terms of mass (m), length (L), time (t), moles (n), and temperature (T).

Symbol	Definition	
A	Area	$[L^2]$
C_p	Specific heat capacity at constant pressure	$[L^2t^{-2}T^{-1}]$
C_p^*	Molar specific heat capacity at constant pressure	$[L^2mt^{-2}T^{-1}n^{-1}]$
D	Surface Diameter	[L]
g	Gravitational acceleration	$[Lt^{-2}]$
h	Local plume depth	[L]
k	Thermal conductivity	$[mLT^{-1}t^{-3}]$
L	Length	[L]
M	Molecular weight	$[mn^{-1}]$
n	Mole	[n]
p	Velocity power law exponent	-
Q	Volumetric rate of gas flow	$[L^3t^{-1}]$
T	Temperature	[T]
ΔT	Temperature difference across some reference layer	[T]
t	time	[t]
u_*	Friction velocity	$[Lt^{-1}]$
U	Velocity	$[Lt^{-1}]$
V	Volume	$[L^3]$
W	Plume vertical velocity	$[Lt^{-1}]$
x	General downwind coordinate	[L]
y	General lateral coordinate	[L]
z	General vertical coordinate	[L]
z_o	Surface roughness parameter	[L]

LIST OF SYMBOLS (continued)

Symbol	Definition	
δ	Boundary layer thickness	[L]
Λ	Integral length scale of turbulence	[L]
ρ	Density	$[mL^{-3}]$
σ	Standard deviation	
χ	Mole fraction of gas component	
Ω	Angukar velocity of earth = 0.726×10^{-4} (radians/sec)	$[t^{-1}]$
ν	Kinematic viscosity	$[L^2t^{-1}]$

Subscripts

a	Air
Ar	Argon
b.o.	Boiloff
g	Gas
i	Cartesian index
LNG	Liquefied Natural Gas
m	Model
o	Reference Conditions
p	Prototype
s	Source Gas

1. INTRODUCTION

Natural gas is a highly desirable form of energy in the United States, since it is convenient to transport. A sophisticated distribution network already services a major part of the country. Recent efforts to expand this nation's natural gas supply include the transport of natural gas in a liquid state from distant gas fields and the temporary storage of surplus capacity in peak shaving facilities. To transport and store liquefied natural gas (LNG) it is cooled to a temperature of -162°C. At this temperature if a storage tank on a ship or land were to rupture and the contents spill out onto the earth's surface, rapid boiling of the LNG would ensue and the liberation of a flammable vapor would result [Fay, 1973; Burgess et al., 1972]. Past studies [American Gas Association, 1974; Neff et al., 1976] have demonstrated that the cold LNG vapor plume will remain negatively buoyant for a majority of its flammable lifetime. This hazard will extend downwind until the atmosphere has diluted the LNG vapor below the lower flammability limit (LFL; the maximum local concentration below which the gas is not flammable; 5 percent by volume for methane).

It is important that accurate predictive models for LNG vapor cloud physics be developed, so that the associated hazards of transportation and storage may be evaluated. Various industrial and governmental agencies have sponsored a combination of analytical, empirical and physical modeling studies to analyze problems associated with the transportation and storage of LNG. Field experiments on the dispersion of heavy gases started around 1970, but have included a very limited set of data on the mitigating effects of vapor barrier fences, obstacles, and water or steam spray curtains. As observed by Wiersma [1983] this means the focus of most field experiments has been on "idealized release scenarios, especially with no obstacle or terrain effects." These data

do not address the need for "real life" scenarios where such complexities and mitigating dispersion effects exist. Thus new field experiments planned by LLNL and financed by GRI and DOE were planned to provide additional field data on the diluting and hold up effectss of vapor barrier fences.

McQuaid [1982] advised that a limiting characteristic of large-scale field experiments that demand particular attention is the "inability to control the flow conditions..." Hence, he concludes careful preplanning is necessary, and recommends "...Wind tunnel and computer modeling and preliminary tests to try out the engineering of the experimental design...to maximize the probability of success." He further notes "such measures are assuredly cost effective in relation to the cost of an abortive effort in the field."

Hence wind-tunnel pre-field tests were performed to provide data to better define the relative influence of wind velocity, vortex inducers, spill rate, spill volume, and impoundment volume on dispersion in the design of the field experiments. The field experiments were conducted with the assist of the pre wind-tunnel tests data. A series of five large scale pressurized LNG spill tests called Falcon Series were conducted by the Lawrence Livermore National Laboratory (LLNL) for the Dapertment Of Transportation (DOT) and the Gas Research Institute (GRI) as a joint government/industry study in 1987 (Brown et al., 1988). The tests were performed over flat terrain at the Department Of Energy (DOE) Liquefied Gaseous Fuels Spill Test Facility (LGFSTF) in the Frenchman Flat Area of the Nevada Test Site (NTS) which is under the jurisdiction of the DOE Nevada Operations Office (DOE/NV).

The intent of the present wind-tunnel tests was to provide a basis for the analysis of the simulation of physical modeling tests using proper physical modeling techniques and to assist in the development and verification of analytical models. The environmental wind tunnel in the Fluid Dynamics and

Diffusion Laboratory at Colorado State University was operated over scale models in the facilities to measure concentrations of released gas resulting from given set of parameters (wind velocity, spill rate and spill volume). Scaling methods employed during physical modeling of atmospheric and plume motion are discussed in chapter 2. The details of the equipment and experimental measurements are described in chapter 3. Chapter 4 discusses the laboratory tests and the data obtained.

2. SIMILARITY DESCRIPTION

The general concept of similitude is described well in the section 2 of "Guideline for Fluid Modeling of Liquefied Natural Gas Dispersion, Volume II," for GRI [Meroney, GRI 86/0102.2]. The following description is referred to that guideline.

To obtain a predictive model for a specific plume dispersion problem one must quantify the pertinent physical variables and parameters into a logical expression that determines their interrelationships. This task is achieved implicitly for processes occurring in the atmospheric boundary layer by formulating the conservation equations for mass, momentum and energy. These equations together with site and source conditions and associated constitutive relations describe the actual physical interrelationship between the various independent (space and time) and dependent (velocity, temperature, pressure, density, concentration, etc.) variables.

These generalized conservation statements are too complex to be solved by present analytical or numerical techniques. It is also impossible to create a physical model at a reduced geometric scale for which exact similarity exists for all the dependent variables over all the scales of motion present in the atmosphere. Thus, one must resort to various degrees of approximation to obtain a predictive model. At present purely analytical or numerical solutions of plume dispersion are unavailable because of the classical problem of turbulent closure [Hinze, 1975]. Alternative techniques rely heavily upon empirical input from observed or physically modeled data. The empirical-analytical-numerical solutions have been combined into several different predictive approaches [Pasquill, 1974; Ermak et al. 1981; Havens, 1977]. The estimates of dispersion by these approaches are often crude; hence, they should only be used when the approach and site terrain are uniform and without obstacles. Boundary layer wind

tunnels are capable of accurately modeling plume processes in the atmosphere under certain restrictions. Since these restrictions are important and necessary for physical modeling the following sections are included for the completeness of this report.

2.1 PHYSICAL MODELING OF THE ATMOSPHERIC BOUNDARY LAYER

The atmospheric boundary layer is that portion of the atmosphere extending from ground level to a height of approximately 1000 meters within which the major exchanges of mass, momentum, and heat occur. This region of the atmosphere is described mathematically by statements of conservation of mass, momentum, and energy [Cermak, 1971]. The mathematical requirements for rigid laboratory-atmospheric-flow similarity may be obtained by fractional analysis of these governing equations [Kline, 1965]. This methodology is accomplished by scaling the pertinent dependent and independent variables and then casting the equations into dimensionless form by dividing by one of the coefficients (the inertial terms in this case). Performing these operations on such dimensional equations yields dimensionless parameters commonly known as:

Reynolds number	$Re = (UL/\nu)_r$	=	$\frac{\text{Inertial Force}}{\text{Viscous Force}}$
Bulk Richardson number	$Ri = [(\Delta T)/T)(L/U^2)g]_r$	=	$\frac{\text{Gravitational Force}}{\text{Inertial Force}}$
Rossby number	$Ro = (U/L\Omega)$	=	$\frac{\text{Inertial Force}}{\text{Coriolis Force}}$
Prandtl number	$Pr = [\nu/(\kappa/\rho C_p)]_r$	=	$\frac{\text{Viscous Diffusivity}}{\text{Thermal Diffusivity}}$
Eckert number	$Ec = [U^2/C_p(\Delta T)]_r$		

For exact similarity between different flows which are described by the same set of equations, each of these dimensionless parameters must be equal for both flow systems. In addition to this requirement, there must be similarity between the surface-boundary conditions and the approach flow wind field.

Surface-boundary condition similarity requires equivalence of the following features:

a. Surface-roughness distributions,

b. Topographic relief, and

c. Surface-temperature distribution.

If all the foregoing requirements are met simultaneously, all atmospheric scales of motion ranging from micro- to mesoscale could be simulated within the same flow field [Cermak, 1975]. However, all of the requirements cannot be satisfied simultaneously by existing laboratory facilities; thus, a partial or approximate simulation must be used. This limitation requires that atmospheric simulation for a particular wind-engineering application be designed to simulate most accurately those scales of motion which are of greatest significance for the given application.

2.1.1 Partial Simulation of the Atmospheric Boundary Layer

Strict equality of several of the forementioned parameters are unnecessarily restrictive and may be relaxed without causing a significant effect on the modeled flow field.

Reynolds Number

The Reynolds number (Re) strongly influences the kinematic and dynamic structure of turbulent flow within a boundary layer [Hinze, 1975]. Reynolds number equality implies $U_m = (L_p/L_m)U_p$. Re equality at a significantly reduced length scale would cause the model's flow velocity to be above sonic; hence, its

equality must be distorted. Since the larger scale motions dominate the transfer of momentum and mass within a boundary layer there is a range of Reynolds numbers for which gross flow characteristics, such as mean and rms velocity profiles, surface drag, plume dispersion, etc., are invariant [Hinze, 1975; Schlichting, 1968]. This invariant nature of the Reynolds number in turbulent flows makes reduced scale physical modeling of atmospheric flows possible. However there is a minimum Reynolds number below which the gross flow characteristics of the boundary layer are not invariant.

Halitsky [1969] reported that for dispersion in the vicinity of a cube placed in a near uniform flow field the Reynolds number required for invariance of the concentration distribution over the cube surface and downwind must exceed 11,000. Because of this invariance exact similarity of Reynolds parameter is neglected when physically modeling the atmosphere.

Prandtl number

Prandtl number equality guarantees equivalent rates of momentum and heat transport. Since it is dependent on the molecular properties of the working fluid which is air for both the atmosphere and the laboratory Prandtl number equality is always maintained.

Rossby number

The Rossby number magnitude controls the extent to which the mean wind direction changes with height. The effect of Coriolis force driven lateral wind shear on plume dispersion is only significant when the plume height is of the same order of magnitude as the boundary layer height. For the case of dispersion of LNG or a neutral plume near the ground level the Coriolis effect on the plume would be extremely small. Thus equality of this parameter need not be specified.

Eckert number

The Eckert number is the ratio of energy dissipation to the convection of energy (in air $Ec = 0.4*Ma^2(T_r/\Delta T_r)$ where Ma is the Mach number [Hinze, 1975]). In both the atmosphere and the laboratory flow the wind velocities and temperature differences are such that the Eckert number is very small; hence, it is neglected.

Quite often during the modeling of a specific flow phenomenon it is sufficient to model only a portion of a boundary layer or a portion of the spectral energy distribution. This relaxation allows more flexibility in the choice of the length scale that is to be used in a model study. When this technique is employed it is common to scale the flow by any combination of the following length scales, δ, the portion of the boundary layer to be simulated; Z_0, the aerodynamic roughness; Λ_i, the integral length scale of the velocity fluctuations, or λ_p, the wavelength at which the peak spectral energy is observed.

Unfortunately many of the scaling parameters and characteristic profiles are difficult to obtain in the atmosphere. They are infrequently known for many of the sites at which a model study is to be performed. To help alleviate this problem Counihan has summarized measured values of some of these different parametric descriptions for the atmospheric flow at many different sites and flow conditions.

2.2 PHYSICAL MODEL OF PLUME MOTION

In addition to modeling the turbulent structure of the atmosphere in the vicinity of a test site it is necessary to properly scale the plume source conditions. One approach would be to follow the methodology used in section 2.1, i.e., writing the conservation statements for the combined flow system followed

by fractional analysis to find the governing parameters. An alternative approach, the one which will be used here, is that of similitude [Kline, 1965]. The method of similitude obtains scaling parameters by reasoning that the mass ratios, force ratios, energy ratios and property ratios should be equal for both model and prototype. When one considers the dynamics of gaseous plume behavior the following nondimensional parameters of importance are identified [Halitsky, 1969; Hall, 1977; Hoot et al., 1974; Skinner and Ludwig, 1978; Snyder, 1981][1,2]

$$\text{Mass Flux Ratio } (M) = \frac{\text{mass flow of plume}}{\text{effective mass flow of air}} = \frac{(\rho WA)_g}{(\rho UA)_a} \overset{\text{at the source}}{=} \frac{\rho_s Q}{\rho_a U_a L^2}$$

$$\text{Momentum Ratio } (F) = \frac{\text{inertia of plume}}{\text{effective inertia of air}} = \frac{(\rho W^2 A)_g}{(\rho U^2 A)_a} = \frac{\rho_s Q^2}{\rho_a U_a^2 L^4}$$

$$\text{Densimetric Froude No. relative to the inertia of air } (Fr) = \frac{\text{effective inertia of air}}{\text{buoyancy of plume}} = \frac{(\rho U^2 A)_a}{g(\rho_g - \rho_a)\forall_g} = \frac{U_a^2}{Lg(\rho_s - \rho_a)/\rho_a}$$

$$\text{Densimetric Froude No. relative to inertia of the plume } (Fr_s) = \frac{\text{inertia of plume}}{\text{buoyancy of plume}} = \frac{(\rho W^2 A)_g}{g(\rho_g - \rho_a)\forall_g} = \frac{Q^2}{L^5 g(\rho_s - \rho_a)/\rho_s}$$

$$\text{Flux Froude No. } (\dot{Fr}) = \frac{\text{momentum flux of air}}{\text{buoyancy momentum flux of plume}} = \frac{(\rho U^2 A)_a}{Qg(\rho_g - \rho_a)(L/U_a)} = \frac{U_a^3 L}{Qg(\rho_s - \rho_a)/\rho_a}$$

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[1]It has been assumed that the dominant transfer mechanism is that of turbulent entrainment. Thus the transfer processes of heat conduction, convection, and radiation are negligible.

[2]The scaling of plume Reynolds number is also a significant parameter. Its effects are invariant over a large range thus making it possible to scale the distribution of mean and turbulent velocities and relax exact parameter equality.

$$\text{Volume Flux Ratio } (V) = \frac{\text{volume flow of plume}}{\text{effective volume flow of air}} = \frac{(WA)_g}{(UA)_a} = \frac{Q}{U_a L^2}$$

It is necessary to maintain equality of the plume's specific gravity, ρ_g/ρ_a, over the plume's entire lifetime to obtain simultaneous simulation of all of these parameters. Unfortunately a requirement for equality of the plume gas specific gravity leads to several complications in practice. It is important to examine each modeling situation and decide if an approximation to complete plume behavior may be employed without a significant loss in the similarity of the modeled plume structure. Section 2.2.1 discusses several different approximation methodologies which help formulate a physical model, and it addresses the errors incurred by such approximations.

2.2.1 Partial Simulation of Plume Motion

Often during physical modeling experiments the proper source density is obtained isothermally through the use of a heavy gas. Unfortunately, there are several thermal effects that can change the density history of a plume as it disperses. Heat transfer across plume boundaries is often small [Neff et al., 1981] even in the case of an LNG vapor plume and, when small, will not significantly affect the plume buoyancy.

The release of latent heat through the entrainment of humid air can have a very significant effect on the density history of a thermal plume. Figure 1 displays the variation of specific gravity from a spill of liquefied natural gas in atmospheres of different humidities. For a LNG vapor plume humidity effects are thus shown to reduce the extent in space and time of plume buoyancy dominance on plume motion. Hence a dry adiabatic model condition should be conservative. During an isothermal physical simulation of humid air/cold gas mixing large deviations in plume similarity would occur.

The restriction to an exact variation of the density ratio for the entire life of a plume is difficult to meet for LNG plumes which simultaneously vary in molecular weight and temperature. To emphasize this point more clearly, consider the mixing of two volumes of gas, one being the source gas, $\forall_s$, the other being ambient air, $\forall_a$. Consideration of the conservation of mass and energy for this system yields [Skinner and Ludwig, 1978][3]:

$$\frac{\rho_g}{\rho_a} = \frac{(\rho_s/\rho_a)\forall_s + \forall_a}{\left(\frac{T_a}{T_s}\forall_s + \forall_a\right)\left(\frac{(C_p^*)_s}{(C_p^*)_a}\forall_s + \forall_a\right)\left(\frac{(C_p^*)_s}{(C_p^*)_a}\frac{T_a}{T_s}\forall_s + \forall_a\right)^{-1}}$$

If the temperature of the air, T_a, equals the temperature of the source gas, T_s, or if the molar specific heat capacity, C_p^* is equal for both source gas and air then the equation reduces to:

$$\frac{\rho_g}{\rho_a} = \frac{(\rho_s/\rho_a)\forall_s + \forall_a}{\forall_s + \forall_a}$$

Thus for two prototype cases: 1) an isothermal plume and 2) a thermal plume which is mostly composed of air; it does not matter how one models the density ratio, thermally or isothermally as long as the initial density ratio is equal for both model and prototype. For the case of a thermal plume whose molar specific heat capacity is different from air, such as an LNG vapor plume, the modeling of the density history variation within the plume can only be approximate. Figure 2 displays the variation in the density history behavior for the isothermal simulation of an LNG vapor plume. Figure 3 displays the variation in the plume cross sectional area as the plume mixes with air for this same situation. Consideration of these two figures suggests that, although an isothermal

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[3]The pertinent assumption in this derivation is that the gases are ideal and properties are constant.

simulation of an adiabatic LNG vapor cloud as it entrains dry air is not exact, it is a good approximation to actual behavior.

Scaling of the effects of heat transfer by conduction, convection, or radiation cannot be reproduced when the model source gas and environment are isothermal. Fortunately in a large majority of industrial plumes the effects of heat transfer by conduction, convection, and radiation from the environment are small enough that the plume buoyancy essentially remains unchanged. In the specific case of a cryogenic liquid spill the influence of heat transfer on cold dense gas dispersion can be divided into two phases. First the temperature (and hence specific gravity) of the plume as exit from a containment tank and surrounding dike area is dependent on the thermal diffusivity of the tank-dike-spill surface materials, the volume of the tank-dike structure, the actual boiloff rate, and details of the spill surface geometry. A second plume phase involves the heat transfer from the ground surface beyond the spill area which lowers plume density.

It is tempting to try to simulate the entire transient spill phenomenon in the laboratory including spill of cryogenic fluid into the dike, heat transfer from the tank and dike materials to the cryogenic fluid, phase change of the liquid and subsequent dispersal of cold gas downwind. Unfortunately, the different scaling laws for the conduction and convection suggest that markedly different time scales occur for these various processes as the length scale changes. Since the volume of dike material storing sensible heat scales with the cube of the length scale whereas the pertinent surface area scales as the square of the length scale one perceives that heat is transferred to a model cold plume much too rapidly within the model containment structures. This effect is apparently unavoidable since a material having a thermal diffusivity low enough to compensate for this effect does not appear to exist. Calculations for the

full-scale situation suggest minimal heating of a cold gas plume by the tank-dike structure; thus it may suffice to cool the model tank-dike walls to reduce the heat transfer to a cold model vapor and study the resultant cold plume.

Boyle and Keevone released under equivalent conditions room temperature propane and LNG onto a water surface. The density of propane at ambient temperatures and methane at -161°C relative to air are the same. Using the modified Froude number as a model law they concluded that the dispersion characteristics were equivalent within experimental error.

A mixture of 50 percent helium and 50 percent nitrogen pre-cooled to 115°K was released from model tank-dike systems by Meroney et al. [1977], to simulate equivalent LNG spill behavior. There was no guarantee that these experiments reproduced quantitatively similar situations in the field. Rather it was expected that the gross influence of different heat transfer conditions could be determined. Since the turbulence characteristics of the flow are dominated by roughness, upstream wind profile shape, and stratification one expects the Stanton number in the field will equal that in the model, and heat transfer rates in the two cases should be in proper relation to plume entrainment rates. On the other hand, if temperature differences are such that free convection heat transfer conditions dominate, scaling inequalities may exist; nontherless, model dispersion rates would be conservative.

Visualization experiments performed by Neff et al. [1986] with equivalent dense isothermal and dense cold plumes revealed no apparent change in plume geometry. Concentration data followed similar trends in both situations. No significant differentiation appeared between insulated versus heat conducting ground surfaces or neutral versus stratified approach flows.

The influence of latent heat release by moisture upon the buoyancy of a plume is a function of the quantity of water vapor present in the plume and the humidity of the ambient atmosphere. Such phase change effects on plume buoyancy can be very pronounced in some prototype situations. A reasonably complete simulation may be obtained in some situations even when a modified density ratio ρ_s/ρ_a is stipulated. The advantage of such a procedure is demonstrated most clearly by the statement of equality of Froude numbers.

$$\left[\frac{U_a^2}{\left(\frac{\rho_s}{\rho_a} - 1\right)L_g}\right]_m = \left[\frac{U_a^2}{\left(\frac{\rho_s}{\rho_a} - 1\right)L_g}\right]_p$$

Solving this equation to find the relationship between model velocity and prototype velocity yields:

$$(U_a)_m = \left[\frac{S.G._m - 1}{S.G._p - 1}\right]^{1/2} \left[\frac{1}{L.S.}\right]^{1/2} (U_a)_p$$

where S.G. is the specific gravity, (ρ_s/ρ_a), and L.S. is the length scale, (L_p/L_m). By increasing the specific gravity of the model gas compared to that of the prototype gas, for a given length scale, one increases the reference velocity used in the model. It is difficult to generate a flow which is similar to that of the atmospheric boundary layer in a wind tunnel run at very low wind speeds. Thus the effect of modifying the model specific gravity extends the range of flow situations which can be modeled accurately. But unfortunately during the adjustment of the specific gravity of the model gases at least two of the four similarity parameters listed must be neglected. The options as to which two of these parameters to retain, if any, depends upon the physical situations being modeled.

(1) Froude No. Equality

Momentum Ratio Equality

Mass Ratio Inequality

Velocity Ratio Inequality[4]

(2) Froude No. Equality

Momentum Ration Inequality

Mass Ratio Inequality

Velocity Ratio Equality

Both of these schemes have been used to model plume dispersion downwind of an electric power plant complex by Isyumov [1976] and Meroney [1974] respectively.

The modeling of the plume Reynolds number is relaxed in all physical model studies. This parameter is thought to be of small importance since the plume character will be dominated by background atmospheric turbulence soon after its emission. But, if one was interested in plume behavior near the source, then steps should be taken to assure that the plume in the model is fully turbulent.

2.2.2 Concentration Scaling Theory

Most plume studies measure the concentration magnitudes at distances far downwind from the source. In the limit as concentrations approach zero, the conventional concentration scaling laws for steady state plumes were developed [Pasquill, 1974]. The form of this expression is:

$$K(x) = \chi U_H L^2 / (\frac{T_a}{T_s}) Q \qquad (1)$$

where T_a and T_s are the temperatures of the ambient air and the source gas

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[4]When this technique is employed distortion in velocity scales or similarity volume flow rates requires that a correction be applied to the measured concentration field.

respectively. Q in this expression is the total source gas flow rate evaluated at source conditions. When modeling the plume at a reduced scale the function K(x) is determined by experimental measurements usually in an isothermal setting where $T_a = T_s$. Provided that the proper similarity requirements were satisfied then the function K(x) will be equal for field and model plumes. The effects of Volume Flux Ratio (V) distortion and source gas temperature differences between model and prototype are corrected by the expression. This technique is completely satisfactory in the limit as concentration approaches zero. In the case of modeling plume concentration in the near field, such as is the case with flammable plumes, this relationship is not satisfactory. The problems lie in the asymptotic behavior as the concentration, χ, approaches one. $K(0) = U_H L^2/(QT_a/T_s)$ indicates that K is not a function of the downwind position, x, alone. It is a function of both x and $U_H L^2/(QT_a/T_s)$. To alleviate these problems the following generalized concentration scaling methodology was formulated by Neff [1989].

Figure 4 will aid in understanding the derivation of this generalized concentration scaling methodology. Continuity of total molar flow rate of source gas at the source (section A-A) and at some downwind cross-sectional area (section B-B) requires that:

$$\dot{n}_s = \int_{B-B} \dot{n}''_s \, dB \, , \tag{2}$$

where $\dot{n}_s$ is the total molar flow rate of source gas and $\dot{n}''_s$ is the molar flux of source gas through some differential area dB. Definition of concentration, χ, requires that:

$$\chi = \dot{n}''_s/(\dot{n}''_s+\dot{n}''_a). \tag{3}$$

Rewriting this expression as;

$$\dot{n}''_s = \dot{n}''_a \, \chi/(1-\chi) \tag{4}$$

and substituting it into expression for $\dot{n}_s$ yields

$$\dot{n}_s = \int_{B\text{-}B} \left(\frac{\chi}{1-\chi}\right)\dot{n}''_a \, dB \ . \tag{5}$$

The mean value theorem of integral calculus allows one to rewrite the equation as

$$\dot{n}_s = \left(\frac{\chi(\xi,\eta)}{1 - \chi(\xi,\eta)}\right) \int_{B\text{-}B} \dot{n}''_a \, dB \ . \tag{6}$$

where $\chi(\xi,\eta)$ is the value of χ at some point, (ξ,η), on the surface B-B. The total molar flow rate of air across the entire plume boundary up to section B-B (surface σ) and the molar flow rate of air through section B-B are equal; hence,

$$\dot{n}_s = \left(\frac{\chi(\xi,\eta)}{1 - \chi(\xi,\eta)}\right) \int_{\sigma} \dot{n}''_a \, d\sigma \ . \tag{7}$$

Letting $\dot{n}_s = PQ/(\bar{R}T_s)$ and $\dot{n}''_a = Pu_e/(\bar{R}T_a)$, where u_e is the entrainment velocity of air across the boundary σ, dividing the entire equation by $\chi/(1-\chi)$, where χ is evaluated at the point of interest on the surface B-B, say $\chi_{\text{℄}}$, and rearranging the equation cancelling constant quantities such as P and $\bar{R}$ yields:

$$\left(\frac{T_s}{T_a}\right)\left(\frac{\chi_{\text{℄}}}{1 - \chi_{\text{℄}}}\right) \frac{\int_\sigma u_e d\sigma}{Q} = \frac{\chi_{\text{℄}}/(1-\chi_{\text{℄}})}{\chi(\xi,\eta)/(1-\chi(\xi,\eta))} \ . \tag{8}$$

The expression on the right side of this equation is a function of the χ profile at the surface B-B; thus, it is a function of downwind position, x, only. Provided that two plumes satisfy the proper similarity requirements then,

$$\frac{(u_e)_m}{(u_e)_p} = \frac{(U_H)_m}{(U_H)_p} \quad (\text{or } u_e \propto U_H), \ \sigma_m/\sigma_p = L_m^2/L_p^2 \ (\text{or } \sigma \propto L^2), \tag{9}$$

and the concentration profiles will have the same form. Utilizing these factors, the final form of a concentration scaling law that relates the concentration distributions in plumes that are physically similar is:

$$\left(\frac{T_s}{T_a}\right)\left(\frac{\chi}{1-\chi}\right)\left(\frac{U_H L^2}{Q}\right) = K(x) \ . \tag{10}$$

Some observations on the utility of this expression are summarized below.

- As concentration, χ approaches zero this expression becomes the conventional form presented in the first part of this section.
- Note that the quantity $U_H L^2/Q$ is the inverse of the Volume Flux Ratio, V; thus this expression corrects the entire concentration field for distortions in the similarity of this parameter as specified in some of the enhanced simulation techniques described in section 2.2.1.
- The quantity T_s/T_a corrects for the fact that concentrations measured at spatially similar points will be different for a thermal plume than for an isothermal plume.
- The function K(x) can be viewed quite simply in the following format

$$K(x) = \frac{\dot{n}_a/\dot{n}_s}{\dot{n}_a''/\dot{n}_s''} \quad . \tag{11}$$

  Thus it is the ratio of the quantity $\dot{n}_a/\dot{n}_s$ evaluated for the entire plume to that same quantity evaluated at a single point within the plume.
- Given the equality of $K(x)_m = K(x)_p$ then a convenient formula for the conversion from a modeled concentration to a prototype concentration is given by

$$\chi_p = \frac{\chi_m}{\chi_m + (1-\chi_m)[(T_a/T_s)V]_m[(T_a/T_s)V]_p} \quad , \tag{12}$$

  where $V = Q/U_H L^2$.

  For reciprocal conversion from prototype to model simply exchange the m's and p's.
- If the indeterminant behavior of this formulation of K(x) as $x \to 1$ is bothersome note that by the transformation

$$K'(x) = K(x)/(K(x)+1) \tag{13}$$

this problem is alleviated.

$$K'(x) = \frac{\chi}{\chi + (1-\chi)[(T_a/T_s)Q/U_H L^2]} \tag{14}$$

This new function $K'(x)$ has the convenient property that as $x \to 0$, $K'(x) \to 0$ and as $x \to 1$, $K'(x) \to 1$.

It is reemphasized that $K(x)$ is only a universal function for plumes that are similar in both entrainment physics and normalized concentration variation in downwind plume cross-sections. All passive plumes in the absence of wake effects and significant initial momentum meet these conditions; hence, $K(x)$ should be a universal function for passive plume dispersion. Measurements on plumes of this type have universally confirmed such correlations. As the source and near field factors such as initial momentum, building wakes, and buoyancy effects become more dominant than the background flow in determining the entrainment physics and plume profiles, the universal character of $K(x)$ is lost. For the specific case of downwind dispersion from negatively buoyant sources it is easily envisioned that, unless the buoyancy and inertial effects are properly matched, the resultant plume profiles will be drastically different.

2.3 MODELING OF PLUME DISPERSION FOR PRESENT STUDY

In the sections above a review of the extent to which wind tunnels can model plume dispersion in the atmospheric boundary layer and concentration scaling theory has been presented. In this section these arguments will be applied to the specific case of an LNG spill by LLNL at the Department of Energy spill site in Nevada.

2.3.1 Physical Modeling of the Field Site Atmospheric Surface Layer

In order to obtain a proper wind-tunnel scaling of the Field Site surface layer winds the approach flow characteristics must be similar. To achieve these upstream flow conditions, the wind tunnel must be modified through the introduction of surface roughness elements and boundary layer trip devices in such a way that similarity is obtained in both the mean velocity variation with height and the characteristic length scales of turbulence. A convenient parameter which characterizes the mean velocity variation with height is Z_0, the aerodynamic roughness height [Schlichting, 1968],as defined by log-linear description of velocity variation in a boundary layer. A convenient parameter which characterizes the scales of turbulence velocity fluctuations is Λ_i, the integral scale of turbulence [Hinze, 1975].

The wind-tunnel pre-field tests had been conducted by Neff et al. [1986]. The conditions in the wind tunnel were adjusted until both of these length scales were in the same proportion to their atmospheric equivalents (obtained by Counihan [1975]) as the geometric length scale chosen for the model terrain construction. The optimal geometric length scale was chosen to be 1:100. In this present study, four different length scale ratios (LSR) were tested including 1:50, 1:100, 1:150 and 1:200.

The exposed cardboard corrugation for the upstream was introduced to obtain the appropriate wind-tunnel scaling of the upstream Field Site surface layer winds with models of 1:50 and 1:100 LSR. The approach flow characteristics with LSR of 1:150 and 1:200 were simulated with smooth floor.

2.3.2 Physical Modeling of the Field Site LNG Spill Plume

The buoyancy of a plume resulting from an LNG spill is a function of both the mole fraction of methane and temperature. If the plume entrains air adiabatically, then the plume would remain negatively buoyant for its entire lifetime. If the humidity of atmosphere were high then the state of buoyancy of the plume will vary from negative to weakly positive.

Since the adiabatic plume assumption will yield the most conservative downwind dispersion estimates this situation was simulated in the pre-field test by Neff et al. [1986]. (Conservative is defined here to be highest peak concentrations furthest downwind.) Several investigators have confirmed that the Froude number is the parameter which governs plume spread rate, trajectory, plume size and entrainment during initial dense plume dilution [Hoot et al., 1974; Boyle et al., 1973; Bodurtha, 1961; van Ulden, 1974]. The strict equality of model and prototype specific gravity was relaxed so that pure Argon gas (specific gravity at 1.38) could be used for the model source gas. The Froude number was maintained at equal values by adjusting reference wind speed.

Argon provides almost eight times the detection sensitivity for instantaneous concentration measurements as the carbon dioxide used in previous studies [Meroney et al., 1977]. The variation of specific gravity with equivalent observed mole fraction of methane for these different gases is plotted in Figure 5. The use of an isothermal dense model gas such as Argon instead of cold methane vapor also results in a slight distortion of the local dynamic forces acting on equivalent plume volumes as the gas mixes. Unfortunately this distortion is not conservative. The thermal capacitance properties of methane result in plumes which are more dense than the model equivalent. This results in less rapid prototype mixing. Analytical approximations based on the integral entrainment box model of Fay [1980] suggest that buoyancy forces are more at

equivalent time and space positions during adiabatic mixing of methane. Let Fr = $[U(h)^2]/g(\Delta\rho/\rho_a)h]$ be a local Froude number, where h is local plume depth, U(h) is wind speed at plume depth, h, and $\Delta\rho/\rho_a$ is a local density difference ratio. Then given a power law wind profile $U(h) \sim h^p$ one finds

$$\frac{Fr_{\text{isothermal gas}}}{Fr_{\text{LNG vapor}}} = \frac{(1+\chi S)(\beta+(1-\beta)\theta)}{((1+\chi S)+(1+S)(1-\beta)\theta)} \left[\frac{(1+\chi S+\chi(1+S)\theta}{(1-\chi\theta)(1+\chi S)}\right]^{2p} \left[\frac{RLNG}{R_{iso}}\right]^{2-4p}$$

where χ = mole fraction methane vapor

R = local plume spread

$\beta = 1 - M_a/M_s \approx -0.81$

$\theta = 1 - T_s/T_a \approx 0.6$

$S = (Cp_s^*/Cp_a^* - 1) \approx 0.2$

p = velocity power law exponent ≈ 0.5.

The variation of this Froude number ratio with equivalent mole fraction methane is plotted in Figure 6. Over most of the concentration range where buoyancy forces are dominant the variation of Froude number is reasonably simulated by the isothermal model gas.

In addition to Argon gas, Freon 12 gas (specific gravity at 4.2) was used to simulate the test (Falcon 4) conducted at the Field Site for the geometric length scale of 1:150 and 1:200. Because of the increased specific gravity, for a given length scale, the reference velocity in the model was increased.

The actual source condition, boiloff rate per unit area over the time duration of the spill, for a spill of LNG on land is highly unpredictable. However, there were data available on the area inside the fence of the different LNG tests conducted at the Field Site thus the source conditions were approximated by assuming a steady boiloff rate for the duration of the spill over a constant area and adjusting the combination of gas release from the modeled evaporation pond and spider.

Since the thermally variable prototype gas was simulated by an isothermal simulation gas, the gas concentration measurements observed in the model must be adjusted to equivalent concentrations that were measured in the field. This relationship is:

$$\chi_p = \frac{\chi_m}{\chi_m + (1 - \chi_m)\frac{T_s}{T_a}}$$

where

χ_m = volume or mole fraction measured during the model tests,

T_s = source temperature of LNG during field conditions,

T_a = ambient air temperature during field conditions, and

χ_p = volume or mole fraction in the field.

3. DATA ACQUISITION AND ANALYSIS

In this section the method used to make laboratory measurements and the techniques used to convert these measured quantities to meaningful field equivalent quantities are discussed. Attention has been drawn to the limitations in the techniques in an attempt to prevent misinterpretation or misunderstanding of the test results presented in the next chapter. Some of the methods used are conventional and need little elaboration.

3.1 WIND-TUNNEL FACILITIES

The Environmental Wind Tunnel (EWT) shown in Figure 5 was used for all tests performed. This wind tunnel, especially designed to study atmospheric flow phenomena, incorporates special features such as an adjustable ceiling, rotating turntables, transparent boundary walls and a long test section to permit reproduction of micrometeorological behavior at much smaller geometric length scales. Mean wind speeds of 0.15 to 14 m/s can be obtained in the EWT. A boundary layer depth of 1 m thickness at 6 m downstream of the test entrance can be obtained with the use of the vortex generators at the test section entrance and surface roughness on the floor. The flexible test section roof on the EWT is adjustable in height to permit the longitudinal pressure gradient to be set to zero. The vortex generators at the tunnel entrance were followed by 10 m of smooth floor.

3.2 MODEL

From the wind-tunnel pre-field test [Neff et al., 1986] it was decided that the best reproduction of the surface wind characteristics would be at a model scale of 1:100 based on atmospheric data over sites similar to that of the field site. However, four different model scales including 1:50, 1:100, 1:150 and

1:200 were tested to investigate the reproducibility of various model scales. Figure 6 displays the layout of the source area, the vortex generating barrier and the vapor fence. The field dimensions are in meters and the model dimensions are in centimeters. To insure a uniform release of source gas over the modeled evaporation pond the 58.4 cm × 39.6 cm area was sectioned into twelve squares for the model scale of 1:100. The evaporation pond was taped over to the proper size for the model scales of 1:150 and 1:200. In the case of the model scale of 1:50, the modeled pond used for the pre-field test and the present modeled pond for the model scale of 1:100 were combined. Figure 7 through 9 show the locations of concentration measurements in the wind tunnel. All dimensions were converted into field values. The simulant gas, Argon and Freon 12, stored in a pressurized cylinder was directed through a solenoid valve, a flowmeter, and into the square area mounted in the model's vapor containment area and pipe spider.

3.3 FLOW VISUALIZATION TECHNIQUES

Smoke was used to define plume behavior over the China Lake site. The smoke was produced by passing the simulation gas through an Rosco Model 8215 Fog/Smoke Machine located outside the wind tunnel. The plume was illuminated with arc-lamp beams. A visible record was obtained with a VHS video camera.

3.4 WIND PROFILE AND TURBULENCE MEASUREMENTS

Velocity profile measurements, reference wind speed conditions and turbulence measurements were obtained with a Thermo-Systems Inc. (TSI) 1050 anemometer and a TSI model 1210 hot-film probe. Since the voltage response of these anemometers is nonlinear with respect to velocity, a multi-point calibration of system response versus velocity was utilized for data reduction.

The velocity standard used in the present study is depicted in Figure 10. This velocity calibrator consisted of a Matheson model 8116-0154 mass flowmeter, a Yellowsprings thermistor and a profile conditioning section designed and calibrated by the FDDL staff at CSU. The mass flowmeter measures mass flow rate independent of temperature and pressure, the thermistor measures the temperature at the exit conditions and the profile conditioning section forms a flat velocity profile of very low turbulence at the position where the probe is to be located. Incorporating a measurement of the ambient atmospheric pressure and a profile correction factor permits the calibration of velocity at the measurement station from 0.1 to 2.2 m/s ± 20 percent or ± 5.0 cm/s, whichever is smaller. During calibration of the single film probe, anemometer voltage response values over the velocity range of interest were fit to a King's law expression [Sandborn, 1972] with a variable exponent. The accuracy of this technique is approximately ± 2 percent of the actual longitudinal velocity.

The velocity sensors were mounted on a vertical traverse and positioned over the measurement location in the wind tunnel. The anemometer's responses were fed to a IBM AT analog-to-digital converter and then directly to a IBM AT computer for immediate interpretation.

3.5 CONCENTRATION MEASUREMENTS

To obtain the concentration time histories at points downwind of the spill site a rack of eight hot-wire aspirating probes were designed and constructed by Neff [1986] at Colorado State University. A layout of this design is presented in Figure 11. The films on this probes were replaced with 0.005 in. platinum wire to improve signal-to-noise characteristics. The eight instantaneous concentration sensors were connected to an eight-channel TSI hot-wire anemometer system. The output voltages from the TSI unit are conditioned

for input to the analog-to-digital converter by a DC-suppression circuit, a passive low-pass filter circuit set to 100 Hz, and an operational amplifier of times five again. Furthermore, Wavetek filters with 40 Hz cut-off were used in some cases to eliminate significant noise. A schedule of this process is shown in Figure 12.

3.5.1 Aspirating Hot-Wire Probes

Hot-wire katharometer probes measure rapid concentration fluctuations. Such probes permit one to specify concentration spectra, concentration standard deviation, peak to mean ratios, etc. at any point. The basic principles governing the behavior of aspirating hot-wire probes have been discussed by Blackshear and Fingerson [1962], Netterville [1979] and Kuretsky [1967]. A vacuum source sufficient to choke the flow through the small orifice just downwind of the sensing element was applied. The wire was operated in a constant temperature mode at a temperature above the ambient air temperature. A feedback amplifier maintained a constant overheat resistance through adjustment of the heating current. A change in output voltage from this sensor circuit corresponds to a change in heat transfer between the hot wire and the sampling environment.

The heat transfer rate from a hot wire to a gas flowing over it depends primarily upon the wire diameter, the temperature difference between the wire and the gas, the thermal conductivity and viscosity of the gas and the gas velocity. For a wire in an aspirated probe with a sonic throat, the gas velocity can be expressed as a function of the ratio of the probe cross-sectional area at the wire position to the area at the throat, the specific heat ratio and the speed of sound in the gas. The latter two parameters, as well as the thermal conductivity and viscosity of the gas mentioned earlier, are determined by the gas composition and temperature. Hence, for a fixed probe geometry and wire

temperature, the heat transfer rate or the related voltage drop across the wire is a function of only the gas composition and temperature. Since all tests performed in this study were in an isothermal flow situation the wire's response was only a function of gas composition.

During probe calibration known compositions of either Argon-Air or Freon 12-Air mixtures were passed through a pre-heat exchanger to condition the gas to the tunnel temperature environment. These known compositions for the Argon-Air calibration systems were drawn from bottles of prepared gas composition provided by Matheson Laboratories. For the Freon 12-Air calibration system known compositions were produced from pure Freon 12 and pure Air passed through a Matheson gas proportioner. An overheat ratio (temperature of wire/ambient temperature) of 1.65 was used to maximize signal response while maintaining acceptable noise and signal drifting levels.

3.5.2 Errors in Concentration Measurements with Aspirating Probes

The effective sampling area of the probe inlet is a function of the probe's aspiration rate and the distribution of approach velocities of the gases to be sampled. The effective sampling area was approximately 0.5 cm^2.

The travel time from the sensor to the sonic choke limits the upper frequency response of the probe. At high frequencies the correlation between concentration fluctuations and velocity fluctuations (velocity fluctuations are a result of the changes of sonic velocity with concentration) at the sensor begin to decline. The CSU aspirated probe is expected to have a 1000 Hz upper frequency response, but to improve signal to noise characteristics the signal was filtered at 100 Hz. This is well above the expected frequencies for concentration fluctuations in this test program.

The accumulative error[1], due to the combined effect of calibration uncertainties and nonlinear voltage drifting during the testing time, is estimated to be approximately ±20 percent of component value in the range of 5-15 percent equivalent methane concentrations.

3.5.3 Test Procedure

The test procedure consisted of:

(1) Setting the proper tunnel wind speed,

(2) Releasing a metered mixture of source gas from the release area source,

(3) Withdrawing gas samples over a fixed time period, from the designated sampling locations, and

(4) Storing the time series of concentration response from each probe into a IBM AT computer.

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[1]These errors are estimated ranges of approximately two to three standard deviations.

4. TEST PROGRAM AND DATA

Sixteen different sets of post-field tests were simulated in the Environmental Wind Tunnel (EWT) at Colorado State University at length scale ratios of 1:50, 1:100, 1:150 and 1:200. Video tape movies of simulation of the Falcon 4 test with length scale of 1:100 were obtained from several points of view. Each test was repeated 5 times to investigate concentration variation. Table 1 summarizes the post-field simulation tests conducted. It specifies the array angle of the model and the combination of source gas (from the plenum and spider). Figure 12 shows the spatial locations of the different measurement points.

The measurements at X = 250 m with length scale of 150 and 200 were not performed since the measurement locations were not specified in the field test report provided. For length scale of 50, the measurements were not taken because of the spatial limitation of the EWT. Falcon 1 tests were not conducted because the wind velocity was too low to simulate in the EWT. The simulation with the length scale of 1:50 for Falcon 3 was not performed since the gas flow rate was too large to supply through the model source tube.

In addition to the simulations of field tests, additional tests were performed with different array angles to evaluate the effects of wind direction variation during the period of measurements.

Different combinations of source gas (from the plenum and spider) were evaluated to select the best combination to simulate the field test.

Table 2 summarizes the comparison of parameters of prototype and model. The following equations were used to convert field values to model values.

$$L_m = \frac{1}{L.S.} L_p,$$

$$U_m = \left(\frac{S.G._m - 1}{S.G._p - 1}\right)^{1/2} \left(\frac{L_m}{L_p}\right)^{1/2} U_p,$$

$$Q_m = \left(\frac{S.G._m - 1}{S.G._p - 1}\right)^{1/2} \left(\frac{L_m}{L_p}\right)^{5/2} Q_p,$$

$$t_m = \left(\frac{S.G._p - 1}{S.G._m - 1}\right)^{1/2} \left(\frac{L_m}{L_p}\right)^{1/2} t_p,$$

where L is length, U is wind speed, Q^1 is plume vapor flow rate at the source, t is time, L.S. is length scale factor, and S.G. is the plume specific gravity at the source. The subscript m and p indicate model and prototype (field) conditions respectively.

This present study was designed to provide a basis for the analysis of the simulation of physical modeling to the field tests using proper physical modeling techniques and to assist in the development and verification of analytical models. All tests were performed in the Environmental Wind Tunnel described in section 3.1. The plumes were released from an area source mounted to the wind tunnel floor and/or a spider. The floor in the vicinity of the plume was always flat and smooth with no obstacles other than the vapor barrier fence and vortex generator to cause wake effects.

Section 4.1 discusses the approach wind field for all tests. Section 4.2 discusses the data from additional tests with the change of array angle and source combinations. Section 4.3 summarizes the data obtained for all the simulations of continuous release concentration tests.

4.1 VELOCITY DATA RESULTS

The technique employed in the acquisition of upwind velocity information are discussed in section 3.4. The major purpose for laboratory plume dispersion

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[1]LNG vapor at the boiloff temperature of -162°C requires 253 times the volume as LNG.

measurements is to predict plume behavior at atmospheric scales. A critical requirement for accurate extrapolation is similarity in the distribution od upwind turbulent velocities. To demonstrate similarity between the model and prototype wind fields it is sufficient to compare the vertical variation of mean velocity, rms velocity and turbulent intensity. Sections 4.1.1 and 4.1.2 discuss model to field comparisons for the mean velocity and rms velocity.

4.1.1 Mean Wind Profiles

Figures 13 through 16 show the velocity variation of mean velocity for Falcon 2, 3, 4 and 5 respectively, with various length scale ratios (LSR). In each figure the mean wind profile for the field test is compared to those of physically modeled cases with different LSR. In each figure the solid line represents the result. According to these figures, the roughness length characterizing the field condition was, z_o = 0.003~0.096m, and it was reasonably simulated with models of various length scales.

Figures 17 through 20 display the power law correlation of the mean velocity profiles of the field tests and compare the profiles to those of modeled tests. If the power index, p, could describe the entire profile then the terrain conditions predicted would be invariant with respect to the chosen length scale. As seen in this figure there is a systematic variation of the index p with height. The index p becomes larger with decreasing height, which is essentially equivalent to the observed scale dependence of z_o.

Figures 21 through 24 show the characteristic velocity profiles of post-field tests with various length scales. The exposed cardboard corrugation for the upstream was introduced with length scales of 1:50 and 1:100. Smooth floor was used for the upstream with length scales of 1:150 and 1:200. It is shown from figures that the characteristic velocity profiles are reasonably similar

for all LSR. However the mean velocity profiles show reasonable overlap over a portion of the shear layer.

4.1.2 Turbulent Intensity Profiles

The turbulent intensity of a turbulent velocity is defined as the rms velocity divided by the local mean velocity. Figures 16 through 19 show the variation in this turbulent intensity with height for both the field tests and the simulation tests. As mentioned in section 4.1.1 the mean velocity profile for the field and simulation tests overlapped; thus the differences in intensity are attributed solely to a change of magnitude of the rms velocity fluctuations. It is shown that the variation of turbulent intensity over the section from the ground to 16 m was from 6 percent to 20 percent for runs with mean velocity from 4.0 m/s to 6.8 m/s at the reference height of 9 m.

Since the present problem is to simulate the near field dispersion of a heavy gas plume released at the ground level it is only necessary that there be a good comparison of the turbulent intensities near the ground. It appears from the profiles that there is not a specific length scale which fits most of the profile of the field tests. Figures 20 through 23 are the characteristic turbulent intensity profiles scaled by several different length scales.

4.2 ADDITIONAL CONCENTRATION TESTS

4.2.1 Change of Array Angle

Additional concentration tests were performed to investigate the dispersion of heavy gas plume according to the change of array angle. Since the wind direction was not constant during the period of field measurement the most representative angle for the field condition had to be chosen before the

simulations. According to the data provided from LLNL the array angle of 225°T was selected for the simulations of Falcon 2, Falcon 3 and Falcon 5. However 225°T was not appropriate for the simulation of Falcon 4. Thus Falcon 4 was simulated using 225°T and 235°T respectively. According to the results of concentration measurements it was shown that there was strong drift in the concentrations downwind direction. But it was difficult to simulate the concentration profiles inside the fence from the field tests since the wind direction from the field tests varied continuously and the response of concentration to a wind direction was sensitive.

4.2.2 Change of the Combinations of Source Gas

First the source gas was released from entirely from the spider. Concentration measurements were taken at fixed locations inside fence. Then 90% of the source gas was released from the spider and 10% was released from the simulating pond. Gradually the gas from the spider decreased by 10% each run and the rest of gas was released from the pond. Concentrations were measured for each run at fixed locations. According to the results at showed that as the percentage from the spider increased the turbulence increased and the peak concentration increased.

However it was realized that different field run had different field condition resulting different concentration profile for each run. Thus the source of the heavy gas was from the evaporating pond and the spider the best combination of the gas supply from the simulating pond (plenum) and the spider had to be selected prior to post-field tests. Referring to the field data inside the fence the best combination to simulate the concentration time series was selected for each run after several trials of different combinations.

In addition gas was released separately from the pond and from the spider, respectively, to investigate the dispersion downwind for each case. According to the results the gas showed wider spread downwind in the case of 100 percent release from the pond. On the other hand higher gas concentrations downwind were shown during 100 percent release from the spider.

4.3 POST-FIELD CONCENTRATION TESTS

Sixteen different sets of post-field tests were simulated. Falcon 2 and Falcon 4 were simulated using models with the length scales of 1:50, 1:100, 1:150 and 1:200. Falcon 3 and Falcon 5 were simulated with models of the length scales of 1:100, 1:150 and 1:200. Argon gas was used as a simulant gas and Freon 12 gas was also used for the simulation of Falcon 4 with the models of the length scales of 1:150 and 1:200.

Appendix A include the reduced concentration data listings for all runs performed. Computer prepared tables list field positions, peak concentrations, and arrival times (i.e. 5 percent, 10 percent, and peak arrival times, and 5 percent and 10 percent departure times). Files are listed in the order of increasing distance in X direction. Runs with models of the length scale of 1:50 display the concentration measurements up to X = 150 m. Runs with the length scale of 1:100 show the concentration up to X = 250 m. All runs with the length scale of 1:150 and 1:200 display the results up to X = 150 m except Falcon 2 simulations which has the measurements up to X = 250 m. In the column labeled SUM is the integral value of concentration over time for the duration of the plume passage. Assuming a constant wind speed at the probe height the SUM value is related to plume dosage, which in turn is related to mass balance. Negative values of SUM should be disregarded. They occur near zero concentration as a result of base line drift in the measurement instrumentation.

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Table 1. Wind- Tunnel Tests Conducted

Test	Length Scale	Source Combination	Array Angle	Locations Tested Argon	Locations Tested Freon 12	Angle Change	Source Change
Falcon 1	50			X(a)			
	100			X(b)			
	150			X(c)			
	200			X(d)			
Falcon 2	50			114			
	100	50% S + 50% P	225°T	161			
	150	100% S	225°T	161			
	200	100% S	225°T	90			
Falcon 3	50			X(e)			
	100	70% S + 30% P	225°T	161			
	150	50% S + 50% P	225°T	105			
	200	70% S + 30% P	225°T	77			
Falcon 4	50	90% S + 10% P	235°T	114			
	100	70% S + 30% P	235°T	161			
	150	70% S + 30% P	235°T	116	132	225°,232°	100%S,100%P
	200	70% S + 30% P	235°T	88	90		
Falcon 5	50			X			
	100	70% S + 30% P	225°T	161			
	150	50% S + 50% P	225°T	90			
	200	50% S + 50% P	225°T	77			

Locations Tested: Measurement locations (Repetitions - 5 times each)
S: Spider
P: Plenum
X: No experiment
(a) - (d): Wind velocity was too low to simulate in EWT.
(e): Gas flow rate was too large to supply through model source tube.

Table 2. Comparison of Parameters of Prototype and Model

Trial Name	Scale Ratio	(S.G.)p	(S.G.)m	(Vol)p m**3	(Vol)m cm**3	(Rate)p m**3/min	(Rate)m cm**3/s	(U2)p m/s	(U2)m cm/s	(Re)p	(Re)m
Falcon1	50	1.5	1.38	66.4	134393.6	28.7	5968.056	1.6	19.73	773059.7	1906.18
Falcon2	50	1.5	1.38	20.6	41694.4	15.9	3306.345	4.7	57.95	986187.7	2431.71
Falcon3	50	1.5	1.38	50.7	102616.8	18.9	3930.183	4	49.32	991911.7	2445.82
Falcon4	50	1.5	1.38	44.9	90877.6	8.7	1809.132	5.1	62.88	759900.7	1873.74
Falcon5	50	1.5	1.38	43.9	88853.6	30.3	6300.770	2.7	33.29	1031847.	2544.29
Falcon1	100	1.5	1.38	66.4	16799.2	28.7	1055.013	1.6	13.95	773059.7	673.94
Falcon2	100	1.5	1.38	20.6	5211.8	15.9	584.4847	4.7	40.97	986187.7	859.74
Falcon3	100	1.5	1.38	50.7	12827.1	18.9	694.7649	4	34.87	991911.7	864.73
Falcon4	100	1.5	1.38	44.9	11359.7	8.7	319.8124	5.1	44.46	759900.7	662.47
Falcon5	100	1.5	1.38	43.9	11106.7	30.3	1113.829	2.7	23.54	1031847.	899.54
Falcon1	150	1.5	1.38	66.4	4977.540	28.7	382.8510	1.6	11.39	773059.7	366.85
Falcon2	150	1.5	1.38	20.6	1544.237	15.9	212.1021	4.7	33.45	986187.7	467.98
Falcon3	150	1.5	1.38	50.7	3800.622	18.9	252.1214	4	28.47	991911.7	470.70
Falcon4	150	1.5	1.38	44.9	3365.837	8.7	116.0558	5.1	36.30	759900.7	360.60
Falcon5	150	1.5	1.38	43.9	3290.874	30.3	404.1946	2.7	19.22	1031847.	489.65
Falcon1	200	1.5	1.38	66.4	2099.9	28.7	186.5017	1.6	9.86	773059.7	238.27
Falcon2	200	1.5	1.38	20.6	651.475	15.9	103.3232	4.7	28.97	986187.7	303.96
Falcon3	200	1.5	1.38	50.7	1603.387	18.9	122.8182	4	24.66	991911.7	305.73
Falcon4	200	1.5	1.38	44.9	1419.962	8.7	56.53538	5.1	31.44	759900.7	234.22
Falcon5	200	1.5	1.38	43.9	1388.337	30.3	196.8990	2.7	16.64	1031847.	318.04
Falcon4	150	1.5	4.2	44.9	3365.837	8.7	336.7831	5.1	105.35	759900.7	1046.43
Falcon4	200	1.5	4.2	44.9	1419.962	8.7	164.0603	5.1	91.23	759900.7	679.68

Trial Name	Scale Ratio	(S.G.)p	(S.G.)m	(U*)p m/s	(U*)m m/s	(Ri)B	(Ri*)m	(Pe/Ri)m	(Pe*/Re*)m
Falcon1	50	1.5	1.38	0.0471	0.013216	0.1451	3708.276	6.893574	0.0021
Falcon2	50	1.5	1.38	0.3327	0.038823	-0.0229	186.6315	174.7342	0.0526
Falcon3	50	1.5	1.38	0.2811	0.033041	-0.0057	304.5173	107.7121	0.0324
Falcon4	50	1.5	1.38	0.3322	0.042127	0.0291	112.5551	223.2518	0.0671
Falcon5	50	1.5	1.38	0.1337	0.022302	0.0937	1030.013	33.12651	0.0100
Falcon1	100	1.5	1.38	0.0471	0.009345	0.1451	3708.276	2.437246	0.0007
Falcon2	100	1.5	1.38	0.3327	0.027452	-0.0229	186.6315	61.77789	0.0186
Falcon3	100	1.5	1.38	0.2811	0.023363	-0.0057	304.5173	38.08197	0.0115
Falcon4	100	1.5	1.38	0.3322	0.029788	0.0291	112.5551	78.93144	0.0237
Falcon5	100	1.5	1.38	0.1337	0.015770	0.0937	1030.013	11.71199	0.0035
Falcon1	150	1.5	1.38	0.0471	0.007630	0.1451	3708.276	1.326669	0.0004
Falcon2	150	1.5	1.38	0.3327	0.022414	-0.0229	186.6315	33.62762	0.0101
Falcon3	150	1.5	1.38	0.2811	0.019076	-0.0057	304.5173	20.72920	0.0062
Falcon4	150	1.5	1.38	0.3322	0.024322	0.0291	112.5551	42.96483	0.0129
Falcon5	150	1.5	1.38	0.1337	0.012876	0.0937	1030.013	6.375201	0.0019
Falcon1	200	1.5	1.38	0.0471	0.006608	0.1451	3708.276	0.861696	0.0003
Falcon2	200	1.5	1.38	0.3327	0.019411	-0.0229	186.6315	21.84178	0.0066
Falcon3	200	1.5	1.38	0.2811	0.016520	-0.0057	304.5173	13.46401	0.0040
Falcon4	200	1.5	1.38	0.3322	0.021063	0.0291	112.5551	27.90648	0.0084
Falcon5	200	1.5	1.38	0.1337	0.011151	0.0937	1030.013	4.140814	0.0012
Falcon4	150	1.5	4.2	0.3322	0.070581	0.0291	112.5551	124.6798	0.0375
Falcon4	200	1.5	4.2	0.3322	0.061125	0.0291	112.5551	80.98195	0.0244

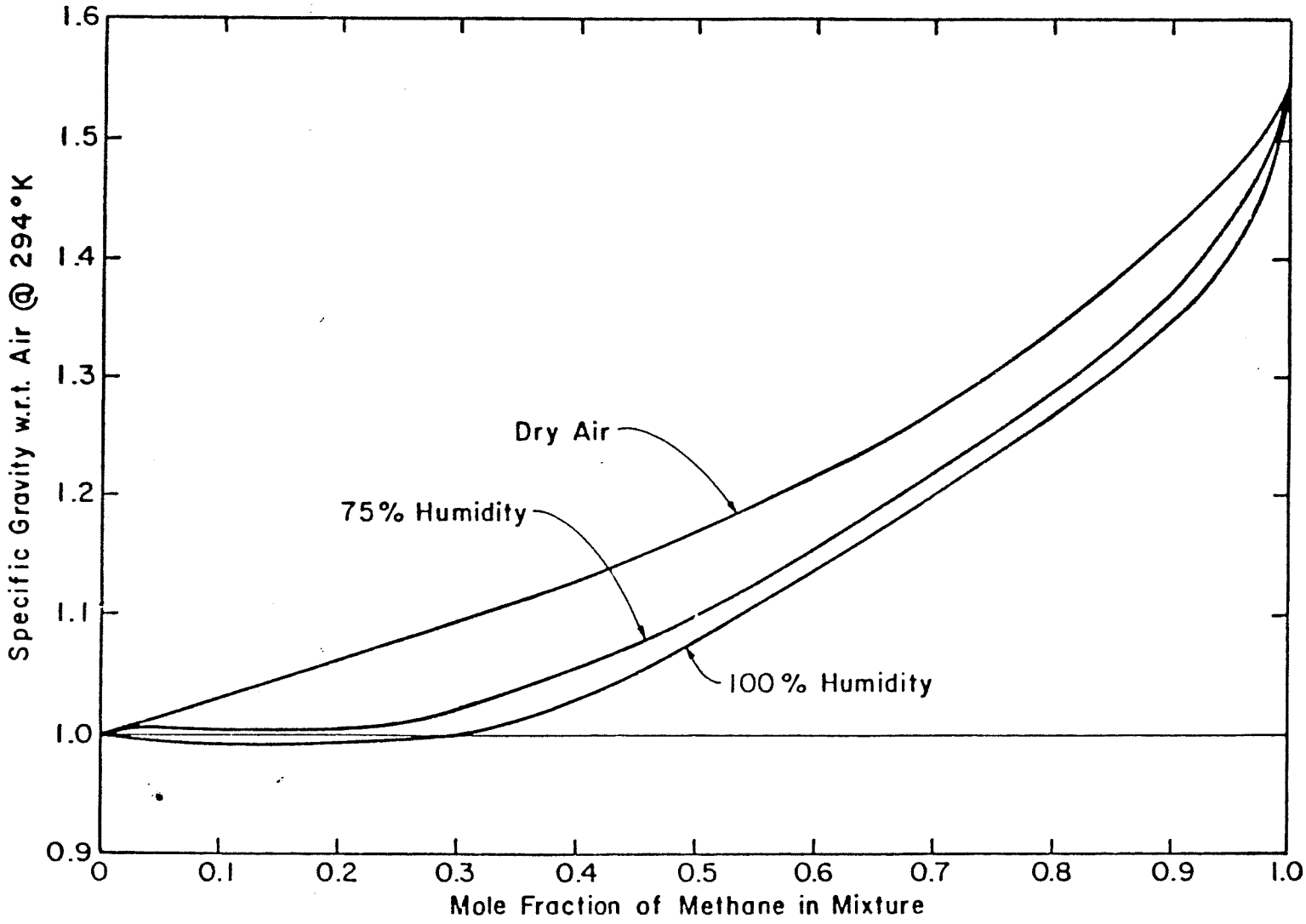


Figure 1. Specific Gravity of LNG Vapor - Humid Atmospheric Mixtures

Figure 2

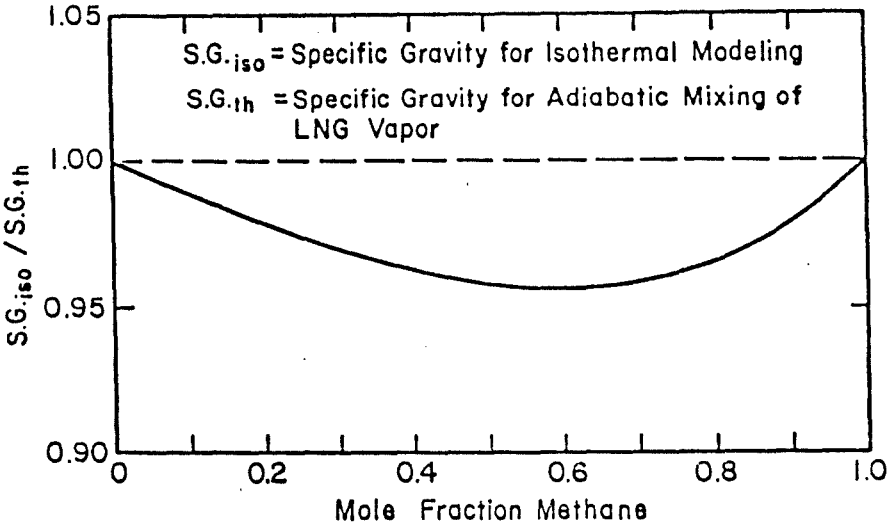
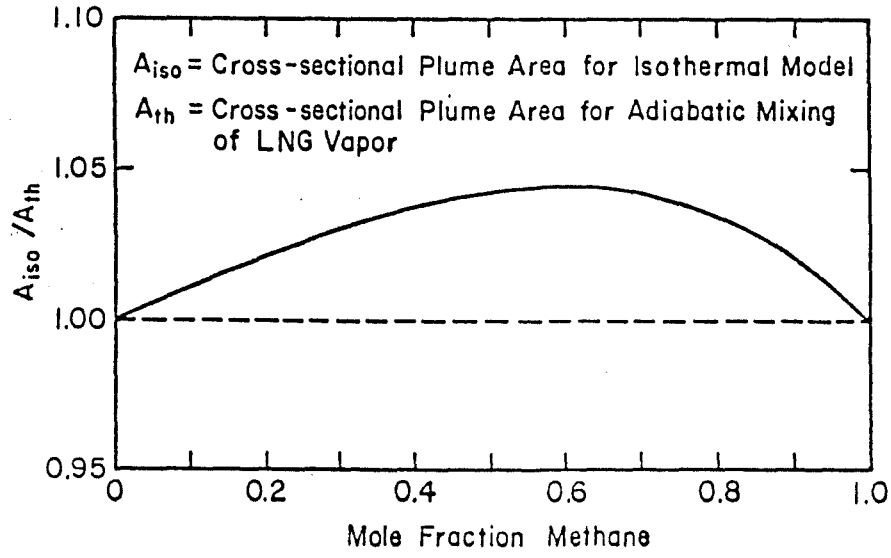


Figure 3



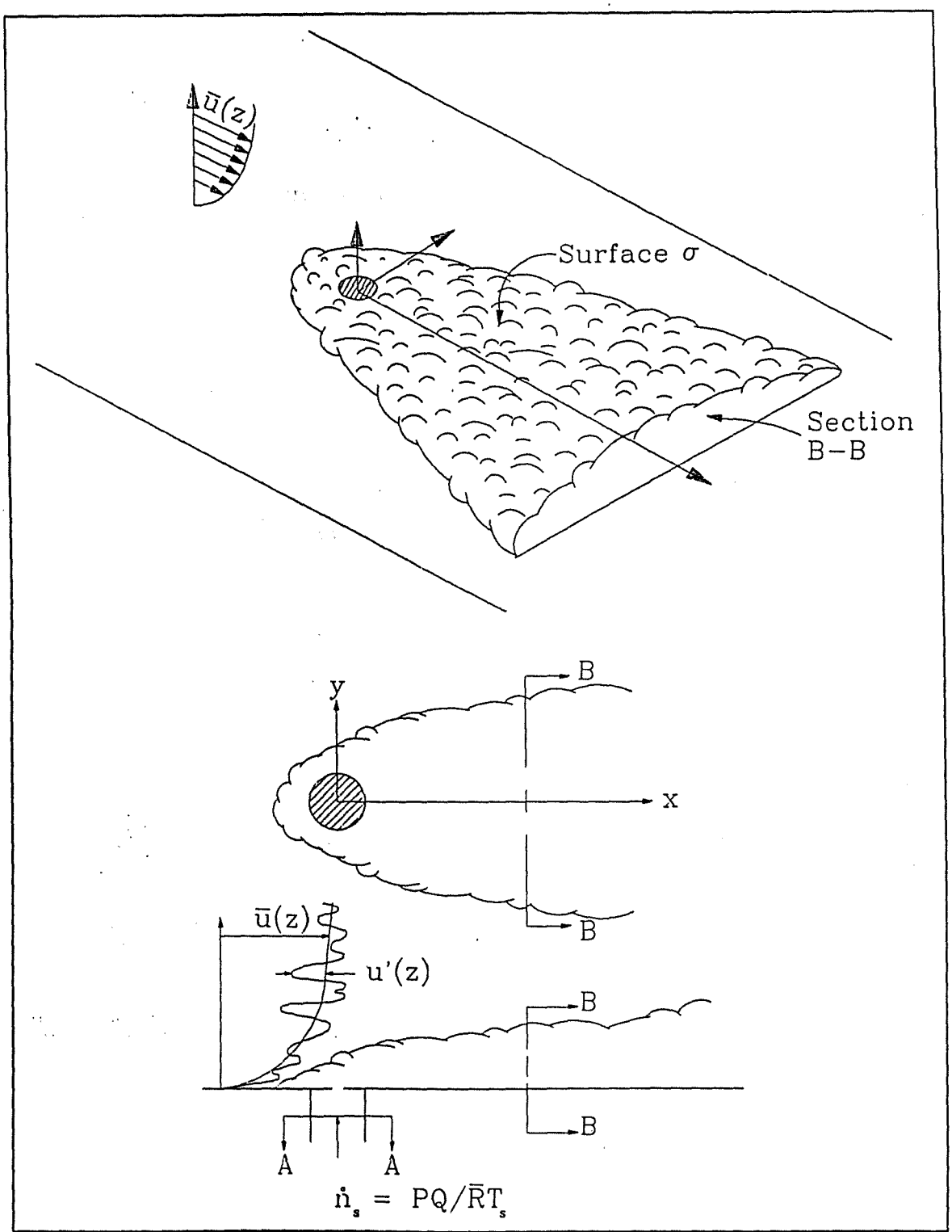


Figure ~~12~~ 4 Notation Definition Diagram for Concentration Scaling Theory Derivation

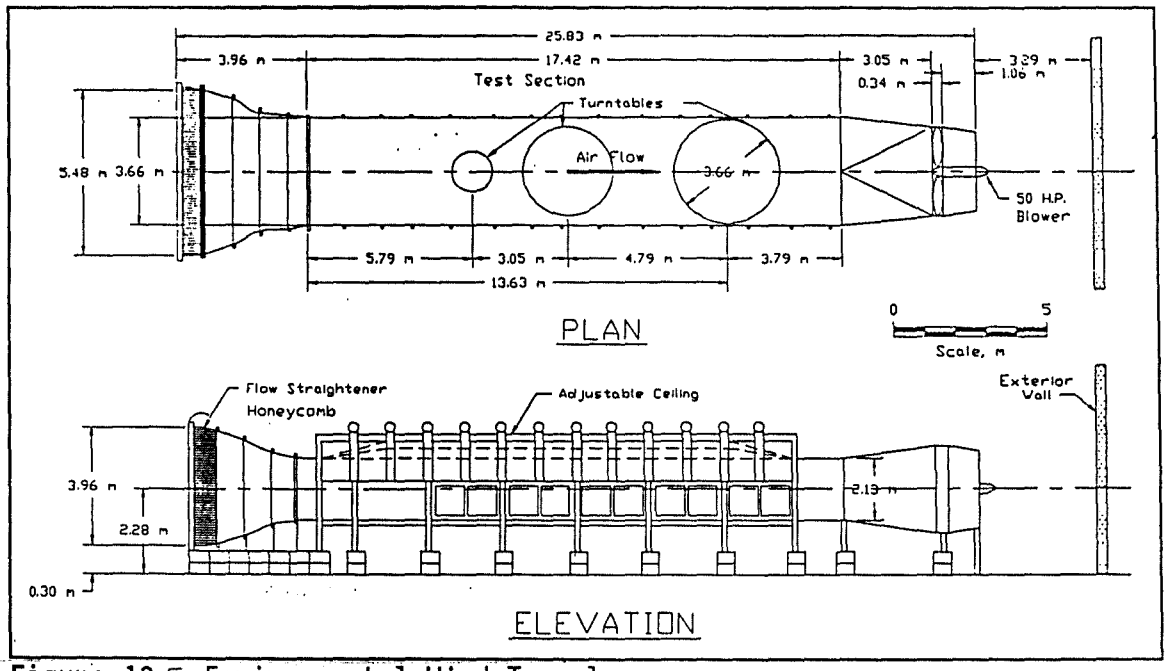


Figure ~~13~~ 5 Environmental Wind Tunnel

Figure 6

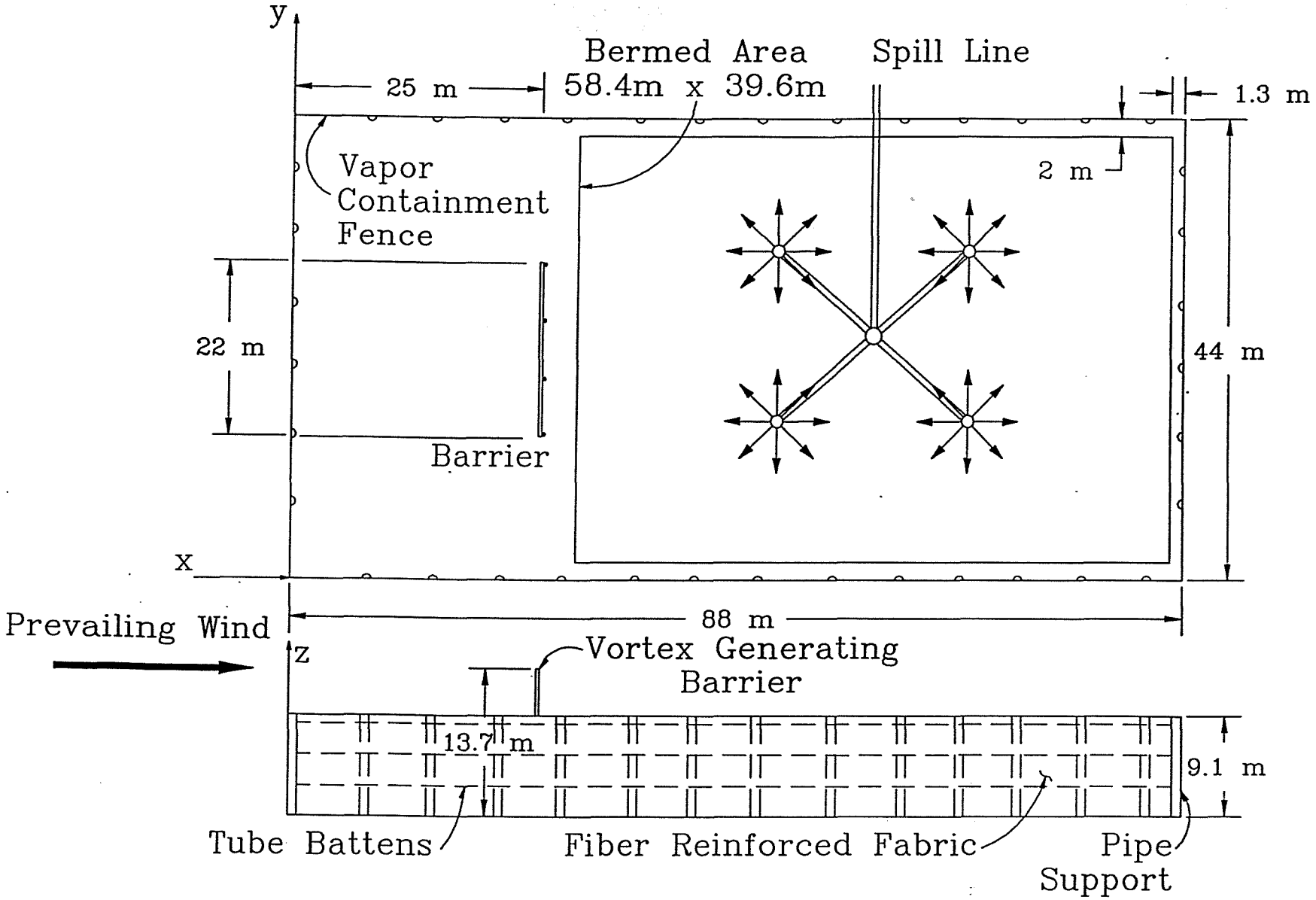
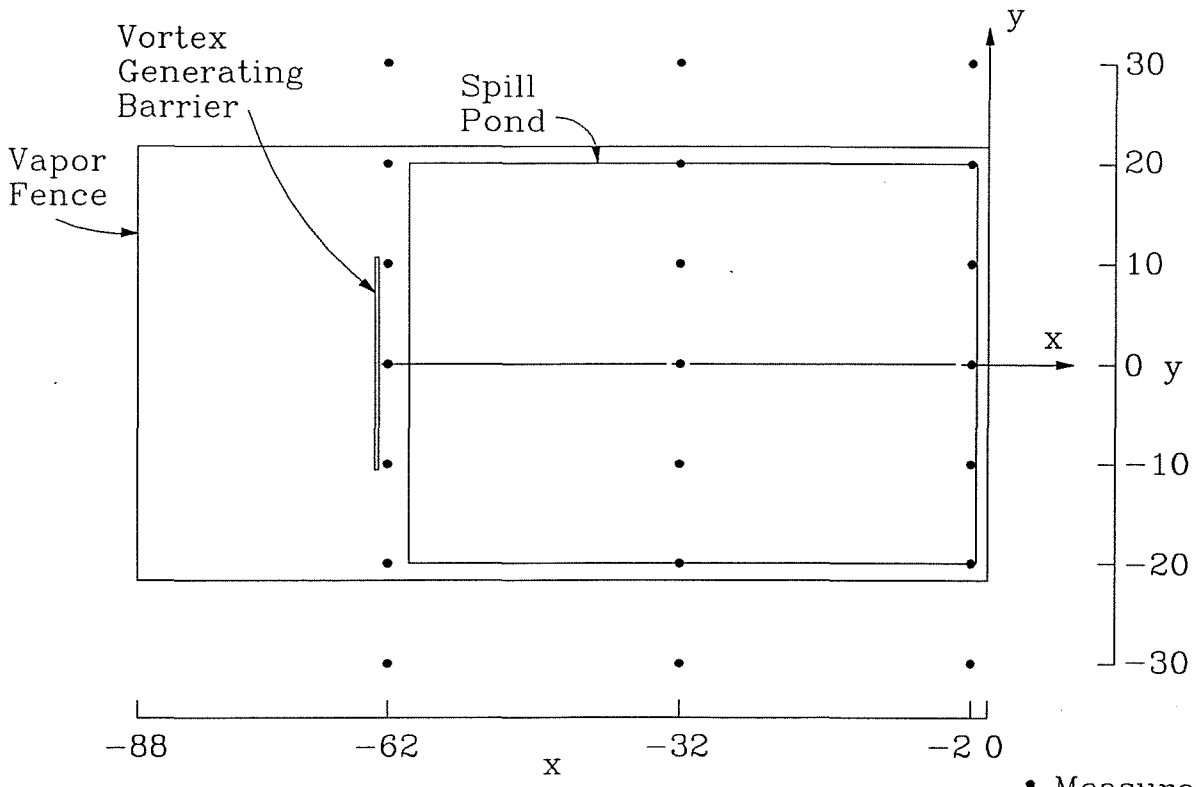

y
Bermed Area
58.4m x 39.6m
Spill Line
25 m
1.3 m
Vapor
Containment
Fence
2 m
22 m
44 m
Barrier
x
Prevailing Wind
88 m
z
Vortex Generating
Barrier
13.7 m
9.1 m
Tube Battens
Fiber Reinforced Fabric
Pipe
Support

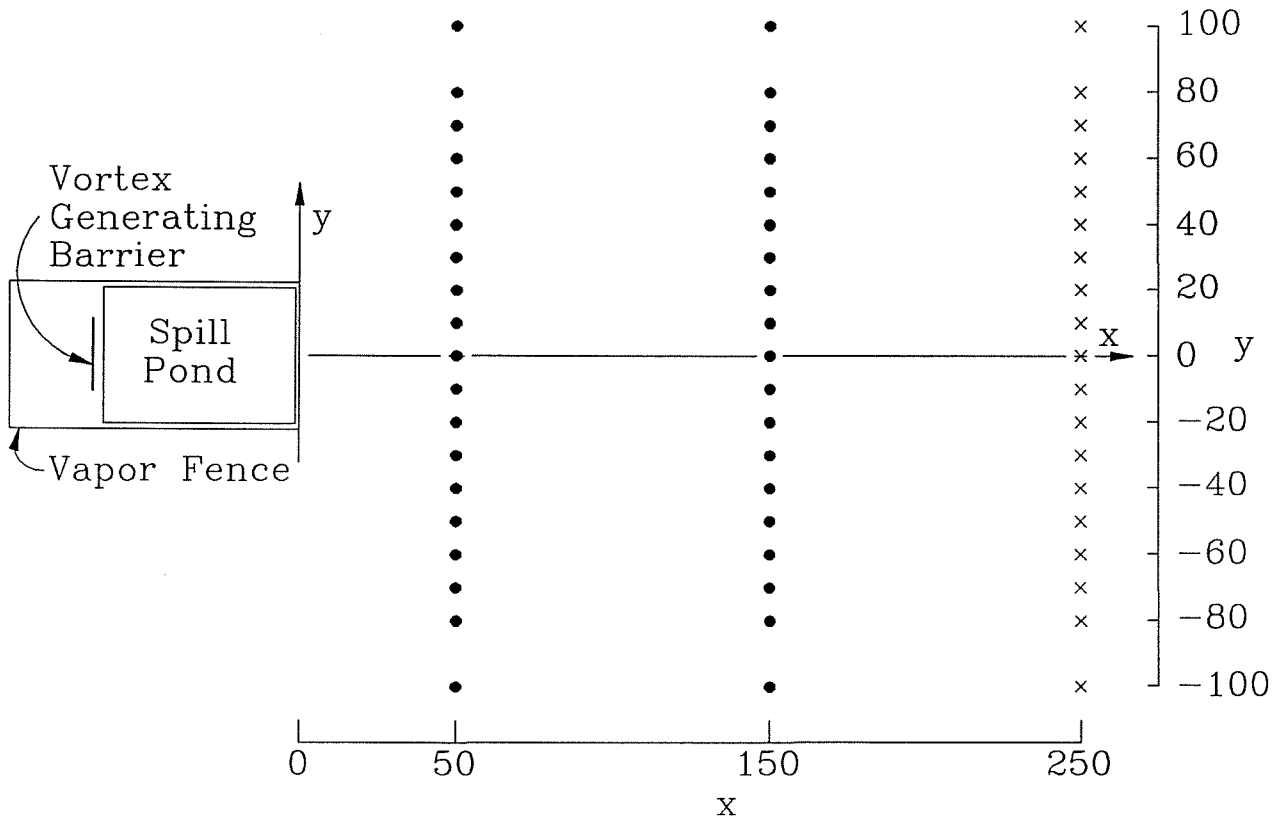
Figure 7



All Dimensions in meters

• Measurement separation distance varied for appropriate condition

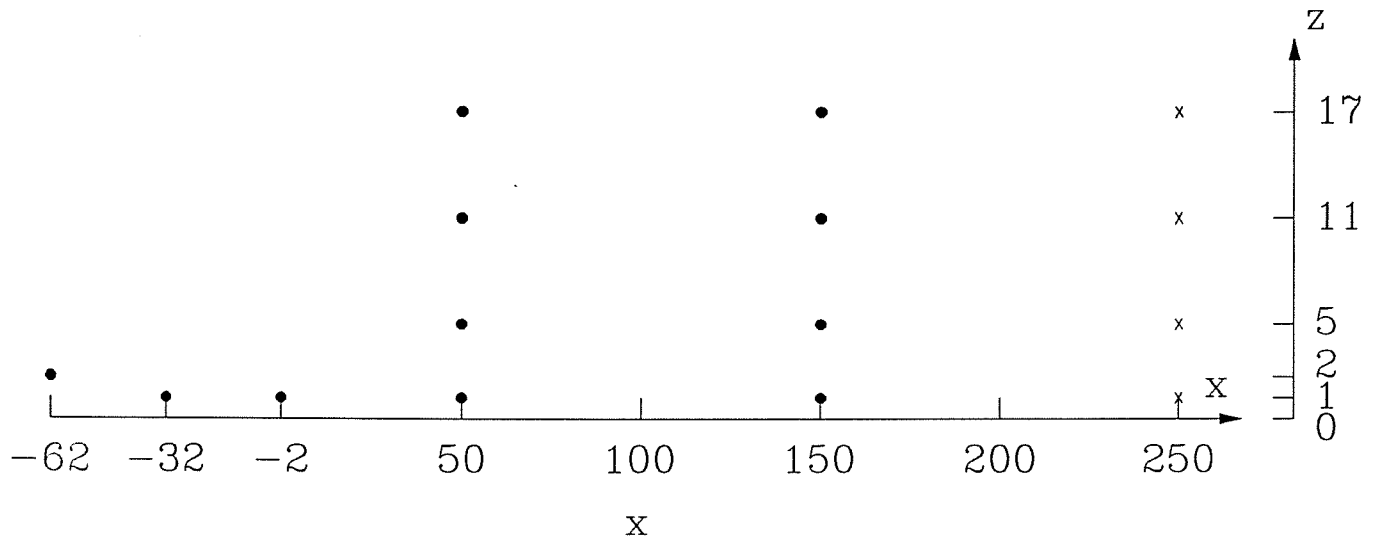
Figure 8



All Dimensions in meters

- • Measurement separation distance varied for appropriate condition
- × Measurements were performed only for certain cases

Figure 9



All Dimensions in meters

• Measurement points for all cases

x Measurements were performed only for certain cases

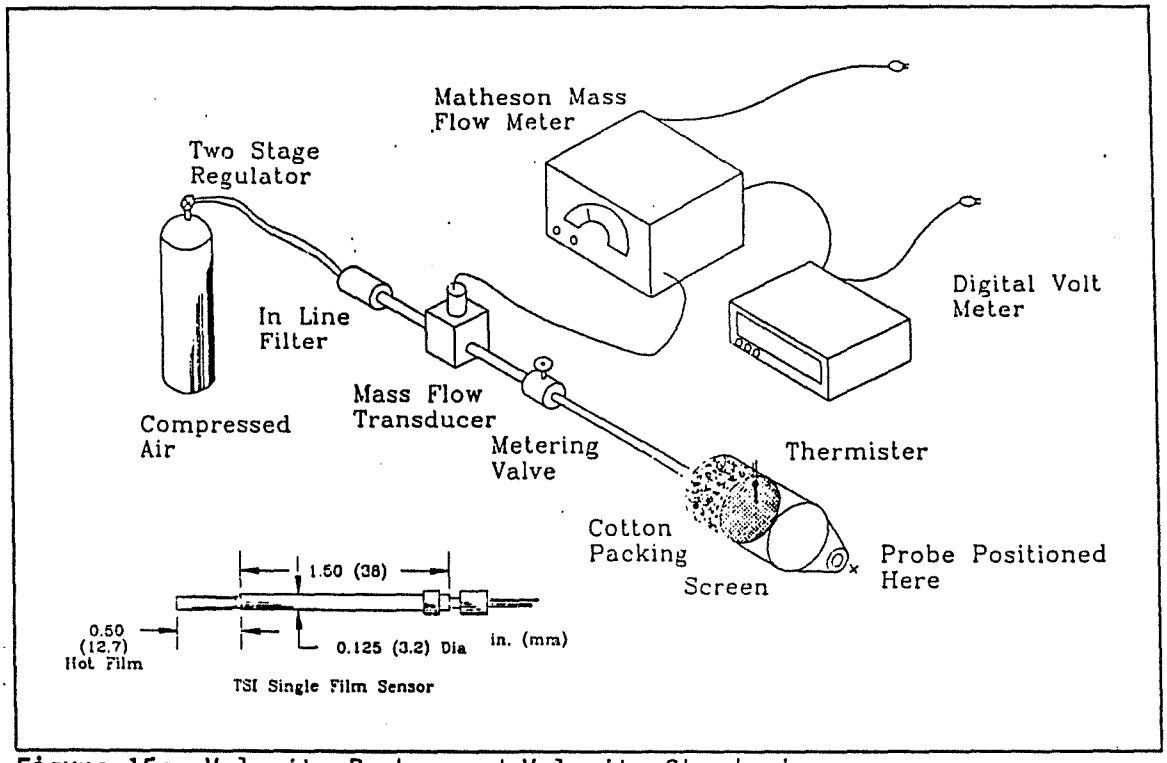


Figure ~~15~~ 10 Velocity Probes and Velocity Standard

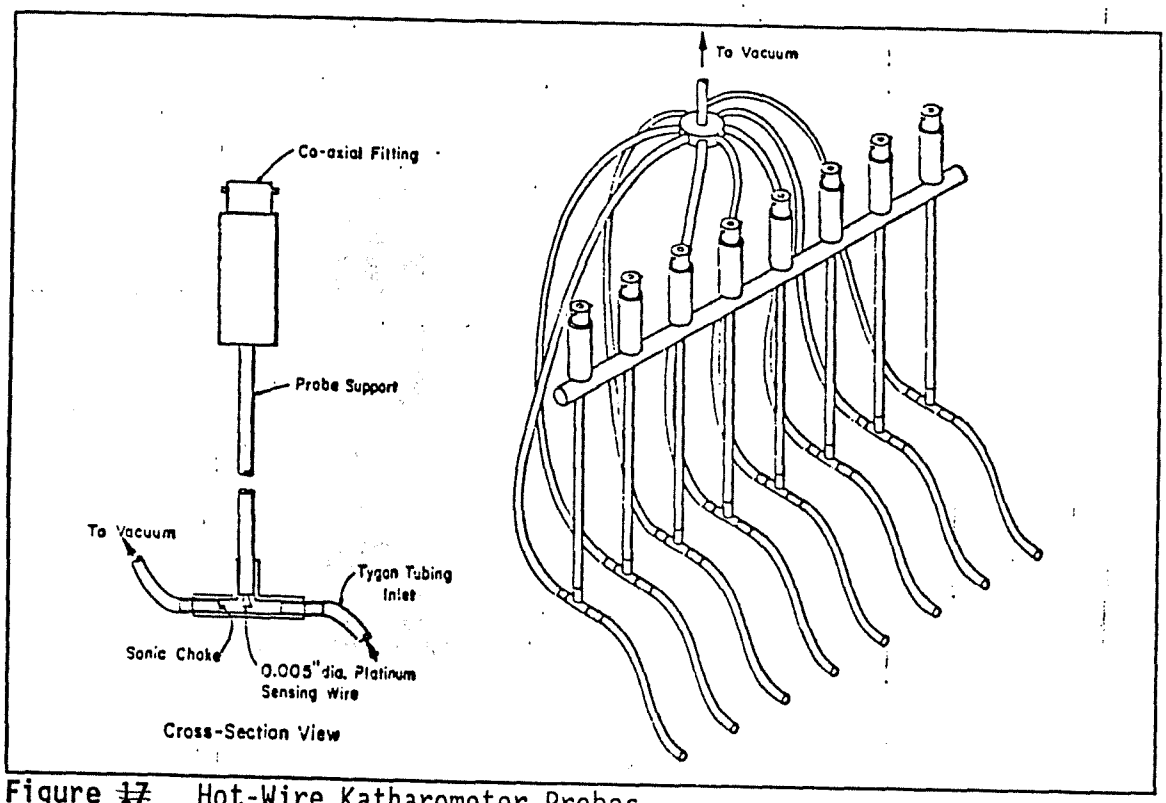


Figure ~~17~~ 11 Hot-Wire Katharometer Probes

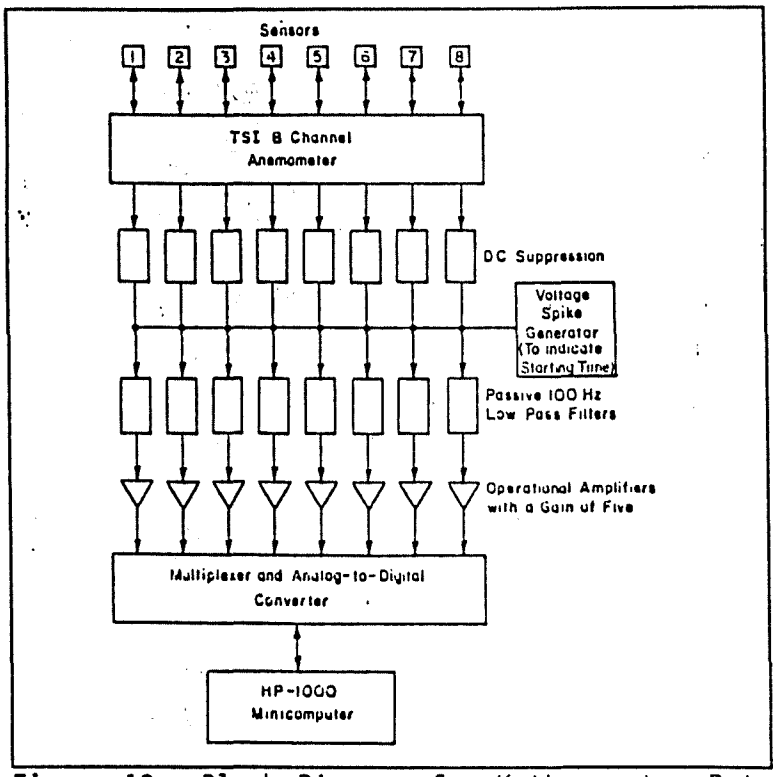
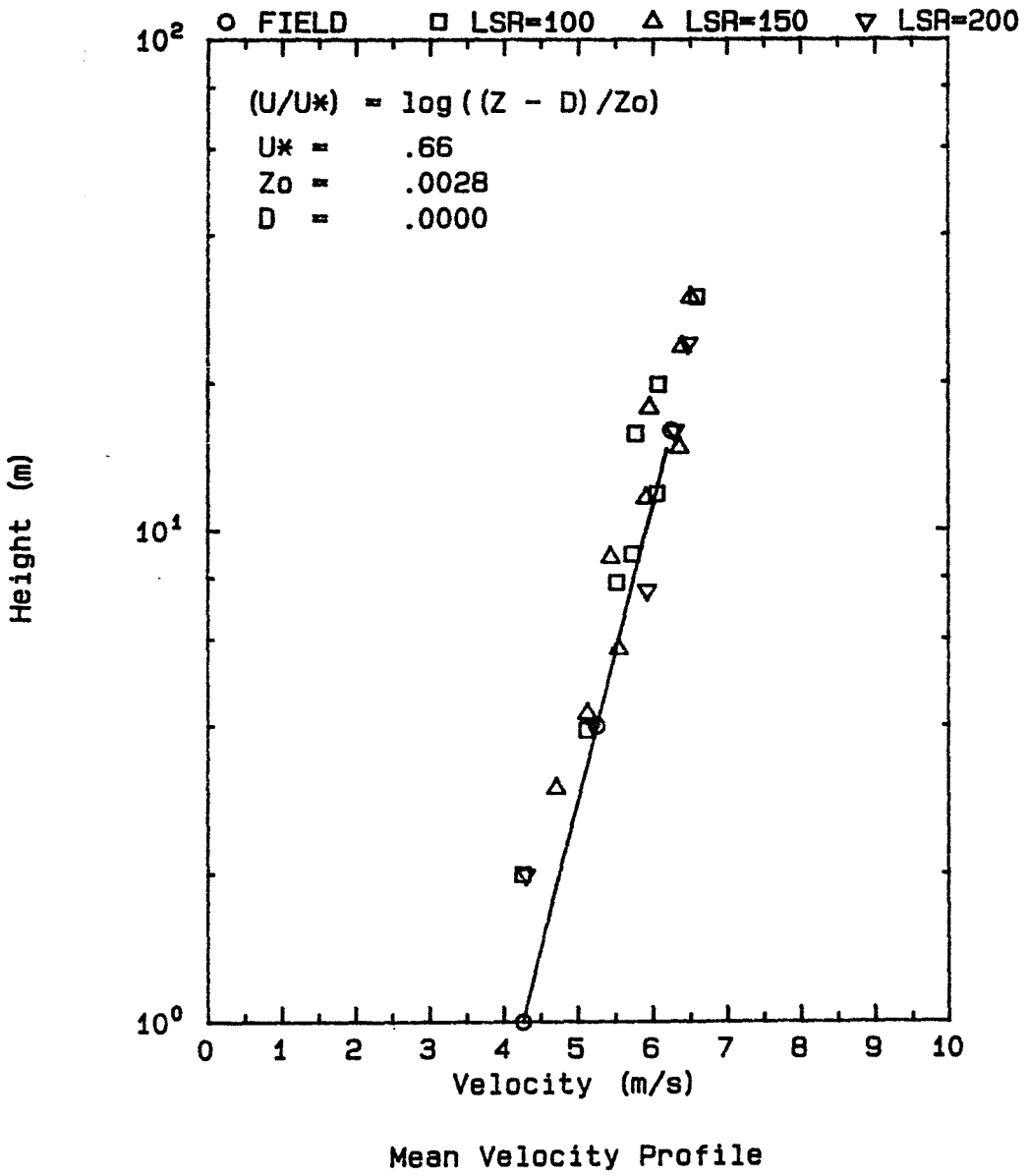


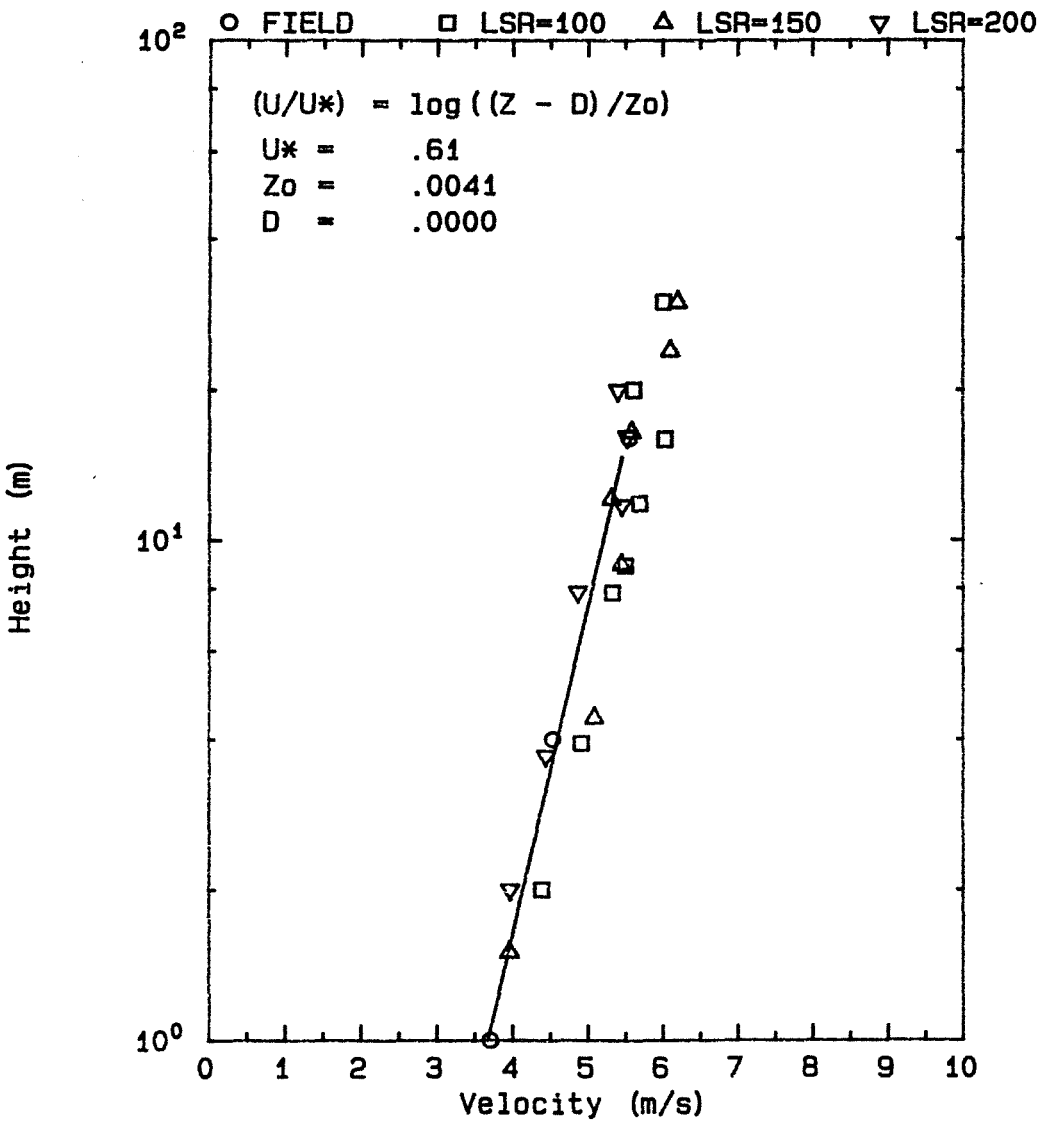
Figure ~~18~~ 12 Block Diagram for Katharometer Data Reduction

Figure 13 (Falcon 2)



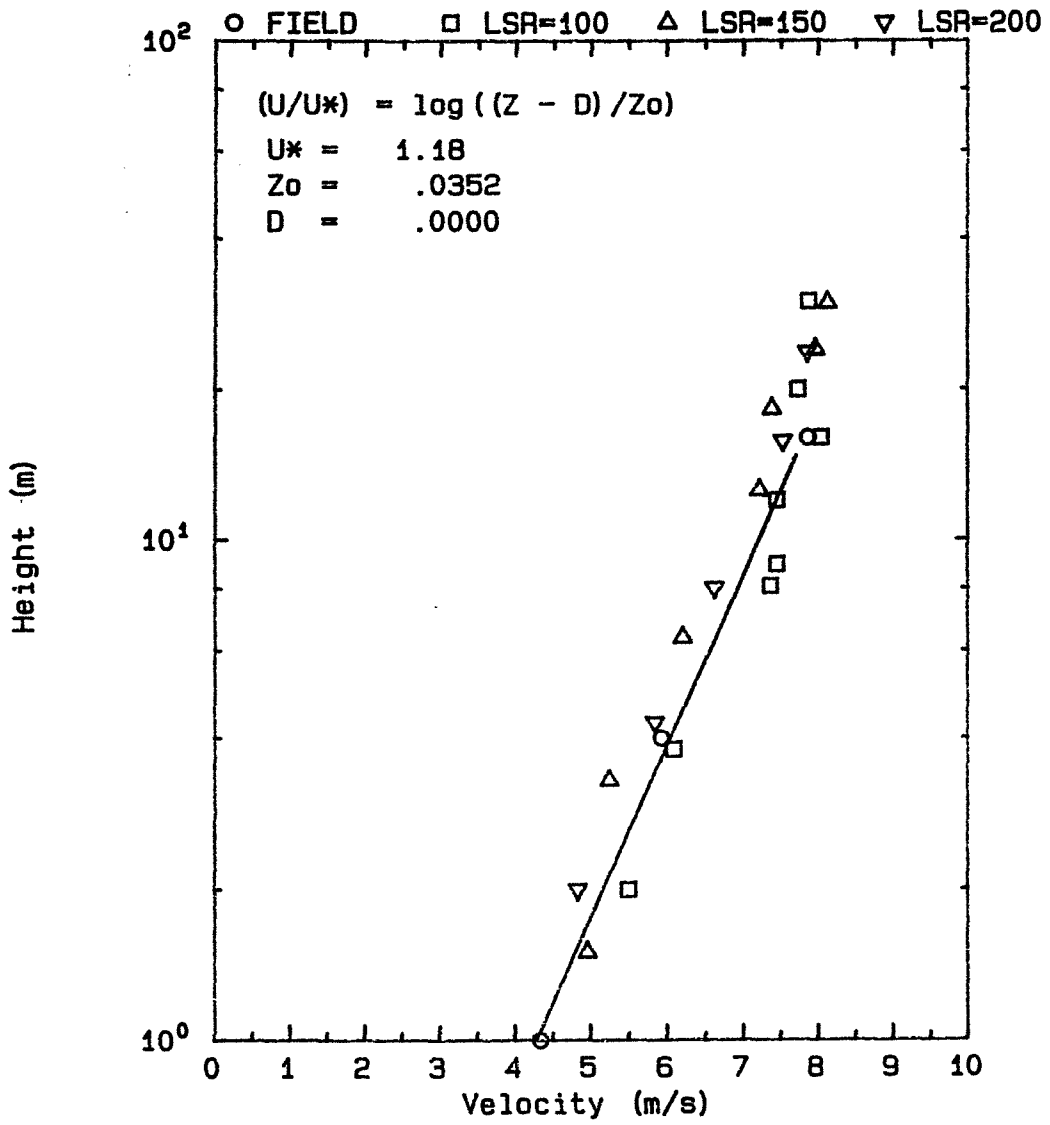
Mean Velocity Profile

Figure 14 (Falcon 3)



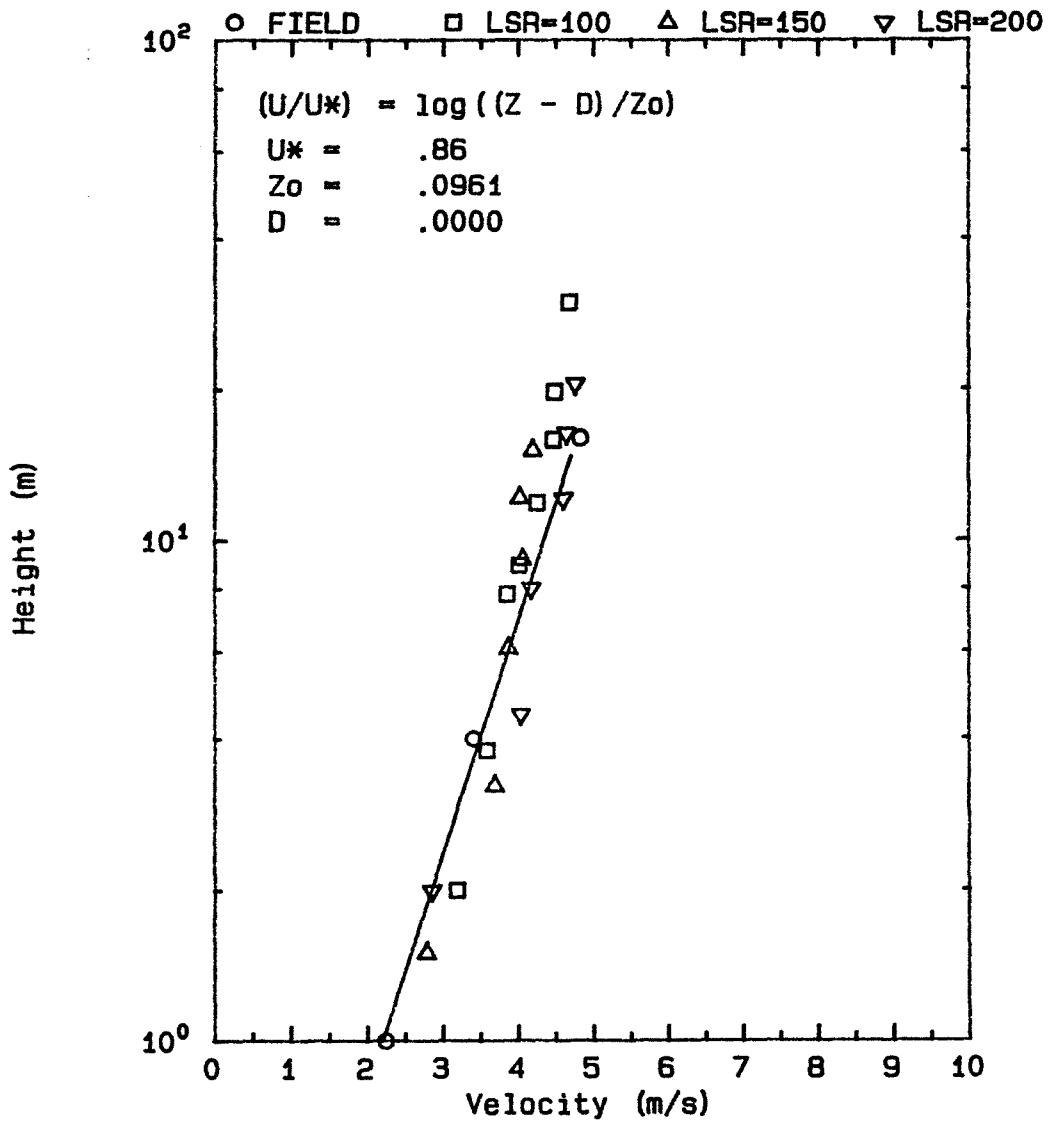
Mean Velocity Profile

Figure 15 (Falcon 4)



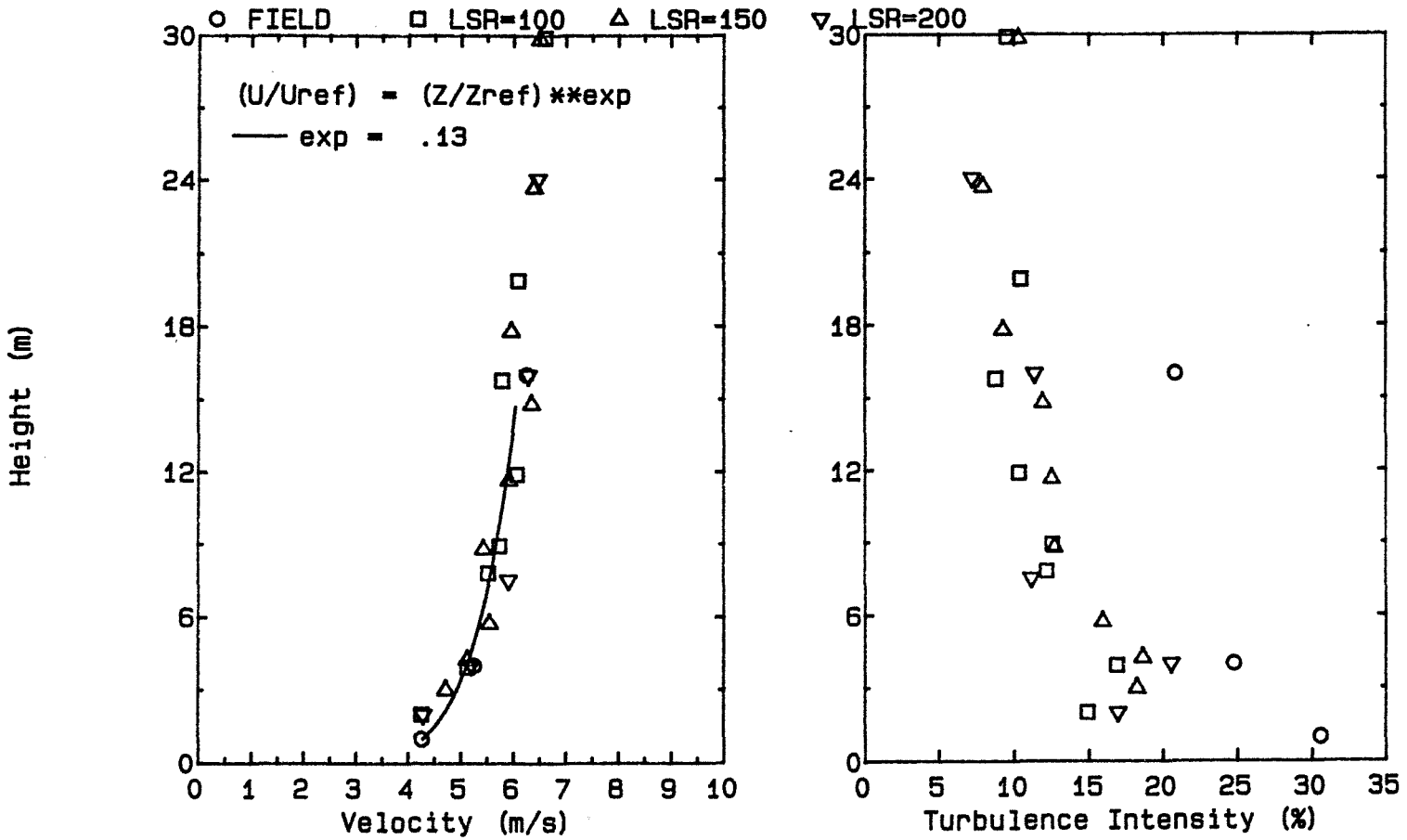
Mean Velocity Profile

Figure 16 (Falcon 5)



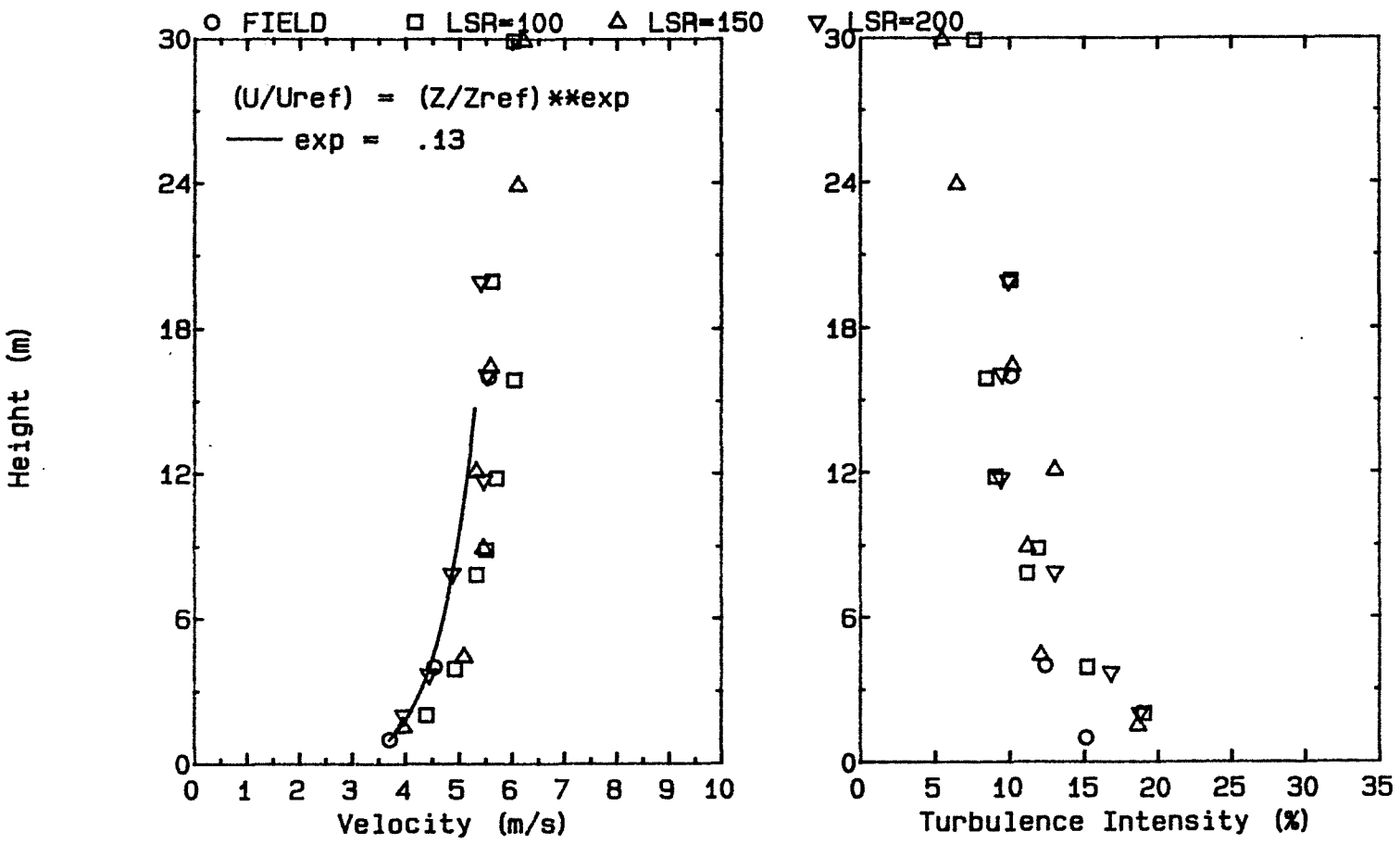
Mean Velocity Profile

Figure 19 (Falcon 2)



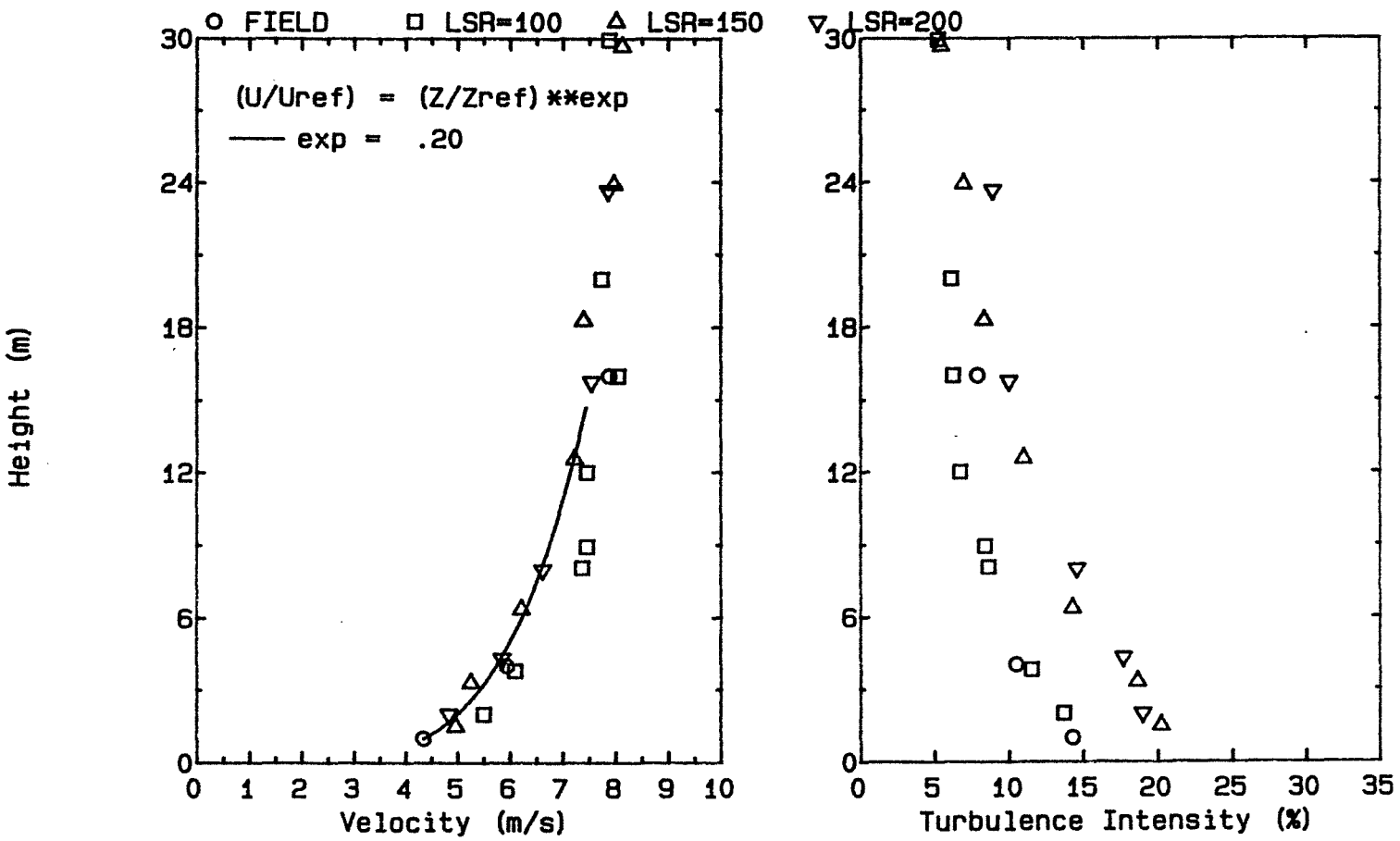
Mean Velocity and Local Turbulence Intensity Profile

Figure 18 (Falcon 3)



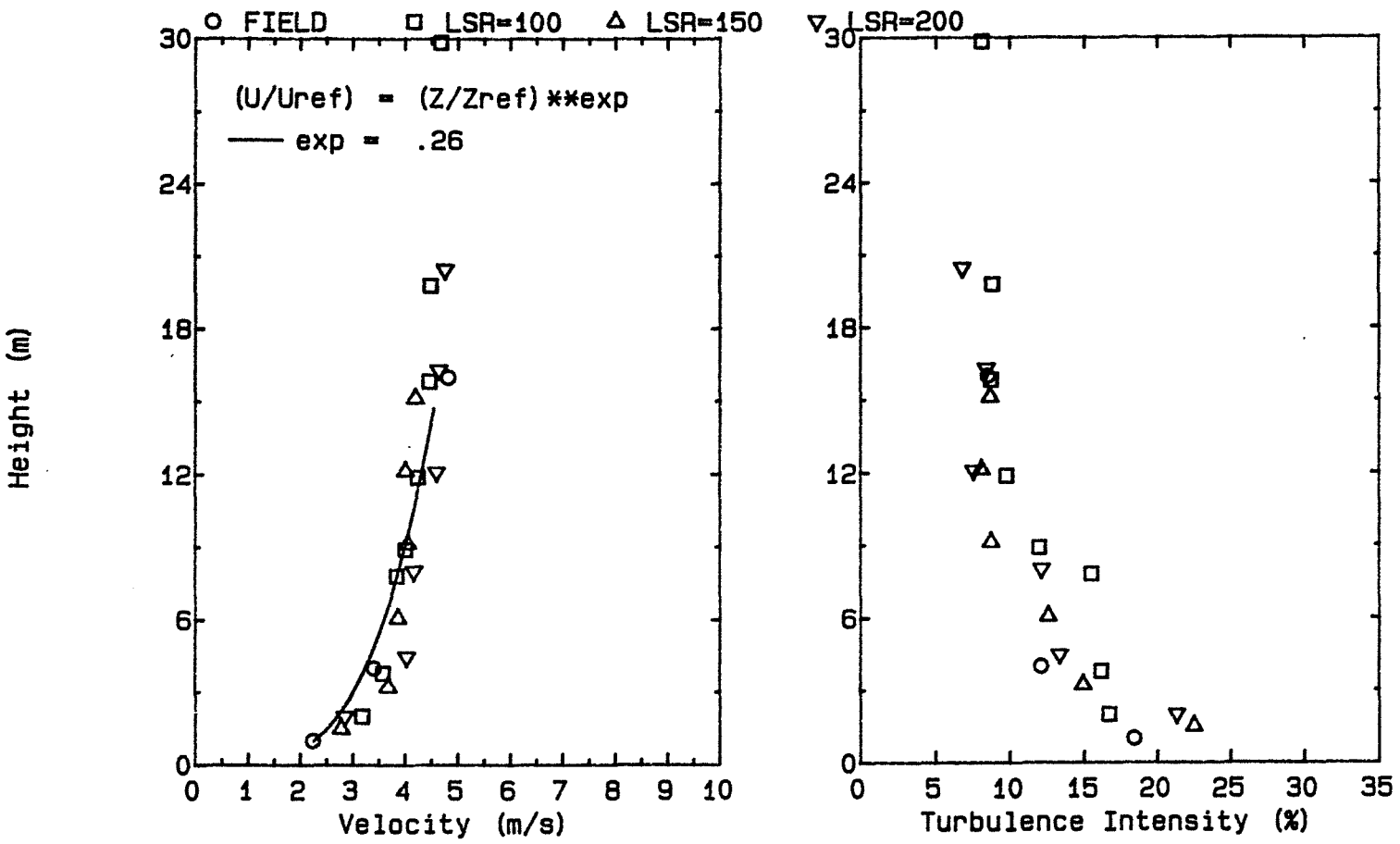
Mean Velocity and Local Turbulence Intensity Profile

Figure 19 (Falcon 4)



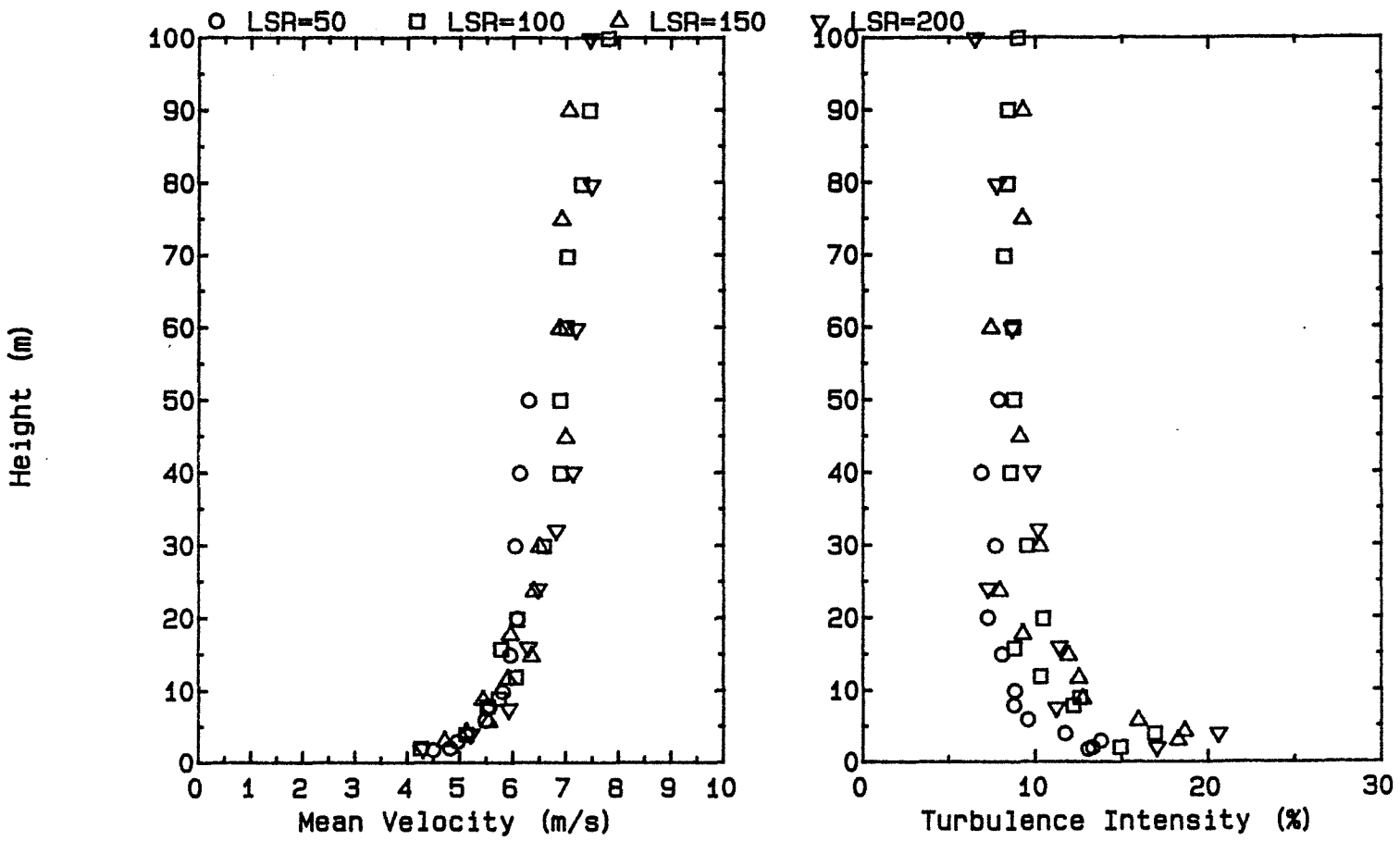
Mean Velocity and Local Turbulence Intensity Profile

Figure 20 (Falcon 5)



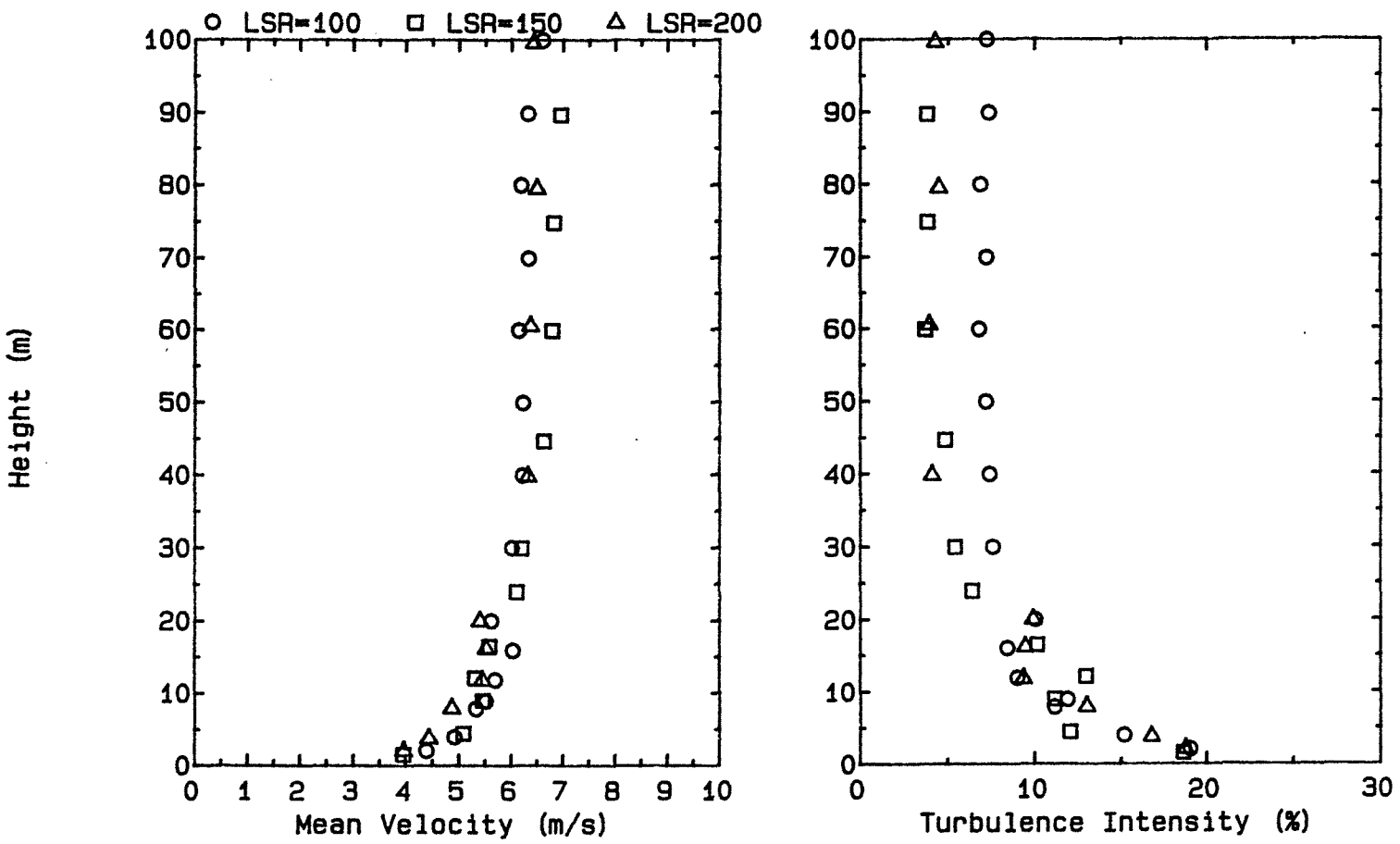
Mean Velocity and Local Turbulence Intensity Profile

Figure 21 (Falcon 2)



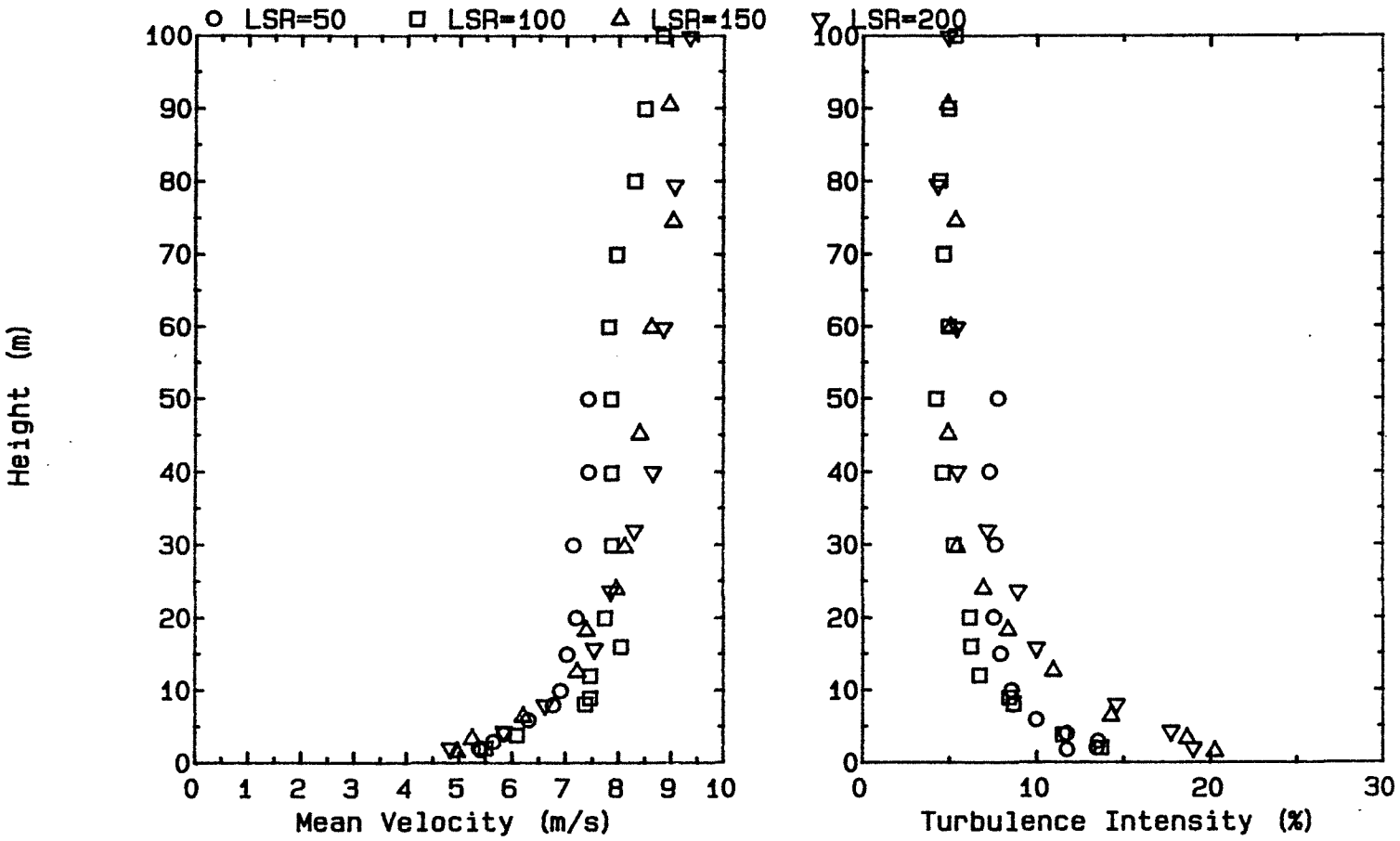
Mean Velocity and Local Turbulence Intensity Profile

Figure 22 (Falcon 3)



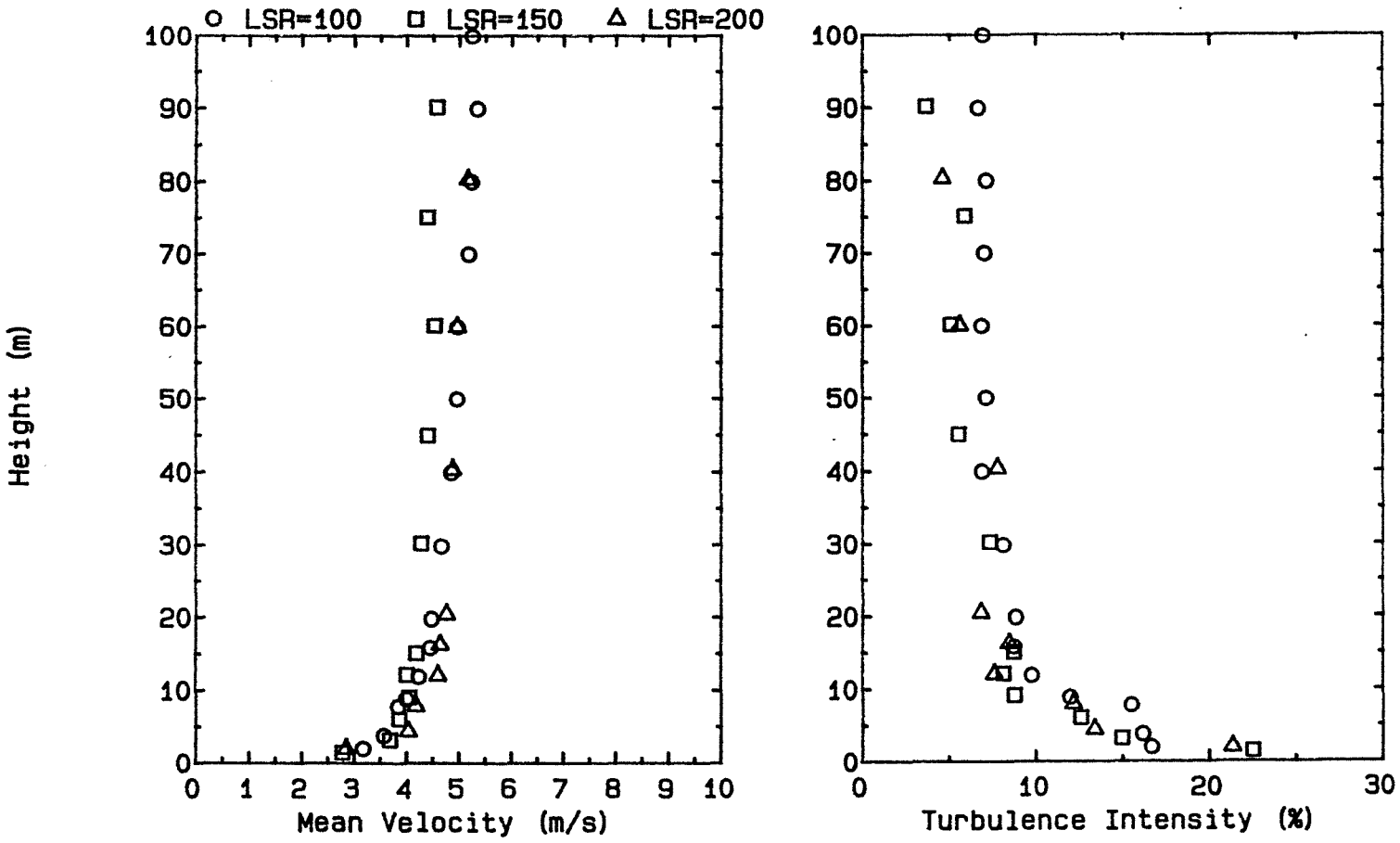
Mean Velocity and Local Turbulence Intensity Profile

Falcon 23 (Falcon 4)



Mean Velocity and Local Turbulence Intensity Profile

Figure 24 (Falcon 5)



Mean Velocity and Local Turbulence Intensity Profile

APPENDIX A

Reduced Concentration Data Listings

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210A1.004	.1	.0	.0	.0	-.02	-62.0	40.0	2.0	.2	0.	0.	0.	0.	0.	.03
N210A1.005	1.1	14.9	14.9	14.9	.05	-62.0	30.0	2.0	2.9	0.	0.	130.	0.	0.	1.25
N210A1.006	15.9	2.2	11.9	53.4	1.99	-62.0	20.0	2.0	33.9	19.	23.	103.	250.	355.	41.45
N210A1.007	19.3	2.8	10.4	73.3	3.03	-62.0	10.0	2.0	39.2	24.	24.	90.	328.	479.	63.00
N210A1.008	18.4	2.1	9.5	74.2	2.95	-62.0	.0	2.0	37.9	18.	31.	83.	416.	597.	62.26
N210A1.009	16.7	2.3	11.3	82.4	2.78	-62.0	-10.0	2.0	35.1	20.	21.	98.	278.	600.	59.03
N210A1.010	17.7	2.5	9.7	58.9	1.78	-62.0	-20.0	2.0	36.7	22.	49.	85.	210.	275.	37.17
N210A2.004	.2	.0	.0	.0	.02	-62.0	40.0	2.0	.5	0.	0.	0.	0.	0.	.41
N210A2.005	1.0	.0	9.4	.0	.07	-62.0	30.0	2.0	2.6	0.	0.	82.	0.	0.	1.64
N210A2.006	16.8	2.4	10.9	52.0	2.22	-62.0	20.0	2.0	35.3	35.	36.	95.	226.	380.	46.23
N210A2.007	17.1	1.9	8.9	83.1	3.12	-62.0	10.0	2.0	35.8	17.	31.	78.	432.	684.	65.27
N210A2.008	18.9	1.3	8.3	89.0	3.03	-62.0	.0	2.0	38.7	17.	30.	72.	313.	550.	63.66
N210A2.009	15.5	1.6	11.8	78.2	2.71	-62.0	-10.0	2.0	33.2	15.	25.	102.	317.	526.	57.77
N210A2.010	15.8	4.5	8.3	44.7	1.88	-62.0	-20.0	2.0	33.7	41.	42.	72.	274.	360.	39.24
N210A3.004	.5	.0	14.9	.0	.00	-62.0	40.0	2.0	1.3	0.	0.	130.	0.	0.	.24
N210A3.005	1.1	14.5	16.1	16.2	.02	-62.0	30.0	2.0	2.9	0.	0.	141.	0.	0.	.80
N210A3.006	14.3	3.0	9.6	44.3	2.05	-62.0	20.0	2.0	31.2	26.	33.	84.	206.	355.	42.44
N210A3.007	16.4	2.3	8.4	78.3	3.11	-62.0	10.0	2.0	34.6	20.	21.	73.	355.	636.	65.30
N210A3.008	20.1	2.4	10.2	90.2	2.89	-62.0	.0	2.0	40.4	22.	26.	89.	346.	540.	60.53
N210A3.009	16.3	2.3	13.9	83.6	2.99	-62.0	-10.0	2.0	34.5	23.	25.	121.	342.	594.	62.58
N210A3.010	18.3	3.4	11.3	53.1	1.80	-62.0	-20.0	2.0	37.8	33.	41.	99.	207.	243.	37.31
N210A4.004	.3	.0	28.7	.0	.02	-62.0	40.0	2.0	.7	0.	0.	250.	0.	0.	.45
N210A4.005	1.3	14.3	14.4	17.4	.05	-62.0	30.0	2.0	3.5	0.	0.	125.	0.	0.	1.32
N210A4.006	16.4	3.9	12.2	49.1	2.22	-62.0	20.0	2.0	34.6	34.	41.	106.	284.	300.	46.29
N210A4.007	19.5	2.4	8.7	89.0	3.52	-62.0	10.0	2.0	39.6	21.	26.	76.	402.	598.	73.17
N210A4.008	20.9	1.9	9.5	83.8	3.33	-62.0	.0	2.0	41.7	17.	23.	83.	383.	537.	69.48
N210A4.009	16.8	1.9	8.0	87.3	2.93	-62.0	-10.0	2.0	35.4	17.	22.	69.	266.	577.	61.31
N210A4.010	20.4	2.4	10.2	60.2	2.21	-62.0	-20.0	2.0	40.9	22.	22.	89.	230.	368.	44.89
N210A5.004	.3	.0	16.1	.0	-.01	-62.0	40.0	2.0	.7	0.	0.	141.	0.	0.	.11
N210A5.005	.9	.0	19.9	.0	.04	-62.0	30.0	2.0	2.5	0.	0.	174.	0.	0.	1.08
N210A5.006	17.3	3.1	12.9	49.4	2.39	-62.0	20.0	2.0	36.1	36.	39.	113.	269.	323.	49.18
N210A5.007	19.3	2.1	10.3	72.8	3.07	-62.0	10.0	2.0	39.3	18.	19.	90.	397.	523.	63.74
N210A5.008	19.8	1.6	9.8	90.5	3.29	-62.0	.0	2.0	40.1	14.	20.	86.	391.	626.	68.33
N210A5.009	16.8	2.3	9.7	85.5	2.63	-62.0	-10.0	2.0	35.3	24.	25.	84.	323.	597.	56.11
N210A5.010	17.3	3.8	9.6	52.8	2.09	-62.0	-20.0	2.0	36.1	40.	50.	84.	232.	284.	42.87
N210B1.004	.4	.0	13.6	.0	.04	-32.0	40.0	1.0	1.2	0.	0.	118.	0.	0.	.95
N210B1.005	1.2	26.1	26.1	26.1	.07	-32.0	30.0	1.0	3.2	0.	0.	227.	0.	0.	1.64
N210B1.006	14.3	2.9	8.5	80.1	1.57	-32.0	20.0	1.0	31.1	29.	36.	74.	222.	224.	33.06
N210B1.007	22.5	2.1	5.2	48.1	1.64	-32.0	10.0	1.0	44.0	22.	23.	45.	145.	349.	33.84
N210B1.008	21.9	1.9	9.4	85.7	2.86	-32.0	.0	1.0	43.1	17.	28.	82.	323.	739.	60.18
N210B1.009	22.9	1.0	8.6	77.4	2.26	-32.0	-10.0	1.0	44.5	24.	25.	75.	241.	549.	45.57
N210B1.010	21.7	3.0	9.1	86.2	2.03	-32.0	-20.0	1.0	42.9	26.	29.	80.	288.	662.	42.01

integral value of Conc. over time

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205B3.009	.6	.0	28.0	.0	.15	-32.0	25.0	1.0	1.5	0.	0.	172.	0.	0.	2.54
N205B3.008	10.2	1.9	13.5	24.0	.84	-32.0	20.0	1.0	23.4	12.	12.	83.	88.	90.	13.05
N205B3.007	14.3	1.9	11.8	18.8	.96	-32.0	15.0	1.0	31.1	13.	13.	73.	88.	89.	14.48
N205B3.006	26.7	.5	10.9	30.7	1.51	-32.0	10.0	1.0	49.5	3.	3.	67.	87.	88.	21.20
N205B3.005	23.0	1.1	10.2	67.3	2.37	-32.0	5.0	1.0	44.7	6.	6.	63.	121.	134.	32.34
N205B3.004	27.5	1.8	9.7	69.3	3.37	-32.0	.0	1.0	50.7	11.	13.	59.	140.	426.	45.65
N205B4.009	.5	.0	21.9	.0	.10	-32.0	25.0	1.0	1.3	0.	0.	135.	0.	0.	1.68
N205B4.008	22.3	1.4	15.8	23.6	1.03	-32.0	20.0	1.0	43.6	10.	11.	97.	139.	145.	15.54
N205B4.007	23.6	1.0	15.4	22.7	.97	-32.0	15.0	1.0	45.5	6.	7.	95.	138.	139.	14.60
N205B4.006	17.5	1.0	11.1	28.2	1.27	-32.0	10.0	1.0	36.4	6.	10.	68.	140.	141.	18.62
N205B4.005	23.4	1.9	9.9	77.4	1.78	-32.0	5.0	1.0	45.2	12.	13.	61.	237.	237.	25.70
N205B4.004	24.2	1.9	12.9	102.0	2.87	-32.0	.0	1.0	46.3	12.	16.	79.	179.	253.	41.17
N205B5.009	.7	.0	31.0	.0	.16	-32.0	25.0	1.0	1.8	0.	0.	191.	0.	0.	2.66
N205B5.008	9.5	1.5	12.2	23.2	.92	-32.0	20.0	1.0	22.2	10.	15.	75.	97.	132.	14.44
N205B5.007	13.0	1.2	10.7	22.6	.98	-32.0	15.0	1.0	28.7	8.	10.	66.	98.	110.	14.96
N205B5.006	20.8	.9	11.8	24.7	1.81	-32.0	10.0	1.0	41.4	6.	6.	73.	100.	102.	25.82
N205B5.005	22.5	.8	10.8	76.1	2.16	-32.0	5.0	1.0	43.9	5.	7.	66.	133.	444.	30.13
N205B5.004	22.3	1.1	5.7	71.7	3.07	-32.0	.0	1.0	43.6	7.	7.	35.	155.	261.	42.91
N205C1.009	.4	.0	20.7	.0	.08	-2.0	25.0	1.0	1.2	0.	0.	128.	0.	0.	1.34
N205C1.008	10.3	11.2	15.0	17.3	.41	-2.0	20.0	1.0	23.6	87.	88.	92.	100.	106.	6.44
N205C1.007	3.4	10.6	16.3	17.0	.27	-2.0	15.0	1.0	8.6	88.	0.	100.	0.	100.	4.49
N205C1.006	3.3	10.1	10.3	32.8	.28	-2.0	10.0	1.0	8.4	63.	0.	63.	0.	67.	4.58
N205C1.005	8.7	6.1	14.9	32.9	.29	-2.0	5.0	1.0	20.5	38.	90.	91.	92.	102.	4.82
N205C1.004	12.7	8.8	14.1	43.0	.77	-2.0	.0	1.0	28.2	55.	55.	87.	100.	126.	11.97
N205C2.009	.6	.0	30.2	.0	.11	-2.0	25.0	1.0	1.5	0.	0.	186.	0.	0.	1.81
N205C2.008	7.7	7.2	10.4	18.8	.46	-2.0	20.0	1.0	18.3	45.	63.	64.	80.	88.	7.42
N205C2.007	8.6	7.2	10.9	18.3	.46	-2.0	15.0	1.0	20.2	44.	64.	67.	82.	84.	7.27
N205C2.006	11.8	7.6	11.8	17.8	.53	-2.0	10.0	1.0	26.6	65.	65.	72.	82.	99.	8.11
N205C2.005	14.6	3.2	11.6	36.7	.58	-2.0	5.0	1.0	31.7	69.	70.	72.	87.	115.	8.91
N205C2.004	11.8	3.7	14.9	39.2	.96	-2.0	.0	1.0	26.5	55.	58.	92.	101.	229.	14.49
N205C3.009	.4	.0	31.1	.0	.07	-2.0	25.0	1.0	1.0	0.	0.	192.	0.	0.	1.29
N205C3.008	3.6	4.6	5.0	8.1	.28	-2.0	20.0	1.0	9.2	29.	0.	31.	0.	36.	4.59
N205C3.007	5.6	3.8	4.5	13.8	.29	-2.0	15.0	1.0	13.8	24.	26.	27.	30.	31.	4.82
N205C3.006	4.6	4.6	4.8	14.3	.30	-2.0	10.0	1.0	11.6	29.	29.	30.	31.	39.	4.98
N205C3.005	8.5	5.3	13.9	16.6	.38	-2.0	5.0	1.0	20.0	33.	76.	86.	88.	94.	6.30
N205C3.004	10.3	9.3	12.3	31.8	.52	-2.0	.0	1.0	23.7	75.	75.	76.	95.	98.	8.20
N205C4.009	.4	.0	26.4	.0	.12	-2.0	25.0	1.0	1.2	0.	0.	163.	0.	0.	1.93
N205C4.008	8.0	9.7	12.3	17.9	.50	-2.0	20.0	1.0	19.1	62.	63.	76.	101.	104.	7.98
N205C4.007	7.0	9.4	9.9	16.7	.44	-2.0	15.0	1.0	16.9	58.	59.	61.	95.	102.	7.06
N205C4.006	5.1	9.2	11.9	17.8	.34	-2.0	10.0	1.0	12.7	60.	72.	73.	78.	79.	5.62
N205C4.005	11.1	5.1	11.7	15.8	.50	-2.0	5.0	1.0	25.2	52.	54.	72.	82.	85.	7.95
N205C4.004	15.3	7.4	12.5	32.4	.89	-2.0	.0	1.0	32.9	46.	46.	77.	109.	110.	13.34

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205C5.009	.4	.0	38.6	.0	.08	-2.0	25.0	1.0	1.2	0.	0.	238.	0.	0.	1.49
N205C5.008	3.9	6.6	8.6	14.1	.37	-2.0	20.0	1.0	9.8	41.	0.	53.	0.	71.	6.02
N205C5.007	3.8	5.8	9.2	16.8	.33	-2.0	15.0	1.0	9.6	48.	0.	57.	0.	73.	5.50
N205C5.006	3.4	6.2	8.1	16.3	.34	-2.0	10.0	1.0	8.6	39.	0.	50.	0.	62.	5.64
N205C5.005	4.1	7.7	9.6	26.7	.38	-2.0	5.0	1.0	10.4	56.	59.	59.	61.	157.	6.31
N205C5.004	6.2	7.5	8.7	26.1	.53	-2.0	.0	1.0	15.2	48.	50.	53.	147.	152.	8.50
N205D1.009	.1	.0	.0	.0	.01	50.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.18
N205D1.008	.1	.0	.0	.0	.00	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.14
N205D1.007	.2	.0	.0	.0	.03	50.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.59
N205D1.006	.3	.0	23.0	.0	.03	50.0	28.0	1.0	.7	0.	0.	141.	0.	0.	.58
N205D1.005	.3	.0	29.1	.0	.05	50.0	25.0	1.0	.9	0.	0.	179.	0.	0.	.85
N205D1.004	.3	.0	25.0	.0	.07	50.0	22.0	1.0	.8	0.	0.	154.	0.	0.	1.19
N205D2.009	.0	.0	.0	.0	-.02	50.0	56.0	1.0	.1	0.	0.	0.	0.	0.	.02
N205D2.008	.1	.0	.0	.0	.01	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.28
N205D2.007	.1	.0	.0	.0	.01	50.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.26
N205D2.006	.3	.0	27.7	.0	.01	50.0	28.0	1.0	.9	0.	0.	171.	0.	0.	.42
N205D2.005	.4	.0	36.1	.0	.05	50.0	25.0	1.0	1.1	0.	0.	222.	0.	0.	.91
N205D2.004	.4	.0	27.9	.0	.06	50.0	22.0	1.0	1.0	0.	0.	172.	0.	0.	1.13
N205D3.009	.1	.0	.0	.0	-.01	50.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.06
N205D3.008	.1	.0	.0	.0	-.01	50.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.03
N205D3.007	.1	.0	.0	.0	.01	50.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.31
N205D3.006	.4	.0	22.1	.0	.06	50.0	28.0	1.0	1.0	0.	0.	136.	0.	0.	1.06
N205D3.005	.3	.0	18.7	.0	.06	50.0	25.0	1.0	.8	0.	0.	115.	0.	0.	.95
N205D3.004	.4	.0	17.3	.0	.08	50.0	22.0	1.0	1.1	0.	0.	106.	0.	0.	1.34
N205D4.009	.1	.0	.0	.0	.01	50.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.26
N205D4.008	.1	.0	.0	.0	.00	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.16
N205D4.007	.1	.0	.0	.0	.01	50.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.32
N205D4.006	.3	.0	28.2	.0	.04	50.0	28.0	1.0	.9	0.	0.	174.	0.	0.	.73
N205D4.005	.4	.0	28.6	.0	.04	50.0	25.0	1.0	1.0	0.	0.	176.	0.	0.	.73
N205D4.004	.4	.0	29.4	.0	.06	50.0	22.0	1.0	1.1	0.	0.	181.	0.	0.	1.02
N205D5.009	.1	.0	.0	.0	.01	50.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.26
N205D5.008	.1	.0	.0	.0	.03	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.58
N205D5.007	.2	.0	.0	.0	.04	50.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.63
N205D5.006	.4	.0	34.4	.0	.04	50.0	28.0	1.0	1.0	0.	0.	212.	0.	0.	.75
N205D5.005	.4	.0	22.9	.0	.04	50.0	25.0	1.0	1.0	0.	0.	141.	0.	0.	.72
N205D5.004	.4	.0	25.8	.0	.08	50.0	22.0	1.0	1.1	0.	0.	159.	0.	0.	1.43
N205E1.009	.0	.0	.0	.0	-.03	50.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.00
N205E1.008	.1	.0	.0	.0	-.02	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.03
N205E1.007	.1	.0	.0	.0	-.04	50.0	44.0	5.0	.2	0.	0.	0.	0.	0.	.01
N205E1.006	.3	.0	27.8	.0	.00	50.0	28.0	5.0	.7	0.	0.	171.	0.	0.	.36
N205E1.005	.4	.0	26.9	.0	.04	50.0	25.0	5.0	1.1	0.	0.	166.	0.	0.	.79
N205E1.004	.4	.0	27.1	.0	.06	50.0	22.0	5.0	1.1	0.	0.	167.	0.	0.	1.12

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205E2.009	.0	.0	.0	.0	-.02	50.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.04
N205E2.008	.1	.0	.0	.0	-.02	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.07
N205E2.007	.2	.0	.0	.0	-.01	50.0	44.0	5.0	.5	0.	0.	0.	0.	0.	.02
N205E2.006	.3	.0	28.0	.0	.02	50.0	28.0	5.0	.8	0.	0.	173.	0.	0.	.55
N205E2.005	.3	.0	27.7	.0	.05	50.0	25.0	5.0	.9	0.	0.	171.	0.	0.	.85
N205E2.004	.4	.0	37.3	.0	.06	50.0	22.0	5.0	1.1	0.	0.	230.	0.	0.	1.07
N205E3.009	.0	.0	.0	.0	.00	50.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.12
N205E3.008	.1	.0	.0	.0	.02	50.0	50.0	5.0	.3	0.	0.	0.	0.	0.	.44
N205E3.007	.3	.0	26.3	.0	.02	50.0	44.0	5.0	.7	0.	0.	162.	0.	0.	.43
N205E3.006	.5	.0	27.4	.0	.06	50.0	28.0	5.0	1.2	0.	0.	168.	0.	0.	1.04
N205E3.005	.5	.0	27.7	.0	.08	50.0	25.0	5.0	1.4	0.	0.	170.	0.	0.	1.35
N205E3.004	.5	.0	27.3	.0	.10	50.0	22.0	5.0	1.4	0.	0.	168.	0.	0.	1.61
N205E4.009	.0	.0	.0	.0	.00	50.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.03
N205E4.008	.1	.0	.0	.0	-.01	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.09
N205E4.007	.2	.0	.0	.0	.01	50.0	44.0	5.0	.5	0.	0.	0.	0.	0.	.15
N205E4.006	.4	.0	29.0	.0	.05	50.0	28.0	5.0	1.1	0.	0.	179.	0.	0.	.85
N205E4.005	.4	.0	29.8	.0	.06	50.0	25.0	5.0	1.1	0.	0.	184.	0.	0.	1.08
N205E4.004	.4	.0	28.6	.0	.09	50.0	22.0	5.0	1.1	0.	0.	176.	0.	0.	1.45
N205E5.009	.0	.0	.0	.0	-.01	50.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.03
N205E5.008	.1	.0	.0	.0	.00	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.00
N205E5.007	.1	.0	.0	.0	.01	50.0	44.0	5.0	.4	0.	0.	0.	0.	0.	.13
N205E5.006	.3	.0	15.2	.0	.03	50.0	28.0	5.0	.9	0.	0.	94.	0.	0.	.63
N205E5.005	.4	.0	18.5	.0	.05	50.0	25.0	5.0	1.0	0.	0.	114.	0.	0.	.87
N205E5.004	.4	.0	18.6	.0	.07	50.0	22.0	5.0	1.1	0.	0.	114.	0.	0.	1.22
N205F1.009	.0	.0	.0	.0	.00	50.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.04
N205F1.008	.1	.0	.0	.0	-.01	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.01
N205F1.007	.2	.0	31.1	.0	.01	50.0	44.0	11.0	.6	0.	0.	192.	0.	0.	.27
N205F1.006	.5	.0	17.4	.0	.04	50.0	28.0	11.0	1.2	0.	0.	107.	0.	0.	.68
N205F1.005	.6	.0	17.4	.0	.06	50.0	25.0	11.0	1.7	0.	0.	107.	0.	0.	1.10
N205F1.004	.5	.0	17.5	.0	.07	50.0	22.0	11.0	1.3	0.	0.	108.	0.	0.	1.13
N205F2.009	.0	.0	.0	.0	.00	50.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.12
N205F2.008	.0	.0	.0	.0	-.01	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.11
N205F2.007	.1	.0	.0	.0	-.03	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.03
N205F2.006	.6	.0	15.9	.0	.04	50.0	28.0	11.0	1.6	0.	0.	98.	0.	0.	.70
N205F2.005	.5	.0	15.9	.0	.03	50.0	25.0	11.0	1.2	0.	0.	98.	0.	0.	.72
N205F2.004	.4	.0	30.8	.0	.05	50.0	22.0	11.0	1.1	0.	0.	190.	0.	0.	.91
N205F3.009	.1	.0	.0	.0	.00	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.14
N205F3.008	.1	.0	.0	.0	.00	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.14
N205F3.007	.3	.0	23.4	.0	.01	50.0	44.0	11.0	.9	0.	0.	144.	0.	0.	.35
N205F3.006	.4	.0	17.5	.0	.03	50.0	28.0	11.0	1.1	0.	0.	108.	0.	0.	.72
N205F3.005	.4	.0	35.7	.0	.06	50.0	25.0	11.0	1.0	0.	0.	220.	0.	0.	1.07
N205F3.004	.4	.0	22.4	.0	.07	50.0	22.0	11.0	1.1	0.	0.	138.	0.	0.	1.16

FALCON 2: LSR = 50, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205F4.009	.1	.0	.0	.0	-.01	50.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.03
N205F4.008	.1	.0	.0	.0	-.01	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.05
N205F4.007	.2	.0	.0	.0	-.01	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.14
N205F4.006	.4	.0	26.2	.0	.04	50.0	28.0	11.0	1.0	0.	0.	161.	0.	0.	.79
N205F4.005	.6	.0	16.5	.0	.05	50.0	25.0	11.0	1.6	0.	0.	102.	0.	0.	.86
N205F4.004	.5	.0	16.5	.0	.06	50.0	22.0	11.0	1.4	0.	0.	102.	0.	0.	1.07
N205F5.009	.0	.0	.0	.0	-.02	50.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.05
N205F5.008	.0	.0	.0	.0	-.01	50.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.00
N205F5.007	.1	.0	.0	.0	.00	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.02
N205F5.006	.7	.0	24.2	.0	.05	50.0	28.0	11.0	1.8	0.	0.	149.	0.	0.	.87
N205F5.005	.6	.0	25.2	.0	.06	50.0	25.0	11.0	1.5	0.	0.	155.	0.	0.	1.03
N205F5.004	.5	.0	24.6	.0	.06	50.0	22.0	11.0	1.3	0.	0.	151.	0.	0.	1.06
N205G1.009	.0	.0	.0	.0	-.02	50.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.03
N205G1.008	.0	.0	.0	.0	-.03	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.02
N205G1.007	.0	.0	.0	.0	-.03	50.0	44.0	17.0	.0	0.	0.	0.	0.	0.	.01
N205G1.006	.4	.0	26.2	.0	-.02	50.0	28.0	17.0	1.0	0.	0.	162.	0.	0.	.17
N205G1.005	.4	.0	40.7	.0	.00	50.0	25.0	17.0	1.1	0.	0.	251.	0.	0.	.32
N205G1.004	.4	.0	24.0	.0	.01	50.0	22.0	17.0	1.1	0.	0.	148.	0.	0.	.50
N205G2.009	.0	.0	.0	.0	-.01	50.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.06
N205G2.008	.1	.0	.0	.0	.00	50.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.01
N205G2.007	.1	.0	.0	.0	.00	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.12
N205G2.006	.5	.0	24.7	.0	.03	50.0	28.0	17.0	1.3	0.	0.	152.	0.	0.	.64
N205G2.005	.5	.0	24.8	.0	.04	50.0	25.0	17.0	1.4	0.	0.	153.	0.	0.	.63
N205G2.004	.5	.0	21.8	.0	.05	50.0	22.0	17.0	1.4	0.	0.	134.	0.	0.	.89
N205G3.009	.0	.0	.0	.0	.01	50.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.22
N205G3.008	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.16
N205G3.007	.1	.0	.0	.0	.01	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.10
N205G3.006	.5	.0	23.5	.0	.01	50.0	28.0	17.0	1.4	0.	0.	145.	0.	0.	.43
N205G3.005	.5	.0	23.4	.0	.03	50.0	25.0	17.0	1.3	0.	0.	144.	0.	0.	.64
N205G3.004	.5	.0	23.2	.0	.04	50.0	22.0	17.0	1.2	0.	0.	143.	0.	0.	.79
N205G4.009	.1	.0	.0	.0	-.01	50.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.07
N205G4.008	.1	.0	.0	.0	-.01	50.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.11
N205G4.007	.1	.0	.0	.0	-.01	50.0	44.0	17.0	.4	0.	0.	0.	0.	0.	.14
N205G4.006	.3	.0	30.4	.0	.01	50.0	28.0	17.0	.9	0.	0.	187.	0.	0.	.28
N205G4.005	.4	.0	26.8	.0	.01	50.0	25.0	17.0	1.2	0.	0.	165.	0.	0.	.40
N205G4.004	.5	.0	25.1	.0	.03	50.0	22.0	17.0	1.4	0.	0.	155.	0.	0.	.68
N205G5.009	.1	.0	.0	.0	-.02	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.03
N205G5.008	.1	.0	.0	.0	-.01	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.04
N205G5.007	.1	.0	.0	.0	-.02	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.04
N205G5.006	.4	.0	32.0	.0	.00	50.0	28.0	17.0	1.2	0.	0.	197.	0.	0.	.26
N205G5.005	.4	.0	32.1	.0	.01	50.0	25.0	17.0	1.0	0.	0.	198.	0.	0.	.33
N205G5.004	.5	.0	24.2	.0	.03	50.0	22.0	17.0	1.2	0.	0.	149.	0.	0.	.60

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205H1.009	.4	.0	28.5	.0	.14	50.0	.0	1.0	1.1	0.	0.	175.	0.	0.	2.24
N205H1.008	.3	.0	21.3	.0	.06	50.0	-11.0	1.0	.9	0.	0.	131.	0.	0.	1.10
N205H1.007	.4	.0	23.9	.0	.04	50.0	-22.0	1.0	1.1	0.	0.	147.	0.	0.	.63
N205H1.006	.5	.0	26.7	.0	.04	50.0	-25.0	1.0	1.4	0.	0.	164.	0.	0.	.67
N205H1.005	.7	.0	26.7	.0	.02	50.0	-28.0	1.0	1.8	0.	0.	164.	0.	0.	.46
N205H1.004	.3	.0	26.7	.0	.00	50.0	-44.0	1.0	.9	0.	0.	165.	0.	0.	.22
N205H2.009	.4	.0	28.7	.0	.12	50.0	.0	1.0	1.1	0.	0.	177.	0.	0.	1.93
N205H2.008	.4	.0	21.9	.0	.11	50.0	-11.0	1.0	1.0	0.	0.	135.	0.	0.	1.78
N205H2.007	.4	.0	29.2	.0	.09	50.0	-22.0	1.0	1.0	0.	0.	180.	0.	0.	1.53
N205H2.006	.4	.0	25.0	.0	.10	50.0	-25.0	1.0	1.1	0.	0.	154.	0.	0.	1.63
N205H2.005	.4	.0	25.1	.0	.10	50.0	-28.0	1.0	1.2	0.	0.	155.	0.	0.	1.72
N205H2.004	.3	.0	30.7	.0	.06	50.0	-44.0	1.0	.7	0.	0.	189.	0.	0.	.99
N205H3.009	.4	.0	28.1	.0	.12	50.0	.0	1.0	1.0	0.	0.	173.	0.	0.	1.97
N205H3.008	.4	.0	24.6	.0	.10	50.0	-11.0	1.0	1.0	0.	0.	151.	0.	0.	1.60
N205H3.007	.5	.0	25.8	.0	.07	50.0	-22.0	1.0	1.3	0.	0.	159.	0.	0.	1.21
N205H3.006	.4	.0	26.2	.0	.06	50.0	-25.0	1.0	1.1	0.	0.	162.	0.	0.	1.07
N205H3.005	.4	.0	26.2	.0	.04	50.0	-28.0	1.0	1.1	0.	0.	161.	0.	0.	.86
N205H3.004	.2	.0	27.1	.0	.02	50.0	-44.0	1.0	.6	0.	0.	167.	0.	0.	.49
N205H4.009	.4	.0	24.1	.0	.13	50.0	.0	1.0	.9	0.	0.	148.	0.	0.	2.23
N205H4.008	.3	.0	26.5	.0	.09	50.0	-11.0	1.0	.9	0.	0.	163.	0.	0.	1.55
N205H4.007	.3	.0	36.9	.0	.06	50.0	-22.0	1.0	.8	0.	0.	227.	0.	0.	.98
N205H4.006	.3	.0	18.4	.0	.05	50.0	-25.0	1.0	.7	0.	0.	113.	0.	0.	.87
N205H4.005	.3	.0	19.4	.0	.03	50.0	-28.0	1.0	.9	0.	0.	119.	0.	0.	.59
N205H4.004	.1	.0	.0	.0	.05	50.0	-44.0	1.0	.4	0.	0.	0.	0.	0.	.83
N205H5.009	.5	.0	24.4	.0	.19	50.0	.0	1.0	1.4	0.	0.	150.	0.	0.	3.09
N205H5.008	.3	.0	23.3	.0	.08	50.0	-11.0	1.0	.9	0.	0.	144.	0.	0.	1.47
N205H5.007	.3	.0	17.8	.0	.04	50.0	-22.0	1.0	.7	0.	0.	109.	0.	0.	.76
N205H5.006	.3	.0	36.3	.0	.05	50.0	-25.0	1.0	.9	0.	0.	223.	0.	0.	.82
N205H5.005	.3	.0	27.4	.0	.03	50.0	-28.0	1.0	.7	0.	0.	168.	0.	0.	.56
N205H5.004	.2	.0	31.5	.0	.01	50.0	-44.0	1.0	.6	0.	0.	194.	0.	0.	.28
N205I1.009	.4	.0	30.1	.0	.13	50.0	.0	5.0	1.2	0.	0.	185.	0.	0.	2.18
N205I1.008	.4	.0	31.8	.0	.11	50.0	-11.0	5.0	1.0	0.	0.	196.	0.	0.	1.80
N205I1.007	.3	.0	17.6	.0	.07	50.0	-22.0	5.0	.9	0.	0.	108.	0.	0.	1.29
N205I1.006	.4	.0	33.4	.0	.03	50.0	-25.0	5.0	1.1	0.	0.	206.	0.	0.	.79
N205I1.005	.4	.0	33.3	.0	.04	50.0	-28.0	5.0	1.0	0.	0.	205.	0.	0.	.72
N205I1.004	.1	.0	.0	.0	.02	50.0	-44.0	5.0	.3	0.	0.	0.	0.	0.	.41
N205I2.009	.5	.0	27.2	.0	.14	50.0	.0	5.0	1.4	0.	0.	168.	0.	0.	2.44
N205I2.008	.4	.0	26.9	.0	.10	50.0	-11.0	5.0	1.0	0.	0.	165.	0.	0.	1.74
N205I2.007	.3	.0	21.4	.0	.07	50.0	-22.0	5.0	.9	0.	0.	132.	0.	0.	1.24
N205I2.006	.4	.0	22.5	.0	.07	50.0	-25.0	5.0	1.0	0.	0.	138.	0.	0.	1.24
N205I2.005	.4	.0	22.2	.0	.05	50.0	-28.0	5.0	1.0	0.	0.	137.	0.	0.	.85
N205I2.004	.0	.0	.0	.0	-.03	50.0	-44.0	5.0	.1	0.	0.	0.	0.	0.	.04

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205I3.009	.3	.0	35.2	.0	.14	50.0	.0	5.0	.9	0.	0.	217.	0.	0.	2.35
N205I3.008	.4	.0	23.7	.0	.10	50.0	-11.0	5.0	1.1	0.	0.	146.	0.	0.	1.71
N205I3.007	.5	.0	15.1	.0	.07	50.0	-22.0	5.0	1.3	0.	0.	93.	0.	0.	1.33
N205I3.006	.6	.0	15.0	.0	.06	50.0	-25.0	5.0	1.5	0.	0.	93.	0.	0.	1.11
N205I3.005	.5	.0	15.0	.0	.04	50.0	-28.0	5.0	1.4	0.	0.	92.	0.	0.	.87
N205I3.004	.1	.0	.0	.0	.01	50.0	-44.0	5.0	.3	0.	0.	0.	0.	0.	.24
N205I4.009	.4	.0	32.2	.0	.13	50.0	.0	5.0	1.2	0.	0.	198.	0.	0.	2.28
N205I4.008	.5	.0	25.0	.0	.11	50.0	-11.0	5.0	1.2	0.	0.	154.	0.	0.	1.86
N205I4.007	.5	.0	23.6	.0	.06	50.0	-22.0	5.0	1.2	0.	0.	145.	0.	0.	1.10
N205I4.006	.4	.0	24.1	.0	.06	50.0	-25.0	5.0	1.2	0.	0.	148.	0.	0.	1.11
N205I4.005	.4	.0	24.4	.0	.05	50.0	-28.0	5.0	1.1	0.	0.	150.	0.	0.	.80
N205I4.004	.2	.0	22.2	.0	.04	50.0	-44.0	5.0	.6	0.	0.	137.	0.	0.	.71
N205I5.009	.3	.0	21.7	.0	.09	50.0	.0	5.0	.9	0.	0.	134.	0.	0.	1.74
N205I5.008	.4	.0	16.9	.0	.13	50.0	-11.0	5.0	1.0	0.	0.	104.	0.	0.	2.13
N205I5.007	.3	.0	17.0	.0	.07	50.0	-22.0	5.0	.9	0.	0.	105.	0.	0.	1.21
N205I5.006	.3	.0	17.3	.0	.05	50.0	-25.0	5.0	.9	0.	0.	106.	0.	0.	.79
N205I5.005	.3	.0	17.1	.0	.04	50.0	-28.0	5.0	.9	0.	0.	105.	0.	0.	.65
N205I5.004	.1	.0	.0	.0	.00	50.0	-44.0	5.0	.2	0.	0.	0.	0.	0.	.18
N205J1.009	.4	.0	30.7	.0	.09	50.0	.0	11.0	1.0	0.	0.	189.	0.	0.	1.59
N205J1.008	.5	.0	31.2	.0	.09	50.0	-11.0	11.0	1.3	0.	0.	192.	0.	0.	1.52
N205J1.007	.4	.0	30.3	.0	.09	50.0	-22.0	11.0	1.1	0.	0.	187.	0.	0.	1.48
N205J1.006	.5	.0	30.5	.0	.07	50.0	-25.0	11.0	1.3	0.	0.	188.	0.	0.	1.17
N205J1.005	.4	.0	27.7	.0	.03	50.0	-28.0	11.0	1.1	0.	0.	171.	0.	0.	.55
N205J1.004	.2	.0	.0	.0	.04	50.0	-44.0	11.0	.5	0.	0.	0.	0.	0.	.69
N205J2.009	.6	.0	27.5	.0	.03	50.0	.0	11.0	1.6	0.	0.	170.	0.	0.	1.40
N205J2.008	.4	.0	26.9	.0	.07	50.0	-11.0	11.0	1.1	0.	0.	166.	0.	0.	1.26
N205J2.007	.4	.0	25.9	.0	.06	50.0	-22.0	11.0	1.0	0.	0.	160.	0.	0.	.99
N205J2.006	.3	.0	25.9	.0	.03	50.0	-25.0	11.0	.9	0.	0.	159.	0.	0.	.65
N205J2.005	.3	.0	27.9	.0	.01	50.0	-28.0	11.0	.9	0.	0.	172.	0.	0.	.39
N205J2.004	.1	.0	.0	.0	-.03	50.0	-44.0	11.0	.1	0.	0.	0.	0.	0.	.06
N205J3.009	.4	.0	29.1	.0	.13	50.0	.0	11.0	1.1	0.	0.	179.	0.	0.	2.23
N205J3.008	.4	.0	28.3	.0	.08	50.0	-11.0	11.0	1.1	0.	0.	174.	0.	0.	1.30
N205J3.007	.3	.0	30.3	.0	.06	50.0	-22.0	11.0	.9	0.	0.	187.	0.	0.	1.16
N205J3.006	.3	.0	17.6	.0	.06	50.0	-25.0	11.0	.9	0.	0.	108.	0.	0.	1.10
N205J3.005	.5	.0	22.4	.0	.06	50.0	-28.0	11.0	1.2	0.	0.	138.	0.	0.	1.03
N205J3.004	.2	.0	.0	.0	.03	50.0	-44.0	11.0	.4	0.	0.	0.	0.	0.	.63
N205J4.009	.4	.0	25.3	.0	.11	50.0	.0	11.0	1.1	0.	0.	156.	0.	0.	1.88
N205J4.008	.4	.0	23.4	.0	.06	50.0	-11.0	11.0	1.0	0.	0.	144.	0.	0.	1.14
N205J4.007	.4	.0	23.5	.0	.08	50.0	-22.0	11.0	1.2	0.	0.	144.	0.	0.	1.48
N205J4.006	.5	.0	15.2	.0	.04	50.0	-25.0	11.0	1.4	0.	0.	93.	0.	0.	.86
N205J4.005	.4	.0	30.5	.0	.03	50.0	-28.0	11.0	1.2	0.	0.	188.	0.	0.	.64
N205J4.004	.1	.0	.0	.0	-.02	50.0	-44.0	11.0	.3	0.	0.	0.	0.	0.	.13

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205J5.009	.4	.0	31.8	.0	.08	50.0	.0	11.0	1.1	0.	0.	196.	0.	0.	1.45
N205J5.008	.4	.0	21.8	.0	.06	50.0	-11.0	11.0	1.2	0.	0.	134.	0.	0.	1.19
N205J5.007	.3	.0	20.8	.0	.06	50.0	-22.0	11.0	.9	0.	0.	128.	0.	0.	1.06
N205J5.006	.4	.0	20.8	.0	.04	50.0	-25.0	11.0	1.1	0.	0.	128.	0.	0.	.68
N205J5.005	.3	.0	15.9	.0	.02	50.0	-28.0	11.0	.9	0.	0.	98.	0.	0.	.37
N205J5.004	.1	.0	.0	.0	.00	50.0	-44.0	11.0	.2	0.	0.	0.	0.	0.	.26
N205K1.009	.5	.0	28.4	.0	.07	50.0	.0	17.0	1.3	0.	0.	175.	0.	0.	1.18
N205K1.008	.5	.0	28.4	.0	.04	50.0	-11.0	17.0	1.4	0.	0.	175.	0.	0.	.78
N205K1.007	.3	.0	29.4	.0	.03	50.0	-22.0	17.0	.9	0.	0.	181.	0.	0.	.62
N205K1.006	.3	.0	24.3	.0	.02	50.0	-25.0	17.0	.9	0.	0.	150.	0.	0.	.41
N205K1.005	.3	.0	34.0	.0	.01	50.0	-28.0	17.0	.7	0.	0.	209.	0.	0.	.33
N205K1.004	.1	.0	.0	.0	-.01	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.17
N205K2.009	.5	.0	21.5	.0	.05	50.0	.0	17.0	1.3	0.	0.	132.	0.	0.	1.08
N205K2.008	.5	.0	17.8	.0	.08	50.0	-11.0	17.0	1.4	0.	0.	110.	0.	0.	1.41
N205K2.007	.3	.0	17.5	.0	.02	50.0	-22.0	17.0	.9	0.	0.	108.	0.	0.	.37
N205K2.006	.4	.0	14.9	.0	.02	50.0	-25.0	17.0	1.0	0.	0.	92.	0.	0.	.48
N205K2.005	.3	.0	37.7	.0	.04	50.0	-28.0	17.0	.8	0.	0.	232.	0.	0.	.60
N205K2.004	.1	.0	.0	.0	-.02	50.0	-44.0	17.0	.1	0.	0.	0.	0.	0.	.11
N205K3.009	.5	.0	34.3	.0	.06	50.0	.0	17.0	1.2	0.	0.	211.	0.	0.	1.22
N205K3.008	.5	.0	24.0	.0	.03	50.0	-11.0	17.0	1.3	0.	0.	148.	0.	0.	.64
N205K3.007	.6	.0	18.0	.0	.01	50.0	-22.0	17.0	1.5	0.	0.	111.	0.	0.	.42
N205K3.006	.5	.0	34.2	.0	.02	50.0	-25.0	17.0	1.3	0.	0.	211.	0.	0.	.55
N205K3.005	.4	.0	33.9	.0	.02	50.0	-28.0	17.0	1.1	0.	0.	209.	0.	0.	.42
N205K3.004	.1	.0	.0	.0	-.01	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.04
N205K4.009	.4	.0	34.8	.0	.00	50.0	.0	17.0	.9	0.	0.	214.	0.	0.	.59
N205K4.008	.4	.0	35.7	.0	.03	50.0	-11.0	17.0	1.0	0.	0.	220.	0.	0.	.58
N205K4.007	.3	.0	11.3	.0	.01	50.0	-22.0	17.0	.7	0.	0.	70.	0.	0.	.45
N205K4.006	.5	.0	16.6	.0	.02	50.0	-25.0	17.0	1.2	0.	0.	102.	0.	0.	.40
N205K4.005	.5	.0	16.7	.0	.01	50.0	-28.0	17.0	1.3	0.	0.	103.	0.	0.	.24
N205K4.004	.1	.0	.0	.0	-.01	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.08
N205K5.009	.5	.0	23.9	.0	.03	50.0	.0	17.0	1.4	0.	0.	147.	0.	0.	.75
N205K5.008	.5	.0	16.6	.0	.06	50.0	-11.0	17.0	1.3	0.	0.	102.	0.	0.	.99
N205K5.007	.6	.0	16.9	.0	.05	50.0	-22.0	17.0	1.5	0.	0.	104.	0.	0.	.90
N205K5.006	.5	.0	16.7	.0	.05	50.0	-25.0	17.0	1.3	0.	0.	103.	0.	0.	.85
N205K5.005	.5	.0	21.1	.0	.04	50.0	-28.0	17.0	1.2	0.	0.	130.	0.	0.	.80
N205K5.004	.1	.0	.0	.0	.01	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.11
N205L1.009	.1	.0	.0	.0	.03	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.58
N205L1.008	.1	.0	.0	.0	-.01	150.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.11
N205L1.007	.2	.0	26.8	.0	.04	150.0	44.0	1.0	.6	0.	0.	165.	0.	0.	.65
N205L1.006	.3	.0	27.0	.0	.04	150.0	28.0	1.0	.7	0.	0.	166.	0.	0.	.79
N205L1.005	.2	.0	27.0	.0	.07	150.0	25.0	1.0	.7	0.	0.	166.	0.	0.	1.11
N205L1.004	.3	.0	33.2	.0	.06	150.0	22.0	1.0	.8	0.	0.	205.	0.	0.	1.12

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205L2.009	.1	.0	.0	.0	.00	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.22
N205L2.008	.1	.0	.0	.0	.01	150.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.17
N205L2.007	.2	.0	.0	.0	.02	150.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.41
N205L2.006	.2	.0	29.2	.0	.06	150.0	28.0	1.0	.6	0.	0.	180.	0.	0.	1.02
N205L2.005	.3	.0	45.0	.0	.06	150.0	25.0	1.0	.7	0.	0.	277.	0.	0.	1.02
N205L2.004	.3	.0	28.4	.0	.05	150.0	22.0	1.0	.7	0.	0.	175.	0.	0.	.91
N205L3.009	.1	.0	.0	.0	.01	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.18
N205L3.008	.1	.0	.0	.0	.01	150.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.19
N205L3.007	.2	.0	.0	.0	.02	150.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.44
N205L3.006	.3	.0	29.8	.0	.06	150.0	28.0	1.0	.9	0.	0.	183.	0.	0.	1.03
N205L3.005	.3	.0	28.1	.0	.06	150.0	25.0	1.0	.8	0.	0.	173.	0.	0.	1.07
N205L3.004	.4	.0	46.2	.0	.08	150.0	22.0	1.0	1.0	0.	0.	285.	0.	0.	1.34
N205L4.009	.1	.0	.0	.0	-.01	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.17
N205L4.008	.1	.0	.0	.0	.02	150.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.39
N205L4.007	.1	.0	.0	.0	.01	150.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.25
N205L4.006	.3	.0	43.2	.0	.07	150.0	28.0	1.0	.7	0.	0.	266.	0.	0.	1.21
N205L4.005	.2	.0	31.5	.0	.07	150.0	25.0	1.0	.6	0.	0.	194.	0.	0.	1.11
N205L4.004	.3	.0	37.1	.0	.06	150.0	22.0	1.0	.7	0.	0.	228.	0.	0.	1.00
N205L5.009	.1	.0	.0	.0	.01	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.29
N205L5.008	.2	.0	45.4	.0	.01	150.0	50.0	1.0	.7	0.	0.	279.	0.	0.	.39
N205L5.007	.2	.0	44.9	.0	.03	150.0	44.0	1.0	.6	0.	0.	276.	0.	0.	.55
N205L5.006	.2	.0	22.2	.0	.04	150.0	28.0	1.0	.6	0.	0.	137.	0.	0.	.79
N205L5.005	.3	.0	33.8	.0	.06	150.0	25.0	1.0	.7	0.	0.	208.	0.	0.	1.03
N205L5.004	.3	.0	30.8	.0	.06	150.0	22.0	1.0	.8	0.	0.	189.	0.	0.	1.13
N205M1.009	.1	.0	.0	.0	.01	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.20
N205M1.008	.2	.0	37.3	.0	.02	150.0	50.0	5.0	.6	0.	0.	230.	0.	0.	.41
N205M1.007	.2	.0	.0	.0	.02	150.0	44.0	5.0	.5	0.	0.	0.	0.	0.	.37
N205M1.006	.2	.0	26.7	.0	.05	150.0	28.0	5.0	.6	0.	0.	165.	0.	0.	.94
N205M1.005	.2	.0	26.1	.0	.06	150.0	25.0	5.0	.7	0.	0.	161.	0.	0.	1.05
N205M1.004	.3	.0	28.7	.0	.07	150.0	22.0	5.0	.9	0.	0.	176.	0.	0.	1.19
N205M2.009	.1	.0	.0	.0	.02	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.33
N205M2.008	.2	.0	25.5	.0	.02	150.0	50.0	5.0	.7	0.	0.	157.	0.	0.	.39
N205M2.007	.2	.0	25.5	.0	.04	150.0	44.0	5.0	.6	0.	0.	157.	0.	0.	.72
N205M2.006	.2	.0	26.5	.0	.05	150.0	28.0	5.0	.6	0.	0.	163.	0.	0.	.82
N205M2.005	.2	.0	29.8	.0	.04	150.0	25.0	5.0	.7	0.	0.	184.	0.	0.	.75
N205M2.004	.3	.0	30.3	.0	.07	150.0	22.0	5.0	.9	0.	0.	187.	0.	0.	1.22
N205M3.009	.1	.0	.0	.0	.00	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.10
N205M3.008	.2	.0	35.5	.0	.01	150.0	50.0	5.0	.6	0.	0.	218.	0.	0.	.28
N205M3.007	.2	.0	.0	.0	.02	150.0	44.0	5.0	.5	0.	0.	0.	0.	0.	.40
N205M3.006	.3	.0	32.6	.0	.04	150.0	28.0	5.0	.7	0.	0.	201.	0.	0.	.74
N205M3.005	.2	.0	29.8	.0	.05	150.0	25.0	5.0	.7	0.	0.	184.	0.	0.	.87
N205M3.004	.3	.0	29.9	.0	.06	150.0	22.0	5.0	.9	0.	0.	184.	0.	0.	1.09

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205M4.009	.1	.0	.0	.0	.01	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.23
N205M4.008	.1	.0	.0	.0	.02	150.0	50.0	5.0	.4	0.	0.	0.	0.	0.	.37
N205M4.007	.1	.0	.0	.0	.03	150.0	44.0	5.0	.4	0.	0.	0.	0.	0.	.53
N205M4.006	.3	.0	41.2	.0	.03	150.0	28.0	5.0	.8	0.	0.	254.	0.	0.	.64
N205M4.005	.2	.0	28.4	.0	.05	150.0	25.0	5.0	.6	0.	0.	175.	0.	0.	.85
N205M4.004	.2	.0	26.0	.0	.03	150.0	22.0	5.0	.6	0.	0.	160.	0.	0.	.68
N205M5.009	.1	.0	.0	.0	.02	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.31
N205M5.008	.2	.0	.0	.0	.02	150.0	50.0	5.0	.5	0.	0.	0.	0.	0.	.27
N205M5.007	.2	.0	29.9	.0	.04	150.0	44.0	5.0	.7	0.	0.	184.	0.	0.	.64
N205M5.006	.2	.0	32.9	.0	.04	150.0	28.0	5.0	.6	0.	0.	203.	0.	0.	.78
N205M5.005	.3	.0	33.8	.0	.06	150.0	25.0	5.0	.7	0.	0.	208.	0.	0.	1.00
N205M5.004	.3	.0	33.9	.0	.05	150.0	22.0	5.0	.8	0.	0.	209.	0.	0.	.97
N205N1.009	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.03
N205N1.008	.1	.0	.0	.0	-.01	150.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.05
N205N1.007	.1	.0	.0	.0	-.01	150.0	44.0	11.0	.3	0.	0.	0.	0.	0.	.04
N205N1.006	.2	.0	21.2	.0	.02	150.0	28.0	11.0	.6	0.	0.	131.	0.	0.	.33
N205N1.005	.3	.0	36.0	.0	.03	150.0	25.0	11.0	.8	0.	0.	222.	0.	0.	.51
N205N1.004	.3	.0	36.1	.0	.03	150.0	22.0	11.0	.9	0.	0.	222.	0.	0.	.68
N205N2.009	.1	.0	.0	.0	-.01	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.04
N205N2.008	.1	.0	.0	.0	-.01	150.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.11
N205N2.007	.2	.0	.0	.0	.01	150.0	44.0	11.0	.5	0.	0.	0.	0.	0.	.26
N205N2.006	.2	.0	29.9	.0	.03	150.0	28.0	11.0	.6	0.	0.	184.	0.	0.	.49
N205N2.005	.2	.0	41.6	.0	.04	150.0	25.0	11.0	.6	0.	0.	256.	0.	0.	.65
N205N2.004	.3	.0	42.0	.0	.05	150.0	22.0	11.0	.9	0.	0.	259.	0.	0.	.83
N205N3.009	.0	.0	.0	.0	.00	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.08
N205N3.008	.1	.0	.0	.0	.00	150.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.05
N205N3.007	.1	.0	.0	.0	.01	150.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.11
N205N3.006	.3	.0	33.5	.0	.01	150.0	28.0	11.0	.9	0.	0.	206.	0.	0.	.37
N205N3.005	.3	.0	33.7	.0	.04	150.0	25.0	11.0	.8	0.	0.	208.	0.	0.	.64
N205N3.004	.3	.0	28.2	.0	.04	150.0	22.0	11.0	.7	0.	0.	174.	0.	0.	.72
N205N4.009	.1	.0	.0	.0	.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.21
N205N4.008	.1	.0	.0	.0	.00	150.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.02
N205N4.007	.1	.0	.0	.0	-.01	150.0	44.0	11.0	.3	0.	0.	0.	0.	0.	.04
N205N4.006	.3	.0	30.0	.0	.03	150.0	28.0	11.0	.7	0.	0.	185.	0.	0.	.58
N205N4.005	.3	.0	34.8	.0	.04	150.0	25.0	11.0	.7	0.	0.	214.	0.	0.	.66
N205N4.004	.3	.0	23.3	.0	.05	150.0	22.0	11.0	.9	0.	0.	143.	0.	0.	.88
N205N5.009	.1	.0	.0	.0	.00	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.08
N205N5.008	.1	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.15
N205N5.007	.1	.0	.0	.0	.00	150.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.06
N205N5.006	.2	.0	.0	.0	.03	150.0	28.0	11.0	.5	0.	0.	0.	0.	0.	.59
N205N5.005	.2	.0	31.0	.0	.04	150.0	25.0	11.0	.6	0.	0.	191.	0.	0.	.65
N205N5.004	.3	.0	31.1	.0	.04	150.0	22.0	11.0	.7	0.	0.	191.	0.	0.	.77

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N20501.009	.1	.0	.0	.0	-.01	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.03
N20501.008	.1	.0	.0	.0	-.01	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.04
N20501.007	.1	.0	.0	.0	.00	150.0	44.0	17.0	.4	0.	0.	0.	0.	0.	.07
N20501.006	.3	.0	42.0	.0	.03	150.0	28.0	17.0	.7	0.	0.	259.	0.	0.	.52
N20501.005	.3	.0	34.0	.0	.02	150.0	25.0	17.0	.7	0.	0.	209.	0.	0.	.42
N20501.004	.2	.0	41.8	.0	.01	150.0	22.0	17.0	.7	0.	0.	258.	0.	0.	.48
N20502.009	.1	.0	.0	.0	.00	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.07
N20502.008	.1	.0	.0	.0	.00	150.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.05
N20502.007	.1	.0	.0	.0	.00	150.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.22
N20502.006	.2	.0	24.0	.0	.02	150.0	28.0	17.0	.6	0.	0.	148.	0.	0.	.34
N20502.005	.2	.0	.0	.0	.02	150.0	25.0	17.0	.5	0.	0.	0.	0.	0.	.35
N20502.004	.2	.0	46.0	.0	.02	150.0	22.0	17.0	.6	0.	0.	284.	0.	0.	.45
N20503.009	.1	.0	.0	.0	.01	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.27
N20503.008	.1	.0	.0	.0	.01	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.13
N20503.007	.2	.0	.0	.0	.01	150.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.20
N20503.006	.2	.0	25.7	.0	.02	150.0	28.0	17.0	.6	0.	0.	158.	0.	0.	.41
N20503.005	.2	.0	45.8	.0	.03	150.0	25.0	17.0	.7	0.	0.	282.	0.	0.	.53
N20503.004	.2	.0	25.9	.0	.02	150.0	22.0	17.0	.6	0.	0.	160.	0.	0.	.33
N20504.009	.1	.0	.0	.0	.01	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.14
N20504.008	.1	.0	.0	.0	.00	150.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.04
N20504.007	.1	.0	.0	.0	.00	150.0	44.0	17.0	.4	0.	0.	0.	0.	0.	.09
N20504.006	.2	.0	34.3	.0	.01	150.0	28.0	17.0	.6	0.	0.	211.	0.	0.	.34
N20504.005	.2	.0	28.9	.0	.02	150.0	25.0	17.0	.6	0.	0.	178.	0.	0.	.40
N20504.004	.3	.0	34.0	.0	.02	150.0	22.0	17.0	.7	0.	0.	209.	0.	0.	.51
N20505.009	.1	.0	.0	.0	.00	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.11
N20505.008	.1	.0	.0	.0	.01	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.25
N20505.007	.1	.0	.0	.0	.00	150.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.22
N20505.006	.2	.0	31.7	.0	.02	150.0	28.0	17.0	.6	0.	0.	195.	0.	0.	.29
N20505.005	.2	.0	.0	.0	.02	150.0	25.0	17.0	.5	0.	0.	0.	0.	0.	.41
N20505.004	.2	.0	.0	.0	.02	150.0	22.0	17.0	.5	0.	0.	0.	0.	0.	.43
N205P1.009	.3	.0	29.3	.0	.06	150.0	.0	1.0	.7	0.	0.	180.	0.	0.	1.11
N205P1.008	.3	.0	36.2	.0	.10	150.0	-11.0	1.0	.8	0.	0.	223.	0.	0.	1.73
N205P1.007	.3	.0	37.2	.0	.08	150.0	-22.0	1.0	.7	0.	0.	229.	0.	0.	1.31
N205P1.006	.2	.0	.0	.0	.02	150.0	-25.0	1.0	.4	0.	0.	0.	0.	0.	.53
N205P1.005	.2	.0	.0	.0	.05	150.0	-28.0	1.0	.4	0.	0.	0.	0.	0.	.88
N205P1.004	.1	.0	.0	.0	.01	150.0	-44.0	1.0	.3	0.	0.	0.	0.	0.	.26
N205P2.009	.3	.0	38.1	.0	.07	150.0	.0	1.0	.9	0.	0.	234.	0.	0.	1.42
N205P2.008	.2	.0	35.0	.0	.06	150.0	-11.0	1.0	.6	0.	0.	215.	0.	0.	1.05
N205P2.007	.3	.0	33.1	.0	.07	150.0	-22.0	1.0	.7	0.	0.	204.	0.	0.	1.11
N205P2.006	.3	.0	35.4	.0	.04	150.0	-25.0	1.0	.8	0.	0.	218.	0.	0.	.76
N205P2.005	.2	.0	32.8	.0	.03	150.0	-28.0	1.0	.6	0.	0.	202.	0.	0.	.51
N205P2.004	.1	.0	.0	.0	.00	150.0	-44.0	1.0	.4	0.	0.	0.	0.	0.	.27

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205P3.009	.4	.0	36.2	.0	.13	150.0	.0	1.0	1.0	0.	0.	223.	0.	0.	2.15
N205P3.008	.3	.0	31.1	.0	.08	150.0	-11.0	1.0	.8	0.	0.	192.	0.	0.	1.34
N205P3.007	.2	.0	34.7	.0	.04	150.0	-22.0	1.0	.6	0.	0.	214.	0.	0.	.68
N205P3.006	.2	.0	37.0	.0	.04	150.0	-25.0	1.0	.6	0.	0.	228.	0.	0.	.74
N205P3.005	.2	.0	38.0	.0	.03	150.0	-28.0	1.0	.6	0.	0.	234.	0.	0.	.49
N205P3.004	.1	.0	.0	.0	.02	150.0	-44.0	1.0	.3	0.	0.	0.	0.	0.	.41
N205P4.009	.3	.0	31.0	.0	.08	150.0	.0	1.0	.8	0.	0.	191.	0.	0.	1.46
N205P4.008	.2	.0	29.2	.0	.07	150.0	-11.0	1.0	.7	0.	0.	180.	0.	0.	1.24
N205P4.007	.3	.0	28.7	.0	.06	150.0	-22.0	1.0	.7	0.	0.	176.	0.	0.	.96
N205P4.006	.3	.0	30.4	.0	.03	150.0	-25.0	1.0	.7	0.	0.	187.	0.	0.	.73
N205P4.005	.2	.0	28.4	.0	.04	150.0	-28.0	1.0	.6	0.	0.	175.	0.	0.	.78
N205P4.004	.1	.0	.0	.0	-.04	150.0	-44.0	1.0	.3	0.	0.	0.	0.	0.	.04
N205P5.009	.3	.0	36.2	.0	.05	150.0	.0	1.0	.8	0.	0.	223.	0.	0.	1.08
N205P5.008	.3	.0	34.1	.0	.07	150.0	-11.0	1.0	.8	0.	0.	210.	0.	0.	1.32
N205P5.007	.3	.0	29.5	.0	.08	150.0	-22.0	1.0	.7	0.	0.	182.	0.	0.	1.30
N205P5.006	.2	.0	31.6	.0	.05	150.0	-25.0	1.0	.6	0.	0.	195.	0.	0.	.80
N205P5.005	.2	.0	.0	.0	.04	150.0	-28.0	1.0	.5	0.	0.	0.	0.	0.	.74
N205P5.004	.2	.0	.0	.0	.07	150.0	-44.0	1.0	.5	0.	0.	0.	0.	0.	1.12
N205Q1.009	.3	.0	37.0	.0	.06	150.0	.0	5.0	.8	0.	0.	228.	0.	0.	1.07
N205Q1.008	.3	.0	33.2	.0	.10	150.0	-11.0	5.0	.8	0.	0.	205.	0.	0.	1.64
N205Q1.007	.3	.0	36.4	.0	.05	150.0	-22.0	5.0	.7	0.	0.	224.	0.	0.	.80
N205Q1.006	.2	.0	46.9	.0	.06	150.0	-25.0	5.0	.6	0.	0.	289.	0.	0.	.95
N205Q1.005	.2	.0	36.6	.0	.05	150.0	-28.0	5.0	.6	0.	0.	225.	0.	0.	.81
N205Q1.004	.1	.0	.0	.0	.01	150.0	-44.0	5.0	.2	0.	0.	0.	0.	0.	.23
N205Q2.009	.3	.0	25.5	.0	.07	150.0	.0	5.0	.7	0.	0.	157.	0.	0.	1.13
N205Q2.008	.3	.0	35.7	.0	.03	150.0	-11.0	5.0	.7	0.	0.	220.	0.	0.	.75
N205Q2.007	.3	.0	31.7	.0	.03	150.0	-22.0	5.0	.7	0.	0.	195.	0.	0.	.57
N205Q2.006	.3	.0	31.6	.0	.02	150.0	-25.0	5.0	.8	0.	0.	195.	0.	0.	.42
N205Q2.005	.2	.0	30.8	.0	.00	150.0	-28.0	5.0	.6	0.	0.	189.	0.	0.	.32
N205Q2.004	.3	.0	31.6	.0	.05	150.0	-44.0	5.0	.7	0.	0.	195.	0.	0.	.78
N205Q3.009	.3	.0	33.6	.0	.08	150.0	.0	5.0	.7	0.	0.	207.	0.	0.	1.37
N205Q3.008	.3	.0	31.9	.0	.08	150.0	-11.0	5.0	.7	0.	0.	197.	0.	0.	1.34
N205Q3.007	.3	.0	28.6	.0	.08	150.0	-22.0	5.0	.7	0.	0.	176.	0.	0.	1.37
N205Q3.006	.2	.0	28.6	.0	.06	150.0	-25.0	5.0	.6	0.	0.	176.	0.	0.	.97
N205Q3.005	.2	.0	54.1	.0	.05	150.0	-28.0	5.0	.6	0.	0.	333.	0.	0.	.82
N205Q3.004	.1	.0	.0	.0	.01	150.0	-44.0	5.0	.3	0.	0.	0.	0.	0.	.26
N205Q4.009	.3	.0	33.6	.0	.09	150.0	.0	5.0	.8	0.	0.	207.	0.	0.	1.47
N205Q4.008	.2	.0	31.4	.0	.08	150.0	-11.0	5.0	.7	0.	0.	193.	0.	0.	1.41
N205Q4.007	.1	.0	.0	.0	.01	150.0	-22.0	5.0	.4	0.	0.	0.	0.	0.	.32
N205Q4.006	.2	.0	.0	.0	.02	150.0	-25.0	5.0	.5	0.	0.	0.	0.	0.	.41
N205Q4.005	.2	.0	.0	.0	.02	150.0	-28.0	5.0	.5	0.	0.	0.	0.	0.	.47
N205Q4.004	.1	.0	.0	.0	.01	150.0	-44.0	5.0	.2	0.	0.	0.	0.	0.	.25

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205Q5.009	.2	.0	24.3	.0	.05	150.0	.0	5.0	.6	0.	0.	150.	0.	0.	1.00
N205Q5.008	.3	.0	32.7	.0	.08	150.0	-11.0	5.0	.8	0.	0.	201.	0.	0.	1.29
N205Q5.007	.3	.0	32.7	.0	.04	150.0	-22.0	5.0	.7	0.	0.	201.	0.	0.	.75
N205Q5.006	.3	.0	32.7	.0	.03	150.0	-25.0	5.0	.8	0.	0.	201.	0.	0.	.55
N205Q5.005	.2	.0	.0	.0	.00	150.0	-28.0	5.0	.5	0.	0.	0.	0.	0.	.23
N205Q5.004	.1	.0	.0	.0	-.01	150.0	-44.0	5.0	.2	0.	0.	0.	0.	0.	.16
N205R1.009	.2	.0	31.8	.0	.02	150.0	.0	11.0	.6	0.	0.	196.	0.	0.	.67
N205R1.008	.2	.0	33.4	.0	.02	150.0	-11.0	11.0	.6	0.	0.	206.	0.	0.	.54
N205R1.007	.2	.0	.0	.0	.01	150.0	-22.0	11.0	.5	0.	0.	0.	0.	0.	.40
N205R1.006	.3	.0	31.0	.0	.01	150.0	-25.0	11.0	.7	0.	0.	191.	0.	0.	.32
N205R1.005	.2	.0	.0	.0	-.01	150.0	-28.0	11.0	.4	0.	0.	0.	0.	0.	.17
N205R1.004	.1	.0	.0	.0	-.01	150.0	-44.0	11.0	.4	0.	0.	0.	0.	0.	.14
N205R2.009	.3	.0	26.0	.0	.05	150.0	.0	11.0	.7	0.	0.	160.	0.	0.	.81
N205R2.008	.3	.0	27.9	.0	.06	150.0	-11.0	11.0	.7	0.	0.	172.	0.	0.	.98
N205R2.007	.2	.0	.0	.0	.00	150.0	-22.0	11.0	.4	0.	0.	0.	0.	0.	.31
N205R2.006	.2	.0	.0	.0	.03	150.0	-25.0	11.0	.5	0.	0.	0.	0.	0.	.51
N205R2.005	.2	.0	.0	.0	.01	150.0	-28.0	11.0	.4	0.	0.	0.	0.	0.	.34
N205R2.004	.1	.0	.0	.0	-.02	150.0	-44.0	11.0	.3	0.	0.	0.	0.	0.	.08
N205R3.009	.2	.0	25.1	.0	.02	150.0	.0	11.0	.6	0.	0.	155.	0.	0.	.63
N205R3.008	.3	.0	31.1	.0	.05	150.0	-11.0	11.0	.8	0.	0.	192.	0.	0.	1.06
N205R3.007	.2	.0	39.9	.0	.00	150.0	-22.0	11.0	.6	0.	0.	245.	0.	0.	.20
N205R3.006	.2	.0	.0	.0	.01	150.0	-25.0	11.0	.5	0.	0.	0.	0.	0.	.28
N205R3.005	.2	.0	.0	.0	.01	150.0	-28.0	11.0	.4	0.	0.	0.	0.	0.	.31
N205R3.004	.1	.0	.0	.0	.00	150.0	-44.0	11.0	.3	0.	0.	0.	0.	0.	.19
N205R4.009	.2	.0	28.0	.0	.05	150.0	.0	11.0	.6	0.	0.	172.	0.	0.	.93
N205R4.008	.3	.0	22.4	.0	.07	150.0	-11.0	11.0	.7	0.	0.	138.	0.	0.	1.23
N205R4.007	.3	.0	32.4	.0	.03	150.0	-22.0	11.0	.7	0.	0.	199.	0.	0.	.69
N205R4.006	.3	.0	32.3	.0	.02	150.0	-25.0	11.0	.7	0.	0.	199.	0.	0.	.42
N205R4.005	.2	.0	40.4	.0	.02	150.0	-28.0	11.0	.6	0.	0.	249.	0.	0.	.39
N205R4.004	.1	.0	.0	.0	.01	150.0	-44.0	11.0	.3	0.	0.	0.	0.	0.	.12
N205R5.009	.3	.0	30.9	.0	.06	150.0	.0	11.0	.7	0.	0.	190.	0.	0.	1.00
N205R5.008	.2	.0	30.5	.0	.05	150.0	-11.0	11.0	.6	0.	0.	188.	0.	0.	.89
N205R5.007	.2	.0	22.8	.0	.03	150.0	-22.0	11.0	.6	0.	0.	141.	0.	0.	.46
N205R5.006	.3	.0	22.9	.0	.04	150.0	-25.0	11.0	.7	0.	0.	141.	0.	0.	.67
N205R5.005	.3	.0	23.0	.0	.03	150.0	-28.0	11.0	.7	0.	0.	141.	0.	0.	.53
N205R5.004	.1	.0	.0	.0	.01	150.0	-44.0	11.0	.3	0.	0.	0.	0.	0.	.38
N205S1.009	.3	.0	34.9	.0	.03	150.0	.0	17.0	.8	0.	0.	215.	0.	0.	.49
N205S1.008	.2	.0	.0	.0	.01	150.0	-11.0	17.0	.5	0.	0.	0.	0.	0.	.37
N205S1.007	.1	.0	.0	.0	-.02	150.0	-22.0	17.0	.4	0.	0.	0.	0.	0.	.09
N205S1.006	.2	.0	.0	.0	.00	150.0	-25.0	17.0	.5	0.	0.	0.	0.	0.	.08
N205S1.005	.2	.0	.0	.0	.00	150.0	-28.0	17.0	.5	0.	0.	0.	0.	0.	.03
N205S1.004	.1	.0	.0	.0	.00	150.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.10

FALCON 2: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N205S2.009	.2	.0	37.9	.0	.04	150.0	.0	17.0	.7	0.	0.	234.	0.	0.	.71
N205S2.008	.2	.0	28.5	.0	.03	150.0	-11.0	17.0	.6	0.	0.	175.	0.	0.	.57
N205S2.007	.2	.0	.0	.0	.04	150.0	-22.0	17.0	.5	0.	0.	0.	0.	0.	.59
N205S2.006	.2	.0	.0	.0	.02	150.0	-25.0	17.0	.5	0.	0.	0.	0.	0.	.37
N205S2.005	.1	.0	.0	.0	.03	150.0	-28.0	17.0	.4	0.	0.	0.	0.	0.	.44
N205S2.004	.1	.0	.0	.0	.01	150.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.39
N205S3.009	.3	.0	35.7	.0	.06	150.0	.0	17.0	.9	0.	0.	220.	0.	0.	.97
N205S3.008	.3	.0	37.1	.0	.01	150.0	-11.0	17.0	.7	0.	0.	229.	0.	0.	.25
N205S3.007	.2	.0	.0	.0	.02	150.0	-22.0	17.0	.5	0.	0.	0.	0.	0.	.46
N205S3.006	.2	.0	17.3	.0	.02	150.0	-25.0	17.0	.6	0.	0.	106.	0.	0.	.37
N205S3.005	.2	.0	.0	.0	.01	150.0	-28.0	17.0	.4	0.	0.	0.	0.	0.	.29
N205S3.004	.1	.0	.0	.0	-.01	150.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.09
N205S4.009	.3	.0	32.1	.0	.06	150.0	.0	17.0	.7	0.	0.	198.	0.	0.	1.01
N205S4.008	.2	.0	33.7	.0	.03	150.0	-11.0	17.0	.7	0.	0.	207.	0.	0.	.49
N205S4.007	.2	.0	43.5	.0	.02	150.0	-22.0	17.0	.6	0.	0.	268.	0.	0.	.35
N205S4.006	.2	.0	.0	.0	.01	150.0	-25.0	17.0	.5	0.	0.	0.	0.	0.	.11
N205S4.005	.1	.0	.0	.0	.01	150.0	-28.0	17.0	.3	0.	0.	0.	0.	0.	.35
N205S4.004	.1	.0	.0	.0	.00	150.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.18
N205S5.009	.3	.0	27.9	.0	.04	150.0	.0	17.0	.8	0.	0.	172.	0.	0.	.75
N205S5.008	.3	.0	27.9	.0	.04	150.0	-11.0	17.0	.8	0.	0.	172.	0.	0.	.65
N205S5.007	.2	.0	28.7	.0	.01	150.0	-22.0	17.0	.6	0.	0.	177.	0.	0.	.22
N205S5.006	.2	.0	27.4	.0	.01	150.0	-25.0	17.0	.6	0.	0.	169.	0.	0.	.14
N205S5.005	.2	.0	28.7	.0	.01	150.0	-28.0	17.0	.6	0.	0.	177.	0.	0.	.34
N205S5.004	.1	.0	.0	.0	.00	150.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.06

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210A1.004	.1	.0	.0	.0	-.02	-62.0	40.0	2.0	.2	0.	0.	0.	0.	0.	.03
N210A1.005	1.1	14.9	14.9	14.9	.05	-62.0	30.0	2.0	2.9	0.	0.	130.	0.	0.	1.25
N210A1.006	15.9	2.2	11.9	53.4	1.99	-62.0	20.0	2.0	33.9	19.	23.	103.	250.	355.	41.45
N210A1.007	19.3	2.8	10.4	73.3	3.03	-62.0	10.0	2.0	39.2	24.	24.	90.	328.	479.	63.00
N210A1.008	18.4	2.1	9.5	74.2	2.95	-62.0	.0	2.0	37.9	18.	31.	83.	416.	597.	62.26
N210A1.009	16.7	2.3	11.3	82.4	2.78	-62.0	-10.0	2.0	35.1	20.	21.	98.	278.	600.	59.03
N210A1.010	17.7	2.5	9.7	58.9	1.78	-62.0	-20.0	2.0	36.7	22.	49.	85.	210.	275.	37.17
N210A2.004	.2	.0	.0	.0	.02	-62.0	40.0	2.0	.5	0.	0.	0.	0.	0.	.41
N210A2.005	1.0	.0	9.4	.0	.07	-62.0	30.0	2.0	2.6	0.	0.	82.	0.	0.	1.64
N210A2.006	16.8	2.4	10.9	52.0	2.22	-62.0	20.0	2.0	35.3	35.	36.	95.	226.	380.	46.23
N210A2.007	17.1	1.9	8.9	83.1	3.12	-62.0	10.0	2.0	35.8	17.	31.	78.	432.	684.	65.27
N210A2.008	18.9	1.3	8.3	89.0	3.03	-62.0	.0	2.0	38.7	17.	30.	72.	313.	550.	63.66
N210A2.009	15.5	1.6	11.8	78.2	2.71	-62.0	-10.0	2.0	33.2	15.	25.	102.	317.	526.	57.77
N210A2.010	15.8	4.5	8.3	44.7	1.88	-62.0	-20.0	2.0	33.7	41.	42.	72.	274.	360.	39.24
N210A3.004	.5	.0	14.9	.0	.00	-62.0	40.0	2.0	1.3	0.	0.	130.	0.	0.	.24
N210A3.005	1.1	14.5	16.1	16.2	.02	-62.0	30.0	2.0	2.9	0.	0.	141.	0.	0.	.80
N210A3.006	14.3	3.0	9.6	44.3	2.05	-62.0	20.0	2.0	31.2	26.	33.	84.	206.	355.	42.44
N210A3.007	16.4	2.3	8.4	78.3	3.11	-62.0	10.0	2.0	34.6	20.	21.	73.	355.	636.	65.30
N210A3.008	20.1	2.4	10.2	90.2	2.89	-62.0	.0	2.0	40.4	22.	26.	89.	346.	540.	60.53
N210A3.009	16.3	2.3	13.9	83.6	2.99	-62.0	-10.0	2.0	34.5	23.	25.	121.	342.	594.	62.58
N210A3.010	18.3	3.4	11.3	53.1	1.80	-62.0	-20.0	2.0	37.8	33.	41.	99.	207.	243.	37.31
N210A4.004	.3	.0	28.7	.0	.02	-62.0	40.0	2.0	.7	0.	0.	250.	0.	0.	.45
N210A4.005	1.3	14.3	14.4	17.4	.05	-62.0	30.0	2.0	3.5	0.	0.	125.	0.	0.	1.32
N210A4.006	16.4	3.9	12.2	49.1	2.22	-62.0	20.0	2.0	34.6	34.	41.	106.	284.	300.	46.29
N210A4.007	19.5	2.4	8.7	89.0	3.52	-62.0	10.0	2.0	39.6	21.	26.	76.	402.	598.	73.17
N210A4.008	20.9	1.9	9.5	83.8	3.33	-62.0	.0	2.0	41.7	17.	23.	83.	383.	537.	69.48
N210A4.009	16.8	1.9	8.0	87.3	2.93	-62.0	-10.0	2.0	35.4	17.	22.	69.	266.	577.	61.31
N210A4.010	20.4	2.4	10.2	60.2	2.21	-62.0	-20.0	2.0	40.9	22.	22.	89.	230.	368.	44.89
N210A5.004	.3	.0	16.1	.0	-.01	-62.0	40.0	2.0	.7	0.	0.	141.	0.	0.	.11
N210A5.005	.9	.0	19.9	.0	.04	-62.0	30.0	2.0	2.5	0.	0.	174.	0.	0.	1.08
N210A5.006	17.3	3.1	12.9	49.4	2.39	-62.0	20.0	2.0	36.1	36.	39.	113.	269.	323.	49.18
N210A5.007	19.3	2.1	10.3	72.8	3.07	-62.0	10.0	2.0	39.3	18.	19.	90.	397.	523.	63.74
N210A5.008	19.8	1.6	9.8	90.5	3.29	-62.0	.0	2.0	40.1	14.	20.	86.	391.	626.	68.33
N210A5.009	16.8	2.3	9.7	85.5	2.63	-62.0	-10.0	2.0	35.3	24.	25.	84.	323.	597.	56.11
N210A5.010	17.3	3.8	9.6	52.8	2.09	-62.0	-20.0	2.0	36.1	40.	50.	84.	232.	284.	42.87
N210B1.004	.4	.0	13.6	.0	.04	-32.0	40.0	1.0	1.2	0.	0.	118.	0.	0.	.95
N210B1.005	1.2	26.1	26.1	26.1	.07	-32.0	30.0	1.0	3.2	0.	0.	227.	0.	0.	1.64
N210B1.006	14.3	2.9	8.5	80.1	1.57	-32.0	20.0	1.0	31.1	29.	36.	74.	222.	224.	33.06
N210B1.007	22.5	2.1	5.2	48.1	1.64	-32.0	10.0	1.0	44.0	22.	23.	45.	145.	349.	33.84
N210B1.008	21.9	1.9	9.4	85.7	2.86	-32.0	.0	1.0	43.1	17.	28.	82.	323.	739.	60.18
N210B1.009	22.9	1.0	8.6	77.4	2.26	-32.0	-10.0	1.0	44.5	24.	25.	75.	241.	549.	45.57
N210B1.010	21.7	3.0	9.1	86.2	2.03	-32.0	-20.0	1.0	42.9	26.	29.	80.	288.	662.	42.01

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210B2.004	.4	.0	33.0	.0	.04	-32.0	40.0	1.0	1.1	0.	0.	288.	0.	0.	1.02
N210B2.005	1.0	17.6	17.6	17.6	.07	-32.0	30.0	1.0	2.8	0.	0.	153.	0.	0.	1.71
N210B2.006	20.4	1.6	10.1	63.8	2.02	-32.0	20.0	1.0	40.9	15.	16.	88.	173.	260.	41.73
N210B2.007	24.4	1.4	9.9	54.4	2.14	-32.0	10.0	1.0	46.6	12.	13.	86.	144.	308.	41.82
N210B2.008	20.4	1.2	10.0	85.2	3.00	-32.0	.0	1.0	40.9	11.	12.	87.	345.	659.	62.53
N210B2.009	28.4	1.7	8.8	88.2	3.03	-32.0	-10.0	1.0	51.8	15.	16.	77.	299.	624.	59.25
N210B2.010	22.0	2.7	10.5	90.2	2.37	-32.0	-20.0	1.0	43.2	25.	31.	91.	214.	724.	47.58
N210B3.004	.2	.0	.0	.0	-.02	-32.0	40.0	1.0	.4	0.	0.	0.	0.	0.	.14
N210B3.005	.8	.0	14.5	.0	.07	-32.0	30.0	1.0	2.1	0.	0.	127.	0.	0.	1.76
N210B3.006	21.3	2.1	9.8	66.0	1.98	-32.0	20.0	1.0	42.3	24.	25.	85.	165.	256.	40.14
N210B3.007	26.4	1.2	8.6	66.2	1.63	-32.0	10.0	1.0	49.3	11.	19.	75.	157.	400.	34.38
N210B3.008	21.5	2.0	9.1	86.8	3.04	-32.0	.0	1.0	42.6	23.	24.	79.	377.	626.	62.87
N210B3.009	24.8	.8	6.3	64.1	2.48	-32.0	-10.0	1.0	47.1	19.	21.	55.	444.	556.	50.00
N210B3.010	19.8	3.1	7.4	81.6	2.29	-32.0	-20.0	1.0	40.0	28.	28.	65.	384.	694.	46.69
N210B4.004	.4	.0	15.2	.0	.00	-32.0	40.0	1.0	1.0	0.	0.	133.	0.	0.	.42
N210B4.005	1.1	15.2	15.2	15.3	.07	-32.0	30.0	1.0	3.0	0.	0.	133.	0.	0.	1.74
N210B4.006	21.6	1.2	9.9	81.6	1.99	-32.0	20.0	1.0	42.7	10.	25.	86.	220.	405.	40.50
N210B4.007	32.5	2.1	9.5	66.9	2.68	-32.0	10.0	1.0	56.5	18.	19.	83.	213.	455.	51.92
N210B4.008	24.9	1.0	8.7	91.3	3.12	-32.0	.0	1.0	47.3	10.	22.	76.	290.	607.	64.03
N210B4.009	36.2	2.8	9.4	89.9	2.10	-32.0	-10.0	1.0	60.5	25.	25.	82.	288.	649.	42.16
N210B4.010	22.8	2.1	9.9	88.0	2.69	-32.0	-20.0	1.0	44.4	27.	32.	86.	283.	744.	54.67
N210B5.004	.6	.0	14.9	.0	.03	-32.0	40.0	1.0	1.7	0.	0.	130.	0.	0.	.76
N210B5.005	1.0	14.2	14.2	14.3	.09	-32.0	30.0	1.0	2.7	0.	0.	124.	0.	0.	2.14
N210B5.006	14.8	2.5	9.9	61.2	1.96	-32.0	20.0	1.0	32.0	23.	26.	86.	230.	239.	41.11
N210B5.007	23.7	1.5	9.3	69.5	2.48	-32.0	10.0	1.0	45.6	15.	16.	81.	186.	605.	48.86
N210B5.008	21.1	1.1	9.3	68.8	2.72	-32.0	.0	1.0	42.0	10.	10.	81.	371.	568.	58.42
N210B5.009	23.7	.5	8.5	84.8	1.69	-32.0	-10.0	1.0	45.6	11.	11.	74.	605.	670.	34.50
N210B5.010	21.4	3.2	8.5	69.6	2.15	-32.0	-20.0	1.0	42.4	30.	32.	74.	258.	550.	43.52
N210C1.004	.6	.0	16.9	.0	.04	-2.0	40.0	1.0	1.5	0.	0.	147.	0.	0.	1.22
N210C1.005	.9	.0	18.5	.0	.06	-2.0	30.0	1.0	2.4	0.	0.	161.	0.	0.	1.74
N210C1.006	10.6	3.0	8.5	34.3	.65	-2.0	20.0	1.0	24.3	27.	66.	74.	106.	116.	14.41
N210C1.007	10.8	6.0	10.9	34.8	.75	-2.0	10.0	1.0	24.6	67.	69.	95.	140.	142.	16.77
N210C1.008	8.9	5.5	9.5	94.9	.69	-2.0	.0	1.0	20.8	72.	73.	83.	119.	125.	15.54
N210C1.009	9.1	6.0	9.5	48.5	.64	-2.0	-10.0	1.0	21.4	79.	79.	83.	151.	198.	14.50
N210C1.010	4.0	7.1	18.8	41.2	.70	-2.0	-20.0	1.0	10.1	62.	163.	164.	166.	198.	16.06
N210C2.004	.6	.0	15.8	.0	.01	-2.0	40.0	1.0	1.6	0.	0.	138.	0.	0.	.91
N210C2.005	.8	.0	15.9	.0	.09	-2.0	30.0	1.0	2.2	0.	0.	138.	0.	0.	2.38
N210C2.006	7.9	5.7	6.8	40.9	.61	-2.0	20.0	1.0	18.9	55.	56.	59.	85.	134.	13.85
N210C2.007	8.0	2.5	13.0	47.0	.69	-2.0	10.0	1.0	19.1	23.	62.	114.	119.	229.	15.72
N210C2.008	13.3	3.0	11.9	38.4	.82	-2.0	.0	1.0	29.4	56.	58.	104.	110.	230.	18.13
N210C2.009	8.7	5.5	11.5	42.5	.54	-2.0	-10.0	1.0	20.5	89.	91.	100.	105.	106.	12.23
N210C2.010	7.2	10.8	11.4	41.3	.39	-2.0	-20.0	1.0	17.2	95.	96.	100.	103.	274.	9.47

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210C3.004	.4	.0	20.0	.0	.06	-2.0	40.0	1.0	1.0	0.	0.	174.	0.	0.	1.59
N210C3.005	1.0	23.2	23.2	23.2	.12	-2.0	30.0	1.0	2.7	0.	0.	202.	0.	0.	2.74
N210C3.006	12.3	3.2	9.5	21.4	.83	-2.0	20.0	1.0	27.5	28.	28.	82.	106.	146.	18.11
N210C3.007	7.6	3.8	11.1	21.9	.66	-2.0	10.0	1.0	18.1	33.	36.	97.	128.	138.	14.94
N210C3.008	12.8	4.9	11.7	62.0	.82	-2.0	.0	1.0	28.5	47.	48.	102.	169.	170.	18.19
N210C3.009	9.6	4.7	10.3	52.8	.64	-2.0	-10.0	1.0	22.4	56.	58.	90.	102.	297.	14.62
N210C3.010	13.1	8.5	10.8	46.7	.71	-2.0	-20.0	1.0	29.0	91.	92.	94.	162.	293.	16.35
N210C4.004	.7	.0	25.5	.0	.05	-2.0	40.0	1.0	2.0	0.	0.	223.	0.	0.	1.42
N210C4.005	.9	.0	25.4	.0	.11	-2.0	30.0	1.0	2.3	0.	0.	222.	0.	0.	2.58
N210C4.006	9.1	4.4	8.7	13.6	.72	-2.0	20.0	1.0	21.2	39.	40.	76.	88.	117.	15.81
N210C4.007	7.7	3.2	7.6	54.0	.48	-2.0	10.0	1.0	18.4	62.	63.	66.	94.	109.	11.09
N210C4.008	8.9	3.5	8.5	48.7	.59	-2.0	.0	1.0	21.0	65.	68.	74.	104.	275.	13.44
N210C4.009	6.4	8.4	10.2	47.7	.45	-2.0	-10.0	1.0	15.5	75.	86.	89.	97.	414.	10.45
N210C4.010	5.6	7.9	16.0	40.3	.82	-2.0	-20.0	1.0	13.9	129.	132.	139.	176.	302.	18.81
N210C5.004	.5	.0	18.5	.0	.02	-2.0	40.0	1.0	1.3	0.	0.	161.	0.	0.	.79
N210C5.005	.7	.0	16.7	.0	.08	-2.0	30.0	1.0	1.9	0.	0.	145.	0.	0.	1.79
N210C5.006	9.7	5.1	10.2	24.5	.71	-2.0	20.0	1.0	22.5	45.	45.	89.	100.	207.	15.74
N210C5.007	6.1	4.6	11.0	28.9	.50	-2.0	10.0	1.0	15.0	65.	91.	96.	98.	204.	11.47
N210C5.008	10.1	3.1	10.5	68.5	.66	-2.0	.0	1.0	23.4	28.	88.	92.	171.	240.	14.92
N210C5.009	8.9	6.6	10.7	35.9	.51	-2.0	-10.0	1.0	21.0	60.	92.	94.	107.	133.	11.75
N210C5.010	7.6	10.0	11.4	35.1	.38	-2.0	-20.0	1.0	18.3	90.	91.	99.	107.	133.	9.45
N210D1.004	.2	.0	.0	.0	.01	50.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.41
N210D1.005	.1	.0	.0	.0	.00	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.22
N210D1.006	.2	.0	26.2	.0	-.01	50.0	56.0	1.0	.6	0.	0.	228.	0.	0.	.10
N210D1.007	.5	.0	10.4	.0	.03	50.0	44.0	1.0	1.3	0.	0.	91.	0.	0.	.90
N210D1.008	.5	.0	10.2	.0	.06	50.0	28.0	1.0	1.3	0.	0.	89.	0.	0.	1.40
N210D1.009	.5	.0	25.2	.0	.08	50.0	22.0	1.0	1.4	0.	0.	220.	0.	0.	1.97
N210D1.010	.6	.0	11.8	.0	.16	50.0	.0	1.0	1.5	0.	0.	103.	0.	0.	3.90
N210D2.004	.1	.0	.0	.0	-.02	50.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.09
N210D2.005	.1	.0	.0	.0	-.01	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.13
N210D2.006	.1	.0	.0	.0	.00	50.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.13
N210D2.007	.3	.0	26.4	.0	.01	50.0	44.0	1.0	.7	0.	0.	230.	0.	0.	.43
N210D2.008	.6	.0	23.5	.0	.07	50.0	28.0	1.0	1.7	0.	0.	205.	0.	0.	1.57
N210D2.009	.5	.0	23.2	.0	.10	50.0	22.0	1.0	1.4	0.	0.	202.	0.	0.	2.45
N210D2.010	.6	.0	24.3	.0	.18	50.0	.0	1.0	1.6	0.	0.	212.	0.	0.	4.20
N210D3.004	.1	.0	.0	.0	.00	50.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.26
N210D3.005	.1	.0	.0	.0	.01	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.36
N210D3.006	.2	.0	.0	.0	.01	50.0	56.0	1.0	.5	0.	0.	0.	0.	0.	.22
N210D3.007	.4	.0	21.5	.0	.01	50.0	44.0	1.0	1.0	0.	0.	187.	0.	0.	.52
N210D3.008	.6	.0	33.3	.0	.08	50.0	28.0	1.0	1.7	0.	0.	291.	0.	0.	1.96
N210D3.009	1.0	.0	19.3	.0	.09	50.0	22.0	1.0	2.6	0.	0.	168.	0.	0.	2.23
N210D3.010	.6	.0	11.6	.0	.16	50.0	.0	1.0	1.5	0.	0.	101.	0.	0.	3.72

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210D4.004	.1	.0	.0	.0	-.02	50.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.08
N210D4.005	.1	.0	.0	.0	-.03	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.01
N210D4.006	.2	.0	.0	.0	.03	50.0	56.0	1.0	.5	0.	0.	0.	0.	0.	.72
N210D4.007	.3	.0	50.7	.0	-.02	50.0	44.0	1.0	.7	0.	0.	442.	0.	0.	.59
N210D4.008	.6	.0	25.9	.0	.06	50.0	28.0	1.0	1.5	0.	0.	226.	0.	0.	1.47
N210D4.009	.6	.0	27.3	.0	.10	50.0	22.0	1.0	1.5	0.	0.	238.	0.	0.	2.28
N210D4.010	.6	.0	22.8	.0	.18	50.0	.0	1.0	1.5	0.	0.	199.	0.	0.	4.22
N210D5.004	.1	.0	.0	.0	-.01	50.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.19
N210D5.005	.0	.0	.0	.0	-.01	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.06
N210D5.006	.1	.0	.0	.0	.01	50.0	56.0	1.0	.1	0.	0.	0.	0.	0.	.36
N210D5.007	.2	.0	.0	.0	.01	50.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.45
N210D5.008	.5	.0	30.8	.0	.06	50.0	28.0	1.0	1.4	0.	0.	269.	0.	0.	1.37
N210D5.009	.5	.0	23.6	.0	.08	50.0	22.0	1.0	1.3	0.	0.	206.	0.	0.	1.94
N210D5.010	.6	.0	17.1	.0	.13	50.0	.0	1.0	1.7	0.	0.	149.	0.	0.	3.07
N210E1.004	.1	.0	.0	.0	.00	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.20
N210E1.005	.1	.0	.0	.0	-.01	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.07
N210E1.006	.3	.0	18.0	.0	.00	50.0	56.0	5.0	.8	0.	0.	157.	0.	0.	.14
N210E1.007	.3	.0	7.7	.0	-.15	50.0	44.0	5.0	.7	0.	0.	67.	0.	0.	.06
N210E1.008	.8	.0	18.8	.0	.09	50.0	28.0	5.0	2.1	0.	0.	164.	0.	0.	2.25
N210E1.009	1.2	18.2	18.2	18.3	.11	50.0	22.0	5.0	3.1	0.	0.	159.	0.	0.	2.72
N210E1.010	.8	.0	12.0	.0	.16	50.0	.0	5.0	2.2	0.	0.	104.	0.	0.	3.88
N210E2.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.26
N210E2.005	.1	.0	.0	.0	.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.52
N210E2.006	.5	.0	18.7	.0	.03	50.0	56.0	5.0	1.3	0.	0.	163.	0.	0.	.65
N210E2.007	.5	.0	18.7	.0	.01	50.0	44.0	5.0	1.4	0.	0.	163.	0.	0.	.45
N210E2.008	.8	.0	21.5	.0	.14	50.0	28.0	5.0	2.0	0.	0.	187.	0.	0.	3.41
N210E2.009	.7	.0	11.4	.0	.14	50.0	22.0	5.0	1.9	0.	0.	99.	0.	0.	3.35
N210E2.010	.6	.0	25.8	.0	.15	50.0	.0	5.0	1.6	0.	0.	225.	0.	0.	3.66
N210E3.004	.1	.0	.0	.0	-.02	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.12
N210E3.005	.1	.0	.0	.0	-.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.07
N210E3.006	.3	.0	24.0	.0	.00	50.0	56.0	5.0	.9	0.	0.	209.	0.	0.	.38
N210E3.007	.5	.0	10.4	.0	-.07	50.0	44.0	5.0	1.3	0.	0.	91.	0.	0.	.17
N210E3.008	.7	.0	20.0	.0	.09	50.0	28.0	5.0	1.9	0.	0.	174.	0.	0.	2.06
N210E3.009	.8	.0	10.1	.0	.13	50.0	22.0	5.0	2.1	0.	0.	88.	0.	0.	3.02
N210E3.010	.7	.0	14.7	.0	.15	50.0	.0	5.0	1.9	0.	0.	128.	0.	0.	3.50
N210E4.004	.1	.0	.0	.0	-.02	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.04
N210E4.005	.1	.0	.0	.0	-.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.07
N210E4.006	.3	.0	25.5	.0	-.01	50.0	56.0	5.0	.9	0.	0.	222.	0.	0.	.11
N210E4.007	.5	.0	25.6	.0	.02	50.0	44.0	5.0	1.3	0.	0.	223.	0.	0.	.64
N210E4.008	.8	.0	8.6	.0	.06	50.0	28.0	5.0	2.0	0.	0.	75.	0.	0.	1.51
N210E4.009	1.0	8.7	8.7	8.7	.10	50.0	22.0	5.0	2.8	0.	0.	75.	0.	0.	2.29
N210E4.010	.7	.0	22.1	.0	.16	50.0	.0	5.0	1.9	0.	0.	192.	0.	0.	3.83

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210E5.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.31
N210E5.005	.0	.0	.0	.0	-.01	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.07
N210E5.006	.1	.0	.0	.0	.00	50.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.14
N210E5.007	.6	.0	21.2	.0	.07	50.0	44.0	5.0	1.5	0.	0.	185.	0.	0.	1.62
N210E5.008	1.0	10.5	10.5	10.6	.09	50.0	28.0	5.0	2.7	0.	0.	92.	0.	0.	2.27
N210E5.009	.9	.0	8.6	.0	.14	50.0	22.0	5.0	2.3	0.	0.	75.	0.	0.	3.29
N210E5.010	.6	.0	11.9	.0	.19	50.0	.0	5.0	1.7	0.	0.	103.	0.	0.	4.39
N210F1.004	.1	.0	.0	.0	.00	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.21
N210F1.005	.1	.0	.0	.0	.01	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.35
N210F1.006	.2	.0	26.6	.0	.02	50.0	56.0	11.0	.6	0.	0.	232.	0.	0.	.44
N210F1.007	.6	.0	19.3	.0	.00	50.0	44.0	11.0	1.5	0.	0.	168.	0.	0.	.17
N210F1.008	.7	.0	20.4	.0	.08	50.0	28.0	11.0	1.9	0.	0.	178.	0.	0.	1.90
N210F1.009	.6	.0	28.9	.0	.08	50.0	22.0	11.0	1.6	0.	0.	252.	0.	0.	2.00
N210F1.010	.6	.0	19.1	.0	.10	50.0	.0	11.0	1.7	0.	0.	167.	0.	0.	2.55
N210F2.004	.0	.0	.0	.0	-.01	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.04
N210F2.005	.1	.0	.0	.0	-.01	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.00
N210F2.006	.2	.0	.0	.0	-.01	50.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.22
N210F2.007	.4	.0	20.6	.0	.00	50.0	44.0	11.0	1.1	0.	0.	180.	0.	0.	.21
N210F2.008	.6	.0	12.3	.0	.06	50.0	28.0	11.0	1.6	0.	0.	107.	0.	0.	1.48
N210F2.009	.7	.0	7.3	.0	.09	50.0	22.0	11.0	1.8	0.	0.	64.	0.	0.	2.26
N210F2.010	.6	.0	13.8	.0	.13	50.0	.0	11.0	1.7	0.	0.	120.	0.	0.	3.08
N210F3.004	.1	.0	.0	.0	.00	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.26
N210F3.005	.1	.0	.0	.0	-.01	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.14
N210F3.006	.1	.0	.0	.0	-.01	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.08
N210F3.007	.4	.0	34.6	.0	.00	50.0	44.0	11.0	1.2	0.	0.	301.	0.	0.	.19
N210F3.008	.8	.0	18.6	.0	.05	50.0	28.0	11.0	2.1	0.	0.	162.	0.	0.	1.29
N210F3.009	.9	.0	18.8	.0	.08	50.0	22.0	11.0	2.3	0.	0.	164.	0.	0.	2.08
N210F3.010	.7	.0	15.8	.0	.15	50.0	.0	11.0	1.8	0.	0.	137.	0.	0.	3.62
N210F4.004	.0	.0	.0	.0	-.02	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.08
N210F4.005	.0	.0	.0	.0	-.01	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.01
N210F4.006	.1	.0	.0	.0	.00	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.08
N210F4.007	.3	.0	29.1	.0	.00	50.0	44.0	11.0	.8	0.	0.	254.	0.	0.	.25
N210F4.008	.9	.0	10.4	.0	.03	50.0	28.0	11.0	2.3	0.	0.	91.	0.	0.	1.03
N210F4.009	.9	.0	13.6	.0	.08	50.0	22.0	11.0	2.3	0.	0.	118.	0.	0.	1.87
N210F4.010	.8	.0	12.9	.0	.12	50.0	.0	11.0	2.0	0.	0.	113.	0.	0.	2.94
N210F5.004	.0	.0	.0	.0	-.02	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.08
N210F5.005	.0	.0	.0	.0	.00	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.13
N210F5.006	.2	.0	.0	.0	.00	50.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.20
N210F5.007	.3	.0	17.2	.0	-.01	50.0	44.0	11.0	.9	0.	0.	150.	0.	0.	.17
N210F5.008	.7	.0	13.2	.0	.07	50.0	28.0	11.0	1.8	0.	0.	115.	0.	0.	1.86
N210F5.009	.7	.0	12.6	.0	.10	50.0	22.0	11.0	2.0	0.	0.	110.	0.	0.	2.35
N210F5.010	.5	.0	19.8	.0	.13	50.0	.0	11.0	1.4	0.	0.	173.	0.	0.	3.11

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210G1.004	.0	.0	.0	.0	-.04	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.03
N210G1.005	.1	.0	.0	.0	-.06	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.00
N210G1.006	.0	.0	.0	.0	-.04	50.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.01
N210G1.007	.2	.0	36.0	.0	.00	50.0	44.0	17.0	.6	0.	0.	314.	0.	0.	.21
N210G1.008	.6	.0	18.5	.0	.02	50.0	28.0	17.0	1.7	0.	0.	161.	0.	0.	.82
N210G1.009	.8	.0	5.4	.0	.11	50.0	22.0	17.0	2.0	0.	0.	47.	0.	0.	2.53
N210G1.010	.8	.0	19.9	.0	.11	50.0	.0	17.0	2.1	0.	0.	174.	0.	0.	2.79
N210G2.004	.1	.0	.0	.0	.00	50.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.13
N210G2.005	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.16
N210G2.006	.0	.0	.0	.0	-.01	50.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.09
N210G2.007	.1	.0	.0	.0	.01	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.24
N210G2.008	.7	.0	14.0	.0	.02	50.0	28.0	17.0	1.9	0.	0.	122.	0.	0.	.61
N210G2.009	.7	.0	19.4	.0	.04	50.0	22.0	17.0	1.8	0.	0.	169.	0.	0.	1.00
N210G2.010	.9	.0	13.4	.0	.05	50.0	.0	17.0	2.4	0.	0.	117.	0.	0.	1.67
N210G3.004	.1	.0	.0	.0	.01	50.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.41
N210G3.005	.1	.0	.0	.0	.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.21
N210G3.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.36
N210G3.007	.4	.0	60.5	.0	-.12	50.0	44.0	17.0	1.2	0.	0.	528.	0.	0.	.98
N210G3.008	.7	.0	28.8	.0	.03	50.0	28.0	17.0	1.8	0.	0.	251.	0.	0.	.73
N210G3.009	.6	.0	10.9	.0	.05	50.0	22.0	17.0	1.7	0.	0.	95.	0.	0.	1.27
N210G3.010	.7	.0	22.9	.0	.12	50.0	.0	17.0	1.8	0.	0.	200.	0.	0.	2.89
N210G4.004	.1	.0	.0	.0	.00	50.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.04
N210G4.005	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.13
N210G4.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.02
N210G4.007	.1	.0	.0	.0	.00	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.09
N210G4.008	.6	.0	28.2	.0	.03	50.0	28.0	17.0	1.7	0.	0.	246.	0.	0.	.87
N210G4.009	.7	.0	13.2	.0	.03	50.0	22.0	17.0	2.0	0.	0.	115.	0.	0.	.96
N210G4.010	.7	.0	29.3	.0	.11	50.0	.0	17.0	1.9	0.	0.	255.	0.	0.	2.65
N210H1.004	.5	.0	11.2	.0	.09	50.0	.0	1.0	1.4	0.	0.	98.	0.	0.	2.36
N210H1.005	.6	.0	24.0	.0	.12	50.0	-22.0	1.0	1.5	0.	0.	209.	0.	0.	2.93
N210H1.006	.6	.0	18.6	.0	.12	50.0	-28.0	1.0	1.5	0.	0.	162.	0.	0.	2.82
N210H1.007	2.3	33.0	33.0	65.9	.40	50.0	-44.0	1.0	5.9	288.	0.	288.	0.	288.	12.52
N210H1.008	.3	.0	27.6	.0	.03	50.0	-56.0	1.0	.8	0.	0.	241.	0.	0.	.72
N210H1.009	.1	.0	.0	.0	.02	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.46
N210H1.010	.1	.0	.0	.0	-.01	50.0	-75.0	1.0	.2	0.	0.	0.	0.	0.	.24
N210H2.004	.6	.0	12.1	.0	.13	50.0	.0	1.0	1.6	0.	0.	106.	0.	0.	3.11
N210H2.005	.6	.0	16.4	.0	.12	50.0	-22.0	1.0	1.5	0.	0.	143.	0.	0.	2.92
N210H2.006	.6	.0	17.4	.0	.10	50.0	-28.0	1.0	1.7	0.	0.	152.	0.	0.	2.26
N210H2.007	.3	.0	10.5	.0	-.04	50.0	-44.0	1.0	.9	0.	0.	92.	0.	0.	.41
N210H2.008	.1	.0	.0	.0	-.01	50.0	-56.0	1.0	.3	0.	0.	0.	0.	0.	.16
N210H2.009	.1	.0	.0	.0	-.01	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.10
N210H2.010	.1	.0	.0	.0	-.02	50.0	-75.0	1.0	.2	0.	0.	0.	0.	0.	.07

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210H3.004	.6	.0	18.6	.0	.13	50.0	.0	1.0	1.7	0.	0.	162.	0.	0.	3.09
N210H3.005	.6	.0	25.5	.0	.11	50.0	-22.0	1.0	1.6	0.	0.	223.	0.	0.	2.65
N210H3.006	.6	.0	16.8	.0	.11	50.0	-28.0	1.0	1.7	0.	0.	147.	0.	0.	2,55
N210H3.007	.5	.0	16.0	.0	.02	50.0	-44.0	1.0	1.2	0.	0.	139.	0.	0.	.69
N210H3.008	.3	.0	27.1	.0	.00	50.0	-56.0	1.0	.9	0.	0.	236.	0.	0.	.36
N210H3.009	.1	.0	.0	.0	.01	50.0	-66.0	1.0	.3	0.	0.	0.	0.	0.	.36
N210H3.010	.1	.0	.0	.0	.01	50.0	-75.0	1.0	.2	0.	0.	0.	0.	0.	.12
N210H4.004	.6	.0	19.5	.0	.16	50.0	.0	1.0	1.5	0.	0.	170.	0.	0.	3.80
N210H4.005	.5	.0	17.6	.0	.09	50.0	-22.0	1.0	1.3	0.	0.	153.	0.	0.	2.15
N210H4.006	.6	.0	28.1	.0	.08	50.0	-28.0	1.0	1.5	0.	0.	245.	0.	0.	1.96
N210H4.007	.4	.0	17.2	.0	.02	50.0	-44.0	1.0	1.1	0.	0.	150.	0.	0.	.70
N210H4.008	.1	.0	.0	.0	.02	50.0	-56.0	1.0	.3	0.	0.	0.	0.	0.	.16
N210H4.009	.1	.0	.0	.0	.02	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.10
N210H4.010	.1	.0	.0	.0	.00	50.0	-75.0	1.0	.3	0.	0.	0.	0.	0.	.20
N210H5.004	.6	.0	16.2	.0	.13	50.0	.0	1.0	1.5	0.	0.	141.	0.	0.	3.16
N210H5.005	.7	.0	17.5	.0	.11	50.0	-22.0	1.0	1.8	0.	0.	152.	0.	0.	2.59
N210H5.006	.6	.0	17.7	.0	.08	50.0	-28.0	1.0	1.7	0.	0.	154.	0.	0.	2.05
N210H5.007	.3	.0	26.1	.0	.01	50.0	-44.0	1.0	.7	0.	0.	227.	0.	0.	.55
N210H5.008	.2	.0	.0	.0	.01	50.0	-56.0	1.0	.4	0.	0.	0.	0.	0.	.31
N210H5.009	.1	.0	.0	.0	.00	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.20
N210H5.010	.1	.0	.0	.0	.00	50.0	-75.0	1.0	.2	0.	0.	0.	0.	0.	.27
N210I1.004	.6	.0	22.1	.0	.13	50.0	.0	5.0	1.5	0.	0.	193.	0.	0.	3.17
N210I1.005	.6	.0	14.1	.0	.09	50.0	-22.0	5.0	1.6	0.	0.	123.	0.	0.	2.12
N210I1.006	.8	.0	14.0	.0	.06	50.0	-28.0	5.0	2.2	0.	0.	122.	0.	0.	1.57
N210I1.007	.2	.0	37.7	.0	.02	50.0	-44.0	5.0	.7	0.	0.	329.	0.	0.	.64
N210I1.008	.3	.0	23.9	.0	.00	50.0	-56.0	5.0	.7	0.	0.	208.	0.	0.	.21
N210I1.009	.1	.0	.0	.0	.02	50.0	-66.0	5.0	.3	0.	0.	0.	0.	0.	.42
N210I1.010	.1	.0	.0	.0	.01	50.0	-75.0	5.0	.2	0.	0.	0.	0.	0.	.32
N210I2.004	.7	.0	26.8	.0	.17	50.0	.0	5.0	1.8	0.	0.	233.	0.	0.	4.06
N210I2.005	.7	.0	28.8	.0	.09	50.0	-22.0	5.0	2.0	0.	0.	251.	0.	0.	2.25
N210I2.006	.8	.0	28.7	.0	.07	50.0	-28.0	5.0	2.1	0.	0.	250.	0.	0.	1.67
N210I2.007	.4	.0	25.3	.0	.02	50.0	-44.0	5.0	1.1	0.	0.	220.	0.	0.	.61
N210I2.008	.1	.0	.0	.0	.00	50.0	-56.0	5.0	.4	0.	0.	0.	0.	0.	.11
N210I2.009	.1	.0	.0	.0	.01	50.0	-66.0	5.0	.3	0.	0.	0.	0.	0.	.37
N210I2.010	.1	.0	.0	.0	.01	50.0	-75.0	5.0	.4	0.	0.	0.	0.	0.	.41
N210I3.004	.7	.0	26.7	.0	.14	50.0	.0	5.0	2.0	0.	0.	233.	0.	0.	3.45
N210I3.005	.7	.0	32.3	.0	.12	50.0	-22.0	5.0	2.0	0.	0.	282.	0.	0.	2.85
N210I3.006	.7	.0	32.3	.0	.07	50.0	-28.0	5.0	1.9	0.	0.	282.	0.	0.	1.79
N210I3.007	.4	.0	33.3	.0	.04	50.0	-44.0	5.0	.9	0.	0.	290.	0.	0.	.97
N210I3.008	.1	.0	.0	.0	.01	50.0	-56.0	5.0	.3	0.	0.	0.	0.	0.	.51
N210I3.009	.1	.0	.0	.0	.00	50.0	-66.0	5.0	.3	0.	0.	0.	0.	0.	.22
N210I3.010	.1	.0	.0	.0	.03	50.0	-75.0	5.0	.4	0.	0.	0.	0.	0.	.64

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210I4.004	.6	.0	12.9	.0	.17	50.0	.0	5.0	1.6	0.	0.	112.	0.	0.	3.90
N210I4.005	.8	.0	11.4	.0	.15	50.0	-22.0	5.0	2.1	0.	0.	99.	0.	0.	3.45
N210I4.006	.7	.0	15.4	.0	.09	50.0	-28.0	5.0	2.0	0.	0.	134.	0.	0.	2.13
N210I4.007	.3	.0	23.4	.0	.01	50.0	-44.0	5.0	.9	0.	0.	204.	0.	0.	.30
N210I4.008	.1	.0	.0	.0	.02	50.0	-56.0	5.0	.4	0.	0.	0.	0.	0.	.37
N210I4.009	.1	.0	.0	.0	.02	50.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.51
N210I4.010	.1	.0	.0	.0	.02	50.0	-75.0	5.0	.2	0.	0.	0.	0.	0.	.47
N210I5.004	.9	.0	15.1	.0	.13	50.0	.0	5.0	2.3	0.	0.	132.	0.	0.	3.21
N210I5.005	.8	.0	16.7	.0	.07	50.0	-22.0	5.0	2.2	0.	0.	145.	0.	0.	1.84
N210I5.006	.6	.0	20.0	.0	.05	50.0	-28.0	5.0	1.6	0.	0.	174.	0.	0.	1.38
N210I5.007	.6	.0	17.1	.0	.02	50.0	-44.0	5.0	1.6	0.	0.	149.	0.	0.	.58
N210I5.008	.5	.0	19.7	.0	.02	50.0	-56.0	5.0	1.2	0.	0.	172.	0.	0.	.54
N210I5.009	.1	.0	.0	.0	-.02	50.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.17
N210I5.010	.2	.0	.0	.0	-.03	50.0	-75.0	5.0	.4	0.	0.	0.	0.	0.	.11
N210J1.004	.7	.0	21.9	.0	.16	50.0	.0	11.0	1.9	0.	0.	191.	0.	0.	3.73
N210J1.005	.6	.0	15.5	.0	.07	50.0	-22.0	11.0	1.5	0.	0.	135.	0.	0.	1.85
N210J1.006	.7	.0	15.7	.0	.05	50.0	-28.0	11.0	1.8	0.	0.	137.	0.	0.	1.27
N210J1.007	.6	.0	29.8	.0	.02	50.0	-44.0	11.0	1.6	0.	0.	260.	0.	0.	.45
N210J1.008	.2	.0	.0	.0	.01	50.0	-56.0	11.0	.4	0.	0.	0.	0.	0.	.34
N210J1.009	.1	.0	.0	.0	.01	50.0	-66.0	11.0	.3	0.	0.	0.	0.	0.	.36
N210J1.010	.1	.0	.0	.0	.02	50.0	-75.0	11.0	.3	0.	0.	0.	0.	0.	.59
N210J2.004	.6	.0	22.2	.0	.11	50.0	.0	11.0	1.7	0.	0.	194.	0.	0.	2.67
N210J2.005	1.0	.0	12.4	.0	.13	50.0	-22.0	11.0	2.6	0.	0.	108.	0.	0.	3.21
N210J2.006	1.1	12.4	12.4	12.4	.11	50.0	-28.0	11.0	3.0	0.	0.	108.	0.	0.	2.52
N210J2.007	.4	.0	16.2	.0	.03	50.0	-44.0	11.0	1.1	0.	0.	141.	0.	0.	.75
N210J2.008	.3	.0	14.7	.0	.03	50.0	-56.0	11.0	.7	0.	0.	128.	0.	0.	.70
N210J2.009	.2	.0	.0	.0	.02	50.0	-66.0	11.0	.4	0.	0.	0.	0.	0.	.41
N210J2.010	.1	.0	.0	.0	.03	50.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.75
N210J3.004	.8	.0	20.9	.0	.15	50.0	.0	11.0	2.0	0.	0.	182.	0.	0.	3.46
N210J3.005	.9	.0	15.2	.0	.07	50.0	-22.0	11.0	2.5	0.	0.	133.	0.	0.	1.76
N210J3.006	.8	.0	20.1	.0	.03	50.0	-28.0	11.0	2.1	0.	0.	175.	0.	0.	1.13
N210J3.007	.7	.0	19.7	.0	.00	50.0	-44.0	11.0	1.8	0.	0.	171.	0.	0.	.33
N210J3.008	.1	.0	.0	.0	-.03	50.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.13
N210J3.009	.1	.0	.0	.0	-.04	50.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.08
N210J3.010	.0	.0	.0	.0	-.05	50.0	-75.0	11.0	.1	0.	0.	0.	0.	0.	.06
N210J4.004	.7	.0	10.9	.0	.11	50.0	.0	11.0	1.8	0.	0.	95.	0.	0.	2.57
N210J4.005	1.0	.0	6.6	.0	.09	50.0	-22.0	11.0	2.6	0.	0.	58.	0.	0.	2.19
N210J4.006	.9	.0	19.1	.0	.08	50.0	-28.0	11.0	2.3	0.	0.	166.	0.	0.	1.93
N210J4.007	.4	.0	16.7	.0	-.01	50.0	-44.0	11.0	1.2	0.	0.	146.	0.	0.	.17
N210J4.008	.1	.0	.0	.0	-.01	50.0	-56.0	11.0	.4	0.	0.	0.	0.	0.	.11
N210J4.009	.0	.0	.0	.0	-.01	50.0	-66.0	11.0	.1	0.	0.	0.	0.	0.	.12
N210J4.010	.1	.0	.0	.0	.01	50.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.29

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210J5.004	1.1	19.1	19.1	19.1	.13	50.0	.0	11.0	2.8	0.	0.	167.	0.	0.	3.11
N210J5.005	.8	.0	17.0	.0	.11	50.0	-22.0	11.0	2.1	0.	0.	149.	0.	0.	2.61
N210J5.006	.8	.0	14.2	.0	.08	50.0	-28.0	11.0	2.2	0.	0.	124.	0.	0.	2.06
N210J5.007	.5	.0	27.5	.0	.02	50.0	-44.0	11.0	1.4	0.	0.	240.	0.	0.	.54
N210J5.008	.2	.0	.0	.0	.02	50.0	-56.0	11.0	.5	0.	0.	0.	0.	0.	.44
N210J5.009	.1	.0	.0	.0	.02	50.0	-66.0	11.0	.3	0.	0.	0.	0.	0.	.59
N210J5.010	.1	.0	.0	.0	.02	50.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.50
N210K1.004	1.0	.0	18.5	.0	.10	50.0	.0	17.0	2.6	0.	0.	161.	0.	0.	2.44
N210K1.005	1.0	18.5	18.5	18.5	.04	50.0	-22.0	17.0	2.7	0.	0.	161.	0.	0.	1.09
N210K1.006	.6	.0	17.7	.0	.02	50.0	-28.0	17.0	1.7	0.	0.	154.	0.	0.	.66
N210K1.007	.0	.0	.0	.0	-.04	50.0	-44.0	17.0	.0	0.	0.	0.	0.	0.	.00
N210K1.008	.0	.0	.0	.0	-.04	50.0	-56.0	17.0	.1	0.	0.	0.	0.	0.	.01
N210K1.009	.1	.0	.0	.0	-.02	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.03
N210K1.010	.0	.0	.0	.0	-.02	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.02
N210K2.004	.9	.0	15.7	.0	.10	50.0	.0	17.0	2.3	0.	0.	137.	0.	0.	2.54
N210K2.005	.6	.0	16.0	.0	.03	50.0	-22.0	17.0	1.6	0.	0.	140.	0.	0.	.86
N210K2.006	.6	.0	16.3	.0	.02	50.0	-28.0	17.0	1.6	0.	0.	142.	0.	0.	.59
N210K2.007	.1	.0	.0	.0	.00	50.0	-44.0	17.0	.3	0.	0.	0.	0.	0.	.21
N210K2.008	.1	.0	.0	.0	.00	50.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.03
N210K2.009	.1	.0	.0	.0	-.02	50.0	-66.0	17.0	.1	0.	0.	0.	0.	0.	.05
N210K2.010	.0	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.04
N210K3.004	.9	.0	18.9	.0	.11	50.0	.0	17.0	2.4	0.	0.	164.	0.	0.	2.62
N210K3.005	.9	.0	13.3	.0	.04	50.0	-22.0	17.0	2.5	0.	0.	116.	0.	0.	1.01
N210K3.006	.6	.0	18.8	.0	.02	50.0	-28.0	17.0	1.7	0.	0.	164.	0.	0.	.61
N210K3.007	.1	.0	.0	.0	-.02	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.03
N210K3.008	.1	.0	.0	.0	-.01	50.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.01
N210K3.009	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.17
N210K3.010	.1	.0	.0	.0	.01	50.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.25
N210K4.004	.7	.0	19.4	.0	.10	50.0	.0	17.0	2.0	0.	0.	169.	0.	0.	2.58
N210K4.005	.6	.0	18.7	.0	.04	50.0	-22.0	17.0	1.7	0.	0.	163.	0.	0.	1.07
N210K4.006	.7	.0	18.4	.0	.02	50.0	-28.0	17.0	2.0	0.	0.	161.	0.	0.	.62
N210K4.007	.1	.0	.0	.0	-.01	50.0	-44.0	17.0	.1	0.	0.	0.	0.	0.	.11
N210K4.008	.1	.0	.0	.0	.00	50.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.12
N210K4.009	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.10
N210K4.010	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.08
N210K5.004	.9	.0	16.5	.0	.11	50.0	.0	17.0	2.3	0.	0.	144.	0.	0.	2.79
N210K5.005	.8	.0	15.9	.0	.03	50.0	-22.0	17.0	2.1	0.	0.	139.	0.	0.	.96
N210K5.006	.6	.0	22.1	.0	.02	50.0	-28.0	17.0	1.6	0.	0.	193.	0.	0.	.66
N210K5.007	.0	.0	.0	.0	-.11	50.0	-44.0	17.0	.1	0.	0.	0.	0.	0.	.06
N210K5.008	.0	.0	.0	.0	-.04	50.0	-56.0	17.0	.0	0.	0.	0.	0.	0.	.01
N210K5.009	.1	.0	.0	.0	-.01	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.02
N210K5.010	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.10

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210L1.004	.1	.0	.0	.0	.01	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.41
N210L1.005	.2	.0	.0	.0	.05	150.0	56.0	1.0	.5	0.	0.	0.	0.	0.	1.14
N210L1.006	.2	.0	.0	.0	.01	150.0	50.0	1.0	.5	0.	0.	0.	0.	0.	.45
N210L1.007	.2	.0	28.5	.0	.01	150.0	44.0	1.0	.6	0.	0.	249.	0.	0.	.50
N210L1.008	.4	.0	15.3	.0	.06	150.0	28.0	1.0	1.0	0.	0.	133.	0.	0.	1.46
N210L1.009	.3	.0	12.5	.0	.07	150.0	22.0	1.0	.9	0.	0.	109.	0.	0.	1.79
N210L1.010	.4	.0	23.0	.0	.10	150.0	.0	1.0	1.0	0.	0.	201.	0.	0.	2.43
N210L2.004	.1	.0	.0	.0	-.01	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.15
N210L2.005	.1	.0	.0	.0	.00	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.13
N210L2.006	.1	.0	.0	.0	.01	150.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.30
N210L2.007	.1	.0	.0	.0	.01	150.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.28
N210L2.008	.3	.0	15.5	.0	.02	150.0	28.0	1.0	.7	0.	0.	135.	0.	0.	.78
N210L2.009	.3	.0	15.4	.0	.03	150.0	22.0	1.0	.8	0.	0.	135.	0.	0.	1.04
N210L2.010	.4	.0	29.1	.0	.11	150.0	.0	1.0	1.0	0.	0.	254.	0.	0.	2.69
N210L3.004	.1	.0	.0	.0	-.03	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.08
N210L3.005	.1	.0	.0	.0	.03	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.76
N210L3.006	.1	.0	.0	.0	.01	150.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.35
N210L3.007	.2	.0	.0	.0	.03	150.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.70
N210L3.008	.3	.0	16.2	.0	.06	150.0	28.0	1.0	.8	0.	0.	141.	0.	0.	1.47
N210L3.009	.2	.0	19.7	.0	.03	150.0	22.0	1.0	.6	0.	0.	172.	0.	0.	1.06
N210L3.010	.3	.0	18.9	.0	.08	150.0	.0	1.0	.9	0.	0.	164.	0.	0.	2.03
N210L4.004	.0	.0	.0	.0	-.04	150.0	75.0	1.0	.0	0.	0.	0.	0.	0.	.06
N210L4.005	.1	.0	.0	.0	.02	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.54
N210L4.006	.1	.0	.0	.0	.01	150.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.31
N210L4.007	.2	.0	.0	.0	.01	150.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.37
N210L4.008	.3	.0	32.5	.0	.04	150.0	28.0	1.0	.7	0.	0.	283.	0.	0.	1.12
N210L4.009	.3	.0	31.8	.0	.03	150.0	22.0	1.0	.7	0.	0.	277.	0.	0.	.84
N210L4.010	.3	.0	24.7	.0	.08	150.0	.0	1.0	.9	0.	0.	216.	0.	0.	2.01
N210L5.004	.1	.0	.0	.0	.01	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.53
N210L5.005	.1	.0	.0	.0	.03	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.65
N210L5.006	.2	.0	19.0	.0	.05	150.0	50.0	1.0	.6	0.	0.	165.	0.	0.	1.25
N210L5.007	.2	.0	.0	.0	.03	150.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.77
N210L5.008	.3	.0	21.2	.0	.04	150.0	28.0	1.0	.8	0.	0.	185.	0.	0.	1.13
N210L5.009	.4	.0	29.7	.0	.09	150.0	22.0	1.0	1.1	0.	0.	259.	0.	0.	2.02
N210L5.010	.5	.0	29.7	.0	.11	150.0	.0	1.0	1.2	0.	0.	259.	0.	0.	2.75
N210M1.004	.1	.0	.0	.0	.00	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.28
N210M1.005	.1	.0	.0	.0	.01	150.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.37
N210M1.006	.2	.0	17.3	.0	.03	150.0	50.0	5.0	.6	0.	0.	151.	0.	0.	.80
N210M1.007	.3	.0	18.9	.0	.04	150.0	44.0	5.0	.8	0.	0.	165.	0.	0.	1.03
N210M1.008	.4	.0	15.1	.0	.08	150.0	28.0	5.0	1.1	0.	0.	132.	0.	0.	1.98
N210M1.009	.5	.0	22.1	.0	.09	150.0	22.0	5.0	1.2	0.	0.	193.	0.	0.	2.04
N210M1.010	.4	.0	18.9	.0	.10	150.0	.0	5.0	1.1	0.	0.	165.	0.	0.	2.38

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210M2.004	.1	.0	.0	.0	.02	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.48
N210M2.005	.3	.0	24.8	.0	.04	150.0	56.0	5.0	.8	0.	0.	216.	0.	0.	.92
N210M2.006	.4	.0	26.7	.0	.02	150.0	50.0	5.0	.9	0.	0.	233.	0.	0.	.60
N210M2.007	.4	.0	23.7	.0	.02	150.0	44.0	5.0	1.1	0.	0.	207.	0.	0.	.71
N210M2.008	.5	.0	20.5	.0	.08	150.0	28.0	5.0	1.2	0.	0.	179.	0.	0.	2.04
N210M2.009	.5	.0	19.9	.0	.09	150.0	22.0	5.0	1.4	0.	0.	174.	0.	0.	2.30
N210M2.010	.4	.0	28.1	.0	.09	150.0	.0	5.0	1.2	0.	0.	245.	0.	0.	2.21
N210M3.004	.1	.0	.0	.0	.00	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.20
N210M3.005	.2	.0	.0	.0	.01	150.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.37
N210M3.006	.2	.0	20.7	.0	.02	150.0	50.0	5.0	.6	0.	0.	180.	0.	0.	.51
N210M3.007	.3	.0	20.4	.0	.04	150.0	44.0	5.0	.9	0.	0.	178.	0.	0.	1.02
N210M3.008	.5	.0	19.9	.0	.06	150.0	28.0	5.0	1.3	0.	0.	173.	0.	0.	1.47
N210M3.009	.5	.0	19.8	.0	.08	150.0	22.0	5.0	1.4	0.	0.	173.	0.	0.	2.01
N210M3.010	.4	.0	23.3	.0	.07	150.0	.0	5.0	1.1	0.	0.	203.	0.	0.	1.73
N210M4.004	.1	.0	.0	.0	.02	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.45
N210M4.005	.4	.0	14.0	.0	.03	150.0	56.0	5.0	1.1	0.	0.	122.	0.	0.	.76
N210M4.006	.4	.0	14.1	.0	.04	150.0	50.0	5.0	1.1	0.	0.	123.	0.	0.	.89
N210M4.007	.3	.0	14.0	.0	.04	150.0	44.0	5.0	.8	0.	0.	122.	0.	0.	.92
N210M4.008	.3	.0	13.8	.0	.05	150.0	28.0	5.0	.9	0.	0.	120.	0.	0.	1.25
N210M4.009	.4	.0	21.2	.0	.08	150.0	22.0	5.0	1.1	0.	0.	184.	0.	0.	1.92
N210M4.010	.4	.0	23.0	.0	.08	150.0	.0	5.0	1.2	0.	0.	201.	0.	0.	2.01
N210M5.004	.1	.0	.0	.0	.00	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.11
N210M5.005	.2	.0	18.6	.0	.01	150.0	56.0	5.0	.6	0.	0.	162.	0.	0.	.17
N210M5.006	.4	.0	30.9	.0	.01	150.0	50.0	5.0	1.0	0.	0.	270.	0.	0.	.29
N210M5.007	.4	.0	29.8	.0	.02	150.0	44.0	5.0	1.0	0.	0.	260.	0.	0.	.55
N210M5.008	.4	.0	30.1	.0	.04	150.0	28.0	5.0	1.1	0.	0.	262.	0.	0.	1.05
N210M5.009	.4	.0	30.1	.0	.06	150.0	22.0	5.0	1.1	0.	0.	262.	0.	0.	1.60
N210M5.010	.4	.0	25.9	.0	.09	150.0	.0	5.0	1.1	0.	0.	226.	0.	0.	2.11
N210N1.004	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.03
N210N1.005	.2	.0	.0	.0	.01	150.0	56.0	11.0	.5	0.	0.	0.	0.	0.	.23
N210N1.006	.2	.0	10.6	.0	.01	150.0	50.0	11.0	.6	0.	0.	92.	0.	0.	.34
N210N1.007	.3	.0	22.5	.0	.01	150.0	44.0	11.0	.8	0.	0.	196.	0.	0.	.28
N210N1.008	.3	.0	23.4	.0	.02	150.0	28.0	11.0	.9	0.	0.	204.	0.	0.	.65
N210N1.009	.4	.0	23.1	.0	.05	150.0	22.0	11.0	1.1	0.	0.	201.	0.	0.	1.21
N210N1.010	.4	.0	25.8	.0	.07	150.0	.0	11.0	1.1	0.	0.	225.	0.	0.	1.84
N210N2.004	.1	.0	.0	.0	.01	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.43
N210N2.005	.1	.0	.0	.0	-.01	150.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.07
N210N2.006	.2	.0	39.2	.0	.01	150.0	50.0	11.0	.6	0.	0.	341.	0.	0.	.22
N210N2.007	.2	.0	29.8	.0	.02	150.0	44.0	11.0	.6	0.	0.	260.	0.	0.	.47
N210N2.008	.4	.0	21.0	.0	.05	150.0	28.0	11.0	.9	0.	0.	183.	0.	0.	1.10
N210N2.009	.4	.0	24.1	.0	.05	150.0	22.0	11.0	1.1	0.	0.	210.	0.	0.	1.29
N210N2.010	.4	.0	22.5	.0	.08	150.0	.0	11.0	1.1	0.	0.	196.	0.	0.	1.94

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210N3.004	.1	.0	.0	.0	-.02	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.06
N210N3.005	.2	.0	.0	.0	-.01	150.0	56.0	11.0	.5	0.	0.	0.	0.	0.	.03
N210N3.006	.3	.0	24.9	.0	.00	150.0	50.0	11.0	.8	0.	0.	217.	0.	0.	.08
N210N3.007	.3	.0	24.6	.0	.00	150.0	44.0	11.0	.8	0.	0.	214.	0.	0.	.19
N210N3.008	.3	.0	21.2	.0	.01	150.0	28.0	11.0	.9	0.	0.	184.	0.	0.	.63
N210N3.009	.4	.0	23.4	.0	.02	150.0	22.0	11.0	1.1	0.	0.	204.	0.	0.	.92
N210N3.010	.4	.0	17.8	.0	.05	150.0	.0	11.0	1.0	0.	0.	155.	0.	0.	1.41
N210N4.004	.1	.0	.0	.0	.03	150.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.71
N210N4.005	.2	.0	.0	.0	.04	150.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.89
N210N4.006	.3	.0	28.0	.0	.03	150.0	50.0	11.0	.9	0.	0.	244.	0.	0.	.70
N210N4.007	.4	.0	25.6	.0	.03	150.0	44.0	11.0	.9	0.	0.	224.	0.	0.	.72
N210N4.008	.5	.0	25.8	.0	.06	150.0	28.0	11.0	1.3	0.	0.	225.	0.	0.	1.51
N210N4.009	.5	.0	19.2	.0	.08	150.0	22.0	11.0	1.3	0.	0.	168.	0.	0.	1.99
N210N4.010	.4	.0	19.5	.0	.04	150.0	.0	11.0	1.0	0.	0.	170.	0.	0.	1.29
N210N5.004	.1	.0	.0	.0	-.01	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.08
N210N5.005	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.07
N210N5.006	.1	.0	.0	.0	-.02	150.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.05
N210N5.007	.2	.0	25.2	.0	.02	150.0	44.0	11.0	.6	0.	0.	220.	0.	0.	.48
N210N5.008	.4	.0	21.9	.0	.03	150.0	28.0	11.0	1.0	0.	0.	191.	0.	0.	.87
N210N5.009	.4	.0	16.1	.0	.04	150.0	22.0	11.0	1.0	0.	0.	141.	0.	0.	1.06
N210N5.010	.4	.0	24.8	.0	.10	150.0	.0	11.0	1.1	0.	0.	216.	0.	0.	2.37
N21001.004	.1	.0	.0	.0	.01	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.32
N21001.005	.2	.0	23.7	.0	.02	150.0	56.0	17.0	.7	0.	0.	207.	0.	0.	.40
N21001.006	.2	.0	.0	.0	.01	150.0	50.0	17.0	.4	0.	0.	0.	0.	0.	.39
N21001.007	.3	.0	23.9	.0	.02	150.0	44.0	17.0	.8	0.	0.	209.	0.	0.	.40
N21001.008	.3	.0	24.0	.0	.04	150.0	28.0	17.0	.9	0.	0.	210.	0.	0.	1.09
N21001.009	.4	.0	23.8	.0	.04	150.0	22.0	17.0	1.0	0.	0.	207.	0.	0.	.97
N21001.010	.3	.0	19.6	.0	.03	150.0	.0	17.0	.8	0.	0.	171.	0.	0.	.89
N21002.004	.1	.0	.0	.0	.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.34
N21002.005	.3	.0	25.1	.0	.01	150.0	56.0	17.0	.7	0.	0.	218.	0.	0.	.28
N21002.006	.2	.0	12.9	.0	-.01	150.0	50.0	17.0	.6	0.	0.	112.	0.	0.	.14
N21002.007	.3	.0	21.1	.0	.01	150.0	44.0	17.0	.9	0.	0.	184.	0.	0.	.40
N21002.008	.3	.0	17.1	.0	.02	150.0	28.0	17.0	.9	0.	0.	149.	0.	0.	.83
N21002.009	.4	.0	20.2	.0	.05	150.0	22.0	17.0	1.0	0.	0.	176.	0.	0.	1.21
N21002.010	.3	.0	20.0	.0	-.02	150.0	.0	17.0	.8	0.	0.	174.	0.	0.	.62
N21003.004	.1	.0	.0	.0	.00	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.20
N21003.005	.1	.0	.0	.0	.02	150.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.61
N21003.006	.2	.0	39.5	.0	.01	150.0	50.0	17.0	.6	0.	0.	344.	0.	0.	.42
N21003.007	.3	.0	19.9	.0	.04	150.0	44.0	17.0	.8	0.	0.	173.	0.	0.	.91
N21003.008	.4	.0	31.8	.0	.07	150.0	28.0	17.0	1.0	0.	0.	277.	0.	0.	1.66
N21003.009	.4	.0	25.9	.0	.06	150.0	22.0	17.0	1.1	0.	0.	226.	0.	0.	1.49
N21003.010	.4	.0	29.8	.0	.04	150.0	.0	17.0	1.0	0.	0.	260.	0.	0.	1.15

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N21004.004	.1	.0	.0	.0	.00	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.21
N21004.005	.1	.0	.0	.0	-.02	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.11
N21004.006	.1	.0	.0	.0	-.02	150.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.06
N21004.007	.3	.0	33.9	.0	-.01	150.0	44.0	17.0	.7	0.	0.	296.	0.	0.	.08
N21004.008	.4	.0	22.3	.0	.00	150.0	28.0	17.0	1.1	0.	0.	195.	0.	0.	.49
N21004.009	.5	.0	26.3	.0	.03	150.0	22.0	17.0	1.4	0.	0.	230.	0.	0.	.92
N21004.010	.4	.0	27.6	.0	.05	150.0	.0	17.0	1.0	0.	0.	241.	0.	0.	1.25
N21005.004	.1	.0	.0	.0	.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.27
N21005.005	.2	.0	22.8	.0	.02	150.0	56.0	17.0	.6	0.	0.	199.	0.	0.	.42
N21005.006	.2	.0	21.1	.0	.03	150.0	50.0	17.0	.6	0.	0.	184.	0.	0.	.72
N21005.007	.2	.0	44.1	.0	.06	150.0	44.0	17.0	.6	0.	0.	384.	0.	0.	1.34
N21005.008	.6	.0	20.2	.0	.06	150.0	28.0	17.0	1.6	0.	0.	176.	0.	0.	1.51
N21005.009	.4	.0	26.1	.0	.05	150.0	22.0	17.0	1.2	0.	0.	227.	0.	0.	1.23
N21005.010	.4	.0	20.1	.0	.05	150.0	.0	17.0	1.0	0.	0.	176.	0.	0.	1.36
N210P1.004	.5	.0	28.4	.0	.13	150.0	.0	1.0	1.3	0.	0.	247.	0.	0.	3.12
N210P1.005	.4	.0	25.3	.0	.11	150.0	-22.0	1.0	1.1	0.	0.	221.	0.	0.	2.51
N210P1.006	.5	.0	28.9	.0	.11	150.0	-28.0	1.0	1.3	0.	0.	252.	0.	0.	2.66
N210P1.007	.4	.0	20.5	.0	.08	150.0	-44.0	1.0	1.0	0.	0.	179.	0.	0.	1.87
N210P1.008	.3	.0	33.6	.0	.07	150.0	-56.0	1.0	.8	0.	0.	293.	0.	0.	1.71
N210P1.009	.2	.0	.0	.0	.03	150.0	-66.0	1.0	.5	0.	0.	0.	0.	0.	.74
N210P1.010	.1	.0	.0	.0	-.01	150.0	-75.0	1.0	.4	0.	0.	0.	0.	0.	.22
N210P2.004	.5	.0	28.1	.0	.10	150.0	.0	1.0	1.2	0.	0.	245.	0.	0.	2.42
N210P2.005	.5	.0	21.8	.0	.11	150.0	-22.0	1.0	1.3	0.	0.	190.	0.	0.	2.70
N210P2.006	.5	.0	22.1	.0	.12	150.0	-28.0	1.0	1.4	0.	0.	193.	0.	0.	2.77
N210P2.007	.4	.0	18.2	.0	.07	150.0	-44.0	1.0	1.1	0.	0.	159.	0.	0.	1.62
N210P2.008	.5	.0	18.8	.0	.05	150.0	-56.0	1.0	1.2	0.	0.	164.	0.	0.	1.24
N210P2.009	.4	.0	19.0	.0	.02	150.0	-66.0	1.0	1.2	0.	0.	166.	0.	0.	.66
N210P2.010	.4	.0	18.9	.0	.06	150.0	-75.0	1.0	1.1	0.	0.	165.	0.	0.	1.36
N210P3.004	.4	.0	27.2	.0	.12	150.0	.0	1.0	1.2	0.	0.	237.	0.	0.	2.75
N210P3.005	.4	.0	22.7	.0	.10	150.0	-22.0	1.0	1.2	0.	0.	198.	0.	0.	2.37
N210P3.006	.4	.0	23.9	.0	.10	150.0	-28.0	1.0	1.1	0.	0.	208.	0.	0.	2.27
N210P3.007	.2	.0	30.6	.0	.03	150.0	-44.0	1.0	.6	0.	0.	267.	0.	0.	.89
N210P3.008	.2	.0	18.0	.0	.03	150.0	-56.0	1.0	.6	0.	0.	157.	0.	0.	.67
N210P3.009	.1	.0	.0	.0	-.01	150.0	-66.0	1.0	.3	0.	0.	0.	0.	0.	.14
N210P3.010	.2	.0	41.5	.0	.00	150.0	-75.0	1.0	.6	0.	0.	362.	0.	0.	.96
N210P4.004	.4	.0	22.4	.0	.14	150.0	.0	1.0	1.1	0.	0.	195.	0.	0.	3.22
N210P4.005	.4	.0	25.6	.0	.08	150.0	-22.0	1.0	1.0	0.	0.	223.	0.	0.	2.04
N210P4.006	.4	.0	21.7	.0	.08	150.0	-28.0	1.0	1.0	0.	0.	189.	0.	0.	1.96
N210P4.007	.3	.0	25.9	.0	.05	150.0	-44.0	1.0	.7	0.	0.	226.	0.	0.	1.31
N210P4.008	.2	.0	.0	.0	.04	150.0	-56.0	1.0	.5	0.	0.	0.	0.	0.	.93
N210P4.009	.1	.0	.0	.0	.01	150.0	-66.0	1.0	.4	0.	0.	0.	0.	0.	.43
N210P4.010	.1	.0	.0	.0	.03	150.0	-75.0	1.0	.4	0.	0.	0.	0.	0.	.81

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210P5.004	.3	.0	22.0	.0	.07	150.0	.0	1.0	.9	0.	0.	191.	0.	0.	1.85
N210P5.005	.4	.0	15.7	.0	.08	150.0	-22.0	1.0	1.0	0.	0.	136.	0.	0.	2.04
N210P5.006	.4	.0	15.6	.0	.08	150.0	-28.0	1.0	1.1	0.	0.	136.	0.	0.	1.84
N210P5.007	.2	.0	16.2	.0	.04	150.0	-44.0	1.0	.6	0.	0.	141.	0.	0.	1.07
N210P5.008	.1	.0	.0	.0	.02	150.0	-56.0	1.0	.3	0.	0.	0.	0.	0.	.47
N210P5.009	.1	.0	.0	.0	.00	150.0	-66.0	1.0	.3	0.	0.	0.	0.	0.	.18
N210P5.010	.1	.0	.0	.0	.00	150.0	-75.0	1.0	.3	0.	0.	0.	0.	0.	.25
N210Q1.004	.4	.0	22.8	.0	.11	150.0	.0	5.0	1.2	0.	0.	198.	0.	0.	2.52
N210Q1.005	.4	.0	19.9	.0	.09	150.0	-22.0	5.0	1.1	0.	0.	174.	0.	0.	2.16
N210Q1.006	.4	.0	22.2	.0	.07	150.0	-28.0	5.0	1.1	0.	0.	194.	0.	0.	1.80
N210Q1.007	.4	.0	16.3	.0	.04	150.0	-44.0	5.0	1.0	0.	0.	142.	0.	0.	1.13
N210Q1.008	.3	.0	16.5	.0	.06	150.0	-56.0	5.0	.9	0.	0.	143.	0.	0.	1.30
N210Q1.009	.2	.0	.0	.0	.02	150.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.57
N210Q1.010	.2	.0	.0	.0	.02	150.0	-75.0	5.0	.5	0.	0.	0.	0.	0.	.65
N210Q2.004	.5	.0	22.6	.0	.11	150.0	.0	5.0	1.2	0.	0.	197.	0.	0.	2.64
N210Q2.005	.5	.0	19.5	.0	.11	150.0	-22.0	5.0	1.3	0.	0.	170.	0.	0.	2.50
N210Q2.006	.4	.0	19.3	.0	.09	150.0	-28.0	5.0	1.1	0.	0.	168.	0.	0.	2.07
N210Q2.007	.3	.0	25.5	.0	.02	150.0	-44.0	5.0	.8	0.	0.	222.	0.	0.	.72
N210Q2.008	.3	.0	20.3	.0	.03	150.0	-56.0	5.0	.9	0.	0.	177.	0.	0.	.68
N210Q2.009	.3	.0	25.6	.0	.03	150.0	-66.0	5.0	.7	0.	0.	223.	0.	0.	.80
N210Q2.010	.1	.0	.0	.0	.03	150.0	-75.0	5.0	.3	0.	0.	0.	0.	0.	.70
N210Q3.004	.4	.0	14.7	.0	.09	150.0	.0	5.0	1.1	0.	0.	128.	0.	0.	2.25
N210Q3.005	.4	.0	16.2	.0	.08	150.0	-22.0	5.0	1.1	0.	0.	141.	0.	0.	1.98
N210Q3.006	.4	.0	21.0	.0	.07	150.0	-28.0	5.0	1.1	0.	0.	183.	0.	0.	1.67
N210Q3.007	.4	.0	21.2	.0	.05	150.0	-44.0	5.0	1.1	0.	0.	185.	0.	0.	1.18
N210Q3.008	.3	.0	18.8	.0	.02	150.0	-56.0	5.0	.7	0.	0.	164.	0.	0.	.60
N210Q3.009	.2	.0	20.7	.0	.02	150.0	-66.0	5.0	.6	0.	0.	180.	0.	0.	.53
N210Q3.010	.1	.0	.0	.0	.00	150.0	-75.0	5.0	.3	0.	0.	0.	0.	0.	.15
N210Q4.004	.4	.0	23.7	.0	.11	150.0	.0	5.0	1.2	0.	0.	206.	0.	0.	2.66
N210Q4.005	.4	.0	25.7	.0	.08	150.0	-22.0	5.0	1.2	0.	0.	224.	0.	0.	1.99
N210Q4.006	.4	.0	17.0	.0	.07	150.0	-28.0	5.0	1.2	0.	0.	148.	0.	0.	1.64
N210Q4.007	.4	.0	16.5	.0	.04	150.0	-44.0	5.0	1.1	0.	0.	143.	0.	0.	1.02
N210Q4.008	.3	.0	17.9	.0	.03	150.0	-56.0	5.0	.8	0.	0.	156.	0.	0.	.76
N210Q4.009	.3	.0	16.9	.0	.02	150.0	-66.0	5.0	.7	0.	0.	147.	0.	0.	.56
N210Q4.010	.2	.0	17.1	.0	.02	150.0	-75.0	5.0	.6	0.	0.	149.	0.	0.	.51
N210Q5.004	.4	.0	20.4	.0	.10	150.0	.0	5.0	1.2	0.	0.	178.	0.	0.	2.38
N210Q5.005	.5	.0	20.4	.0	.07	150.0	-22.0	5.0	1.3	0.	0.	178.	0.	0.	1.79
N210Q5.006	.5	.0	19.0	.0	.08	150.0	-28.0	5.0	1.2	0.	0.	166.	0.	0.	1.89
N210Q5.007	.3	.0	22.0	.0	.05	150.0	-44.0	5.0	.9	0.	0.	192.	0.	0.	1.26
N210Q5.008	.4	.0	25.7	.0	.02	150.0	-56.0	5.0	.9	0.	0.	224.	0.	0.	.59
N210Q5.009	.2	.0	.0	.0	.03	150.0	-66.0	5.0	.5	0.	0.	0.	0.	0.	.74
N210Q5.010	.1	.0	.0	.0	.02	150.0	-75.0	5.0	.4	0.	0.	0.	0.	0.	.61

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210R1.004	.4	.0	22.3	.0	.11	150.0	.0	11.0	1.2	0.	0.	194.	0.	0.	2.60
N210R1.005	.5	.0	27.1	.0	.10	150.0	-22.0	11.0	1.3	0.	0.	236.	0.	0.	2.27
N210R1.006	.5	.0	21.2	.0	.08	150.0	-28.0	11.0	1.3	0.	0.	185.	0.	0.	1.86
N210R1.007	.3	.0	20.8	.0	.04	150.0	-44.0	11.0	.9	0.	0.	182.	0.	0.	1.05
N210R1.008	.3	.0	27.4	.0	.04	150.0	-56.0	11.0	.8	0.	0.	239.	0.	0.	.84
N210R1.009	.2	.0	.0	.0	.04	150.0	-66.0	11.0	.5	0.	0.	0.	0.	0.	.94
N210R1.010	.1	.0	.0	.0	.02	150.0	-75.0	11.0	.4	0.	0.	0.	0.	0.	.47
N210R2.004	.5	.0	27.7	.0	.10	150.0	.0	11.0	1.4	0.	0.	241.	0.	0.	2.27
N210R2.005	.6	.0	27.3	.0	.07	150.0	-22.0	11.0	1.5	0.	0.	238.	0.	0.	1.63
N210R2.006	.4	.0	23.1	.0	.04	150.0	-28.0	11.0	1.1	0.	0.	201.	0.	0.	1.05
N210R2.007	.4	.0	23.1	.0	.04	150.0	-44.0	11.0	1.1	0.	0.	201.	0.	0.	1.03
N210R2.008	.2	.0	21.3	.0	.01	150.0	-56.0	11.0	.6	0.	0.	186.	0.	0.	.27
N210R2.009	.1	.0	.0	.0	.01	150.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.33
N210R2.010	.1	.0	.0	.0	.01	150.0	-75.0	11.0	.1	0.	0.	0.	0.	0.	.31
N210R3.004	.4	.0	25.3	.0	.08	150.0	.0	11.0	1.2	0.	0.	221.	0.	0.	1.83
N210R3.005	.4	.0	26.4	.0	.07	150.0	-22.0	11.0	1.2	0.	0.	230.	0.	0.	1.64
N210R3.006	.5	.0	24.1	.0	.06	150.0	-28.0	11.0	1.3	0.	0.	210.	0.	0.	1.40
N210R3.007	.4	.0	34.0	.0	.03	150.0	-44.0	11.0	1.0	0.	0.	297.	0.	0.	.78
N210R3.008	.2	.0	.0	.0	.02	150.0	-56.0	11.0	.5	0.	0.	0.	0.	0.	.54
N210R3.009	.3	.0	34.9	.0	.00	150.0	-66.0	11.0	.7	0.	0.	304.	0.	0.	.24
N210R3.010	.1	.0	.0	.0	.01	150.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.24
N210R4.004	.4	.0	19.1	.0	.08	150.0	.0	11.0	1.2	0.	0.	166.	0.	0.	1.87
N210R4.005	.4	.0	22.3	.0	.07	150.0	-22.0	11.0	1.2	0.	0.	194.	0.	0.	1.73
N210R4.006	.4	.0	22.4	.0	.05	150.0	-28.0	11.0	1.1	0.	0.	195.	0.	0.	1.26
N210R4.007	.3	.0	28.0	.0	.03	150.0	-44.0	11.0	.9	0.	0.	244.	0.	0.	.68
N210R4.008	.2	.0	.0	.0	.02	150.0	-56.0	11.0	.4	0.	0.	0.	0.	0.	.42
N210R4.009	.2	.0	.0	.0	.03	150.0	-66.0	11.0	.4	0.	0.	0.	0.	0.	.69
N210R4.010	.1	.0	.0	.0	.02	150.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.43
N210R5.004	.6	.0	28.4	.0	.07	150.0	.0	11.0	1.5	0.	0.	248.	0.	0.	1.77
N210R5.005	.4	.0	22.3	.0	.04	150.0	-22.0	11.0	1.1	0.	0.	194.	0.	0.	1.04
N210R5.006	.5	.0	28.4	.0	.03	150.0	-28.0	11.0	1.3	0.	0.	248.	0.	0.	.88
N210R5.007	.3	.0	38.8	.0	.02	150.0	-44.0	11.0	.8	0.	0.	338.	0.	0.	.64
N210R5.008	.3	.0	38.3	.0	.00	150.0	-56.0	11.0	.8	0.	0.	334.	0.	0.	.32
N210R5.009	.1	.0	.0	.0	.01	150.0	-66.0	11.0	.3	0.	0.	0.	0.	0.	.37
N210R5.010	.1	.0	.0	.0	.00	150.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.20
N210S1.004	.4	.0	23.6	.0	.06	150.0	.0	17.0	1.1	0.	0.	205.	0.	0.	1.43
N210S1.005	.4	.0	20.3	.0	.04	150.0	-22.0	17.0	1.0	0.	0.	177.	0.	0.	1.13
N210S1.006	.4	.0	19.3	.0	.05	150.0	-28.0	17.0	1.0	0.	0.	169.	0.	0.	1.31
N210S1.007	.3	.0	31.0	.0	.02	150.0	-44.0	17.0	.9	0.	0.	270.	0.	0.	.55
N210S1.008	.2	.0	.0	.0	-.01	150.0	-56.0	17.0	.5	0.	0.	0.	0.	0.	.13
N210S1.009	.1	.0	.0	.0	.00	150.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.14
N210S1.010	.1	.0	.0	.0	.00	150.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.16

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210S2.004	.5	.0	15.2	.0	.05	150.0	.0	17.0	1.3	0.	0.	133.	0.	0.	1.24
N210S2.005	.4	.0	22.1	.0	.08	150.0	-22.0	17.0	1.2	0.	0.	192.	0.	0.	1.87
N210S2.006	.4	.0	20.9	.0	.05	150.0	-28.0	17.0	1.1	0.	0.	182.	0.	0.	1.26
N210S2.007	.4	.0	17.2	.0	.06	150.0	-44.0	17.0	1.0	0.	0.	150.	0.	0.	1.43
N210S2.008	.2	.0	34.3	.0	.03	150.0	-56.0	17.0	.6	0.	0.	299.	0.	0.	.70
N210S2.009	.2	.0	16.6	.0	.03	150.0	-66.0	17.0	.6	0.	0.	145.	0.	0.	.72
N210S2.010	.2	.0	.0	.0	.03	150.0	-75.0	17.0	.5	0.	0.	0.	0.	0.	.65
N210S3.004	.3	.0	20.6	.0	.05	150.0	.0	17.0	.9	0.	0.	179.	0.	0.	1.27
N210S3.005	.3	.0	16.2	.0	.03	150.0	-22.0	17.0	.9	0.	0.	141.	0.	0.	.90
N210S3.006	.4	.0	21.9	.0	.03	150.0	-28.0	17.0	1.0	0.	0.	191.	0.	0.	.72
N210S3.007	.2	.0	33.6	.0	.04	150.0	-44.0	17.0	.7	0.	0.	293.	0.	0.	1.04
N210S3.008	.3	.0	33.5	.0	.00	150.0	-56.0	17.0	.7	0.	0.	292.	0.	0.	.08
N210S3.009	.1	.0	.0	.0	-.02	150.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.07
N210S3.010	.0	.0	.0	.0	-.04	150.0	-75.0	17.0	.0	0.	0.	0.	0.	0.	.00
N210S4.004	.4	.0	26.7	.0	.06	150.0	.0	17.0	1.2	0.	0.	233.	0.	0.	1.43
N210S4.005	.3	.0	25.2	.0	.02	150.0	-22.0	17.0	.8	0.	0.	220.	0.	0.	.71
N210S4.006	.3	.0	18.9	.0	.02	150.0	-28.0	17.0	.8	0.	0.	165.	0.	0.	.55
N210S4.007	.2	.0	30.1	.0	.00	150.0	-44.0	17.0	.6	0.	0.	262.	0.	0.	.38
N210S4.008	.1	.0	.0	.0	.00	150.0	-56.0	17.0	.3	0.	0.	0.	0.	0.	.31
N210S4.009	.1	.0	.0	.0	.00	150.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.17
N210S4.010	.0	.0	.0	.0	.00	150.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.12
N210S5.004	.5	.0	25.9	.0	.04	150.0	.0	17.0	1.2	0.	0.	225.	0.	0.	1.22
N210S5.005	.4	.0	29.2	.0	.02	150.0	-22.0	17.0	1.1	0.	0.	255.	0.	0.	.70
N210S5.006	.3	.0	29.9	.0	.01	150.0	-28.0	17.0	.9	0.	0.	260.	0.	0.	.42
N210S5.007	.3	.0	33.3	.0	.04	150.0	-44.0	17.0	.8	0.	0.	291.	0.	0.	1.11
N210S5.008	.1	.0	.0	.0	.00	150.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.22
N210S5.009	.1	.0	.0	.0	.01	150.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.25
N210S5.010	.0	.0	.0	.0	.00	150.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.08
N210T1.004	.1	.0	.0	.0	.02	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.68
N210T1.005	.1	.0	.0	.0	.03	250.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.82
N210T1.006	.2	.0	.0	.0	.05	250.0	56.0	1.0	.5	0.	0.	0.	0.	0.	1.19
N210T1.007	.3	.0	23.6	.0	.06	250.0	44.0	1.0	.8	0.	0.	206.	0.	0.	1.49
N210T1.008	.3	.0	26.5	.0	.09	250.0	28.0	1.0	.9	0.	0.	231.	0.	0.	2.05
N210T1.009	.4	.0	27.0	.0	.09	250.0	22.0	1.0	1.1	0.	0.	235.	0.	0.	2.10
N210T1.010	.3	.0	27.1	.0	.09	250.0	.0	1.0	.9	0.	0.	236.	0.	0.	2.21
N210T2.004	.1	.0	.0	.0	-.01	250.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.10
N210T2.005	.1	.0	.0	.0	.01	250.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.35
N210T2.006	.1	.0	.0	.0	-.01	250.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.16
N210T2.007	.2	.0	.0	.0	-.01	250.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.27
N210T2.008	.2	.0	.0	.0	.04	250.0	28.0	1.0	.5	0.	0.	0.	0.	0.	1.23
N210T2.009	.3	.0	29.4	.0	.06	250.0	22.0	1.0	.8	0.	0.	256.	0.	0.	1.48
N210T2.010	.3	.0	24.7	.0	.07	250.0	.0	1.0	.7	0.	0.	215.	0.	0.	1.66

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210T3.004	.1	.0	.0	.0	-.03	250.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.04
N210T3.005	.1	.0	.0	.0	-.02	250.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.10
N210T3.006	.1	.0	.0	.0	-.02	250.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.09
N210T3.007	.2	.0	.0	.0	.01	250.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.65
N210T3.008	.2	.0	20.2	.0	.04	250.0	28.0	1.0	.6	0.	0.	176.	0.	0.	.85
N210T3.009	.3	.0	27.3	.0	.06	250.0	22.0	1.0	.8	0.	0.	238.	0.	0.	1.39
N210T3.010	.3	.0	21.8	.0	.08	250.0	.0	1.0	.9	0.	0.	190.	0.	0.	1.90
N210T4.004	.1	.0	.0	.0	.01	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.33
N210T4.005	.1	.0	.0	.0	.01	250.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.35
N210T4.006	.1	.0	.0	.0	.03	250.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.62
N210T4.007	.2	.0	38.1	.0	.04	250.0	44.0	1.0	.6	0.	0.	332.	0.	0.	1.24
N210T4.008	.3	.0	30.4	.0	.07	250.0	28.0	1.0	.8	0.	0.	265.	0.	0.	1.74
N210T4.009	.4	.0	30.6	.0	.07	250.0	22.0	1.0	1.1	0.	0.	267.	0.	0.	1.76
N210T4.010	.4	.0	27.7	.0	.09	250.0	.0	1.0	1.2	0.	0.	241.	0.	0.	2.26
N210T5.004	.2	.0	.0	.0	.05	250.0	75.0	1.0	.4	0.	0.	0.	0.	0.	1.17
N210T5.005	.1	.0	.0	.0	.00	250.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.30
N210T5.006	.1	.0	.0	.0	.02	250.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.53
N210T5.007	.1	.0	.0	.0	.00	250.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.27
N210T5.008	.3	.0	32.8	.0	.07	250.0	28.0	1.0	.8	0.	0.	286.	0.	0.	1.67
N210T5.009	.3	.0	32.8	.0	.08	250.0	22.0	1.0	.9	0.	0.	286.	0.	0.	1.89
N210T5.010	.4	.0	37.8	.0	.08	250.0	.0	1.0	1.0	0.	0.	329.	0.	0.	1.95
N210U1.004	.1	.0	.0	.0	.02	250.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.51
N210U1.005	.1	.0	.0	.0	.02	250.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.52
N210U1.006	.1	.0	.0	.0	.01	250.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.38
N210U1.007	.2	.0	.0	.0	.03	250.0	44.0	5.0	.5	0.	0.	0.	0.	0.	.71
N210U1.008	.3	.0	29.4	.0	.05	250.0	28.0	5.0	.8	0.	0.	256.	0.	0.	1.27
N210U1.009	.3	.0	28.9	.0	.03	250.0	22.0	5.0	.8	0.	0.	252.	0.	0.	.86
N210U1.010	.4	.0	32.8	.0	.06	250.0	.0	5.0	1.0	0.	0.	286.	0.	0.	1.43
N210U2.004	.1	.0	.0	.0	-.02	250.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.07
N210U2.005	.1	.0	.0	.0	.00	250.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.23
N210U2.006	.2	.0	.0	.0	.01	250.0	56.0	5.0	.5	0.	0.	0.	0.	0.	.36
N210U2.007	.3	.0	21.9	.0	.04	250.0	44.0	5.0	.7	0.	0.	191.	0.	0.	.98
N210U2.008	.3	.0	27.8	.0	.03	250.0	28.0	5.0	.8	0.	0.	242.	0.	0.	.80
N210U2.009	.3	.0	21.2	.0	.04	250.0	22.0	5.0	.9	0.	0.	185.	0.	0.	1.10
N210U2.010	.3	.0	26.5	.0	.05	250.0	.0	5.0	.9	0.	0.	231.	0.	0.	1.34
N210U3.004	.1	.0	.0	.0	.01	250.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.39
N210U3.005	.2	.0	.0	.0	.01	250.0	66.0	5.0	.4	0.	0.	0.	0.	0.	.35
N210U3.006	.3	.0	36.0	.0	.02	250.0	56.0	5.0	.7	0.	0.	313.	0.	0.	.54
N210U3.007	.2	.0	20.4	.0	.02	250.0	44.0	5.0	.6	0.	0.	178.	0.	0.	.66
N210U3.008	.4	.0	31.5	.0	.04	250.0	28.0	5.0	1.0	0.	0.	274.	0.	0.	1.14
N210U3.009	.4	.0	30.8	.0	.05	250.0	22.0	5.0	1.1	0.	0.	269.	0.	0.	1.38
N210U3.010	.3	.0	35.1	.0	.07	250.0	.0	5.0	.8	0.	0.	306.	0.	0.	1.69

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210U5.004	.1	.0	.0	.0	.00	250.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.24
N210U5.005	.1	.0	.0	.0	.00	250.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.10
N210U5.006	.1	.0	.0	.0	.00	250.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.17
N210U5.007	.1	.0	.0	.0	-.01	250.0	44.0	5.0	.3	0.	0.	0.	0.	0.	.11
N210U5.008	.2	.0	18.6	.0	.02	250.0	28.0	5.0	.5	0.	0.	162.	0.	0.	.51
N210U5.009	.3	.0	21.3	.0	.03	250.0	22.0	5.0	.7	0.	0.	186.	0.	0.	.91
N210U5.010	.4	.0	27.1	.0	.05	250.0	.0	5.0	1.0	0.	0.	237.	0.	0.	1.38
N210V1.004	.1	.0	.0	.0	.01	250.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.38
N210V1.005	.1	.0	.0	.0	.00	250.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.25
N210V1.006	.1	.0	.0	.0	.00	250.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.12
N210V1.007	.1	.0	.0	.0	.00	250.0	44.0	11.0	.3	0.	0.	0.	0.	0.	.19
N210V1.008	.2	.0	.0	.0	.00	250.0	28.0	11.0	.5	0.	0.	0.	0.	0.	.33
N210V1.009	.2	.0	18.8	.0	.01	250.0	22.0	11.0	.6	0.	0.	164.	0.	0.	.56
N210V1.010	.3	.0	21.8	.0	.05	250.0	.0	11.0	.8	0.	0.	190.	0.	0.	1.26
N210V2.004	.1	.0	.0	.0	.00	250.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.14
N210V2.005	.1	.0	.0	.0	.01	250.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.43
N210V2.006	.1	.0	.0	.0	.01	250.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.39
N210V2.007	.1	.0	.0	.0	.00	250.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.19
N210V2.008	.2	.0	14.1	.0	.05	250.0	28.0	11.0	.6	0.	0.	123.	0.	0.	1.08
N210V2.009	.4	.0	26.4	.0	.04	250.0	22.0	11.0	1.0	0.	0.	230.	0.	0.	.99
N210V2.010	.3	.0	26.1	.0	.06	250.0	.0	11.0	.9	0.	0.	228.	0.	0.	1.48
N210V3.004	.1	.0	.0	.0	.02	250.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.53
N210V3.005	.1	.0	.0	.0	.03	250.0	66.0	11.0	.4	0.	0.	0.	0.	0.	.79
N210V3.006	.3	.0	33.0	.0	.01	250.0	56.0	11.0	.7	0.	0.	288.	0.	0.	.44
N210V3.007	.2	.0	32.6	.0	.02	250.0	44.0	11.0	.6	0.	0.	284.	0.	0.	.67
N210V3.008	.3	.0	30.9	.0	.02	250.0	28.0	11.0	.7	0.	0.	269.	0.	0.	.65
N210V3.009	.3	.0	31.0	.0	.03	250.0	22.0	11.0	.8	0.	0.	271.	0.	0.	.84
N210V3.010	.3	.0	28.5	.0	.03	250.0	.0	11.0	.7	0.	0.	249.	0.	0.	.79
N210V4.004	.1	.0	.0	.0	-.01	250.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.13
N210V4.005	.1	.0	.0	.0	-.01	250.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.13
N210V4.006	.2	.0	.0	.0	.00	250.0	56.0	11.0	.5	0.	0.	0.	0.	0.	.06
N210V4.007	.2	.0	28.5	.0	.01	250.0	44.0	11.0	.6	0.	0.	248.	0.	0.	.34
N210V4.008	.3	.0	22.2	.0	.00	250.0	28.0	11.0	.8	0.	0.	193.	0.	0.	.42
N210V4.009	.3	.0	23.4	.0	.02	250.0	22.0	11.0	.8	0.	0.	204.	0.	0.	.63
N210V4.010	.3	.0	24.3	.0	.03	250.0	.0	11.0	.9	0.	0.	212.	0.	0.	.92
N210V5.004	.1	.0	.0	.0	-.01	250.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.15
N210V5.005	.1	.0	.0	.0	.01	250.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.41
N210V5.006	.2	.0	.0	.0	.00	250.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.28
N210V5.007	.2	.0	22.8	.0	.00	250.0	44.0	11.0	.6	0.	0.	199.	0.	0.	.28
N210V5.008	.3	.0	25.6	.0	.02	250.0	28.0	11.0	.9	0.	0.	223.	0.	0.	.64
N210V5.009	.4	.0	27.7	.0	.05	250.0	22.0	11.0	1.0	0.	0.	242.	0.	0.	1.27
N210V5.010	.4	.0	25.9	.0	.08	250.0	.0	11.0	1.0	0.	0.	225.	0.	0.	1.85

FALCON 2: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N210W1.004	.1	.0	.0	.0	-.01	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.12
N210W1.005	.1	.0	.0	.0	-.01	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.05
N210W1.006	.0	.0	.0	.0	-.01	250.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.07
N210W1.007	.0	.0	.0	.0	-.02	250.0	44.0	17.0	.1	0.	0.	0.	0.	0.	.03
N210W1.008	.1	.0	.0	.0	.00	250.0	28.0	17.0	.4	0.	0.	0.	0.	0.	.09
N210W1.009	.2	.0	21.8	.0	-.01	250.0	22.0	17.0	.6	0.	0.	190.	0.	0.	.12
N210W1.010	.2	.0	16.5	.0	-.01	250.0	.0	17.0	.6	0.	0.	144.	0.	0.	.34
N210W2.004	.1	.0	.0	.0	.00	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.14
N210W2.005	.1	.0	.0	.0	.01	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.27
N210W2.006	.1	.0	.0	.0	.02	250.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.62
N210W2.007	.1	.0	.0	.0	.01	250.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.41
N210W2.008	.2	.0	.0	.0	.02	250.0	28.0	17.0	.5	0.	0.	0.	0.	0.	.60
N210W2.009	.2	.0	.0	.0	.01	250.0	22.0	17.0	.5	0.	0.	0.	0.	0.	.44
N210W2.010	.3	.0	28.9	.0	.04	250.0	.0	17.0	.7	0.	0.	252.	0.	0.	1.01
N210W3.004	.1	.0	.0	.0	.01	250.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.47
N210W3.005	.1	.0	.0	.0	.01	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.26
N210W3.006	.1	.0	.0	.0	.01	250.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.33
N210W3.007	.2	.0	.0	.0	.01	250.0	44.0	17.0	.4	0.	0.	0.	0.	0.	.26
N210W3.008	.2	.0	.0	.0	.00	250.0	28.0	17.0	.5	0.	0.	0.	0.	0.	.04
N210W3.009	.2	.0	25.7	.0	.00	250.0	22.0	17.0	.6	0.	0.	224.	0.	0.	.29
N210W3.010	.2	.0	19.2	.0	-.02	250.0	.0	17.0	.6	0.	0.	167.	0.	0.	.34
N210W4.004	.1	.0	.0	.0	.01	250.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.44
N210W4.005	.1	.0	.0	.0	.01	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.34
N210W4.006	.2	.0	.0	.0	.02	250.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.47
N210W4.007	.2	.0	.0	.0	.01	250.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.39
N210W4.008	.2	.0	36.3	.0	.01	250.0	28.0	17.0	.6	0.	0.	317.	0.	0.	.42
N210W4.009	.2	.0	25.6	.0	.02	250.0	22.0	17.0	.6	0.	0.	223.	0.	0.	.49
N210W4.010	.3	.0	24.8	.0	.03	250.0	.0	17.0	.7	0.	0.	216.	0.	0.	.85
N210W5.004	.1	.0	.0	.0	.01	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.35
N210W5.005	.1	.0	.0	.0	.01	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.32
N210W5.006	.1	.0	.0	.0	.02	250.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.42
N210W5.007	.2	.0	.0	.0	.01	250.0	44.0	17.0	.4	0.	0.	0.	0.	0.	.30
N210W5.008	.3	.0	28.8	.0	.03	250.0	28.0	17.0	.7	0.	0.	251.	0.	0.	.78
N210W5.009	.3	.0	28.4	.0	.02	250.0	22.0	17.0	.7	0.	0.	248.	0.	0.	.65
N210W5.010	.3	.0	28.3	.0	.03	250.0	.0	17.0	.7	0.	0.	247.	0.	0.	.89

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215A1.004	.7	.0	12.5	.0	-.02	-62.0	40.0	2.0	1.9	0.	0.	134.	0.	0.	.07
N215A1.005	2.0	8.3	12.1	20.4	.07	-62.0	30.0	2.0	5.3	118.	0.	129.	0.	129.	1.94
N215A1.006	17.4	3.1	7.9	24.7	1.38	-62.0	20.0	2.0	36.2	33.	33.	84.	166.	210.	34.46
N215A1.007	16.5	2.1	7.5	31.0	1.74	-62.0	10.0	2.0	34.7	23.	24.	80.	211.	242.	44.20
N215A1.008	16.6	.9	7.7	28.8	1.85	-62.0	.0	2.0	35.0	11.	18.	82.	203.	249.	46.82
N215A1.009	17.5	1.4	6.9	29.3	1.95	-62.0	-10.0	2.0	36.5	15.	18.	74.	196.	268.	48.79
N215A1.010	13.7	3.3	10.9	29.0	1.46	-62.0	-20.0	2.0	30.1	35.	35.	116.	194.	214.	37.35
N215A2.004	2.3	14.3	14.4	15.2	.00	-62.0	40.0	2.0	6.0	154.	0.	154.	0.	154.	.22
N215A2.005	2.4	8.3	14.3	18.2	.10	-62.0	30.0	2.0	6.2	98.	0.	153.	0.	161.	2.85
N215A2.006	18.5	1.8	8.1	23.3	1.60	-62.0	20.0	2.0	38.0	20.	26.	87.	201.	209.	39.77
N215A2.007	13.6	1.4	7.9	27.5	1.75	-62.0	10.0	2.0	29.8	15.	20.	84.	205.	233.	44.27
N215A2.008	14.6	.7	6.1	30.4	1.97	-62.0	.0	2.0	31.7	15.	26.	65.	232.	250.	49.78
N215A2.009	15.9	1.0	8.1	30.4	1.90	-62.0	-10.0	2.0	33.9	16.	17.	87.	239.	269.	47.85
N215A2.010	13.5	2.5	10.6	31.7	1.52	-62.0	-20.0	2.0	29.7	27.	44.	114.	201.	269.	38.70
N215A3.004	1.2	12.7	12.7	12.8	.01	-62.0	40.0	2.0	3.1	0.	0.	136.	0.	0.	.38
N215A3.005	2.9	7.2	10.3	15.9	.09	-62.0	30.0	2.0	7.5	109.	0.	110.	0.	110.	2.60
N215A3.006	17.3	3.8	8.2	23.8	1.25	-62.0	20.0	2.0	36.0	41.	41.	88.	172.	237.	31.62
N215A3.007	13.8	1.4	9.9	27.3	1.72	-62.0	10.0	2.0	30.2	15.	15.	105.	211.	273.	43.83
N215A3.008	14.2	.9	7.0	31.9	1.98	-62.0	.0	2.0	30.9	10.	13.	75.	213.	265.	49.89
N215A3.009	14.9	1.1	6.9	29.4	1.93	-62.0	-10.0	2.0	32.1	12.	20.	74.	221.	283.	48.86
N215A3.010	11.6	2.5	8.4	29.6	1.39	-62.0	-20.0	2.0	26.2	27.	28.	89.	214.	241.	35.81
N215A4.004	1.3	11.2	11.2	11.2	.01	-62.0	40.0	2.0	3.3	0.	0.	119.	0.	0.	.46
N215A4.005	2.2	6.4	14.4	18.5	.10	-62.0	30.0	2.0	5.8	74.	0.	154.	0.	155.	3.05
N215A4.006	16.6	2.5	6.5	25.9	1.58	-62.0	20.0	2.0	35.0	27.	28.	69.	182.	188.	39.17
N215A4.007	14.6	1.1	7.6	31.9	1.85	-62.0	10.0	2.0	31.5	12.	12.	81.	228.	263.	46.98
N215A4.008	16.1	.9	6.2	31.9	1.99	-62.0	.0	2.0	34.1	10.	16.	66.	225.	277.	50.08
N215A4.009	15.8	1.5	7.5	30.6	2.05	-62.0	-10.0	2.0	33.6	20.	23.	80.	228.	291.	51.42
N215A4.010	16.3	3.2	6.2	26.6	1.67	-62.0	-20.0	2.0	34.5	35.	35.	66.	207.	254.	41.75
N215A5.004	1.4	12.5	12.5	12.6	-.01	-62.0	40.0	2.0	3.7	0.	0.	133.	0.	0.	.33
N215A5.005	2.2	10.4	12.1	23.6	.07	-62.0	30.0	2.0	5.6	129.	0.	129.	0.	130.	2.26
N215A5.006	17.1	2.9	7.7	26.0	1.73	-62.0	20.0	2.0	35.7	32.	32.	83.	207.	219.	42.89
N215A5.007	15.0	.9	6.9	32.3	1.92	-62.0	10.0	2.0	32.4	18.	18.	73.	221.	270.	48.52
N215A5.008	14.1	.5	8.3	32.6	2.10	-62.0	.0	2.0	30.8	10.	11.	89.	237.	297.	53.23
N215A5.009	14.5	1.5	8.7	33.2	2.07	-62.0	-10.0	2.0	31.4	16.	19.	93.	241.	302.	52.31
N215A5.010	14.5	3.0	8.6	38.1	1.67	-62.0	-20.0	2.0	31.4	33.	36.	92.	193.	236.	42.17
N215B1.004	.8	.0	13.1	.0	.03	-32.0	40.0	1.0	2.0	0.	0.	140.	0.	0.	.90
N215B1.005	1.6	11.1	11.2	12.9	.06	-32.0	30.0	1.0	4.2	0.	0.	119.	0.	0.	1.66
N215B1.006	22.3	.7	2.2	24.0	1.85	-32.0	20.0	1.0	43.6	7.	18.	23.	197.	222.	45.23
N215B1.007	21.1	.1	6.1	26.8	1.89	-32.0	10.0	1.0	41.9	1.	1.	65.	198.	204.	45.83
N215B1.008	20.4	.3	7.2	21.1	1.41	-32.0	.0	1.0	40.9	3.	4.	77.	124.	215.	34.66
N215B1.009	15.9	.1	1.2	18.0	.79	-32.0	-10.0	1.0	33.8	1.	1.	13.	104.	157.	20.59
N215B1.010	14.6	1.1	10.8	21.0	1.25	-32.0	-20.0	1.0	31.7	15.	15.	115.	145.	184.	31.55

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215B2.004	1.4	10.2	10.9	11.7	.06	-32.0	40.0	1.0	3.7	0.	0.	116.	0.	0.	1.76
N215B2.005	1.1	10.7	10.9	11.2	.09	-32.0	30.0	1.0	3.0	0.	0.	117.	0.	0.	2.57
N215B2.006	20.6	.7	7.4	24.8	1.36	-32.0	20.0	1.0	41.1	17.	20.	79.	177.	201.	34.17
N215B2.007	20.8	.1	4.3	32.3	1.63	-32.0	10.0	1.0	41.6	1.	1.	46.	137.	216.	39.70
N215B2.008	18.7	.2	8.7	19.7	1.17	-32.0	.0	1.0	38.3	2.	2.	93.	107.	148.	29.29
N215B2.009	21.7	.1	8.5	22.2	1.00	-32.0	-10.0	1.0	42.8	1.	1.	91.	113.	167.	25.21
N215B2.010	16.6	.4	7.4	56.6	1.53	-32.0	-20.0	1.0	34.9	6.	26.	79.	176.	226.	38.36
N215B3.004	1.1	11.1	11.1	11.2	.04	-32.0	40.0	1.0	3.0	0.	0.	119.	0.	0.	1.21
N215B3.005	1.1	9.3	10.6	13.9	.09	-32.0	30.0	1.0	3.0	0.	0.	113.	0.	0.	2.55
N215B3.006	23.8	1.3	6.2	24.8	1.52	-32.0	20.0	1.0	45.8	23.	26.	66.	168.	256.	38.15
N215B3.007	23.8	.1	7.8	15.1	.49	-32.0	10.0	1.0	45.8	1.	2.	83.	161.	161.	41.28
N215B3.008	15.8	.2	7.0	20.8	1.10	-32.0	.0	1.0	33.7	2.	2.	74.	112.	134.	28.13
N215B3.009	18.2	.1	2.8	24.5	.89	-32.0	-10.0	1.0	37.5	1.	1.	30.	137.	174.	22.89
N215B3.010	20.6	.7	7.9	21.5	1.51	-32.0	-20.0	1.0	41.2	7.	25.	84.	170.	228.	37.47
N215B4.004	1.0	13.1	13.1	13.1	.03	-32.0	40.0	1.0	2.7	0.	0.	140.	0.	0.	.99
N215B4.005	1.0	12.1	12.1	12.2	.06	-32.0	30.0	1.0	2.8	0.	0.	130.	0.	0.	1.85
N215B4.006	17.9	.5	3.7	34.5	1.46	-32.0	20.0	1.0	37.0	5.	9.	39.	142.	236.	36.93
N215B4.007	18.7	.1	5.7	35.1	1.89	-32.0	10.0	1.0	38.4	1.	1.	61.	181.	298.	46.26
N215B4.008	18.9	.2	6.2	22.7	1.35	-32.0	.0	1.0	38.6	2.	3.	66.	116.	175.	33.51
N215B4.009	18.0	.1	4.2	21.9	1.10	-32.0	-10.0	1.0	37.2	1.	1.	45.	120.	185.	27.88
N215B4.010	23.4	1.2	8.2	27.3	1.71	-32.0	-20.0	1.0	45.2	15.	28.	88.	196.	242.	41.45
N215B5.004	1.7	9.4	9.5	9.8	.03	-32.0	40.0	1.0	4.4	0.	0.	101.	0.	0.	1.11
N215B5.005	1.5	9.4	9.7	11.3	.08	-32.0	30.0	1.0	4.1	0.	0.	103.	0.	0.	2.41
N215B5.006	18.4	.5	4.3	25.4	1.20	-32.0	20.0	1.0	37.8	7.	11.	46.	105.	213.	30.05
N215B5.007	20.6	.1	7.7	23.0	1.48	-32.0	10.0	1.0	41.2	1.	1.	82.	189.	245.	37.30
N215B5.008	16.4	.2	6.5	21.0	1.13	-32.0	.0	1.0	34.6	2.	2.	69.	109.	140.	28.32
N215B5.009	19.5	.1	6.1	24.3	.94	-32.0	-10.0	1.0	39.6	1.	1.	65.	95.	148.	23.95
N215B5.010	21.3	.4	7.8	25.8	1.64	-32.0	-20.0	1.0	42.3	10.	29.	83.	193.	238.	40.90
N215C1.004	1.9	10.0	10.5	10.7	.05	-2.0	40.0	1.0	5.0	0.	0.	112.	0.	0.	1.47
N215C1.005	1.3	9.3	10.5	14.3	.07	-2.0	30.0	1.0	3.4	0.	0.	112.	0.	0.	1.94
N215C1.006	11.7	2.4	7.4	19.5	.86	-2.0	20.0	1.0	26.4	35.	38.	79.	142.	172.	22.49
N215C1.007	11.3	1.4	8.0	18.3	.79	-2.0	10.0	1.0	25.5	15.	21.	86.	101.	130.	20.57
N215C1.008	7.9	2.3	5.8	16.5	.45	-2.0	.0	1.0	18.8	38.	40.	61.	69.	103.	12.15
N215C1.009	5.3	2.2	6.1	18.1	.31	-2.0	-10.0	1.0	13.1	31.	61.	66.	67.	103.	8.71
N215C1.010	9.7	2.6	6.5	17.4	.42	-2.0	-20.0	1.0	22.6	28.	30.	69.	89.	110.	11.49
N215C2.004	1.2	9.8	12.4	15.0	.05	-2.0	40.0	1.0	3.2	0.	0.	133.	0.	0.	1.58
N215C2.005	1.2	9.8	9.8	12.7	.08	-2.0	30.0	1.0	3.2	0.	0.	104.	0.	0.	2.30
N215C2.006	9.8	2.7	7.3	19.0	.97	-2.0	20.0	1.0	22.6	38.	39.	78.	156.	181.	25.51
N215C2.007	13.6	3.4	4.4	20.9	.89	-2.0	10.0	1.0	29.9	36.	36.	47.	128.	136.	22.73
N215C2.008	14.4	2.7	7.2	16.1	.45	-2.0	.0	1.0	31.2	30.	32.	77.	89.	121.	12.06
N215C2.009	13.4	2.5	7.5	16.1	.41	-2.0	-10.0	1.0	29.5	27.	71.	80.	89.	117.	11.28
N215C2.010	8.9	2.9	8.3	16.8	.40	-2.0	-20.0	1.0	20.8	62.	63.	89.	96.	177.	11.10

FALCON 2: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215C3.004	1.1	9.0	10.2	13.2	.06	-2.0	40.0	1.0	2.8	0.	0.	108.	0.	0.	1.92
N215C3.005	1.2	8.8	11.5	14.6	.12	-2.0	30.0	1.0	3.3	0.	0.	123.	0.	0.	3.31
N215C3.006	10.0	3.3	6.2	22.9	.71	-2.0	20.0	1.0	23.2	54.	55.	66.	102.	187.	18.85
N215C3.007	11.3	1.4	6.9	22.5	.57	-2.0	10.0	1.0	25.6	17.	53.	73.	88.	144.	15.44
N215C3.008	8.4	2.0	7.1	22.6	.54	-2.0	.0	1.0	19.8	32.	32.	76.	90.	137.	14.79
N215C3.009	14.1	1.5	8.0	20.5	.79	-2.0	-10.0	1.0	30.6	16.	17.	85.	101.	129.	20.34
N215C3.010	10.8	1.9	9.7	20.2	.79	-2.0	-20.0	1.0	24.6	23.	43.	104.	124.	148.	20.74
N215C4.004	1.0	.0	14.2	.0	.06	-2.0	40.0	1.0	2.6	0.	0.	152.	0.	0.	1.72
N215C4.005	1.3	3.7	13.8	14.5	.09	-2.0	30.0	1.0	3.5	0.	0.	147.	0.	0.	2.64
N215C4.006	9.5	2.1	8.1	20.2	.91	-2.0	20.0	1.0	22.2	24.	37.	86.	132.	161.	23.86
N215C4.007	13.8	1.6	7.1	20.1	.55	-2.0	10.0	1.0	30.1	30.	33.	76.	95.	96.	14.62
N215C4.008	12.1	1.5	7.8	17.1	.32	-2.0	.0	1.0	27.1	59.	80.	83.	90.	105.	8.81
N215C4.009	10.4	1.1	7.5	17.9	.34	-2.0	-10.0	1.0	23.9	77.	78.	80.	92.	95.	9.40
N215C4.010	4.7	1.6	8.4	18.1	.32	-2.0	-20.0	1.0	11.7	18.	86.	89.	93.	97.	8.96
N215C5.004	2.0	9.6	9.7	13.2	.03	-2.0	40.0	1.0	5.1	103.	0.	103.	0.	103.	1.00
N215C5.005	1.5	9.8	9.8	12.6	.05	-2.0	30.0	1.0	4.1	0.	0.	105.	0.	0.	1.56
N215C5.006	8.0	2.4	9.2	19.2	.61	-2.0	20.0	1.0	19.0	44.	76.	98.	118.	161.	16.61
N215C5.007	9.7	.8	6.8	17.6	.55	-2.0	10.0	1.0	22.4	22.	38.	72.	100.	155.	15.00
N215C5.008	10.3	3.0	6.4	17.3	.40	-2.0	.0	1.0	23.7	33.	34.	68.	85.	132.	11.02
N215C5.009	3.9	2.6	2.7	13.7	.28	-2.0	-10.0	1.0	9.9	28.	0.	28.	0.	129.	8.05
N215C5.010	8.4	3.1	6.5	16.2	.42	-2.0	-20.0	1.0	19.9	37.	53.	69.	90.	131.	11.63
N215D1.004	.1	.0	.0	.0	-.01	50.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.12
N215D1.005	.0	.0	.0	.0	-.02	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.06
N215D1.006	.1	.0	.0	.0	.01	50.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.42
N215D1.007	.3	.0	12.2	.0	.04	50.0	44.0	1.0	.7	0.	0.	130.	0.	0.	1.25
N215D1.008	.6	.0	10.6	.0	.04	50.0	28.0	1.0	1.6	0.	0.	113.	0.	0.	1.30
N215D1.009	.9	.0	10.7	.0	.06	50.0	22.0	1.0	2.5	0.	0.	114.	0.	0.	1.83
N215D1.010	1.1	10.6	12.1	12.3	.14	50.0	.0	1.0	2.8	0.	0.	130.	0.	0.	4.09
N215D2.004	.1	.0	.0	.0	.02	50.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.84
N215D2.005	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.19
N215D2.006	.1	.0	.0	.0	.00	50.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.19
N215D2.007	.5	.0	14.8	.0	.03	50.0	44.0	1.0	1.2	0.	0.	158.	0.	0.	1.00
N215D2.008	.8	.0	7.8	.0	.04	50.0	28.0	1.0	2.1	0.	0.	83.	0.	0.	1.15
N215D2.009	.9	.0	8.9	.0	.07	50.0	22.0	1.0	2.4	0.	0.	95.	0.	0.	2.04
N215D2.010	.9	.0	7.6	.0	.13	50.0	.0	1.0	2.3	0.	0.	81.	0.	0.	3.83
N215D3.004	.1	.0	.0	.0	-.01	50.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.15
N215D3.005	.1	.0	.0	.0	.01	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.28
N215D3.006	.1	.0	.0	.0	.00	50.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.33
N215D3.007	.3	.0	16.1	.0	.05	50.0	44.0	1.0	.7	0.	0.	172.	0.	0.	1.39
N215D3.008	.7	.0	7.5	.0	.03	50.0	28.0	1.0	1.9	0.	0.	80.	0.	0.	.98
N215D3.009	1.5	9.2	9.2	9.3	.05	50.0	22.0	1.0	3.9	0.	0.	98.	0.	0.	1.61
N215D3.010	1.2	8.2	8.2	8.3	.14	50.0	.0	1.0	3.2	0.	0.	88.	0.	0.	4.06

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215D4.004	.0	.0	.0	.0	-.01	50.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.08
N215D4.005	.1	.0	.0	.0	.00	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.17
N215D4.006	.1	.0	.0	.0	-.01	50.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.13
N215D4.007	.1	.0	.0	.0	.00	50.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.26
N215D4.008	.7	.0	10.7	.0	.03	50.0	28.0	1.0	1.9	0.	0.	114.	0.	0.	1.08
N215D4.009	1.3	9.7	9.8	10.7	.07	50.0	22.0	1.0	3.4	0.	0.	104.	0.	0.	2.08
N215D4.010	.9	.0	11.4	.0	.13	50.0	.0	1.0	2.4	0.	0.	122.	0.	0.	3.60
N215D5.004	.1	.0	.0	.0	-.02	50.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.02
N215D5.005	.1	.0	.0	.0	-.01	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.07
N215D5.006	.1	.0	.0	.0	.01	50.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.29
N215D5.007	.1	.0	.0	.0	.01	50.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.37
N215D5.008	1.0	10.4	10.4	10.4	.03	50.0	28.0	1.0	2.8	0.	0.	111.	0.	0.	.85
N215D5.009	1.3	8.3	8.3	10.4	.08	50.0	22.0	1.0	3.4	0.	0.	89.	0.	0.	2.35
N215D5.010	1.1	10.1	10.1	10.1	.17	50.0	.0	1.0	2.8	0.	0.	108.	0.	0.	4.84
N215E1.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.36
N215E1.005	.1	.0	.0	.0	.01	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.25
N215E1.006	.2	.0	13.9	.0	.00	50.0	56.0	5.0	.6	0.	0.	148.	0.	0.	.05
N215E1.007	.1	.0	.0	.0	-.59	50.0	44.0	5.0	.2	0.	0.	0.	0.	0.	.08
N215E1.008	1.0	12.2	12.2	12.3	.01	50.0	28.0	5.0	2.7	0.	0.	130.	0.	0.	.62
N215E1.009	1.0	12.3	12.3	12.4	.06	50.0	22.0	5.0	2.7	0.	0.	132.	0.	0.	1.78
N215E1.010	1.0	.0	14.2	.0	.16	50.0	.0	5.0	2.6	0.	0.	151.	0.	0.	4.58
N215E2.004	.1	.0	.0	.0	-.01	50.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.08
N215E2.005	.1	.0	.0	.0	-.02	50.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.05
N215E2.006	.1	.0	.0	.0	-.01	50.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.08
N215E2.007	.4	.0	20.6	.0	.05	50.0	44.0	5.0	1.0	0.	0.	220.	0.	0.	1.59
N215E2.008	.7	.0	5.9	.0	.02	50.0	28.0	5.0	2.0	0.	0.	63.	0.	0.	.74
N215E2.009	1.3	6.0	6.0	6.1	.06	50.0	22.0	5.0	3.4	0.	0.	64.	0.	0.	1.76
N215E2.010	.9	.0	12.3	.0	.16	50.0	.0	5.0	2.4	0.	0.	132.	0.	0.	4.67
N215E3.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.23
N215E3.005	.1	.0	.0	.0	-.01	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.00
N215E3.006	.1	.0	.0	.0	-.01	50.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.05
N215E3.007	.2	.0	.0	.0	-.02	50.0	44.0	5.0	.4	0.	0.	0.	0.	0.	.11
N215E3.008	1.2	11.9	12.0	12.0	.02	50.0	28.0	5.0	3.1	0.	0.	128.	0.	0.	.73
N215E3.009	1.5	10.2	10.3	11.9	.06	50.0	22.0	5.0	3.9	0.	0.	110.	0.	0.	1.87
N215E3.010	1.1	12.8	12.8	12.8	.11	50.0	.0	5.0	2.8	0.	0.	137.	0.	0.	3.28
N215E4.004	.1	.0	.0	.0	-.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.12
N215E4.005	.0	.0	.0	.0	-.02	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.00
N215E4.006	.1	.0	.0	.0	.00	50.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.07
N215E4.007	.2	.0	.0	.0	.02	50.0	44.0	5.0	.4	0.	0.	0.	0.	0.	.84
N215E4.008	1.6	9.2	9.4	9.4	.03	50.0	28.0	5.0	4.3	0.	0.	100.	0.	0.	.94
N215E4.009	1.4	8.7	8.9	8.9	.07	50.0	22.0	5.0	3.6	0.	0.	95.	0.	0.	1.98
N215E4.010	1.0	.0	9.4	.0	.11	50.0	.0	5.0	2.6	0.	0.	100.	0.	0.	3.28

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215E5.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.28
N215E5.005	.1	.0	.0	.0	.01	50.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.30
N215E5.006	.1	.0	.0	.0	.00	50.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.10
N215E5.007	.5	.0	18.5	.0	.06	50.0	44.0	5.0	1.2	0.	0.	197.	0.	0.	1.83
N215E5.008	1.1	12.6	12.6	12.7	.03	50.0	28.0	5.0	2.9	0.	0.	135.	0.	0.	1.06
N215E5.009	1.2	8.8	8.8	12.8	.08	50.0	22.0	5.0	3.1	0.	0.	94.	0.	0.	2.48
N215E5.010	1.2	8.6	8.6	9.4	.15	50.0	.0	5.0	3.2	0.	0.	92.	0.	0.	4.41
N215F1.004	.1	.0	.0	.0	.00	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.03
N215F1.005	.1	.0	.0	.0	.00	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.07
N215F1.006	.1	.0	.0	.0	.01	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.30
N215F1.007	.2	.0	.0	.0	-.14	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.19
N215F1.008	.7	.0	12.3	.0	.03	50.0	28.0	11.0	1.9	0.	0.	131.	0.	0.	1.00
N215F1.009	1.2	5.0	5.1	9.5	.07	50.0	22.0	11.0	3.1	0.	0.	54.	0.	0.	1.97
N215F1.010	1.1	12.3	12.5	12.6	.15	50.0	.0	11.0	2.9	0.	0.	134.	0.	0.	4.32
N215F2.004	.1	.0	.0	.0	.00	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.23
N215F2.005	.1	.0	.0	.0	.00	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.20
N215F2.006	.1	.0	.0	.0	.00	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.01
N215F2.007	.1	.0	.0	.0	-.03	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.23
N215F2.008	.6	.0	7.5	.0	.00	50.0	28.0	11.0	1.7	0.	0.	80.	0.	0.	.46
N215F2.009	1.6	8.2	8.2	8.4	.05	50.0	22.0	11.0	4.2	0.	0.	88.	0.	0.	1.64
N215F2.010	1.0	5.0	5.0	5.1	.13	50.0	.0	11.0	2.7	0.	0.	54.	0.	0.	3.73
N215F3.004	.1	.0	.0	.0	.01	50.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.44
N215F3.005	.1	.0	.0	.0	.00	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.08
N215F3.006	.1	.0	.0	.0	.01	50.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.50
N215F3.007	.2	.0	7.8	.0	.06	50.0	44.0	11.0	.6	0.	0.	84.	0.	0.	1.87
N215F3.008	1.4	7.6	7.7	7.7	-.01	50.0	28.0	11.0	3.8	0.	0.	82.	0.	0.	.34
N215F3.009	1.1	12.2	12.2	12.2	.03	50.0	22.0	11.0	2.9	0.	0.	130.	0.	0.	1.13
N215F3.010	1.0	9.0	9.0	10.7	.10	50.0	.0	11.0	2.7	0.	0.	96.	0.	0.	2.99
N215F4.004	.1	.0	.0	.0	.00	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.03
N215F4.005	.0	.0	.0	.0	.01	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.27
N215F4.006	.1	.0	.0	.0	.02	50.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.49
N215F4.007	.2	.0	14.5	.0	-.06	50.0	44.0	11.0	.6	0.	0.	155.	0.	0.	.08
N215F4.008	.9	.0	7.3	.0	.01	50.0	28.0	11.0	2.4	0.	0.	78.	0.	0.	.41
N215F4.009	.8	.0	6.7	.0	.04	50.0	22.0	11.0	2.0	0.	0.	71.	0.	0.	1.36
N215F4.010	1.4	7.5	7.5	8.1	.13	50.0	.0	11.0	3.6	0.	0.	80.	0.	0.	3.76
N215F5.004	.1	.0	.0	.0	.00	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.05
N215F5.005	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.38
N215F5.006	.1	.0	.0	.0	.00	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.06
N215F5.007	.2	.0	.0	.0	-.07	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.29
N215F5.008	.9	.0	13.2	.0	.00	50.0	28.0	11.0	2.5	0.	0.	141.	0.	0.	.55
N215F5.009	.9	.0	10.8	.0	.05	50.0	22.0	11.0	2.5	0.	0.	115.	0.	0.	1.63
N215F5.010	1.0	13.8	13.8	13.8	.13	50.0	.0	11.0	2.7	0.	0.	147.	0.	0.	3.66

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215G1.004	.1	.0	.0	.0	.00	50.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.12
N215G1.005	.0	.0	.0	.0	-.01	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.02
N215G1.006	.0	.0	.0	.0	-.03	50.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.01
N215G1.007	.1	.0	.0	.0	-.01	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.11
N215G1.008	.9	.0	13.4	.0	.01	50.0	28.0	17.0	2.3	0.	0.	143.	0.	0.	.53
N215G1.009	1.3	9.3	11.7	11.7	.03	50.0	22.0	17.0	3.3	0.	0.	125.	0.	0.	1.06
N215G1.010	1.0	7.7	7.7	7.8	.06	50.0	.0	17.0	2.7	0.	0.	83.	0.	0.	2.05
N215G2.004	.0	.0	.0	.0	-.01	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.15
N215G2.005	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.06
N215G2.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.22
N215G2.007	.2	.0	5.3	.0	-.05	50.0	44.0	17.0	.5	0.	0.	56.	0.	0.	.06
N215G2.008	.8	.0	16.4	.0	.01	50.0	28.0	17.0	2.3	0.	0.	175.	0.	0.	.25
N215G2.009	.9	.0	7.0	.0	.03	50.0	22.0	17.0	2.3	0.	0.	75.	0.	0.	.85
N215G2.010	1.8	8.1	8.1	10.9	.07	50.0	.0	17.0	4.6	0.	0.	86.	0.	0.	2.18
N215G3.004	.1	.0	.0	.0	.01	50.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.32
N215G3.005	.1	.0	.0	.0	.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.38
N215G3.006	.1	.0	.0	.0	-.01	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.05
N215G3.007	.2	.0	.0	.0	-.02	50.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.07
N215G3.008	1.0	.0	5.6	.0	.01	50.0	28.0	17.0	2.6	0.	0.	59.	0.	0.	.34
N215G3.009	.8	.0	13.9	.0	.02	50.0	22.0	17.0	2.2	0.	0.	149.	0.	0.	.87
N215G3.010	1.3	5.8	7.6	9.7	.06	50.0	.0	17.0	3.4	0.	0.	81.	0.	0.	2.02
N215G4.004	.1	.0	.0	.0	.01	50.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.44
N215G4.005	.1	.0	.0	.0	.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.16
N215G4.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.25
N215G4.007	.0	.0	.0	.0	-.08	50.0	44.0	17.0	.1	0.	0.	0.	0.	0.	.02
N215G4.008	.6	.0	8.4	.0	-.01	50.0	28.0	17.0	1.7	0.	0.	90.	0.	0.	.18
N215G4.009	1.5	10.4	10.4	10.5	.01	50.0	22.0	17.0	3.9	0.	0.	111.	0.	0.	.69
N215G4.010	.9	.0	5.9	.0	.07	50.0	.0	17.0	2.4	0.	0.	63.	0.	0.	2.12
N215G5.004	.1	.0	.0	.0	-.01	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.02
N215G5.005	.1	.0	.0	.0	.00	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.14
N215G5.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.06
N215G5.007	.1	.0	.0	.0	-.27	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.08
N215G5.008	1.1	3.9	4.0	4.0	.03	50.0	28.0	17.0	2.9	0.	0.	42.	0.	0.	.88
N215G5.009	1.1	6.8	6.8	6.8	.04	50.0	22.0	17.0	3.0	0.	0.	72.	0.	0.	1.33
N215G5.010	1.1	9.0	9.0	9.2	.11	50.0	.0	17.0	2.8	0.	0.	96.	0.	0.	3.30
N215H1.004	1.3	10.4	10.8	11.1	.14	50.0	.0	1.0	3.3	0.	0.	115.	0.	0.	4.13
N215H1.005	1.0	.0	8.3	.0	.06	50.0	-22.0	1.0	2.6	0.	0.	89.	0.	0.	1.77
N215H1.006	.5	.0	18.6	.0	.05	50.0	-28.0	1.0	1.4	0.	0.	198.	0.	0.	1.32
N215H1.007	.2	.0	.0	.0	.03	50.0	-44.0	1.0	.4	0.	0.	0.	0.	0.	1.03
N215H1.008	.1	.0	.0	.0	.01	50.0	-56.0	1.0	.1	0.	0.	0.	0.	0.	.37
N215H1.009	.1	.0	.0	.0	.01	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.39
N215H1.010	.1	.0	.0	.0	.01	50.0	-75.0	1.0	.3	0.	0.	0.	0.	0.	.48

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215H2.004	.8	.0	11.6	.0	.16	50.0	.0	1.0	2.0	0.	0.	124.	0.	0.	4.50
N215H2.005	.7	.0	11.3	.0	.08	50.0	-22.0	1.0	1.9	0.	0.	121.	0.	0.	2.24
N215H2.006	.6	.0	8.5	.0	.05	50.0	-28.0	1.0	1.7	0.	0.	91.	0.	0.	1,47
N215H2.007	.2	.0	.0	.0	.01	50.0	-44.0	1.0	.5	0.	0.	0.	0.	0.	.70
N215H2.008	.1	.0	.0	.0	.00	50.0	-56.0	1.0	.2	0.	0.	0.	0.	0.	.28
N215H2.009	.1	.0	.0	.0	.01	50.0	-66.0	1.0	.3	0.	0.	0.	0.	0.	.23
N215H2.010	.1	.0	.0	.0	.01	50.0	-75.0	1.0	.2	0.	0.	0.	0.	0.	.31
N215H3.004	.9	.0	16.2	.0	.17	50.0	.0	1.0	2.4	0.	0.	173.	0.	0.	4.76
N215H3.005	1.0	.0	12.0	.0	.08	50.0	-22.0	1.0	2.6	0.	0.	128.	0.	0.	2.21
N215H3.006	.9	.0	5.9	.0	.05	50.0	-28.0	1.0	2.5	0.	0.	63.	0.	0.	1.69
N215H3.007	.6	.0	15.4	.0	.01	50.0	-44.0	1.0	1.5	0.	0.	165.	0.	0.	.53
N215H3.008	.3	.0	16.3	.0	.01	50.0	-56.0	1.0	.9	0.	0.	174.	0.	0.	.37
N215H3.009	.1	.0	.0	.0	.01	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.38
N215H3.010	.1	.0	.0	.0	.03	50.0	-75.0	1.0	.3	0.	0.	0.	0.	0.	.88
N215H4.004	.9	.0	11.1	.0	.15	50.0	.0	1.0	2.4	0.	0.	118.	0.	0.	4.29
N215H4.005	.9	.0	9.5	.0	.06	50.0	-22.0	1.0	2.5	0.	0.	101.	0.	0.	1.90
N215H4.006	1.2	9.1	9.2	9.2	.05	50.0	-28.0	1.0	3.1	0.	0.	98.	0.	0.	1.58
N215H4.007	.1	.0	.0	.0	-.03	50.0	-44.0	1.0	.3	0.	0.	0.	0.	0.	.02
N215H4.008	.0	.0	.0	.0	-.01	50.0	-56.0	1.0	.1	0.	0.	0.	0.	0.	.13
N215H4.009	.1	.0	.0	.0	.01	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.25
N215H4.010	.1	.0	.0	.0	.00	50.0	-75.0	1.0	.3	0.	0.	0.	0.	0.	.25
N215H5.004	1.0	.0	12.5	.0	.16	50.0	.0	1.0	2.6	0.	0.	133.	0.	0.	4.51
N215H5.005	.9	.0	9.5	.0	.08	50.0	-22.0	1.0	2.5	0.	0.	102.	0.	0.	2.50
N215H5.006	.7	.0	6.8	.0	.06	50.0	-28.0	1.0	1.9	0.	0.	73.	0.	0.	1.69
N215H5.007	.2	.0	.0	.0	.04	50.0	-44.0	1.0	.5	0.	0.	0.	0.	0.	1.24
N215H5.008	.1	.0	.0	.0	.01	50.0	-56.0	1.0	.2	0.	0.	0.	0.	0.	.43
N215H5.009	.1	.0	.0	.0	.01	50.0	-66.0	1.0	.3	0.	0.	0.	0.	0.	.39
N215H5.010	.1	.0	.0	.0	.00	50.0	-75.0	1.0	.2	0.	0.	0.	0.	0.	.21
N215I1.004	1.0	.0	13.0	.0	.11	50.0	.0	5.0	2.6	0.	0.	139.	0.	0.	3.41
N215I1.005	1.0	.0	12.1	.0	.07	50.0	-22.0	5.0	2.6	0.	0.	129.	0.	0.	2.12
N215I1.006	1.0	13.9	13.9	14.0	.04	50.0	-28.0	5.0	2.7	0.	0.	149.	0.	0.	1.22
N215I1.007	.5	.0	20.6	.0	.01	50.0	-44.0	5.0	1.2	0.	0.	220.	0.	0.	.32
N215I1.008	.0	.0	.0	.0	.00	50.0	-56.0	5.0	.1	0.	0.	0.	0.	0.	.20
N215I1.009	.1	.0	.0	.0	-.02	50.0	-66.0	5.0	.2	0.	0.	0.	0.	0.	.07
N215I1.010	.0	.0	.0	.0	-.03	50.0	-75.0	5.0	.1	0.	0.	0.	0.	0.	.02
N215I2.004	1.0	.0	12.9	.0	.14	50.0	.0	5.0	2.6	0.	0.	137.	0.	0.	4.01
N215I2.005	.8	.0	11.3	.0	.06	50.0	-22.0	5.0	2.2	0.	0.	120.	0.	0.	1.80
N215I2.006	.6	.0	14.3	.0	.03	50.0	-28.0	5.0	1.7	0.	0.	152.	0.	0.	.88
N215I2.007	.1	.0	.0	.0	.02	50.0	-44.0	5.0	.3	0.	0.	0.	0.	0.	.55
N215I2.008	.1	.0	.0	.0	.01	50.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.36
N215I2.009	.1	.0	.0	.0	.02	50.0	-66.0	5.0	.3	0.	0.	0.	0.	0.	.63
N215I2.010	.1	.0	.0	.0	.02	50.0	-75.0	5.0	.2	0.	0.	0.	0.	0.	.65

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215I3.004	.9	.0	10.9	.0	.13	50.0	.0	5.0	2.5	0.	0.	116.	0.	0.	3.87
N215I3.005	1.1	9.6	9.6	9.7	.06	50.0	-22.0	5.0	3.0	0.	0.	103.	0.	0.	1.86
N215I3.006	1.0	8.7	8.7	8.7	.04	50.0	-28.0	5.0	2.8	0.	0.	93.	0.	0.	1.29
N215I3.007	.2	.0	.0	.0	.04	50.0	-44.0	5.0	.5	0.	0.	0.	0.	0.	1.11
N215I3.008	.1	.0	.0	.0	.00	50.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.04
N215I3.009	.1	.0	.0	.0	.01	50.0	-66.0	5.0	.3	0.	0.	0.	0.	0.	.48
N215I3.010	.1	.0	.0	.0	.01	50.0	-75.0	5.0	.2	0.	0.	0.	0.	0.	.28
N215I4.004	1.2	12.1	14.5	14.5	.16	50.0	.0	5.0	3.1	0.	0.	155.	0.	0.	4.52
N215I4.005	1.0	8.3	8.3	8.3	.07	50.0	-22.0	5.0	2.7	0.	0.	88.	0.	0.	2.02
N215I4.006	.8	.0	16.9	.0	.03	50.0	-28.0	5.0	2.0	0.	0.	180.	0.	0.	.88
N215I4.007	.1	.0	.0	.0	.01	50.0	-44.0	5.0	.3	0.	0.	0.	0.	0.	.50
N215I4.008	.1	.0	.0	.0	.00	50.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.29
N215I4.009	.1	.0	.0	.0	.02	50.0	-66.0	5.0	.3	0.	0.	0.	0.	0.	.59
N215I4.010	.1	.0	.0	.0	.04	50.0	-75.0	5.0	.3	0.	0.	0.	0.	0.	1.16
N215I5.004	1.2	9.8	9.8	9.8	.14	50.0	.0	5.0	3.2	0.	0.	104.	0.	0.	3.92
N215I5.005	.7	.0	10.9	.0	.07	50.0	-22.0	5.0	1.9	0.	0.	116.	0.	0.	2.11
N215I5.006	.9	.0	9.5	.0	.04	50.0	-28.0	5.0	2.5	0.	0.	102.	0.	0.	1.12
N215I5.007	.1	.0	.0	.0	-.04	50.0	-44.0	5.0	.2	0.	0.	0.	0.	0.	.07
N215I5.008	.1	.0	.0	.0	.00	50.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.23
N215I5.009	.1	.0	.0	.0	-.01	50.0	-66.0	5.0	.2	0.	0.	0.	0.	0.	.10
N215I5.010	.0	.0	.0	.0	.00	50.0	-75.0	5.0	.1	0.	0.	0.	0.	0.	.15
N215J1.004	1.4	9.3	9.3	9.5	.09	50.0	.0	11.0	3.8	0.	0.	100.	0.	0.	2.80
N215J1.005	1.3	9.4	9.5	9.5	.05	50.0	-22.0	11.0	3.5	0.	0.	101.	0.	0.	1.39
N215J1.006	.8	.0	16.4	.0	.00	50.0	-28.0	11.0	2.2	0.	0.	176.	0.	0.	.44
N215J1.007	.2	.0	31.0	.0	.00	50.0	-44.0	11.0	.6	0.	0.	331.	0.	0.	.37
N215J1.008	.1	.0	.0	.0	.00	50.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.00
N215J1.009	.1	.0	.0	.0	.01	50.0	-66.0	11.0	.4	0.	0.	0.	0.	0.	.23
N215J1.010	.1	.0	.0	.0	.01	50.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.47
N215J2.004	.9	.0	11.9	.0	.12	50.0	.0	11.0	2.4	0.	0.	127.	0.	0.	3.43
N215J2.005	1.0	11.8	11.8	11.8	.06	50.0	-22.0	11.0	2.7	0.	0.	126.	0.	0.	1.75
N215J2.006	.9	.0	18.0	.0	.03	50.0	-28.0	11.0	2.5	0.	0.	192.	0.	0.	.72
N215J2.007	.2	.0	.0	.0	.04	50.0	-44.0	11.0	.5	0.	0.	0.	0.	0.	1.05
N215J2.008	.1	.0	.0	.0	.00	50.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.04
N215J2.009	.1	.0	.0	.0	.01	50.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.34
N215J2.010	.1	.0	.0	.0	.03	50.0	-75.0	11.0	.3	0.	0.	0.	0.	0.	.75
N215J3.004	1.7	7.1	8.7	8.8	.10	50.0	.0	11.0	4.5	0.	0.	93.	0.	0.	3.02
N215J3.005	1.1	5.9	5.9	8.2	.05	50.0	-22.0	11.0	2.9	0.	0.	63.	0.	0.	1.37
N215J3.006	.8	.0	14.9	.0	.00	50.0	-28.0	11.0	2.1	0.	0.	159.	0.	0.	.46
N215J3.007	.3	.0	37.8	.0	.02	50.0	-44.0	11.0	.7	0.	0.	403.	0.	0.	.73
N215J3.008	.1	.0	.0	.0	-.01	50.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.06
N215J3.009	.1	.0	.0	.0	.00	50.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.26
N215J3.010	.1	.0	.0	.0	.03	50.0	-75.0	11.0	.3	0.	0.	0.	0.	0.	.89

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215J4.004	1.0	.0	10.3	.0	.10	50.0	.0	11.0	2.6	0.	0.	110.	0.	0.	2.98
N215J4.005	1.0	.0	9.4	.0	.06	50.0	-22.0	11.0	2.6	0.	0.	100.	0.	0.	1.70
N215J4.006	.9	.0	15.8	.0	.03	50.0	-28.0	11.0	2.4	0.	0.	169.	0.	0.	.83
N215J4.007	.2	.0	39.3	.0	.03	50.0	-44.0	11.0	.6	0.	0.	420.	0.	0.	.93
N215J4.008	.1	.0	.0	.0	.00	50.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.11
N215J4.009	.1	.0	.0	.0	.00	50.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.22
N215J4.010	.0	.0	.0	.0	.00	50.0	-75.0	11.0	.1	0.	0.	0.	0.	0.	.09
N215J5.004	.9	.0	10.1	.0	.09	50.0	.0	11.0	2.4	0.	0.	107.	0.	0.	2.67
N215J5.005	1.4	10.3	10.3	13.4	.06	50.0	-22.0	11.0	3.6	0.	0.	110.	0.	0.	1.85
N215J5.006	1.0	.0	10.2	.0	.03	50.0	-28.0	11.0	2.6	0.	0.	109.	0.	0.	.89
N215J5.007	.2	.0	.0	.0	.00	50.0	-44.0	11.0	.5	0.	0.	0.	0.	0.	.23
N215J5.008	.1	.0	.0	.0	.00	50.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.00
N215J5.009	.1	.0	.0	.0	.00	50.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.12
N215J5.010	.0	.0	.0	.0	.00	50.0	-75.0	11.0	.0	0.	0.	0.	0.	0.	.00
N215K1.004	1.4	9.1	9.1	14.3	.08	50.0	.0	17.0	3.7	0.	0.	97.	0.	0.	2.45
N215K1.005	.9	.0	14.2	.0	.03	50.0	-22.0	17.0	2.3	0.	0.	152.	0.	0.	1.05
N215K1.006	1.2	12.2	12.2	12.2	.02	50.0	-28.0	17.0	3.2	0.	0.	130.	0.	0.	.75
N215K1.007	.2	.0	.0	.0	.00	50.0	-44.0	17.0	.5	0.	0.	0.	0.	0.	.26
N215K1.008	.1	.0	.0	.0	-.01	50.0	-56.0	17.0	.1	0.	0.	0.	0.	0.	.06
N215K1.009	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.23
N215K1.010	.0	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.04
N215K2.004	1.2	9.1	12.9	16.1	.09	50.0	.0	17.0	3.1	0.	0.	138.	0.	0.	2.54
N215K2.005	1.1	8.5	11.2	11.2	.05	50.0	-22.0	17.0	3.0	0.	0.	119.	0.	0.	1.54
N215K2.006	1.2	8.1	8.1	8.2	.03	50.0	-28.0	17.0	3.1	0.	0.	87.	0.	0.	.96
N215K2.007	.1	.0	.0	.0	-.10	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.03
N215K2.008	.1	.0	.0	.0	-.01	50.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.12
N215K2.009	.1	.0	.0	.0	-.01	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.21
N215K2.010	.0	.0	.0	.0	-.01	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.04
N215K3.004	1.4	11.1	11.1	12.2	.08	50.0	.0	17.0	3.7	0.	0.	119.	0.	0.	2.36
N215K3.005	1.0	.0	11.0	.0	.03	50.0	-22.0	17.0	2.6	0.	0.	117.	0.	0.	1.22
N215K3.006	1.1	6.2	6.2	9.0	.04	50.0	-28.0	17.0	2.9	0.	0.	66.	0.	0.	1.14
N215K3.007	.4	.0	22.7	.0	.05	50.0	-44.0	17.0	1.0	0.	0.	242.	0.	0.	1.49
N215K3.008	.1	.0	.0	.0	.00	50.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.18
N215K3.009	.1	.0	.0	.0	.01	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.34
N215K3.010	.0	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.14
N215K4.004	1.1	8.4	14.7	18.6	.07	50.0	.0	17.0	3.0	0.	0.	157.	0.	0.	2.03
N215K4.005	1.5	9.8	9.8	14.9	.05	50.0	-22.0	17.0	3.9	0.	0.	105.	0.	0.	1.64
N215K4.006	1.0	11.3	11.3	11.3	.04	50.0	-28.0	17.0	2.8	0.	0.	120.	0.	0.	1.26
N215K4.007	.5	.0	13.4	.0	.03	50.0	-44.0	17.0	1.4	0.	0.	143.	0.	0.	.77
N215K4.008	.1	.0	.0	.0	.01	50.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.30
N215K4.009	.1	.0	.0	.0	.01	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.40
N215K4.010	.1	.0	.0	.0	.02	50.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.53

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215K5.004	1.4	5.4	5.4	11.2	.10	50.0	.0	17.0	3.7	0.	0.	58.	0.	0.	2.86
N215K5.005	.9	.0	12.5	.0	.01	50.0	-22.0	17.0	2.4	0.	0.	133.	0.	0.	.76
N215K5.006	.8	.0	14.2	.0	.00	50.0	-28.0	17.0	2.2	0.	0.	152.	0.	0.	.38
N215K5.007	.7	.0	9.4	.0	-.02	50.0	-44.0	17.0	1.8	0.	0.	100.	0.	0.	.07
N215K5.008	.1	.0	.0	.0	.00	50.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.23
N215K5.009	.1	.0	.0	.0	.01	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.34
N215K5.010	.1	.0	.0	.0	.01	50.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.41
N215L1.004	.1	.0	.0	.0	.00	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.27
N215L1.005	.1	.0	.0	.0	.00	150.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.23
N215L1.006	.1	.0	.0	.0	.04	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	1.28
N215L1.007	.4	.0	33.1	.0	.07	150.0	44.0	1.0	1.0	0.	0.	353.	0.	0.	2.13
N215L1.008	.4	.0	13.8	.0	.04	150.0	28.0	1.0	1.0	0.	0.	148.	0.	0.	1.35
N215L1.009	.4	.0	13.1	.0	.06	150.0	22.0	1.0	1.2	0.	0.	140.	0.	0.	1.79
N215L1.010	.6	.0	14.9	.0	.07	150.0	.0	1.0	1.6	0.	0.	159.	0.	0.	2.27
N215L2.004	.1	.0	.0	.0	.00	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.24
N215L2.005	.1	.0	.0	.0	.02	150.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.53
N215L2.006	.1	.0	.0	.0	.01	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.35
N215L2.007	.8	.0	56.5	.0	.22	150.0	44.0	1.0	2.2	0.	0.	604.	0.	0.	6.40
N215L2.008	.6	.0	15.4	.0	.09	150.0	28.0	1.0	1.7	0.	0.	164.	0.	0.	2.57
N215L2.009	.6	.0	15.1	.0	.09	150.0	22.0	1.0	1.7	0.	0.	161.	0.	0.	2.60
N215L2.010	.6	.0	19.6	.0	.11	150.0	.0	1.0	1.7	0.	0.	210.	0.	0.	3.29
N215L3.004	.1	.0	.0	.0	.00	150.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.36
N215L3.005	.1	.0	.0	.0	.00	150.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.14
N215L3.006	.0	.0	.0	.0	.00	150.0	56.0	1.0	.0	0.	0.	0.	0.	0.	.00
N215L3.007	.3	.0	23.3	.0	.02	150.0	44.0	1.0	.7	0.	0.	249.	0.	0.	1.07
N215L3.008	.5	.0	17.6	.0	.04	150.0	28.0	1.0	1.3	0.	0.	188.	0.	0.	1.18
N215L3.009	.5	.0	16.6	.0	.05	150.0	22.0	1.0	1.4	0.	0.	178.	0.	0.	1.64
N215L3.010	.6	.0	16.2	.0	.11	150.0	.0	1.0	1.6	0.	0.	172.	0.	0.	3.10
N215L4.004	.1	.0	.0	.0	.00	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.25
N215L4.005	.1	.0	.0	.0	.01	150.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.48
N215L4.006	.1	.0	.0	.0	.02	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.63
N215L4.007	.3	.0	17.3	.0	.01	150.0	44.0	1.0	.8	0.	0.	185.	0.	0.	.56
N215L4.008	.5	.0	15.8	.0	.06	150.0	28.0	1.0	1.3	0.	0.	169.	0.	0.	1.74
N215L4.009	.6	.0	18.6	.0	.08	150.0	22.0	1.0	1.5	0.	0.	198.	0.	0.	2.20
N215L4.010	.6	.0	16.9	.0	.09	150.0	.0	1.0	1.5	0.	0.	180.	0.	0.	2.59
N215L5.004	.1	.0	.0	.0	.02	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.53
N215L5.005	.1	.0	.0	.0	.02	150.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.68
N215L5.006	.1	.0	.0	.0	.00	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.25
N215L5.007	.4	.0	55.6	.0	-.40	150.0	44.0	1.0	1.0	0.	0.	593.	0.	0.	.21
N215L5.008	.4	.0	15.5	.0	.05	150.0	28.0	1.0	1.0	0.	0.	165.	0.	0.	1.58
N215L5.009	.5	.0	14.8	.0	.07	150.0	22.0	1.0	1.4	0.	0.	158.	0.	0.	2.11
N215L5.010	.6	.0	16.4	.0	.10	150.0	.0	1.0	1.6	0.	0.	175.	0.	0.	3.02

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215M1.004	.1	.0	.0	.0	.00	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.12
N215M1.005	.1	.0	.0	.0	-.01	150.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.01
N215M1.006	.1	.0	.0	.0	.00	150.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.03
N215M1.007	.5	.0	14.1	.0	-.10	150.0	44.0	5.0	1.3	0.	0.	150.	0.	0.	.57
N215M1.008	.5	.0	14.4	.0	.04	150.0	28.0	5.0	1.3	0.	0.	154.	0.	0.	1.21
N215M1.009	.6	.0	14.3	.0	.06	150.0	22.0	5.0	1.6	0.	0.	153.	0.	0.	1.70
N215M1.010	.7	.0	13.8	.0	.06	150.0	.0	5.0	1.8	0.	0.	147.	0.	0.	1.90
N215M2.004	.1	.0	.0	.0	.00	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.16
N215M2.005	.1	.0	.0	.0	.01	150.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.31
N215M2.006	.1	.0	.0	.0	.01	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.36
N215M2.007	.2	.0	15.5	.0	.03	150.0	44.0	5.0	.6	0.	0.	165.	0.	0.	.82
N215M2.008	.4	.0	14.8	.0	.02	150.0	28.0	5.0	1.0	0.	0.	158.	0.	0.	.73
N215M2.009	.6	.0	11.0	.0	.03	150.0	22.0	5.0	1.7	0.	0.	117.	0.	0.	1.17
N215M2.010	.7	.0	13.4	.0	.08	150.0	.0	5.0	1.8	0.	0.	143.	0.	0.	2.35
N215M3.004	.1	.0	.0	.0	.02	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.59
N215M3.005	.1	.0	.0	.0	.00	150.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.24
N215M3.006	.1	.0	.0	.0	.00	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.14
N215M3.007	.5	.0	29.1	.0	.09	150.0	44.0	5.0	1.4	0.	0.	311.	0.	0.	2.67
N215M3.008	.4	.0	18.0	.0	.03	150.0	28.0	5.0	1.0	0.	0.	192.	0.	0.	.90
N215M3.009	.6	.0	12.5	.0	.05	150.0	22.0	5.0	1.6	0.	0.	134.	0.	0.	1.55
N215M3.010	.6	.0	15.7	.0	.10	150.0	.0	5.0	1.7	0.	0.	167.	0.	0.	2.89
N215M4.004	.0	.0	.0	.0	-.03	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.01
N215M4.005	.1	.0	.0	.0	-.01	150.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.05
N215M4.006	.1	.0	.0	.0	-.03	150.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.00
N215M4.007	.3	.0	18.2	.0	.00	150.0	44.0	5.0	.7	0.	0.	194.	0.	0.	.18
N215M4.008	.5	.0	15.5	.0	.02	150.0	28.0	5.0	1.4	0.	0.	166.	0.	0.	.66
N215M4.009	.5	.0	12.6	.0	.05	150.0	22.0	5.0	1.3	0.	0.	134.	0.	0.	1.60
N215M4.010	.6	.0	16.4	.0	.08	150.0	.0	5.0	1.7	0.	0.	175.	0.	0.	2.27
N215M5.004	.1	.0	.0	.0	-.02	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.00
N215M5.005	.1	.0	.0	.0	.00	150.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.16
N215M5.006	.1	.0	.0	.0	.00	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.02
N215M5.007	.3	.0	11.8	.0	-.01	150.0	44.0	5.0	.7	0.	0.	126.	0.	0.	.38
N215M5.008	.5	.0	12.7	.0	.03	150.0	28.0	5.0	1.3	0.	0.	136.	0.	0.	1.15
N215M5.009	.6	.0	13.9	.0	.05	150.0	22.0	5.0	1.6	0.	0.	148.	0.	0.	1.58
N215M5.010	.7	.0	12.5	.0	.09	150.0	.0	5.0	1.8	0.	0.	134.	0.	0.	2.50
N215N1.004	.0	.0	.0	.0	-.01	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.06
N215N1.005	.1	.0	.0	.0	.00	150.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.08
N215N1.006	.0	.0	.0	.0	-.01	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.12
N215N1.007	.2	.0	15.1	.0	.03	150.0	44.0	11.0	.6	0.	0.	162.	0.	0.	1.08
N215N1.008	.5	.0	14.6	.0	.02	150.0	28.0	11.0	1.4	0.	0.	156.	0.	0.	.60
N215N1.009	.6	.0	14.4	.0	.03	150.0	22.0	11.0	1.7	0.	0.	154.	0.	0.	1.06
N215N1.010	.7	.0	14.5	.0	.09	150.0	.0	11.0	1.8	0.	0.	155.	0.	0.	2.55

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215N2.004	.0	.0	.0	.0	-.02	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.04
N215N2.005	.1	.0	.0	.0	.00	150.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.05
N215N2.006	.1	.0	.0	.0	.00	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.00
N215N2.007	.9	.0	14.6	.0	.28	150.0	44.0	11.0	2.4	0.	0.	156.	0.	0.	8.13
N215N2.008	.4	.0	19.2	.0	.00	150.0	28.0	11.0	1.1	0.	0.	205.	0.	0.	.35
N215N2.009	.5	.0	14.3	.0	.02	150.0	22.0	11.0	1.3	0.	0.	152.	0.	0.	.85
N215N2.010	.7	.0	15.9	.0	.07	150.0	.0	11.0	1.8	0.	0.	170.	0.	0.	1.95
N215N3.004	.1	.0	.0	.0	-.01	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.10
N215N3.005	.1	.0	.0	.0	-.01	150.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.01
N215N3.006	.1	.0	.0	.0	-.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.06
N215N3.007	.3	.0	33.0	.0	.02	150.0	44.0	11.0	.7	0.	0.	352.	0.	0.	1.43
N215N3.008	.4	.0	15.4	.0	.00	150.0	28.0	11.0	1.0	0.	0.	164.	0.	0.	.40
N215N3.009	.5	.0	17.4	.0	.02	150.0	22.0	11.0	1.3	0.	0.	186.	0.	0.	.67
N215N3.010	.6	.0	11.9	.0	.03	150.0	.0	11.0	1.6	0.	0.	127.	0.	0.	1.13
N215N4.004	.1	.0	.0	.0	.00	150.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.16
N215N4.005	.1	.0	.0	.0	.00	150.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.07
N215N4.006	.1	.0	.0	.0	-.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.19
N215N4.007	.3	.0	51.2	.0	-.11	150.0	44.0	11.0	.7	0.	0.	546.	0.	0.	.57
N215N4.008	.4	.0	12.2	.0	.02	150.0	28.0	11.0	1.2	0.	0.	130.	0.	0.	.56
N215N4.009	.5	.0	12.0	.0	.05	150.0	22.0	11.0	1.3	0.	0.	128.	0.	0.	1.43
N215N4.010	.5	.0	12.1	.0	.07	150.0	.0	11.0	1.5	0.	0.	129.	0.	0.	2.15
N215N5.004	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.19
N215N5.005	.1	.0	.0	.0	.00	150.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.08
N215N5.006	.1	.0	.0	.0	.01	150.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.25
N215N5.007	.3	.0	16.7	.0	.04	150.0	44.0	11.0	.9	0.	0.	179.	0.	0.	1.37
N215N5.008	.6	.0	16.9	.0	.03	150.0	28.0	11.0	1.5	0.	0.	180.	0.	0.	.83
N215N5.009	.7	.0	16.8	.0	.05	150.0	22.0	11.0	1.9	0.	0.	179.	0.	0.	1.36
N215N5.010	.6	.0	18.1	.0	.04	150.0	.0	11.0	1.7	0.	0.	193.	0.	0.	1.64
N21501.004	.1	.0	.0	.0	-.01	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.04
N21501.005	.0	.0	.0	.0	-.01	150.0	66.0	17.0	.0	0.	0.	0.	0.	0.	.07
N21501.006	.1	.0	.0	.0	-.01	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.12
N21501.007	.1	.0	.0	.0	-.02	150.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.09
N21501.008	.2	.0	22.7	.0	.01	150.0	28.0	17.0	.6	0.	0.	242.	0.	0.	.40
N21501.009	.6	.0	14.6	.0	.02	150.0	22.0	17.0	1.7	0.	0.	156.	0.	0.	.70
N21501.010	.5	.0	14.3	.0	.06	150.0	.0	17.0	1.3	0.	0.	153.	0.	0.	1.75
N21502.004	.1	.0	.0	.0	.00	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.16
N21502.005	.0	.0	.0	.0	-.01	150.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.06
N21502.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.23
N21502.007	.2	.0	16.1	.0	.01	150.0	44.0	17.0	.6	0.	0.	172.	0.	0.	.42
N21502.008	.3	.0	17.6	.0	.01	150.0	28.0	17.0	.8	0.	0.	188.	0.	0.	.48
N21502.009	.4	.0	13.8	.0	.02	150.0	22.0	17.0	1.0	0.	0.	147.	0.	0.	.65
N21502.010	.4	.0	16.1	.0	.04	150.0	.0	17.0	1.2	0.	0.	172.	0.	0.	1.16

FALCON 2: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N21503.004	.0	.0	.0	.0	.00	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.09
N21503.005	.1	.0	.0	.0	-.01	150.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.05
N21503.006	.2	.0	21.0	.0	-.02	150.0	56.0	17.0	.6	0.	0.	224.	0.	0.	.04
N21503.007	.3	.0	21.0	.0	.00	150.0	44.0	17.0	.9	0.	0.	224.	0.	0.	.35
N21503.008	.4	.0	13.6	.0	.01	150.0	28.0	17.0	1.0	0.	0.	145.	0.	0.	.29
N21503.009	.9	.0	13.5	.0	.02	150.0	22.0	17.0	2.3	0.	0.	145.	0.	0.	.77
N21503.010	.6	.0	18.1	.0	.04	150.0	.0	17.0	1.5	0.	0.	193.	0.	0.	1.35
N21504.004	.0	.0	.0	.0	-.01	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.04
N21504.005	.0	.0	.0	.0	-.01	150.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.01
N21504.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.14
N21504.007	.1	.0	.0	.0	-.04	150.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.08
N21504.008	.3	.0	23.7	.0	.02	150.0	28.0	17.0	.8	0.	0.	253.	0.	0.	.56
N21504.009	.5	.0	13.4	.0	.03	150.0	22.0	17.0	1.2	0.	0.	143.	0.	0.	.87
N21504.010	.6	.0	17.6	.0	.06	150.0	.0	17.0	1.5	0.	0.	188.	0.	0.	1.68
N21505.004	.1	.0	.0	.0	.00	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.00
N21505.005	.1	.0	.0	.0	.00	150.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.00
N21505.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.00
N21505.007	.1	.0	.0	.0	-.44	150.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.04
N21505.008	.3	.0	16.9	.0	.00	150.0	28.0	17.0	.7	0.	0.	180.	0.	0.	.18
N21505.009	.6	.0	11.1	.0	.01	150.0	22.0	17.0	1.6	0.	0.	119.	0.	0.	.61
N21505.010	.5	.0	11.3	.0	.05	150.0	.0	17.0	1.4	0.	0.	121.	0.	0.	1.48
N215P1.004	.5	.0	14.5	.0	.06	150.0	.0	1.0	1.3	0.	0.	155.	0.	0.	1.88
N215P1.005	.6	.0	13.8	.0	.07	150.0	-22.0	1.0	1.5	0.	0.	147.	0.	0.	2.12
N215P1.006	.5	.0	11.6	.0	.08	150.0	-28.0	1.0	1.4	0.	0.	124.	0.	0.	2.44
N215P1.007	.5	.0	13.3	.0	.07	150.0	-44.0	1.0	1.3	0.	0.	142.	0.	0.	2.04
N215P1.008	.4	.0	13.6	.0	.05	150.0	-56.0	1.0	1.2	0.	0.	145.	0.	0.	1.50
N215P1.009	.4	.0	17.1	.0	.03	150.0	-66.0	1.0	1.0	0.	0.	182.	0.	0.	1.20
N215P1.010	.3	.0	16.6	.0	.03	150.0	-75.0	1.0	.9	0.	0.	177.	0.	0.	.89
N215P2.004	.5	.0	14.6	.0	.07	150.0	.0	1.0	1.4	0.	0.	156.	0.	0.	2.02
N215P2.005	.5	.0	15.7	.0	.08	150.0	-22.0	1.0	1.4	0.	0.	168.	0.	0.	2.20
N215P2.006	.6	.0	18.1	.0	.08	150.0	-28.0	1.0	1.5	0.	0.	194.	0.	0.	2.33
N215P2.007	.6	.0	12.5	.0	.08	150.0	-44.0	1.0	1.6	0.	0.	133.	0.	0.	2.43
N215P2.008	.6	.0	12.5	.0	.05	150.0	-56.0	1.0	1.5	0.	0.	133.	0.	0.	1.67
N215P2.009	.5	.0	14.7	.0	.04	150.0	-66.0	1.0	1.3	0.	0.	157.	0.	0.	1.35
N215P2.010	.4	.0	20.3	.0	.01	150.0	-75.0	1.0	1.1	0.	0.	217.	0.	0.	.64
N215P3.004	.6	.0	15.1	.0	.07	150.0	.0	1.0	1.7	0.	0.	161.	0.	0.	2.11
N215P3.005	.6	.0	14.1	.0	.09	150.0	-22.0	1.0	1.6	0.	0.	151.	0.	0.	2.52
N215P3.006	.5	.0	15.6	.0	.08	150.0	-28.0	1.0	1.4	0.	0.	166.	0.	0.	2.41
N215P3.007	.5	.0	13.7	.0	.09	150.0	-44.0	1.0	1.3	0.	0.	147.	0.	0.	2.67
N215P3.008	.4	.0	16.5	.0	.07	150.0	-56.0	1.0	1.2	0.	0.	176.	0.	0.	2.12
N215P3.009	.4	.0	12.6	.0	.06	150.0	-66.0	1.0	1.1	0.	0.	134.	0.	0.	1.70
N215P3.010	.4	.0	14.6	.0	.07	150.0	-75.0	1.0	1.1	0.	0.	156.	0.	0.	2.22

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215P4.004	.6	.0	18.4	.0	.08	150.0	.0	1.0	1.5	0.	0.	196.	0.	0.	2.28
N215P4.005	.6	.0	13.2	.0	.07	150.0	-22.0	1.0	1.5	0.	0.	140.	0.	0.	2.14
N215P4.006	.6	.0	13.4	.0	.09	150.0	-28.0	1.0	1.6	0.	0.	143.	0.	0.	2.58
N215P4.007	.5	.0	15.0	.0	.09	150.0	-44.0	1.0	1.3	0.	0.	161.	0.	0.	2.55
N215P4.008	.5	.0	13.7	.0	.10	150.0	-56.0	1.0	1.3	0.	0.	146.	0.	0.	2.83
N215P4.009	.5	.0	17.3	.0	.07	150.0	-66.0	1.0	1.3	0.	0.	184.	0.	0.	2.18
N215P4.010	.4	.0	17.4	.0	.05	150.0	-75.0	1.0	1.1	0.	0.	185.	0.	0.	1.46
N215P5.004	.4	.0	12.1	.0	.06	150.0	.0	1.0	1.2	0.	0.	130.	0.	0.	1.85
N215P5.005	.5	.0	12.3	.0	.07	150.0	-22.0	1.0	1.3	0.	0.	131.	0.	0.	2.05
N215P5.006	.6	.0	13.6	.0	.08	150.0	-28.0	1.0	1.5	0.	0.	145.	0.	0.	2.41
N215P5.007	.5	.0	12.9	.0	.10	150.0	-44.0	1.0	1.5	0.	0.	137.	0.	0.	2.99
N215P5.008	.5	.0	15.5	.0	.08	150.0	-56.0	1.0	1.4	0.	0.	165.	0.	0.	2.16
N215P5.009	.6	.0	12.9	.0	.07	150.0	-66.0	1.0	1.5	0.	0.	138.	0.	0.	2.11
N215P5.010	.5	.0	14.9	.0	.09	150.0	-75.0	1.0	1.3	0.	0.	159.	0.	0.	2.50
N215Q1.004	.6	.0	11.5	.0	.09	150.0	.0	5.0	1.7	0.	0.	123.	0.	0.	2.75
N215Q1.005	.6	.0	12.1	.0	.09	150.0	-22.0	5.0	1.7	0.	0.	129.	0.	0.	2.48
N215Q1.006	.7	.0	12.0	.0	.08	150.0	-28.0	5.0	1.9	0.	0.	128.	0.	0.	2.34
N215Q1.007	.6	.0	16.5	.0	.07	150.0	-44.0	5.0	1.5	0.	0.	176.	0.	0.	2.16
N215Q1.008	.6	.0	12.0	.0	.02	150.0	-56.0	5.0	1.5	0.	0.	128.	0.	0.	.83
N215Q1.009	.5	.0	17.9	.0	.03	150.0	-66.0	5.0	1.3	0.	0.	191.	0.	0.	.85
N215Q1.010	.2	.0	.0	.0	.00	150.0	-75.0	5.0	.5	0.	0.	0.	0.	0.	.25
N215Q2.004	.6	.0	16.0	.0	.08	150.0	.0	5.0	1.6	0.	0.	171.	0.	0.	2.36
N215Q2.005	.6	.0	15.3	.0	.06	150.0	-22.0	5.0	1.6	0.	0.	164.	0.	0.	1.77
N215Q2.006	.6	.0	15.1	.0	.07	150.0	-28.0	5.0	1.6	0.	0.	161.	0.	0.	2.10
N215Q2.007	.6	.0	15.0	.0	.07	150.0	-44.0	5.0	1.6	0.	0.	160.	0.	0.	1.97
N215Q2.008	.5	.0	15.1	.0	.03	150.0	-56.0	5.0	1.3	0.	0.	161.	0.	0.	1.06
N215Q2.009	.4	.0	13.7	.0	.03	150.0	-66.0	5.0	1.2	0.	0.	146.	0.	0.	.81
N215Q2.010	.2	.0	.0	.0	.00	150.0	-75.0	5.0	.5	0.	0.	0.	0.	0.	.25
N215Q3.004	.6	.0	14.9	.0	.06	150.0	.0	5.0	1.7	0.	0.	159.	0.	0.	1.78
N215Q3.005	.6	.0	15.9	.0	.06	150.0	-22.0	5.0	1.7	0.	0.	169.	0.	0.	1.81
N215Q3.006	.7	.0	14.0	.0	.07	150.0	-28.0	5.0	1.9	0.	0.	150.	0.	0.	1.90
N215Q3.007	.7	.0	17.6	.0	.05	150.0	-44.0	5.0	1.7	0.	0.	188.	0.	0.	1.63
N215Q3.008	.6	.0	13.3	.0	.03	150.0	-56.0	5.0	1.5	0.	0.	142.	0.	0.	1.06
N215Q3.009	.4	.0	12.1	.0	.00	150.0	-66.0	5.0	1.1	0.	0.	130.	0.	0.	.44
N215Q3.010	.3	.0	18.7	.0	.00	150.0	-75.0	5.0	.8	0.	0.	200.	0.	0.	.36
N215Q4.004	.6	.0	13.6	.0	.07	150.0	.0	5.0	1.7	0.	0.	145.	0.	0.	1.97
N215Q4.005	.6	.0	14.1	.0	.05	150.0	-22.0	5.0	1.5	0.	0.	150.	0.	0.	1.60
N215Q4.006	.6	.0	13.9	.0	.06	150.0	-28.0	5.0	1.6	0.	0.	148.	0.	0.	1.74
N215Q4.007	.6	.0	17.4	.0	.06	150.0	-44.0	5.0	1.5	0.	0.	185.	0.	0.	1.82
N215Q4.008	.5	.0	13.8	.0	.02	150.0	-56.0	5.0	1.3	0.	0.	147.	0.	0.	.96
N215Q4.009	.4	.0	13.5	.0	.01	150.0	-66.0	5.0	1.0	0.	0.	144.	0.	0.	.60
N215Q4.010	.3	.0	16.4	.0	.02	150.0	-75.0	5.0	.9	0.	0.	175.	0.	0.	.63

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215Q5.004	.5	.0	16.6	.0	.07	150.0	.0	5.0	1.4	0.	0.	177.	0.	0.	1.99
N215Q5.005	.7	.0	16.6	.0	.08	150.0	-22.0	5.0	1.8	0.	0.	177.	0.	0.	2.22
N215Q5.006	.6	.0	17.9	.0	.07	150.0	-28.0	5.0	1.7	0.	0.	191.	0.	0.	2.09
N215Q5.007	.6	.0	12.4	.0	.04	150.0	-44.0	5.0	1.6	0.	0.	133.	0.	0.	1.40
N215Q5.008	.7	.0	12.5	.0	.05	150.0	-56.0	5.0	1.8	0.	0.	133.	0.	0.	1.38
N215Q5.009	.4	.0	16.8	.0	.05	150.0	-66.0	5.0	1.2	0.	0.	179.	0.	0.	1.42
N215Q5.010	.2	.0	30.2	.0	.02	150.0	-75.0	5.0	.6	0.	0.	323.	0.	0.	.72
N215R1.004	.7	.0	11.6	.0	.06	150.0	.0	11.0	2.0	0.	0.	124.	0.	0.	1.81
N215R1.005	.6	.0	16.0	.0	.05	150.0	-22.0	11.0	1.6	0.	0.	171.	0.	0.	1.54
N215R1.006	.7	.0	14.2	.0	.05	150.0	-28.0	11.0	1.8	0.	0.	151.	0.	0.	1.51
N215R1.007	.5	.0	12.7	.0	.02	150.0	-44.0	11.0	1.3	0.	0.	135.	0.	0.	.83
N215R1.008	.3	.0	12.8	.0	.01	150.0	-56.0	11.0	.9	0.	0.	137.	0.	0.	.41
N215R1.009	.3	.0	17.9	.0	.02	150.0	-66.0	11.0	.8	0.	0.	191.	0.	0.	.72
N215R1.010	.2	.0	.0	.0	.03	150.0	-75.0	11.0	.4	0.	0.	0.	0.	0.	.92
N215R2.004	.6	.0	13.8	.0	.06	150.0	.0	11.0	1.7	0.	0.	148.	0.	0.	1.72
N215R2.005	.6	.0	14.1	.0	.06	150.0	-22.0	11.0	1.7	0.	0.	150.	0.	0.	1.78
N215R2.006	.5	.0	10.8	.0	.05	150.0	-28.0	11.0	1.4	0.	0.	115.	0.	0.	1.43
N215R2.007	.5	.0	15.8	.0	.03	150.0	-44.0	11.0	1.4	0.	0.	169.	0.	0.	1.05
N215R2.008	.3	.0	19.7	.0	.00	150.0	-56.0	11.0	.8	0.	0.	210.	0.	0.	.39
N215R2.009	.3	.0	19.8	.0	.02	150.0	-66.0	11.0	.9	0.	0.	212.	0.	0.	.55
N215R2.010	.2	.0	.0	.0	.02	150.0	-75.0	11.0	.5	0.	0.	0.	0.	0.	.67
N215R3.004	.6	.0	16.3	.0	.06	150.0	.0	11.0	1.6	0.	0.	174.	0.	0.	1.93
N215R3.005	.6	.0	15.4	.0	.08	150.0	-22.0	11.0	1.7	0.	0.	165.	0.	0.	2.26
N215R3.006	.7	.0	16.1	.0	.07	150.0	-28.0	11.0	1.8	0.	0.	172.	0.	0.	2.13
N215R3.007	.4	.0	9.8	.0	-.05	150.0	-44.0	11.0	1.2	0.	0.	105.	0.	0.	.23
N215R3.008	.4	.0	14.8	.0	.01	150.0	-56.0	11.0	1.2	0.	0.	158.	0.	0.	.45
N215R3.009	.3	.0	16.0	.0	.01	150.0	-66.0	11.0	.9	0.	0.	171.	0.	0.	.50
N215R3.010	.2	.0	.0	.0	.02	150.0	-75.0	11.0	.4	0.	0.	0.	0.	0.	.50
N215R4.004	.7	.0	12.6	.0	.07	150.0	.0	11.0	1.8	0.	0.	135.	0.	0.	2.03
N215R4.005	.6	.0	13.3	.0	.05	150.0	-22.0	11.0	1.6	0.	0.	142.	0.	0.	1.55
N215R4.006	.5	.0	16.9	.0	.04	150.0	-28.0	11.0	1.4	0.	0.	180.	0.	0.	1.06
N215R4.007	.4	.0	20.5	.0	.03	150.0	-44.0	11.0	.9	0.	0.	219.	0.	0.	.82
N215R4.008	.3	.0	22.7	.0	.01	150.0	-56.0	11.0	.8	0.	0.	242.	0.	0.	.41
N215R4.009	.2	.0	.0	.0	.01	150.0	-66.0	11.0	.5	0.	0.	0.	0.	0.	.39
N215R4.010	.1	.0	.0	.0	.01	150.0	-75.0	11.0	.3	0.	0.	0.	0.	0.	.49
N215R5.004	.7	.0	14.3	.0	.06	150.0	.0	11.0	1.7	0.	0.	153.	0.	0.	1.88
N215R5.005	.6	.0	12.5	.0	.06	150.0	-22.0	11.0	1.6	0.	0.	134.	0.	0.	1.82
N215R5.006	.6	.0	15.8	.0	.05	150.0	-28.0	11.0	1.7	0.	0.	169.	0.	0.	1.61
N215R5.007	.5	.0	16.4	.0	.00	150.0	-44.0	11.0	1.3	0.	0.	175.	0.	0.	.46
N215R5.008	.4	.0	12.7	.0	.00	150.0	-56.0	11.0	1.0	0.	0.	135.	0.	0.	.27
N215R5.009	.3	.0	13.9	.0	.01	150.0	-66.0	11.0	.9	0.	0.	149.	0.	0.	.33
N215R5.010	.3	.0	15.6	.0	-.02	150.0	-75.0	11.0	.8	0.	0.	166.	0.	0.	.09

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215S1.004	.5	.0	18.8	.0	.04	150.0	.0	17.0	1.4	0.	0.	201.	0.	0.	1.44
N215S1.005	.6	.0	14.2	.0	.03	150.0	-22.0	17.0	1.6	0.	0.	151.	0.	0.	.92
N215S1.006	.5	.0	14.1	.0	.02	150.0	-28.0	17.0	1.3	0.	0.	151.	0.	0.	,70
N215S1.007	.4	.0	11.5	.0	.03	150.0	-44.0	17.0	1.2	0.	0.	123.	0.	0.	.97
N215S1.008	.2	.0	14.9	.0	.02	150.0	-56.0	17.0	.7	0.	0.	159.	0.	0.	.51
N215S1.009	.1	.0	.0	.0	.00	150.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.25
N215S1.010	.1	.0	.0	.0	.00	150.0	-75.0	17.0	.4	0.	0.	0.	0.	0.	.20
N215S2.004	.6	.0	16.7	.0	.06	150.0	.0	17.0	1.6	0.	0.	179.	0.	0.	1.70
N215S2.005	.6	.0	13.7	.0	.04	150.0	-22.0	17.0	1.5	0.	0.	146.	0.	0.	1.19
N215S2.006	.6	.0	18.3	.0	.03	150.0	-28.0	17.0	1.6	0.	0.	196.	0.	0.	.93
N215S2.007	.5	.0	22.6	.0	.01	150.0	-44.0	17.0	1.3	0.	0.	241.	0.	0.	.46
N215S2.008	.4	.0	22.9	.0	-.01	150.0	-56.0	17.0	1.0	0.	0.	244.	0.	0.	.09
N215S2.009	.1	.0	.0	.0	.00	150.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.22
N215S2.010	.0	.0	.0	.0	-.01	150.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.12
N215S3.004	.5	.0	15.8	.0	.03	150.0	.0	17.0	1.4	0.	0.	168.	0.	0.	1.06
N215S3.005	.7	.0	15.1	.0	.04	150.0	-22.0	17.0	2.0	0.	0.	162.	0.	0.	1.11
N215S3.006	.5	.0	14.9	.0	.03	150.0	-28.0	17.0	1.4	0.	0.	159.	0.	0.	.90
N215S3.007	.6	.0	13.1	.0	.03	150.0	-44.0	17.0	1.6	0.	0.	140.	0.	0.	.83
N215S3.008	.3	.0	8.3	.0	.00	150.0	-56.0	17.0	.8	0.	0.	89.	0.	0.	.37
N215S3.009	.2	.0	14.5	.0	.01	150.0	-66.0	17.0	.6	0.	0.	155.	0.	0.	.50
N215S3.010	.1	.0	.0	.0	.02	150.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.51
N215S4.004	.8	.0	13.0	.0	.03	150.0	.0	17.0	2.2	0.	0.	138.	0.	0.	1.03
N215S4.005	.6	.0	12.1	.0	.03	150.0	-22.0	17.0	1.6	0.	0.	129.	0.	0.	1.06
N215S4.006	.5	.0	11.6	.0	.03	150.0	-28.0	17.0	1.5	0.	0.	124.	0.	0.	.99
N215S4.007	1.0	11.6	11.6	11.6	.00	150.0	-44.0	17.0	2.7	0.	0.	123.	0.	0.	.37
N215S4.008	.2	.0	18.9	.0	.00	150.0	-56.0	17.0	.6	0.	0.	202.	0.	0.	.23
N215S4.009	.3	.0	12.1	.0	.02	150.0	-66.0	17.0	.9	0.	0.	130.	0.	0.	.77
N215S4.010	.2	.0	11.9	.0	.02	150.0	-75.0	17.0	.6	0.	0.	127.	0.	0.	.61
N215S5.004	.4	.0	12.5	.0	.03	150.0	.0	17.0	1.2	0.	0.	134.	0.	0.	1.01
N215S5.005	.5	.0	12.9	.0	.05	150.0	-22.0	17.0	1.4	0.	0.	138.	0.	0.	1.44
N215S5.006	.5	.0	12.7	.0	.05	150.0	-28.0	17.0	1.4	0.	0.	136.	0.	0.	1.38
N215S5.007	.4	.0	12.0	.0	.04	150.0	-44.0	17.0	1.2	0.	0.	129.	0.	0.	1.03
N215S5.008	.3	.0	12.4	.0	.01	150.0	-56.0	17.0	.8	0.	0.	133.	0.	0.	.39
N215S5.009	.2	.0	.0	.0	.01	150.0	-66.0	17.0	.4	0.	0.	0.	0.	0.	.37
N215S5.010	.3	.0	12.5	.0	.00	150.0	-75.0	17.0	.8	0.	0.	133.	0.	0.	.22
N215T1.004	.1	.0	.0	.0	-.01	250.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.11
N215T1.005	.1	.0	.0	.0	-.01	250.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.04
N215T1.006	.1	.0	.0	.0	.00	250.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.15
N215T1.007	.1	.0	.0	.0	-.04	250.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.06
N215T1.008	.2	.0	17.7	.0	.02	250.0	28.0	1.0	.6	0.	0.	189.	0.	0.	.77
N215T1.009	.3	.0	20.6	.0	.05	250.0	22.0	1.0	.8	0.	0.	220.	0.	0.	1.57
N215T1.010	.5	.0	18.9	.0	.10	250.0	.0	1.0	1.2	0.	0.	201.	0.	0.	2.87

FALCON 2: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215T2.004	.1	.0	.0	.0	.02	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.54
N215T2.005	.1	.0	.0	.0	.00	250.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.15
N215T2.006	.0	.0	.0	.0	.00	250.0	56.0	1.0	.1	0.	0.	0.	0.	0.	.23
N215T2.007	.1	.0	.0	.0	.02	250.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.69
N215T2.008	.2	.0	.0	.0	.01	250.0	28.0	1.0	.5	0.	0.	0.	0.	0.	.56
N215T2.009	.3	.0	19.4	.0	.06	250.0	22.0	1.0	.8	0.	0.	208.	0.	0.	1.64
N215T2.010	.5	.0	22.7	.0	.08	250.0	.0	1.0	1.3	0.	0.	242.	0.	0.	2.47
N215T3.004	.1	.0	.0	.0	-.01	250.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.09
N215T3.005	.1	.0	.0	.0	.00	250.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.29
N215T3.006	.1	.0	.0	.0	.00	250.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.04
N215T3.007	.1	.0	.0	.0	.01	250.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.54
N215T3.008	.3	.0	15.9	.0	.02	250.0	28.0	1.0	.8	0.	0.	170.	0.	0.	.80
N215T3.009	.3	.0	15.4	.0	.04	250.0	22.0	1.0	.7	0.	0.	164.	0.	0.	1.32
N215T3.010	.5	.0	21.3	.0	.06	250.0	.0	1.0	1.2	0.	0.	227.	0.	0.	1.81
N215T4.004	.1	.0	.0	.0	.00	250.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.19
N215T4.005	.0	.0	.0	.0	-.01	250.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.08
N215T4.006	.1	.0	.0	.0	-.01	250.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.01
N215T4.007	.2	.0	.0	.0	.02	250.0	44.0	1.0	.5	0.	0.	0.	0.	0.	1.03
N215T4.008	.1	.0	.0	.0	.00	250.0	28.0	1.0	.3	0.	0.	0.	0.	0.	.34
N215T4.009	.3	.0	25.2	.0	.03	250.0	22.0	1.0	.7	0.	0.	269.	0.	0.	.99
N215T4.010	.4	.0	20.6	.0	.05	250.0	.0	1.0	1.2	0.	0.	220.	0.	0.	1.72
N215T5.004	.1	.0	.0	.0	.00	250.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.22
N215T5.005	.1	.0	.0	.0	-.02	250.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.06
N215T5.006	.1	.0	.0	.0	.01	250.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.39
N215T5.007	.2	.0	19.9	.0	.00	250.0	44.0	1.0	.6	0.	0.	212.	0.	0.	.50
N215T5.008	.3	.0	18.4	.0	.03	250.0	28.0	1.0	.9	0.	0.	197.	0.	0.	.99
N215T5.009	.3	.0	15.7	.0	.03	250.0	22.0	1.0	.9	0.	0.	167.	0.	0.	1.04
N215T5.010	.4	.0	19.2	.0	.06	250.0	.0	1.0	1.1	0.	0.	205.	0.	0.	1.92
N215U1.004	.1	.0	.0	.0	.00	250.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.17
N215U1.005	.1	.0	.0	.0	.01	250.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.30
N215U1.006	.2	.0	20.6	.0	.01	250.0	56.0	5.0	.6	0.	0.	220.	0.	0.	.44
N215U1.007	.3	.0	17.9	.0	.02	250.0	44.0	5.0	.8	0.	0.	192.	0.	0.	.76
N215U1.008	.5	.0	17.5	.0	.05	250.0	28.0	5.0	1.2	0.	0.	187.	0.	0.	1.55
N215U1.009	.5	.0	19.0	.0	.06	250.0	22.0	5.0	1.4	0.	0.	203.	0.	0.	1.86
N215U1.010	.4	.0	19.4	.0	.08	250.0	.0	5.0	1.1	0.	0.	207.	0.	0.	2.42
N215U2.004	.0	.0	.0	.0	-.03	250.0	75.0	5.0	.0	0.	0.	0.	0.	0.	.04
N215U2.005	.1	.0	.0	.0	.00	250.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.14
N215U2.006	.1	.0	.0	.0	-.03	250.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.02
N215U2.007	.1	.0	.0	.0	-.02	250.0	44.0	5.0	.3	0.	0.	0.	0.	0.	.07
N215U2.008	.4	.0	17.4	.0	.02	250.0	28.0	5.0	1.0	0.	0.	185.	0.	0.	.67
N215U2.009	.4	.0	13.9	.0	.03	250.0	22.0	5.0	1.1	0.	0.	148.	0.	0.	.82
N215U2.010	.4	.0	15.6	.0	.03	250.0	.0	5.0	1.2	0.	0.	166.	0.	0.	1.20

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215U3.004	.1	.0	.0	.0	-.02	250.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.07
N215U3.005	.1	.0	.0	.0	-.01	250.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.05
N215U3.006	.1	.0	.0	.0	-.01	250.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.03
N215U3.007	.3	.0	23.2	.0	.01	250.0	44.0	5.0	.8	0.	0.	248.	0.	0.	.45
N215U3.008	.4	.0	18.6	.0	.02	250.0	28.0	5.0	1.0	0.	0.	199.	0.	0.	.63
N215U3.009	.4	.0	17.6	.0	.02	250.0	22.0	5.0	1.1	0.	0.	188.	0.	0.	.80
N215U3.010	.4	.0	13.6	.0	.03	250.0	.0	5.0	1.0	0.	0.	146.	0.	0.	1.11
N215U4.004	.1	.0	.0	.0	-.01	250.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.09
N215U4.005	.1	.0	.0	.0	.00	250.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.18
N215U4.006	.3	.0	19.2	.0	.02	250.0	56.0	5.0	.7	0.	0.	205.	0.	0.	.66
N215U4.007	.3	.0	19.5	.0	.05	250.0	44.0	5.0	.8	0.	0.	208.	0.	0.	1.48
N215U4.008	.4	.0	21.1	.0	.04	250.0	28.0	5.0	1.2	0.	0.	225.	0.	0.	1.11
N215U4.009	.4	.0	21.1	.0	.07	250.0	22.0	5.0	1.2	0.	0.	225.	0.	0.	1.89
N215U4.010	.6	.0	19.7	.0	.10	250.0	.0	5.0	1.5	0.	0.	211.	0.	0.	2.95
N215U5.004	.1	.0	.0	.0	.00	250.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.15
N215U5.005	.1	.0	.0	.0	.00	250.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.23
N215U5.006	.2	.0	.0	.0	.02	250.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.53
N215U5.007	.5	.0	20.8	.0	.13	250.0	44.0	5.0	1.2	0.	0.	222.	0.	0.	3.66
N215U5.008	.4	.0	19.5	.0	.04	250.0	28.0	5.0	1.2	0.	0.	208.	0.	0.	1.10
N215U5.009	.4	.0	17.7	.0	.05	250.0	22.0	5.0	1.2	0.	0.	189.	0.	0.	1.57
N215U5.010	.5	.0	19.3	.0	.06	250.0	.0	5.0	1.3	0.	0.	206.	0.	0.	1.76
N215V1.004	.0	.0	.0	.0	-.02	250.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.02
N215V1.005	.0	.0	.0	.0	-.02	250.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.01
N215V1.006	.1	.0	.0	.0	-.02	250.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.02
N215V1.007	.2	.0	.0	.0	.00	250.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.10
N215V1.008	.3	.0	20.3	.0	.01	250.0	28.0	11.0	.9	0.	0.	217.	0.	0.	.29
N215V1.009	.4	.0	17.6	.0	.01	250.0	22.0	11.0	1.0	0.	0.	188.	0.	0.	.64
N215V1.010	.4	.0	18.1	.0	.03	250.0	.0	11.0	1.2	0.	0.	193.	0.	0.	.98
N215V2.004	.1	.0	.0	.0	-.02	250.0	75.0	11.0	.4	0.	0.	0.	0.	0.	.06
N215V2.005	.2	.0	20.7	.0	.00	250.0	66.0	11.0	.6	0.	0.	221.	0.	0.	.08
N215V2.006	.2	.0	13.0	.0	.00	250.0	56.0	11.0	.6	0.	0.	138.	0.	0.	.19
N215V2.007	.4	.0	21.1	.0	.03	250.0	44.0	11.0	1.1	0.	0.	225.	0.	0.	.82
N215V2.008	.3	.0	13.7	.0	-.01	250.0	28.0	11.0	.9	0.	0.	146.	0.	0.	.32
N215V2.009	.4	.0	21.9	.0	.03	250.0	22.0	11.0	1.1	0.	0.	234.	0.	0.	.88
N215V2.010	.5	.0	20.9	.0	.05	250.0	.0	11.0	1.3	0.	0.	223.	0.	0.	1.35
N215V3.004	.1	.0	.0	.0	-.01	250.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.06
N215V3.005	.1	.0	.0	.0	.00	250.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.15
N215V3.006	.2	.0	.0	.0	.00	250.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.19
N215V3.007	.3	.0	17.4	.0	.01	250.0	44.0	11.0	.8	0.	0.	186.	0.	0.	.46
N215V3.008	.4	.0	15.6	.0	.01	250.0	28.0	11.0	.9	0.	0.	167.	0.	0.	.51
N215V3.009	.4	.0	17.6	.0	.01	250.0	22.0	11.0	1.0	0.	0.	187.	0.	0.	.54
N215V3.010	.4	.0	15.3	.0	.00	250.0	.0	11.0	1.1	0.	0.	163.	0.	0.	.69

FALCON 2: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215V4.004	.1	.0	.0	.0	-.01	250.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.09
N215V4.005	.0	.0	.0	.0	-.02	250.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.03
N215V4.006	.0	.0	.0	.0	-.02	250.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.06
N215V4.007	.4	.0	20.9	.0	.06	250.0	44.0	11.0	1.1	0.	0.	223.	0.	0.	1.92
N215V4.008	.2	.0	.0	.0	.02	250.0	28.0	11.0	.5	0.	0.	0.	0.	0.	.57
N215V4.009	.3	.0	17.3	.0	.02	250.0	22.0	11.0	.8	0.	0.	185.	0.	0.	.66
N215V4.010	.4	.0	17.5	.0	.02	250.0	.0	11.0	1.1	0.	0.	187.	0.	0.	.83
N215V5.004	.1	.0	.0	.0	.02	250.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.70
N215V5.005	.1	.0	.0	.0	.03	250.0	66.0	11.0	.4	0.	0.	0.	0.	0.	.80
N215V5.006	.1	.0	.0	.0	.01	250.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.38
N215V5.007	.4	.0	19.1	.0	.05	250.0	44.0	11.0	1.1	0.	0.	204.	0.	0.	1.54
N215V5.008	.3	.0	20.4	.0	.02	250.0	28.0	11.0	.8	0.	0.	217.	0.	0.	.62
N215V5.009	.4	.0	17.3	.0	.02	250.0	22.0	11.0	1.1	0.	0.	185.	0.	0.	.66
N215V5.010	.5	.0	17.1	.0	.04	250.0	.0	11.0	1.4	0.	0.	182.	0.	0.	1.29
N215W1.004	.0	.0	.0	.0	-.01	250.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.12
N215W1.005	.0	.0	.0	.0	.00	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.20
N215W1.006	.1	.0	.0	.0	-.01	250.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.05
N215W1.007	.1	.0	.0	.0	-.01	250.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.05
N215W1.008	.1	.0	.0	.0	-.02	250.0	28.0	17.0	.4	0.	0.	0.	0.	0.	.13
N215W1.009	.3	.0	26.4	.0	.00	250.0	22.0	17.0	.7	0.	0.	282.	0.	0.	.26
N215W1.010	.4	.0	18.0	.0	.01	250.0	.0	17.0	1.0	0.	0.	192.	0.	0.	.56
N215W2.004	.1	.0	.0	.0	.00	250.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.03
N215W2.005	.0	.0	.0	.0	.00	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.16
N215W2.006	.1	.0	.0	.0	-.01	250.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.14
N215W2.007	.4	.0	15.6	.0	.02	250.0	44.0	17.0	1.1	0.	0.	166.	0.	0.	.66
N215W2.008	.3	.0	15.5	.0	.01	250.0	28.0	17.0	.7	0.	0.	166.	0.	0.	.23
N215W2.009	.3	.0	14.1	.0	.03	250.0	22.0	17.0	.9	0.	0.	151.	0.	0.	.90
N215W2.010	.5	.0	19.1	.0	.02	250.0	.0	17.0	1.3	0.	0.	203.	0.	0.	.84
N215W2.004	.1	.0	.0	.0	.00	250.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.03
N215W2.005	.0	.0	.0	.0	.00	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.16
N215W2.006	.1	.0	.0	.0	-.01	250.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.14
N215W2.007	.4	.0	15.6	.0	.02	250.0	44.0	17.0	1.1	0.	0.	166.	0.	0.	.66
N215W2.008	.3	.0	15.5	.0	.01	250.0	28.0	17.0	.7	0.	0.	166.	0.	0.	.23
N215W2.009	.3	.0	14.1	.0	.03	250.0	22.0	17.0	.9	0.	0.	151.	0.	0.	.90
N215W2.010	.5	.0	19.1	.0	.02	250.0	.0	17.0	1.3	0.	0.	203.	0.	0.	.84
N215W3.004	.1	.0	.0	.0	.00	250.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.02
N215W3.005	.1	.0	.0	.0	-.01	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.02
N215W3.006	.2	.0	.0	.0	.00	250.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.09
N215W3.007	.3	.0	19.1	.0	.02	250.0	44.0	17.0	.7	0.	0.	203.	0.	0.	.63
N215W3.008	.4	.0	17.0	.0	.03	250.0	28.0	17.0	1.1	0.	0.	182.	0.	0.	.86
N215W3.009	.4	.0	21.4	.0	.03	250.0	22.0	17.0	1.1	0.	0.	229.	0.	0.	.94
N215W3.010	.5	.0	18.7	.0	.03	250.0	.0	17.0	1.2	0.	0.	200.	0.	0.	1.06

FALCON 2: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N215W4.004	.1	.0	.0	.0	.00	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.23
N215W4.005	.1	.0	.0	.0	.00	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.07
N215W4.006	.2	.0	.0	.0	.00	250.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.16
N215W4.007	.2	.0	.0	.0	-.01	250.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.25
N215W4.008	.3	.0	17.9	.0	.01	250.0	28.0	17.0	.7	0.	0.	191.	0.	0.	.17
N215W4.009	.3	.0	16.3	.0	.02	250.0	22.0	17.0	.8	0.	0.	174.	0.	0.	.74
N215W4.010	.5	.0	15.7	.0	.03	250.0	.0	17.0	1.3	0.	0.	167.	0.	0.	.91
N215W5.004	.1	.0	.0	.0	.01	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.31
N215W5.005	.1	.0	.0	.0	.00	250.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.24
N215W5.006	.2	.0	.0	.0	.00	250.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.16
N215W5.007	.5	.0	21.1	.0	.06	250.0	44.0	17.0	1.3	0.	0.	225.	0.	0.	2.04
N215W5.008	.3	.0	13.2	.0	.01	250.0	28.0	17.0	.9	0.	0.	141.	0.	0.	.32
N215W5.009	.4	.0	14.6	.0	.03	250.0	22.0	17.0	1.2	0.	0.	155.	0.	0.	.93
N215W5.010	.5	.0	14.3	.0	.04	250.0	.0	17.0	1.3	0.	0.	153.	0.	0.	1.30

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220A1.010	1.4	10.0	12.6	13.1	.07	-62.0	30.0	2.0	3.7	0.	0.	155.	0.	0.	2.43
N220A1.009	17.8	4.0	7.2	18.7	.87	-62.0	20.0	2.0	36.9	50.	68.	89.	178.	216.	26.14
N220A1.008	13.9	2.1	8.3	26.0	1.41	-62.0	10.0	2.0	30.4	26.	27.	103.	202.	285.	41.88
N220A1.007	16.5	1.5	7.4	28.3	1.51	-62.0	.0	2.0	34.7	22.	26.	91.	227.	270.	44.26
N220A1.005	9.8	3.9	7.3	24.5	.94	-62.0	-20.0	2.0	22.8	48.	49.	90.	150.	255.	28.34
N220A1.004	.3	.0	9.2	.0	-.01	-62.0	-30.0	2.0	.9	0.	0.	114.	0.	0.	.17
N220A2.010	3.4	8.1	8.2	12.0	.08	-62.0	30.0	2.0	8.7	100.	0.	101.	0.	102.	2.72
N220A2.009	23.0	2.7	6.0	23.7	1.57	-62.0	20.0	2.0	44.7	33.	33.	74.	189.	256.	43.78
N220A2.008	20.6	1.8	7.0	27.4	1.87	-62.0	10.0	2.0	41.2	22.	23.	86.	257.	312.	53.50
N220A2.007	21.6	1.3	7.2	30.4	2.17	-62.0	.0	2.0	42.7	22.	24.	89.	227.	308.	60.86
N220A2.005	13.6	1.4	7.2	31.5	1.07	-62.0	-20.0	2.0	29.8	20.	27.	88.	204.	252.	32.60
N220A2.004	.9	.0	9.1	.0	.01	-62.0	-30.0	2.0	2.3	0.	0.	113.	0.	0.	.34
N220A3.010	1.8	7.6	16.0	16.4	.06	-62.0	30.0	2.0	4.7	0.	0.	197.	0.	0.	2.18
N220A3.009	19.2	2.1	6.1	42.8	1.48	-62.0	20.0	2.0	39.1	26.	28.	75.	175.	263.	42.76
N220A3.008	20.2	1.4	7.1	31.0	1.95	-62.0	10.0	2.0	40.7	18.	21.	87.	236.	299.	54.89
N220A3.007	19.8	1.4	7.5	33.8	2.19	-62.0	.0	2.0	40.0	28.	33.	92.	233.	302.	61.65
N220A3.005	13.0	.6	5.9	31.3	1.40	-62.0	-20.0	2.0	28.7	18.	32.	72.	178.	323.	41.96
N220A3.004	.3	.0	9.3	.0	.00	-62.0	-30.0	2.0	.8	0.	0.	114.	0.	0.	.23
N220A4.010	1.5	12.5	12.5	20.2	.06	-62.0	30.0	2.0	3.9	0.	0.	154.	0.	0.	2.00
N220A4.009	20.3	1.7	7.0	27.2	1.57	-62.0	20.0	2.0	40.8	21.	28.	86.	207.	272.	44.26
N220A4.008	19.7	1.0	6.3	28.9	2.01	-62.0	10.0	2.0	39.9	20.	20.	77.	256.	325.	57.39
N220A4.007	17.4	1.1	7.0	24.7	1.67	-62.0	.0	2.0	36.2	15.	26.	87.	216.	252.	49.89
N220A4.005	14.3	1.6	7.9	36.9	1.26	-62.0	-20.0	2.0	31.1	20.	49.	97.	185.	299.	38.17
N220A4.004	.9	.0	14.8	.0	.01	-62.0	-30.0	2.0	2.4	0.	0.	182.	0.	0.	.58
N220A5.010	1.5	9.2	9.3	20.2	.04	-62.0	30.0	2.0	3.9	0.	0.	114.	0.	0.	1.60
N220A5.009	17.8	2.9	8.3	38.1	1.50	-62.0	20.0	2.0	37.0	37.	38.	102.	190.	242.	43.07
N220A5.008	18.8	1.7	5.7	31.4	1.93	-62.0	10.0	2.0	38.5	21.	22.	70.	227.	284.	55.41
N220A5.007	19.8	1.3	6.2	29.3	2.14	-62.0	.0	2.0	40.1	18.	25.	77.	262.	309.	60.53
N220A5.005	13.4	.9	9.0	29.4	1.28	-62.0	-20.0	2.0	29.5	17.	27.	110.	197.	296.	38.51
N220A5.004	.2	.0	7.7	.0	.00	-62.0	-30.0	2.0	.6	0.	0.	95.	0.	0.	.26
N220B1.010	.7	.0	13.4	.0	.03	-32.0	30.0	1.0	1.8	0.	0.	166.	0.	0.	1.23
N220B1.009	22.9	1.0	6.7	21.3	1.63	-32.0	20.0	1.0	44.5	15.	25.	82.	148.	255.	44.49
N220B1.008	40.6	.2	6.2	26.6	3.53	-32.0	10.0	1.0	64.9	2.	2.	76.	235.	278.	84.98
N220B1.007	31.2	.2	6.7	23.1	2.16	-32.0	.0	1.0	55.1	2.	2.	82.	157.	193.	55.09
N220B1.005	16.8	.2	7.1	19.2	1.14	-32.0	-20.0	1.0	35.3	2.	18.	88.	143.	188.	33.20
N220B1.004	.5	.0	23.2	.0	.01	-32.0	-30.0	1.0	1.3	0.	0.	285.	0.	0.	.54
N220B2.010	1.0	9.2	9.2	9.2	.04	-32.0	30.0	1.0	2.8	0.	0.	113.	0.	0.	1.50
N220B2.009	20.1	1.5	5.4	26.6	1.90	-32.0	20.0	1.0	40.5	20.	21.	66.	202.	212.	52.25
N220B2.008	41.4	.2	3.7	23.1	3.46	-32.0	10.0	1.0	65.7	2.	2.	45.	175.	221.	79.95
N220B2.007	34.4	.1	4.5	20.8	2.41	-32.0	.0	1.0	58.7	2.	2.	55.	164.	176.	60.56
N220B2.005	16.4	.1	7.3	21.3	.77	-32.0	-20.0	1.0	34.6	2.	2.	90.	108.	190.	23.19
N220B2.004	.7	.0	12.1	.0	.03	-32.0	-30.0	1.0	2.0	0.	0.	149.	0.	0.	1.04

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220B3.010	1.1	11.9	11.9	12.1	.05	-32.0	30.0	1.0	2.9	0.	0.	147.	0.	0.	1.98
N220B3.009	20.5	2.0	6.9	23.1	1.66	-32.0	20.0	1.0	41.1	26.	28.	85.	225.	275.	47.38
N220B3.008	39.0	.2	6.3	24.4	3.26	-32.0	10.0	1.0	63.4	2.	2.	77.	182.	225.	78.90
N220B3.007	31.2	.2	5.0	20.7	1.94	-32.0	.0	1.0	55.1	2.	2.	62.	169.	170.	48.92
N220B3.005	11.0	.1	7.8	20.0	.84	-32.0	-20.0	1.0	25.0	2.	2.	96.	145.	175.	25.70
N220B3.004	.8	.0	12.8	.0	.01	-32.0	-30.0	1.0	2.1	0.	0.	157.	0.	0.	.55
N220B4.010	1.0	13.0	13.0	13.0	.05	-32.0	30.0	1.0	2.8	0.	0.	160.	0.	0.	1.77
N220B4.009	18.6	2.2	6.7	24.6	1.58	-32.0	20.0	1.0	38.1	31.	35.	83.	205.	240.	44.65
N220B4.008	38.8	.2	5.3	29.8	3.34	-32.0	10.0	1.0	63.1	2.	2.	65.	227.	265.	81.79
N220B4.007	37.5	.2	5.9	22.2	2.38	-32.0	.0	1.0	61.9	2.	2.	72.	154.	259.	60.66
N220B4.005	10.6	.2	4.4	18.1	.73	-32.0	-20.0	1.0	24.3	2.	29.	54.	167.	197.	22.69
N220B4.004	.2	.0	.0	.0	-.01	-32.0	-30.0	1.0	.4	0.	0.	0.	0.	0.	.17
N220B5.010	.9	.0	13.3	.0	.07	-32.0	30.0	1.0	2.4	0.	0.	164.	0.	0.	2.30
N220B5.009	24.9	.8	5.5	23.3	1.72	-32.0	20.0	1.0	47.3	24.	26.	68.	189.	257.	47.29
N220B5.008	44.6	.2	5.1	22.1	3.23	-32.0	10.0	1.0	68.5	2.	2.	62.	242.	245.	77.15
N220B5.007	33.3	.2	6.4	24.1	2.15	-32.0	.0	1.0	57.4	2.	2.	78.	177.	226.	55.06
N220B5.005	12.1	.1	7.0	17.5	.76	-32.0	-20.0	1.0	27.1	2.	2.	86.	133.	180.	23.13
N220B5.004	.7	.0	12.0	.0	.03	-32.0	-30.0	1.0	1.8	0.	0.	147.	0.	0.	1.13
N220C1.010	1.5	10.4	13.1	13.2	.07	-2.0	30.0	1.0	3.9	0.	0.	161.	0.	0.	2.29
N220C1.009	17.0	1.1	7.5	19.5	1.15	-2.0	20.0	1.0	35.7	15.	17.	93.	165.	194.	33.22
N220C1.008	22.2	.6	6.8	18.8	1.15	-2.0	10.0	1.0	43.6	8.	12.	84.	111.	139.	31.60
N220C1.007	16.2	.8	3.7	13.9	.44	-2.0	.0	1.0	34.3	10.	43.	45.	95.	98.	13.44
N220C1.005	11.3	1.8	5.4	12.9	.70	-2.0	-20.0	1.0	25.7	23.	52.	67.	122.	154.	20.92
N220C1.004	.4	.0	9.7	.0	.03	-2.0	-30.0	1.0	1.2	0.	0.	119.	0.	0.	1.04
N220C2.010	1.0	9.9	9.9	9.9	.05	-2.0	30.0	1.0	2.7	0.	0.	121.	0.	0.	1.74
N220C2.009	14.2	1.3	7.6	16.0	.92	-2.0	20.0	1.0	30.9	19.	34.	94.	132.	139.	27.09
N220C2.008	22.9	.5	7.1	15.7	1.27	-2.0	10.0	1.0	44.6	7.	7.	88.	114.	133.	34.70
N220C2.007	22.9	1.1	7.4	19.3	.90	-2.0	.0	1.0	44.5	36.	46.	91.	117.	169.	25.60
N220C2.005	13.1	4.2	5.9	18.7	.53	-2.0	-20.0	1.0	29.0	52.	55.	73.	91.	183.	16.42
N220C2.004	1.1	12.4	12.4	12.4	.07	-2.0	-30.0	1.0	2.8	0.	0.	152.	0.	0.	2.42
N220C3.010	4.7	4.5	4.6	4.7	.07	-2.0	30.0	1.0	11.8	56.	56.	57.	57.	57.	2.42
N220C3.009	16.7	1.4	4.1	16.9	1.12	-2.0	20.0	1.0	35.1	21.	22.	51.	157.	183.	32.51
N220C3.008	21.0	1.5	6.9	15.8	1.09	-2.0	10.0	1.0	41.9	20.	21.	85.	155.	157.	29.86
N220C3.007	19.6	1.2	5.1	15.4	.57	-2.0	.0	1.0	39.7	41.	60.	63.	97.	113.	16.59
N220C3.005	13.3	2.3	7.1	12.8	.45	-2.0	-20.0	1.0	29.3	73.	79.	88.	112.	121.	13.87
N220C3.004	.9	.0	8.9	.0	.01	-2.0	-30.0	1.0	2.5	0.	0.	110.	0.	0.	.61
N220C4.010	2.4	2.9	7.6	14.0	.07	-2.0	30.0	1.0	6.2	36.	0.	94.	0.	94.	2.34
N220C4.009	21.3	1.4	5.8	19.5	1.35	-2.0	20.0	1.0	42.3	24.	33.	71.	172.	216.	38.73
N220C4.008	27.3	1.1	5.2	19.1	1.34	-2.0	10.0	1.0	50.4	32.	33.	64.	120.	213.	36.34
N220C4.007	16.9	1.4	5.9	18.7	.38	-2.0	.0	1.0	35.4	18.	47.	72.	105.	146.	11.72
N220C4.005	4.9	1.3	3.7	15.0	.24	-2.0	-20.0	1.0	12.2	42.	44.	46.	50.	59.	7.79
N220C4.004	1.0	11.3	11.3	11.3	.03	-2.0	-30.0	1.0	2.8	0.	0.	139.	0.	0.	.93

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220C5.010	1.0	.0	9.3	.0	.06	-2.0	30.0	1.0	2.6	0.	0.	114.	0.	0.	2.11
N220C5.009	19.3	1.9	6.6	19.2	1.11	-2.0	20.0	1.0	39.2	28.	30.	81.	139.	191.	32.48
N220C5.008	22.1	1.0	4.1	15.9	1.02	-2.0	10.0	1.0	43.4	12.	13.	51.	124.	193.	29.02
N220C5.007	21.2	1.9	4.6	14.6	.82	-2.0	.0	1.0	42.0	28.	29.	57.	111.	139.	23.34
N220C5.005	12.8	4.0	5.8	14.7	.54	-2.0	-20.0	1.0	28.4	62.	63.	71.	114.	120.	16.32
N220C5.004	1.1	10.9	12.3	12.4	.04	-2.0	-30.0	1.0	2.8	0.	0.	152.	0.	0.	1.48
N220D1.010	.1	.0	.0	.0	.01	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.53
N220D1.009	.7	.0	12.8	.0	.04	50.0	44.0	1.0	1.9	0.	0.	158.	0.	0.	1.44
N220D1.008	.8	.0	12.9	.0	.10	50.0	22.0	1.0	2.1	0.	0.	158.	0.	0.	3.47
N220D1.007	.8	.0	15.2	.0	.09	50.0	.0	1.0	2.0	0.	0.	187.	0.	0.	2.99
N220D1.005	.8	.0	14.5	.0	.05	50.0	-22.0	1.0	2.2	0.	0.	179.	0.	0.	1.74
N220D1.004	.1	.0	.0	.0	.00	50.0	-44.0	1.0	.2	0.	0.	0.	0.	0.	.24
N220D2.010	.1	.0	.0	.0	-.01	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.13
N220D2.009	1.8	7.9	7.9	8.0	.04	50.0	44.0	1.0	4.6	0.	0.	98.	0.	0.	1.35
N220D2.008	1.1	7.7	7.7	7.7	.07	50.0	22.0	1.0	2.9	0.	0.	95.	0.	0.	2.42
N220D2.007	.8	.0	11.9	.0	.10	50.0	.0	1.0	2.1	0.	0.	147.	0.	0.	3.31
N220D2.005	.7	.0	8.9	.0	.05	50.0	-22.0	1.0	1.9	0.	0.	110.	0.	0.	1.79
N220D2.004	.3	.0	10.3	.0	.01	50.0	-44.0	1.0	.8	0.	0.	127.	0.	0.	.36
N220D3.010	.1	.0	.0	.0	.00	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.27
N220D3.009	.6	.0	11.9	.0	.03	50.0	44.0	1.0	1.7	0.	0.	147.	0.	0.	1.09
N220D3.008	.9	.0	9.9	.0	.08	50.0	22.0	1.0	2.4	0.	0.	122.	0.	0.	2.53
N220D3.007	.7	.0	11.3	.0	.10	50.0	.0	1.0	1.9	0.	0.	139.	0.	0.	3.27
N220D3.005	.7	.0	10.9	.0	.06	50.0	-22.0	1.0	1.8	0.	0.	134.	0.	0.	2.15
N220D3.004	.6	.0	4.4	.0	.01	50.0	-44.0	1.0	1.6	0.	0.	54.	0.	0.	.54
N220D4.010	.1	.0	.0	.0	.01	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.39
N220D4.009	.9	.0	12.3	.0	.06	50.0	44.0	1.0	2.3	0.	0.	152.	0.	0.	2.05
N220D4.008	1.2	4.4	4.4	15.5	.09	50.0	22.0	1.0	3.2	0.	0.	54.	0.	0.	2.94
N220D4.007	6.0	6.4	6.4	6.4	.13	50.0	.0	1.0	14.8	78.	78.	78.	79.	79.	4.25
N220D4.005	1.4	7.0	7.0	7.2	.04	50.0	-22.0	1.0	3.7	0.	0.	87.	0.	0.	1.50
N220D4.004	.1	.0	.0	.0	.00	50.0	-44.0	1.0	.2	0.	0.	0.	0.	0.	.21
N220D5.010	.2	.0	.0	.0	.00	50.0	66.0	1.0	.5	0.	0.	0.	0.	0.	.35
N220D5.009	.8	.0	7.2	.0	.03	50.0	44.0	1.0	2.1	0.	0.	88.	0.	0.	1.28
N220D5.008	1.1	5.1	11.8	11.8	.08	50.0	22.0	1.0	3.0	0.	0.	145.	0.	0.	2.78
N220D5.007	.6	.0	4.7	.0	.10	50.0	.0	1.0	1.7	0.	0.	58.	0.	0.	3.27
N220D5.005	.6	.0	10.2	.0	.05	50.0	-22.0	1.0	1.7	0.	0.	125.	0.	0.	1.60
N220D5.004	.2	.0	.0	.0	.02	50.0	-44.0	1.0	.5	0.	0.	0.	0.	0.	.69
N220E1.010	.1	.0	.0	.0	.01	50.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.32
N220E1.009	.9	.0	17.4	.0	.02	50.0	44.0	5.0	2.4	0.	0.	215.	0.	0.	.91
N220E1.008	1.3	8.2	8.2	8.5	.10	50.0	22.0	5.0	3.5	0.	0.	102.	0.	0.	3.44
N220E1.007	.8	.0	9.2	.0	.12	50.0	.0	5.0	2.1	0.	0.	113.	0.	0.	3.89
N220E1.005	.9	.0	12.8	.0	.07	50.0	-22.0	5.0	2.3	0.	0.	158.	0.	0.	2.29
N220E1.004	.2	.0	.0	.0	.02	50.0	-44.0	5.0	.4	0.	0.	0.	0.	0.	.74

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220E2.010	.3	.0	22.8	.0	.03	50.0	66.0	5.0	.9	0.	0.	281.	0.	0.	1.08
N220E2.009	.8	.0	17.5	.0	.05	50.0	44.0	5.0	2.1	0.	0.	215.	0.	0.	1.63
N220E2.008	1.4	5.5	5.5	17.6	.12	50.0	22.0	5.0	3.7	0.	0.	67.	0.	0.	3.90
N220E2.007	1.0	6.8	6.8	6.8	.10	50.0	.0	5.0	2.7	0.	0.	84.	0.	0.	3.38
N220E2.005	.8	.0	4.8	.0	.06	50.0	-22.0	5.0	2.1	0.	0.	59.	0.	0.	1.99
N220E2.004	.2	.0	.0	.0	.03	50.0	-44.0	5.0	.5	0.	0.	0.	0.	0.	.88
N220E3.010	.1	.0	.0	.0	.00	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.35
N220E3.009	.5	.0	11.7	.0	.02	50.0	44.0	5.0	1.5	0.	0.	144.	0.	0.	.84
N220E3.008	1.3	4.4	8.4	10.8	.10	50.0	22.0	5.0	3.4	0.	0.	104.	0.	0.	3.20
N220E3.007	1.3	2.0	13.8	13.9	.11	50.0	.0	5.0	3.3	0.	0.	170.	0.	0.	3.83
N220E3.005	1.3	2.1	2.1	2.2	.07	50.0	-22.0	5.0	3.5	0.	0.	26.	0.	0.	2.26
N220E3.004	.2	.0	10.6	.0	.02	50.0	-44.0	5.0	.6	0.	0.	131.	0.	0.	.77
N220E4.010	.0	.0	.0	.0	-.01	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.12
N220E4.009	.6	.0	2.5	.0	.03	50.0	44.0	5.0	1.6	0.	0.	31.	0.	0.	.97
N220E4.008	1.3	6.9	10.3	10.7	.09	50.0	22.0	5.0	3.4	0.	0.	127.	0.	0.	3.09
N220E4.007	1.2	9.7	9.7	10.5	.11	50.0	.0	5.0	3.3	0.	0.	119.	0.	0.	3.56
N220E4.005	.7	.0	10.2	.0	.06	50.0	-22.0	5.0	1.9	0.	0.	126.	0.	0.	2.10
N220E4.004	.4	.0	16.9	.0	.00	50.0	-44.0	5.0	1.1	0.	0.	208.	0.	0.	.33
N220E5.010	.1	.0	.0	.0	.01	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.33
N220E5.009	.9	.0	4.7	.0	.01	50.0	44.0	5.0	2.5	0.	0.	58.	0.	0.	.52
N220E5.008	1.1	16.7	16.7	16.7	.10	50.0	22.0	5.0	3.0	0.	0.	206.	0.	0.	3.26
N220E5.007	1.0	.0	3.2	.0	.11	50.0	.0	5.0	2.5	0.	0.	39.	0.	0.	3.69
N220E5.005	.8	.0	11.5	.0	.06	50.0	-22.0	5.0	2.1	0.	0.	142.	0.	0.	2.25
N220E5.004	.3	.0	16.4	.0	-.01	50.0	-44.0	5.0	.8	0.	0.	202.	0.	0.	.24
N220F1.010	.1	.0	.0	.0	.02	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.67
N220F1.009	.5	.0	13.9	.0	.01	50.0	44.0	11.0	1.4	0.	0.	171.	0.	0.	.50
N220F1.008	1.3	4.2	4.2	8.4	.08	50.0	22.0	11.0	3.3	0.	0.	52.	0.	0.	2.76
N220F1.007	1.5	2.5	2.5	2.7	.10	50.0	.0	11.0	3.9	0.	0.	31.	0.	0.	3.40
N220F1.005	1.0	.0	12.3	.0	.05	50.0	-22.0	11.0	2.6	0.	0.	151.	0.	0.	1.58
N220F1.004	.6	.0	3.1	.0	.00	50.0	-44.0	11.0	1.7	0.	0.	38.	0.	0.	.17
N220F2.010	.0	.0	.0	.0	-.01	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.00
N220F2.009	.7	.0	15.3	.0	.00	50.0	44.0	11.0	1.9	0.	0.	188.	0.	0.	.31
N220F2.008	1.2	9.5	9.5	13.7	.12	50.0	22.0	11.0	3.2	0.	0.	117.	0.	0.	4.05
N220F2.007	.9	.0	12.5	.0	.09	50.0	.0	11.0	2.4	0.	0.	154.	0.	0.	2.90
N220F2.005	.8	.0	9.2	.0	.04	50.0	-22.0	11.0	2.2	0.	0.	114.	0.	0.	1.52
N220F2.004	.4	.0	10.2	.0	.00	50.0	-44.0	11.0	1.2	0.	0.	125.	0.	0.	.25
N220F3.010	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.38
N220F3.009	.8	.0	15.3	.0	.01	50.0	44.0	11.0	2.0	0.	0.	188.	0.	0.	.63
N220F3.008	1.1	7.2	7.2	15.3	.07	50.0	22.0	11.0	3.0	0.	0.	89.	0.	0.	2.44
N220F3.007	.9	.0	9.9	.0	.09	50.0	.0	11.0	2.3	0.	0.	122.	0.	0.	3.06
N220F3.005	.9	.0	7.1	.0	.05	50.0	-22.0	11.0	2.4	0.	0.	88.	0.	0.	1.77
N220F3.004	.4	.0	14.7	.0	.00	50.0	-44.0	11.0	1.1	0.	0.	181.	0.	0.	.23

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220F4.010	.1	.0	.0	.0	.00	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.30
N220F4.009	.6	.0	12.8	.0	.02	50.0	44.0	11.0	1.7	0.	0.	157.	0.	0.	.80
N220F4.008	1.4	2.1	2.1	12.6	.08	50.0	22.0	11.0	3.7	0.	0.	25.	0.	0.	2.63
N220F4.007	1.2	9.4	9.4	9.5	.08	50.0	.0	11.0	3.1	0.	0.	115.	0.	0.	2.69
N220F4.005	1.4	10.1	11.2	11.6	.05	50.0	-22.0	11.0	3.8	0.	0.	138.	0.	0.	1.78
N220F4.004	.4	.0	16.5	.0	.01	50.0	-44.0	11.0	1.0	0.	0.	203.	0.	0.	.31
N220F5.010	.0	.0	.0	.0	-.01	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.04
N220F5.009	.4	.0	16.7	.0	.01	50.0	44.0	11.0	1.2	0.	0.	206.	0.	0.	.46
N220F5.008	1.5	3.3	3.3	7.4	.09	50.0	22.0	11.0	3.9	0.	0.	41.	0.	0.	3.10
N220F5.007	1.1	1.9	1.9	1.9	.08	50.0	.0	11.0	2.9	0.	0.	23.	0.	0.	2.77
N220F5.005	.9	.0	10.5	.0	.05	50.0	-22.0	11.0	2.4	0.	0.	130.	0.	0.	1.65
N220F5.004	.7	.0	8.7	.0	.01	50.0	-44.0	11.0	1.9	0.	0.	107.	0.	0.	.49
N220G1.010	.0	.0	.0	.0	-.01	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.03
N220G1.009	.5	.0	14.0	.0	.00	50.0	44.0	17.0	1.4	0.	0.	172.	0.	0.	.27
N220G1.008	1.0	.0	2.3	.0	.06	50.0	22.0	17.0	2.6	0.	0.	29.	0.	0.	2.01
N220G1.007	.8	.0	8.2	.0	.06	50.0	.0	17.0	2.0	0.	0.	102.	0.	0.	1.89
N220G1.005	.9	.0	14.1	.0	.03	50.0	-22.0	17.0	2.4	0.	0.	174.	0.	0.	1.10
N220G1.004	.3	.0	20.2	.0	.01	50.0	-44.0	17.0	.7	0.	0.	249.	0.	0.	.32
N220G2.010	.0	.0	.0	.0	-.02	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.01
N220G2.009	.6	.0	19.7	.0	.00	50.0	44.0	17.0	1.7	0.	0.	243.	0.	0.	.35
N220G2.008	1.2	11.6	13.0	13.1	.05	50.0	22.0	17.0	3.1	0.	0.	160.	0.	0.	1.77
N220G2.007	1.3	12.8	13.1	13.3	.06	50.0	.0	17.0	3.5	0.	0.	162.	0.	0.	2.22
N220G2.005	.6	.0	7.4	.0	.02	50.0	-22.0	17.0	1.6	0.	0.	91.	0.	0.	.85
N220G2.004	.1	.0	.0	.0	.01	50.0	-44.0	17.0	.4	0.	0.	0.	0.	0.	.41
N220G3.010	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.22
N220G3.009	.5	.0	12.7	.0	.03	50.0	44.0	17.0	1.4	0.	0.	156.	0.	0.	.87
N220G3.008	1.0	8.8	8.8	10.7	.06	50.0	22.0	17.0	2.7	0.	0.	108.	0.	0.	2.18
N220G3.007	1.5	6.4	6.4	11.9	.07	50.0	.0	17.0	3.8	0.	0.	79.	0.	0.	2.40
N220G3.005	.7	.0	14.2	.0	.03	50.0	-22.0	17.0	2.0	0.	0.	174.	0.	0.	1.10
N220G3.004	.3	.0	12.0	.0	.00	50.0	-44.0	17.0	.9	0.	0.	148.	0.	0.	.19
N220G4.010	.1	.0	.0	.0	.00	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.07
N220G4.009	.8	.0	15.1	.0	.01	50.0	44.0	17.0	2.2	0.	0.	187.	0.	0.	.61
N220G4.008	1.2	14.1	15.0	15.0	.06	50.0	22.0	17.0	3.1	0.	0.	185.	0.	0.	2.07
N220G4.007	1.2	11.0	11.0	11.8	.07	50.0	.0	17.0	3.1	0.	0.	135.	0.	0.	2.28
N220G4.005	.8	.0	10.4	.0	.02	50.0	-22.0	17.0	2.2	0.	0.	128.	0.	0.	.86
N220G4.004	.1	.0	.0	.0	.00	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.18
N220G5.010	.0	.0	.0	.0	-.01	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.10
N220G5.009	.4	.0	19.6	.0	.01	50.0	44.0	17.0	1.1	0.	0.	242.	0.	0.	.46
N220G5.008	1.0	.0	7.7	.0	.05	50.0	22.0	17.0	2.6	0.	0.	95.	0.	0.	1.91
N220G5.007	1.0	12.3	12.3	12.3	.04	50.0	.0	17.0	2.7	0.	0.	151.	0.	0.	1.76
N220G5.005	1.0	9.8	9.8	9.8	.01	50.0	-22.0	17.0	2.7	0.	0.	121.	0.	0.	.82
N220G5.004	.1	.0	.0	.0	-.01	50.0	-44.0	17.0	.2	0.	0.	0.	0.	0.	.14

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220H1.010	.5	.0	15.0	.0	.03	150.0	75.0	1.0	1.3	0.	0.	185.	0.	0.	.95
N220H1.009	.4	.0	11.8	.0	.05	150.0	56.0	1.0	1.1	0.	0.	145.	0.	0.	1.66
N220H1.008	.6	.0	13.3	.0	.07	150.0	28.0	1.0	1.5	0.	0.	163.	0.	0.	2.47
N220H1.007	.5	.0	14.7	.0	.05	150.0	.0	1.0	1.2	0.	0.	182.	0.	0.	1.96
N220H1.005	.3	.0	10.6	.0	.03	150.0	-28.0	1.0	.8	0.	0.	131.	0.	0.	1.18
N220H1.004	.1	.0	.0	.0	.01	150.0	-56.0	1.0	.2	0.	0.	0.	0.	0.	.40
N220H2.010	.3	.0	15.4	.0	.04	150.0	75.0	1.0	.9	0.	0.	190.	0.	0.	1.38
N220H2.009	.5	.0	14.6	.0	.05	150.0	56.0	1.0	1.4	0.	0.	180.	0.	0.	1.77
N220H2.008	.5	.0	13.0	.0	.09	150.0	28.0	1.0	1.4	0.	0.	160.	0.	0.	2.94
N220H2.007	.5	.0	11.7	.0	.07	150.0	.0	1.0	1.2	0.	0.	144.	0.	0.	2.26
N220H2.005	.4	.0	9.4	.0	.03	150.0	-28.0	1.0	1.0	0.	0.	116.	0.	0.	.93
N220H2.004	.1	.0	.0	.0	-.01	150.0	-56.0	1.0	.3	0.	0.	0.	0.	0.	.15
N220H3.010	.3	.0	16.9	.0	.01	150.0	75.0	1.0	.9	0.	0.	209.	0.	0.	.63
N220H3.009	.5	.0	7.9	.0	.04	150.0	56.0	1.0	1.3	0.	0.	97.	0.	0.	1.52
N220H3.008	.7	.0	14.2	.0	.06	150.0	28.0	1.0	1.9	0.	0.	175.	0.	0.	2.11
N220H3.007	.5	.0	14.4	.0	.07	150.0	.0	1.0	1.3	0.	0.	178.	0.	0.	2.23
N220H3.005	.3	.0	14.3	.0	.01	150.0	-28.0	1.0	.9	0.	0.	176.	0.	0.	.65
N220H3.004	.2	.0	.0	.0	.04	150.0	-56.0	1.0	.4	0.	0.	0.	0.	0.	1.19
N220H4.010	.4	.0	14.0	.0	.03	150.0	75.0	1.0	1.1	0.	0.	173.	0.	0.	1.21
N220H4.009	.5	.0	15.6	.0	.04	150.0	56.0	1.0	1.4	0.	0.	192.	0.	0.	1.43
N220H4.008	.5	.0	13.8	.0	.07	150.0	28.0	1.0	1.4	0.	0.	170.	0.	0.	2.40
N220H4.007	.4	.0	11.6	.0	.04	150.0	.0	1.0	1.2	0.	0.	142.	0.	0.	1.66
N220H4.005	.3	.0	14.3	.0	.04	150.0	-28.0	1.0	.8	0.	0.	176.	0.	0.	1.25
N220H4.004	.1	.0	.0	.0	.03	150.0	-56.0	1.0	.4	0.	0.	0.	0.	0.	1.14
N220H5.010	.4	.0	13.8	.0	.05	150.0	75.0	1.0	1.2	0.	0.	170.	0.	0.	1.71
N220H5.009	.7	.0	11.0	.0	.07	150.0	56.0	1.0	1.9	0.	0.	135.	0.	0.	2.43
N220H5.008	.6	.0	15.0	.0	.07	150.0	28.0	1.0	1.7	0.	0.	185.	0.	0.	2.42
N220H5.007	.5	.0	16.4	.0	.06	150.0	.0	1.0	1.3	0.	0.	202.	0.	0.	2.02
N220H5.005	.4	.0	15.8	.0	.02	150.0	-28.0	1.0	1.0	0.	0.	194.	0.	0.	.84
N220H5.004	.1	.0	.0	.0	-.01	150.0	-56.0	1.0	.2	0.	0.	0.	0.	0.	.10
N220I1.010	.8	.0	11.7	.0	.02	150.0	75.0	5.0	2.1	0.	0.	144.	0.	0.	.77
N220I1.009	.7	.0	11.5	.0	.05	150.0	56.0	5.0	1.9	0.	0.	142.	0.	0.	1.83
N220I1.008	.7	.0	11.1	.0	.06	150.0	28.0	5.0	1.8	0.	0.	137.	0.	0.	1.99
N220I1.007	.4	.0	9.4	.0	.04	150.0	.0	5.0	1.1	0.	0.	116.	0.	0.	1.48
N220I1.005	.4	.0	7.3	.0	.02	150.0	-28.0	5.0	1.0	0.	0.	90.	0.	0.	.69
N220I1.004	.1	.0	.0	.0	.00	150.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.24
N220I2.010	.5	.0	15.9	.0	.02	150.0	75.0	5.0	1.3	0.	0.	196.	0.	0.	.84
N220I2.009	.5	.0	15.6	.0	.05	150.0	56.0	5.0	1.3	0.	0.	192.	0.	0.	1.58
N220I2.008	.6	.0	15.4	.0	.08	150.0	28.0	5.0	1.7	0.	0.	190.	0.	0.	2.58
N220I2.007	.5	.0	16.6	.0	.06	150.0	.0	5.0	1.3	0.	0.	205.	0.	0.	2.07
N220I2.005	.3	.0	7.4	.0	.04	150.0	-28.0	5.0	.7	0.	0.	92.	0.	0.	1.31
N220I2.004	.1	.0	.0	.0	-.02	150.0	-56.0	5.0	.1	0.	0.	0.	0.	0.	.04

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220I3.010	.4	.0	10.3	.0	.00	150.0	75.0	5.0	1.0	0.	0.	127.	0.	0.	.41
N220I3.009	.5	.0	14.6	.0	.04	150.0	56.0	5.0	1.4	0.	0.	179.	0.	0.	1.23
N220I3.008	.8	.0	14.0	.0	.07	150.0	28.0	5.0	2.1	0.	0.	173.	0.	0.	2.24
N220I3.007	.5	.0	8.8	.0	.05	150.0	.0	5.0	1.3	0.	0.	108.	0.	0.	1.74
N220I3.005	.3	.0	13.6	.0	.01	150.0	-28.0	5.0	.9	0.	0.	168.	0.	0.	.40
N220I3.004	.1	.0	.0	.0	-.01	150.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.02
N220I4.010	.4	.0	14.2	.0	.00	150.0	75.0	5.0	1.0	0.	0.	175.	0.	0.	.31
N220I4.009	.6	.0	16.2	.0	.04	150.0	56.0	5.0	1.5	0.	0.	199.	0.	0.	1.46
N220I4.008	.7	.0	15.9	.0	.07	150.0	28.0	5.0	1.9	0.	0.	196.	0.	0.	2.20
N220I4.007	.6	.0	3.9	.0	.05	150.0	.0	5.0	1.6	0.	0.	48.	0.	0.	1.81
N220I4.005	.3	.0	15.8	.0	.03	150.0	-28.0	5.0	.7	0.	0.	195.	0.	0.	1.08
N220I4.004	.1	.0	.0	.0	.01	150.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.25
N220I5.010	.3	.0	18.5	.0	.02	150.0	75.0	5.0	.7	0.	0.	227.	0.	0.	.60
N220I5.009	.6	.0	14.0	.0	.05	150.0	56.0	5.0	1.6	0.	0.	173.	0.	0.	1.61
N220I5.008	.6	.0	11.2	.0	.07	150.0	28.0	5.0	1.7	0.	0.	138.	0.	0.	2.32
N220I5.007	.5	.0	11.1	.0	.05	150.0	.0	5.0	1.3	0.	0.	136.	0.	0.	1.77
N220I5.005	.3	.0	8.8	.0	.03	150.0	-28.0	5.0	.7	0.	0.	109.	0.	0.	.86
N220I5.004	.1	.0	.0	.0	.00	150.0	-56.0	5.0	.3	0.	0.	0.	0.	0.	.21
N220J1.010	.3	.0	15.3	.0	.02	150.0	75.0	11.0	.8	0.	0.	189.	0.	0.	.66
N220J1.009	.5	.0	15.7	.0	.03	150.0	56.0	11.0	1.4	0.	0.	193.	0.	0.	1.03
N220J1.008	.6	.0	14.0	.0	.05	150.0	28.0	11.0	1.6	0.	0.	173.	0.	0.	1.91
N220J1.007	.4	.0	16.3	.0	.05	150.0	.0	11.0	1.2	0.	0.	201.	0.	0.	1.65
N220J1.005	.3	.0	16.5	.0	.00	150.0	-28.0	11.0	.9	0.	0.	204.	0.	0.	.21
N220J1.004	.3	.0	10.4	.0	.01	150.0	-56.0	11.0	.8	0.	0.	129.	0.	0.	.45
N220J2.010	.2	.0	.0	.0	.02	150.0	75.0	11.0	.5	0.	0.	0.	0.	0.	.61
N220J2.009	.5	.0	7.2	.0	.02	150.0	56.0	11.0	1.2	0.	0.	89.	0.	0.	.86
N220J2.008	.6	.0	11.9	.0	.06	150.0	28.0	11.0	1.7	0.	0.	147.	0.	0.	2.03
N220J2.007	.6	.0	12.6	.0	.05	150.0	.0	11.0	1.5	0.	0.	155.	0.	0.	1.59
N220J2.005	.4	.0	16.1	.0	.02	150.0	-28.0	11.0	1.0	0.	0.	199.	0.	0.	.70
N220J2.004	.1	.0	.0	.0	.00	150.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.25
N220J3.010	.3	.0	10.8	.0	-.01	150.0	75.0	11.0	.7	0.	0.	133.	0.	0.	.18
N220J3.009	.5	.0	12.5	.0	.02	150.0	56.0	11.0	1.4	0.	0.	154.	0.	0.	.84
N220J3.008	.7	.0	15.1	.0	.05	150.0	28.0	11.0	1.8	0.	0.	186.	0.	0.	1.67
N220J3.007	.5	.0	8.6	.0	.01	150.0	.0	11.0	1.5	0.	0.	106.	0.	0.	.81
N220J3.005	.3	.0	7.4	.0	.02	150.0	-28.0	11.0	.9	0.	0.	91.	0.	0.	.61
N220J3.004	.0	.0	.0	.0	-.02	150.0	-56.0	11.0	.1	0.	0.	0.	0.	0.	.03
N220J4.010	.4	.0	11.7	.0	.00	150.0	75.0	11.0	1.0	0.	0.	144.	0.	0.	.23
N220J4.009	.6	.0	9.0	.0	.03	150.0	56.0	11.0	1.6	0.	0.	111.	0.	0.	1.08
N220J4.008	.7	.0	10.2	.0	.04	150.0	28.0	11.0	1.8	0.	0.	126.	0.	0.	1.48
N220J4.007	.5	.0	15.1	.0	.04	150.0	.0	11.0	1.3	0.	0.	186.	0.	0.	1.31
N220J4.005	.3	.0	13.8	.0	.00	150.0	-28.0	11.0	.9	0.	0.	171.	0.	0.	.21
N220J4.004	.1	.0	.0	.0	.00	150.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.20

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220J5.010	.3	.0	14.3	.0	.00	150.0	75.0	11.0	.8	0.	0.	177.	0.	0.	.09
N220J5.009	.8	.0	10.3	.0	.02	150.0	56.0	11.0	2.0	0.	0.	127.	0.	0.	.71
N220J5.008	.7	.0	8.3	.0	.06	150.0	28.0	11.0	1.9	0.	0.	103.	0.	0.	2:05
N220J5.007	.5	.0	8.8	.0	.04	150.0	.0	11.0	1.3	0.	0.	108.	0.	0.	1.20
N220J5.005	.4	.0	8.4	.0	.01	150.0	-28.0	11.0	1.0	0.	0.	103.	0.	0.	.46
N220J5.004	.1	.0	.0	.0	.00	150.0	-56.0	11.0	.3	0.	0.	0.	0.	0.	.24
N220K1.010	.2	.0	.0	.0	-.01	150.0	75.0	17.0	.5	0.	0.	0.	0.	0.	.07
N220K1.009	.4	.0	16.0	.0	.00	150.0	56.0	17.0	1.1	0.	0.	197.	0.	0.	.37
N220K1.008	.5	.0	14.4	.0	.01	150.0	28.0	17.0	1.4	0.	0.	177.	0.	0.	.84
N220K1.007	.5	.0	9.9	.0	.02	150.0	.0	17.0	1.3	0.	0.	122.	0.	0.	.76
N220K1.005	.2	.0	9.9	.0	-.01	150.0	-28.0	17.0	.7	0.	0.	122.	0.	0.	.13
N220K1.004	.1	.0	.0	.0	-.01	150.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.06
N220K2.010	.2	.0	.0	.0	.00	150.0	75.0	17.0	.4	0.	0.	0.	0.	0.	.26
N220K2.009	.3	.0	4.4	.0	.00	150.0	56.0	17.0	.9	0.	0.	54.	0.	0.	.40
N220K2.008	.6	.0	11.3	.0	.02	150.0	28.0	17.0	1.5	0.	0.	139.	0.	0.	.81
N220K2.007	.6	.0	12.1	.0	.07	150.0	.0	17.0	1.5	0.	0.	150.	0.	0.	2.39
N220K2.005	.5	.0	10.3	.0	.02	150.0	-28.0	17.0	1.4	0.	0.	127.	0.	0.	.75
N220K2.004	.1	.0	.0	.0	.00	150.0	-56.0	17.0	.4	0.	0.	0.	0.	0.	.26
N220K3.010	.1	.0	.0	.0	.00	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.21
N220K3.009	.3	.0	19.1	.0	.01	150.0	56.0	17.0	.7	0.	0.	236.	0.	0.	.33
N220K3.008	.5	.0	11.9	.0	.03	150.0	28.0	17.0	1.3	0.	0.	146.	0.	0.	1.00
N220K3.007	.5	.0	14.8	.0	.04	150.0	.0	17.0	1.4	0.	0.	182.	0.	0.	1.22
N220K3.005	.3	.0	12.9	.0	.01	150.0	-28.0	17.0	.8	0.	0.	159.	0.	0.	.59
N220K3.004	.1	.0	.0	.0	.00	150.0	-56.0	17.0	.3	0.	0.	0.	0.	0.	.16
N220K4.010	.4	.0	7.4	.0	.00	150.0	75.0	17.0	.9	0.	0.	91.	0.	0.	.17
N220K4.009	.3	.0	4.8	.0	.01	150.0	56.0	17.0	.8	0.	0.	59.	0.	0.	.48
N220K4.008	.6	.0	10.6	.0	.04	150.0	28.0	17.0	1.7	0.	0.	130.	0.	0.	1.27
N220K4.007	.5	.0	16.5	.0	.04	150.0	.0	17.0	1.3	0.	0.	203.	0.	0.	1.24
N220K4.005	.2	.0	14.4	.0	.02	150.0	-28.0	17.0	.6	0.	0.	177.	0.	0.	.57
N220K4.004	.1	.0	.0	.0	.00	150.0	-56.0	17.0	.3	0.	0.	0.	0.	0.	.05
N220K5.010	.3	.0	16.4	.0	.00	150.0	75.0	17.0	.8	0.	0.	203.	0.	0.	.21
N220K5.009	.5	.0	12.7	.0	.01	150.0	56.0	17.0	1.2	0.	0.	157.	0.	0.	.58
N220K5.008	.6	.0	14.0	.0	.04	150.0	28.0	17.0	1.5	0.	0.	172.	0.	0.	1.31
N220K5.007	.6	.0	9.9	.0	.03	150.0	.0	17.0	1.6	0.	0.	122.	0.	0.	1.09
N220K5.005	.3	.0	3.5	.0	.01	150.0	-28.0	17.0	.9	0.	0.	44.	0.	0.	.30
N220K5.004	.1	.0	.0	.0	.01	150.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.43
N220L1.010	.4	.0	19.4	.0	.03	250.0	75.0	1.0	1.0	0.	0.	239.	0.	0.	1.19
N220L1.009	.4	.0	18.7	.0	.05	250.0	56.0	1.0	1.0	0.	0.	231.	0.	0.	1.59
N220L1.008	.4	.0	22.8	.0	.06	250.0	28.0	1.0	1.0	0.	0.	281.	0.	0.	2.21
N220L1.007	.3	.0	14.5	.0	.04	250.0	.0	1.0	.7	0.	0.	179.	0.	0.	1.41
N220L1.005	.2	.0	12.8	.0	.03	250.0	-28.0	1.0	.6	0.	0.	158.	0.	0.	1.02
N220L1.004	.1	.0	.0	.0	.02	250.0	-56.0	1.0	.4	0.	0.	0.	0.	0.	.74

FALCON 2: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220L2.010	.3	.0	21.1	.0	.04	250.0	75.0	1.0	.9	0.	0.	260.	0.	0.	1.35
N220L2.009	.4	.0	21.6	.0	.07	250.0	56.0	1.0	1.0	0.	0.	267.	0.	0.	2.44
N220L2.008	.3	.0	15.2	.0	.05	250.0	28.0	1.0	.9	0.	0.	187.	0.	0.	1.67
N220L2.007	.3	.0	21.0	.0	.06	250.0	.0	1.0	.7	0.	0.	258.	0.	0.	1.97
N220L2.005	.1	.0	.0	.0	.00	250.0	-28.0	1.0	.3	0.	0.	0.	0.	0.	.19
N220L2.004	.1	.0	.0	.0	-.01	250.0	-56.0	1.0	.1	0.	0.	0.	0.	0.	.03
N220L3.010	.2	.0	24.0	.0	.03	250.0	75.0	1.0	.6	0.	0.	296.	0.	0.	1.06
N220L3.009	.4	.0	20.5	.0	.07	250.0	56.0	1.0	1.0	0.	0.	253.	0.	0.	2.33
N220L3.008	.5	.0	15.1	.0	.05	250.0	28.0	1.0	1.2	0.	0.	186.	0.	0.	1.69
N220L3.007	.3	.0	15.2	.0	.03	250.0	.0	1.0	.8	0.	0.	187.	0.	0.	1.22
N220L3.005	.2	.0	15.4	.0	.02	250.0	-28.0	1.0	.6	0.	0.	189.	0.	0.	.75
N220L3.004	.1	.0	.0	.0	.01	250.0	-56.0	1.0	.3	0.	0.	0.	0.	0.	.39
N220L4.010	.4	.0	21.8	.0	.03	250.0	75.0	1.0	1.0	0.	0.	269.	0.	0.	1.28
N220L4.009	.4	.0	16.1	.0	.05	250.0	56.0	1.0	1.0	0.	0.	199.	0.	0.	1.79
N220L4.008	.4	.0	20.0	.0	.05	250.0	28.0	1.0	1.0	0.	0.	247.	0.	0.	1.73
N220L4.007	.3	.0	18.2	.0	.03	250.0	.0	1.0	.8	0.	0.	224.	0.	0.	1.01
N220L4.005	.3	.0	15.2	.0	.04	250.0	-28.0	1.0	.8	0.	0.	187.	0.	0.	1.25
N220L4.004	.1	.0	.0	.0	.01	250.0	-56.0	1.0	.3	0.	0.	0.	0.	0.	.29
N220L5.010	.4	.0	17.2	.0	.06	250.0	75.0	1.0	1.1	0.	0.	212.	0.	0.	2.04
N220L5.009	.4	.0	14.3	.0	.05	250.0	56.0	1.0	1.0	0.	0.	176.	0.	0.	1.68
N220L5.008	.3	.0	13.3	.0	.05	250.0	28.0	1.0	.8	0.	0.	164.	0.	0.	1.52
N220L5.007	.2	.0	.0	.0	.05	250.0	.0	1.0	.5	0.	0.	0.	0.	0.	1.68
N220L5.005	.2	.0	.0	.0	.01	250.0	-28.0	1.0	.4	0.	0.	0.	0.	0.	.45
N220L5.004	.1	.0	.0	.0	.01	250.0	-56.0	1.0	.4	0.	0.	0.	0.	0.	.55
N220M1.010	.4	.0	13.3	.0	.04	250.0	75.0	5.0	1.0	0.	0.	164.	0.	0.	1.44
N220M1.009	.4	.0	11.3	.0	.05	250.0	56.0	5.0	1.1	0.	0.	140.	0.	0.	1.75
N220M1.008	.3	.0	11.9	.0	.03	250.0	28.0	5.0	.9	0.	0.	147.	0.	0.	1.20
N220M1.007	.3	.0	11.2	.0	.04	250.0	.0	5.0	.8	0.	0.	138.	0.	0.	1.21
N220M1.005	.2	.0	.0	.0	.01	250.0	-28.0	5.0	.5	0.	0.	0.	0.	0.	.50
N220M1.004	.1	.0	.0	.0	.00	250.0	-56.0	5.0	.4	0.	0.	0.	0.	0.	.21
N220M2.010	.3	.0	16.4	.0	.01	250.0	75.0	5.0	.9	0.	0.	202.	0.	0.	.49
N220M2.009	.4	.0	18.0	.0	.03	250.0	56.0	5.0	1.1	0.	0.	222.	0.	0.	1.26
N220M2.008	.4	.0	15.9	.0	.03	250.0	28.0	5.0	1.2	0.	0.	196.	0.	0.	1.24
N220M2.007	.3	.0	16.9	.0	.02	250.0	.0	5.0	.9	0.	0.	208.	0.	0.	.85
N220M2.005	.2	.0	.0	.0	.01	250.0	-28.0	5.0	.5	0.	0.	0.	0.	0.	.45
N220M2.004	.1	.0	.0	.0	-.01	250.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.11
N220M3.010	.4	.0	15.0	.0	.04	250.0	75.0	5.0	1.0	0.	0.	185.	0.	0.	1.35
N220M3.009	.5	.0	15.6	.0	.06	250.0	56.0	5.0	1.3	0.	0.	192.	0.	0.	2.16
N220M3.008	.5	.0	18.1	.0	.05	250.0	28.0	5.0	1.3	0.	0.	224.	0.	0.	1.77
N220M3.007	.3	.0	18.7	.0	.02	250.0	.0	5.0	.9	0.	0.	230.	0.	0.	.99
N220M3.005	.4	.0	20.2	.0	.01	250.0	-28.0	5.0	1.0	0.	0.	249.	0.	0.	.50
N220M3.004	.1	.0	.0	.0	.00	250.0	-56.0	5.0	.2	0.	0.	0.	0.	0.	.22

FALCON 2: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N220M4.010	.3	.0	13.3	.0	.02	250.0	75.0	5.0	.9	0.	0.	163.	0.	0.	.68
N220M4.009	.4	.0	15.2	.0	.04	250.0	56.0	5.0	.9	0.	0.	187.	0.	0.	1.30
N220M4.008	.4	.0	15.3	.0	.05	250.0	28.0	5.0	1.1	0.	0.	188.	0.	0.	1.66
N220M4.007	.3	.0	15.1	.0	.03	250.0	.0	5.0	.9	0.	0.	186.	0.	0.	.97
N220M4.005	.2	.0	16.8	.0	.02	250.0	-28.0	5.0	.6	0.	0.	207.	0.	0.	.77
N220M4.004	.1	.0	.0	.0	.00	250.0	-56.0	5.0	.3	0.	0.	0.	0.	0.	.30
N220M5.010	.3	.0	13.8	.0	.04	250.0	75.0	5.0	.9	0.	0.	170.	0.	0.	1.36
N220M5.009	.4	.0	14.8	.0	.04	250.0	56.0	5.0	1.0	0.	0.	182.	0.	0.	1.51
N220M5.008	.5	.0	14.2	.0	.06	250.0	28.0	5.0	1.3	0.	0.	175.	0.	0.	2.05
N220M5.007	.4	.0	14.9	.0	.04	250.0	.0	5.0	1.0	0.	0.	184.	0.	0.	1.49
N220M5.005	.3	.0	11.7	.0	.04	250.0	-28.0	5.0	.8	0.	0.	144.	0.	0.	1.22
N220M5.004	.1	.0	.0	.0	.03	250.0	-56.0	5.0	.4	0.	0.	0.	0.	0.	1.09
N220N1.010	.4	.0	16.0	.0	.02	250.0	75.0	11.0	1.2	0.	0.	197.	0.	0.	.76
N220N1.009	.5	.0	16.2	.0	.03	250.0	56.0	11.0	1.3	0.	0.	200.	0.	0.	1.08
N220N1.008	.4	.0	16.4	.0	.03	250.0	28.0	11.0	1.1	0.	0.	202.	0.	0.	1.11
N220N1.007	.3	.0	16.7	.0	.02	250.0	.0	11.0	.9	0.	0.	206.	0.	0.	.86
N220N1.005	.2	.0	.0	.0	.00	250.0	-28.0	11.0	.4	0.	0.	0.	0.	0.	.18
N220N1.004	.1	.0	.0	.0	.01	250.0	-56.0	11.0	.3	0.	0.	0.	0.	0.	.45
N220N2.010	.4	.0	17.3	.0	.02	250.0	75.0	11.0	1.1	0.	0.	213.	0.	0.	.69
N220N2.009	.4	.0	16.3	.0	.03	250.0	56.0	11.0	1.0	0.	0.	201.	0.	0.	1.22
N220N2.008	.4	.0	13.0	.0	.03	250.0	28.0	11.0	1.0	0.	0.	160.	0.	0.	1.05
N220N2.007	.3	.0	22.0	.0	.01	250.0	.0	11.0	.8	0.	0.	271.	0.	0.	.42
N220N2.005	.2	.0	.0	.0	.00	250.0	-28.0	11.0	.4	0.	0.	0.	0.	0.	.19
N220N2.004	.0	.0	.0	.0	.00	250.0	-56.0	11.0	.1	0.	0.	0.	0.	0.	.15
N220N3.010	.4	.0	17.2	.0	.02	250.0	75.0	11.0	1.0	0.	0.	211.	0.	0.	.63
N220N3.009	.4	.0	17.2	.0	.03	250.0	56.0	11.0	1.0	0.	0.	212.	0.	0.	1.02
N220N3.008	.4	.0	11.4	.0	.04	250.0	28.0	11.0	1.0	0.	0.	140.	0.	0.	1.36
N220N3.007	.3	.0	13.6	.0	.01	250.0	.0	11.0	.7	0.	0.	167.	0.	0.	.53
N220N3.005	.1	.0	.0	.0	.00	250.0	-28.0	11.0	.4	0.	0.	0.	0.	0.	.28
N220N3.004	.1	.0	.0	.0	-.01	250.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.06
N220N4.010	.5	.0	12.2	.0	.03	250.0	75.0	11.0	1.3	0.	0.	150.	0.	0.	1.13
N220N4.009	.3	.0	12.2	.0	.03	250.0	56.0	11.0	.8	0.	0.	150.	0.	0.	1.19
N220N4.008	.4	.0	14.6	.0	.03	250.0	28.0	11.0	1.1	0.	0.	180.	0.	0.	1.06
N220N4.007	.3	.0	17.0	.0	.01	250.0	.0	11.0	.9	0.	0.	210.	0.	0.	.49
N220N4.005	.2	.0	.0	.0	.00	250.0	-28.0	11.0	.5	0.	0.	0.	0.	0.	.24
N220N4.004	.1	.0	.0	.0	.01	250.0	-56.0	11.0	.3	0.	0.	0.	0.	0.	.47
N220N5.010	.4	.0	13.4	.0	.03	250.0	75.0	11.0	1.0	0.	0.	165.	0.	0.	1.16
N220N5.009	.4	.0	17.3	.0	.03	250.0	56.0	11.0	1.1	0.	0.	213.	0.	0.	1.09
N220N5.008	.4	.0	17.4	.0	.04	250.0	28.0	11.0	1.0	0.	0.	215.	0.	0.	1.33
N220N5.007	.2	.0	22.0	.0	.03	250.0	.0	11.0	.7	0.	0.	271.	0.	0.	.94
N220N5.005	.1	.0	.0	.0	.00	250.0	-28.0	11.0	.3	0.	0.	0.	0.	0.	.10
N220N5.004	.1	.0	.0	.0	.00	250.0	-56.0	11.0	.2	0.	0.	0.	0.	0.	.19

FALCON 2: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N22001.010	.3	.0	14.2	.0	.00	250.0	75.0	17.0	.8	0.	0.	175.	0.	0.	.34
N22001.009	.3	.0	18.4	.0	.01	250.0	56.0	17.0	.9	0.	0.	226.	0.	0.	.51
N22001.008	.4	.0	6.0	.0	.01	250.0	28.0	17.0	1.1	0.	0.	74.	0.	0.	.74
N22001.007	.3	.0	14.1	.0	.00	250.0	.0	17.0	.9	0.	0.	174.	0.	0.	.41
N22001.005	.2	.0	16.5	.0	.02	250.0	-28.0	17.0	.6	0.	0.	203.	0.	0.	.57
N22001.004	.1	.0	.0	.0	.01	250.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.42
N22002.010	.3	.0	9.7	.0	.03	250.0	75.0	17.0	.8	0.	0.	120.	0.	0.	.92
N22002.009	.4	.0	20.5	.0	.02	250.0	56.0	17.0	1.1	0.	0.	253.	0.	0.	.97
N22002.008	.4	.0	17.4	.0	.03	250.0	28.0	17.0	1.0	0.	0.	214.	0.	0.	1.02
N22002.007	.2	.0	12.4	.0	.01	250.0	.0	17.0	.6	0.	0.	152.	0.	0.	.40
N22002.005	.1	.0	.0	.0	.00	250.0	-28.0	17.0	.3	0.	0.	0.	0.	0.	.14
N22002.004	.1	.0	.0	.0	.00	250.0	-56.0	17.0	.1	0.	0.	0.	0.	0.	.08
N22003.010	.3	.0	13.7	.0	.01	250.0	75.0	17.0	.8	0.	0.	169.	0.	0.	.47
N22003.009	.3	.0	21.5	.0	.02	250.0	56.0	17.0	.9	0.	0.	265.	0.	0.	.79
N22003.008	.4	.0	17.4	.0	.03	250.0	28.0	17.0	1.1	0.	0.	215.	0.	0.	.95
N22003.007	.3	.0	13.9	.0	.02	250.0	.0	17.0	.8	0.	0.	172.	0.	0.	.58
N22003.005	.2	.0	.0	.0	.01	250.0	-28.0	17.0	.5	0.	0.	0.	0.	0.	.46
N22003.004	.1	.0	.0	.0	.01	250.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.37
N22004.010	.3	.0	14.8	.0	.01	250.0	75.0	17.0	.9	0.	0.	183.	0.	0.	.43
N22004.009	.4	.0	17.3	.0	.04	250.0	56.0	17.0	1.1	0.	0.	213.	0.	0.	1.26
N22004.008	.4	.0	18.2	.0	.02	250.0	28.0	17.0	1.0	0.	0.	224.	0.	0.	.79
N22004.007	.2	.0	.0	.0	.00	250.0	.0	17.0	.5	0.	0.	0.	0.	0.	.22
N22004.005	.2	.0	.0	.0	.01	250.0	-28.0	17.0	.4	0.	0.	0.	0.	0.	.24
N22004.004	.1	.0	.0	.0	.00	250.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.11
N22005.010	.4	.0	20.1	.0	.02	250.0	75.0	17.0	1.1	0.	0.	247.	0.	0.	.83
N22005.009	.7	.0	18.2	.0	.12	250.0	56.0	17.0	1.9	0.	0.	224.	0.	0.	4.74
N22005.008	.4	.0	9.9	.0	.03	250.0	28.0	17.0	1.1	0.	0.	122.	0.	0.	1.12
N22005.007	.3	.0	17.4	.0	.02	250.0	.0	17.0	.7	0.	0.	214.	0.	0.	.66
N22005.005	.1	.0	.0	.0	.01	250.0	-28.0	17.0	.3	0.	0.	0.	0.	0.	.49
N22005.004	.1	.0	.0	.0	.01	250.0	-56.0	17.0	.2	0.	0.	0.	0.	0.	.41

FALCON 3: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310A1.004	1.5	15.0	17.4	17.5	.02	-62.0	40.0	2.0	3.9	0.	0.	152.	0.	0.	0.81
N310A1.005	9.1	9.2	19.8	60.9	.41	-62.0	30.0	2.0	21.3	110.	172.	172.	173.	311.	9.47
N310A1.006	30.9	2.1	21.6	90.8	10.98	-62.0	20.0	2.0	54.7	20.	21.	188.	580.	663.	194.71
N310A1.007	31.7	3.0	18.0	86.3	11.09	-62.0	10.0	2.0	55.6	27.	28.	157.	627.	705.	197.17
N310A1.008	30.8	2.2	21.0	91.7	10.57	-62.0	.0	2.0	54.6	19.	21.	183.	646.	744.	190.20
N310A1.009	30.9	2.4	23.9	89.4	10.18	-62.0	-10.0	2.0	54.7	24.	39.	208.	600.	712.	184.30
N310A1.010	30.6	2.2	18.6	86.4	10.22	-62.0	-20.0	2.0	54.4	19.	19.	162.	575.	654.	182.93
N310A2.004	1.1	31.0	31.0	31.0	.05	-62.0	40.0	2.0	3.0	0.	0.	270.	0.	0.	1.31
N310A2.005	2.6	15.2	41.1	73.6	.38	-62.0	30.0	2.0	6.6	147.	0.	358.	0.	358.	8.97
N310A2.006	31.4	2.2	20.0	87.3	13.64	-62.0	20.0	2.0	55.3	20.	40.	174.	705.	756.	238.66
N310A2.007	32.4	2.4	21.7	97.2	13.43	-62.0	10.0	2.0	56.4	21.	22.	189.	678.	846.	235.83
N310A2.008	32.2	1.8	21.6	99.2	13.04	-62.0	.0	2.0	56.3	16.	18.	188.	746.	855.	229.09
N310A2.009	31.5	2.0	21.4	99.2	12.57	-62.0	-10.0	2.0	55.4	30.	31.	186.	698.	804.	223.91
N310A2.010	31.8	2.5	22.3	89.0	12.52	-62.0	-20.0	2.0	55.8	22.	23.	195.	692.	755.	221.05
N310A3.004	2.5	20.5	21.9	27.6	.06	-62.0	40.0	2.0	6.4	191.	0.	191.	0.	192.	1.46
N310A3.005	5.4	11.0	20.7	63.4	.33	-62.0	30.0	2.0	13.4	120.	180.	180.	183.	332.	7.61
N310A3.006	31.2	3.3	20.7	95.5	13.48	-62.0	20.0	2.0	55.0	29.	29.	180.	698.	784.	235.54
N310A3.007	32.2	2.0	21.6	95.0	12.99	-62.0	10.0	2.0	56.2	19.	19.	188.	645.	798.	228.34
N310A3.008	32.3	1.9	21.6	96.8	12.65	-62.0	.0	2.0	56.4	17.	28.	189.	643.	776.	222.89
N310A3.009	30.7	2.0	21.3	99.3	11.61	-62.0	-10.0	2.0	54.5	24.	26.	186.	665.	786.	208.79
N310A3.010	34.6	2.7	19.6	96.0	12.53	-62.0	-20.0	2.0	58.8	24.	24.	171.	645.	810.	221.58
N310A4.004	1.8	20.0	20.5	21.0	.02	-62.0	40.0	2.0	4.8	0.	0.	178.	0.	0.	.66
N310A4.005	2.4	12.0	43.6	68.5	.31	-62.0	30.0	2.0	6.3	105.	0.	380.	0.	382.	7.25
N310A4.006	32.0	2.4	18.6	98.9	13.53	-62.0	20.0	2.0	56.0	22.	25.	162.	699.	799.	236.97
N310A4.007	32.5	2.9	19.7	100.0	13.26	-62.0	10.0	2.0	56.6	26.	27.	172.	722.	862.	233.36
N310A4.008	32.0	2.9	20.4	95.4	13.06	-62.0	.0	2.0	56.0	26.	35.	178.	670.	828.	228.63
N310A4.009	32.4	2.4	19.6	95.4	12.15	-62.0	-10.0	2.0	56.4	21.	29.	171.	663.	775.	217.61
N310A4.010	31.7	3.7	22.3	95.6	13.34	-62.0	-20.0	2.0	55.6	33.	35.	194.	720.	811.	235.81
N310A5.004	1.5	18.5	33.0	33.1	.02	-62.0	40.0	2.0	3.9	0.	0.	288.	0.	0.	.67
N310A5.005	3.1	11.2	31.8	75.6	.33	-62.0	30.0	2.0	7.9	126.	0.	278.	0.	278.	7.78
N310A5.006	31.0	3.2	19.1	89.9	13.09	-62.0	20.0	2.0	54.8	28.	28.	167.	674.	782.	228.80
N310A5.007	30.4	3.5	19.0	94.4	12.65	-62.0	10.0	2.0	54.2	31.	35.	166.	715.	807.	222.26
N310A5.008	32.0	3.1	22.6	92.8	12.54	-62.0	.0	2.0	55.9	27.	28.	197.	645.	738.	220.94
N310A5.009	33.6	1.7	20.3	96.8	11.79	-62.0	-10.0	2.0	57.8	15.	36.	177.	643.	722.	210.94
N310A5.010	34.5	2.9	17.7	92.3	12.11	-62.0	-20.0	2.0	58.8	25.	34.	154.	686.	772.	214.29
N310B1.004	.9	.0	32.0	.0	.10	-32.0	40.0	1.0	2.5	0.	0.	279.	0.	0.	2.54
N310B1.005	1.8	19.9	24.7	34.3	.29	-32.0	30.0	1.0	4.7	0.	0.	215.	0.	0.	6.94
N310B1.006	40.0	.7	16.8	87.7	12.68	-32.0	20.0	1.0	64.3	7.	13.	147.	645.	652.	215.63
N310B1.007	52.2	.4	17.6	99.4	15.66	-32.0	10.0	1.0	74.7	5.	6.	154.	733.	864.	252.20
N310B1.008	40.3	1.4	16.5	99.3	11.77	-32.0	.0	1.0	64.6	13.	16.	144.	591.	865.	199.15
N310B1.009	54.6	.5	17.1	77.7	15.28	-32.0	-10.0	1.0	76.5	5.	7.	149.	567.	677.	233.38
N310B1.010	48.8	1.1	17.4	91.3	13.94	-32.0	-20.0	1.0	72.0	10.	11.	152.	568.	699.	226.35

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310B2.004	1.6	13.9	18.0	41.6	.23	-32.0	40.0	1.0	4.1	0.	0.	157.	0.	0.	5.35
N310B2.005	1.6	13.9	20.7	42.6	.39	-32.0	30.0	1.0	4.2	0.	0.	181.	0.	0.	9.19
N310B2.006	40.1	.9	18.6	83.7	12.29	-32.0	20.0	1.0	64.4	8.	9.	162.	604.	645.	207.78
N310B2.007	52.3	.7	14.6	98.4	15.59	-32.0	10.0	1.0	74.8	6.	7.	127.	648.	841.	250.80
N310B2.008	38.2	1.0	19.3	88.0	11.05	-32.0	.0	1.0	62.6	9.	19.	168.	486.	767.	186.92
N310B2.009	54.7	.4	17.4	76.1	14.14	-32.0	-10.0	1.0	76.6	3.	7.	152.	521.	663.	217.27
N310B2.010	48.3	1.2	15.9	91.3	13.27	-32.0	-20.0	1.0	71.6	11.	12.	139.	564.	663.	218.16
N310B3.004	1.0	.0	31.3	.0	.09	-32.0	40.0	1.0	2.5	0.	0.	273.	0.	0.	2.38
N310B3.005	2.1	12.5	23.8	39.1	.34	-32.0	30.0	1.0	5.4	207.	0.	207.	0.	207.	7.91
N310B3.006	39.7	.9	18.2	84.4	13.26	-32.0	20.0	1.0	64.1	8.	8.	159.	607.	732.	222.83
N310B3.007	53.0	.7	18.6	89.3	16.14	-32.0	10.0	1.0	75.3	7.	7.	162.	588.	729.	256.33
N310B3.008	37.6	1.4	18.2	99.9	13.26	-32.0	.0	1.0	62.0	15.	19.	159.	673.	848.	228.11
N310B3.009	55.4	.5	17.7	86.0	16.53	-32.0	-10.0	1.0	77.1	5.	12.	154.	616.	750.	253.96
N310B3.010	52.2	1.4	18.4	88.8	14.80	-32.0	-20.0	1.0	74.7	12.	13.	160.	587.	760.	239.72
N310B4.004	1.7	18.6	26.0	26.5	.13	-32.0	40.0	1.0	4.4	0.	0.	227.	0.	0.	3.23
N310B4.005	2.2	14.8	25.4	47.4	.32	-32.0	30.0	1.0	5.6	222.	0.	222.	0.	225.	7.58
N310B4.006	39.1	1.7	19.0	89.0	12.27	-32.0	20.0	1.0	63.4	15.	16.	166.	539.	632.	208.84
N310B4.007	53.6	1.0	17.8	94.5	15.32	-32.0	10.0	1.0	75.8	9.	10.	155.	668.	736.	244.91
N310B4.008	40.1	1.3	20.5	78.7	11.44	-32.0	.0	1.0	64.4	12.	12.	179.	554.	661.	198.07
N310B4.009	55.6	1.0	18.6	62.7	14.37	-32.0	-10.0	1.0	77.2	9.	10.	162.	543.	545.	221.43
N310B4.010	49.7	.9	18.6	97.7	13.52	-32.0	-20.0	1.0	72.8	11.	11.	162.	543.	605.	219.16
N310B5.004	1.7	19.4	22.6	38.8	.20	-32.0	40.0	1.0	4.4	0.	0.	197.	0.	0.	4.79
N310B5.005	2.4	13.7	19.5	38.7	.34	-32.0	30.0	1.0	6.2	121.	0.	170.	0.	330.	8.07
N310B5.006	36.9	2.3	22.5	86.2	11.40	-32.0	20.0	1.0	61.3	20.	20.	196.	536.	660.	195.98
N310B5.007	51.1	.7	18.9	90.3	13.74	-32.0	10.0	1.0	73.8	8.	12.	165.	644.	785.	224.88
N310B5.008	34.0	1.0	19.1	93.2	11.75	-32.0	.0	1.0	58.2	9.	9.	167.	593.	773.	202.71
N310B5.009	53.3	.5	18.3	90.6	15.17	-32.0	-10.0	1.0	75.5	4.	5.	160.	534.	622.	232.91
N310B5.010	46.7	.9	20.7	88.3	13.70	-32.0	-20.0	1.0	70.3	9.	11.	180.	576.	630.	223.25
N310C1.004	1.3	14.8	23.9	30.7	.24	-2.0	40.0	1.0	3.5	0.	0.	208.	0.	0.	5.73
N310C1.005	2.3	14.5	14.6	33.6	.31	-2.0	30.0	1.0	6.0	127.	0.	127.	0.	164.	7.28
N310C1.006	27.2	2.0	23.3	86.4	7.64	-2.0	20.0	1.0	50.3	17.	19.	203.	486.	614.	144.51
N310C1.007	30.1	3.1	26.7	77.2	7.55	-2.0	10.0	1.0	53.8	28.	37.	232.	652.	660.	139.04
N310C1.008	30.2	3.9	20.6	71.6	6.76	-2.0	.0	1.0	53.9	35.	35.	179.	438.	499.	122.43
N310C1.009	34.2	3.6	19.4	71.5	6.06	-2.0	-10.0	1.0	58.5	45.	59.	169.	434.	436.	108.20
N310C1.010	30.0	5.4	19.0	85.2	6.85	-2.0	-20.0	1.0	53.7	53.	54.	166.	433.	570.	123.74
N310C2.004	1.3	20.9	20.9	26.4	.24	-2.0	40.0	1.0	3.5	0.	0.	183.	0.	0.	5.63
N310C2.005	2.0	19.1	20.7	30.7	.29	-2.0	30.0	1.0	5.3	180.	0.	180.	0.	181.	6.78
N310C2.006	24.7	1.7	27.0	73.0	8.38	-2.0	20.0	1.0	47.0	15.	16.	235.	575.	627.	156.79
N310C2.007	31.0	3.9	24.5	67.7	7.69	-2.0	10.0	1.0	54.8	35.	37.	214.	494.	567.	140.95
N310C2.008	33.6	6.6	21.4	67.9	6.32	-2.0	.0	1.0	57.8	60.	61.	186.	475.	490.	112.18
N310C2.009	36.4	2.1	20.5	63.6	6.83	-2.0	-10.0	1.0	60.7	61.	62.	178.	423.	492.	118.50
N310C2.010	33.9	3.1	18.8	66.7	7.26	-2.0	-20.0	1.0	58.0	59.	60.	164.	429.	493.	127.85

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310C3.004	1.7	21.2	23.2	30.3	.23	-2.0	40.0	1.0	4.4	0.	0.	202.	0.	0.	5.53
N310C3.005	2.0	14.9	15.0	41.1	.35	-2.0	30.0	1.0	5.1	131.	0.	131.	0.	131.	8.24
N310C3.006	28.2	3.0	24.6	62.1	7.31	-2.0	20.0	1.0	51.5	26.	28.	215.	472.	521.	135.87
N310C3.007	32.5	3.4	24.2	90.4	7.36	-2.0	10.0	1.0	56.5	34.	35.	211.	442.	583.	134.25
N310C3.008	32.9	3.5	24.6	72.2	6.45	-2.0	.0	1.0	57.0	30.	30.	214.	395.	471.	113.98
N310C3.009	36.4	4.2	19.5	64.6	6.85	-2.0	-10.0	1.0	60.8	36.	37.	170.	393.	548.	117.95
N310C3.010	33.1	4.7	20.6	80.5	6.80	-2.0	-20.0	1.0	57.3	41.	41.	180.	427.	563.	119.17
N310C4.004	1.5	18.2	24.0	32.1	.22	-2.0	40.0	1.0	3.9	0.	0.	209.	0.	0.	5.25
N310C4.005	1.8	16.0	24.8	32.5	.30	-2.0	30.0	1.0	4.6	0.	0.	216.	0.	0.	7.15
N310C4.006	28.0	2.5	25.4	86.2	7.19	-2.0	20.0	1.0	51.2	22.	23.	221.	478.	496.	133.44
N310C4.007	30.8	3.6	22.6	93.5	7.58	-2.0	10.0	1.0	54.6	33.	35.	197.	466.	731.	138.64
N310C4.008	33.5	3.6	22.1	68.9	7.39	-2.0	.0	1.0	57.7	34.	36.	193.	402.	565.	130.61
N310C4.009	36.7	3.5	21.0	79.3	7.15	-2.0	-10.0	1.0	61.1	31.	50.	183.	405.	618.	124.26
N310C4.010	38.6	5.2	20.1	79.4	7.52	-2.0	-20.0	1.0	63.0	45.	46.	175.	380.	622.	133.49
N310C5.004	1.8	18.4	23.8	26.9	.27	-2.0	40.0	1.0	4.7	0.	0.	208.	0.	0.	6.30
N310C5.005	2.0	15.9	23.5	37.8	.29	-2.0	30.0	1.0	5.3	139.	0.	205.	0.	205.	6.96
N310C5.006	26.0	1.9	19.4	64.3	8.02	-2.0	20.0	1.0	48.7	17.	20.	169.	496.	555.	148.84
N310C5.007	30.7	2.2	24.2	91.2	8.36	-2.0	10.0	1.0	54.5	20.	36.	211.	543.	788.	153.19
N310C5.008	32.0	3.4	23.2	75.1	7.48	-2.0	.0	1.0	56.0	30.	32.	202.	537.	538.	134.48
N310C5.009	35.0	3.5	22.1	79.0	7.69	-2.0	-10.0	1.0	59.3	32.	62.	193.	526.	554.	134.78
N310C5.010	37.6	3.6	21.2	94.2	8.12	-2.0	-20.0	1.0	61.9	32.	40.	184.	530.	808.	144.69
N310D1.004	.1	.0	.0	.0	-.03	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.09
N310D1.005	.6	.0	32.2	.0	.04	50.0	55.0	1.0	1.6	0.	0.	281.	0.	0.	1.26
N310D1.006	1.0	19.3	24.2	24.2	.20	50.0	44.0	1.0	2.7	0.	0.	211.	0.	0.	4.66
N310D1.007	1.5	14.3	20.0	53.8	.29	50.0	33.0	1.0	4.0	0.	0.	174.	0.	0.	6.87
N310D1.008	1.9	6.5	18.8	42.8	.42	50.0	22.0	1.0	5.1	164.	0.	164.	0.	164.	9.85
N310D1.009	1.9	7.4	19.0	43.5	.48	50.0	11.0	1.0	4.9	0.	0.	166.	0.	0.	11.22
N310D1.010	1.8	17.1	21.2	34.8	.39	50.0	.0	1.0	4.8	0.	0.	185.	0.	0.	9.17
N310D2.004	.2	.0	28.5	.0	.04	50.0	66.0	1.0	.6	0.	0.	249.	0.	0.	1.08
N310D2.005	.8	.0	28.1	.0	.07	50.0	55.0	1.0	2.2	0.	0.	245.	0.	0.	1.63
N310D2.006	.9	.0	23.9	.0	.14	50.0	44.0	1.0	2.5	0.	0.	209.	0.	0.	3.40
N310D2.007	2.4	8.6	16.0	27.9	.15	50.0	33.0	1.0	6.3	139.	0.	139.	0.	140.	3.98
N310D2.008	1.7	6.2	21.7	29.2	.30	50.0	22.0	1.0	4.5	0.	0.	189.	0.	0.	6.98
N310D2.009	1.7	6.4	16.4	33.5	.44	50.0	11.0	1.0	4.5	0.	0.	143.	0.	0.	10.23
N310D2.010	1.7	6.8	23.5	35.6	.44	50.0	.0	1.0	4.5	0.	0.	205.	0.	0.	10.24
N310D3.004	.1	.0	.0	.0	-.01	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.30
N310D3.005	.5	.0	26.5	.0	.01	50.0	55.0	1.0	1.3	0.	0.	231.	0.	0.	.69
N310D3.006	.8	.0	24.5	.0	.11	50.0	44.0	1.0	2.2	0.	0.	214.	0.	0.	2.72
N310D3.007	1.7	14.2	19.8	26.7	.16	50.0	33.0	1.0	4.4	0.	0.	173.	0.	0.	3.96
N310D3.008	1.4	15.0	20.4	28.1	.23	50.0	22.0	1.0	3.6	0.	0.	178.	0.	0.	5.50
N310D3.009	2.0	11.6	17.2	32.4	.40	50.0	11.0	1.0	5.2	149.	0.	150.	0.	150.	9.36
N310D3.010	1.4	14.0	17.9	36.0	.41	50.0	.0	1.0	3.6	0.	0.	156.	0.	0.	9.69

FALCON 3: LSR = 100, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310D4.004	.1	.0	.0	.0	.01	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.55
N310D4.005	.5	.0	32.1	.0	.01	50.0	55.0	1.0	1.3	0.	0.	280.	0.	0.	.59
N310D4.006	1.0	28.7	28.7	28.8	.11	50.0	44.0	1.0	2.7	0.	0.	251.	0.	0.	2.64
N310D4.007	1.6	16.0	21.2	25.5	.21	50.0	33.0	1.0	4.3	0.	0.	185.	0.	0.	5.04
N310D4.008	2.0	12.1	22.5	46.1	.29	50.0	22.0	1.0	5.3	196.	0.	196.	0.	197.	6.77
N310D4.009	2.0	12.5	21.1	38.5	.45	50.0	11.0	1.0	5.3	184.	0.	184.	0.	196.	10.53
N310D4.010	1.5	18.5	23.3	32.0	.41	50.0	.0	1.0	4.0	0.	0.	203.	0.	0.	9.64
N310D5.004	.2	.0	16.4	.0	.04	50.0	66.0	1.0	.6	0.	0.	143.	0.	0.	1.14
N310D5.005	1.0	.0	24.8	.0	.01	50.0	55.0	1.0	2.6	0.	0.	217.	0.	0.	.56
N310D5.006	.9	.0	24.8	.0	.17	50.0	44.0	1.0	2.3	0.	0.	216.	0.	0.	4.03
N310D5.007	1.2	23.4	23.5	23.8	.23	50.0	33.0	1.0	3.3	0.	0.	205.	0.	0.	5.41
N310D5.008	2.7	7.4	19.2	44.2	.29	50.0	22.0	1.0	7.1	166.	0.	167.	0.	168.	6.98
N310D5.009	1.9	6.7	22.7	45.2	.45	50.0	11.0	1.0	4.9	0.	0.	198.	0.	0.	10.46
N310D5.010	1.5	15.3	22.9	31.0	.40	50.0	.0	1.0	4.0	0.	0.	200.	0.	0.	9.46
N310E1.004	.5	.0	26.5	.0	.03	50.0	66.0	5.0	1.2	0.	0.	231.	0.	0.	.68
N310E1.005	.7	.0	23.0	.0	.03	50.0	55.0	5.0	1.9	0.	0.	200.	0.	0.	.81
N310E1.006	.7	.0	17.5	.0	.07	50.0	44.0	5.0	1.8	0.	0.	152.	0.	0.	1.64
N310E1.007	1.7	15.2	22.0	27.5	.15	50.0	33.0	5.0	4.6	0.	0.	192.	0.	0.	3.56
N310E1.008	1.6	18.8	27.4	39.2	.28	50.0	22.0	5.0	4.3	0.	0.	239.	0.	0.	6.55
N310E1.009	1.7	17.2	27.8	41.5	.39	50.0	11.0	5.0	4.5	0.	0.	242.	0.	0.	9.24
N310E1.010	1.5	20.0	27.7	48.3	.39	50.0	.0	5.0	4.0	0.	0.	242.	0.	0.	9.10
N310E2.004	.3	.0	25.5	.0	.00	50.0	66.0	5.0	.8	0.	0.	223.	0.	0.	.30
N310E2.005	.7	.0	25.5	.0	.05	50.0	55.0	5.0	1.9	0.	0.	222.	0.	0.	1.11
N310E2.006	.9	.0	25.1	.0	.10	50.0	44.0	5.0	2.5	0.	0.	218.	0.	0.	2.30
N310E2.007	1.6	17.6	21.4	25.0	.10	50.0	33.0	5.0	4.2	0.	0.	186.	0.	0.	2.52
N310E2.008	2.6	15.4	21.8	39.0	.26	50.0	22.0	5.0	6.7	189.	0.	190.	0.	191.	6.29
N310E2.009	2.0	9.1	22.3	46.7	.40	50.0	11.0	5.0	5.1	194.	0.	194.	0.	194.	9.35
N310E2.010	1.6	15.3	21.8	40.1	.40	50.0	.0	5.0	4.1	0.	0.	190.	0.	0.	9.34
N310E3.004	.1	.0	.0	.0	.00	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.09
N310E3.005	.6	.0	27.2	.0	.02	50.0	55.0	5.0	1.6	0.	0.	237.	0.	0.	.69
N310E3.006	.9	.0	22.8	.0	.06	50.0	44.0	5.0	2.5	0.	0.	199.	0.	0.	1.58
N310E3.007	1.2	20.2	20.2	22.9	.09	50.0	33.0	5.0	3.3	0.	0.	176.	0.	0.	2.41
N310E3.008	2.0	11.2	19.8	31.4	.26	50.0	22.0	5.0	5.1	172.	0.	172.	0.	173.	6.33
N310E3.009	2.1	15.0	19.8	44.7	.42	50.0	11.0	5.0	5.5	173.	0.	173.	0.	173.	9.74
N310E3.010	1.6	13.8	20.0	35.8	.43	50.0	.0	5.0	4.2	0.	0.	175.	0.	0.	10.11
N310E4.004	.5	.0	29.8	.0	.03	50.0	66.0	5.0	1.4	0.	0.	260.	0.	0.	.70
N310E4.005	1.0	.0	27.3	.0	.08	50.0	55.0	5.0	2.5	0.	0.	238.	0.	0.	1.81
N310E4.006	1.0	.0	21.6	.0	.10	50.0	44.0	5.0	2.5	0.	0.	189.	0.	0.	2.39
N310E4.007	1.5	21.2	27.6	27.7	.15	50.0	33.0	5.0	3.9	0.	0.	240.	0.	0.	3.66
N310E4.008	1.7	14.9	21.6	45.6	.31	50.0	22.0	5.0	4.4	0.	0.	188.	0.	0.	7.47
N310E4.009	1.6	7.0	17.8	44.6	.39	50.0	11.0	5.0	4.1	0.	0.	155.	0.	0.	9.16
N310E4.010	1.7	17.4	21.8	36.2	.37	50.0	.0	5.0	4.4	0.	0.	190.	0.	0.	8.79

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310E5.004	.1	.0	.0	.0	-.01	50.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.15
N310E5.005	.7	.0	26.0	.0	-.01	50.0	55.0	5.0	1.8	0.	0.	227.	0.	0.	.32
N310E5.006	1.2	22.5	22.5	22.5	.06	50.0	44.0	5.0	3.2	0.	0.	196.	0.	0.	1.48
N310E5.007	1.4	10.7	15.7	28.4	.13	50.0	33.0	5.0	3.7	0.	0.	137.	0.	0.	3.03
N310E5.008	2.0	13.5	15.8	34.2	.27	50.0	22.0	5.0	5.2	138.	0.	138.	0.	138.	6.50
N310E5.009	1.9	13.6	21.6	37.1	.41	50.0	11.0	5.0	4.9	0.	0.	189.	0.	0.	9.60
N310E5.010	2.1	13.5	13.6	39.2	.43	50.0	.0	5.0	5.6	118.	0.	118.	0.	119.	10.10
N310F1.004	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.28
N310F1.005	.5	.0	23.4	.0	.00	50.0	55.0	11.0	1.3	0.	0.	204.	0.	0.	.07
N310F1.006	.8	.0	18.4	.0	.04	50.0	44.0	11.0	2.1	0.	0.	160.	0.	0.	1.02
N310F1.007	.9	.0	24.3	.0	.07	50.0	33.0	11.0	2.3	0.	0.	212.	0.	0.	1.60
N310F1.008	1.4	14.4	20.9	27.0	.17	50.0	22.0	11.0	3.8	0.	0.	182.	0.	0.	4.20
N310F1.009	1.8	15.8	22.4	61.7	.34	50.0	11.0	11.0	4.6	0.	0.	195.	0.	0.	8.07
N310F1.010	1.7	8.3	18.3	42.5	.30	50.0	.0	11.0	4.5	0.	0.	160.	0.	0.	7.16
N310F2.004	.1	.0	.0	.0	.00	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.25
N310F2.005	.5	.0	30.7	.0	.02	50.0	55.0	11.0	1.4	0.	0.	268.	0.	0.	.44
N310F2.006	.5	.0	30.0	.0	.02	50.0	44.0	11.0	1.4	0.	0.	262.	0.	0.	.59
N310F2.007	.9	.0	5.4	.0	.06	50.0	33.0	11.0	2.5	0.	0.	47.	0.	0.	1.56
N310F2.008	1.5	12.9	28.9	33.3	.20	50.0	22.0	11.0	3.9	0.	0.	252.	0.	0.	4.83
N310F2.009	1.5	13.4	22.0	50.9	.26	50.0	11.0	11.0	4.0	0.	0.	192.	0.	0.	6.37
N310F2.010	2.0	16.7	21.3	31.2	.33	50.0	.0	11.0	5.3	185.	0.	185.	0.	186.	7.85
N310F3.004	.1	.0	.0	.0	.00	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.19
N310F3.005	.1	.0	.0	.0	-.01	50.0	55.0	11.0	.4	0.	0.	0.	0.	0.	.10
N310F3.006	.9	.0	22.9	.0	.02	50.0	44.0	11.0	2.5	0.	0.	199.	0.	0.	.68
N310F3.007	1.1	25.7	25.8	25.8	.05	50.0	33.0	11.0	2.8	0.	0.	225.	0.	0.	1.38
N310F3.008	2.1	15.6	16.2	42.7	.12	50.0	22.0	11.0	5.5	141.	0.	141.	0.	142.	3.55
N310F3.009	1.6	17.2	19.9	30.0	.24	50.0	11.0	11.0	4.3	0.	0.	174.	0.	0.	6.03
N310F3.010	1.4	18.7	23.5	46.4	.32	50.0	.0	11.0	3.8	0.	0.	205.	0.	0.	7.53
N310F4.004	.1	.0	.0	.0	.01	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.37
N310F4.005	.2	.0	40.1	.0	.02	50.0	55.0	11.0	.6	0.	0.	349.	0.	0.	.45
N310F4.006	.6	.0	38.0	.0	.03	50.0	44.0	11.0	1.6	0.	0.	331.	0.	0.	.64
N310F4.007	1.0	.0	19.5	.0	.04	50.0	33.0	11.0	2.6	0.	0.	170.	0.	0.	1.26
N310F4.008	1.4	21.2	35.6	35.7	.17	50.0	22.0	11.0	3.6	0.	0.	310.	0.	0.	4.29
N310F4.009	1.9	6.6	18.2	47.2	.29	50.0	11.0	11.0	4.8	0.	0.	159.	0.	0.	7.06
N310F4.010	1.5	15.2	22.8	43.9	.32	50.0	.0	11.0	4.0	0.	0.	198.	0.	0.	7.50
N310F5.004	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.45
N310F5.005	.3	.0	21.0	.0	.00	50.0	55.0	11.0	.7	0.	0.	183.	0.	0.	.23
N310F5.006	.6	.0	24.3	.0	.01	50.0	44.0	11.0	1.5	0.	0.	212.	0.	0.	.51
N310F5.007	1.0	18.3	18.3	18.3	.03	50.0	33.0	11.0	2.7	0.	0.	159.	0.	0.	1.01
N310F5.008	1.4	10.7	17.6	25.6	.09	50.0	22.0	11.0	3.7	0.	0.	153.	0.	0.	2.87
N310F5.009	1.4	13.9	17.9	34.4	.21	50.0	11.0	11.0	3.7	0.	0.	156.	0.	0.	5.44
N310F5.010	1.3	17.4	22.0	34.7	.31	50.0	.0	11.0	3.4	0.	0.	192.	0.	0.	7.38

FALCON 3: LSR = 100, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310G1.004	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.07
N310G1.005	.2	.0	.0	.0	-.02	50.0	55.0	17.0	.5	0.	0.	0.	0.	0.	.08
N310G1.006	.5	.0	27.0	.0	-.01	50.0	44.0	17.0	1.3	0.	0.	235.	0.	0.	.17
N310G1.007	.7	.0	38.7	.0	.00	50.0	33.0	17.0	1.8	0.	0.	338.	0.	0.	.48
N310G1.008	1.3	14.8	14.8	17.6	-.01	50.0	22.0	17.0	3.4	0.	0.	129.	0.	0.	1.18
N310G1.009	1.3	14.3	27.9	28.0	.07	50.0	11.0	17.0	3.5	0.	0.	244.	0.	0.	2.96
N310G1.010	1.4	7.7	28.5	43.3	.16	50.0	.0	17.0	3.7	0.	0.	248.	0.	0.	4.39
N310G2.004	.0	.0	.0	.0	-.02	50.0	66.0	17.0	.0	0.	0.	0.	0.	0.	.06
N310G2.005	.2	.0	.0	.0	.00	50.0	55.0	17.0	.4	0.	0.	0.	0.	0.	.03
N310G2.006	.3	.0	61.2	.0	-.01	50.0	44.0	17.0	.7	0.	0.	533.	0.	0.	.11
N310G2.007	1.0	14.8	14.8	16.1	-.01	50.0	33.0	17.0	2.8	0.	0.	129.	0.	0.	.55
N310G2.008	1.3	20.5	32.8	32.8	.06	50.0	22.0	17.0	3.5	0.	0.	286.	0.	0.	2.23
N310G2.009	1.5	10.4	10.5	49.0	.16	50.0	11.0	17.0	3.9	0.	0.	91.	0.	0.	4.34
N310G2.010	1.6	17.4	21.2	41.6	.22	50.0	.0	17.0	4.1	0.	0.	185.	0.	0.	5.45
N310G3.004	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.09
N310G3.005	.1	.0	.0	.0	.01	50.0	55.0	17.0	.3	0.	0.	0.	0.	0.	.39
N310G3.006	.3	.0	30.0	.0	.01	50.0	44.0	17.0	.7	0.	0.	262.	0.	0.	.29
N310G3.007	.6	.0	56.7	.0	-.01	50.0	33.0	17.0	1.7	0.	0.	494.	0.	0.	.28
N310G3.008	1.0	.0	27.3	.0	.05	50.0	22.0	17.0	2.6	0.	0.	238.	0.	0.	1.83
N310G3.009	1.4	11.4	24.1	55.0	.16	50.0	11.0	17.0	3.7	0.	0.	210.	0.	0.	4.15
N310G3.010	1.2	20.2	25.3	42.6	.17	50.0	.0	17.0	3.2	0.	0.	220.	0.	0.	4.43
N310G4.004	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.14
N310G4.005	.2	.0	27.7	.0	.00	50.0	55.0	17.0	.6	0.	0.	241.	0.	0.	.09
N310G4.006	.3	.0	21.9	.0	.02	50.0	44.0	17.0	.7	0.	0.	191.	0.	0.	.50
N310G4.007	1.1	16.5	16.5	30.1	.01	50.0	33.0	17.0	3.0	0.	0.	144.	0.	0.	.67
N310G4.008	1.2	10.3	30.3	47.3	.03	50.0	22.0	17.0	3.3	0.	0.	264.	0.	0.	1.54
N310G4.009	1.7	15.0	21.7	34.7	.12	50.0	11.0	17.0	4.4	0.	0.	189.	0.	0.	3.63
N310G4.010	1.6	15.1	20.2	47.7	.20	50.0	.0	17.0	4.1	0.	0.	176.	0.	0.	5.09
N310G5.004	.1	.0	.0	.0	.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.41
N310G5.005	.2	.0	20.7	.0	.00	50.0	55.0	17.0	.6	0.	0.	180.	0.	0.	.09
N310G5.006	.3	.0	20.5	.0	.00	50.0	44.0	17.0	.9	0.	0.	179.	0.	0.	.21
N310G5.007	.6	.0	11.2	.0	.00	50.0	33.0	17.7	0.	0.	97.	0.	0.	.50	.
N310G5.008	1.3	11.9	11.9	50.1	.04	50.0	22.0	17.0	3.5	0.	0.	104.	0.	0.	1.76
N310G5.009	1.6	8.9	31.8	31.8	.10	50.0	11.0	17.0	4.2	0.	0.	277.	0.	0.	3.43
N310G5.010	1.2	24.0	24.1	30.4	.07	50.0	.0	17.0	3.1	0.	0.	210.	0.	0.	2.82
N310H1.004	1.3	21.0	27.2	34.2	.47	50.0	.0	1.0	3.5	0.	0.	237.	0.	0.	10.94
N310H1.005	1.4	21.2	22.5	48.1	.50	50.0	-11.0	1.0	3.6	0.	0.	196.	0.	0.	11.57
N310H1.006	1.6	17.4	22.7	48.0	.40	50.0	-22.0	1.0	4.1	0.	0.	198.	0.	0.	9.29
N310H1.007	1.5	21.9	28.7	48.5	.32	50.0	-33.0	1.0	3.9	0.	0.	251.	0.	0.	7.47
N310H1.008	1.0	.0	24.8	.0	.21	50.0	-44.0	1.0	2.6	0.	0.	216.	0.	0.	4.85
N310H1.009	.8	.0	26.0	.0	.14	50.0	-55.0	1.0	2.1	0.	0.	227.	0.	0.	3.33
N310H1.010	.3	.0	26.1	.0	-.05	50.0	-66.0	1.0	.8	0.	0.	228.	0.	0.	.30

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310H2.004	1.7	17.7	24.5	36.7	.51	50.0	.0	1.0	4.5	0.	0.	213.	0.	0.	11.84
N310H2.005	1.7	17.3	29.6	41.0	.53	50.0	-11.0	1.0	4.4	0.	0.	258.	0.	0.	12.31
N310H2.006	1.8	20.6	30.2	32.6	.42	50.0	-22.0	1.0	4.7	0.	0.	263.	0.	0.	9.92
N310H2.007	1.8	14.9	30.6	30.9	.38	50.0	-33.0	1.0	4.8	0.	0.	267.	0.	0.	8.99
N310H2.008	1.7	20.2	20.6	28.1	.27	50.0	-44.0	1.0	4.5	0.	0.	179.	0.	0.	6.39
N310H2.009	1.1	20.7	20.7	20.7	.16	50.0	-55.0	1.0	2.9	0.	0.	181.	0.	0.	3.78
N310H2.010	.7	.0	51.0	.0	.13	50.0	-66.0	1.0	1.8	0.	0.	445.	0.	0.	3.03
N310H3.004	1.4	19.4	23.1	37.7	.44	50.0	.0	1.0	3.7	0.	0.	202.	0.	0.	10.27
N310H3.005	1.5	15.1	23.8	41.6	.47	50.0	-11.0	1.0	4.1	0.	0.	207.	0.	0.	10.86
N310H3.006	1.7	18.3	22.2	41.3	.41	50.0	-22.0	1.0	4.4	0.	0.	193.	0.	0.	9.47
N310H3.007	2.2	17.4	24.8	36.4	.35	50.0	-33.0	1.0	5.7	216.	0.	216.	0.	216.	8.21
N310H3.008	1.6	17.9	22.5	35.9	.24	50.0	-44.0	1.0	4.3	0.	0.	196.	0.	0.	5.82
N310H3.009	1.2	24.9	25.8	26.3	.17	50.0	-55.0	1.0	3.2	0.	0.	225.	0.	0.	4.02
N310H3.010	.9	.0	30.0	.0	.16	50.0	-66.0	1.0	2.4	0.	0.	261.	0.	0.	3.68
N310H4.004	1.5	19.6	21.3	36.6	.53	50.0	.0	1.0	4.1	0.	0.	186.	0.	0.	12.42
N310H4.005	1.5	17.5	29.4	46.4	.49	50.0	-11.0	1.0	4.1	0.	0.	256.	0.	0.	11.44
N310H4.006	1.4	16.9	29.3	33.3	.46	50.0	-22.0	1.0	3.7	0.	0.	255.	0.	0.	10.84
N310H4.007	1.4	21.5	22.5	31.0	.32	50.0	-33.0	1.0	3.7	0.	0.	196.	0.	0.	7.58
N310H4.008	1.2	24.5	31.2	31.2	.24	50.0	-44.0	1.0	3.1	0.	0.	272.	0.	0.	5.71
N310H4.009	1.0	19.4	19.4	19.4	.09	50.0	-55.0	1.0	2.7	0.	0.	169.	0.	0.	2.18
N310H4.010	.5	.0	26.2	.0	-.05	50.0	-66.0	1.0	1.4	0.	0.	229.	0.	0.	.17
N310H5.004	1.4	17.7	21.7	42.0	.50	50.0	.0	1.0	3.8	0.	0.	189.	0.	0.	11.80
N310H5.005	1.4	17.6	22.9	44.6	.50	50.0	-11.0	1.0	3.8	0.	0.	200.	0.	0.	11.58
N310H5.006	1.5	19.2	38.3	38.5	.42	50.0	-22.0	1.0	3.8	0.	0.	334.	0.	0.	9.90
N310H5.007	1.7	18.6	22.2	39.2	.35	50.0	-33.0	1.0	4.5	0.	0.	194.	0.	0.	8.26
N310H5.008	1.2	22.4	23.9	25.8	.24	50.0	-44.0	1.0	3.1	0.	0.	209.	0.	0.	5.57
N310H5.009	.7	.0	27.2	.0	.14	50.0	-55.0	1.0	1.9	0.	0.	237.	0.	0.	3.25
N310H5.010	.2	.0	55.2	.0	.02	50.0	-66.0	1.0	.6	0.	0.	481.	0.	0.	.87
N310I1.004	1.4	17.2	23.6	34.0	.47	50.0	.0	5.0	3.7	0.	0.	206.	0.	0.	10.99
N310I1.005	1.3	17.3	24.1	28.0	.37	50.0	-11.0	5.0	3.6	0.	0.	210.	0.	0.	8.67
N310I1.006	1.2	16.5	24.6	27.4	.31	50.0	-22.0	5.0	3.1	0.	0.	215.	0.	0.	7.27
N310I1.007	1.0	24.5	24.5	33.4	.13	50.0	-33.0	5.0	2.7	0.	0.	214.	0.	0.	3.38
N310I1.008	.6	.0	23.9	.0	.10	50.0	-44.0	5.0	1.7	0.	0.	209.	0.	0.	2.49
N310I1.009	.4	.0	36.4	.0	.02	50.0	-55.0	5.0	1.0	0.	0.	318.	0.	0.	.82
N310I1.010	.1	.0	.0	.0	-.05	50.0	-66.0	5.0	.2	0.	0.	0.	0.	0.	.06
N310I2.004	1.4	18.2	19.1	35.3	.50	50.0	.0	5.0	3.7	0.	0.	167.	0.	0.	11.58
N310I2.005	1.6	23.1	31.0	53.6	.40	50.0	-11.0	5.0	4.1	0.	0.	271.	0.	0.	9.48
N310I2.006	1.6	22.1	22.5	54.0	.36	50.0	-22.0	5.0	4.3	0.	0.	196.	0.	0.	8.38
N310I2.007	1.4	22.2	23.2	52.5	.17	50.0	-33.0	5.0	3.7	0.	0.	202.	0.	0.	4.22
N310I2.008	1.0	.0	31.2	.0	.10	50.0	-44.0	5.0	2.6	0.	0.	272.	0.	0.	2.54
N310I2.009	.9	.0	25.9	.0	.13	50.0	-55.0	5.0	2.4	0.	0.	226.	0.	0.	3.02
N310I2.010	.3	.0	34.4	.0	.08	50.0	-66.0	5.0	.9	0.	0.	300.	0.	0.	1.99

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310I3.004	1.3	20.6	24.7	38.0	.43	50.0	.0	5.0	3.4	0.	0.	215.	0.	0.	10.13
N310I3.005	1.5	21.7	22.8	38.3	.42	50.0	-11.0	5.0	4.0	0.	0.	199.	0.	0.	9.90
N310I3.006	1.3	20.9	32.5	48.5	.37	50.0	-22.0	5.0	3.3	0.	0.	283.	0.	0.	8:60
N310I3.007	1.1	13.3	26.2	48.4	.17	50.0	-33.0	5.0	3.0	0.	0.	229.	0.	0.	4.07
N310I3.008	.9	.0	36.9	.0	.07	50.0	-44.0	5.0	2.4	0.	0.	321.	0.	0.	1.87
N310I3.009	.7	.0	28.1	.0	.01	50.0	-55.0	5.0	2.0	0.	0.	245.	0.	0.	.81
N310I3.010	.3	.0	36.7	.0	.04	50.0	-66.0	5.0	.9	0.	0.	320.	0.	0.	1.08
N310I4.004	1.3	21.4	21.4	35.6	.43	50.0	.0	5.0	3.4	0.	0.	187.	0.	0.	10.01
N310I4.005	1.4	19.0	35.4	37.9	.41	50.0	-11.0	5.0	3.8	0.	0.	309.	0.	0.	9.59
N310I4.006	1.3	19.5	19.5	38.7	.39	50.0	-22.0	5.0	3.5	0.	0.	170.	0.	0.	9.12
N310I4.007	1.2	20.3	25.0	44.2	.20	50.0	-33.0	5.0	3.3	0.	0.	218.	0.	0.	4.63
N310I4.008	1.2	25.0	25.1	44.1	.10	50.0	-44.0	5.0	3.2	0.	0.	219.	0.	0.	2.51
N310I4.009	.9	.0	25.2	.0	.07	50.0	-55.0	5.0	2.4	0.	0.	220.	0.	0.	1.76
N310I4.010	.4	.0	44.9	.0	-.02	50.0	-66.0	5.0	1.0	0.	0.	391.	0.	0.	.17
N310I5.004	1.5	20.3	29.6	37.9	.38	50.0	.0	5.0	3.9	0.	0.	258.	0.	0.	8.92
N310I5.005	1.3	18.5	29.1	38.1	.38	50.0	-11.0	5.0	3.5	0.	0.	253.	0.	0.	8.98
N310I5.006	1.8	20.0	26.1	37.7	.36	50.0	-22.0	5.0	4.6	0.	0.	228.	0.	0.	8.46
N310I5.007	1.7	19.4	31.8	37.8	.24	50.0	-33.0	5.0	4.6	0.	0.	277.	0.	0.	5.60
N310I5.008	1.0	22.8	22.8	22.9	.13	50.0	-44.0	5.0	2.7	0.	0.	199.	0.	0.	3.17
N310I5.009	.6	.0	37.4	.0	.07	50.0	-55.0	5.0	1.6	0.	0.	326.	0.	0.	1.70
N310I5.010	.4	.0	34.6	.0	-.02	50.0	-66.0	5.0	1.1	0.	0.	302.	0.	0.	.47
N310J1.004	1.5	14.1	22.3	32.2	.35	50.0	.0	11.0	4.1	0.	0.	194.	0.	0.	8.23
N310J1.005	1.8	19.9	26.5	31.2	.27	50.0	-11.0	11.0	4.7	0.	0.	231.	0.	0.	6.46
N310J1.006	1.6	15.7	26.1	40.1	.24	50.0	-22.0	11.0	4.2	0.	0.	227.	0.	0.	5.70
N310J1.007	1.7	15.5	22.0	29.1	.10	50.0	-33.0	11.0	4.5	0.	0.	192.	0.	0.	2.60
N310J1.008	.8	.0	24.6	.0	.05	50.0	-44.0	11.0	2.1	0.	0.	214.	0.	0.	1.18
N310J1.009	.8	.0	28.7	.0	.04	50.0	-55.0	11.0	2.0	0.	0.	251.	0.	0.	1.02
N310J1.010	.3	.0	30.7	.0	.04	50.0	-66.0	11.0	.9	0.	0.	268.	0.	0.	1.06
N310J2.004	1.7	13.7	22.5	45.5	.36	50.0	.0	11.0	4.6	0.	0.	196.	0.	0.	8.51
N310J2.005	1.5	16.4	19.4	34.2	.29	50.0	-11.0	11.0	3.9	0.	0.	169.	0.	0.	6.87
N310J2.006	1.5	17.4	25.3	31.3	.21	50.0	-22.0	11.0	3.9	0.	0.	220.	0.	0.	5.25
N310J2.007	1.9	13.2	23.6	26.6	.13	50.0	-33.0	11.0	4.9	0.	0.	206.	0.	0.	3.20
N310J2.008	1.4	23.4	23.5	23.5	.04	50.0	-44.0	11.0	3.7	0.	0.	205.	0.	0.	1.01
N310J2.009	.6	.0	23.2	.0	.05	50.0	-55.0	11.0	1.7	0.	0.	203.	0.	0.	1.29
N310J2.010	.8	.0	23.5	.0	.03	50.0	-66.0	11.0	2.1	0.	0.	205.	0.	0.	1.09
N310J3.004	2.3	12.3	26.6	39.8	.38	50.0	.0	11.0	5.9	232.	0.	232.	0.	235.	9.02
N310J3.005	1.8	16.8	24.7	35.4	.31	50.0	-11.0	11.0	4.7	0.	0.	215.	0.	0.	7.28
N310J3.006	1.7	19.3	24.8	51.6	.21	50.0	-22.0	11.0	4.5	0.	0.	217.	0.	0.	5.13
N310J3.007	1.2	23.3	25.6	50.9	.13	50.0	-33.0	11.0	3.2	0.	0.	223.	0.	0.	3.19
N310J3.008	.8	.0	25.5	.0	.04	50.0	-44.0	11.0	2.3	0.	0.	222.	0.	0.	1.12
N310J3.009	.9	.0	25.5	.0	.04	50.0	-55.0	11.0	2.3	0.	0.	222.	0.	0. 0.	1.04
N310J3.010	.4	.0	26.4	.0	.06	50.0	-66.0	11.0	1.1	0.	0.	230.	0.	0.	1.48

FALCON 3: LSR = 100, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310J4.004	2.0	13.9	23.7	35.3	.33	50.0	.0	11.0	5.2	207.	0.	207.	0.	207.	7.87
N310J4.005	1.6	17.8	18.7	40.3	.26	50.0	-11.0	11.0	4.3	0.	0.	163.	0.	0.	6.37
N310J4.006	1.5	18.0	27.6	33.9	.23	50.0	-22.0	11.0	3.9	0.	0.	241.	0.	0.	5.55
N310J4.007	1.3	16.9	27.2	42.4	.04	50.0	-33.0	11.0	3.5	0.	0.	237.	0.	0.	2.07
N310J4.008	.6	.0	36.1	.0	.03	50.0	-44.0	11.0	1.6	0.	0.	315.	0.	0.	.93
N310J4.009	.4	.0	20.0	.0	.00	50.0	-55.0	11.0	1.0	0.	0.	175.	0.	0.	.50
N310J4.010	.4	.0	19.7	.0	.00	50.0	-66.0	11.0	1.1	0.	0.	172.	0.	0.	.32
N310J5.004	1.3	15.6	22.4	39.3	.33	50.0	.0	11.0	3.5	0.	0.	196.	0.	0.	7.83
N310J5.005	1.3	18.8	31.9	46.6	.28	50.0	-11.0	11.0	3.4	0.	0.	278.	0.	0.	6.81
N310J5.006	1.5	16.5	21.2	39.4	.27	50.0	-22.0	11.0	3.9	0.	0.	184.	0.	0.	6.40
N310J5.007	1.6	21.4	37.4	39.5	.18	50.0	-33.0	11.0	4.3	0.	0.	326.	0.	0.	4.53
N310J5.008	1.2	27.8	27.8	27.9	.09	50.0	-44.0	11.0	3.1	0.	0.	243.	0.	0.	2.21
N310J5.009	.8	.0	30.2	.0	.06	50.0	-55.0	11.0	2.2	0.	0.	263.	0.	0.	1.57
N310J5.010	.6	.0	28.0	.0	.06	50.0	-66.0	11.0	1.5	0.	0.	244.	0.	0.	1.50
N310K1.004	1.7	21.1	30.8	35.4	.19	50.0	.0	17.0	4.6	0.	0.	268.	0.	0.	5.03
N310K1.005	1.6	21.7	21.8	33.9	.17	50.0	-11.0	17.0	4.2	0.	0.	190.	0.	0.	4.18
N310K1.006	1.4	38.3	38.3	38.5	.10	50.0	-22.0	17.0	3.6	0.	0.	334.	0.	0.	2.62
N310K1.007	.8	.0	52.7	.0	.03	50.0	-33.0	17.0	2.1	0.	0.	460.	0.	0.	.79
N310K1.008	.3	.0	27.9	.0	-.02	50.0	-44.0	17.0	.8	0.	0.	243.	0.	0.	.09
N310K1.009	.1	.0	.0	.0	-.01	50.0	-55.0	17.0	.2	0.	0.	0.	0.	0.	.21
N310K1.010	.0	.0	.0	.0	-.02	50.0	-66.0	17.0	.1	0.	0.	0.	0.	0.	.14
N310K2.004	1.7	7.1	27.1	46.6	.17	50.0	.0	17.0	4.4	0.	0.	236.	0.	0.	4.77
N310K2.005	1.5	7.4	20.2	33.5	.12	50.0	-11.0	17.0	3.8	0.	0.	176.	0.	0.	3.58
N310K2.006	1.0	.0	22.9	.0	.04	50.0	-22.0	17.0	2.5	0.	0.	200.	0.	0.	1.72
N310K2.007	.9	.0	17.1	.0	.03	50.0	-33.0	17.0	2.4	0.	0.	149.	0.	0.	.76
N310K2.008	.4	.0	21.4	.0	-.01	50.0	-44.0	17.0	1.0	0.	0.	187.	0.	0.	.18
N310K2.009	.2	.0	.0	.0	.00	50.0	-55.0	17.0	.5	0.	0.	0.	0.	0.	.21
N310K2.010	.1	.0	.0	.0	.02	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.49
N310K3.004	1.7	16.6	16.6	50.4	.21	50.0	.0	17.0	4.4	0.	0.	145.	0.	0.	5.58
N310K3.005	1.3	26.4	29.2	33.4	.15	50.0	-11.0	17.0	3.3	0.	0.	254.	0.	0.	4.16
N310K3.006	1.1	22.2	26.0	26.0	.03	50.0	-22.0	17.0	2.8	0.	0.	227.	0.	0.	1.74
N310K3.007	.8	.0	45.8	.0	.04	50.0	-33.0	17.0	2.2	0.	0.	400.	0.	0.	1.06
N310K3.008	.3	.0	44.3	.0	.03	50.0	-44.0	17.0	.8	0.	0.	386.	0.	0.	.98
N310K3.009	.2	.0	30.4	.0	.00	50.0	-55.0	17.0	.6	0.	0.	265.	0.	0.	.22
N310K3.010	.1	.0	.0	.0	-.01	50.0	-66.0	17.0	.1	0.	0.	0.	0.	0.	.17
N310K4.004	1.7	14.3	15.5	33.3	.28	50.0	.0	17.0	4.5	0.	0.	135.	0.	0.	6.82
N310K4.005	1.2	5.5	40.3	40.6	.20	50.0	-11.0	17.0	3.1	0.	0.	351.	0.	0.	4.96
N310K4.006	1.4	15.4	28.9	32.9	.12	50.0	-22.0	17.0	3.7	0.	0.	252.	0.	0.	3.12
N310K4.007	.8	.0	21.8	.0	.07	50.0	-33.0	17.0	2.1	0.	0.	190.	0.	0.	1.77
N310K4.008	.4	.0	70.0	.0	.04	50.0	-44.0	17.0	1.2	0.	0.	610.	0.	0.	1.11
N310K4.009	.3	.0	25.5	.0	.00	50.0	-55.0	17.0	.8	0.	0.	222.	0.	0.	.23
N310K4.010	.1	.0	.0	.0	-.04	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.08

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310K5.004	1.4	22.4	29.0	40.0	.17	50.0	.0	17.0	3.8	0.	0.	253.	0.	0.	4.72
N310K5.005	1.5	10.8	40.1	40.2	.12	50.0	-11.0	17.0	4.1	0.	0.	350.	0.	0.	3.70
N310K5.006	1.7	27.8	31.4	33.6	.13	50.0	-22.0	17.0	4.4	0.	0.	274.	0.	0.	3.18
N310K5.007	1.2	33.1	38.2	43.6	.08	50.0	-33.0	17.0	3.2	0.	0.	333.	0.	0.	1.87
N310K5.008	.9	.0	32.9	.0	.08	50.0	-44.0	17.0	2.5	0.	0.	287.	0.	0.	1.82
N310K5.009	.5	.0	34.7	.0	.04	50.0	-55.0	17.0	1.3	0.	0.	302.	0.	0.	.98
N310K5.010	.2	.0	.0	.0	.03	50.0	-66.0	17.0	.4	0.	0.	0.	0.	0.	.67
N310L1.004	.1	.0	.0	.0	-.05	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.12
N310L1.005	.1	.0	.0	.0	-.05	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.08
N310L1.006	.1	.0	.0	.0	.02	150.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.65
N310L1.007	.2	.0	.0	.0	-.09	150.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.12
N310L1.008	.6	.0	25.2	.0	.03	150.0	28.0	1.0	1.7	0.	0.	219.	0.	0.	1.52
N310L1.009	.7	.0	25.5	.0	.04	150.0	25.0	1.0	1.8	0.	0.	222.	0.	0.	1.83
N310L1.010	.8	.0	26.0	.0	.23	150.0	.0	1.0	2.2	0.	0.	227.	0.	0.	5.54
N310L2.004	.2	.0	.0	.0	-.02	150.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.34
N310L2.005	.1	.0	.0	.0	-.03	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.12
N310L2.006	.1	.0	.0	.0	.01	150.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.42
N310L2.007	.3	.0	23.3	.0	.01	150.0	44.0	1.0	.7	0.	0.	203.	0.	0.	.74
N310L2.008	1.0	.0	25.9	.0	.22	150.0	28.0	1.0	2.6	0.	0.	226.	0.	0.	5.14
N310L2.009	1.0	.0	25.3	.0	.24	150.0	25.0	1.0	2.6	0.	0.	221.	0.	0.	5.75
N310L2.010	.9	.0	27.9	.0	.16	150.0	.0	1.0	2.3	0.	0.	243.	0.	0.	4.21
N310L3.004	.2	.0	28.3	.0	.09	150.0	75.0	1.0	.6	0.	0.	247.	0.	0.	2.17
N310L3.005	.4	.0	27.8	.0	.09	150.0	56.0	1.0	1.2	0.	0.	242.	0.	0.	2.15
N310L3.006	.5	.0	23.8	.0	.06	150.0	50.0	1.0	1.4	0.	0.	208.	0.	0.	1.56
N310L3.007	.6	.0	23.8	.0	.05	150.0	44.0	1.0	1.7	0.	0.	208.	0.	0.	1.83
N310L3.008	.8	.0	23.3	.0	.17	150.0	28.0	1.0	2.1	0.	0.	203.	0.	0.	3.90
N310L3.009	.8	.0	23.3	.0	.17	150.0	25.0	1.0	2.0	0.	0.	203.	0.	0.	4.05
N310L3.010	.8	.0	25.8	.0	.30	150.0	.0	1.0	2.2	0.	0.	225.	0.	0.	7.22
N310L4.004	.1	.0	.0	.0	-.07	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.08
N310L4.005	.1	.0	.0	.0	-.03	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.12
N310L4.006	.2	.0	.0	.0	.02	150.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.64
N310L4.007	.4	.0	34.7	.0	.05	150.0	44.0	1.0	1.1	0.	0.	302.	0.	0.	1.39
N310L4.008	.8	.0	29.7	.0	.11	150.0	28.0	1.0	2.0	0.	0.	259.	0.	0.	2.68
N310L4.009	.6	.0	22.3	.0	.16	150.0	25.0	1.0	1.7	0.	0.	195.	0.	0.	3.88
N310L4.010	.7	.0	26.5	.0	.21	150.0	.0	1.0	1.8	0.	0.	231.	0.	0.	5.10
N310L5.004	.2	.0	.0	.0	.03	150.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.95
N310L5.005	.1	.0	.0	.0	.00	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.33
N310L5.006	.1	.0	.0	.0	-.02	150.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.17
N310L5.007	.3	.0	32.3	.0	.09	150.0	44.0	1.0	.7	0.	0.	281.	0.	0.	2.18
N310L5.008	.6	.0	32.4	.0	.11	150.0	28.0	1.0	1.6	0.	0.	283.	0.	0.	2.55
N310L5.009	.7	.0	32.5	.0	.14	150.0	25.0	1.0	1.8	0.	0.	283.	0.	0.	3.38
N310L5.010	.8	.0	29.2	.0	.22	150.0	.0	1.0	2.1	0.	0.	254.	0.	0.	5.13

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310M1.004	.1	.0	.0	.0	.02	150.0	75.0	5.0	.4	0.	0.	0.	0.	0.	.57
N310M1.005	.1	.0	.0	.0	-.01	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.14
N310M1.006	.0	.0	.0	.0	-.02	150.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.07
N310M1.007	.3	.0	40.8	.0	-.03	150.0	44.0	5.0	.9	0.	0.	356.	0.	0.	.13
N310M1.008	.8	.0	26.3	.0	.08	150.0	28.0	5.0	2.0	0.	0.	229.	0.	0.	1.84
N310M1.009	.7	.0	30.1	.0	.09	150.0	25.0	5.0	1.9	0.	0.	263.	0.	0.	2.12
N310M1.010	.9	.0	30.8	.0	.20	150.0	.0	5.0	2.5	0.	0.	269.	0.	0.	4.67
N310M2.004	.1	.0	.0	.0	-.03	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.16
N310M2.005	.2	.0	.0	.0	.01	150.0	56.0	5.0	.5	0.	0.	0.	0.	0.	.47
N310M2.006	.3	.0	31.4	.0	.01	150.0	50.0	5.0	.8	0.	0.	274.	0.	0.	.61
N310M2.007	.6	.0	27.9	.0	.04	150.0	44.0	5.0	1.5	0.	0.	243.	0.	0.	1.46
N310M2.008	.7	.0	19.7	.0	.10	150.0	28.0	5.0	1.9	0.	0.	171.	0.	0.	2.48
N310M2.009	.7	.0	23.1	.0	.10	150.0	25.0	5.0	1.9	0.	0.	202.	0.	0.	2.52
N310M2.010	.9	.0	32.0	.0	.27	150.0	.0	5.0	2.4	0.	0.	279.	0.	0.	6.28
N310M3.004	.1	.0	.0	.0	.02	150.0	75.0	5.0	.4	0.	0.	0.	0.	0.	.67
N310M3.005	.4	.0	26.1	.0	.00	150.0	56.0	5.0	1.0	0.	0.	228.	0.	0.	.23
N310M3.006	.5	.0	26.3	.0	-.01	150.0	50.0	5.0	1.4	0.	0.	229.	0.	0.	.36
N310M3.007	.5	.0	26.1	.0	.00	150.0	44.0	5.0	1.4	0.	0.	228.	0.	0.	.66
N310M3.008	.7	.0	23.1	.0	.11	150.0	28.0	5.0	1.9	0.	0.	201.	0.	0.	2.68
N310M3.009	.8	.0	23.9	.0	.12	150.0	25.0	5.0	2.0	0.	0.	208.	0.	0.	2.81
N310M3.010	.8	.0	30.7	.0	.19	150.0	.0	5.0	2.1	0.	0.	267.	0.	0.	4.63
N310M4.004	.1	.0	.0	.0	-.05	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.05
N310M4.005	.1	.0	.0	.0	.00	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.18
N310M4.006	.1	.0	.0	.0	-.02	150.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.12
N310M4.007	.1	.0	.0	.0	.01	150.0	44.0	5.0	.4	0.	0.	0.	0.	0.	.51
N310M4.008	.5	.0	25.8	.0	.07	150.0	28.0	5.0	1.2	0.	0.	225.	0.	0.	1.64
N310M4.009	.5	.0	33.7	.0	.06	150.0	25.0	5.0	1.2	0.	0.	294.	0.	0.	1.61
N310M4.010	1.0	29.5	29.5	29.6	.16	150.0	.0	5.0	2.7	0.	0.	257.	0.	0.	4.06
N310M5.004	.2	.0	.0	.0	.04	150.0	75.0	5.0	.4	0.	0.	0.	0.	0.	1.05
N310M5.005	.1	.0	.0	.0	.01	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.45
N310M5.006	.2	.0	.0	.0	.01	150.0	50.0	5.0	.4	0.	0.	0.	0.	0.	.56
N310M5.007	.3	.0	28.7	.0	.06	150.0	44.0	5.0	.9	0.	0.	250.	0.	0.	1.31
N310M5.008	.5	.0	23.6	.0	.07	150.0	28.0	5.0	1.4	0.	0.	206.	0.	0.	1.71
N310M5.009	.7	.0	29.0	.0	.09	150.0	25.0	5.0	1.9	0.	0.	253.	0.	0.	2.12
N310M5.010	.9	.0	30.6	.0	.13	150.0	.0	5.0	2.4	0.	0.	267.	0.	0.	3.31
N310N1.004	.1	.0	.0	.0	.01	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.42
N310N1.005	.1	.0	.0	.0	-.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.06
N310N1.006	.2	.0	32.3	.0	.02	150.0	50.0	11.0	.6	0.	0.	282.	0.	0.	.56
N310N1.007	.2	.0	32.4	.0	-.01	150.0	44.0	11.0	.6	0.	0.	283.	0.	0.	.15
N310N1.008	.5	.0	29.3	.0	.02	150.0	28.0	11.0	1.3	0.	0.	255.	0.	0.	.51
N310N1.009	.7	.0	29.3	.0	.03	150.0	25.0	11.0	1.8	0.	0.	256.	0.	0.	.72
N310N1.010	.9	.0	25.4	.0	.10	150.0	.0	11.0	2.3	0.	0.	221.	0.	0.	2.54

FALCON 3: LSR = 100, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310N2.004	.1	.0	.0	.0	-.01	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.15
N310N2.005	.1	.0	.0	.0	-.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.15
N310N2.006	.1	.0	.0	.0	-.02	150.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.07
N310N2.007	.2	.0	24.9	.0	-.01	150.0	44.0	11.0	.5	0.	0.	217.	0.	0.	.27
N310N2.008	.5	.0	43.3	.0	.02	150.0	28.0	11.0	1.3	0.	0.	378.	0.	0.	.71
N310N2.009	.5	.0	24.8	.0	.03	150.0	25.0	11.0	1.3	0.	0.	216.	0.	0.	.94
N310N2.010	.8	.0	28.6	.0	.10	150.0	.0	11.0	2.0	0.	0.	250.	0.	0.	2.67
N310N3.004	.1	.0	.0	.0	.01	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.18
N310N3.005	.1	.0	.0	.0	.00	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.05
N310N3.006	.1	.0	.0	.0	.00	150.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.08
N310N3.007	.1	.0	.0	.0	-.05	150.0	44.0	11.0	.3	0.	0.	0.	0.	0.	.14
N310N3.008	.4	.0	22.7	.0	.02	150.0	28.0	11.0	1.1	0.	0.	198.	0.	0.	.47
N310N3.009	.5	.0	23.2	.0	.03	150.0	25.0	11.0	1.5	0.	0.	202.	0.	0.	.85
N310N3.010	.7	.0	32.2	.0	.09	150.0	.0	11.0	1.8	0.	0.	280.	0.	0.	2.29
N310N4.004	.1	.0	.0	.0	-.02	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.03
N310N4.005	.3	.0	28.6	.0	-.01	150.0	56.0	11.0	.9	0.	0.	250.	0.	0.	.12
N310N4.006	.2	.0	.0	.0	-.01	150.0	50.0	11.0	.5	0.	0.	0.	0.	0.	.03
N310N4.007	.2	.0	.0	.0	-.01	150.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.32
N310N4.008	.5	.0	33.0	.0	.05	150.0	28.0	11.0	1.3	0.	0.	287.	0.	0.	1.20
N310N4.009	.5	.0	27.6	.0	.04	150.0	25.0	11.0	1.2	0.	0.	241.	0.	0.	1.11
N310N4.010	.9	.0	29.0	.0	.12	150.0	.0	11.0	2.4	0.	0.	253.	0.	0.	3.06
N310N5.004	.1	.0	.0	.0	.01	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.36
N310N5.005	.3	.0	28.5	.0	.04	150.0	56.0	11.0	.7	0.	0.	249.	0.	0.	.87
N310N5.006	.4	.0	38.1	.0	.02	150.0	50.0	11.0	1.1	0.	0.	333.	0.	0.	.57
N310N5.007	.3	.0	33.4	.0	.06	150.0	44.0	11.0	.9	0.	0.	292.	0.	0.	1.39
N310N5.008	.6	.0	30.7	.0	.08	150.0	28.0	11.0	1.6	0.	0.	268.	0.	0.	1.92
N310N5.009	.6	.0	30.8	.0	.07	150.0	25.0	11.0	1.6	0.	0.	268.	0.	0.	1.78
N310N5.010	.9	.0	24.9	.0	.17	150.0	.0	11.0	2.5	0.	0.	217.	0.	0.	3.96
N31001.004	.1	.0	.0	.0	.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.35
N31001.005	.1	.0	.0	.0	-.01	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.15
N31001.006	.2	.0	34.4	.0	.00	150.0	50.0	17.0	.6	0.	0.	300.	0.	0.	.15
N31001.007	.2	.0	39.0	.0	-.04	150.0	44.0	17.0	.6	0.	0.	340.	0.	0.	.09
N31001.008	.5	.0	38.6	.0	.01	150.0	28.0	17.0	1.3	0.	0.	336.	0.	0.	.37
N31001.009	.4	.0	38.9	.0	.00	150.0	25.0	17.0	1.1	0.	0.	339.	0.	0.	.39
N31001.010	.8	.0	26.1	.0	.04	150.0	.0	17.0	2.1	0.	0.	228.	0.	0.	1.53
N31002.004	.1	.0	.0	.0	-.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.04
N31002.005	.1	.0	.0	.0	.00	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.02
N31002.006	.1	.0	.0	.0	-.02	150.0	50.0	17.0	.4	0.	0.	0.	0.	0.	.19
N31002.007	.1	.0	.0	.0	-.05	150.0	44.0	17.0	.4	0.	0.	0.	0.	0.	.07
N31002.008	.4	.0	30.0	.0	-.02	150.0	28.0	17.0	1.0	0.	0.	262.	0.	0.	.15
N31002.009	.4	.0	30.0	.0	-.02	150.0	25.0	17.0	1.2	0.	0.	262.	0.	0.	.22
N31002.010	1.1	25.4	25.4	25.5	.04	150.0	.0	17.0	2.8	0.	0.	221.	0.	0.	1.38

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N31003.004	.1	.0	.0	.0	.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.20
N31003.005	.1	.0	.0	.0	.01	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.31
N31003.006	.3	.0	21.7	.0	.01	150.0	50.0	17.0	.8	0.	0.	190.	0.	0.	.16
N31003.007	.2	.0	.0	.0	.01	150.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.60
N31003.008	.6	.0	29.7	.0	.03	150.0	28.0	17.0	1.7	0.	0.	259.	0.	0.	.85
N31003.009	.8	.0	29.7	.0	.02	150.0	25.0	17.0	2.0	0.	0.	259.	0.	0.	.68
N31003.010	.9	.0	31.4	.0	.07	150.0	.0	17.0	2.3	0.	0.	273.	0.	0.	1.78
N31004.004	.1	.0	.0	.0	-.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.17
N31004.005	.1	.0	.0	.0	.00	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.16
N31004.006	.3	.0	26.6	.0	-.01	150.0	50.0	17.0	.7	0.	0.	232.	0.	0.	.24
N31004.007	.1	.0	.0	.0	-.03	150.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.05
N31004.008	.4	.0	50.4	.0	.03	150.0	28.0	17.0	1.1	0.	0.	439.	0.	0.	.82
N31004.009	.3	.0	30.0	.0	.03	150.0	25.0	17.0	.9	0.	0.	262.	0.	0.	.73
N31004.010	.7	.0	36.1	.0	.05	150.0	.0	17.0	1.8	0.	0.	315.	0.	0.	1.67
N31005.004	.1	.0	.0	.0	-.05	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.04
N31005.005	.0	.0	.0	.0	-.01	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.09
N31005.006	.1	.0	.0	.0	.00	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.12
N31005.007	.1	.0	.0	.0	.00	150.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.35
N31005.008	.5	.0	17.2	.0	.00	150.0	28.0	17.0	1.4	0.	0.	150.	0.	0.	.28
N31005.009	.5	.0	17.2	.0	.01	150.0	25.0	17.0	1.4	0.	0.	150.	0.	0.	.46
N31005.010	.7	.0	27.2	.0	.05	150.0	.0	17.0	1.9	0.	0.	237.	0.	0.	1.45
N310P1.004	1.0	.0	26.7	.0	.29	150.0	.0	1.0	2.6	0.	0.	233.	0.	0.	6.93
N310P1.005	.9	.0	30.1	.0	.28	150.0	-25.0	1.0	2.4	0.	0.	262.	0.	0.	6.53
N310P1.006	1.0	30.6	30.6	30.8	.28	150.0	-28.0	1.0	2.7	0.	0.	267.	0.	0.	6.66
N310P1.007	.9	.0	26.4	.0	.23	150.0	-44.0	1.0	2.5	0.	0.	230.	0.	0.	5.58
N310P1.008	1.1	26.9	27.1	27.2	.32	150.0	-50.0	1.0	2.9	0.	0.	236.	0.	0.	7.51
N310P1.009	1.1	26.3	26.5	26.8	.33	150.0	-56.0	1.0	3.0	0.	0.	231.	0.	0.	7.74
N310P1.010	1.0	.0	25.6	.0	.30	150.0	-75.0	1.0	2.6	0.	0.	223.	0.	0.	7.03
N310P2.004	.9	.0	32.6	.0	.26	150.0	.0	1.0	2.3	0.	0.	284.	0.	0.	6.16
N310P2.005	.9	.0	31.9	.0	.24	150.0	-25.0	1.0	2.3	0.	0.	278.	0.	0.	5.76
N310P2.006	.9	.0	30.8	.0	.29	150.0	-28.0	1.0	2.4	0.	0.	269.	0.	0.	6.86
N310P2.007	1.0	.0	34.9	.0	.32	150.0	-44.0	1.0	2.6	0.	0.	304.	0.	0.	7.46
N310P2.008	1.1	34.9	35.0	35.3	.31	150.0	-50.0	1.0	3.0	0.	0.	305.	0.	0.	7.31
N310P2.009	1.0	.0	31.7	.0	.33	150.0	-56.0	1.0	2.6	0.	0.	276.	0.	0.	7.69
N310P2.010	1.0	34.1	34.1	34.1	.34	150.0	-75.0	1.0	2.7	0.	0.	297.	0.	0.	8.03
N310P3.004	1.0	.0	31.4	.0	.26	150.0	.0	1.0	2.6	0.	0.	274.	0.	0.	6.18
N310P3.005	.9	.0	26.6	.0	.22	150.0	-25.0	1.0	2.5	0.	0.	232.	0.	0.	5.19
N310P3.006	1.0	.0	25.1	.0	.23	150.0	-28.0	1.0	2.6	0.	0.	219.	0.	0.	5.55
N310P3.007	1.0	28.1	28.1	28.1	.28	150.0	-44.0	1.0	2.7	0.	0.	245.	0.	0.	6.59
N310P3.008	1.1	26.9	27.6	28.3	.30	150.0	-50.0	1.0	2.9	0.	0.	241.	0.	0.	7.07
N310P3.009	1.0	28.3	28.3	28.6	.29	150.0	-56.0	1.0	2.7	0.	0.	247.	0.	0.	6.92
N310P3.010	.9	.0	28.1	.0	.30	150.0	-75.0	1.0	2.4	0.	0.	245.	0.	0.	7.12

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310P4.004	.8	.0	26.6	.0	.18	150.0	.0	1.0	2.0	0.	0.	232.	0.	0.	4.41
N310P4.005	.9	.0	29.7	.0	.20	150.0	-25.0	1.0	2.4	0.	0.	259.	0.	0.	4.99
N310P4.006	.9	.0	29.7	.0	.22	150.0	-28.0	1.0	2.4	0.	0.	259.	0.	0.	5.25
N310P4.007	1.0	.0	28.3	.0	.27	150.0	-44.0	1.0	2.6	0.	0.	247.	0.	0.	6.30
N310P4.008	1.0	28.3	28.3	28.9	.27	150.0	-50.0	1.0	2.8	0.	0.	247.	0.	0.	6.31
N310P4.009	1.0	25.7	25.7	28.6	.27	150.0	-56.0	1.0	2.8	0.	0.	224.	0.	0.	6.45
N310P4.010	1.1	25.1	26.9	28.3	.27	150.0	-75.0	1.0	2.8	0.	0.	234.	0.	0.	6.39
N310P5.004	1.0	23.6	23.6	23.6	.22	150.0	.0	1.0	2.7	0.	0.	206.	0.	0.	5.32
N310P5.005	.8	.0	24.0	.0	.22	150.0	-25.0	1.0	2.2	0.	0.	209.	0.	0.	5.27
N310P5.006	.9	.0	24.1	.0	.25	150.0	-28.0	1.0	2.4	0.	0.	210.	0.	0.	5.97
N310P5.007	.9	.0	24.2	.0	.26	150.0	-44.0	1.0	2.4	0.	0.	211.	0.	0.	6.04
N310P5.008	.9	.0	33.7	.0	.26	150.0	-50.0	1.0	2.5	0.	0.	294.	0.	0.	6.22
N310P5.009	.9	.0	27.6	.0	.24	150.0	-56.0	1.0	2.4	0.	0.	241.	0.	0.	5.64
N310P5.010	1.0	.0	24.1	.0	.27	150.0	-75.0	1.0	2.6	0.	0.	210.	0.	0.	6.31
N310Q1.004	1.0	.0	29.7	.0	.19	150.0	.0	5.0	2.6	0.	0.	259.	0.	0.	4.47
N310Q1.005	1.0	.0	29.4	.0	.14	150.0	-25.0	5.0	2.6	0.	0.	256.	0.	0.	3.54
N310Q1.006	1.1	29.4	29.4	29.6	.16	150.0	-28.0	5.0	2.9	0.	0.	257.	0.	0.	3.96
N310Q1.007	.1	.0	.0	.0	.00	150.0	-44.0	5.0	.1	0.	0.	0.	0.	0.	.00
N310Q1.008	1.1	22.4	30.1	31.7	.25	150.0	-50.0	5.0	3.0	0.	0.	262.	0.	0.	5.82
N310Q1.009	1.1	25.6	25.7	30.0	.21	150.0	-56.0	5.0	2.8	0.	0.	224.	0.	0.	5.11
N310Q1.010	.9	.0	32.3	.0	.18	150.0	-75.0	5.0	2.5	0.	0.	281.	0.	0.	4.25
N310Q2.004	1.1	24.2	24.2	24.3	.15	150.0	.0	5.0	2.9	0.	0.	211.	0.	0.	3.70
N310Q2.005	.9	.0	24.9	.0	.14	150.0	-25.0	5.0	2.4	0.	0.	217.	0.	0.	3.51
N310Q2.006	.9	.0	28.5	.0	.16	150.0	-28.0	5.0	2.4	0.	0.	249.	0.	0.	4.12
N310Q2.007	1.0	.0	36.4	.0	.17	150.0	-44.0	5.0	2.6	0.	0.	317.	0.	0.	4.11
N310Q2.008	1.0	.0	31.6	.0	.21	150.0	-50.0	5.0	2.5	0.	0.	276.	0.	0.	4.97
N310Q2.009	1.0	24.6	24.6	24.7	.21	150.0	-56.0	5.0	2.7	0.	0.	215.	0.	0.	4.93
N310Q2.010	.9	.0	33.8	.0	.15	150.0	-75.0	5.0	2.4	0.	0.	294.	0.	0.	3.81
N310Q3.004	1.2	22.2	30.8	31.4	.23	150.0	.0	5.0	3.1	0.	0.	269.	0.	0.	5.49
N310Q3.005	.9	.0	27.7	.0	.19	150.0	-25.0	5.0	2.4	0.	0.	241.	0.	0.	4.72
N310Q3.006	.9	.0	27.8	.0	.21	150.0	-28.0	5.0	2.4	0.	0.	242.	0.	0.	5.09
N310Q3.007	1.1	30.0	30.0	30.2	.19	150.0	-44.0	5.0	2.9	0.	0.	262.	0.	0.	4.57
N310Q3.008	1.1	27.3	29.9	30.0	.21	150.0	-50.0	5.0	2.9	0.	0.	260.	0.	0.	4.94
N310Q3.009	1.1	24.8	28.3	28.5	.21	150.0	-56.0	5.0	2.8	0.	0.	247.	0.	0.	4.99
N310Q3.010	1.2	25.8	27.3	27.4	.19	150.0	-75.0	5.0	3.2	0.	0.	238.	0.	0.	4.58
N310Q4.004	1.3	27.1	27.5	35.3	.28	150.0	.0	5.0	3.3	0.	0.	240.	0.	0.	6.58
N310Q4.005	1.0	27.2	27.2	27.3	.17	150.0	-25.0	5.0	2.7	0.	0.	237.	0.	0.	4.15
N310Q4.006	1.1	26.9	26.9	27.2	.19	150.0	-28.0	5.0	2.8	0.	0.	234.	0.	0.	4.51
N310Q4.007	1.1	24.3	24.3	27.4	.21	150.0	-44.0	5.0	3.0	0.	0.	212.	0.	0.	5.02
N310Q4.008	1.2	24.4	26.0	32.7	.22	150.0	-50.0	5.0	3.2	0.	0.	226.	0.	0.	5.23
N310Q4.009	1.2	25.7	25.9	32.5	.22	150.0	-56.0	5.0	3.2	0.	0.	226.	0.	0.	5.34
N310Q4.010	1.1	26.0	26.1	26.2	.12	150.0	-75.0	5.0	3.0	0.	0.	227.	0.	0.	2.83

FALCON 3: LSR = 100, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310Q5.004	.9	.0	26.1	.0	.21	150.0	.0	5.0	2.5	0.	0.	227.	0.	0.	4.92
N310Q5.005	1.0	.0	24.0	.0	.21	150.0	-25.0	5.0	2.6	0.	0.	209.	0.	0.	4.96
N310Q5.006	1.0	27.1	27.1	33.7	.23	150.0	-28.0	5.0	2.8	0.	0.	237.	0.	0.	5.31
N310Q5.007	1.1	26.3	26.4	27.0	.20	150.0	-44.0	5.0	3.0	0.	0.	230.	0.	0.	4.94
N310Q5.008	1.2	25.2	26.7	29.5	.25	150.0	-50.0	5.0	3.3	0.	0.	233.	0.	0.	5.81
N310Q5.009	1.2	24.6	26.3	29.4	.22	150.0	-56.0	5.0	3.3	0.	0.	229.	0.	0.	5.22
N310Q5.010	1.0	26.0	26.0	26.0	.11	150.0	-75.0	5.0	2.8	0.	0.	227.	0.	0.	2.93
N310R1.004	1.0	.0	35.5	.0	.17	150.0	.0	11.0	2.6	0.	0.	310.	0.	0.	4.16
N310R1.005	1.0	22.7	22.7	22.7	.10	150.0	-25.0	11.0	2.7	0.	0.	198.	0.	0.	2.74
N310R1.006	.9	.0	26.1	.0	.11	150.0	-28.0	11.0	2.5	0.	0.	228.	0.	0.	2.98
N310R1.007	1.2	25.8	25.9	25.9	.16	150.0	-44.0	11.0	3.2	0.	0.	226.	0.	0.	3.90
N310R1.008	1.1	25.9	25.9	25.9	.13	150.0	-50.0	11.0	2.9	0.	0.	226.	0.	0.	3.27
N310R1.009	.9	.0	32.8	.0	.07	150.0	-56.0	11.0	2.5	0.	0.	286.	0.	0.	1.94
N310R1.010	.6	.0	22.4	.0	.07	150.0	-75.0	11.0	1.5	0.	0.	196.	0.	0.	1.59
N310R2.004	.8	.0	24.8	.0	.20	150.0	.0	11.0	2.3	0.	0.	216.	0.	0.	4.85
N310R2.005	.8	.0	24.7	.0	.09	150.0	-25.0	11.0	2.0	0.	0.	216.	0.	0.	2.68
N310R2.006	.8	.0	27.8	.0	.11	150.0	-28.0	11.0	2.2	0.	0.	242.	0.	0.	3.03
N310R2.007	.9	.0	26.9	.0	.10	150.0	-44.0	11.0	2.3	0.	0.	235.	0.	0.	2.70
N310R2.008	.8	.0	35.0	.0	.12	150.0	-50.0	11.0	2.1	0.	0.	305.	0.	0.	2.92
N310R2.009	.8	.0	27.2	.0	.05	150.0	-56.0	11.0	2.2	0.	0.	237.	0.	0.	1.60
N310R2.010	.4	.0	29.8	.0	.07	150.0	-75.0	11.0	1.1	0.	0.	260.	0.	0.	1.72
N310R3.004	1.0	26.4	26.4	26.5	.22	150.0	.0	11.0	2.7	0.	0.	230.	0.	0.	5.21
N310R3.005	.8	.0	24.5	.0	.11	150.0	-25.0	11.0	2.1	0.	0.	213.	0.	0.	3.03
N310R3.006	.8	.0	30.9	.0	.11	150.0	-28.0	11.0	2.2	0.	0.	270.	0.	0.	3.07
N310R3.007	.9	.0	33.5	.0	.12	150.0	-44.0	11.0	2.4	0.	0.	292.	0.	0.	3.08
N310R3.008	.7	.0	33.3	.0	.09	150.0	-50.0	11.0	2.0	0.	0.	291.	0.	0.	2.34
N310R3.009	.7	.0	46.1	.0	.05	150.0	-56.0	11.0	1.8	0.	0.	402.	0.	0.	1.54
N310R3.010	.5	.0	28.4	.0	.06	150.0	-75.0	11.0	1.4	0.	0.	247.	0.	0.	1.51
N310R4.004	1.0	23.8	23.8	23.9	.14	150.0	.0	11.0	2.7	0.	0.	208.	0.	0.	3.37
N310R4.005	.8	.0	27.0	.0	.10	150.0	-25.0	11.0	2.0	0.	0.	236.	0.	0.	2.81
N310R4.006	.8	.0	27.8	.0	.10	150.0	-28.0	11.0	2.2	0.	0.	242.	0.	0.	2.86
N310R4.007	.8	.0	36.4	.0	.12	150.0	-44.0	11.0	2.1	0.	0.	317.	0.	0.	3.15
N310R4.008	.9	.0	36.6	.0	.12	150.0	-50.0	11.0	2.3	0.	0.	319.	0.	0.	3.15
N310R4.009	.8	.0	25.6	.0	.10	150.0	-56.0	11.0	2.2	0.	0.	223.	0.	0.	2.73
N310R4.010	.8	.0	27.5	.0	.06	150.0	-75.0	11.0	2.3	0.	0.	240.	0.	0.	1.70
N310R5.004	.9	.0	28.3	.0	.13	150.0	.0	11.0	2.5	0.	0.	246.	0.	0.	3.35
N310R5.005	.9	.0	28.7	.0	.09	150.0	-25.0	11.0	2.4	0.	0.	250.	0.	0.	2.70
N310R5.006	.9	.0	28.6	.0	.11	150.0	-28.0	11.0	2.5	0.	0.	249.	0.	0.	3.02
N310R5.007	.1	.0	.0	.0	.02	150.0	-44.0	11.0	.3	0.	0.	0.	0.	0.	.44
N310R5.008	1.0	29.7	29.7	29.7	.12	150.0	-50.0	11.0	2.7	0.	0.	259.	0.	0.	3.05
N310R5.009	1.0	27.3	27.3	27.3	.09	150.0	-56.0	11.0	2.7	0.	0.	238.	0.	0.	2.44
N310R5.010	.6	.0	32.3	.0	.06	150.0	-75.0	11.0	1.6	0.	0.	281.	0.	0.	1.39

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310S1.004	.8	.0	32.2	.0	.08	150.0	.0	17.0	2.2	0.	0.	281.	0.	0.	2.09
N310S1.005	.8	.0	29.9	.0	.03	150.0	-25.0	17.0	2.1	0.	0.	261.	0.	0.	1.39
N310S1.006	.9	.0	29.9	.0	.01	150.0	-28.0	17.0	2.3	0.	0.	261.	0.	0.	1.22
N310S1.007	.1	.0	.0	.0	.01	150.0	-44.0	17.0	.1	0.	0.	0.	0.	0.	.33
N310S1.008	.9	.0	29.7	.0	.06	150.0	-50.0	17.0	2.3	0.	0.	259.	0.	0.	1.54
N310S1.009	.6	.0	43.6	.0	.04	150.0	-56.0	17.0	1.5	0.	0.	380.	0.	0.	1.30
N310S1.010	.3	.0	26.0	.0	.01	150.0	-75.0	17.0	.8	0.	0.	227.	0.	0.	.46
N310S2.004	.9	.0	37.2	.0	.10	150.0	.0	17.0	2.4	0.	0.	325.	0.	0.	2.61
N310S2.005	.7	.0	22.2	.0	.03	150.0	-25.0	17.0	1.9	0.	0.	194.	0.	0.	1.31
N310S2.006	.7	.0	30.4	.0	.02	150.0	-28.0	17.0	1.9	0.	0.	265.	0.	0.	1.13
N310S2.007	.1	.0	.0	.0	.00	150.0	-44.0	17.0	.1	0.	0.	0.	0.	0.	.01
N310S2.008	.7	.0	32.5	.0	.03	150.0	-50.0	17.0	1.8	0.	0.	284.	0.	0.	1.34
N310S2.009	.7	.0	25.3	.0	.04	150.0	-56.0	17.0	1.9	0.	0.	220.	0.	0.	1.06
N310S2.010	.4	.0	49.2	.0	.06	150.0	-75.0	17.0	1.0	0.	0.	429.	0.	0.	1.34
N310S3.004	.9	.0	30.3	.0	.05	150.0	.0	17.0	2.5	0.	0.	264.	0.	0.	1.79
N310S3.005	.9	.0	30.5	.0	.02	150.0	-25.0	17.0	2.3	0.	0.	266.	0.	0.	1.34
N310S3.006	.8	.0	30.6	.0	.03	150.0	-28.0	17.0	2.2	0.	0.	267.	0.	0.	1.41
N310S3.007	.0	.0	.0	.0	.00	150.0	-44.0	17.0	.0	0.	0.	0.	0.	0.	.32
N310S3.008	1.1	30.4	30.4	30.5	.05	150.0	-50.0	17.0	2.9	0.	0.	265.	0.	0.	1.43
N310S3.009	.8	.0	27.8	.0	.04	150.0	-56.0	17.0	2.0	0.	0.	243.	0.	0.	1.16
N310S3.010	.3	.0	23.4	.0	.00	150.0	-75.0	17.0	.8	0.	0.	204.	0.	0.	.40
N310S4.004	.8	.0	27.3	.0	.04	150.0	.0	17.0	2.1	0.	0.	238.	0.	0.	1.72
N310S4.005	.7	.0	29.5	.0	.01	150.0	-25.0	17.0	1.8	0.	0.	258.	0.	0.	1.16
N310S4.006	.7	.0	33.1	.0	.04	150.0	-28.0	17.0	1.8	0.	0.	289.	0.	0.	1.53
N310S4.007	.0	.0	.0	.0	.00	150.0	-44.0	17.0	.0	0.	0.	0.	0.	0.	.34
N310S4.008	.7	.0	34.4	.0	.03	150.0	-50.0	17.0	1.9	0.	0.	300.	0.	0.	1.16
N310S4.009	.6	.0	40.0	.0	.01	150.0	-56.0	17.0	1.6	0.	0.	349.	0.	0.	.69
N310S4.010	.5	.0	28.5	.0	.01	150.0	-75.0	17.0	1.3	0.	0.	248.	0.	0.	.22
N310S5.004	.8	.0	23.6	.0	.08	150.0	.0	17.0	2.1	0.	0.	206.	0.	0.	2.32
N310S5.005	.9	.0	26.1	.0	.02	150.0	-25.0	17.0	2.3	0.	0.	227.	0.	0.	1.32
N310S5.006	.9	.0	26.2	.0	.03	150.0	-28.0	17.0	2.4	0.	0.	228.	0.	0.	1.34
N310S5.007	.2	.0	94.1	.0	-.09	150.0	-44.0	17.0	.6	0.	0.	820.	0.	0.	.35
N310S5.008	.6	.0	19.1	.0	.01	150.0	-50.0	17.0	1.5	0.	0.	167.	0.	0.	1.00
N310S5.009	.6	.0	33.9	.0	.03	150.0	-56.0	17.0	1.7	0.	0.	296.	0.	0.	.84
N310S5.010	.5	.0	19.6	.0	.05	150.0	-75.0	17.0	1.3	0.	0.	171.	0.	0.	1.24
N310T1.004	.2	.0	29.5	.0	.05	250.0	75.0	1.0	.6	0.	0.	258.	0.	0.	1.34
N310T1.005	.1	.0	.0	.0	.05	250.0	66.0	1.0	.4	0.	0.	0.	0.	0.	1.13
N310T1.006	.2	.0	33.7	.0	.04	250.0	56.0	1.0	.6	0.	0.	294.	0.	0.	.97
N310T1.007	.1	.0	.0	.0	.02	250.0	44.0	1.0	.2	0.	0.	0.	0.	0.	.52
N310T1.008	.7	.0	33.3	.0	.09	250.0	33.0	1.0	1.8	0.	0.	290.	0.	0.	2.19
N310T1.009	.8	.0	28.6	.0	.17	250.0	25.0	1.0	2.1	0.	0.	249.	0.	0.	4.08
N310T1.010	.7	.0	24.2	.0	.16	250.0	.0	1.0	1.8	0.	0.	211.	0.	0.	3.94

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310T2.004	.1	.0	.0	.0	-.05	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.19
N310T2.005	.2	.0	.0	.0	.03	250.0	66.0	1.0	.4	0.	0.	0.	0.	0.	1.05
N310T2.006	.2	.0	.0	.0	.01	250.0	56.0	1.0	.5	0.	0.	0.	0.	0.	.53
N310T2.007	.5	.0	31.3	.0	.09	250.0	44.0	1.0	1.4	0.	0.	273.	0.	0.	2.30
N310T2.008	.5	.0	29.4	.0	.02	250.0	33.0	1.0	1.4	0.	0.	256.	0.	0.	1.06
N310T2.009	.5	.0	28.2	.0	.06	250.0	25.0	1.0	1.5	0.	0.	246.	0.	0.	1.73
N310T2.010	.7	.0	27.7	.0	.23	250.0	.0	1.0	1.8	0.	0.	242.	0.	0.	5.35
N310T3.004	.1	.0	.0	.0	.00	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.50
N310T3.005	.1	.0	.0	.0	-.07	250.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.04
N310T3.006	.1	.0	.0	.0	.00	250.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.36
N310T3.007	.1	.0	.0	.0	.00	250.0	44.0	1.0	.3	0.	0.	0.	0.	0.	.44
N310T3.008	.3	.0	37.8	.0	.02	250.0	33.0	1.0	.9	0.	0.	329.	0.	0.	.75
N310T3.009	.3	.0	36.5	.0	.04	250.0	25.0	1.0	.9	0.	0.	318.	0.	0.	1.22
N310T3.010	.6	.0	26.2	.0	.21	250.0	.0	1.0	1.6	0.	0.	229.	0.	0.	5.03
N310T4.004	.1	.0	.0	.0	.02	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.70
N310T4.005	.1	.0	.0	.0	-.02	250.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.15
N310T4.006	.1	.0	.0	.0	.02	250.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.63
N310T4.007	.4	.0	32.0	.0	.01	250.0	44.0	1.0	1.0	0.	0.	279.	0.	0.	.94
N310T4.008	.8	.0	30.3	.0	.09	250.0	33.0	1.0	2.1	0.	0.	264.	0.	0.	2.25
N310T4.009	.6	.0	31.3	.0	.09	250.0	25.0	1.0	1.6	0.	0.	273.	0.	0.	2.33
N310T4.010	.6	.0	30.0	.0	.12	250.0	.0	1.0	1.5	0.	0.	262.	0.	0.	3.05
N310T5.004	.1	.0	.0	.0	-.04	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.19
N310T5.005	.1	.0	.0	.0	.05	250.0	66.0	1.0	.3	0.	0.	0.	0.	0.	1.31
N310T5.006	.1	.0	.0	.0	.01	250.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.43
N310T5.007	.2	.0	.0	.0	.02	250.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.78
N310T5.008	.6	.0	32.7	.0	.09	250.0	33.0	1.0	1.6	0.	0.	285.	0.	0.	2.15
N310T5.009	.7	.0	32.6	.0	.14	250.0	25.0	1.0	1.8	0.	0.	285.	0.	0.	3.42
N310T5.010	.6	.0	23.9	.0	.10	250.0	.0	1.0	1.5	0.	0.	209.	0.	0.	3.12
N310U1.004	.1	.0	.0	.0	-.01	250.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.29
N310U1.005	.1	.0	.0	.0	-.01	250.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.32
N310U1.006	.1	.0	.0	.0	.01	250.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.21
N310U1.007	.1	.0	.0	.0	.01	250.0	44.0	5.0	.2	0.	0.	0.	0.	0.	.15
N310U1.008	.2	.0	29.2	.0	.03	250.0	33.0	5.0	.6	0.	0.	254.	0.	0.	.94
N310U1.009	.4	.0	26.4	.0	.05	250.0	25.0	5.0	1.1	0.	0.	230.	0.	0.	1.22
N310U1.010	.7	.0	28.9	.0	.15	250.0	.0	5.0	1.9	0.	0.	252.	0.	0.	3.65
N310U2.004	.1	.0	.0	.0	-.02	250.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.05
N310U2.005	.1	.0	.0	.0	.01	250.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.53
N310U2.006	.1	.0	.0	.0	.01	250.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.41
N310U2.007	.1	.0	.0	.0	.01	250.0	44.0	5.0	.3	0.	0.	0.	0.	0.	.45
N310U2.008	.4	.0	28.5	.0	.04	250.0	33.0	5.0	1.2	0.	0.	248.	0.	0.	.98
N310U2.009	.7	.0	29.8	.0	.06	250.0	25.0	5.0	1.8	0.	0.	260.	0.	0.	1.63
N310U2.010	.7	.0	28.1	.0	.11	250.0	.0	5.0	1.9	0.	0.	245.	0.	0.	2.82

FALCON 3: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310U3.004	.1	.0	.0	.0	.00	250.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.33
N310U3.005	.1	.0	.0	.0	.00	250.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.15
N310U3.006	.1	.0	.0	.0	.04	250.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.91
N310U3.007	.0	.0	.0	.0	-.01	250.0	44.0	5.0	.1	0.	0.	0.	0.	0.	.26
N310U3.008	.5	.0	31.2	.0	.02	250.0	33.0	5.0	1.4	0.	0.	272.	0.	0.	.61
N310U3.009	.6	.0	31.1	.0	.06	250.0	25.0	5.0	1.6	0.	0.	271.	0.	0.	1.64
N310U3.010	.7	.0	31.4	.0	.15	250.0	.0	5.0	1.8	0.	0.	274.	0.	0.	3.51
N310U4.004	.1	.0	.0	.0	-.03	250.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.15
N310U4.005	.1	.0	.0	.0	-.01	250.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.29
N310U4.006	.1	.0	.0	.0	.02	250.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.65
N310U4.007	.1	.0	.0	.0	.00	250.0	44.0	5.0	.2	0.	0.	0.	0.	0.	.15
N310U4.008	.5	.0	32.2	.0	.05	250.0	33.0	5.0	1.3	0.	0.	281.	0.	0.	1.18
N310U4.009	.6	.0	32.5	.0	.09	250.0	25.0	5.0	1.6	0.	0.	283.	0.	0.	2.13
N310U4.010	.7	.0	31.0	.0	.11	250.0	.0	5.0	1.9	0.	0.	270.	0.	0.	2.70
N310U5.004	.1	.0	.0	.0	.00	250.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.37
N310U5.005	.1	.0	.0	.0	.02	250.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.56
N310U5.006	.1	.0	.0	.0	-.02	250.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.13
N310U5.007	.1	.0	.0	.0	.00	250.0	44.0	5.0	.1	0.	0.	0.	0.	0.	.00
N310U5.008	.5	.0	29.4	.0	.02	250.0	33.0	5.0	1.3	0.	0.	256.	0.	0.	.66
N310U5.009	.7	.0	27.0	.0	.08	250.0	25.0	5.0	1.8	0.	0.	235.	0.	0.	1.80
N310U5.010	.5	.0	43.3	.0	.07	250.0	.0	5.0	1.4	0.	0.	378.	0.	0.	1.91
N310V1.004	.1	.0	.0	.0	.02	250.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.59
N310V1.005	.1	.0	.0	.0	.04	250.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.88
N310V1.006	.1	.0	.0	.0	.04	250.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.89
N310V1.007	.2	.0	.0	.0	-.01	250.0	44.0	11.0	.5	0.	0.	0.	0.	0.	.80
N310V1.008	.6	.0	32.3	.0	.04	250.0	33.0	11.0	1.6	0.	0.	281.	0.	0.	.98
N310V1.009	.6	.0	29.7	.0	.03	250.0	25.0	11.0	1.5	0.	0.	259.	0.	0.	.86
N310V1.010	.4	.0	31.4	.0	.03	250.0	.0	11.0	1.2	0.	0.	274.	0.	0.	.98
N310V2.004	.1	.0	.0	.0	.00	250.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.27
N310V2.005	.3	.0	28.4	.0	.00	250.0	66.0	11.0	.7	0.	0.	248.	0.	0.	.04
N310V2.006	.4	.0	27.2	.0	-.01	250.0	56.0	11.0	1.0	0.	0.	237.	0.	0.	.10
N310V2.007	.1	.0	.0	.0	-.04	250.0	44.0	11.0	.3	0.	0.	0.	0.	0.	.06
N310V2.008	.6	.0	21.6	.0	.00	250.0	33.0	11.0	1.7	0.	0.	188.	0.	0.	.49
N310V2.009	.7	.0	27.1	.0	.04	250.0	25.0	11.0	2.0	0.	0.	236.	0.	0.	1.19
N310V2.010	.6	.0	27.4	.0	.05	250.0	.0	11.0	1.5	0.	0.	239.	0.	0.	1.35
N310V3.004	.1	.0	.0	.0	.01	250.0	75.0	11.0	.4	0.	0.	0.	0.	0.	.51
N310V3.005	.1	.0	.0	.0	.02	250.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.61
N310V3.006	.1	.0	.0	.0	.03	250.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.76
N310V3.007	.1	.0	.0	.0	.00	250.0	44.0	11.0	.2	0.	0.	0.	0.	0.	.25
N310V3.008	.5	.0	20.6	.0	.00	250.0	33.0	11.0	1.3	0.	0.	180.	0.	0.	.11
N310V3.009	.6	.0	20.5	.0	.04	250.0	25.0	11.0	1.7	0.	0.	179.	0.	0.	1.13
N310V3.010	.5	.0	32.8	.0	.06	250.0	.0	11.0	1.2	0.	0.	286.	0.	0.	1.43

FALCON 3: LSR = 100, GAS = ARGON

	MODEL CONDITIONS								PROTOTYPE CONDITIONS							
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310V4.004	.1	.0	.0	.0	.00	250.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.23
N310V4.005	.1	.0	.0	.0	-.03	250.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.02
N310V4.006	.1	.0	.0	.0	-.03	250.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.01
N310V4.007	.1	.0	.0	.0	-.01	250.0	44.0	11.0	.1	0.	0.	0.	0.	0.	.01
N310V4.008	.1	.0	.0	.0	-.02	250.0	33.0	11.0	.4	0.	0.	0.	0.	0.	.07
N310V4.009	.6	.0	30.2	.0	.00	250.0	25.0	11.0	1.7	0.	0.	263.	0.	0.	.40
N310V4.010	.6	.0	30.9	.0	.04	250.0	.0	11.0	1.6	0.	0.	270.	0.	0.	1.14
N310V5.004	.1	.0	.0	.0	.04	250.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.97
N310V5.005	.1	.0	.0	.0	-.01	250.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.13
N310V5.006	.1	.0	.0	.0	.01	250.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.30
N310V5.007	.1	.0	.0	.0	.00	250.0	44.0	11.0	.2	0.	0.	0.	0.	0.	.01
N310V5.008	.6	.0	23.5	.0	.05	250.0	33.0	11.0	1.5	0.	0.	205.	0.	0.	1.36
N310V5.009	.6	.0	25.2	.0	.08	250.0	25.0	11.0	1.6	0.	0.	219.	0.	0.	1.88
N310V5.010	.4	.0	33.7	.0	.04	250.0	.0	11.0	1.2	0.	0.	294.	0.	0.	1.24
N310W1.004	.1	.0	.0	.0	-.02	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.29
N310W1.005	.1	.0	.0	.0	-.01	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.20
N310W1.006	.1	.0	.0	.0	-.01	250.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.22
N310W1.007	.0	.0	.0	.0	.00	250.0	44.0	17.0	.0	0.	0.	0.	0.	0.	.25
N310W1.008	.2	.0	39.5	.0	-.02	250.0	33.0	17.0	.6	0.	0.	345.	0.	0.	.16
N310W1.009	.2	.0	38.9	.0	-.03	250.0	25.0	17.0	.6	0.	0.	339.	0.	0.	.12
N310W1.010	.4	.0	38.4	.0	.03	250.0	.0	17.0	1.2	0.	0.	335.	0.	0.	.93
N310W2.004	.0	.0	.0	.0	-.06	250.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.06
N310W2.005	.1	.0	.0	.0	-.04	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.03
N310W2.006	.1	.0	.0	.0	.01	250.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.49
N310W2.007	.2	.0	.0	.0	.05	250.0	44.0	17.0	.5	0.	0.	0.	0.	0.	1.11
N310W2.008	.4	.0	27.7	.0	.05	250.0	33.0	17.0	1.1	0.	0.	242.	0.	0.	1.13
N310W2.009	.5	.0	21.8	.0	.04	250.0	25.0	17.0	1.2	0.	0.	190.	0.	0.	1.13
N310W2.010	.4	.0	22.4	.0	.04	250.0	.0	17.0	1.0	0.	0.	195.	0.	0.	1.01
N310W3.004	.1	.0	.0	.0	.01	250.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.47
N310W3.005	.1	.0	.0	.0	-.01	250.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.10
N310W3.006	.1	.0	.0	.0	-.03	250.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.03
N310W3.007	.2	.0	.0	.0	-.04	250.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.04
N310W3.008	.5	.0	28.3	.0	.00	250.0	33.0	17.0	1.4	0.	0.	246.	0.	0.	.27
N310W3.009	.4	.0	28.1	.0	.01	250.0	25.0	17.0	1.0	0.	0.	245.	0.	0.	.52
N310W3.010	.4	.0	36.3	.0	.01	250.0	.0	17.0	1.2	0.	0.	317.	0.	0.	.73
N310W4.004	.1	.0	.0	.0	.02	250.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.65
N310W4.005	.1	.0	.0	.0	.01	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.17
N310W4.006	.1	.0	.0	.0	.00	250.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.06
N310W4.007	.1	.0	.0	.0	-.03	250.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.09
N310W4.008	.2	.0	30.6	.0	.01	250.0	33.0	17.0	.6	0.	0.	267.	0.	0.	.17
N310W4.009	.3	.0	26.5	.0	.00	250.0	25.0	17.0	.8	0.	0.	231.	0.	0.	.32
N310W4.010	.5	.0	34.1	.0	.00	250.0	.0	17.0	1.3	0.	0.	297.	0.	0.	.49

FALCON 3: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N310W5.004	.1	.0	.0	.0	.00	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.22
N310W5.005	.1	.0	.0	.0	-.01	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.16
N310W5.006	.1	.0	.0	.0	.02	250.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.64
N310W5.007	.2	.0	.0	.0	.00	250.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.26
N310W5.008	.3	.0	25.5	.0	.02	250.0	33.0	17.0	.8	0.	0.	223.	0.	0.	.66
N310W5.009	.4	.0	29.0	.0	.01	250.0	25.0	17.0	1.1	0.	0.	253.	0.	0.	.47
N310W5.010	.5	.0	31.3	.0	.03	250.0	.0	17.0	1.3	0.	0.	273.	0.	0.	.83

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N315A1.009	4.1	7.7	18.4	36.6	.21	-62.0	30.0	300.0	10.3	125.	197.	197.	197.	197.	6.18
N315A1.008	26.8	.8	15.5	120.7	4.32	-62.0	20.0	300.0	49.7	10.	28.	166.	356.	708.	100.73
N315A1.007	24.5	1.1	15.2	119.6	5.26	-62.0	10.0	300.0	46.8	13.	21.	162.	430.	984.	125.83
N315A1.006	24.6	2.0	13.1	117.3	5.56	-62.0	.0	300.0	46.9	23.	24.	140.	472.	988.	132.88
N315A1.005	21.5	1.8	13.7	117.7	4.40	-62.0	-10.0	300.0	42.5	33.	35.	146.	486.	806.	108.54
N315A1.004	20.5	4.1	17.3	105.8	3.22	-62.0	-20.0	300.0	41.0	44.	52.	184.	396.	1086.	80.13
N315A2.009	2.4	9.6	22.1	50.7	.28	-62.0	30.0	300.0	6.2	183.	0.	236.	0.	237.	8.16
N315A2.008	26.7	1.6	15.5	110.8	5.34	-62.0	20.0	300.0	49.6	18.	19.	165.	406.	610.	121.92
N315A2.007	25.1	.7	12.9	112.5	5.77	-62.0	10.0	300.0	47.6	10.	20.	137.	486.	812.	137.48
N315A2.006	29.4	1.7	16.4	120.3	6.57	-62.0	.0	300.0	52.9	19.	22.	175.	553.	1036.	152.94
N315A2.005	25.3	1.7	15.6	115.4	5.88	-62.0	-10.0	300.0	47.8	22.	31.	167.	507.	1134.	141.05
N315A2.004	23.6	2.1	18.2	106.1	4.24	-62.0	-20.0	300.0	45.4	49.	50.	194.	453.	589.	102.57
N315A3.009	2.5	8.3	20.0	36.6	.17	-62.0	4500.0	300.0	6.6	148.	0.	214.	0.	268.	5.37
N315A3.008	28.7	1.6	16.3	105.8	4.68	-62.0	3000.0	300.0	52.1	32.	33.	174.	375.	1093.	107.20
N315A3.007	28.1	1.3	16.0	114.3	5.40	-62.0	1500.0	300.0	51.4	19.	23.	170.	477.	977.	128.79
N315A3.006	25.7	1.0	14.5	118.9	5.62	-62.0	.0	300.0	48.4	11.	22.	155.	483.	1061.	133.51
N315A3.005	23.2	1.6	15.9	105.6	4.62	-62.0	-1500.0	300.0	45.0	18.	32.	170.	431.	877.	114.45
N315A3.004	28.3	.8	16.2	116.5	4.20	-62.0	-3000.0	300.0	51.7	18.	51.	173.	373.	965.	100.18
N315A4.009	3.5	6.7	20.7	38.1	.29	-62.0	4500.0	300.0	9.0	125.	0.	221.	0.	303.	8.32
N315A4.008	29.6	1.7	14.9	112.7	5.24	-62.0	3000.0	300.0	53.2	20.	45.	159.	405.	982.	118.79
N315A4.007	25.3	1.2	14.2	120.7	5.79	-62.0	1500.0	300.0	47.8	14.	23.	152.	472.	808.	137.78
N315A4.006	27.3	1.1	16.1	111.4	5.91	-62.0	.0	300.0	50.4	15.	23.	171.	542.	746.	140.12
N315A4.005	24.0	1.2	14.8	120.2	5.33	-62.0	-1500.0	300.0	46.0	15.	23.	158.	490.	792.	129.13
N315A4.004	27.2	2.4	17.2	117.1	4.17	-62.0	-3000.0	300.0	50.3	26.	43.	184.	406.	685.	100.02
N315A5.009	3.6	7.5	14.6	38.5	.23	-62.0	4500.0	300.0	9.3	122.	0.	156.	0.	277.	6.62
N315A5.008	24.8	1.6	16.1	117.2	4.55	-62.0	3000.0	300.0	47.2	18.	30.	172.	345.	576.	106.45
N315A5.007	27.6	.8	14.0	105.1	5.48	-62.0	1500.0	300.0	50.8	9.	20.	150.	445.	938.	131.11
N315A5.006	25.8	1.5	14.8	111.3	6.02	-62.0	.0	300.0	48.4	17.	22.	158.	602.	976.	143.57
N315A5.005	23.8	3.0	15.0	121.0	4.94	-62.0	-1500.0	300.0	45.8	32.	33.	160.	525.	1032.	120.84
N315A5.004	25.2	2.2	15.4	120.9	4.28	-62.0	-3000.0	300.0	47.7	34.	36.	164.	452.	590.	101.98
N315B1.009	1.6	13.2	26.0	31.0	.21	-32.0	4500.0	150.0	4.2	0.	0.	278.	0.	0.	6.11
N315B1.008	26.7	1.0	15.4	96.8	3.57	-32.0	3000.0	150.0	49.6	13.	53.	165.	405.	993.	86.53
N315B1.007	32.0	.2	14.5	87.6	5.07	-32.0	1500.0	150.0	56.0	2.	3.	155.	430.	715.	117.88
N315B1.006	30.2	.2	14.9	46.4	3.64	-32.0	.0	150.0	53.9	3.	3.	159.	272.	298.	82.51
N315B1.005	28.5	.2	11.8	66.9	2.73	-32.0	-1500.0	150.0	51.9	2.	2.	126.	259.	378.	63.63
N315B1.004	23.9	3.1	10.3	63.4	3.24	-32.0	-3000.0	150.0	45.9	40.	41.	110.	543.	548.	80.97
N315B2.009	1.6	7.0	21.2	30.2	.23	-32.0	4500.0	150.0	4.3	0.	0.	226.	0.	0.	6.73
N315B2.008	27.1	.8	15.1	80.8	3.65	-32.0	3000.0	150.0	50.1	9.	22.	161.	367.	860.	88.52
N315B2.007	33.4	.2	11.5	108.8	5.66	-32.0	1500.0	150.0	57.6	2.	2.	123.	374.	650.	129.15
N315B2.006	27.6	.2	14.5	49.3	3.20	-32.0	.0	150.0	50.7	2.	2.	155.	246.	313.	73.79
N315B2.005	31.4	.1	13.3	63.9	2.68	-32.0	-1500.0	150.0	55.3	1.	2.	142.	302.	455.	63.06
N315B2.004	22.6	.7	16.2	86.1	3.09	-32.0	-3000.0	150.0	44.2	36.	45.	173.	313.	689.	76.86

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N315B3.009	2.0	14.1	18.2	32.8	.20	-32.0	4500.0	150.0	5.1	194.	0.	194.	0.	195.	5.92
N315B3.008	26.3	.5	14.8	100.8	4.61	-32.0	3000.0	150.0	49.1	5.	28.	158.	390.	971.	108.66
N315B3.007	30.3	.2	15.0	85.1	5.30	-32.0	1500.0	150.0	54.0	2.	2.	160.	368.	834.	122.92
N315B3.006	28.8	.3	15.6	53.9	3.63	-32.0	.0	150.0	52.3	3.	3.	167.	251.	408.	82.77
N315B3.005	28.6	.1	10.6	62.1	2.60	-32.0	-1500.0	150.0	52.0	2.	2.	113.	236.	535.	61.51
N315B3.004	19.9	1.3	13.3	80.2	3.37	-32.0	-3000.0	150.0	40.2	26.	33.	142.	311.	497.	84.13
N315B4.009	1.9	11.1	18.6	25.5	.23	-32.0	4500.0	150.0	5.0	0.	0.	199.	0.	0.	6.77
N315B4.008	25.8	2.1	15.6	100.2	3.97	-32.0	3000.0	150.0	48.4	23.	27.	167.	334.	920.	96.38
N315B4.007	31.9	.2	12.6	107.1	5.21	-32.0	1500.0	150.0	55.9	2.	2.	135.	415.	781.	121.60
N315B4.006	28.7	.2	14.6	54.7	3.27	-32.0	.0	150.0	52.1	3.	3.	156.	225.	341.	75.60
N315B4.005	30.0	.1	14.9	100.1	2.33	-32.0	-1500.0	150.0	53.7	2.	2.	159.	341.	405.	56.16
N315B4.004	23.4	1.3	14.5	74.9	3.31	-32.0	-3000.0	150.0	45.2	17.	21.	155.	388.	727.	84.48
N315B5.009	2.0	10.1	19.3	31.9	.29	-32.0	4500.0	150.0	5.2	206.	0.	206.	0.	206.	8.56
N315B5.008	25.7	1.1	15.0	99.5	3.57	-32.0	3000.0	150.0	48.3	13.	16.	160.	383.	760.	86.65
N315B5.007	32.8	.1	11.9	81.4	5.01	-32.0	1500.0	150.0	56.9	2.	2.	127.	451.	734.	115.71
N315B5.006	27.9	.2	15.0	109.6	3.30	-32.0	.0	150.0	51.1	2.	5.	160.	269.	370.	77.14
N315B5.005	29.5	.2	12.3	70.8	2.39	-32.0	-1500.0	150.0	53.0	2.	2.	131.	323.	716.	57.93
N315B5.004	22.0	1.1	13.6	99.6	3.94	-32.0	-3000.0	150.0	43.3	17.	25.	145.	362.	998.	96.86
N315C1.009	1.8	12.1	16.5	36.0	.23	-2.0	4500.0	150.0	4.6	0.	0.	176.	0.	0.	6.75
N315C1.008	12.2	2.8	18.7	87.7	1.99	-2.0	3000.0	150.0	27.3	37.	98.	199.	291.	814.	52.71
N315C1.007	19.0	.8	17.0	86.5	1.25	-2.0	1500.0	150.0	38.9	36.	82.	182.	268.	308.	32.89
N315C1.006	9.1	2.7	11.1	64.5	.76	-2.0	.0	150.0	21.2	30.	98.	119.	128.	468.	21.47
N315C1.005	3.9	2.8	10.3	80.1	.62	-2.0	-1500.0	150.0	9.8	99.	0.	110.	0.	315.	17.66
N315C1.004	6.4	9.4	14.7	86.2	.81	-2.0	-3000.0	150.0	15.7	102.	153.	156.	160.	731.	22.75
N315C2.009	1.7	12.6	22.9	28.2	.23	-2.0	4500.0	150.0	4.4	0.	0.	245.	0.	0.	6.69
N315C2.008	18.1	1.0	15.9	78.0	2.84	-2.0	3000.0	150.0	37.4	28.	54.	169.	456.	567.	75.52
N315C2.007	27.3	.8	16.0	81.0	2.79	-2.0	1500.0	150.0	50.3	10.	30.	171.	749.	755.	67.62
N315C2.006	25.6	.2	16.4	80.5	2.05	-2.0	.0	150.0	48.1	28.	59.	175.	222.	312.	50.24
N315C2.005	20.5	4.5	16.4	80.5	1.17	-2.0	-1500.0	150.0	41.1	52.	66.	175.	192.	494.	30.86
N315C2.004	14.8	5.0	13.8	89.3	1.28	-2.0	-3000.0	150.0	32.0	60.	99.	148.	200.	492.	34.21
N315C3.009	3.0	7.6	16.2	37.6	.33	-2.0	4500.0	150.0	7.7	172.	0.	172.	0.	270.	9.34
N315C3.008	21.8	.2	16.4	91.2	3.43	-2.0	3000.0	150.0	42.9	31.	34.	175.	420.	966.	85.93
N315C3.007	25.6	2.8	15.6	86.8	1.84	-2.0	1500.0	150.0	48.2	38.	77.	166.	382.	384.	49.77
N315C3.006	24.7	3.0	15.9	84.4	.88	-2.0	.0	150.0	46.9	85.	89.	170.	214.	266.	28.88
N315C3.005	17.0	8.1	15.9	43.4	.86	-2.0	-1500.0	150.0	35.6	91.	129.	169.	258.	457.	23.23
N315C3.004	20.3	1.1	17.6	74.7	1.72	-2.0	-3000.0	150.0	40.8	15.	96.	188.	648.	778.	45.25
N315C4.009	2.3	11.9	19.1	36.9	.27	-2.0	4500.0	150.0	6.0	204.	0.	204.	0.	214.	7.85
N315C4.008	17.8	.6	16.2	91.6	2.69	-2.0	3000.0	150.0	36.9	42.	59.	173.	485.	876.	69.82
N315C4.007	21.4	3.1	13.2	48.5	.84	-2.0	1500.0	150.0	42.4	35.	43.	141.	199.	272.	35.42
N315C4.006	22.6	2.0	14.2	78.4	1.12	-2.0	.0	150.0	44.1	77.	78.	151.	196.	272.	29.76
N315C4.005	12.9	5.3	17.8	78.7	.67	-2.0	-1500.0	150.0	28.5	80.	83.	190.	194.	437.	19.27
N315C4.004	16.1	5.1	15.0	87.2	1.36	-2.0	-3000.0	150.0	34.2	57.	79.	160.	224.	727.	36.76

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N315C5.009	1.8	11.6	18.8	30.7	.24	-2.0	4500.0	150.0	4.8	0.	0.	201.	0.	0.	6.89
N315C5.008	20.7	3.5	15.9	86.1	3.03	-2.0	3000.0	150.0	41.3	44.	65.	169.	589.	786.	77.89
N315C5.007	28.7	.4	15.2	84.7	3.20	-2.0	1500.0	150.0	52.1	20.	48.	162.	598.	855.	77.48
N315C5.006	25.2	.9	15.6	56.9	2.57	-2.0	.0	150.0	47.7	50.	53.	167.	272.	601.	62.00
N315C5.005	20.3	1.1	17.7	64.9	1.78	-2.0	-1500.0	150.0	40.7	58.	107.	189.	397.	595.	44.44
N315C5.004	18.4	6.5	14.4	79.7	1.88	-2.0	-3000.0	150.0	37.8	74.	106.	154.	428.	487.	48.11
F315D1.006	.1	.0	.0	.0	.02	50.0	9900.0	150.0	.4	0.	0.	0.	0.	0.	.58
F315D1.007	.2	.0	24.4	.0	.06	50.0	6600.0	150.0	.6	0.	0.	261.	0.	0.	1.81
F315D1.008	.8	.0	7.3	.0	.04	50.0	3300.0	150.0	2.2	0.	0.	78.	0.	0.	1.15
F315D1.009	.8	.0	13.7	.0	.15	50.0	.0	150.0	2.0	0.	0.	146.	0.	0.	4.46
F315D1.010	.8	.0	16.9	.0	.16	50.0	-3300.0	150.0	2.3	0.	0.	180.	0.	0.	4.68
F315D1.011	.9	.0	11.5	.0	.11	50.0	-6600.0	150.0	2.5	0.	0.	123.	0.	0.	3.17
F315D1.012	.7	.0	23.4	.0	.07	50.0	-9900.0	150.0	1.9	0.	0.	250.	0.	0.	2.17
F315D2.006	.0	.0	.0	.0	-.03	50.0	9900.0	150.0	.1	0.	0.	0.	0.	0.	.04
F315D2.007	.1	.0	.0	.0	.00	50.0	6600.0	150.0	.3	0.	0.	0.	0.	0.	.34
F315D2.008	.7	.0	4.9	.0	.03	50.0	3300.0	150.0	1.8	0.	0.	52.	0.	0.	.92
F315D2.009	.8	.0	19.4	.0	.15	50.0	.0	150.0	2.1	0.	0.	208.	0.	0.	4.27
F315D2.010	.9	.0	20.1	.0	.17	50.0	-3300.0	150.0	2.4	0.	0.	215.	0.	0.	5.01
F315D2.011	1.0	.0	19.2	.0	.14	50.0	-6600.0	150.0	2.6	0.	0.	205.	0.	0.	4.20
F315D2.012	.7	.0	18.1	.0	.05	50.0	-9900.0	150.0	1.7	0.	0.	193.	0.	0.	1.41
F315D3.006	.1	.0	.0	.0	-.02	50.0	9900.0	150.0	.2	0.	0.	0.	0.	0.	.03
F315D3.007	.2	.0	14.2	.0	.04	50.0	6600.0	150.0	.6	0.	0.	151.	0.	0.	1.19
F315D3.008	1.0	.0	19.3	.0	.05	50.0	3300.0	150.0	2.6	0.	0.	206.	0.	0.	1.36
F315D3.009	.8	.0	20.2	.0	.14	50.0	.0	150.0	2.1	0.	0.	216.	0.	0.	4.14
F315D3.010	1.1	13.6	18.6	22.9	.28	50.0	-3300.0	150.0	2.9	0.	0.	198.	0.	0.	7.94
F315D3.011	1.1	18.9	18.9	19.0	.15	50.0	-6600.0	150.0	2.8	0.	0.	202.	0.	0.	4.39
F315D3.012	.5	.0	18.3	.0	.06	50.0	-9900.0	150.0	1.4	0.	0.	195.	0.	0.	1.86
F315D4.006	.1	.0	.0	.0	.00	50.0	9900.0	150.0	.2	0.	0.	0.	0.	0.	.18
F315D4.007	.1	.0	.0	.0	-.02	50.0	6600.0	150.0	.3	0.	0.	0.	0.	0.	.09
F315D4.008	.5	.0	12.4	.0	.03	50.0	3300.0	150.0	1.3	0.	0.	132.	0.	0.	1.03
F315D4.009	.9	.0	18.0	.0	.17	50.0	.0	150.0	2.4	0.	0.	192.	0.	0.	4.76
F315D4.010	.9	.0	19.1	.0	.19	50.0	-3300.0	150.0	2.5	0.	0.	204.	0.	0.	5.57
F315D4.011	.8	.0	15.0	.0	.08	50.0	-6600.0	150.0	2.1	0.	0.	160.	0.	0.	2.43
F315D4.012	.1	.0	.0	.0	.02	50.0	-9900.0	150.0	.4	0.	0.	0.	0.	0.	.57
F315D5.006	.1	.0	.0	.0	.00	50.0	9900.0	150.0	.2	0.	0.	0.	0.	0.	.08
F315D5.007	.1	.0	.0	.0	.02	50.0	6600.0	150.0	.4	0.	0.	0.	0.	0.	.66
F315D5.008	.8	.0	17.3	.0	.06	50.0	3300.0	150.0	2.2	0.	0.	184.	0.	0.	1.87
F315D5.009	1.0	20.7	20.7	20.7	.22	50.0	.0	150.0	2.8	0.	0.	221.	0.	0.	6.25
F315D5.010	1.1	19.7	19.8	20.0	.17	50.0	-3300.0	150.0	2.9	0.	0.	211.	0.	0.	4.95
F315D5.011	.8	.0	18.4	.0	.06	50.0	-6600.0	150.0	2.1	0.	0.	196.	0.	0.	2.13
F315D5.012	.2	.0	22.1	.0	-.01	50.0	-9900.0	150.0	.6	0.	0.	236.	0.	0.	.22
F315E1.006	.1	.0	.0	.0	-.02	50.0	9900.0	750.0	.2	0.	0.	0.	0.	0.	.08

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315E1.007	.1	.0	.0	.0	.01	50.0	6600.0	750.0	.4	0.	0.	0.	0.	0.	.35
F315E1.008	1.1	23.7	23.8	23.8	.06	50.0	3300.0	750.0	2.9	0.	0.	254.	0.	0.	1.66
F315E1.009	1.1	16.9	19.4	20.1	.17	50.0	.0	750.0	3.0	0.	0.	207.	0.	0.	4.94
F315E1.010	1.5	16.2	17.3	24.7	.19	50.0	-3300.0	750.0	4.0	0.	0.	184.	0.	0.	5.48
F315E1.011	1.3	21.2	22.4	24.9	.09	50.0	-6600.0	750.0	3.5	0.	0.	239.	0.	0.	2.66
F315E1.012	.3	.0	23.3	.0	.02	50.0	-9900.0	750.0	.9	0.	0.	249.	0.	0.	.56
F315E2.006	.1	.0	.0	.0	.01	50.0	9900.0	750.0	.2	0.	0.	0.	0.	0.	.21
F315E2.007	.1	.0	.0	.0	.01	50.0	6600.0	750.0	.3	0.	0.	0.	0.	0.	.40
F315E2.008	.9	.0	20.4	.0	.04	50.0	3300.0	750.0	2.4	0.	0.	218.	0.	0.	1.13
F315E2.009	1.0	23.5	23.5	23.6	.17	50.0	.0	750.0	2.7	0.	0.	251.	0.	0.	4.86
F315E2.010	1.3	15.3	15.4	15.4	.20	50.0	-3300.0	750.0	3.3	0.	0.	164.	0.	0.	5.68
F315E2.011	1.0	.0	25.3	.0	.09	50.0	-6600.0	750.0	2.5	0.	0.	270.	0.	0.	2.73
F315E2.012	.4	.0	26.6	.0	.03	50.0	-9900.0	750.0	1.0	0.	0.	284.	0.	0.	.96
F315E3.006	.1	.0	.0	.0	.00	50.0	9900.0	750.0	.2	0.	0.	0.	0.	0.	.00
F315E3.007	.5	.0	17.7	.0	.01	50.0	6600.0	750.0	1.3	0.	0.	189.	0.	0.	.50
F315E3.008	1.0	.0	22.7	.0	.06	50.0	3300.0	750.0	2.6	0.	0.	242.	0.	0.	1.66
F315E3.009	.9	.0	23.0	.0	.18	50.0	.0	750.0	2.4	0.	0.	246.	0.	0.	5.14
F315E3.010	1.0	21.6	21.6	24.1	.19	50.0	-3300.0	750.0	2.7	0.	0.	230.	0.	0.	5.38
F315E3.011	1.2	18.5	23.3	23.3	.11	50.0	-6600.0	750.0	3.1	0.	0.	249.	0.	0.	3.29
F315E3.012	.2	.0	.0	.0	-.01	50.0	-9900.0	750.0	.5	0.	0.	0.	0.	0.	.12
F315E4.006	.1	.0	.0	.0	-.03	50.0	9900.0	750.0	.1	0.	0.	0.	0.	0.	.07
F315E4.007	.1	.0	.0	.0	-.01	50.0	6600.0	750.0	.3	0.	0.	0.	0.	0.	.14
F315E4.008	1.1	11.8	16.2	16.3	.06	50.0	3300.0	750.0	2.8	0.	0.	173.	0.	0.	1.93
F315E4.009	1.5	12.1	16.7	17.7	.20	50.0	.0	750.0	3.9	0.	0.	178.	0.	0.	5.68
F315E4.010	1.1	21.3	21.3	21.3	.18	50.0	-3300.0	750.0	2.8	0.	0.	227.	0.	0.	5.10
F315E4.011	1.2	21.9	21.9	22.0	.06	50.0	-6600.0	750.0	3.2	0.	0.	234.	0.	0.	1.96
F315E4.012	.3	.0	27.3	.0	.00	50.0	-9900.0	750.0	.8	0.	0.	291.	0.	0.	.29
F315E5.006	.1	.0	.0	.0	.00	50.0	9900.0	750.0	.2	0.	0.	0.	0.	0.	.07
F315E5.007	.2	.0	.0	.0	.00	50.0	6600.0	750.0	.5	0.	0.	0.	0.	0.	.30
F315E5.008	.8	.0	8.6	.0	.06	50.0	3300.0	750.0	2.3	0.	0.	91.	0.	0.	1.90
F315E5.009	1.1	18.7	22.9	24.3	.18	50.0	.0	750.0	2.9	0.	0.	245.	0.	0.	5.14
F315E5.010	1.0	.0	20.8	.0	.16	50.0	-3300.0	750.0	2.6	0.	0.	222.	0.	0.	4.49
F315E5.011	1.1	15.8	15.8	15.8	.07	50.0	-6600.0	750.0	2.8	0.	0.	168.	0.	0.	2.08
F315E5.012	.3	.0	21.8	.0	.00	50.0	-9900.0	750.0	.7	0.	0.	233.	0.	0.	.28
F315F1.006	.1	.0	.0	.0	-.01	50.0	9900.0	1650.0	.2	0.	0.	0.	0.	0.	.07
F315F1.007	.2	.0	.0	.0	-.03	50.0	6600.0	1650.0	.4	0.	0.	0.	0.	0.	.03
F315F1.008	1.3	9.8	15.0	19.3	.07	50.0	3300.0	1650.0	3.4	0.	0.	160.	0.	0.	2.08
F315F1.009	1.0	13.7	13.7	22.9	.13	50.0	.0	1650.0	2.7	0.	0.	146.	0.	0.	3.94
F315F1.010	1.0	15.2	24.5	24.6	.16	50.0	-3300.0	1650.0	2.7	0.	0.	262.	0.	0.	4.72
F315F1.011	1.1	20.7	20.8	24.1	.04	50.0	-6600.0	1650.0	2.8	0.	0.	222.	0.	0.	1.41
F315F1.012	.2	.0	.0	.0	.02	50.0	-9900.0	1650.0	.5	0.	0.	0.	0.	0.	.56

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315F2.006	.1	.0	.0	.0	.00	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.13
F315F2.007	.2	.0	.0	.0	.00	50.0	44.0	11.0	.5	0.	0.	0.	0.	0.	.17
F315F2.008	1.2	14.2	14.2	14.7	.09	50.0	22.0	11.0	3.2	0.	0.	152.	0.	0.	2.73
F315F2.009	1.4	11.0	24.6	25.0	.17	50.0	.0	11.0	3.6	0.	0.	263.	0.	0.	4.89
F315F2.010	1.2	15.8	25.1	25.2	.16	50.0	-22.0	11.0	3.2	0.	0.	268.	0.	0.	4.57
F315F2.011	1.1	17.9	17.9	19.6	.08	50.0	-44.0	11.0	2.8	0.	0.	191.	0.	0.	2.28
F315F2.012	.3	.0	24.0	.0	.02	50.0	-66.0	11.0	.7	0.	0.	256.	0.	0.	.63
F315F3.006	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.40
F315F3.007	.6	.0	21.8	.0	-.01	50.0	44.0	11.0	1.5	0.	0.	233.	0.	0.	.15
F315F3.008	1.0	13.3	13.3	17.2	.09	50.0	22.0	11.0	2.7	0.	0.	142.	0.	0.	2.78
F315F3.009	1.7	17.7	18.3	22.9	.16	50.0	.0	11.0	4.5	0.	0.	195.	0.	0.	4.60
F315F3.010	1.4	17.9	18.2	25.4	.15	50.0	-22.0	11.0	3.7	0.	0.	194.	0.	0.	4.35
F315F3.011	.9	.0	19.0	.0	.00	50.0	-44.0	11.0	2.4	0.	0.	202.	0.	0.	.85
F315F3.012	.4	.0	26.1	.0	.02	50.0	-66.0	11.0	1.1	0.	0.	279.	0.	0.	.78
F315F4.006	.1	.0	.0	.0	.02	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.50
F315F4.007	.5	.0	16.5	.0	.02	50.0	44.0	11.0	1.3	0.	0.	176.	0.	0.	.57
F315F4.008	1.1	20.9	21.9	29.7	.09	50.0	22.0	11.0	3.0	0.	0.	233.	0.	0.	2.78
F315F4.009	1.2	16.0	16.1	23.3	.17	50.0	.0	11.0	3.1	0.	0.	171.	0.	0.	4.79
F315F4.010	1.3	11.5	11.5	27.8	.13	50.0	-22.0	11.0	3.4	0.	0.	123.	0.	0.	3.79
F315F4.011	.9	.0	20.3	.0	.02	50.0	-44.0	11.0	2.5	0.	0.	216.	0.	0.	.88
F315F4.012	.3	.0	21.5	.0	.00	50.0	-66.0	11.0	.9	0.	0.	229.	0.	0.	.19
F315F5.006	.1	.0	.0	.0	.00	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.21
F315F5.007	.4	.0	4.0	.0	.01	50.0	44.0	11.0	1.1	0.	0.	43.	0.	0.	.48
F315F5.008	1.6	12.6	13.4	17.7	.07	50.0	22.0	11.0	4.1	0.	0.	143.	0.	0.	2.18
F315F5.009	1.4	17.0	22.1	26.9	.13	50.0	.0	11.0	3.7	0.	0.	236.	0.	0.	3.95
F315F5.010	1.3	17.5	19.1	20.7	.13	50.0	-22.0	11.0	3.3	0.	0.	204.	0.	0.	3.77
F315F5.011	1.2	7.5	14.8	21.9	.09	50.0	-44.0	11.0	3.3	0.	0.	158.	0.	0.	2.63
F315F5.012	.3	.0	28.5	.0	.02	50.0	-66.0	11.0	.9	0.	0.	305.	0.	0.	.72
F315G1.006	.0	.0	.0	.0	-.02	50.0	66.0	17.0	.0	0.	0.	0.	0.	0.	.01
F315G1.007	.0	.0	.0	.0	-.01	50.0	44.0	17.0	.1	0.	0.	0.	0.	0.	.07
F315G1.008	1.2	23.7	23.7	24.6	.07	50.0	22.0	17.0	3.2	0.	0.	253.	0.	0.	2.08
F315G1.009	1.6	17.9	29.2	34.1	.18	50.0	.0	17.0	4.3	0.	0.	311.	0.	0.	5.24
F315G1.010	1.3	21.4	29.1	29.1	.09	50.0	-22.0	17.0	3.3	0.	0.	311.	0.	0.	2.76
F315G1.011	.9	.0	28.5	.0	-.01	50.0	-44.0	17.0	2.5	0.	0.	305.	0.	0.	.28
F315G1.012	.1	.0	.0	.0	-.01	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.06
F315G2.006	.4	.0	51.1	.0	-.03	50.0	66.0	17.0	1.2	0.	0.	545.	0.	0.	1.26
F315G2.007	.0	.0	.0	.0	-.02	50.0	44.0	17.0	.1	0.	0.	0.	0.	0.	.02
F315G2.008	1.1	23.6	23.6	23.7	.02	50.0	22.0	17.0	2.9	0.	0.	252.	0.	0.	1.17
F315G2.009	1.1	6.6	19.7	25.3	.13	50.0	.0	17.0	3.0	0.	0.	210.	0.	0.	3.76
F315G2.010	1.3	22.7	24.2	24.3	.12	50.0	-22.0	17.0	3.5	0.	0.	259.	0.	0.	3.65
F315G2.011	1.3	14.9	14.9	15.2	.04	50.0	-44.0	17.0	3.3	0.	0.	159.	0.	0.	1.06
F315G2.012	.2	.0	34.6	.0	.02	50.0	-66.0	17.0	.6	0.	0.	369.	0.	0.	.61

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315G3.006	.5	.0	61.8	.0	.02	50.0	66.0	17.0	1.3	0.	0.	660.	0.	0.	.56
F315G3.007	.1	.0	.0	.0	-.03	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.01
F315G3.008	.9	.0	6.7	.0	.05	50.0	22.0	17.0	2.5	0.	0.	72.	0.	0.	1.47
F315G3.009	1.2	11.3	24.3	24.4	.11	50.0	.0	17.0	3.1	0.	0.	260.	0.	0.	3.35
F315G3.010	1.1	19.3	19.3	26.8	.13	50.0	-22.0	17.0	2.9	0.	0.	206.	0.	0.	3.73
F315G3.011	.9	.0	21.5	.0	.02	50.0	-44.0	17.0	2.4	0.	0.	229.	0.	0.	.76
F315G3.012	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.09
F315G4.006	.0	.0	.0	.0	-1.65	50.0	66.0	17.0	.0	0.	0.	0.	0.	0.	.00
F315G4.007	.1	.0	.0	.0	.00	50.0	44.0	17.0	.4	0.	0.	0.	0.	0.	.25
F315G4.008	1.2	15.4	29.3	29.3	.05	50.0	22.0	17.0	3.2	0.	0.	312.	0.	0.	1.60
F315G4.009	1.3	13.3	20.3	29.3	.11	50.0	.0	17.0	3.3	0.	0.	217.	0.	0.	3.37
F315G4.010	1.3	16.1	27.2	27.2	.13	50.0	-22.0	17.0	3.4	0.	0.	290.	0.	0.	3.69
F315G4.011	.9	.0	24.5	.0	.02	50.0	-44.0	17.0	2.4	0.	0.	262.	0.	0.	.76
F315G4.012	.2	.0	.0	.0	.00	50.0	-66.0	17.0	.5	0.	0.	0.	0.	0.	.12
F315G5.006	.6	.0	40.7	.0	.21	50.0	66.0	17.0	1.5	0.	0.	434.	0.	0.	5.89
F315G5.007	.3	.0	16.3	.0	.00	50.0	44.0	17.0	.9	0.	0.	174.	0.	0.	.34
F315G5.008	1.0	.0	26.6	.0	.05	50.0	22.0	17.0	2.6	0.	0.	284.	0.	0.	1.54
F315G5.009	1.2	18.7	18.7	18.8	.11	50.0	.0	17.0	3.3	0.	0.	200.	0.	0.	3.21
F315G5.010	1.4	18.4	24.4	24.5	.10	50.0	-22.0	17.0	3.7	0.	0.	260.	0.	0.	2.96
F315G5.011	1.2	16.4	16.4	16.5	.02	50.0	-44.0	17.0	3.1	0.	0.	176.	0.	0.	.71
F315G5.012	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.09
F315H1.006	.1	.0	.0	.0	.00	150.0	84.0	150.0	.2	0.	0.	0.	0.	0.	.24
F315H1.007	.1	.0	.0	.0	-.01	150.0	75.0	150.0	.3	0.	0.	0.	0.	0.	.15
F315H1.008	.0	.0	.0	.0	-.01	150.0	56.0	150.0	.1	0.	0.	0.	0.	0.	.12
F315H1.009	.1	.0	.0	.0	.00	150.0	50.0	150.0	.2	0.	0.	0.	0.	0.	.24
F315H1.010	.1	.0	.0	.0	.01	150.0	28.0	150.0	.3	0.	0.	0.	0.	0.	.35
F315H1.011	.2	.0	40.1	.0	.02	150.0	25.0	150.0	.5	0.	0.	429.	0.	0.	.81
F315H1.012	.6	.0	31.1	.0	.09	150.0	.0	150.0	1.6	0.	0.	332.	0.	0.	2.76
F315H2.006	.1	.0	.0	.0	.01	150.0	84.0	150.0	.2	0.	0.	0.	0.	0.	.33
F315H2.007	.1	.0	.0	.0	.01	150.0	75.0	150.0	.3	0.	0.	0.	0.	0.	.37
F315H2.008	.1	.0	.0	.0	.01	150.0	56.0	150.0	.3	0.	0.	0.	0.	0.	.46
F315H2.009	.2	.0	19.9	.0	.02	150.0	50.0	150.0	.6	0.	0.	213.	0.	0.	.76
F315H2.010	.6	.0	21.1	.0	.06	150.0	28.0	150.0	1.7	0.	0.	226.	0.	0.	1.74
F315H2.011	.6	.0	27.7	.0	.09	150.0	25.0	150.0	1.7	0.	0.	296.	0.	0.	2.68
F315H2.012	.6	.0	26.2	.0	.10	150.0	.0	150.0	1.6	0.	0.	279.	0.	0.	3.02
F315H3.006	.1	.0	.0	.0	.02	150.0	84.0	150.0	.3	0.	0.	0.	0.	0.	.66
F315H3.007	.1	.0	.0	.0	.01	150.0	75.0	150.0	.4	0.	0.	0.	0.	0.	.49
F315H3.008	.1	.0	.0	.0	.01	150.0	56.0	150.0	.4	0.	0.	0.	0.	0.	.46
F315H3.009	.2	.0	.0	.0	.01	150.0	50.0	150.0	.4	0.	0.	0.	0.	0.	.47
F315H3.010	.5	.0	18.1	.0	.06	150.0	28.0	150.0	1.3	0.	0.	194.	0.	0.	1.69
F315H3.011	.5	.0	18.3	.0	.08	150.0	25.0	150.0	1.4	0.	0.	195.	0.	0.	2.48
F315H3.012	.6	.0	19.2	.0	.13	150.0	.0	150.0	1.6	0.	0.	205.	0.	0.	3.78

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315H4.006	.1	.0	.0	.0	.01	150.0	84.0	150.0	.2	0.	0.	0.	0.	0.	.26
F315H4.007	.1	.0	.0	.0	-.02	150.0	75.0	150.0	.2	0.	0.	0.	0.	0.	.08
F315H4.008	.1	.0	.0	.0	.00	150.0	56.0	150.0	.2	0.	0.	0.	0.	0.	.33
F315H4.009	.1	.0	.0	.0	.03	150.0	50.0	150.0	.4	0.	0.	0.	0.	0.	.79
F315H4.010	.4	.0	24.5	.0	.01	150.0	28.0	150.0	1.0	0.	0.	262.	0.	0.	.38
F315H4.011	.5	.0	23.8	.0	.02	150.0	25.0	150.0	1.3	0.	0.	254.	0.	0.	1.11
F315H4.012	.5	.0	23.0	.0	.12	150.0	.0	150.0	1.4	0.	0.	246.	0.	0.	3.37
F315H5.006	.1	.0	.0	.0	.00	150.0	84.0	150.0	.2	0.	0.	0.	0.	0.	.13
F315H5.007	.1	.0	.0	.0	.01	150.0	75.0	150.0	.4	0.	0.	0.	0.	0.	.49
F315H5.008	.1	.0	.0	.0	.00	150.0	56.0	150.0	.3	0.	0.	0.	0.	0.	.27
F315H5.009	.2	.0	.0	.0	.05	150.0	50.0	150.0	.4	0.	0.	0.	0.	0.	1.32
F315H5.010	.5	.0	26.1	.0	.06	150.0	28.0	150.0	1.3	0.	0.	278.	0.	0.	1.83
F315H5.011	.7	.0	25.7	.0	.08	150.0	25.0	150.0	1.9	0.	0.	274.	0.	0.	2.47
F315H5.012	.6	.0	28.3	.0	.14	150.0	.0	150.0	1.7	0.	0.	302.	0.	0.	3.91
F315I1.006	.1	.0	.0	.0	-.01	150.0	84.0	750.0	.1	0.	0.	0.	0.	0.	.09
F315I1.007	.1	.0	.0	.0	.00	150.0	75.0	750.0	.3	0.	0.	0.	0.	0.	.24
F315I1.008	.2	.0	.0	.0	.03	150.0	56.0	750.0	.4	0.	0.	0.	0.	0.	.89
F315I1.009	.0	.0	.0	.0	-.04	150.0	50.0	750.0	.1	0.	0.	0.	0.	0.	.02
F315I1.010	.4	.0	17.5	.0	.01	150.0	28.0	750.0	1.0	0.	0.	187.	0.	0.	.39
F315I1.011	.6	.0	17.5	.0	.02	150.0	25.0	750.0	1.5	0.	0.	187.	0.	0.	.73
F315I1.012	.6	.0	33.4	.0	.12	150.0	.0	750.0	1.6	0.	0.	356.	0.	0.	3.36
F315I2.006	.1	.0	.0	.0	.02	150.0	84.0	750.0	.3	0.	0.	0.	0.	0.	.51
F315I2.007	.1	.0	.0	.0	-.01	150.0	75.0	750.0	.3	0.	0.	0.	0.	0.	.12
F315I2.008	.1	.0	.0	.0	.02	150.0	56.0	750.0	.3	0.	0.	0.	0.	0.	.48
F315I2.009	.2	.0	.0	.0	.01	150.0	50.0	750.0	.4	0.	0.	0.	0.	0.	.39
F315I2.010	.5	.0	23.4	.0	.04	150.0	28.0	750.0	1.3	0.	0.	250.	0.	0.	1.09
F315I2.011	.7	.0	23.9	.0	.04	150.0	25.0	750.0	1.8	0.	0.	255.	0.	0.	1.37
F315I2.012	.6	.0	24.4	.0	.09	150.0	.0	750.0	1.6	0.	0.	260.	0.	0.	2.57
F315I3.006	.0	.0	.0	.0	-.22	150.0	84.0	750.0	.1	0.	0.	0.	0.	0.	.01
F315I3.007	.1	.0	.0	.0	.00	150.0	75.0	750.0	.3	0.	0.	0.	0.	0.	.24
F315I3.008	.1	.0	.0	.0	.00	150.0	56.0	750.0	.2	0.	0.	0.	0.	0.	.15
F315I3.009	.1	.0	.0	.0	.02	150.0	50.0	750.0	.4	0.	0.	0.	0.	0.	.70
F315I3.010	.6	.0	25.9	.0	.01	150.0	28.0	750.0	1.7	0.	0.	276.	0.	0.	.67
F315I3.011	.6	.0	25.6	.0	.02	150.0	25.0	750.0	1.7	0.	0.	273.	0.	0.	1.01
F315I3.012	.7	.0	22.2	.0	.11	150.0	.0	750.0	1.8	0.	0.	237.	0.	0.	3.28
F315I4.006	2.6	1.0	29.3	61.5	-.79	150.0	84.0	750.0	6.7	303.	0.	312.	0.	342.	8.72
F315I4.007	.1	.0	.0	.0	.01	150.0	75.0	750.0	.4	0.	0.	0.	0.	0.	.42
F315I4.008	.4	.0	6.7	.0	.10	150.0	56.0	750.0	1.0	0.	0.	72.	0.	0.	2.98
F315I4.009	.3	.0	17.7	.0	.04	150.0	50.0	750.0	.9	0.	0.	189.	0.	0.	1.13
F315I4.010	.5	.0	24.8	.0	.02	150.0	28.0	750.0	1.2	0.	0.	265.	0.	0.	.69
F315I4.011	.6	.0	25.5	.0	.05	150.0	25.0	750.0	1.7	0.	0.	272.	0.	0.	1.47
F315I4.012	.6	.0	27.7	.0	.09	150.0	.0	750.0	1.7	0.	0.	296.	0.	0.	2.52

FALCON 3: LSR = 150, GAS = ARGON

	MODEL CONDITIONS								PROTOTYPE CONDITIONS						
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F3151S.006	3.7	5.0	14.0	48.2	1.06	150.0	84.0	750.0	9.4	79.	0.	149.	0.	351.	29.48
F3151S.007	.2	.0	.0	.0	.02	150.0	75.0	750.0	.5	0.	0.	0.	0.	0.	.81
F3151S.008	.1	.0	.0	.0	.01	150.0	56.0	750.0	.3	0.	0.	0.	0.	0.	.37
F3151S.009	.1	.0	.0	.0	.00	150.0	50.0	750.0	.4	0.	0.	0.	0.	0.	.29
F3151S.010	.6	.0	26.2	.0	.05	150.0	28.0	750.0	1.7	0.	0.	279.	0.	0.	1.52
F3151S.011	.7	.0	28.4	.0	.08	150.0	25.0	750.0	1.8	0.	0.	303.	0.	0.	2.31
F3151S.012	.8	.0	30.0	.0	.13	150.0	.0	750.0	2.0	0.	0.	320.	0.	0.	3.62
F315J1.006	.0	.0	.0	.0	-.17	150.0	84.0	1650.0	.1	0.	0.	0.	0.	0.	.00
F315J1.007	.0	.0	.0	.0	-.01	150.0	75.0	1650.0	.1	0.	0.	0.	0.	0.	.08
F315J1.008	.0	.0	.0	.0	-.01	150.0	56.0	1650.0	.1	0.	0.	0.	0.	0.	.12
F315J1.009	.2	.0	15.0	.0	.00	150.0	50.0	1650.0	.6	0.	0.	160.	0.	0.	.20
F315J1.010	.5	.0	26.8	.0	.02	150.0	28.0	1650.0	1.3	0.	0.	286.	0.	0.	.72
F315J1.011	.6	.0	26.8	.0	.03	150.0	25.0	1650.0	1.7	0.	0.	286.	0.	0.	1.24
F315J1.012	.6	.0	23.2	.0	.10	150.0	.0	1650.0	1.7	0.	0.	248.	0.	0.	2.81
F315J2.006	.1	.0	.0	.0	-.01	150.0	84.0	1650.0	.1	0.	0.	0.	0.	0.	.09
F315J2.007	.1	.0	.0	.0	-.01	150.0	75.0	1650.0	.2	0.	0.	0.	0.	0.	.07
F315J2.008	.1	.0	.0	.0	.00	150.0	56.0	1650.0	.2	0.	0.	0.	0.	0.	.10
F315J2.009	.0	.0	.0	.0	-.02	150.0	50.0	1650.0	.1	0.	0.	0.	0.	0.	.06
F315J2.010	.3	.0	21.7	.0	.01	150.0	28.0	1650.0	.9	0.	0.	231.	0.	0.	.42
F315J2.011	.6	.0	29.9	.0	.02	150.0	25.0	1650.0	1.7	0.	0.	319.	0.	0.	.83
F315J2.012	.6	.0	25.0	.0	.08	150.0	.0	1650.0	1.7	0.	0.	267.	0.	0.	2.46
F315J3.006	.1	.0	.0	.0	-.01	150.0	84.0	1650.0	.2	0.	0.	0.	0.	0.	.08
F315J3.007	.1	.0	.0	.0	.00	150.0	75.0	1650.0	.2	0.	0.	0.	0.	0.	.04
F315J3.008	.0	.0	.0	.0	-.01	150.0	56.0	1650.0	.1	0.	0.	0.	0.	0.	.10
F315J3.009	.0	.0	.0	.0	.00	150.0	50.0	1650.0	.0	0.	0.	0.	0.	0.	.09
F315J3.010	.4	.0	23.9	.0	.01	150.0	28.0	1650.0	1.0	0.	0.	255.	0.	0.	.32
F315J3.011	.6	.0	26.4	.0	.00	150.0	25.0	1650.0	1.5	0.	0.	282.	0.	0.	.40
F315J3.012	.8	.0	28.8	.0	.16	150.0	.0	1650.0	2.2	0.	0.	307.	0.	0.	4.69
F315J4.006	.1	.0	.0	.0	-.02	150.0	84.0	1650.0	.2	0.	0.	0.	0.	0.	.00
F315J4.007	.1	.0	.0	.0	-.01	150.0	75.0	1650.0	.2	0.	0.	0.	0.	0.	.04
F315J4.008	.0	.0	.0	.0	-.05	150.0	56.0	1650.0	.1	0.	0.	0.	0.	0.	.02
F315J4.009	.1	.0	.0	.0	-.04	150.0	50.0	1650.0	.2	0.	0.	0.	0.	0.	.01
F315J4.010	.4	.0	17.4	.0	.00	150.0	28.0	1650.0	1.0	0.	0.	186.	0.	0.	.26
F315J4.011	.5	.0	30.6	.0	.01	150.0	25.0	1650.0	1.3	0.	0.	327.	0.	0.	.50
F315J4.012	.7	.0	30.1	.0	.10	150.0	.0	1650.0	1.8	0.	0.	322.	0.	0.	2.84
F315J5.006	.1	.0	.0	.0	.00	150.0	84.0	1650.0	.1	0.	0.	0.	0.	0.	.11
F315J5.007	.0	.0	.0	.0	-.01	150.0	75.0	1650.0	.1	0.	0.	0.	0.	0.	.11
F315J5.008	.0	.0	.0	.0	-.03	150.0	56.0	1650.0	.0	0.	0.	0.	0.	0.	.01
F315J5.009	.1	.0	.0	.0	.00	150.0	50.0	1650.0	.3	0.	0.	0.	0.	0.	.20
F315J5.010	.4	.0	28.6	.0	.01	150.0	28.0	1650.0	1.2	0.	0.	305.	0.	0.	.49
F315J5.011	.5	.0	28.6	.0	.03	150.0	25.0	1650.0	1.5	0.	0.	306.	0.	0.	1.02
F315J5.012	.6	.0	25.3	.0	.08	150.0	.0	1650.0	1.6	0.	0.	270.	0.	0.	2.39

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315K1.006	.0	.0	.0	.0	.00	150.0	84.0	2550.0	.1	0.	0.	0.	0.	0.	.20
F315K1.007	.1	.0	.0	.0	.00	150.0	75.0	2550.0	.2	0.	0.	0.	0.	0.	.09
F315K1.008	.1	.0	.0	.0	.00	150.0	56.0	2550.0	.1	0.	0.	0.	0.	0.	.19
F315K1.009	.1	.0	.0	.0	.00	150.0	50.0	2550.0	.3	0.	0.	0.	0.	0.	.17
F315K1.010	.5	.0	19.2	.0	.02	150.0	28.0	2550.0	1.2	0.	0.	205.	0.	0.	.64
F315K1.011	.6	.0	19.3	.0	.02	150.0	25.0	2550.0	1.5	0.	0.	206.	0.	0.	.72
F315K1.012	.6	.0	6.5	.0	.06	150.0	.0	2550.0	1.6	0.	0.	70.	0.	0.	1.77
F315K2.006	.0	.0	.0	.0	-.01	150.0	84.0	2550.0	.1	0.	0.	0.	0.	0.	.01
F315K2.007	.1	.0	.0	.0	-.01	150.0	75.0	2550.0	.2	0.	0.	0.	0.	0.	.05
F315K2.008	.1	.0	.0	.0	.00	150.0	56.0	2550.0	.2	0.	0.	0.	0.	0.	.18
F315K2.009	.0	.0	.0	.0	.00	150.0	50.0	2550.0	.1	0.	0.	0.	0.	0.	.13
F315K2.010	.4	.0	32.7	.0	.01	150.0	28.0	2550.0	1.0	0.	0.	349.	0.	0.	.41
F315K2.011	.5	.0	29.9	.0	.02	150.0	25.0	2550.0	1.2	0.	0.	319.	0.	0.	.71
F315K2.012	.6	.0	25.1	.0	.09	150.0	.0	2550.0	1.6	0.	0.	268.	0.	0.	2.58
F315K3.006	.1	.0	.0	.0	.00	150.0	84.0	2550.0	.2	0.	0.	0.	0.	0.	.00
F315K3.007	.0	.0	.0	.0	-.02	150.0	75.0	2550.0	.0	0.	0.	0.	0.	0.	.01
F315K3.008	.1	.0	.0	.0	.00	150.0	56.0	2550.0	.2	0.	0.	0.	0.	0.	.03
F315K3.009	.1	.0	.0	.0	.00	150.0	50.0	2550.0	.2	0.	0.	0.	0.	0.	.10
F315K3.010	.4	.0	23.5	.0	.02	150.0	28.0	2550.0	1.1	0.	0.	251.	0.	0.	.74
F315K3.011	.5	.0	26.9	.0	.05	150.0	25.0	2550.0	1.3	0.	0.	288.	0.	0.	1.40
F315K3.012	.7	.0	21.8	.0	.08	150.0	.0	2550.0	1.9	0.	0.	233.	0.	0.	2.31
F315K4.006	.1	.0	.0	.0	-.01	150.0	84.0	2550.0	.1	0.	0.	0.	0.	0.	.05
F315K4.007	.1	.0	.0	.0	-.01	150.0	75.0	2550.0	.1	0.	0.	0.	0.	0.	.04
F315K4.008	.0	.0	.0	.0	-.01	150.0	56.0	2550.0	.1	0.	0.	0.	0.	0.	.02
F315K4.009	.2	.0	.0	.0	-.01	150.0	50.0	2550.0	.5	0.	0.	0.	0.	0.	.09
F315K4.010	.4	.0	35.1	.0	.02	150.0	28.0	2550.0	1.2	0.	0.	375.	0.	0.	.75
F315K4.011	.5	.0	23.1	.0	.04	150.0	25.0	2550.0	1.4	0.	0.	246.	0.	0.	1.29
F315K4.012	.7	.0	23.0	.0	.07	150.0	.0	2550.0	1.8	0.	0.	246.	0.	0.	1.96
F315K5.006	.0	.0	.0	.0	-.02	150.0	84.0	2550.0	.1	0.	0.	0.	0.	0.	.02
F315K5.007	.0	.0	.0	.0	-.01	150.0	75.0	2550.0	.1	0.	0.	0.	0.	0.	.05
F315K5.008	.4	.0	40.1	.0	.05	150.0	56.0	2550.0	1.0	0.	0.	428.	0.	0.	2.24
F315K5.009	.1	.0	.0	.0	.00	150.0	50.0	2550.0	.2	0.	0.	0.	0.	0.	.06
F315K5.010	.5	.0	24.3	.0	.01	150.0	28.0	2550.0	1.2	0.	0.	260.	0.	0.	.39
F315K5.011	.5	.0	24.4	.0	.02	150.0	25.0	2550.0	1.4	0.	0.	261.	0.	0.	.53
F315K5.012	.6	.0	22.6	.0	.07	150.0	.0	2550.0	1.7	0.	0.	241.	0.	0.	2.12
F315L1.008	.5	.0	20.5	.0	.09	150.0	-28.0	150.0	1.4	0.	0.	219.	0.	0.	2.67
F315L1.009	.2	.0	21.0	.0	.02	150.0	-50.0	150.0	.6	0.	0.	224.	0.	0.	.59
F315L1.010	.2	.0	.0	.0	.01	150.0	-56.0	150.0	.4	0.	0.	0.	0.	0.	.35
F315L1.011	.1	.0	.0	.0	.01	150.0	-75.0	150.0	.3	0.	0.	0.	0.	0.	.36
F315L1.012	.1	.0	.0	.0	.01	150.0	-84.0	150.0	.2	0.	0.	0.	0.	0.	.36
F315L2.006	.6	.0	21.8	.0	.10	150.0	.0	150.0	1.5	0.	0.	232.	0.	0.	2.93
F315L2.007	.6	.0	24.2	.0	.09	150.0	-25.0	150.0	1.5	0.	0.	258.	0.	0.	2.60

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315L2.008	.5	.0	24.5	.0	.08	150.0	-28.0	150.0	1.4	0.	0.	262.	0.	0.	2.41
F315L2.009	.4	.0	25.3	.0	.04	150.0	-50.0	150.0	1.0	0.	0.	270.	0.	0.	1.04
F315L2.010	.2	.0	24.5	.0	.03	150.0	-56.0	150.0	.6	0.	0.	262.	0.	0.	.80
F315L2.011	.1	.0	.0	.0	.01	150.0	-75.0	150.0	.3	0.	0.	0.	0.	0.	.44
F315L2.012	.0	.0	.0	.0	-.02	150.0	-84.0	150.0	.1	0.	0.	0.	0.	0.	.02
F315L3.006	.8	.0	23.9	.0	.11	150.0	.0	150.0	2.0	0.	0.	255.	0.	0.	3.12
F315L3.007	.7	.0	23.1	.0	.08	150.0	-25.0	150.0	1.8	0.	0.	247.	0.	0.	2.51
F315L3.008	.6	.0	23.7	.0	.08	150.0	-28.0	150.0	1.7	0.	0.	253.	0.	0.	2.37
F315L3.009	.6	.0	24.1	.0	.04	150.0	-50.0	150.0	1.5	0.	0.	258.	0.	0.	1.22
F315L3.010	.5	.0	23.7	.0	.04	150.0	-56.0	150.0	1.4	0.	0.	253.	0.	0.	1.09
F315L3.011	.1	.0	.0	.0	.02	150.0	-75.0	150.0	.3	0.	0.	0.	0.	0.	.49
F315L3.012	.1	.0	.0	.0	.01	150.0	-84.0	150.0	.2	0.	0.	0.	0.	0.	.40
F315L4.006	.6	.0	23.9	.0	.09	150.0	.0	150.0	1.6	0.	0.	255.	0.	0.	2.81
F315L4.007	.7	.0	24.3	.0	.13	150.0	-25.0	150.0	1.8	0.	0.	259.	0.	0.	3.65
F315L4.008	.6	.0	24.1	.0	.11	150.0	-28.0	150.0	1.7	0.	0.	257.	0.	0.	3.31
F315L4.009	.4	.0	22.0	.0	.07	150.0	-50.0	150.0	1.2	0.	0.	235.	0.	0.	1.92
F315L4.010	.4	.0	26.1	.0	.03	150.0	-56.0	150.0	1.2	0.	0.	279.	0.	0.	.93
F315L4.011	.1	.0	.0	.0	-.03	150.0	-75.0	150.0	.2	0.	0.	0.	0.	0.	.08
F315L4.012	.1	.0	.0	.0	-.02	150.0	-84.0	150.0	.2	0.	0.	0.	0.	0.	.11
F315L5.006	.7	.0	25.7	.0	.08	150.0	.0	150.0	1.8	0.	0.	274.	0.	0.	2.58
F315L5.007	.6	.0	25.4	.0	.11	150.0	-25.0	150.0	1.7	0.	0.	271.	0.	0.	3.39
F315L5.008	.6	.0	25.7	.0	.09	150.0	-28.0	150.0	1.7	0.	0.	274.	0.	0.	2.72
F315L5.009	.5	.0	27.2	.0	.07	150.0	-50.0	150.0	1.4	0.	0.	290.	0.	0.	2.02
F315L5.010	.5	.0	28.0	.0	.05	150.0	-56.0	150.0	1.4	0.	0.	299.	0.	0.	1.56
F315L5.011	.2	.0	.0	.0	-.01	150.0	-75.0	150.0	.4	0.	0.	0.	0.	0.	.16
F315L5.012	.1	.0	.0	.0	.02	150.0	-84.0	150.0	.2	0.	0.	0.	0.	0.	.45
F315M1.006	.6	.0	23.5	.0	.12	150.0	.0	750.0	1.7	0.	0.	251.	0.	0.	3.38
F315M1.007	.6	.0	16.2	.0	.10	150.0	-25.0	750.0	1.7	0.	0.	173.	0.	0.	2.96
F315M1.008	.7	.0	25.1	.0	.10	150.0	-28.0	750.0	1.8	0.	0.	268.	0.	0.	2.93
F315M1.009	.3	.0	24.8	.0	.00	150.0	-50.0	750.0	.9	0.	0.	265.	0.	0.	.27
F315M1.010	.3	.0	32.5	.0	-.01	150.0	-56.0	750.0	.9	0.	0.	347.	0.	0.	.17
F315M1.011	.0	.0	.0	.0	-.05	150.0	-75.0	750.0	.1	0.	0.	0.	0.	0.	.01
F315M1.012	.1	.0	.0	.0	-.02	150.0	-84.0	750.0	.1	0.	0.	0.	0.	0.	.06
F315M2.006	.7	.0	21.5	.0	.11	150.0	.0	750.0	1.9	0.	0.	230.	0.	0.	3.12
F315M2.007	.7	.0	17.3	.0	.08	150.0	-25.0	750.0	1.8	0.	0.	185.	0.	0.	2.42
F315M2.008	.6	.0	19.9	.0	.08	150.0	-28.0	750.0	1.5	0.	0.	212.	0.	0.	2.27
F315M2.009	.5	.0	22.0	.0	.01	150.0	-50.0	750.0	1.4	0.	0.	234.	0.	0.	.65
F315M2.010	.4	.0	22.3	.0	.01	150.0	-56.0	750.0	1.1	0.	0.	238.	0.	0.	.55
F315M2.011	.2	.0	26.2	.0	-.01	150.0	-75.0	750.0	.6	0.	0.	279.	0.	0.	.08
F315M2.012	.1	.0	.0	.0	-.01	150.0	-84.0	750.0	.1	0.	0.	0.	0.	0.	.03
F315M3.006	.7	.0	19.8	.0	.10	150.0	.0	750.0	1.8	0.	0.	211.	0.	0.	3.04
F315M3.007	.8	.0	22.1	.0	.10	150.0	-25.0	750.0	2.2	0.	0.	236.	0.	0.	2.94

FALCON 3: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315M3.008	.8	.0	22.3	.0	.08	150.0	-28.0	750.0	2.1	0.	0.	238.	0.	0.	2.24
F315M3.009	.5	.0	20.0	.0	.03	150.0	-50.0	750.0	1.5	0.	0.	213.	0.	0.	.90
F315M3.010	.5	.0	20.2	.0	.02	150.0	-56.0	750.0	1.3	0.	0.	216.	0.	0.	.55
F315M3.011	.2	.0	.0	.0	.03	150.0	-75.0	750.0	.5	0.	0.	0.	0.	0.	.75
F315M3.012	.1	.0	.0	.0	.01	150.0	-84.0	750.0	.2	0.	0.	0.	0.	0.	.32
F315M4.006	.7	.0	21.2	.0	.14	150.0	.0	750.0	1.8	0.	0.	226.	0.	0.	4.05
F315M4.007	.6	.0	23.0	.0	.07	150.0	-25.0	750.0	1.6	0.	0.	245.	0.	0.	2.01
F315M4.008	.6	.0	21.8	.0	.06	150.0	-28.0	750.0	1.7	0.	0.	233.	0.	0.	1.69
F315M4.009	.4	.0	22.0	.0	.03	150.0	-50.0	750.0	.9	0.	0.	235.	0.	0.	.96
F315M4.010	.3	.0	16.9	.0	.01	150.0	-56.0	750.0	.8	0.	0.	181.	0.	0.	.22
F315M4.011	.1	.0	.0	.0	.01	150.0	-75.0	750.0	.4	0.	0.	0.	0.	0.	.39
F315M4.012	.1	.0	.0	.0	.01	150.0	-84.0	750.0	.3	0.	0.	0.	0.	0.	.38
F315M5.006	.6	.0	21.3	.0	.11	150.0	.0	750.0	1.6	0.	0.	228.	0.	0.	3.22
F315M5.007	.6	.0	21.5	.0	.08	150.0	-25.0	750.0	1.7	0.	0.	230.	0.	0.	2.39
F315M5.008	.7	.0	25.0	.0	.08	150.0	-28.0	750.0	1.8	0.	0.	267.	0.	0.	2.38
F315M5.009	.4	.0	24.2	.0	.02	150.0	-50.0	750.0	1.2	0.	0.	258.	0.	0.	.77
F315M5.010	.3	.0	23.2	.0	.01	150.0	-56.0	750.0	.7	0.	0.	248.	0.	0.	.38
F315M5.011	.1	.0	.0	.0	-.03	150.0	-75.0	750.0	.3	0.	0.	0.	0.	0.	.02
F315M5.012	.1	.0	.0	.0	-.01	150.0	-84.0	750.0	.1	0.	0.	0.	0.	0.	.10
F315N1.006	.9	.0	18.5	.0	.09	150.0	.0	1650.0	2.4	0.	0.	198.	0.	0.	2.70
F315N1.007	.6	.0	23.8	.0	.06	150.0	-25.0	1650.0	1.6	0.	0.	255.	0.	0.	1.92
F315N1.008	.6	.0	20.6	.0	.08	150.0	-28.0	1650.0	1.7	0.	0.	219.	0.	0.	2.23
F315N1.009	.4	.0	19.1	.0	.04	150.0	-50.0	1650.0	1.2	0.	0.	204.	0.	0.	1.02
F315N1.010	.4	.0	19.4	.0	.02	150.0	-56.0	1650.0	1.1	0.	0.	208.	0.	0.	.61
F315N1.011	.2	.0	22.4	.0	.02	150.0	-75.0	1650.0	.6	0.	0.	239.	0.	0.	.70
F315N1.012	.1	.0	.0	.0	.00	150.0	-84.0	1650.0	.3	0.	0.	0.	0.	0.	.20
F315N2.006	.9	.0	25.6	.0	.13	150.0	.0	1650.0	2.4	0.	0.	273.	0.	0.	3.85
F315N2.007	.6	.0	22.0	.0	.06	150.0	-25.0	1650.0	1.7	0.	0.	235.	0.	0.	1.68
F315N2.008	.5	.0	21.2	.0	.05	150.0	-28.0	1650.0	1.4	0.	0.	227.	0.	0.	1.47
F315N2.009	.5	.0	25.2	.0	.02	150.0	-50.0	1650.0	1.3	0.	0.	269.	0.	0.	.67
F315N2.010	.5	.0	33.3	.0	.01	150.0	-56.0	1650.0	1.3	0.	0.	356.	0.	0.	.43
F315N2.011	.5	.0	33.2	.0	.01	150.0	-75.0	1650.0	1.3	0.	0.	354.	0.	0.	.38
F315N2.012	.2	.0	.0	.0	.00	150.0	-84.0	1650.0	.5	0.	0.	0.	0.	0.	.15
F315N3.006	.7	.0	20.6	.0	.10	150.0	.0	1650.0	1.9	0.	0.	220.	0.	0.	2.87
F315N3.007	.6	.0	26.1	.0	.05	150.0	-25.0	1650.0	1.7	0.	0.	279.	0.	0.	1.64
F315N3.008	.6	.0	25.9	.0	.05	150.0	-28.0	1650.0	1.6	0.	0.	276.	0.	0.	1.50
F315N3.009	.3	.0	15.7	.0	.01	150.0	-50.0	1650.0	.9	0.	0.	167.	0.	0.	.45
F315N3.010	.2	.0	.0	.0	.00	150.0	-56.0	1650.0	.5	0.	0.	0.	0.	0.	.15
F315N3.011	.1	.0	.0	.0	-.02	150.0	-75.0	1650.0	.3	0.	0.	0.	0.	0.	.08
F315N3.012	.1	.0	.0	.0	-.01	150.0	-84.0	1650.0	.2	0.	0.	0.	0.	0.	.03
F315N4.006	.7	.0	20.7	.0	.07	150.0	.0	1650.0	1.8	0.	0.	221.	0.	0.	2.15
F315N4.007	.6	.0	19.1	.0	.05	150.0	-25.0	1650.0	1.6	0.	0.	204.	0.	0.	1.77

FALCON 3: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F315N4.008	.7	.0	23.9	.0	.04	150.0	-28.0	1650.0	1.8	0.	0.	255.	0.	0.	1.46
F315N4.009	.7	.0	24.7	.0	.03	150.0	-50.0	1650.0	1.8	0.	0.	263.	0.	0.	.87
F315N4.010	.7	.0	22.3	.0	.04	150.0	-56.0	1650.0	1.8	0.	0.	238.	0.	0.	1.04
F315N4.011	.4	.0	22.9	.0	.03	150.0	-75.0	1650.0	1.1	0.	0.	244.	0.	0.	.96
F315N4.012	.4	.0	23.0	.0	.02	150.0	-84.0	1650.0	1.0	0.	0.	245.	0.	0.	.54
F315N5.006	.7	.0	21.7	.0	.11	150.0	.0	1650.0	1.9	0.	0.	232.	0.	0.	3.17
F315N5.007	.6	.0	22.0	.0	.06	150.0	-25.0	1650.0	1.7	0.	0.	235.	0.	0.	1.92
F315N5.008	.6	.0	23.1	.0	.06	150.0	-28.0	1650.0	1.7	0.	0.	247.	0.	0.	1.85
F315N5.009	.4	.0	20.2	.0	.02	150.0	-50.0	1650.0	1.1	0.	0.	216.	0.	0.	.65
F315N5.010	.4	.0	20.1	.0	.01	150.0	-56.0	1650.0	.9	0.	0.	215.	0.	0.	.31
F315N5.011	.2	.0	27.3	.0	-.01	150.0	-75.0	1650.0	.6	0.	0.	291.	0.	0.	.17
F315N5.012	.1	.0	.0	.0	-.01	150.0	-84.0	1650.0	.1	0.	0.	0.	0.	0.	.08
F31501.006	.5	.0	30.1	.0	.04	150.0	.0	2550.0	1.4	0.	0.	321.	0.	0.	1.41
F31501.007	.6	.0	21.0	.0	.04	150.0	-25.0	2550.0	1.5	0.	0.	224.	0.	0.	1.39
F31501.008	.6	.0	27.2	.0	.03	150.0	-28.0	2550.0	1.5	0.	0.	290.	0.	0.	1.13
F31501.009	.5	.0	29.4	.0	.05	150.0	-50.0	2550.0	1.4	0.	0.	314.	0.	0.	1.38
F31501.010	.5	.0	20.0	.0	.03	150.0	-56.0	2550.0	1.3	0.	0.	213.	0.	0.	.95
F31501.011	.2	.0	.0	.0	.00	150.0	-75.0	2550.0	.4	0.	0.	0.	0.	0.	.24
F31501.012	.2	.0	14.4	.0	.01	150.0	-84.0	2550.0	.6	0.	0.	153.	0.	0.	.43
F31502.006	.6	.0	18.9	.0	.04	150.0	.0	2550.0	1.6	0.	0.	202.	0.	0.	1.44
F31502.007	.7	.0	15.6	.0	.03	150.0	-25.0	2550.0	1.8	0.	0.	166.	0.	0.	1.34
F31502.008	.6	.0	15.0	.0	.03	150.0	-28.0	2550.0	1.7	0.	0.	160.	0.	0.	1.21
F31502.009	.6	.0	21.7	.0	.05	150.0	-50.0	2550.0	1.7	0.	0.	232.	0.	0.	1.44
F31502.010	.4	.0	17.7	.0	.04	150.0	-56.0	2550.0	1.2	0.	0.	189.	0.	0.	1.05
F31502.011	.3	.0	26.2	.0	.02	150.0	-75.0	2550.0	.8	0.	0.	280.	0.	0.	.56
F31502.012	.1	.0	.0	.0	.00	150.0	-84.0	2550.0	.4	0.	0.	0.	0.	0.	.26
F31503.006	.7	.0	24.9	.0	.05	150.0	.0	2550.0	1.9	0.	0.	266.	0.	0.	1.59
F31503.007	.8	.0	20.4	.0	.04	150.0	-25.0	2550.0	2.0	0.	0.	218.	0.	0.	1.37
F31503.008	.7	.0	20.4	.0	.04	150.0	-28.0	2550.0	2.0	0.	0.	218.	0.	0.	1.28
F31503.009	.5	.0	20.7	.0	.03	150.0	-50.0	2550.0	1.3	0.	0.	221.	0.	0.	.98
F31503.010	.5	.0	17.7	.0	.04	150.0	-56.0	2550.0	1.4	0.	0.	189.	0.	0.	1.15
F31503.011	.3	.0	22.7	.0	.04	150.0	-75.0	2550.0	.9	0.	0.	242.	0.	0.	1.02
F31503.012	.2	.0	.0	.0	.02	150.0	-84.0	2550.0	.4	0.	0.	0.	0.	0.	.46
F31504.006	.8	.0	23.2	.0	.08	150.0	.0	2550.0	2.0	0.	0.	247.	0.	0.	2.48
F31504.007	.9	.0	27.0	.0	.06	150.0	-25.0	2550.0	2.5	0.	0.	288.	0.	0.	1.92
F31504.008	.7	.0	16.8	.0	.05	150.0	-28.0	2550.0	1.8	0.	0.	180.	0.	0.	1.45
F31504.009	.4	.0	20.9	.0	.01	150.0	-50.0	2550.0	1.0	0.	0.	223.	0.	0.	.55
F31504.010	.3	.0	23.2	.0	.01	150.0	-56.0	2550.0	.8	0.	0.	248.	0.	0.	.27
F31504.011	.1	.0	.0	.0	.00	150.0	-75.0	2550.0	.3	0.	0.	0.	0.	0.	.08
F31504.012	.0	.0	.0	.0	.00	150.0	-84.0	2550.0	.1	0.	0.	0.	0.	0.	.10
F31505.006	.8	.0	24.0	.0	.09	150.0	.0	2550.0	2.2	0.	0.	256.	0.	0.	2.74
F31505.007	.6	.0	16.1	.0	.08	150.0	-25.0	2550.0	1.6	0.	0.	172.	0.	0.	2.27

FALCON 3: LSR = 150, GAS = ARGON

MODEL CONDITIONS									PROTOTYPE CONDITIONS						
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F31505.008	.6	.0	19.5	.0	.08	150.0	-28.0	2550.0	1.6	0.	0.	208.	0.	0.	2.26
F31505.009	.5	.0	27.7	.0	.03	150.0	-50.0	2550.0	1.4	0.	0.	296.	0.	0.	.82
F31505.010	.4	.0	28.6	.0	.01	150.0	-56.0	2550.0	1.1	0.	0.	305.	0.	0.	.43
F31505.011	.1	.0	.0	.0	-.02	150.0	-75.0	2550.0	.4	0.	0.	0.	0.	0.	.09
F31505.012	.1	.0	.0	.0	.01	150.0	-84.0	2550.0	.3	0.	0.	0.	0.	0.	.35

FALCON 3: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)	
N320A1.009	1.5	19.9	19.9	20.0	.01	-62.0	30.0	2.0	3.9	0.	0.	246.	0.	0.	.54	
N320A1.008	22.8	2.6	14.1	54.8	2.95	-62.0	20.0	2.0	44.4	32.	57.	173.	329.	599.	81.05	
N320A1.007	22.4	1.8	14.3	47.7	2.77	-62.0	10.0	2.0	43.9	27.	35.	176.	352.	587.	79.08	
N320A1.006	23.0	2.0	13.2	44.2	3.48	-62.0	.0	2.0	44.6	25.	26.	163.	371.	455.	95.33	
N320A1.005	23.6	3.6	11.7	35.6	2.69	-62.0	-20.0	2.0	45.5	46.	53.	145.	326.	371.	74.29	
N320A1.004	2.3	9.2	17.3	26.2	.08	-62.0	-30.0	2.0	5.9	144.	0.	213.	0.	219.	2.59	
N320A2.009	1.6	11.1	17.2	17.2	.01	-62.0	30.0	2.0	4.3	0.	0.	212.	0.	0.	.74	
N320A2.008	26.5	2.3	13.9	60.2	3.45	-62.0	20.0	2.0	49.3	34.	35.	171.	348.	737.	92.51	
N320A2.007	23.5	1.9	11.9	61.5	3.59	-62.0	10.0	2.0	45.4	24.	27.	147.	458.	753.	99.14	
N320A2.006	24.8	1.1	13.8	54.2	3.96	-62.0	.0	2.0	47.2	19.	21.	170.	356.	507.	106.10	
N320A2.005	26.8	1.2	14.1	33.6	2.85	-62.0	-20.0	2.0	49.7	20.	29.	173.	317.	356.	76.92	
N320A2.004	2.0	11.7	22.4	22.6	.08	-62.0	-30.0	2.0	5.2	276.	0.	276.	0.	276.	2.67	
N320A3.009	2.6	9.7	14.8	20.3	.07	-62.0	30.0	2.0	6.8	182.	0.	183.	0.	183.	2.45	
N320A3.008	25.2	1.1	13.5	61.5	3.32	-62.0	20.0	2.0	47.6	30.	32.	167.	390.	557.	90.51	
N320A3.007	23.1	1.0	15.1	59.8	3.64	-62.0	10.0	2.0	44.8	14.	34.	186.	483.	729.	100.31	
N320A3.006	24.8	.7	13.2	60.3	4.19	-62.0	.0	2.0	47.2	12.	23.	163.	459.	583.	113.11	
N320A3.005	24.8	2.4	13.9	36.2	2.70	-62.0	-20.0	2.0	47.1	31.	36.	171.	354.	384.	74.38	
N320A3.004	2.0	12.5	23.3	23.4	.08	-62.0	-30.0	2.0	5.2	287.	0.	287.	0.	288.	2.65	
N320A4.009	2.5	14.8	16.9	30.6	.01	-62.0	30.0	2.0	6.6	197.	0.	208.	0.	208.	1.16	
N320A4.008	28.0	1.1	13.0	90.0	4.12	-62.0	20.0	2.0	51.2	37.	41.	160.	429.	899.	109.20	
N320A4.007	25.0	1.8	11.5	81.4	3.81	-62.0	10.0	2.0	47.4	23.	29.	141.	464.	780.	107.14	
N320A4.006	25.8	1.0	13.4	88.3	4.71	-62.0	.0	2.0	48.4	13.	23.	165.	436.	578.	127.31	
N320A4.005	26.9	1.2	13.4	38.5	3.55	-62.0	-20.0	2.0	49.8	20.	23.	166.	358.	410.	95.90	
N320A4.004	3.3	7.3	17.6	25.1	.05	-62.0	-30.0	2.0	8.4	172.	0.	217.	0.	218.	2.62	
N320A5.009	2.0	7.1	7.1	16.8	.03	-62.0	30.0	2.0	5.2	88.	0.	88.	0.	88.	1.57	
N320A5.008	27.3	.2	13.1	90.7	3.94	-62.0	20.0	2.0	50.3	17.	27.	161.	374.	973.	105.21	
N320A5.007	25.2	.8	14.1	91.6	4.24	-62.0	10.0	2.0	47.6	15.	29.	174.	434.	958.	116.76	
N320A5.006	26.1	.6	12.0	91.1	4.72	-62.0	.0	2.0	48.8	10.	18.	147.	432.	682.	127.19	
N320A5.005	30.8	1.7	14.2	42.8	3.62	-62.0	-20.0	2.0	54.6	22.	40.	174.	339.	493.	96.21	
N320A5.004	2.8	10.7	14.2	15.3	.04	-62.0	-30.0	2.0	7.3	174.	0.	174.	0.	175.	2.20	
N320B1.009	1.4	13.9	24.5	28.4	.10	-32.0	30.0	1.0	200.0	3.6	0.	0.	302.	0.	0.	3.54
N320B1.008	36.1	.7	13.0	117.0	4.66	-32.0	20.0	1.0	60.4	9.	18.	160.	368.	888.	120.74	
N320B1.007	36.6	.1	13.2	102.6	4.56	-32.0	10.0	1.0	61.0	2.	2.	163.	314.	589.	116.07	
N320B1.006	32.9	.1	13.4	61.9	4.86	-32.0	.0	1.0	57.0	1.	2.	165.	325.	502.	123.30	
N320B1.005	24.5	.1	12.3	80.4	2.49	-32.0	-20.0	1.0	46.7	1.	3.	151.	290.	341.	69.07	
N320B1.004	1.5	13.3	13.4	18.6	.05	-32.0	-30.0	1.0	3.9	0.	0.	165.	0.	0.	1.94	
N320B2.009	1.9	10.5	13.6	28.7	.12	-32.0	30.0	1.0	4.8	0.	0.	167.	0.	0.	4.14	
N320B2.008	33.4	.5	13.8	100.6	4.35	-32.0	20.0	1.0	57.6	6.	25.	171.	382.	883.	114.49	
N320B2.007	36.6	.1	13.0	82.5	3.90	-32.0	10.0	1.0	60.9	2.	2.	161.	350.	426.	99.72	
N320B2.006	37.3	.1	12.0	45.5	4.13	-32.0	.0	1.0	61.7	1.	1.	147.	344.	483.	104.96	
N320B2.005	28.8	.1	12.8	118.5	2.86	-32.0	-20.0	1.0	52.3	1.	1.	158.	239.	384.	78.82	
N320B2.004	2.1	12.0	17.9	19.0	.09	-32.0	-30.0	1.0	5.5	208.	0.	220.	0.	221.	3.27	

FALCON 3: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N320B3.009	3.2	10.4	14.8	31.0	.11	-32.0	30.0	1.0	8.2	182.	0.	182.	0.	183.	4.13
N320B3.008	35.6	.4	11.8	99.5	4.23	-32.0	20.0	1.0	59.9	9.	16.	145.	364.	985.	111.52
N320B3.007	34.7	.1	12.4	80.1	3.77	-32.0	10.0	1.0	59.0	2.	2.	153.	384.	516.	96.92
N320B3.006	38.3	.1	11.3	58.0	4.58	-32.0	.0	1.0	62.7	1.	1.	140.	351.	454.	116.77
N320B3.005	23.4	.1	13.6	89.0	2.74	-32.0	-20.0	1.0	45.2	1.	3.	168.	263.	323.	78.62
N320B3.004	2.0	14.1	14.1	21.4	.07	-32.0	-30.0	1.0	5.1	174.	0.	174.	0.	174.	2.64
N320B4.009	1.9	12.5	21.8	23.5	.06	-32.0	30.0	1.0	5.0	0.	0.	269.	0.	0.	3.26
N320B4.008	33.1	.3	12.6	120.2	4.09	-32.0	20.0	1.0	57.2	3.	20.	155.	316.	705.	107.88
N320B4.007	35.6	.1	10.6	118.0	3.93	-32.0	10.0	1.0	59.9	2.	2.	130.	409.	516.	101.34
N320B4.006	35.7	.1	11.7	60.4	4.77	-32.0	.0	1.0	60.0	1.	1.	144.	312.	522.	118.72
N320B4.005	26.0	.1	14.0	58.2	2.86	-32.0	-20.0	1.0	48.7	1.	3.	173.	282.	371.	78.99
N320B4.004	1.0	.0	23.5	.0	.05	-32.0	-30.0	1.0	2.6	0.	0.	289.	0.	0.	2.24
N320B5.009	1.9	9.5	17.0	25.2	.08	-32.0	30.0	1.0	4.9	0.	0.	209.	0.	0.	3.49
N320B5.008	33.0	.3	13.6	79.8	4.34	-32.0	20.0	1.0	57.2	6.	15.	167.	359.	938.	113.67
N320B5.007	37.1	.1	12.7	102.8	4.32	-32.0	10.0	1.0	61.5	2.	2.	157.	307.	745.	109.08
N320B5.006	39.6	.1	13.4	68.3	4.50	-32.0	.0	1.0	63.9	1.	1.	165.	350.	425.	113.51
N320B5.005	28.5	.1	11.1	68.4	2.67	-32.0	-20.0	1.0	51.8	1.	1.	137.	252.	519.	73.55
N320B5.004	1.4	7.9	18.8	20.1	.01	-32.0	-30.0	1.0	3.6	0.	0.	232.	0.	0.	2.36
N320C1.009	1.9	14.2	19.5	25.9	.14	-2.0	30.0	1.0	5.0	0.	0.	240.	0.	0.	4.93
N320C1.008	19.8	2.8	15.1	79.5	1.81	-2.0	20.0	1.0	40.0	35.	37.	186.	323.	449.	54.82
N320C1.007	17.0	2.3	14.7	49.7	1.41	-2.0	10.0	1.0	35.7	35.	48.	182.	304.	474.	43.06
N320C1.006	13.6	.2	12.1	43.3	1.20	-2.0	.0	1.0	29.9	3.	34.	149.	263.	429.	41.02
N320C1.005	14.8	.1	12.2	108.2	1.61	-2.0	-20.0	1.0	31.9	11.	22.	150.	316.	443.	49.36
N320C1.004	1.8	10.7	20.8	21.6	.09	-2.0	-30.0	1.0	4.8	0.	0.	257.	0.	0.	3.43
N320C2.009	1.6	13.7	17.9	24.7	.14	-2.0	30.0	1.0	4.2	0.	0.	221.	0.	0.	5.07
N320C2.008	16.4	1.3	12.6	113.9	2.10	-2.0	20.0	1.0	34.7	36.	38.	155.	362.	460.	64.49
N320C2.007	19.2	1.9	14.8	62.3	1.91	-2.0	10.0	1.0	39.1	50.	51.	182.	295.	633.	55.75
N320C2.006	21.7	.2	13.4	107.7	1.87	-2.0	.0	1.0	42.9	2.	3.	166.	294.	466.	55.14
N320C2.005	24.9	.1	11.3	94.2	2.35	-2.0	-20.0	1.0	47.3	1.	39.	139.	317.	415.	67.30
N320C2.004	1.5	13.8	16.6	40.1	.07	-2.0	-30.0	1.0	3.9	0.	0.	204.	0.	0.	2.96
N320C3.009	1.9	2.3	18.5	25.8	.19	-2.0	30.0	1.0	5.0	227.	0.	227.	0.	228.	6.20
N320C3.008	11.8	2.2	15.1	91.9	2.13	-2.0	20.0	1.0	26.6	37.	43.	186.	300.	558.	66.67
N320C3.007	16.9	1.4	14.1	115.2	2.03	-2.0	10.0	1.0	35.4	17.	43.	174.	301.	758.	60.86
N320C3.006	22.5	.1	13.7	80.5	1.75	-2.0	.0	1.0	43.9	2.	3.	169.	336.	498.	52.84
N320C3.005	14.6	.1	12.2	65.3	1.43	-2.0	-20.0	1.0	31.5	1.	16.	150.	405.	429.	45.42
N320C3.004	1.5	22.1	22.1	22.9	.10	-2.0	-30.0	1.0	3.9	0.	0.	272.	0.	0.	3.34
N320C4.009	1.7	11.4	21.5	22.5	.14	-2.0	30.0	1.0	4.6	0.	0.	265.	0.	0.	5.17
N320C4.008	19.2	4.5	14.8	60.1	1.49	-2.0	20.0	1.0	39.1	74.	87.	182.	304.	441.	50.42
N320C4.007	19.0	.9	14.1	118.2	2.02	-2.0	10.0	1.0	38.8	14.	61.	174.	302.	784.	61.00
N320C4.006	20.9	.2	13.8	89.5	2.52	-2.0	.0	1.0	41.7	2.	3.	170.	352.	653.	73.46
N320C4.005	26.7	.1	13.4	56.2	2.65	-2.0	-20.0	1.0	49.6	1.	30.	165.	293.	569.	77.82
N320C4.004	2.7	13.1	13.3	26.1	.09	-2.0	-30.0	1.0	7.1	164.	0.	164.	0.	165.	3.37

FALCON 3: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N320C5.009	1.7	9.4	12.8	32.2	.19	-2.0	30.0	1.0	4.6	0.	0.	157.	0.	0.	6.36
N320C5.008	16.3	3.2	12.5	120.5	2.02	-2.0	20.0	1.0	34.4	43.	95.	154.	293.	670.	61.66
N320C5.007	18.9	2.6	13.3	119.1	1.84	-2.0	10.0	1.0	38.7	40.	76.	164.	484.	660.	55.66
N320C5.006	20.7	.1	13.4	109.0	1.82	-2.0	.0	1.0	41.4	2.	3.	165.	335.	497.	55.16
N320C5.005	22.0	.1	14.3	111.4	2.12	-2.0	-20.0	1.0	43.3	1.	9.	177.	308.	516.	62.56
N320C5.004	1.8	14.3	14.4	14.5	.11	-2.0	-30.0	1.0	4.8	0.	0.	177.	0.	0.	3.86
F320D1.006	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.21
F320D1.007	.4	.0	25.5	.0	.04	50.0	44.0	1.0	1.0	0.	0.	315.	0.	0.	1.34
F320D1.008	1.4	14.2	15.8	15.9	.06	50.0	22.0	1.0	3.7	0.	0.	195.	0.	0.	2.11
F320D1.009	1.1	15.4	15.4	15.4	.18	50.0	.0	1.0	2.8	0.	0.	190.	0.	0.	5.96
F320D1.010	1.2	16.6	16.7	22.4	.20	50.0	-22.0	1.0	3.1	0.	0.	205.	0.	0.	6.57
F320D1.011	1.2	21.5	21.6	25.7	.12	50.0	-44.0	1.0	3.2	0.	0.	267.	0.	0.	4.05
F320D1.012	.7	.0	18.0	.0	.02	50.0	-66.0	1.0	1.8	0.	0.	221.	0.	0.	.91
F320D2.006	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.31
F320D2.007	.2	.0	.0	.0	.00	50.0	44.0	1.0	.5	0.	0.	0.	0.	0.	.37
F320D2.008	.9	.0	14.5	.0	.04	50.0	22.0	1.0	2.5	0.	0.	178.	0.	0.	1.55
F320D2.009	1.1	20.1	20.1	22.2	.16	50.0	.0	1.0	3.0	0.	0.	248.	0.	0.	5.39
F320D2.010	1.3	16.3	18.8	24.3	.20	50.0	-22.0	1.0	3.5	0.	0.	232.	0.	0.	6.77
F320D2.011	1.9	14.6	15.9	24.3	.19	50.0	-44.0	1.0	4.9	0.	0.	196.	0.	0.	6.15
F320D2.012	.9	.0	23.2	.0	.08	50.0	-66.0	1.0	2.4	0.	0.	286.	0.	0.	2.66
F320D3.006	.0	.0	.0	.0	-.05	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.03
F320D3.007	.2	.0	9.7	.0	.02	50.0	44.0	1.0	.6	0.	0.	120.	0.	0.	.91
F320D3.008	1.3	14.5	14.6	20.2	.08	50.0	22.0	1.0	3.5	0.	0.	179.	0.	0.	2.87
F320D3.009	1.1	22.8	24.6	26.3	.19	50.0	.0	1.0	2.9	0.	0.	303.	0.	0.	6.23
F320D3.010	1.7	13.9	17.2	27.3	.23	50.0	-22.0	1.0	4.4	0.	0.	212.	0.	0.	7.48
F320D3.011	1.5	9.7	16.9	24.3	.18	50.0	-44.0	1.0	3.9	0.	0.	209.	0.	0.	6.04
F320D3.012	.9	.0	20.0	.0	.12	50.0	-66.0	1.0	2.4	0.	0.	247.	0.	0.	4.18
F320D4.006	.2	.0	.0	.0	.01	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.47
F320D4.007	.2	.0	.0	.0	.01	50.0	44.0	1.0	.4	0.	0.	0.	0.	0.	.51
F320D4.008	1.0	14.9	14.9	14.9	.05	50.0	22.0	1.0	2.8	0.	0.	184.	0.	0.	2.03
F320D4.009	1.0	.0	13.8	.0	.15	50.0	.0	1.0	2.6	0.	0.	170.	0.	0.	5.39
F320D4.010	1.3	17.5	17.8	24.6	.20	50.0	-22.0	1.0	3.5	0.	0.	219.	0.	0.	6.48
F320D4.011	1.2	17.1	17.2	22.3	.15	50.0	-44.0	1.0	3.2	0.	0.	212.	0.	0.	4.98
F320D4.012	.7	.0	22.7	.0	.09	50.0	-66.0	1.0	1.8	0.	0.	279.	0.	0.	2.89
F320D5.006	.1	.0	.0	.0	.00	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.46
F320D5.007	.4	.0	25.6	.0	.01	50.0	44.0	1.0	1.0	0.	0.	315.	0.	0.	.85
F320D5.008	1.3	19.1	19.2	19.2	.08	50.0	22.0	1.0	3.5	0.	0.	236.	0.	0.	2.70
F320D5.009	1.4	16.1	21.7	28.4	.21	50.0	.0	1.0	3.7	0.	0.	267.	0.	0.	6.91
F320D5.010	1.8	10.7	22.3	24.5	.20	50.0	-22.0	1.0	4.6	0.	0.	274.	0.	0.	6.65
F320D5.011	2.1	16.1	21.1	21.5	.13	50.0	-44.0	1.0	5.4	260.	0.	260.	0.	261.	4.41
F320D5.012	.6	.0	21.7	.0	.05	50.0	-66.0	1.0	1.6	0.	0.	267.	0.	0.	1.79
F320E1.006	.1	.0	.0	.0	-.01	50.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.20

FALCON 3: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F320E1.007	.2	.0	29.8	.0	.00	50.0	44.0	5.0	.5	0.	0.	367.	0.	0.	.39
F320E1.008	1.4	3.5	19.5	19.7	.05	50.0	22.0	5.0	3.7	0.	0.	241.	0.	0.	1.81
F320E1.009	1.1	22.4	23.0	23.2	.17	50.0	.0	5.0	2.9	0.	0.	284.	0.	0.	5.59
F320E1.010	1.3	18.4	20.0	27.7	.20	50.0	-22.0	5.0	3.5	0.	0.	246.	0.	0.	6.80
F320E1.011	1.4	17.8	23.5	24.2	.11	50.0	-44.0	5.0	3.6	0.	0.	290.	0.	0.	3.96
F320E1.012	1.2	18.2	19.8	19.8	.06	50.0	-66.0	5.0	3.2	0.	0.	244.	0.	0.	2.22
F320E2.006	.1	.0	.0	.0	.01	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.55
F320E2.007	.1	.0	.0	.0	-.02	50.0	44.0	5.0	.4	0.	0.	0.	0.	0.	.23
F320E2.008	1.4	11.9	12.5	22.3	.08	50.0	22.0	5.0	3.8	0.	0.	154.	0.	0.	2.60
F320E2.009	1.2	12.4	12.4	20.5	.17	50.0	.0	5.0	3.2	0.	0.	153.	0.	0.	5.77
F320E2.010	1.7	14.2	18.1	24.0	.21	50.0	-22.0	5.0	4.4	0.	0.	224.	0.	0.	7.01
F320E2.011	1.5	13.1	13.9	26.6	.13	50.0	-44.0	5.0	3.9	0.	0.	171.	0.	0.	4.42
F320E2.012	1.0	.0	23.5	.0	.03	50.0	-66.0	5.0	2.5	0.	0.	290.	0.	0.	1.31
F320E3.006	.1	.0	.0	.0	-.03	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.11
F320E3.007	.2	.0	.0	.0	.01	50.0	44.0	5.0	.5	0.	0.	0.	0.	0.	.62
F320E3.008	1.7	7.6	7.6	17.2	.03	50.0	22.0	5.0	4.4	0.	0.	94.	0.	0.	1.34
F320E3.009	1.1	14.4	14.4	21.4	.15	50.0	.0	5.0	2.9	0.	0.	178.	0.	0.	5.19
F320E3.010	1.3	17.3	22.6	26.1	.19	50.0	-22.0	5.0	3.5	0.	0.	278.	0.	0.	6.38
F320E3.011	1.6	14.3	22.4	26.3	.20	50.0	-44.0	5.0	4.3	0.	0.	276.	0.	0.	6.69
F320E3.012	1.2	15.7	18.6	22.7	.11	50.0	-66.0	5.0	3.2	0.	0.	229.	0.	0.	3.66
F320E4.006	.1	.0	.0	.0	.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.65
F320E4.007	.6	.0	19.3	.0	.01	50.0	44.0	5.0	1.7	0.	0.	238.	0.	0.	.68
F320E4.008	1.4	7.9	13.5	18.5	.09	50.0	22.0	5.0	3.6	0.	0.	166.	0.	0.	3.04
F320E4.009	1.3	13.3	21.5	29.0	.17	50.0	.0	5.0	3.4	0.	0.	265.	0.	0.	5.81
F320E4.010	1.2	17.5	21.8	21.9	.19	50.0	-22.0	5.0	3.3	0.	0.	269.	0.	0.	6.39
F320E4.011	1.2	14.1	14.5	17.8	.08	50.0	-44.0	5.0	3.3	0.	0.	178.	0.	0.	3.11
F320E4.012	.9	.0	14.0	.0	.04	50.0	-66.0	5.0	2.5	0.	0.	172.	0.	0.	1.46
F320E5.006	.2	.0	.0	.0	.02	50.0	66.0	5.0	.4	0.	0.	0.	0.	0.	.68
F320E5.007	.2	.0	2.5	.0	-.01	50.0	44.0	5.0	.6	0.	0.	30.	0.	0.	.20
F320E5.008	1.7	12.3	12.4	21.0	.08	50.0	22.0	5.0	4.4	0.	0.	153.	0.	0.	2.72
F320E5.009	1.3	14.1	14.1	22.9	.15	50.0	.0	5.0	3.4	0.	0.	174.	0.	0.	5.04
F320E5.010	1.4	10.6	20.4	27.2	.22	50.0	-22.0	5.0	3.7	0.	0.	252.	0.	0.	7.29
F320E5.011	1.2	12.2	21.0	22.3	.11	50.0	-44.0	5.0	3.1	0.	0.	259.	0.	0.	3.79
F320E5.012	1.1	21.6	21.6	21.7	.04	50.0	-66.0	5.0	3.0	0.	0.	267.	0.	0.	1.61
F320F1.006	.2	.0	.0	.0	.02	50.0	66.0	11.0	.4	0.	0.	0.	0.	0.	.67
F320F1.007	1.0	.0	32.7	.0	.04	50.0	44.0	11.0	2.6	0.	0.	403.	0.	0.	1.36
F320F1.008	1.3	10.9	17.8	23.8	.08	50.0	22.0	11.0	3.5	0.	0.	220.	0.	0.	2.89
F320F1.009	1.3	14.7	14.8	23.7	.15	50.0	.0	11.0	3.4	0.	0.	182.	0.	0.	5.26
F320F1.010	1.5	13.5	25.2	25.7	.16	50.0	-22.0	11.0	4.1	0.	0.	311.	0.	0.	5.29
F320F1.011	1.4	16.3	16.4	23.4	.01	50.0	-44.0	11.0	3.7	0.	0.	202.	0.	0.	1.35
F320F1.012	.5	.0	20.5	.0	.00	50.0	-66.0	11.0	1.3	0.	0.	253.	0.	0.	.44
F320F2.006	.1	.0	.0	.0	.00	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.19

FALCON 3: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F320F2.007	.1	.0	.0	.0	-.02	50.0	44.0	11.0	.3	0.	0.	0.	0.	0.	.10
F320F2.008	1.5	10.3	20.8	21.1	.03	50.0	22.0	11.0	4.0	0.	0.	257.	0.	0.	1.68
F320F2.009	1.3	14.1	19.4	28.1	.14	50.0	.0	11.0	3.4	0.	0.	239.	0.	0.	4.74
F320F2.010	2.4	11.7	11.7	30.2	.19	50.0	-22.0	11.0	6.3	144.	0.	144.	0.	145.	6.43
F320F2.011	1.1	20.8	22.1	23.9	.01	50.0	-44.0	11.0	3.0	0.	0.	273.	0.	0.	1.45
F320F2.012	.6	.0	21.6	.0	.01	50.0	-66.0	11.0	1.5	0.	0.	266.	0.	0.	.67
F320F3.006	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.34
F320F3.007	.1	.0	.0	.0	.01	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.58
F320F3.008	1.8	11.2	22.6	22.8	.08	50.0	22.0	11.0	4.7	0.	0.	279.	0.	0.	2.89
F320F3.009	1.2	15.4	19.6	23.5	.13	50.0	.0	11.0	3.2	0.	0.	242.	0.	0.	4.45
F320F3.010	1.8	13.7	21.0	25.5	.19	50.0	-22.0	11.0	4.7	0.	0.	259.	0.	0.	6.26
F320F3.011	1.5	14.4	21.0	21.0	.12	50.0	-44.0	11.0	3.9	0.	0.	258.	0.	0.	3.95
F320F3.012	.8	.0	17.4	.0	.06	50.0	-66.0	11.0	2.2	0.	0.	214.	0.	0.	2.06
F320F4.006	.1	.0	.0	.0	.00	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.11
F320F4.007	.2	.0	11.7	.0	.01	50.0	44.0	11.0	.6	0.	0.	144.	0.	0.	.36
F320F4.008	1.2	18.5	21.5	25.7	.04	50.0	22.0	11.0	3.3	0.	0.	265.	0.	0.	1.52
F320F4.009	1.5	18.4	18.5	22.2	.13	50.0	.0	11.0	4.0	0.	0.	227.	0.	0.	4.30
F320F4.010	1.7	11.9	22.5	23.2	.16	50.0	-22.0	11.0	4.5	0.	0.	277.	0.	0.	5.36
F320F4.011	1.3	19.9	22.7	27.1	.11	50.0	-44.0	11.0	3.4	0.	0.	279.	0.	0.	3.81
F320F4.012	1.1	21.6	21.6	21.6	.03	50.0	-66.0	11.0	2.8	0.	0.	267.	0.	0.	1.37
F320F5.006	.1	.0	.0	.0	.02	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.72
F320F5.007	1.5	20.8	20.8	20.8	.01	50.0	44.0	11.0	3.9	0.	0.	256.	0.	0.	.57
F320F5.008	1.6	2.7	21.5	23.3	.07	50.0	22.0	11.0	4.3	0.	0.	265.	0.	0.	2.48
F320F5.009	1.6	19.2	27.1	27.7	.17	50.0	.0	11.0	4.3	0.	0.	334.	0.	0.	5.58
F320F5.010	1.4	16.2	25.4	25.8	.19	50.0	-22.0	11.0	3.7	0.	0.	314.	0.	0.	6.22
F320F5.011	1.6	14.8	18.5	28.2	.10	50.0	-44.0	11.0	4.1	0.	0.	229.	0.	0.	3.41
F320F5.012	.7	.0	23.6	.0	.06	50.0	-66.0	11.0	1.9	0.	0.	291.	0.	0.	1.94
F320G1.006	.1	.0	.0	.0	.01	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.48
F320G1.007	.1	.0	.0	.0	.00	50.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.30
F320G1.008	1.3	13.3	13.4	23.5	.01	50.0	22.0	17.0	3.3	0.	0.	165.	0.	0.	1.25
F320G1.009	1.3	13.1	19.5	19.8	.08	50.0	.0	17.0	3.5	0.	0.	241.	0.	0.	3.00
F320G1.010	1.5	2.3	19.1	26.6	.10	50.0	-22.0	17.0	3.9	0.	0.	236.	0.	0.	3.49
F320G1.011	1.3	13.4	14.4	30.2	.07	50.0	-44.0	17.0	3.4	0.	0.	177.	0.	0.	2.41
F320G1.012	.5	.0	19.9	.0	.04	50.0	-66.0	17.0	1.3	0.	0.	245.	0.	0.	1.50
F320G2.006	.1	.0	.0	.0	.01	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.53
F320G2.007	.5	.0	36.8	.0	.00	50.0	44.0	17.0	1.3	0.	0.	454.	0.	0.	.27
F320G2.008	1.2	13.6	15.8	21.7	.05	50.0	22.0	17.0	3.2	0.	0.	194.	0.	0.	1.97
F320G2.009	1.7	14.7	20.3	29.2	.12	50.0	.0	17.0	4.6	0.	0.	250.	0.	0.	4.06
F320G2.010	1.4	11.8	16.7	30.3	.09	50.0	-22.0	17.0	3.6	0.	0.	206.	0.	0.	3.44
F320G2.011	1.2	17.4	24.1	30.5	.00	50.0	-44.0	17.0	3.1	0.	0.	297.	0.	0.	1.30
F320G2.012	.3	.0	18.4	.0	-.01	50.0	-66.0	17.0	.7	0.	0.	227.	0.	0.	.24
F320G3.006	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.09

FALCON 3: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F320G3.007	.1	.0	.0	.0	-.01	50.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.11
F320G3.008	1.5	15.5	23.1	28.1	.03	50.0	22.0	17.0	3.9	0.	0.	284.	0.	0.	1.63
F320G3.009	1.0	.0	20.7	.0	.00	50.0	.0	17.0	2.6	0.	0.	255.	0.	0.	1.21
F320G3.010	1.6	4.0	21.0	28.1	.08	50.0	-22.0	17.0	4.1	0.	0.	258.	0.	0.	3.26
F320G3.011	1.4	12.9	13.8	24.3	.05	50.0	-44.0	17.0	3.7	0.	0.	170.	0.	0.	2.31
F320G3.012	.7	.0	8.0	.0	-.02	50.0	-66.0	17.0	1.8	0.	0.	98.	0.	0.	.21
F320G4.006	.1	.0	.0	.0	.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.55
F320G4.007	.2	.0	.0	.0	.02	50.0	44.0	17.0	.5	0.	0.	0.	0.	0.	.69
F320G4.008	1.4	16.6	20.6	28.0	.06	50.0	22.0	17.0	3.6	0.	0.	254.	0.	0.	2.03
F320G4.009	1.3	15.9	26.2	26.7	.11	50.0	.0	17.0	3.4	0.	0.	323.	0.	0.	3.85
F320G4.010	1.4	9.9	19.4	28.5	.12	50.0	-22.0	17.0	3.8	0.	0.	239.	0.	0.	4.12
F320G4.011	1.3	12.1	25.7	28.0	.04	50.0	-44.0	17.0	3.4	0.	0.	317.	0.	0.	1.78
F320G4.012	.4	.0	20.7	.0	-.01	50.0	-66.0	17.0	1.1	0.	0.	255.	0.	0.	.29
F320G5.006	.1	.0	.0	.0	.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.24
F320G5.007	.4	.0	39.2	.0	.00	50.0	44.0	17.0	1.0	0.	0.	483.	0.	0.	.18
F320G5.008	1.6	3.8	21.9	27.1	.05	50.0	22.0	17.0	4.2	0.	0.	270.	0.	0.	1.74
F320G5.009	2.0	9.1	9.2	27.6	.07	50.0	.0	17.0	5.2	113.	0.	113.	0.	113.	2.82
F320G5.010	1.5	9.5	24.5	24.6	.09	50.0	-22.0	17.0	4.0	0.	0.	302.	0.	0.	3.46
F320G5.011	1.4	15.0	15.8	23.8	.06	50.0	-44.0	17.0	3.7	0.	0.	195.	0.	0.	2.40
F320G5.012	.6	.0	16.9	.0	-.01	50.0	-66.0	17.0	1.7	0.	0.	208.	0.	0.	.33
F320H1.006	.1	.0	.0	.0	.00	150.0	84.0	1.0	.3	0.	0.	0.	0.	0.	.35
F320H1.007	.1	.0	.0	.0	-.01	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.12
F320H1.008	.3	.0	21.3	.0	.01	150.0	28.0	1.0	.7	0.	0.	262.	0.	0.	.74
F320H1.009	.6	.0	24.4	.0	.11	150.0	.0	1.0	1.7	0.	0.	300.	0.	0.	3.64
F320H1.010	.7	.0	24.6	.0	.12	150.0	-28.0	1.0	2.0	0.	0.	304.	0.	0.	4.12
F320H1.011	.8	.0	21.3	.0	.13	150.0	-56.0	1.0	2.1	0.	0.	262.	0.	0.	4.44
F320H1.012	.5	.0	21.3	.0	.06	150.0	-84.0	1.0	1.2	0.	0.	263.	0.	0.	2.08
F320H2.006	.2	.0	.0	.0	.03	150.0	84.0	1.0	.4	0.	0.	0.	0.	0.	.87
F320H2.007	.1	.0	.0	.0	.01	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.47
F320H2.008	.2	.0	34.8	.0	.01	150.0	28.0	1.0	.6	0.	0.	429.	0.	0.	.58
F320H2.009	.7	.0	19.8	.0	.11	150.0	.0	1.0	1.9	0.	0.	244.	0.	0.	3.67
F320H2.010	.8	.0	19.8	.0	.12	150.0	-28.0	1.0	2.2	0.	0.	244.	0.	0.	3.94
F320H2.011	.7	.0	18.5	.0	.07	150.0	-56.0	1.0	1.8	0.	0.	228.	0.	0.	2.75
F320H2.012	.6	.0	19.7	.0	.03	150.0	-84.0	1.0	1.5	0.	0.	243.	0.	0.	1.20
F320H3.006	.2	.0	.0	.0	.01	150.0	84.0	1.0	.4	0.	0.	0.	0.	0.	.65
F320H3.007	.2	.0	.0	.0	.03	150.0	56.0	1.0	.5	0.	0.	0.	0.	0.	1.04
F320H3.008	.5	.0	23.7	.0	.07	150.0	28.0	1.0	1.2	0.	0.	292.	0.	0.	2.33
F320H3.009	.7	.0	26.7	.0	.11	150.0	.0	1.0	1.8	0.	0.	329.	0.	0.	3.58
F320H3.010	.7	.0	22.9	.0	.11	150.0	-28.0	1.0	1.9	0.	0.	282.	0.	0.	3.67
F320H3.011	.9	.0	21.3	.0	.12	150.0	-56.0 20	1	2.5	0.	0.	263.	0.	0.	4.27
F320H3.012	.5	.0	24.3	.0	.06	150.0	-84.0	1.0	1.4	0.	0.	300.	0.	0.	1.90
F320H4.006	.1	.0	.0	.0	-.02	150.0	84.0	1.0	.2	0.	0.	0.	0.	0.	.01

FALCON 3: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F320H4.007	.1	.0	.0	.0	.00	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.44
F320H4.008	.5	.0	17.3	.0	.06	150.0	28.0	1.0	1.3	0.	0.	213.	0.	0.	1.90
F320H4.009	.6	.0	30.2	.0	.11	150.0	.0	1.0	1.6	0.	0.	373.	0.	0.	3.60
F320H4.010	.7	.0	22.4	.0	.12	150.0	-28.0	1.0	1.9	0.	0.	276.	0.	0.	3.96
F320H4.011	.7	.0	18.5	.0	.09	150.0	-56.0	1.0	1.9	0.	0.	227.	0.	0.	3.20
F320H4.012	.5	.0	16.7	.0	.02	150.0	-84.0	1.0	1.3	0.	0.	205.	0.	0.	1.35
F320H5.006	.2	.0	.0	.0	.03	150.0	84.0	1.0	.5	0.	0.	0.	0.	0.	1.15
F320H5.007	.1	.0	.0	.0	.00	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.33
F320H5.008	.6	.0	21.4	.0	.04	150.0	28.0	1.0	1.6	0.	0.	264.	0.	0.	1.37
F320H5.009	.5	.0	30.7	.0	.06	150.0	.0	1.0	1.5	0.	0.	379.	0.	0.	2.54
F320H5.010	.7	.0	23.2	.0	.12	150.0	-28.0	1.0	1.8	0.	0.	285.	0.	0.	4.00
F320H5.011	.7	.0	27.1	.0	.10	150.0	-56.0	1.0	1.9	0.	0.	335.	0.	0.	3.36
F320H5.012	.4	.0	23.9	.0	.01	150.0	-84.0	1.0	1.1	0.	0.	295.	0.	0.	.94
F320I1.006	.1	.0	.0	.0	-.04	150.0	84.0	5.0	.2	0.	0.	0.	0.	0.	.01
F320I1.007	.1	.0	.0	.0	-.02	150.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.22
F320I1.008	.3	.0	24.0	.0	.02	150.0	28.0	5.0	.7	0.	0.	296.	0.	0.	.78
F320I1.009	.6	.0	22.6	.0	.08	150.0	.0	5.0	1.5	0.	0.	279.	0.	0.	2.61
F320I1.010	.8	.0	21.3	.0	.11	150.0	-28.0	5.0	2.1	0.	0.	263.	0.	0.	3.62
F320I1.011	.9	.0	22.2	.0	.09	150.0	-56.0	5.0	2.4	0.	0.	274.	0.	0.	3.20
F320I1.012	.7	.0	27.3	.0	.04	150.0	-84.0	5.0	1.8	0.	0.	336.	0.	0.	1.62
F320I2.006	.1	.0	.0	.0	-.01	150.0	84.0	5.0	.2	0.	0.	0.	0.	0.	.02
F320I2.007	.2	.0	.0	.0	.00	150.0	56.0	5.0	.5	0.	0.	0.	0.	0.	.46
F320I2.008	.5	.0	20.9	.0	-.01	150.0	28.0	5.0	1.3	0.	0.	258.	0.	0.	.26
F320I2.009	.6	.0	25.8	.0	.04	150.0	.0	5.0	1.5	0.	0.	318.	0.	0.	1.74
F320I2.010	.7	.0	21.5	.0	.10	150.0	-28.0	5.0	1.9	0.	0.	265.	0.	0.	3.32
F320I2.011	.8	.0	23.5	.0	.15	150.0	-56.0	5.0	2.1	0.	0.	289.	0.	0.	5.15
F320I2.012	.6	.0	23.9	.0	.05	150.0	-84.0	5.0	1.6	0.	0.	295.	0.	0.	2.03
F320I3.006	.1	.0	.0	.0	-.01	150.0	84.0	5.0	.3	0.	0.	0.	0.	0.	.24
F320I3.007	.2	.0	.0	.0	.03	150.0	56.0	5.0	.5	0.	0.	0.	0.	0.	1.08
F320I3.008	.5	.0	25.3	.0	.05	150.0	28.0	5.0	1.3	0.	0.	312.	0.	0.	1.83
F320I3.009	.9	.0	19.4	.0	.11	150.0	.0	5.0	2.4	0.	0.	240.	0.	0.	3.65
F320I3.010	.9	.0	19.8	.0	.11	150.0	-28.0	5.0	2.3	0.	0.	244.	0.	0.	3.61
F320I3.011	.8	.0	18.6	.0	.08	150.0	-56.0	5.0	2.1	0.	0.	229.	0.	0.	2.92
F320I3.012	.6	.0	17.6	.0	.06	150.0	-84.0	5.0	1.7	0.	0.	217.	0.	0.	1.92
F320I4.006	.1	.0	.0	.0	.02	150.0	84.0	5.0	.4	0.	0.	0.	0.	0.	.66
F320I4.007	.1	.0	.0	.0	-.04	150.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.14
F320I4.008	.5	.0	14.0	.0	.03	150.0	28.0	5.0	1.3	0.	0.	172.	0.	0.	1.10
F320I4.009	.7	.0	20.9	.0	.10	150.0	.0	5.0	1.8	0.	0.	257.	0.	0.	3.37
F320I4.010	.9	.0	19.6	.0	.11	150.0	-28.0	5.0	2.5	0.	0.	242.	0.	0.	3.51
F320I4.011	.9	.0	21.3	.0	.12	150.0	-56.0	5.0	2.4	0.	0.	263.	0.	0.	3.97
F320I4.012	.6	.0	22.6	.0	.04	150.0	-84.0	5.0	1.6	0.	0.	278.	0.	0.	1.52
F320I5.006	.1	.0	.0	.0	.00	150.0	84.0	5.0	.3	0.	0.	0.	0.	0.	.27

FALCON 3: LSR = 200, GAS = ARGON

MODEL CONDITIONS									PROTOTYPE CONDITIONS						
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F320I5.007	.2	.0	50.3	.0	.00	150.0	56.0	5.0	.6	0.	0.	621.	0.	0.	.48
F320I5.008	.5	.0	14.9	.0	.02	150.0	28.0	5.0	1.3	0.	0.	183.	0.	0.	.93
F320I5.009	.7	.0	25.7	.0	.08	150.0	.0	5.0	1.8	0.	0.	317.	0.	0.	2.75
F320I5.010	.7	.0	19.1	.0	.11	150.0	-28.0	5.0	1.9	0.	0.	236.	0.	0.	3.83
F320I5.011	.8	.0	21.3	.0	.10	150.0	-56.0	5.0	2.0	0.	0.	262.	0.	0.	3.41
F320I5.012	.5	.0	22.1	.0	.04	150.0	-84.0	5.0	1.4	0.	0.	273.	0.	0.	1.45
F320J1.006	.1	.0	.0	.0	.00	150.0	84.0	11.0	.2	0.	0.	0.	0.	0.	.27
F320J1.007	.3	.0	28.3	.0	-.01	150.0	56.0	11.0	.8	0.	0.	349.	0.	0.	.29
F320J1.008	.5	.0	23.3	.0	.04	150.0	28.0	11.0	1.4	0.	0.	288.	0.	0.	1.43
F320J1.009	.9	.0	23.0	.0	.09	150.0	.0	11.0	2.4	0.	0.	284.	0.	0.	2.97
F320J1.010	.8	.0	19.1	.0	.09	150.0	-28.0	11.0	2.1	0.	0.	236.	0.	0.	3.07
F320J1.011	.8	.0	19.8	.0	.05	150.0	-56.0	11.0	2.2	0.	0.	244.	0.	0.	1.99
F320J1.012	.5	.0	19.6	.0	.01	150.0	-84.0	11.0	1.3	0.	0.	242.	0.	0.	.67
F320J2.006	.2	.0	.0	.0	.02	150.0	84.0	11.0	.4	0.	0.	0.	0.	0.	.92
F320J2.007	.2	.0	25.9	.0	.02	150.0	56.0	11.0	.6	0.	0.	319.	0.	0.	.67
F320J2.008	.5	.0	19.3	.0	.00	150.0	28.0	11.0	1.4	0.	0.	238.	0.	0.	.52
F320J2.009	.7	.0	18.7	.0	.07	150.0	.0	11.0	1.8	0.	0.	230.	0.	0.	2.54
F320J2.010	.8	.0	21.5	.0	.08	150.0	-28.0	11.0	2.0	0.	0.	265.	0.	0.	2.80
F320J2.011	.8	.0	21.8	.0	.03	150.0	-56.0	11.0	2.2	0.	0.	269.	0.	0.	1.56
F320J2.012	.8	.0	25.4	.0	.03	150.0	-84.0	11.0	2.0	0.	0.	313.	0.	0.	1.10
F320J3.006	.1	.0	.0	.0	-.02	150.0	84.0	11.0	.2	0.	0.	0.	0.	0.	.03
F320J3.007	.1	.0	.0	.0	.01	150.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.41
F320J3.008	.6	.0	16.3	.0	.03	150.0	28.0	11.0	1.5	0.	0.	201.	0.	0.	1.05
F320J3.009	.7	.0	21.0	.0	.09	150.0	.0	11.0	1.9	0.	0.	259.	0.	0.	3.08
F320J3.010	.8	.0	20.0	.0	.10	150.0	-28.0	11.0	2.0	0.	0.	246.	0.	0.	3.30
F320J3.011	.8	.0	13.4	.0	.02	150.0	-56.0	11.0	2.0	0.	0.	165.	0.	0.	1.17
F320J3.012	.5	.0	13.3	.0	.02	150.0	-84.0	11.0	1.3	0.	0.	164.	0.	0.	.82
F320J4.006	.1	.0	.0	.0	.00	150.0	84.0	11.0	.2	0.	0.	0.	0.	0.	.14
F320J4.007	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.12
F320J4.008	.5	.0	26.6	.0	.01	150.0	28.0	11.0	1.3	0.	0.	328.	0.	0.	.60
F320J4.009	.7	.0	21.1	.0	.07	150.0	.0	11.0	1.9	0.	0.	260.	0.	0.	2.53
F320J4.010	.7	.0	21.7	.0	.10	150.0	-28.0	11.0	2.0	0.	0.	268.	0.	0.	3.22
F320J4.011	.7	.0	25.6	.0	.08	150.0	-56.0	11.0	2.0	0.	0.	316.	0.	0.	2.61
F320J4.012	.7	.0	26.1	.0	.03	150.0	-84.0	11.0	1.7	0.	0.	321.	0.	0.	1.23
F320J5.006	.1	.0	.0	.0	.00	150.0	84.0	11.0	.3	0.	0.	0.	0.	0.	.33
F320J5.007	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.10
F320J5.008	.5	.0	22.6	.0	.02	150.0	28.0	11.0	1.2	0.	0.	279.	0.	0.	.76
F320J5.009	.6	.0	19.2	.0	.05	150.0	.0	11.0	1.5	0.	0.	237.	0.	0.	1.79
F320J5.010	.8	.0	20.0	.0	.10	150.0	-28.0	11.0	2.1	0.	0.	246.	0.	0.	3.24
F320J5.011	1.0	17.5	17.5	17.5	.09	150.0	-56.0	11.0	2.8	0.	0.	215.	0.	0.	3.04
F320J5.012	.7	.0	20.1	.0	.05	150.0	-84.0	11.0	1.8	0.	0.	247.	0.	0.	1.79
F320K1.006	.1	.0	.0	.0	-.01	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.11

FALCON 3: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS: PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS: POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F320K1.007	.0	.0	.0	.0	-.04	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.01
F320K1.008	.2	.0	.0	.0	-.04	150.0	28.0	17.0	.4	0.	0.	0.	0.	0.	.05
F320K1.009	.5	.0	19.0	.0	.03	150.0	.0	17.0	1.5	0.	0.	234.	0.	0.	1.29
F320K1.010	.6	.0	18.4	.0	.06	150.0	-28.0	17.0	1.7	0.	0.	226.	0.	0.	1.98
F320K1.011	.7	.0	25.4	.0	.09	150.0	-56.0	17.0	1.9	0.	0.	313.	0.	0.	2.97
F320K1.012	.4	.0	25.5	.0	.00	150.0	-84.0	17.0	1.2	0.	0.	315.	0.	0.	.59
F320K2.006	.1	.0	.0	.0	.00	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.13
F320K2.007	.1	.0	.0	.0	-.01	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.17
F320K2.008	.4	.0	21.4	.0	.00	150.0	28.0	17.0	1.2	0.	0.	264.	0.	0.	.31
F320K2.009	.8	.0	19.7	.0	.03	150.0	.0	17.0	2.1	0.	0.	243.	0.	0.	1.11
F320K2.010	.7	.0	19.3	.0	.09	150.0	-28.0	17.0	1.9	0.	0.	238.	0.	0.	2.91
F320K2.011	.8	.0	19.6	.0	.07	150.0	-56.0	17.0	2.1	0.	0.	241.	0.	0.	2.48
F320K2.012	.7	.0	29.0	.0	.02	150.0	-84.0.	17.0	1.8	0.	0.	358.	0.	0.	.86
F320K3.006	.0	.0	.0	.0	-.02	150.0	84.0	17.0	.1	0.	0.	0.	0.	0.	.04
F320K3.007	.1	.0	.0	.0	.01	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.46
F320K3.008	.8	.0	16.7	.0	.07	150.0	28.0	17.0	2.1	0.	0.	206.	0.	0.	2.39
F320K3.009	.8	.0	16.2	.0	.08	150.0	.0	17.0	2.1	0.	0.	200.	0.	0.	2.82
F320K3.010	.7	.0	16.8	.0	.07	150.0	-28.0	17.0	1.8	0.	0.	208.	0.	0.	2.32
F320K3.011	.6	.0	27.6	.0	.04	150.0	-56.0 3	170	1.7	0.	0.	340.	0.	0.	1.42
F320K3.012	.1	.0	.0	.0	-.02	150.0	-84.0 3	170	.2	0.	0.	0.	0.	0.	.05
F320K4.006	.1	.0	.0	.0	.00	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.07
F320K4.007	.1	.0	.0	.0	.02	150.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.60
F320K4.008	.3	.0	32.4	.0	.04	150.0	28.0	17.0	.8	0.	0.	400.	0.	0.	1.24
F320K4.009	.6	.0	17.7	.0	.05	150.0	.0	17.0	1.6	0.	0.	218.	0.	0.	1.76
F320K4.010	.9	.0	18.6	.0	.10	150.0	-28.0	17.0	2.3	0.	0.	230.	0.	0.	3.18
F320K4.011	.8	.0	25.9	.0	.07	150.0	-56.0	17.0	2.1	0.	0.	319.	0.	0.	2.51
F320K4.012	.5	.0	21.0	.0	.01	150.0	-84.0	17.0	1.3	0.	0.	259.	0.	0.	.64
F320K5.006	.1	.0	.0	.0	-.01	150.0	84.0	17.0	.1	0.	0.	0.	0.	0.	.07
F320K5.007	.0	.0	.0	.0	-.03	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.03
F320K5.008	.3	.0	35.3	.0	-.02	150.0	28.0	17.0	.7	0.	0.	436.	0.	0.	.15
F320K5.009	.4	.0	18.4	.0	.00	150.0	.0	17.0	1.2	0.	0.	227.	0.	0.	.71
F320K5.010	.8	.0	21.2	.0	.06	150.0	-28.0	17.0	2.0	0.	0.	261.	0.	0.	2.12
F320K5.011	.9	.0	24.6	.0	.09	150.0	-56.0	17.0	2.5	0.	0.	304.	0.	0.	2.95
F320K5.012	.5	.0	25.1	.0	.00	150.0	-84.0	17.0	1.4	0.	0.	309.	0.	0.	.45

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405A1.009	.4	.0	49.8	.0	.03	-62.0	25.0	2.0	1.0	0.	0.	307.	0.	0.	.67
N405A1.008	10.4	8.6	52.7	74.1	2.01	-62.0	20.0	2.0	23.9	53.	61.	325.	370.	446.	31.54
N405A1.007	7.1	7.0	16.3	76.2	1.48	-62.0	15.0	2.0	17.1	43.	100.	101.	347.	407.	23.66
N405A1.006	16.2	6.1	51.9	71.4	2.59	-62.0	10.0	2.0	34.2	39.	40.	319.	377.	407.	39.78
N405A1.005	18.8	5.6	52.7	72.2	4.31	-62.0	5.0	2.0	38.4	38.	39.	325.	375.	412.	63.34
N405A1.004	25.4	5.3	52.2	71.5	4.09	-62.0	.0	2.0	48.0	32.	35.	322.	375.	404.	60.09
N405A2.009	.6	.0	23.9	.0	.02	-62.0	25.0	2.0	1.6	0.	0.	147.	0.	0.	.34
N405A2.008	12.3	4.6	53.3	72.1	2.08	-62.0	20.0	2.0	27.6	31.	40.	328.	351.	392.	32.65
N405A2.007	7.2	4.0	53.3	72.0	1.57	-62.0	15.0	2.0	17.4	34.	34.	328.	344.	401.	25.00
N405A2.006	14.0	3.1	12.7	69.4	3.23	-62.0	10.0	2.0	30.6	23.	23.	78.	390.	406.	48.52
N405A2.005	21.2	2.7	32.4	70.1	4.94	-62.0	5.0	2.0	42.0	18.	20.	199.	392.	404.	70.75
N405A2.004	21.3	2.5	26.0	72.1	4.78	-62.0	.0	2.0	42.3	16.	16.	160.	389.	406.	68.75
N405A3.009	.9	.0	18.7	.0	.03	-62.0	25.0	2.0	2.5	0.	0.	115.	0.	0.	.58
N405A3.008	12.2	6.0	28.4	75.6	2.85	-62.0	20.0	2.0	27.3	39.	109.	175.	395.	442.	43.57
N405A3.007	9.8	6.0	25.5	73.3	1.93	-62.0	15.0	2.0	22.8	74.	81.	157.	372.	426.	30.26
N405A3.006	15.2	3.6	33.7	72.1	2.35	-62.0	10.0	2.0	32.6	23.	24.	207.	396.	422.	36.38
N405A3.005	20.0	3.0	46.1	71.4	3.93	-62.0	5.0	2.0	40.3	19.	22.	284.	391.	422.	58.18
N405A3.004	20.4	2.4	45.7	77.9	3.71	-62.0	.0	2.0	41.0	15.	26.	281.	388.	436.	55.35
N405A4.009	.3	.0	37.8	.0	.01	-62.0	25.0	2.0	.8	0.	0.	233.	0.	0.	.22
N405A4.008	11.1	9.8	46.9	74.6	2.90	-62.0	20.0	2.0	25.3	61.	94.	289.	353.	435.	44.09
N405A4.007	11.6	3.9	39.0	75.5	1.89	-62.0	15.0	2.0	26.1	36.	85.	240.	343.	413.	29.68
N405A4.006	13.6	3.5	23.0	71.4	2.56	-62.0	10.0	2.0	29.8	22.	29.	142.	348.	389.	39.29
N405A4.005	19.2	2.6	45.7	73.0	4.41	-62.0	5.0	2.0	39.1	17.	25.	281.	366.	408.	63.97
N405A4.004	18.2	2.2	45.4	74.0	4.27	-62.0	.0	2.0	37.5	13.	16.	280.	373.	406.	62.36
N405A5.009	.3	.0	63.5	.0	.02	-62.0	25.0	2.0	.8	0.	0.	391.	0.	0.	.44
N405A5.008	9.1	7.5	35.0	74.8	2.85	-62.0	20.0	2.0	21.3	49.	107.	216.	402.	433.	43.89
N405A5.007	7.5	6.5	30.3	73.7	1.83	-62.0	15.0	2.0	18.0	40.	99.	187.	381.	419.	28.90
N405A5.006	14.2	4.6	43.5	70.8	2.02	-62.0	10.0	2.0	30.9	36.	37.	268.	365.	413.	31.75
N405A5.005	19.0	2.9	43.1	85.1	3.44	-62.0	5.0	2.0	38.7	25.	39.	265.	364.	396.	51.56
N405A5.004	18.7	2.7	42.6	82.8	3.57	-62.0	.0	2.0	38.3	29.	35.	262.	362.	393.	53.01
N405B1.009	.4	.0	31.6	.0	.02	-32.0	25.0	1.0	.9	0.	0.	195.	0.	0.	.54
N405B1.008	29.1	4.1	35.1	77.4	7.36	-32.0	20.0	1.0	52.6	25.	25.	216.	368.	414.	99.59
N405B1.007	29.2	5.2	42.7	117.7	4.17	-32.0	15.0	1.0	52.8	36.	41.	263.	366.	725.	58.56
N405B1.006	20.6	6.2	18.7	78.8	1.53	-32.0	10.0	1.0	41.2	38.	58.	115.	341.	432.	24.17
N405B1.005	12.6	9.3	36.8	77.7	1.14	-32.0	5.0	1.0	28.1	66.	97.	227.	319.	396.	18.33
N405B1.004	19.9	6.2	25.7	76.5	1.21	-32.0	.0	1.0	40.2	45.	73.	158.	340.	398.	19.56
N405B2.009	.2	.0	57.5	.0	.00	-32.0	25.0	1.0	.6	0.	0.	354.	0.	0.	.19
N405B2.008	30.2	2.3	42.7	74.9	7.58	-32.0	20.0	1.0	53.9	18.	25.	263.	371.	417.	101.47
N405B2.007	41.9	4.4	42.1	117.7	4.82	-32.0	15.0	1.0	66.1	36.	36.	259.	362.	479.	65.62
N405B2.006	22.1	5.4	19.2	83.2	1.64	-32.0	10.0	1.0	43.4	57.	57.	118.	361.	384.	25.66
N405B2.005	10.4	5.5	19.6	75.5	1.14	-32.0	5.0	1.0	23.8	68.	99.	121.	320.	383.	18.39
N405B2.004	15.2	1.3	31.9	72.9	1.22	-32.0	.0	1.0	32.6	35.	147.	196.	327.	374.	19.61

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405B3.009	.2	.0	66.7	.0	.01	-32.0	25.0	1.0	.6	0.	0.	411.	0.	0.	.37
N405B3.008	28.2	3.0	35.0	77.9	7.27	-32.0	20.0	1.0	51.5	18.	18.	216.	348.	391.	98.34
N405B3.007	35.9	3.8	50.3	109.7	3.88	-32.0	15.0	1.0	60.2	31.	32.	310.	353.	469.	54.14
N405B3.006	23.4	5.8	19.8	77.3	1.86	-32.0	10.0	1.0	45.2	41.	46.	122.	325.	445.	28.36
N405B3.005	15.7	6.4	12.2	79.8	1.23	-32.0	5.0	1.0	33.4	40.	75.	75.	307.	392.	19.79
N405B3.004	19.0	6.5	44.7	73.1	1.38	-32.0	.0	1.0	38.9	41.	68.	275.	319.	367.	21.88
N405B4.009	.5	.0	51.8	.0	.03	-32.0	25.0	1.0	1.4	0.	0.	319.	0.	0.	.47
N405B4.008	31.1	3.2	48.6	80.3	7.55	-32.0	20.0	1.0	55.0	27.	27.	299.	370.	394.	101.13
N405B4.007	33.8	2.8	49.8	112.6	4.18	-32.0	15.0	1.0	57.9	28.	35.	307.	388.	494.	57.88
N405B4.006	20.1	3.3	49.9	78.3	1.67	-32.0	10.0	1.0	40.5	44.	48.	307.	338.	380.	26.18
N405B4.005	10.1	4.4	22.4	74.7	1.28	-32.0	5.0	1.0	23.2	27.	49.	138.	304.	378.	20.45
N405B4.004	13.8	7.9	36.8	76.2	1.34	-32.0	.0	1.0	30.2	49.	52.	227.	326.	407.	21.52
N405B5.009	.2	.0	62.8	.0	-.02	-32.0	25.0	1.0	.6	0.	0.	387.	0.	0.	.14
N405B5.008	24.9	1.8	35.9	77.9	6.76	-32.0	20.0	1.0	47.3	12.	13.	221.	351.	385.	91.89
N405B5.007	28.6	3.0	34.5	106.5	3.03	-32.0	15.0	1.0	52.0	18.	53.	212.	367.	557.	44.05
N405B5.006	25.3	2.0	46.6	85.1	1.64	-32.0	10.0	1.0	47.7	12.	13.	287.	337.	395.	25.49
N405B5.005	12.2	3.2	47.8	74.6	1.13	-32.0	5.0	1.0	27.3	46.	94.	295.	295.	385.	18.11
N405B5.004	13.5	3.0	49.4	71.4	1.19	-32.0	.0	1.0	29.6	51.	69.	304.	336.	387.	19.08
N405C1.009	.2	.0	37.1	.0	.05	-2.0	25.0	1.0	.7	0.	0.	228.	0.	0.	.89
N405C1.008	4.2	15.8	46.5	69.7	.58	-2.0	20.0	1.0	10.6	225.	286.	286.	287.	358.	9.46
N405C1.007	4.1	14.4	36.2	62.1	.61	-2.0	15.0	1.0	10.3	184.	223.	223.	223.	322.	10.02
N405C1.006	5.0	8.7	49.8	66.7	.64	-2.0	10.0	1.0	12.4	181.	307.	307.	307.	319.	10.45
N405C1.005	2.2	13.7	49.3	63.5	.62	-2.0	5.0	1.0	5.8	171.	0.	303.	0.	304.	10.17
N405C1.004	2.0	13.2	21.0	64.4	.59	-2.0	.0	1.0	5.3	111.	0.	129.	0.	181.	9.65
N405C2.009	.2	.0	62.3	.0	.03	-2.0	25.0	1.0	.5	0.	0.	384.	0.	0.	.54
N405C2.008	11.9	3.8	40.6	68.1	.68	-2.0	20.0	1.0	26.8	72.	101.	250.	258.	265.	10.97
N405C2.007	18.0	9.5	40.4	92.1	.65	-2.0	15.0	1.0	37.2	69.	100.	249.	253.	266.	10.44
N405C2.006	14.9	8.8	40.5	64.5	.60	-2.0	10.0	1.0	32.1	98.	249.	250.	252.	324.	9.78
N405C2.005	7.1	15.6	40.5	64.3	.57	-2.0	5.0	1.0	17.1	97.	249.	249.	251.	311.	9.28
N405C2.004	10.5	8.5	40.5	60.0	.60	-2.0	.0	1.0	24.1	249.	249.	249.	250.	309.	9.75
N405C3.009	.2	.0	38.0	.0	.04	-2.0	25.0	1.0	.6	0.	0.	234.	0.	0.	.75
N405C3.008	2.8	11.3	35.1	73.9	.57	-2.0	20.0	1.0	7.3	162.	0.	216.	0.	322.	9.38
N405C3.007	5.1	10.9	73.6	73.7	.61	-2.0	15.0	1.0	12.8	159.	453.	453.	454.	454.	10.02
N405C3.006	3.2	10.1	25.5	73.4	.60	-2.0	10.0	1.0	8.3	157.	0.	157.	0.	324.	9.79
N405C3.005	5.2	10.4	25.3	73.0	.55	-2.0	5.0	1.0	12.8	155.	155.	156.	156.	319.	9.07
N405C3.004	3.2	9.9	48.5	58.7	.57	-2.0	.0	1.0	8.2	190.	0.	299.	0.	308.	9.37
N405C4.009	.3	.0	66.8	.0	.06	-2.0	25.0	1.0	.8	0.	0.	411.	0.	0.	.99
N405C4.008	4.0	12.8	26.0	67.0	.60	-2.0	20.0	1.0	10.0	151.	160.	160.	161.	334.	9.86
N405C4.007	6.3	12.5	24.4	70.6	.59	-2.0	15.0	1.0	15.4	77.	150.	150.	151.	332.	9.61
N405C4.006	4.8	12.3	25.6	74.5	.58	-2.0	10.0	1.0	11.9	76.	157.	158.	158.	330.	9.59
N405C4.005	3.8	12.3	48.9	77.6	.53	-2.0	5.0	1.0	9.5	300.	0.	301.	0.	317.	8.71
N405C4.004	3.2	13.8	52.3	71.3	.55	-2.0	.0	1.0	8.1	322.	0.	322.	0.	438.	9.10

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405C5.009	.2	.0	50.1	.0	.05	-2.0	25.0	1.0	.6	0.	0.	309.	0.	0.	.79
N405C5.008	3.3	11.1	35.6	70.2	.60	-2.0	20.0	1.0	8.4	153.	0.	220.	0.	313.	9.85
N405C5.007	2.7	8.8	42.4	70.0	.66	-2.0	15.0	1.0	7.0	102.	0.	261.	0.	317.	10.83
N405C5.006	3.0	10.5	35.1	67.6	.61	-2.0	10.0	1.0	7.7	157.	0.	216.	0.	416.	9.97
N405C5.005	2.3	10.4	48.1	69.8	.56	-2.0	5.0	1.0	6.0	215.	0.	296.	0.	338.	9.15
N405C5.004	3.4	10.1	48.1	76.9	.58	-2.0	.0	1.0	8.6	199.	0.	296.	0.	314.	9.58
N405D1.009	.1	.0	.0	.0	.02	50.0	33.0	1.0	.3	0.	0.	0.	0.	0.	.46
N405D1.008	.2	.0	32.0	.0	-.01	50.0	28.0	1.0	.7	0.	0.	197.	0.	0.	.11
N405D1.007	.4	.0	32.7	.0	.07	50.0	25.0	1.0	1.1	0.	0.	201.	0.	0.	1.16
N405D1.006	.6	.0	45.6	.0	.04	50.0	22.0	1.0	1.6	0.	0.	281.	0.	0.	.75
N405D1.005	.6	.0	43.7	.0	.14	50.0	11.0	1.0	1.6	0.	0.	269.	0.	0.	2.32
N405D1.004	.6	.0	54.1	.0	.23	50.0	.0	1.0	1.7	0.	0.	333.	0.	0.	3.90
N405D2.009	.1	.0	.0	.0	.01	50.0	33.0	1.0	.2	0.	0.	0.	0.	0.	.26
N405D2.008	.1	.0	.0	.0	.00	50.0	28.0	1.0	.2	0.	0.	0.	0.	0.	.07
N405D2.007	.6	.0	57.8	.0	.03	50.0	25.0	1.0	1.5	0.	0.	356.	0.	0.	.57
N405D2.006	.5	.0	57.8	.0	.01	50.0	22.0	1.0	1.5	0.	0.	356.	0.	0.	.42
N405D2.005	.9	.0	50.2	.0	.14	50.0	11.0	1.0	2.3	0.	0.	309.	0.	0.	2.39
N405D2.004	1.0	53.0	53.0	53.2	.30	50.0	.0	1.0	2.7	0.	0.	326.	0.	0.	4.92
N405D3.009	.2	.0	.0	.0	.00	50.0	33.0	1.0	.4	0.	0.	0.	0.	0.	.14
N405D3.008	.5	.0	47.3	.0	.01	50.0	28.0	1.0	1.4	0.	0.	291.	0.	0.	.30
N405D3.007	.5	.0	47.3	.0	.04	50.0	25.0	1.0	1.4	0.	0.	291.	0.	0.	.63
N405D3.006	.5	.0	37.2	.0	.05	50.0	22.0	1.0	1.4	0.	0.	229.	0.	0.	.91
N405D3.005	.6	.0	29.2	.0	.16	50.0	11.0	1.0	1.5	0.	0.	180.	0.	0.	2.59
N405D3.004	.7	.0	53.4	.0	.29	50.0	.0	1.0	1.9	0.	0.	329.	0.	0.	4.82
N405D4.009	.1	.0	.0	.0	.01	50.0	33.0	1.0	.1	0.	0.	0.	0.	0.	.24
N405D4.008	.1	.0	.0	.0	.00	50.0	28.0	1.0	.3	0.	0.	0.	0.	0.	.04
N405D4.007	.6	.0	40.3	.0	.02	50.0	25.0	1.0	1.6	0.	0.	248.	0.	0.	.45
N405D4.006	.7	.0	56.7	.0	.04	50.0	22.0	1.0	1.7	0.	0.	349.	0.	0.	.60
N405D4.005	.6	.0	43.3	.0	.10	50.0	11.0	1.0	1.5	0.	0.	267.	0.	0.	1.82
N405D4.004	.8	.0	42.0	.0	.25	50.0	.0	1.0	2.1	0.	0.	259.	0.	0.	4.17
N405D5.009	.1	.0	.0	.0	.02	50.0	33.0	1.0	.3	0.	0.	0.	0.	0.	.34
N405D5.008	.4	.0	52.8	.0	.01	50.0	28.0	1.0	1.2	0.	0.	325.	0.	0.	.31
N405D5.007	.4	.0	53.3	.0	.03	50.0	25.0	1.0	1.2	0.	0.	329.	0.	0.	.54
N405D5.006	.6	.0	49.9	.0	.05	50.0	22.0	1.0	1.6	0.	0.	307.	0.	0.	.90
N405D5.005	.6	.0	53.5	.0	.16	50.0	11.0	1.0	1.7	0.	0.	330.	0.	0.	2.75
N405D5.004	.7	.0	47.2	.0	.29	50.0	.0	1.0	1.9	0.	0.	291.	0.	0.	4.78
N405E1.009	.1	.0	.0	.0	.03	50.0	33.0	5.0	.3	0.	0.	0.	0.	0.	.48
N405E1.008	.5	.0	45.7	.0	.04	50.0	28.0	5.0	1.3	0.	0.	281.	0.	0.	.64
N405E1.007	.6	.0	44.6	.0	.04	50.0	25.0	5.0	1.5	0.	0.	275.	0.	0.	.70
N405E1.006	.7	.0	54.2	.0	.07	50.0	22.0	5.0	1.9	0.	0.	334.	0.	0.	1.23
N405E1.005	.8	.0	45.9	.0	.19	50.0	11.0	5.0	2.0	0.	0.	283.	0.	0.	3.15
N405E1.004	.8	.0	46.6	.0	.26	50.0	.0	5.0	2.2	0.	0.	287.	0.	0.	4.40

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405E2.009	.1	.0	.0	.0	.01	50.0	33.0	5.0	.1	0.	0.	0.	0.	0.	.23
N405E2.008	.7	.0	54.7	.0	.00	50.0	28.0	5.0	2.0	0.	0.	337.	0.	0.	.28
N405E2.007	.5	.0	44.8	.0	.01	50.0	25.0	5.0	1.3	0.	0.	276.	0.	0.	.26
N405E2.006	1.0	46.1	46.1	46.1	.06	50.0	22.0	5.0	2.8	0.	0.	284.	0.	0.	.98
N405E2.005	.9	.0	46.4	.0	.18	50.0	11.0	5.0	2.3	0.	0.	286.	0.	0.	3.04
N405E2.004	.8	.0	23.7	.0	.27	50.0	.0	5.0	2.1	0.	0.	146.	0.	0.	4.59
N405E3.009	.1	.0	.0	.0	.01	50.0	33.0	5.0	.3	0.	0.	0.	0.	0.	.16
N405E3.008	.5	.0	54.8	.0	.02	50.0	28.0	5.0	1.4	0.	0.	338.	0.	0.	.41
N405E3.007	.9	.0	54.9	.0	.02	50.0	25.0	5.0	2.4	0.	0.	338.	0.	0.	.35
N405E3.006	1.1	31.2	31.2	31.2	.03	50.0	22.0	5.0	2.8	0.	0.	192.	0.	0.	.67
N405E3.005	.9	.0	54.9	.0	.16	50.0	11.0	5.0	2.3	0.	0.	338.	0.	0.	2.66
N405E3.004	.7	.0	51.5	.0	.22	50.0	.0	5.0	1.9	0.	0.	317.	0.	0.	3.63
N405E4.009	.1	.0	.0	.0	-.01	50.0	33.0	5.0	.2	0.	0.	0.	0.	0.	.14
N405E4.008	.7	.0	55.9	.0	.00	50.0	28.0	5.0	1.8	0.	0.	344.	0.	0.	.12
N405E4.007	.6	.0	43.5	.0	.02	50.0	25.0	5.0	1.6	0.	0.	268.	0.	0.	.45
N405E4.006	.8	.0	39.3	.0	.03	50.0	22.0	5.0	2.2	0.	0.	242.	0.	0.	.51
N405E4.005	.7	.0	39.4	.0	.18	50.0	11.0	5.0	1.8	0.	0.	243.	0.	0.	2.96
N405E4.004	.7	.0	33.7	.0	.23	50.0	.0	5.0	1.8	0.	0.	207.	0.	0.	3.90
N405E5.009	.1	.0	.0	.0	.02	50.0	33.0	5.0	.2	0.	0.	0.	0.	0.	.36
N405E5.008	.3	.0	44.3	.0	.03	50.0	28.0	5.0	.7	0.	0.	273.	0.	0.	.51
N405E5.007	.5	.0	55.1	.0	.03	50.0	25.0	5.0	1.3	0.	0.	340.	0.	0.	.49
N405E5.006	1.5	50.0	50.0	50.6	.04	50.0	22.0	5.0	4.0	0.	0.	308.	0.	0.	.77
N405E5.005	.9	.0	50.8	.0	.18	50.0	11.0	5.0	2.3	0.	0.	313.	0.	0.	3.05
N405E5.004	.8	.0	43.9	.0	.27	50.0	.0	5.0	2.2	0.	0.	271.	0.	0.	4.57
N405F1.009	.7	.0	45.7	.0	.01	50.0	33.0	11.0	1.8	0.	0.	282.	0.	0.	.09
N405F1.008	.9	.0	42.6	.0	.01	50.0	28.0	11.0	2.3	0.	0.	263.	0.	0.	.31
N405F1.007	1.1	37.1	37.1	37.2	.03	50.0	25.0	11.0	3.0	0.	0.	229.	0.	0.	.75
N405F1.006	1.1	37.0	37.0	37.8	.10	50.0	22.0	11.0	2.8	0.	0.	228.	0.	0.	1.77
N405F1.005	1.0	46.6	46.6	46.6	.24	50.0	11.0	11.0	2.7	0.	0.	287.	0.	0.	4.05
N405F1.004	.9	.0	31.8	.0	.22	50.0	.0	11.0	2.3	0.	0.	196.	0.	0.	3.70
N405F2.009	.0	.0	.0	.0	-.02	50.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.06
N405F2.008	.6	.0	22.3	.0	.00	50.0	28.0	11.0	1.6	0.	0.	138.	0.	0.	.30
N405F2.007	.9	.0	43.9	.0	.01	50.0	25.0	11.0	2.5	0.	0.	271.	0.	0.	.23
N405F2.006	1.3	42.8	52.8	53.2	.08	50.0	22.0	11.0	3.5	0.	0.	325.	0.	0.	1.39
N405F2.005	1.1	48.1	51.0	51.1	.21	50.0	11.0	11.0	2.8	0.	0.	314.	0.	0.	3.50
N405F2.004	1.2	51.1	51.1	51.2	.25	50.0	.0	11.0	3.1	0.	0.	315.	0.	0.	4.18
N405F3.009	.1	.0	.0	.0	.00	50.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.08
N405F3.008	.4	.0	62.7	.0	-.02	50.0	28.0	11.0	1.1	0.	0.	386.	0.	0.	.05
N405F3.007	.9	.0	43.4	.0	.02	50.0	25.0	11.0	2.3	0.	0.	267.	0.	0.	.56
N405F3.006	1.2	43.4	43.4	52.2	.05	50.0	22.0	11.0	3.2	0.	0.	267.	0.	0.	1.08
N405F3.005	.9	.0	52.6	.0	.20	50.0	11.0	11.0	2.3	0.	0.	324.	0.	0.	3.41
N405F3.004	.9	.0	38.6	.0	.23	50.0	.0	11.0	2.4	0.	0.	238.	0.	0.	3.85

FALCON 4: LSR = 50, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405F4.009	.1	.0	.0	.0	.01	50.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.13
N405F4.008	1.3	44.0	44.0	44.1	.01	50.0	28.0	11.0	3.3	0.	0.	271.	0.	0.	.11
N405F4.007	1.0	44.0	44.0	44.1	.04	50.0	25.0	11.0	2.8	0.	0.	271.	0.	0.	.76
N405F4.006	1.0	35.0	35.0	46.9	.08	50.0	22.0	11.0	2.8	0.	0.	215.	0.	0.	1.42
N405F4.005	1.1	42.3	42.3	42.8	.23	50.0	11.0	11.0	2.9	0.	0.	260.	0.	0.	3.88
N405F4.004	1.2	46.4	46.5	46.5	.26	50.0	.0	11.0	3.2	0.	0.	286.	0.	0.	4.40
N405F5.009	.0	.0	.0	.0	-.03	50.0	33.0	11.0	.0	0.	0.	0.	0.	0.	.00
N405F5.008	1.1	55.4	55.4	55.5	.01	50.0	28.0	11.0	3.0	0.	0.	341.	0.	0.	.13
N405F5.007	.9	.0	33.1	.0	-.03	50.0	25.0	11.0	2.5	0.	0.	204.	0.	0.	.32
N405F5.006	1.2	18.9	39.4	52.8	.07	50.0	22.0	11.0	3.1	0.	0.	243.	0.	0.	1.21
N405F5.005	1.0	54.2	54.2	54.2	.19	50.0	11.0	11.0	2.8	0.	0.	334.	0.	0.	3.21
N405F5.004	.8	.0	39.0	.0	.24	50.0	.0	11.0	2.3	0.	0.	240.	0.	0.	4.08
N405G1.009	.3	.0	81.8	.0	.01	50.0	33.0	17.0	.9	0.	0.	504.	0.	0.	.28
N405G1.008	.9	.0	56.0	.0	.01	50.0	28.0	17.0	2.3	0.	0.	345.	0.	0.	.29
N405G1.007	1.2	45.4	45.5	45.6	.02	50.0	25.0	17.0	3.3	0.	0.	280.	0.	0.	.63
N405G1.006	1.4	44.8	45.0	45.6	.08	50.0	22.0	17.0	3.7	0.	0.	277.	0.	0.	1.44
N405G1.005	1.0	34.0	34.0	34.0	.14	50.0	11.0	17.0	2.7	0.	0.	209.	0.	0.	2.48
N405G1.004	1.3	53.0	55.7	55.9	.11	50.0	.0	17.0	3.3	0.	0.	343.	0.	0.	2.16
N405G2.009	.0	.0	.0	.0	-.01	50.0	33.0	17.0	.1	0.	0.	0.	0.	0.	.05
N405G2.008	.6	.0	42.2	.0	-.01	50.0	28.0	17.0	1.6	0.	0.	260.	0.	0.	.15
N405G2.007	1.0	47.1	47.1	47.2	.04	50.0	25.0	17.0	2.7	0.	0.	290.	0.	0.	.82
N405G2.006	1.0	.0	53.6	.0	.08	50.0	22.0	17.0	2.5	0.	0.	330.	0.	0.	1.40
N405G2.005	1.4	44.8	44.8	44.8	.21	50.0	11.0	17.0	3.8	0.	0.	276.	0.	0.	3.46
N405G2.004	1.0	34.8	34.8	34.9	.13	50.0	.0	17.0	2.7	0.	0.	214.	0.	0.	2.37
N405G3.009	.0	.0	.0	.0	-.01	50.0	33.0	17.0	.1	0.	0.	0.	0.	0.	.06
N405G3.008	.7	.0	34.9	.0	.00	50.0	28.0	17.0	1.8	0.	0.	215.	0.	0.	.08
N405G3.007	1.2	44.9	44.9	44.9	.04	50.0	25.0	17.0	3.3	0.	0.	276.	0.	0.	.81
N405G3.006	1.4	21.9	47.8	52.7	.07	50.0	22.0	17.0	3.6	0.	0.	294.	0.	0.	1.29
N405G3.005	1.1	50.1	50.9	51.0	.15	50.0	11.0	17.0	3.0	0.	0.	314.	0.	0.	2.54
N405G3.004	1.1	54.3	54.3	54.4	.13	50.0	.0	17.0	2.9	0.	0.	334.	0.	0.	2.35
N405G4.009	.1	.0	.0	.0	.00	50.0	33.0	17.0	.1	0.	0.	0.	0.	0.	.03
N405G4.008	1.1	50.8	50.8	50.9	.00	50.0	28.0	17.0	3.0	0.	0.	313.	0.	0.	.06
N405G4.007	1.1	44.6	50.9	51.0	.01	50.0	25.0	17.0	2.8	0.	0.	314.	0.	0.	.32
N405G4.006	1.3	47.9	47.9	54.9	.05	50.0	22.0	17.0	3.4	0.	0.	295.	0.	0.	1.08
N405G4.005	1.1	41.9	41.9	41.9	.17	50.0	11.0	17.0	2.8	0.	0.	258.	0.	0.	2.82
N405G4.004	1.2	54.5	56.2	56.4	.15	50.0	.0	17.0	3.1	0.	0.	346.	0.	0.	2.56
N405G5.009	.8	.0	58.3	.0	.00	50.0	33.0	17.0	2.2	0.	0.	359.	0.	0.	.01
N405G5.008	1.1	27.0	27.0	27.0	.01	50.0	28.0	17.0	2.8	0.	0.	166.	0.	0.	.29
N405G5.007	1.1	42.7	42.8	42.8	.02	50.0	25.0	17.0	2.8	0.	0.	264.	0.	0.	.39
N405G5.006	1.3	42.3	53.3	53.4	.06	50.0	22.0	17.0	3.4	0.	0.	328.	0.	0.	1.15
N405G5.005	1.2	53.1	53.1	53.3	.14	50.0	11.0	17.0	3.3	0.	0.	327.	0.	0.	2.46
N405G5.004	1.2	48.0	48.0	50.1	.15	50.0	.0	17.0	3.2	0.	0.	296.	0.	0.	2.61

FALCON 4: LSR = 50, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405H1.009	1.0	.0	56.1	.0	.33	50.0	-25.0	1.0	2.6	0.	0.	345.	0.	0.	5.47
N405H1.008	.8	.0	37.8	.0	.28	50.0	-28.0	1.0	2.2	0.	0.	233.	0.	0.	4.72
N405H1.007	.9	.0	47.6	.0	.26	50.0	-33.0	1.0	2.3	0.	0.	293.	0.	0.	4.41
N405H1.006	1.0	.0	37.2	.0	.19	50.0	-50.0	1.0	2.5	0.	0.	229.	0.	0.	3.13
N405H1.005	.9	.0	52.0	.0	.17	50.0	-56.0	1.0	2.5	0.	0.	321.	0.	0.	2.86
N405H1.004	.4	.0	51.0	.0	.01	50.0	-66.0	1.0	1.2	0.	0.	314.	0.	0.	.60
N405H2.009	1.0	46.0	46.0	46.1	.32	50.0	-25.0	1.0	2.7	0.	0.	284.	0.	0.	5.31
N405H2.008	.9	.0	46.1	.0	.27	50.0	-28.0	1.0	2.4	0.	0.	284.	0.	0.	4.44
N405H2.007	.8	.0	54.0	.0	.28	50.0	-33.0	1.0	2.2	0.	0.	332.	0.	0.	4.62
N405H2.006	.8	.0	49.2	.0	.19	50.0	-50.0	1.0	2.1	0.	0.	303.	0.	0.	3.12
N405H2.005	.8	.0	46.3	.0	.14	50.0	-56.0	1.0	2.0	0.	0.	285.	0.	0.	2.44
N405H2.004	.8	.0	45.9	.0	.09	50.0	-66.0	1.0	2.2	0.	0.	283.	0.	0.	1.61
N405H3.009	.9	.0	52.6	.0	.36	50.0	-25.0	1.0	2.5	0.	0.	324.	0.	0.	5.92
N405H3.008	.9	.0	53.0	.0	.29	50.0	-28.0	1.0	2.4	0.	0.	327.	0.	0.	4.92
N405H3.007	.9	.0	47.5	.0	.31	50.0	-33.0	1.0	2.4	0.	0.	293.	0.	0.	5.17
N405H3.006	.8	.0	52.5	.0	.18	50.0	-50.0	1.0	2.2	0.	0.	323.	0.	0.	3.07
N405H3.005	.9	.0	52.6	.0	.14	50.0	-56.0	1.0	2.4	0.	0.	324.	0.	0.	2.45
N405H3.004	.6	.0	46.5	.0	.05	50.0	-66.0	1.0	1.7	0.	0.	286.	0.	0.	1.10
N405H4.009	.9	.0	51.3	.0	.32	50.0	-25.0	1.0	2.5	0.	0.	316.	0.	0.	5.27
N405H4.008	.8	.0	37.4	.0	.26	50.0	-28.0	1.0	2.2	0.	0.	230.	0.	0.	4.37
N405H4.007	.8	.0	37.4	.0	.28	50.0	-33.0	1.0	2.1	0.	0.	230.	0.	0.	4.59
N405H4.006	.8	.0	53.6	.0	.21	50.0	-50.0	1.0	2.2	0.	0.	330.	0.	0.	3.57
N405H4.005	.8	.0	49.2	.0	.19	50.0	-56.0	1.0	2.1	0.	0.	303.	0.	0.	3.12
N405H4.004	.8	.0	49.3	.0	.06	50.0	-66.0	1.0	2.1	0.	0.	303.	0.	0.	1.09
N405H5.009	1.1	50.3	50.5	55.3	.33	50.0	-25.0	1.0	2.8	0.	0.	311.	0.	0.	5.55
N405H5.008	.9	.0	50.4	.0	.30	50.0	-28.0	1.0	2.5	0.	0.	311.	0.	0.	5.03
N405H5.007	.9	.0	55.5	.0	.31	50.0	-33.0	1.0	2.4	0.	0.	342.	0.	0.	5.17
N405H5.006	1.0	.0	55.6	.0	.21	50.0	-50.0	1.0	2.6	0.	0.	342.	0.	0.	3.53
N405H5.005	.8	.0	55.1	.0	.15	50.0	-56.0	1.0	2.0	0.	0.	339.	0.	0.	2.56
N405H5.004	.8	.0	49.7	.0	.09	50.0	-66.0	1.0	2.3	0.	0.	306.	0.	0.	1.59
N405I1.009	1.0	46.0	46.0	46.1	.28	50.0	-25.0	5.0	2.7	0.	0.	284.	0.	0.	4.62
N405I1.008	.8	.0	46.3	.0	.24	50.0	-28.0	5.0	2.1	0.	0.	285.	0.	0.	3.99
N405I1.007	.9	.0	57.3	.0	.24	50.0	-33.0	5.0	2.5	0.	0.	353.	0.	0.	4.08
N405I1.006	.8	.0	56.4	.0	.13	50.0	-50.0	5.0	2.1	0.	0.	348.	0.	0.	2.25
N405I1.005	.9	.0	56.9	.0	.06	50.0	-56.0	5.0	2.3	0.	0.	351.	0.	0.	1.28
N405I1.004	.8	.0	57.0	.0	.06	50.0	-66.0	5.0	2.2	0.	0.	351.	0.	0.	1.00
N405I2.009	1.0	42.3	42.3	42.3	.35	50.0	-25.0	5.0	2.8	0.	0.	261.	0.	0.	5.87
N405I2.008	.9	.0	61.9	.0	.31	50.0	-28.0	5.0	2.4	0.	0.	381.	0.	0.	5.16
N405I2.007	.9	.0	46.0	.0	.33	50.0	-33.0	5.0	2.4	0.	0.	283.	0.	0.	5.43
N405I2.006	.9	.0	36.8	.0	.17	50.0	-50.0	5.0	2.3	0.	0.	227.	0.	0.	2.80
N405I2.005	.7	.0	36.8	.0	.12	50.0	-56.0	5.0	1.8	0.	0.	226.	0.	0.	1.96
N405I2.004	.7	.0	50.6	.0	.09	50.0	-66.0	5.0	1.9	0.	0.	312.	0.	0.	1.49

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405I3.009	.9	.0	50.6	.0	.36	50.0	-25.0	5.0	2.3	0.	0.	312.	0.	0.	6.01
N405I3.008	.8	.0	50.5	.0	.30	50.0	-28.0	5.0	2.1	0.	0.	311.	0.	0.	5.00
N405I3.007	.9	.0	42.5	.0	.29	50.0	-33.0	5.0	2.4	0.	0.	262.	0.	0.	4.78
N405I3.006	.8	.0	33.9	.0	.15	50.0	-50.0	5.0	2.1	0.	0.	209.	0.	0.	2.55
N405I3.005	.7	.0	28.8	.0	.13	50.0	-56.0	5.0	1.9	0.	0.	178.	0.	0.	2.08
N405I3.004	.7	.0	50.0	.0	.05	50.0	-66.0	5.0	1.8	0.	0.	308.	0.	0.	1.10
N405I4.009	1.1	47.9	47.9	48.0	.33	50.0	-25.0	5.0	3.0	0.	0.	295.	0.	0.	5.43
N405I4.008	1.0	.0	47.8	.0	.30	50.0	-28.0	5.0	2.6	0.	0.	294.	0.	0.	5.06
N405I4.007	1.1	39.8	39.8	39.9	.28	50.0	-33.0	5.0	2.8	0.	0.	245.	0.	0.	4.58
N405I4.006	.8	.0	54.7	.0	.15	50.0	-50.0	5.0	2.1	0.	0.	337.	0.	0.	2.54
N405I4.005	.7	.0	37.9	.0	.11	50.0	-56.0	5.0	1.9	0.	0.	233.	0.	0.	1.84
N405I4.004	.7	.0	49.6	.0	.07	50.0	-66.0	5.0	1.8	0.	0.	305.	0.	0.	1.25
N405I5.009	.8	.0	34.9	.0	.32	50.0	-25.0	5.0	2.2	0.	0.	215.	0.	0.	5.39
N405I5.008	.8	.0	41.9	.0	.27	50.0	-28.0	5.0	2.2	0.	0.	258.	0.	0.	4.47
N405I5.007	.9	.0	56.9	.0	.30	50.0	-33.0	5.0	2.3	0.	0.	350.	0.	0.	5.01
N405I5.006	.8	.0	56.0	.0	.19	50.0	-50.0	5.0	2.1	0.	0.	345.	0.	0.	3.08
N405I5.005	.7	.0	31.5	.0	.11	50.0	-56.0	5.0	1.9	0.	0.	194.	0.	0.	1.92
N405I5.004	.6	.0	31.2	.0	.06	50.0	-66.0	5.0	1.5	0.	0.	192.	0.	0.	1.14
N405J1.009	.9	.0	52.4	.0	.19	50.0	-25.0	11.0	2.5	0.	0.	322.	0.	0.	3.28
N405J1.008	.8	.0	54.6	.0	.21	50.0	-28.0	11.0	2.2	0.	0.	336.	0.	0.	3.55
N405J1.007	.9	.0	58.5	.0	.23	50.0	-33.0	11.0	2.3	0.	0.	360.	0.	0.	3.90
N405J1.006	.9	.0	53.4	.0	.16	50.0	-50.0	11.0	2.4	0.	0.	329.	0.	0.	2.72
N405J1.005	.8	.0	53.5	.0	.08	50.0	-56.0	11.0	2.1	0.	0.	329.	0.	0.	1.47
N405J1.004	.7	.0	50.3	.0	.05	50.0	-66.0	11.0	1.8	0.	0.	310.	0.	0.	.97
N405J2.009	1.1	42.5	42.5	57.3	.27	50.0	-25.0	11.0	2.9	0.	0.	262.	0.	0.	4.49
N405J2.008	.9	.0	42.8	.0	.25	50.0	-28.0	11.0	2.5	0.	0.	263.	0.	0.	4.06
N405J2.007	1.0	61.3	61.3	61.3	.24	50.0	-33.0	11.0	2.7	0.	0.	378.	0.	0.	3.98
N405J2.006	.8	.0	40.4	.0	.09	50.0	-50.0	11.0	2.1	0.	0.	249.	0.	0.	1.69
N405J2.005	.8	.0	50.2	.0	.05	50.0	-56.0	11.0	2.2	0.	0.	309.	0.	0.	.95
N405J2.004	.5	.0	43.3	.0	.01	50.0	-66.0	11.0	1.2	0.	0.	267.	0.	0.	.43
N405J3.009	1.0	.0	41.9	.0	.26	50.0	-25.0	11.0	2.6	0.	0.	258.	0.	0.	4.31
N405J3.008	.8	.0	31.2	.0	.23	50.0	-28.0	11.0	2.2	0.	0.	192.	0.	0.	3.88
N405J3.007	1.0	30.8	30.8	30.9	.23	50.0	-33.0	11.0	2.7	0.	0.	190.	0.	0.	3.76
N405J3.006	.8	.0	39.6	.0	.09	50.0	-50.0	11.0	2.1	0.	0.	244.	0.	0.	1.74
N405J3.005	.8	.0	52.3	.0	.05	50.0	-56.0	11.0	2.0	0.	0.	322.	0.	0.	.92
N405J3.004	.4	.0	41.2	.0	.01	50.0	-66.0	11.0	1.2	0.	0.	254.	0.	0.	.37
N405J4.009	1.0	45.8	45.8	45.8	.26	50.0	-25.0	11.0	2.7	0.	0.	282.	0.	0.	4.28
N405J4.008	.9	.0	41.0	.0	.24	50.0	-28.0	11.0	2.4	0.	0.	253.	0.	0.	4.06
N405J4.007	1.0	.0	40.5	.0	.26	50.0	-33.0	11.0	2.6	0.	0.	249.	0.	0.	4.22
N405J4.006	1.3	53.8	53.9	54.1	.16	50.0	-50.0	11.0	3.4	0.	0.	332.	0.	0.	2.59
N405J4.005	.8	.0	40.1	.0	.07	50.0	-56.0	11.0	2.0	0.	0.	247.	0.	0.	1.21
N405J4.004	.6	.0	40.7	.0	.03	50.0	-66.0	11.0	1.6	0.	0.	251.	0.	0.	.52

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405J5.009	1.0	.0	63.1	.0	.25	50.0	-25.0	11.0	2.6	0.	0.	388.	0.	0.	4.14
N405J5.008	.9	.0	48.7	.0	.25	50.0	-28.0	11.0	2.4	0.	0.	300.	0.	0.	4.14
N405J5.007	1.0	47.9	47.9	48.0	.23	50.0	-33.0	11.0	2.7	0.	0.	295.	0.	0.	3.89
N405J5.006	1.0	49.9	49.9	49.9	.15	50.0	-50.0	11.0	2.7	0.	0.	307.	0.	0.	2.56
N405J5.005	.7	.0	53.3	.0	.09	50.0	-56.0	11.0	1.9	0.	0.	328.	0.	0.	1.53
N405J5.004	.7	.0	53.7	.0	.04	50.0	-66.0	11.0	1.7	0.	0.	331.	0.	0.	.71
N405K1.009	1.0	43.6	43.6	43.6	.13	50.0	-25.0	17.0	2.7	0.	0.	269.	0.	0.	2.39
N405K1.008	1.0	43.7	43.7	43.7	.17	50.0	-28.0	17.0	2.7	0.	0.	269.	0.	0.	2.97
N405K1.007	.9	.0	50.0	.0	.16	50.0	-33.0	17.0	2.3	0.	0.	308.	0.	0.	2.90
N405K1.006	1.0	40.6	40.6	40.7	.09	50.0	-50.0	17.0	2.7	0.	0.	250.	0.	0.	1.57
N405K1.005	.7	.0	58.7	.0	.00	50.0	-56.0	17.0	1.9	0.	0.	361.	0.	0.	.53
N405K1.004	.4	.0	37.0	.0	-.01	50.0	-66.0	17.0	1.2	0.	0.	228.	0.	0.	.13
N405K2.009	.8	.0	49.6	.0	.10	50.0	-25.0	17.0	2.1	0.	0.	305.	0.	0.	2.10
N405K2.008	.8	.0	43.1	.0	.12	50.0	-28.0	17.0	2.0	0.	0.	265.	0.	0.	2.19
N405K2.007	.8	.0	61.0	.0	.12	50.0	-33.0	17.0	2.2	0.	0.	376.	0.	0.	2.27
N405K2.006	.9	.0	55.4	.0	.08	50.0	-50.0	17.0	2.3	0.	0.	341.	0.	0.	1.60
N405K2.005	.8	.0	45.2	.0	.03	50.0	-56.0	17.0	2.0	0.	0.	278.	0.	0.	.76
N405K2.004	.5	.0	31.1	.0	-.01	50.0	-66.0	17.0	1.3	0.	0.	192.	0.	0.	.10
N405K3.009	1.2	49.3	49.3	49.5	.13	50.0	-25.0	17.0	3.1	0.	0.	304.	0.	0.	2.34
N405K3.008	1.4	44.2	49.4	49.5	.15	50.0	-28.0	17.0	3.8	0.	0.	304.	0.	0.	2.63
N405K3.007	.8	.0	49.8	.0	.13	50.0	-33.0	17.0	2.2	0.	0.	306.	0.	0.	2.42
N405K3.006	1.0	.0	43.0	.0	.11	50.0	-50.0	17.0	2.6	0.	0.	265.	0.	0.	1.98
N405K3.005	.8	.0	49.6	.0	.06	50.0	-56.0	17.0	2.1	0.	0.	305.	0.	0.	.97
N405K3.004	.7	.0	54.1	.0	.02	50.0	-66.0	17.0	2.0	0.	0.	333.	0.	0.	.37
N405K5.009	1.0	52.4	52.4	52.4	.15	50.0	-25.0	17.0	2.7	0.	0.	323.	0.	0.	2.74
N405K5.008	.9	.0	52.5	.0	.16	50.0	-28.0	17.0	2.4	0.	0.	323.	0.	0.	2.78
N405K5.007	1.0	.0	51.8	.0	.17	50.0	-33.0	17.0	2.6	0.	0.	319.	0.	0.	3.00
N405K5.006	1.0	57.0	57.0	57.0	.07	50.0	-50.0	17.0	2.7	0.	0.	351.	0.	0.	1.36
N405K5.005	.9	.0	52.7	.0	.00	50.0	-56.0	17.0	2.4	0.	0.	325.	0.	0.	.52
N405K5.004	.5	.0	35.6	.0	-.03	50.0	-66.0	17.0	1.3	0.	0.	220.	0.	0.	.06
N405L1.009	.1	.0	.0	.0	.04	150.0	33.0	1.0	.3	0.	0.	0.	0.	0.	.61
N405L1.008	.2	.0	.0	.0	-.01	150.0	28.0	1.0	.5	0.	0.	0.	0.	0.	.12
N405L1.007	.3	.0	36.8	.0	.01	150.0	25.0	1.0	.8	0.	0.	227.	0.	0.	.18
N405L1.006	.3	.0	36.8	.0	.01	150.0	22.0	1.0	.7	0.	0.	227.	0.	0.	.27
N405L1.005	.4	.0	48.6	.0	.07	150.0	11.0	1.0	1.1	0.	0.	299.	0.	0.	1.21
N405L1.004	.5	.0	48.5	.0	.13	150.0	.0	1.0	1.4	0.	0.	299.	0.	0.	2.25
N405L2.009	.0	.0	.0	.0	-.03	150.0	33.0	1.0	.1	0.	0.	0.	0.	0.	.03
N405L2.008	.1	.0	.0	.0	.00	150.0	28.0	1.0	.1	0.	0.	0.	0.	0.	.31
N405L2.007	.3	.0	58.6	.0	.00	150.0	25.0	1.0	.8	0.	0.	361.	0.	0.	.33
N405L2.006	.4	.0	58.8	.0	-.01	150.0	22.0	1.0	1.0	0.	0.	362.	0.	0.	.14
N405L2.005	.5	.0	53.6	.0	.04	150.0	11.0	1.0	1.3	0.	0.	330.	0.	0.	.70
N405L2.004	.5	.0	53.1	.0	.12	150.0	.0	1.0	1.4	0.	0.	327.	0.	0.	2.05

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405L3.009	.0	.0	.0	.0	-.02	150.0	33.0	1.0	.1	0.	0.	0.	0.	0.	.04
N405L3.008	.1	.0	.0	.0	-.02	150.0	28.0	1.0	.4	0.	0.	0.	0.	0.	.13
N405L3.007	.3	.0	51.5	.0	-.01	150.0	25.0	1.0	.7	0.	0.	317.	0.	0.	.31
N405L3.006	.3	.0	51.3	.0	.02	150.0	22.0	1.0	.8	0.	0.	316.	0.	0.	.42
N405L3.005	.5	.0	51.3	.0	.08	150.0	11.0	1.0	1.4	0.	0.	316.	0.	0.	1.44
N405L3.004	.5	.0	50.0	.0	.11	150.0	.0	1.0	1.4	0.	0.	308.	0.	0.	1.97
N405L4.009	.1	.0	.0	.0	-.01	150.0	33.0	1.0	.2	0.	0.	0.	0.	0.	.09
N405L4.008	.2	.0	.0	.0	-.01	150.0	28.0	1.0	.5	0.	0.	0.	0.	0.	.05
N405L4.007	.3	.0	36.7	.0	.00	150.0	25.0	1.0	.8	0.	0.	226.	0.	0.	.11
N405L4.006	.3	.0	36.7	.0	.00	150.0	22.0	1.0	.8	0.	0.	226.	0.	0.	.22
N405L4.005	.5	.0	59.5	.0	.06	150.0	11.0	1.0	1.4	0.	0.	367.	0.	0.	1.13
N405L4.004	.5	.0	55.7	.0	.13	150.0	.0	1.0	1.3	0.	0.	343.	0.	0.	2.12
N405L5.009	.0	.0	.0	.0	-.01	150.0	33.0	1.0	.1	0.	0.	0.	0.	0.	.22
N405L5.008	.1	.0	.0	.0	.00	150.0	28.0	1.0	.3	0.	0.	0.	0.	0.	.04
N405L5.007	.1	.0	.0	.0	.00	150.0	25.0	1.0	.3	0.	0.	0.	0.	0.	.22
N405L5.006	.3	.0	57.3	.0	.04	150.0	22.0	1.0	.9	0.	0.	353.	0.	0.	.68
N405L5.005	.4	.0	68.3	.0	.11	150.0	11.0	1.0	1.1	0.	0.	421.	0.	0.	1.75
N405L5.004	.4	.0	43.6	.0	.14	150.0	.0	1.0	1.1	0.	0.	269.	0.	0.	2.36
N405M1.009	.0	.0	.0	.0	.00	150.0	33.0	5.0	.1	0.	0.	0.	0.	0.	.24
N405M1.008	.1	.0	.0	.0	.00	150.0	28.0	5.0	.3	0.	0.	0.	0.	0.	.05
N405M1.007	.2	.0	63.5	.0	.00	150.0	25.0	5.0	.6	0.	0.	391.	0.	0.	.08
N405M1.006	.2	.0	37.6	.0	.01	150.0	22.0	5.0	.6	0.	0.	232.	0.	0.	.13
N405M1.005	.4	.0	48.7	.0	.05	150.0	11.0	5.0	1.0	0.	0.	300.	0.	0.	.85
N405M1.004	.4	.0	39.9	.0	.13	150.0	.0	5.0	1.2	0.	0.	246.	0.	0.	2.18
N405M2.009	.2	.0	.0	.0	.00	150.0	33.0	5.0	.4	0.	0.	0.	0.	0.	.03
N405M2.008	.1	.0	.0	.0	.01	150.0	28.0	5.0	.4	0.	0.	0.	0.	0.	.34
N405M2.007	.2	.0	50.9	.0	.01	150.0	25.0	5.0	.6	0.	0.	313.	0.	0.	.14
N405M2.006	.2	.0	51.8	.0	.01	150.0	22.0	5.0	.6	0.	0.	319.	0.	0.	.20
N405M2.005	.3	.0	51.3	.0	.04	150.0	11.0	5.0	.9	0.	0.	316.	0.	0.	.63
N405M2.004	.4	.0	55.1	.0	.11	150.0	.0	5.0	1.1	0.	0.	339.	0.	0.	1.88
N405M3.009	.1	.0	.0	.0	.03	150.0	33.0	5.0	.2	0.	0.	0.	0.	0.	.53
N405M3.008	.2	.0	.0	.0	.04	150.0	28.0	5.0	.5	0.	0.	0.	0.	0.	.63
N405M3.007	.1	.0	.0	.0	.01	150.0	25.0	5.0	.4	0.	0.	0.	0.	0.	.25
N405M3.006	.3	.0	71.1	.0	.05	150.0	22.0	5.0	.9	0.	0.	438.	0.	0.	.76
N405M3.005	.4	.0	64.6	.0	.04	150.0	11.0	5.0	1.0	0.	0.	398.	0.	0.	.82
N405M3.004	.5	.0	55.2	.0	.15	150.0	.0	5.0	1.3	0.	0.	340.	0.	0.	2.50
N405M4.009	.0	.0	.0	.0	-.01	150.0	33.0	5.0	.0	0.	0.	0.	0.	0.	.01
N405M4.008	.1	.0	.0	.0	.00	150.0	28.0	5.0	.1	0.	0.	0.	0.	0.	.07
N405M4.007	.2	.0	.0	.0	-.01	150.0	25.0	5.0	.4	0.	0.	0.	0.	0.	.31
N405M4.006	.2	.0	.0	.0	.00	150.0	22.0	5.0	.5	0.	0.	0.	0.	0.	.11
N405M4.005	.4	.0	51.8	.0	.04	150.0	11.0	5.0	1.1	0.	0.	319.	0.	0.	.88
N405M4.004	.5	.0	56.1	.0	.13	150.0	.0	5.0	1.4	0.	0.	345.	0.	0.	2.20

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS: PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PROTOTYPE CONDITIONS: PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405M5.009	.2	.0	.0	.0	-.02	150.0	33.0	5.0	.4	0.	0.	0.	0.	0.	.05
N405M5.008	.2	.0	.0	.0	-.01	150.0	28.0	5.0	.5	0.	0.	0.	0.	0.	.04
N405M5.007	.2	.0	.0	.0	-.01	150.0	25.0	5.0	.5	0.	0.	0.	0.	0.	.18
N405M5.006	.3	.0	68.1	.0	.00	150.0	22.0	5.0	.7	0.	0.	419.	0.	0.	.18
N405M5.005	.4	.0	50.9	.0	.02	150.0	11.0	5.0	.9	0.	0.	314.	0.	0.	.48
N405M5.004	.5	.0	50.9	.0	.13	150.0	.0	5.0	1.2	0.	0.	314.	0.	0.	2.20
N405N1.009	.0	.0	.0	.0	.00	150.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.23
N405N1.008	.0	.0	.0	.0	.00	150.0	28.0	11.0	.0	0.	0.	0.	0.	0.	.00
N405N1.007	.1	.0	.0	.0	-.01	150.0	25.0	11.0	.1	0.	0.	0.	0.	0.	.24
N405N1.006	.2	.0	.0	.0	.00	150.0	22.0	11.0	.4	0.	0.	0.	0.	0.	.26
N405N1.005	.4	.0	52.0	.0	.04	150.0	11.0	11.0	1.0	0.	0.	320.	0.	0.	.68
N405N1.004	.5	.0	54.7	.0	.10	150.0	.0	11.0	1.2	0.	0.	337.	0.	0.	1.70
N405N2.009	.0	.0	.0	.0	.03	150.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.56
N405N2.008	.1	.0	.0	.0	.04	150.0	28.0	11.0	.3	0.	0.	0.	0.	0.	.69
N405N2.007	.1	.0	.0	.0	.00	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.06
N405N2.006	.2	.0	69.0	.0	.02	150.0	22.0	11.0	.6	0.	0.	425.	0.	0.	.32
N405N2.005	.5	.0	57.1	.0	.05	150.0	11.0	11.0	1.3	0.	0.	351.	0.	0.	.80
N405N2.004	.5	.0	51.9	.0	.12	150.0	.0	11.0	1.2	0.	0.	320.	0.	0.	2.00
N405N3.009	.1	.0	.0	.0	.00	150.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.00
N405N3.008	.1	.0	.0	.0	.00	150.0	28.0	11.0	.2	0.	0.	0.	0.	0.	.15
N405N3.007	.1	.0	.0	.0	.01	150.0	25.0	11.0	.4	0.	0.	0.	0.	0.	.09
N405N3.006	.3	.0	47.7	.0	.01	150.0	22.0	11.0	.9	0.	0.	294.	0.	0.	.28
N405N3.005	.4	.0	62.6	.0	.03	150.0	11.0	11.0	1.1	0.	0.	386.	0.	0.	.49
N405N3.004	.5	.0	62.5	.0	.11	150.0	.0	11.0	1.4	0.	0.	385.	0.	0.	1.80
N405N4.009	.0	.0	.0	.0	.00	150.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.00
N405N4.008	.1	.0	.0	.0	.00	150.0	28.0	11.0	.2	0.	0.	0.	0.	0.	.02
N405N4.007	.1	.0	.0	.0	.00	150.0	25.0	11.0	.3	0.	0.	0.	0.	0.	.26
N405N4.006	.2	.0	.0	.0	.00	150.0	22.0	11.0	.5	0.	0.	0.	0.	0.	.20
N405N4.005	.4	.0	45.7	.0	.05	150.0	11.0	11.0	1.0	0.	0.	281.	0.	0.	.86
N405N4.004	.6	.0	44.0	.0	.12	150.0	.0	11.0	1.7	0.	0.	271.	0.	0.	2.08
N405N5.009	.0	.0	.0	.0	.00	150.0	33.0	11.0	.1	0.	0.	0.	0.	0.	.27
N405N5.008	.1	.0	.0	.0	.01	150.0	28.0	11.0	.2	0.	0.	0.	0.	0.	.20
N405N5.007	.1	.0	.0	.0	-.01	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.01
N405N5.006	.3	.0	42.3	.0	.01	150.0	22.0	11.0	.8	0.	0.	261.	0.	0.	.23
N405N5.005	.6	.0	57.1	.0	.05	150.0	11.0	11.0	1.5	0.	0.	352.	0.	0.	1.02
N405N5.004	.5	.0	43.1	.0	.12	150.0	.0	11.0	1.3	0.	0.	265.	0.	0.	1.98
N405O1.009	.0	.0	.0	.0	.01	150.0	33.0	17.0	.1	0.	0.	0.	0.	0.	.22
N405O1.008	.0	.0	.0	.0	.01	150.0	28.0	17.0	.1	0.	0.	0.	0.	0.	.21
N405O1.007	.1	.0	.0	.0	.00	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.02
N405O1.006	.2	.0	.0	.0	.00	150.0	22.0	17.0	.5	0.	0.	0.	0.	0.	.08
N405O1.005	.4	.0	54.1	.0	.02	150.0	11.0	17.0	.9	0.	0.	333.	0.	0.	.34
N405O1.004	.4	.0	45.9	.0	.07	150.0	.0	17.0	1.0	0.	0.	283.	0.	0.	1.18

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N40502.009	.0	.0	.0	.0	-.04	150.0	33.0	17.0	.0	0.	0.	0.	0.	0.	.02
N40502.008	.1	.0	.0	.0	.00	150.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.00
N40502.007	.1	.0	.0	.0	.00	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.03
N40502.006	.1	.0	.0	.0	.00	150.0	22.0	17.0	.2	0.	0.	0.	0.	0.	.13
N40502.005	.4	.0	43.1	.0	.00	150.0	11.0	17.0	1.0	0.	0.	266.	0.	0.	.29
N40502.004	.4	.0	50.1	.0	.05	150.0	.0	17.0	1.1	0.	0.	309.	0.	0.	.98
N40503.009	.0	.0	.0	.0	-.01	150.0	33.0	17.0	.1	0.	0.	0.	0.	0.	.11
N40503.008	.1	.0	.0	.0	.00	150.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.00
N40503.007	.1	.0	.0	.0	.00	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.00
N40503.006	.2	.0	.0	.0	.00	150.0	22.0	17.0	.5	0.	0.	0.	0.	0.	.24
N40503.005	.3	.0	51.1	.0	.01	150.0	11.0	17.0	.8	0.	0.	315.	0.	0.	.16
N40503.004	.4	.0	49.3	.0	.04	150.0	.0	17.0	1.1	0.	0.	303.	0.	0.	.82
N40504.009	.0	.0	.0	.0	-.02	150.0	33.0	17.0	.1	0.	0.	0.	0.	0.	.03
N40504.008	.1	.0	.0	.0	.00	150.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.16
N40504.007	.2	.0	.0	.0	-.02	150.0	25.0	17.0	.4	0.	0.	0.	0.	0.	.04
N40504.006	.2	.0	50.9	.0	.00	150.0	22.0	17.0	.6	0.	0.	313.	0.	0.	.11
N40504.005	.4	.0	51.9	.0	.01	150.0	11.0	17.0	1.0	0.	0.	320.	0.	0.	.37
N40504.004	.5	.0	50.6	.0	.08	150.0	.0	17.0	1.4	0.	0.	312.	0.	0.	1.32
N40505.009	.0	.0	.0	.0	.00	150.0	33.0	17.0	.0	0.	0.	0.	0.	0.	.00
N40505.008	.0	.0	.0	.0	.00	150.0	28.0	17.0	.0	0.	0.	0.	0.	0.	.19
N40505.007	.1	.0	.0	.0	.01	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.16
N40505.006	.1	.0	.0	.0	.01	150.0	22.0	17.0	.3	0.	0.	0.	0.	0.	.10
N40505.005	.3	.0	59.2	.0	.01	150.0	11.0	17.0	.8	0.	0.	365.	0.	0.	.35
N40505.004	.4	.0	46.5	.0	.07	150.0	.0	17.0	1.2	0.	0.	287.	0.	0.	1.32
N405P1.009	.6	.0	55.3	.0	.14	150.0	-33.0	1.0	1.5	0.	0.	340.	0.	0.	2.42
N405P1.008	.6	.0	57.1	.0	.15	150.0	-28.0	1.0	1.5	0.	0.	352.	0.	0.	2.50
N405P1.007	.6	.0	60.5	.0	.20	150.0	-33.0	1.0	1.6	0.	0.	373.	0.	0.	3.29
N405P1.006	.6	.0	60.5	.0	.22	150.0	-50.0	1.0	1.6	0.	0.	373.	0.	0.	3.61
N405P1.005	.4	.0	60.4	.0	.13	150.0	-56.0	1.0	1.2	0.	0.	372.	0.	0.	2.20
N405P1.004	.5	.0	60.6	.0	.13	150.0	-66.0	1.0	1.5	0.	0.	373.	0.	0.	2.21
N405P2.009	.6	.0	56.7	.0	.20	150.0	-25.0	1.0	1.6	0.	0.	349.	0.	0.	3.39
N405P2.008	.5	.0	56.6	.0	.17	150.0	-28.0	1.0	1.4	0.	0.	349.	0.	0.	2.85
N405P2.007	.5	.0	56.7	.0	.15	150.0	-33.0	1.0	1.4	0.	0.	349.	0.	0.	2.63
N405P2.006	.5	.0	57.2	.0	.17	150.0	-50.0	1.0	1.4	0.	0.	352.	0.	0.	2.84
N405P2.005	.5	.0	41.5	.0	.19	150.0	-56.0	1.0	1.4	0.	0.	255.	0.	0.	3.18
N405P2.004	.5	.0	55.8	.0	.14	150.0	-66.0	1.0	1.3	0.	0.	344.	0.	0.	2.38
N405P3.009	.6	.0	61.1	.0	.19	150.0	-25.0	1.0	1.6	0.	0.	376.	0.	0.	3.21
N405P3.008	.6	.0	60.8	.0	.19	150.0	-28.0	1.0	1.6	0.	0.	375.	0.	0.	3.11
N405P3.007	.6	.0	60.8	.0	.22	150.0	-33.0	1.0	1.6	0.	0.	375.	0.	0.	3.57
N405P3.006	.5	.0	60.7	.0	.18	150.0	-50.0	1.0	1.4	0.	0.	374.	0.	0.	2.95
N405P3.005	.6	.0	48.0	.0	.18	150.0	-56.0	1.0	1.5	0.	0.	295.	0.	0.	3.05
N405P3.004	.5	.0	48.5	.0	.11	150.0	-66.0	1.0	1.4	0.	0.	299.	0.	0.	1.99

FALCON 4: LSR = 50, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405P4.009	.5	.0	50.9	.0	.18	150.0	-25.0	1.0	1.4	0.	0.	314.	0.	0.	3.03
N405P4.008	.5	.0	39.8	.0	.19	150.0	-28.0	1.0	1.3	0.	0.	245.	0.	0.	3.12
N405P4.007	.5	.0	49.6	.0	.19	150.0	-33.0	1.0	1.5	0.	0.	306.	0.	0.	3.12
N405P4.006	.5	.0	60.4	.0	.17	150.0	-50.0	1.0	1.4	0.	0.	372.	0.	0.	2.86
N405P4.005	.5	.0	43.5	.0	.16	150.0	-56.0	1.0	1.3	0.	0.	268.	0.	0.	2.67
N405P4.004	.6	.0	43.4	.0	.18	150.0	-66.0	1.0	1.6	0.	0.	267.	0.	0.	3.02
N405P5.009	.7	.0	56.7	.0	.21	150.0	-25.0	1.0	1.8	0.	0.	349.	0.	0.	3.52
N405P5.008	.6	.0	56.7	.0	.19	150.0	-28.0	1.0	1.5	0.	0.	349.	0.	0.	3.10
N405P5.007	.6	.0	41.7	.0	.20	150.0	-33.0	1.0	1.6	0.	0.	257.	0.	0.	3.27
N405P5.006	.6	.0	47.1	.0	.18	150.0	-50.0	1.0	1.6	0.	0.	290.	0.	0.	3.02
N405P5.005	.6	.0	53.2	.0	.15	150.0	-56.0	1.0	1.6	0.	0.	327.	0.	0.	2.56
N405P5.004	.6	.0	53.2	.0	.16	150.0	-66.0	1.0	1.6	0.	0.	328.	0.	0.	2.67
N405Q1.009	.5	.0	48.6	.0	.17	150.0	-25.0	5.0	1.4	0.	0.	299.	0.	0.	2.90
N405Q1.008	.5	.0	48.6	.0	.18	150.0	-28.0	5.0	1.4	0.	0.	299.	0.	0.	2.97
N405Q1.007	.5	.0	48.7	.0	.18	150.0	-33.0	5.0	1.5	0.	0.	300.	0.	0.	3.01
N405Q1.006	.6	.0	52.1	.0	.18	150.0	-50.0	5.0	1.5	0.	0.	321.	0.	0.	3.05
N405Q1.005	.6	.0	48.7	.0	.19	150.0	-56.0	5.0	1.5	0.	0.	300.	0.	0.	3.15
N405Q1.004	.6	.0	58.1	.0	.14	150.0	-66.0	5.0	1.5	0.	0.	358.	0.	0.	2.37
N405Q2.009	.6	.0	50.1	.0	.17	150.0	-25.0	5.0	1.6	0.	0.	309.	0.	0.	2.88
N405Q2.008	.5	.0	39.5	.0	.17	150.0	-28.0	5.0	1.5	0.	0.	244.	0.	0.	2.79
N405Q2.007	.6	.0	58.2	.0	.19	150.0	-33.0	5.0	1.6	0.	0.	359.	0.	0.	3.14
N405Q2.006	.6	.0	49.5	.0	.16	150.0	-50.0	5.0	1.6	0.	0.	305.	0.	0.	2.66
N405Q2.005	.6	.0	55.3	.0	.17	150.0	-56.0	5.0	1.7	0.	0.	341.	0.	0.	2.84
N405Q2.004	.7	.0	55.2	.0	.14	150.0	-66.0	5.0	1.8	0.	0.	340.	0.	0.	2.42
N405Q3.009	.6	.0	59.6	.0	.18	150.0	-25.0	5.0	1.7	0.	0.	367.	0.	0.	2.95
N405Q3.008	.6	.0	51.0	.0	.17	150.0	-28.0	5.0	1.6	0.	0.	314.	0.	0.	2.79
N405Q3.007	.6	.0	49.8	.0	.18	150.0	-33.0	5.0	1.5	0.	0.	307.	0.	0.	2.99
N405Q3.006	.6	.0	51.1	.0	.17	150.0	-50.0	5.0	1.7	0.	0.	315.	0.	0.	2.87
N405Q3.005	.6	.0	58.5	.0	.17	150.0	-56.0	5.0	1.5	0.	0.	360.	0.	0.	2.78
N405Q3.004	.6	.0	58.0	.0	.15	150.0	-66.0	5.0	1.5	0.	0.	357.	0.	0.	2.46
N405Q4.009	.6	.0	49.5	.0	.18	150.0	-25.0	5.0	1.6	0.	0.	305.	0.	0.	3.00
N405Q4.008	.6	.0	49.2	.0	.17	150.0	-28.0	5.0	1.5	0.	0.	303.	0.	0.	2.86
N405Q4.007	.6	.0	48.8	.0	.15	150.0	-33.0	5.0	1.5	0.	0.	300.	0.	0.	2.50
N405Q4.006	.7	.0	49.3	.0	.18	150.0	-50.0	5.0	1.9	0.	0.	304.	0.	0.	2.96
N405Q4.005	.6	.0	49.1	.0	.16	150.0	-56.0	5.0	1.7	0.	0.	303.	0.	0.	2.68
N405Q4.004	.7	.0	49.0	.0	.15	150.0	-66.0	5.0	1.9	0.	0.	302.	0.	0.	2.54
N405Q5.009	.6	.0	58.7	.0	.17	150.0	-25.0	5.0	1.7	0.	0.	361.	0.	0.	2.80
N405Q5.008	.5	.0	56.9	.0	.16	150.0	-28.0	5.0	1.4	0.	0.	351.	0.	0.	2.70
N405Q5.007	.5	.0	44.6	.0	.17	150.0	-33.0	5.0	1.3	0.	0.	275.	0.	0.	2.77
N405Q5.006	.6	.0	51.5	.0	.17	150.0	-50.0	5.0	1.5	0.	0.	317.	0.	0.	2.81
N405Q5.005	.6	.0	51.6	.0	.16	150.0	-56.0	5.0	1.6	0.	0.	318.	0.	0.	2.64
N405Q5.004	.6	.0	60.6	.0	.14	150.0	-66.0	5.0	1.5	0.	0.	374.	0.	0.	2.28

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405R1.009	.6	.0	46.9	.0	.13	150.0	-25.0	11.0	1.6	0.	0.	289.	0.	0.	2.20
N405R1.008	.5	.0	46.8	.0	.11	150.0	-28.0	11.0	1.4	0.	0.	288.	0.	0.	1.89
N405R1.007	.6	.0	47.0	.0	.13	150.0	-33.0	11.0	1.5	0.	0.	289.	0.	0.	2.21
N405R1.006	.5	.0	42.1	.0	.11	150.0	-50.0	11.0	1.4	0.	0.	259.	0.	0.	1.82
N405R1.005	.5	.0	42.0	.0	.11	150.0	-56.0	11.0	1.4	0.	0.	259.	0.	0.	1.78
N405R1.004	.5	.0	46.0	.0	.09	150.0	-66.0	11.0	1.3	0.	0.	283.	0.	0.	1.48
N405R2.009	.5	.0	60.3	.0	.12	150.0	-25.0	11.0	1.4	0.	0.	371.	0.	0.	2.01
N405R2.008	.5	.0	43.1	.0	.11	150.0	-28.0	11.0	1.4	0.	0.	265.	0.	0.	1.96
N405R2.007	.6	.0	43.3	.0	.12	150.0	-33.0	11.0	1.5	0.	0.	267.	0.	0.	2.02
N405R2.006	.6	.0	42.0	.0	.15	150.0	-50.0	11.0	1.5	0.	0.	258.	0.	0.	2.50
N405R2.005	.6	.0	54.2	.0	.13	150.0	-56.0	11.0	1.5	0.	0.	334.	0.	0.	2.21
N405R2.004	.6	.0	42.0	.0	.10	150.0	-66.0	11.0	1.5	0.	0.	259.	0.	0.	1.70
N405R3.009	.5	.0	52.9	.0	.12	150.0	-25.0	11.0	1.3	0.	0.	326.	0.	0.	1.96
N405R3.008	.4	.0	50.6	.0	.10	150.0	-28.0	11.0	1.2	0.	0.	312.	0.	0.	1.74
N405R3.007	.5	.0	40.5	.0	.13	150.0	-33.0	11.0	1.3	0.	0.	250.	0.	0.	2.11
N405R3.006	.5	.0	61.5	.0	.10	150.0	-50.0	11.0	1.4	0.	0.	379.	0.	0.	1.73
N405R3.005	.6	.0	53.1	.0	.12	150.0	-56.0	11.0	1.5	0.	0.	327.	0.	0.	2.08
N405R3.004	.5	.0	49.9	.0	.08	150.0	-66.0	11.0	1.3	0.	0.	307.	0.	0.	1.37
N405R4.009	.5	.0	52.8	.0	.11	150.0	-25.0	11.0	1.4	0.	0.	325.	0.	0.	1.83
N405R4.008	.6	.0	54.4	.0	.12	150.0	-28.0	11.0	1.5	0.	0.	335.	0.	0.	2.08
N405R4.007	.5	.0	50.3	.0	.13	150.0	-33.0	11.0	1.5	0.	0.	310.	0.	0.	2.32
N405R4.006	.5	.0	54.1	.0	.13	150.0	-50.0	11.0	1.4	0.	0.	333.	0.	0.	2.25
N405R4.005	.5	.0	56.7	.0	.12	150.0	-56.0	11.0	1.4	0.	0.	349.	0.	0.	2.07
N405R4.004	.6	.0	59.1	.0	.10	150.0	-66.0	11.0	1.5	0.	0.	364.	0.	0.	1.74
N405R5.009	.6	.0	46.3	.0	.14	150.0	-25.0	11.0	1.5	0.	0.	285.	0.	0.	2.36
N405R5.008	.5	.0	43.2	.0	.13	150.0	-28.0	11.0	1.3	0.	0.	266.	0.	0.	2.17
N405R5.007	.5	.0	47.9	.0	.12	150.0	-33.0	11.0	1.4	0.	0.	295.	0.	0.	2.12
N405R5.006	.5	.0	44.7	.0	.14	150.0	-50.0	11.0	1.4	0.	0.	275.	0.	0.	2.27
N405R5.005	.5	.0	44.8	.0	.12	150.0	-56.0	11.0	1.4	0.	0.	276.	0.	0.	2.02
N405R5.004	.7	.0	48.8	.0	.10	150.0	-66.0	11.0	1.9	0.	0.	301.	0.	0.	1.66
N405S1.009	.6	.0	48.3	.0	.05	150.0	-25.0	17.0	1.6	0.	0.	297.	0.	0.	1.00
N405S1.008	.7	.0	52.4	.0	.08	150.0	-28.0	17.0	1.8	0.	0.	322.	0.	0.	1.40
N405S1.007	.7	.0	48.5	.0	.05	150.0	-33.0	17.0	1.9	0.	0.	299.	0.	0.	1.10
N405S1.006	.5	.0	49.5	.0	.07	150.0	-50.0	17.0	1.4	0.	0.	305.	0.	0.	1.29
N405S1.005	.5	.0	49.2	.0	.07	150.0	-56.0	17.0	1.4	0.	0.	303.	0.	0.	1.21
N405S1.004	.5	.0	45.1	.0	.04	150.0	-66.0	17.0	1.2	0.	0.	278.	0.	0.	.90
N405S2.009	.6	.0	58.2	.0	.04	150.0	-25.0	17.0	1.5	0.	0.	359.	0.	0.	.92
N405S2.008	.5	.0	39.6	.0	.06	150.0	-28.0	17.0	1.3	0.	0.	244.	0.	0.	1.13
N405S2.007	.6	.0	39.7	.0	.04	150.0	-33.0	17.0	1.5	0.	0.	245.	0.	0.	.98
N405S2.006	.6	.0	51.3	.0	.07	150.0	-50.0	17.0	1.6	0.	0.	316.	0.	0.	1.26
N405S2.005	.5	.0	39.9	.0	.06	150.0	-56.0	17.0	1.3	0.	0.	246.	0.	0.	1.26
N405S2.004	.6	.0	52.3	.0	.05	150.0	-66.0	17.0	1.7	0.	0.	322.	0.	0.	1.09

FALCON 4: LSR = 50, GAS = ARGON

FILE NAME	MODEL CONDITIONS: PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PROTOTYPE CONDITIONS: PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N405S3.009	.6	.0	57.7	.0	.07	150.0	-25.0	17.0	1.6	0.	0.	356.	0.	0.	1.28
N405S3.008	.5	.0	58.0	.0	.06	150.0	-28.0	17.0	1.4	0.	0.	357.	0.	0.	1.22
N405S3.007	.6	.0	48.9	.0	.08	150.0	-33.0	17.0	1.5	0.	0.	301.	0.	0.	1.33
N405S3.006	.6	.0	52.9	.0	.10	150.0	-50.0	17.0	1.6	0.	0.	326.	0.	0.	1.62
N405S3.005	.5	.0	60.1	.0	.08	150.0	-56.0	17.0	1.4	0.	0.	370.	0.	0.	1.32
N405S3.004	.6	.0	60.3	.0	.06	150.0	-66.0	17.0	1.5	0.	0.	371.	0.	0.	1.08
N405S4.009	.5	.0	59.5	.0	.05	150.0	-25.0	17.0	1.3	0.	0.	366.	0.	0.	1.06
N405S4.008	.6	.0	53.2	.0	.07	150.0	-28.0	17.0	1.5	0.	0.	328.	0.	0.	1.21
N405S4.007	.6	.0	53.0	.0	.06	150.0	-33.0	17.0	1.5	0.	0.	326.	0.	0.	1.11
N405S4.006	.5	.0	45.0	.0	.07	150.0	-50.0	17.0	1.3	0.	0.	277.	0.	0.	1.27
N405S4.005	.5	.0	35.7	.0	.07	150.0	-56.0	17.0	1.2	0.	0.	220.	0.	0.	1.25
N405S4.004	.4	.0	40.5	.0	.04	150.0	-66.0	17.0	1.1	0.	0.	249.	0.	0.	.86
N405S5.009	.6	.0	57.2	.0	.06	150.0	-25.0	17.0	1.6	0.	0.	352.	0.	0.	1.18
N405S5.008	.6	.0	56.3	.0	.06	150.0	-28.0	17.0	1.5	0.	0.	347.	0.	0.	1.08
N405S5.007	.6	.0	55.7	.0	.07	150.0	-33.0	17.0	1.5	0.	0.	343.	0.	0.	1.24
N405S5.006	.5	.0	46.1	.0	.08	150.0	-50.0	17.0	1.3	0.	0.	284.	0.	0.	1.43
N405S5.005	.5	.0	48.1	.0	.07	150.0	-56.0	17.0	1.4	0.	0.	296.	0.	0.	1.18
N405S5.004	.5	.0	51.0	.0	.02	150.0	-66.0	17.0	1.3	0.	0.	314.	0.	0.	.67

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410A1.004	.8	.0	29.3	.0	.02	-62.0	30.0	2.0	2.2	0.	0.	255.	0.	0.	.66
N410A1.005	.1	.0	.0	.0	.01	-62.0	40.0	2.0	.2	0.	0.	0.	0.	0.	.31
N410A1.006	17.9	5.3	33.9	90.8	3.77	-62.0	20.0	2.0	37.1	47.	51.	295.	393.	642.	76.51
N410A1.007	22.6	5.8	24.0	79.0	4.16	-62.0	10.0	2.0	44.2	54.	55.	210.	403.	487.	82.61
N410A1.008	24.5	4.7	35.8	90.7	6.47	-62.0	.0	2.0	46.7	41.	45.	312.	506.	720.	124.01
N410A1.009	23.9	3.5	36.3	87.7	5.79	-62.0	-10.0	2.0	46.0	32.	35.	317.	456.	668.	112.17
N410A1.010	20.0	3.6	35.2	66.4	3.29	-62.0	-20.0	2.0	40.4	32.	37.	307.	379.	449.	67.05
N410A2.004	.4	.0	36.9	.0	.02	-62.0	30.0	2.0	1.2	0.	0.	322.	0.	0.	.64
N410A2.005	.1	.0	.0	.0	-.03	-62.0	40.0	2.0	.2	0.	0.	0.	0.	0.	.00
N410A2.006	20.1	1.8	16.9	87.9	5.13	-62.0	20.0	2.0	40.5	16.	34.	147.	533.	763.	102.49
N410A2.007	22.7	5.4	34.1	89.6	4.11	-62.0	10.0	2.0	44.3	47.	53.	297.	422.	716.	81.55
N410A2.008	26.8	2.4	33.2	87.1	7.47	-62.0	.0	2.0	49.7	22.	24.	290.	751.	798.	141.37
N410A2.009	26.0	1.0	28.2	91.7	6.79	-62.0	-10.0	2.0	48.7	11.	18.	246.	553.	795.	128.99
N410A2.010	20.9	1.4	28.4	71.1	4.38	-62.0	-20.0	2.0	41.6	21.	25.	248.	403.	619.	86.97
N410A3.004	.7	.0	40.6	.0	.00	-62.0	30.0	2.0	1.9	0.	0.	354.	0.	0.	.30
N410A3.005	.1	.0	.0	.0	.01	-62.0	40.0	2.0	.2	0.	0.	0.	0.	0.	.33
N410A3.006	22.7	2.9	32.7	91.4	5.19	-62.0	20.0	2.0	44.3	26.	34.	285.	744.	744.	104.47
N410A3.007	25.8	4.1	33.0	85.9	6.01	-62.0	10.0	2.0	48.5	37.	49.	288.	541.	661.	115.07
N410A3.008	26.6	3.0	32.7	85.5	7.52	-62.0	.0	2.0	49.4	32.	37.	285.	528.	653.	140.94
N410A3.009	27.2	1.4	31.6	91.3	7.33	-62.0	-10.0	2.0	50.3	12.	25.	276.	628.	789.	137.52
N410A3.010	22.8	1.2	30.6	66.4	4.62	-62.0	-20.0	2.0	44.4	20.	24.	267.	467.	553.	91.09
N410A4.004	.6	.0	35.2	.0	.03	-62.0	30.0	2.0	1.7	0.	0.	307.	0.	0.	.84
N410A4.005	.1	.0	.0	.0	.03	-62.0	40.0	2.0	.3	0.	0.	0.	0.	0.	.79
N410A4.006	24.2	3.2	34.2	86.0	4.27	-62.0	20.0	2.0	46.4	28.	28.	298.	482.	726.	88.56
N410A4.007	29.4	5.4	33.5	83.6	5.57	-62.0	10.0	2.0	52.9	47.	47.	292.	654.	727.	105.61
N410A4.008	29.3	2.6	32.8	87.5	7.97	-62.0	.0	2.0	52.8	33.	37.	286.	565.	719.	145.87
N410A4.009	29.8	1.5	36.9	89.5	7.08	-62.0	-10.0	2.0	53.4	27.	29.	322.	511.	780.	133.25
N410A4.010	21.5	.7	34.0	74.9	4.84	-62.0	-20.0	2.0	42.6	13.	19.	296.	466.	486.	94.88
N410A5.004	.4	.0	40.5	.0	.00	-62.0	30.0	2.0	1.0	0.	0.	353.	0.	0.	.27
N410A5.005	.1	.0	.0	.0	-.01	-62.0	40.0	2.0	.2	0.	0.	0.	0.	0.	.20
N410A5.006	22.6	2.5	31.9	91.5	5.07	-62.0	20.0	2.0	44.1	24.	30.	278.	758.	758.	101.35
N410A5.007	22.8	3.6	30.9	88.2	4.42	-62.0	10.0	2.0	44.4	33.	33.	269.	452.	603.	87.74
N410A5.008	26.3	2.6	34.1	90.4	7.55	-62.0	.0	2.0	49.1	23.	45.	297.	683.	788.	141.46
N410A5.009	27.5	1.3	29.4	87.6	6.59	-62.0	-10.0	2.0	50.6	12.	17.	256.	569.	762.	125.74
N410A5.010	20.5	1.1	21.4	77.6	4.15	-62.0	-20.0	2.0	41.0	13.	13.	187.	415.	509.	83.13
N410B1.004	.1	.0	.0	.0	.00	-32.0	40.0	1.0	.2	0.	0.	0.	0.	0.	.24
N410B1.005	.1	.0	.0	.0	-.01	-32.0	30.0	1.0	.3	0.	0.	0.	0.	0.	.14
N410B1.006	29.5	1.4	35.5	97.7	7.77	-32.0	20.0	1.0	53.1	15.	15.	310.	426.	521.	143.52
N410B1.007	20.4	1.3	30.7	56.7	1.38	-32.0	10.0	1.0	40.9	13.	14.	268.	318.	430.	30.45
N410B1.008	17.6	1.4	35.3	52.3	1.55	-32.0	.0	1.0	36.6	13.	45.	307.	338.	398.	33.32
N410B1.009	30.8	4.9	24.8	100.2	3.93	-32.0	-10.0	1.0	54.6	43.	44.	217.	641.	874.	74.95
N410B1.010	14.8	1.5	16.5	78.2	2.38	-32.0	-20.0	1.0	32.0	14.	37.	144.	397.	446.	51.16

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410B2.004	.1	.0	.0	.0	-.01	-32.0	40.0	1.0	.2	0.	0.	0.	0.	0.	.14
N410B2.005	.4	.0	44.5	.0	.04	-32.0	30.0	1.0	.9	0.	0.	388.	0.	0.	.92
N410B2.006	28.6	1.6	31.8	91.8	7.56	-32.0	20.0	1.0	52.0	15.	16.	277.	442.	593.	139.58
N410B2.007	24.2	.4	37.0	61.7	1.75	-32.0	10.0	1.0	46.3	5.	63.	322.	380.	423.	37.37
N410B2.008	19.4	.4	26.7	67.1	2.22	-32.0	.0	1.0	39.4	23.	83.	233.	359.	395.	46.28
N410B2.009	32.1	2.8	32.6	97.3	5.19	-32.0	-10.0	1.0	56.1	24.	25.	285.	740.	794.	98.04
N410B2.010	21.7	2.0	22.2	69.4	2.21	-32.0	-20.0	1.0	42.8	23.	23.	193.	413.	495.	47.81
N410B3.004	.1	.0	.0	.0	-.01	-32.0	40.0	1.0	.3	0.	0.	0.	0.	0.	.23
N410B3.005	.3	.0	42.4	.0	.05	-32.0	30.0	1.0	.7	0.	0.	370.	0.	0.	1.18
N410B3.006	27.3	1.7	35.9	99.1	7.64	-32.0	20.0	1.0	50.3	16.	19.	313.	407.	862.	140.66
N410B3.007	24.0	1.2	25.2	56.9	1.47	-32.0	10.0	1.0	46.0	15.	67.	220.	322.	415.	31.82
N410B3.008	18.0	1.6	32.5	57.0	1.65	-32.0	.0	1.0	37.2	35.	81.	283.	351.	412.	35.45
N410B3.009	32.6	1.2	25.1	100.0	4.85	-32.0	-10.0	1.0	56.6	25.	25.	218.	747.	751.	92.71
N410B3.010	19.3	1.9	28.9	99.0	2.37	-32.0	-20.0	1.0	39.3	17.	18.	252.	565.	606.	50.37
N410B4.004	.1	.0	.0	.0	.02	-32.0	40.0	1.0	.3	0.	0.	0.	0.	0.	.59
N410B4.005	.3	.0	32.6	.0	.02	-32.0	30.0	1.0	.8	0.	0.	285.	0.	0.	.64
N410B4.006	26.1	.7	24.1	83.5	6.75	-32.0	20.0	1.0	48.9	17.	18.	210.	686.	686.	126.84
N410B4.007	18.8	1.5	35.4	58.9	1.22	-32.0	10.0	1.0	38.4	16.	84.	308.	322.	420.	27.37
N410B4.008	19.3	.8	25.8	83.1	1.84	-32.0	.0	1.0	39.2	19.	78.	225.	325.	422.	39.50
N410B4.009	32.2	1.2	34.3	99.0	5.32	-32.0	-10.0	1.0	56.2	19.	20.	299.	812.	837.	101.47
N410B4.010	17.0	1.9	33.1	86.9	2.10	-32.0	-20.0	1.0	35.6	17.	30.	288.	347.	489.	45.39
N410B5.004	.1	.0	.0	.0	.02	-32.0	40.0	1.0	.4	0.	0.	0.	0.	0.	.69
N410B5.005	.4	.0	29.3	.0	.01	-32.0	30.0	1.0	1.0	0.	0.	255.	0.	0.	.59
N410B5.006	32.0	1.1	23.5	92.7	7.17	-32.0	20.0	1.0	56.0	10.	10.	205.	418.	617.	133.02
N410B5.007	16.5	1.3	22.4	67.5	1.29	-32.0	10.0	1.0	34.9	71.	77.	195.	320.	393.	28.61
N410B5.008	17.5	.3	23.5	59.6	1.76	-32.0	.0	1.0	36.4	36.	37.	205.	349.	489.	38.30
N410B5.009	27.6	1.4	27.2	99.3	5.52	-32.0	-10.0	1.0	50.7	13.	15.	237.	672.	800.	105.21
N410B5.010	15.5	5.1	30.9	74.5	2.41	-32.0	-20.0	1.0	33.2	44.	45.	270.	341.	504.	51.51
N410C1.004	.1	.0	.0	.0	.00	-2.0	40.0	1.0	.3	0.	0.	0.	0.	0.	.28
N410C1.005	.3	.0	38.0	.0	.03	-2.0	30.0	1.0	.8	0.	0.	331.	0.	0.	.79
N410C1.006	8.8	6.8	33.5	47.7	.82	-2.0	20.0	1.0	20.7	59.	252.	292.	329.	362.	18.60
N410C1.007	4.1	3.2	30.4	45.9	.57	-2.0	10.0	1.0	10.3	99.	264.	265.	265.	351.	13.27
N410C1.008	2.6	11.0	16.7	43.0	.37	-2.0	.0	1.0	6.7	145.	0.	145.	0.	146.	8.70
N410C1.009	3.0	6.0	21.3	49.3	.40	-2.0	-10.0	1.0	7.7	184.	0.	186.	0.	339.	9.41
N410C1.010	1.7	4.9	21.9	43.2	.44	-2.0	-20.0	1.0	4.4	0.	0.	191.	0.	0.	10.28
N410C2.004	.1	.0	.0	.0	-.01	-2.0	40.0	1.0	.2	0.	0.	0.	0.	0.	.14
N410C2.005	.3	.0	47.6	.0	.02	-2.0	30.0	1.0	.9	0.	0.	415.	0.	0.	.68
N410C2.006	16.1	4.2	33.5	45.6	1.46	-2.0	20.0	1.0	34.2	37.	37.	292.	332.	384.	31.73
N410C2.007	4.9	4.1	33.8	50.2	.64	-2.0	10.0	1.0	12.3	80.	142.	294.	295.	367.	14.69
N410C2.008	6.7	5.9	33.5	42.3	.57	-2.0	.0	1.0	16.4	82.	206.	292.	293.	336.	13.08
N410C2.009	3.0	9.6	9.7	50.3	.51	-2.0	-10.0	1.0	7.6	84.	0.	84.	0.	340.	11.77
N410C2.010	4.8	8.9	30.3	44.0	.52	-2.0	-20.0	1.0	11.9	263.	263.	264.	265.	371.	12.02

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410C3.004	.1	.0	.0	.0	.03	-2.0	40.0	1.0	.3	0.	0.	0.	0.	0.	.76
N410C3.005	.3	.0	16.4	.0	.01	-2.0	30.0	1.0	.8	0.	0.	143.	0.	0.	.47
N410C3.006	11.9	7.7	36.3	51.0	.94	-2.0	20.0	1.0	26.8	72.	131.	317.	333.	357.	21.27
N410C3.007	5.3	7.6	33.7	48.6	.55	-2.0	10.0	1.0	13.1	86.	293.	294.	294.	317.	12.79
N410C3.008	2.7	5.2	33.8	48.2	.38	-2.0	.0	1.0	7.1	214.	0.	294.	0.	295.	8.86
N410C3.009	2.1	7.7	36.7	42.6	.39	-2.0	-10.0	1.0	5.6	320.	0.	320.	0.	320.	9.20
N410C3.010	2.1	20.8	36.6	44.0	.40	-2.0	-20.0	1.0	5.4	319.	0.	319.	0.	324.	9.42
N410C4.004	.1	.0	.0	.0	.00	-2.0	40.0	1.0	.2	0.	0.	0.	0.	0.	.15
N410C4.005	.1	.0	.0	.0	-.01	-2.0	30.0	1.0	.2	0.	0.	0.	0.	0.	.07
N410C4.006	18.8	12.9	34.7	52.3	1.56	-2.0	20.0	1.0	38.5	113.	169.	303.	348.	360.	33.35
N410C4.007	4.4	4.2	31.7	53.1	.62	-2.0	10.0	1.0	11.2	107.	246.	276.	306.	402.	14.29
N410C4.008	2.4	12.2	35.3	52.9	.47	-2.0	.0	1.0	6.2	107.	0.	308.	0.	347.	10.86
N410C4.009	3.3	12.3	33.2	47.5	.48	-2.0	-10.0	1.0	8.4	178.	0.	290.	0.	315.	11.34
N410C4.010	3.2	21.1	35.0	46.8	.49	-2.0	-20.0	1.0	8.2	189.	0.	305.	0.	323.	11.51
N410C5.004	.1	.0	.0	.0	.01	-2.0	40.0	1.0	.3	0.	0.	0.	0.	0.	.48
N410C5.005	.2	.0	.0	.0	.01	-2.0	30.0	1.0	.4	0.	0.	0.	0.	0.	.39
N410C5.006	20.9	6.8	36.1	54.3	1.55	-2.0	20.0	1.0	41.7	105.	222.	315.	346.	372.	32.35
N410C5.007	3.9	6.7	26.0	57.7	.61	-2.0	10.0	1.0	9.8	133.	0.	226.	0.	357.	14.18
N410C5.008	2.8	12.6	37.6	47.4	.47	-2.0	.0	1.0	7.3	133.	0.	328.	0.	345.	10.92
N410C5.009	3.4	7.1	32.9	47.5	.43	-2.0	-10.0	1.0	8.7	227.	0.	286.	0.	386.	9.94
N410C5.010	2.2	15.3	36.6	46.0	.49	-2.0	-20.0	1.0	5.8	227.	0.	319.	0.	345.	11.36
N410D1.004	.1	.0	.0	.0	-.06	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.06
N410D1.005	.0	.0	.0	.0	-.03	50.0	58.0	1.0	.1	0.	0.	0.	0.	0.	.09
N410D1.006	.1	.0	.0	.0	-.03	50.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.08
N410D1.007	.3	.0	23.3	.0	.07	50.0	42.0	1.0	.8	0.	0.	203.	0.	0.	1.64
N410D1.008	.1	.0	.0	.0	.01	50.0	33.0	1.0	.2	0.	0.	0.	0.	0.	.37
N410D1.009	1.0	39.9	39.9	40.0	.06	50.0	17.0	1.0	2.7	0.	0.	348.	0.	0.	1.46
N410D1.010	1.0	.0	33.8	.0	.27	50.0	.0	1.0	2.6	0.	0.	295.	0.	0.	6.37
N410D2.004	.1	.0	.0	.0	-.04	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.24
N410D2.005	.1	.0	.0	.0	-.01	50.0	58.0	1.0	.2	0.	0.	0.	0.	0.	.15
N410D2.006	.1	.0	.0	.0	-.01	50.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.08
N410D2.007	.2	.0	.0	.0	-.01	50.0	42.0	1.0	.5	0.	0.	0.	0.	0.	.36
N410D2.008	.1	.0	.0	.0	.00	50.0	33.0	1.0	.3	0.	0.	0.	0.	0.	.20
N410D2.009	.8	.0	32.7	.0	.09	50.0	17.0	1.0	2.0	0.	0.	285.	0.	0.	2.21
N410D2.010	.9	.0	29.2	.0	.27	50.0	.0	1.0	2.3	0.	0.	255.	0.	0.	6.41
N410D3.004	.1	.0	.0	.0	.00	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.51
N410D3.005	.1	.0	.0	.0	-.01	50.0	58.0	1.0	.3	0.	0.	0.	0.	0.	.14
N410D3.006	.1	.0	.0	.0	.00	50.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.19
N410D3.007	.1	.0	.0	.0	-.02	50.0	42.0	1.0	.4	0.	0.	0.	0.	0.	.38
N410D3.008	.1	.0	.0	.0	-.03	50.0	33.0	1.0	.2	0.	0.	0.	0.	0.	.07
N410D3.009	1.0	.0	35.5	.0	.10	50.0	17.0	1.0	2.6	0.	0.	310.	0.	0.	2.31
N410D3.010	.8	.0	34.6	.0	.20	50.0	.0	1.0	2.1	0.	0.	301.	0.	0.	4.69

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410D4.004	.2	.0	.0	.0	.05	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	1.11
N410D4.005	.2	.0	.0	.0	.06	50.0	58.0	1.0	.5	0.	0.	0.	0.	0.	1.35
N410D4.006	.1	.0	.0	.0	.02	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.60
N410D4.007	.2	.0	33.9	.0	-.02	50.0	42.0	1.0	.6	0.	0.	296.	0.	0.	.30
N410D4.008	.1	.0	.0	.0	.01	50.0	33.0	1.0	.3	0.	0.	0.	0.	0.	.36
N410D4.009	.7	.0	44.1	.0	.08	50.0	17.0	1.0	1.9	0.	0.	385.	0.	0.	1.91
N410D4.010	.9	.0	29.3	.0	.26	50.0	.0	1.0	2.3	0.	0.	255.	0.	0.	6.15
N410D5.004	.1	.0	.0	.0	-.01	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.37
N410D5.005	.1	.0	.0	.0	.04	50.0	58.0	1.0	.4	0.	0.	0.	0.	0.	1.03
N410D5.006	.1	.0	.0	.0	.02	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.54
N410D5.007	.2	.0	64.7	.0	.03	50.0	42.0	1.0	.6	0.	0.	564.	0.	0.	.96
N410D5.008	.2	.0	.0	.0	.02	50.0	33.0	1.0	.5	0.	0.	0.	0.	0.	.67
N410D5.009	.7	.0	43.9	.0	.09	50.0	17.0	1.0	1.9	0.	0.	383.	0.	0.	2.14
N410D5.010	1.0	.0	43.0	.0	.27	50.0	.0	1.0	2.6	0.	0.	375.	0.	0.	6.43
N410E1.004	.0	.0	.0	.0	-.03	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.04
N410E1.005	.1	.0	.0	.0	.00	50.0	58.0	5.0	.2	0.	0.	0.	0.	0.	.19
N410E1.006	.1	.0	.0	.0	.01	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.28
N410E1.007	.1	.0	.0	.0	-.01	50.0	42.0	5.0	.3	0.	0.	0.	0.	0.	.23
N410E1.008	.5	.0	23.7	.0	-.01	50.0	33.0	5.0	1.3	0.	0.	206.	0.	0.	.17
N410E1.009	.9	.0	39.9	.0	.11	50.0	17.0	5.0	2.4	0.	0.	347.	0.	0.	2.64
N410E1.010	.9	.0	43.0	.0	.22	50.0	.0	5.0	2.3	0.	0.	375.	0.	0.	5.29
N410E2.004	.1	.0	.0	.0	.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.55
N410E2.005	.1	.0	.0	.0	.02	50.0	58.0	5.0	.3	0.	0.	0.	0.	0.	.65
N410E2.006	.1	.0	.0	.0	.01	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.33
N410E2.007	.1	.0	.0	.0	-.01	50.0	42.0	5.0	.3	0.	0.	0.	0.	0.	.32
N410E2.008	.5	.0	34.1	.0	.01	50.0	33.0	5.0	1.2	0.	0.	297.	0.	0.	.40
N410E2.009	1.1	22.1	22.1	34.1	.12	50.0	17.0	5.0	3.0	0.	0.	193.	0.	0.	2.97
N410E2.010	1.0	42.6	42.6	42.7	.27	50.0	.0	5.0	2.7	0.	0.	372.	0.	0.	6.25
N410E3.004	.1	.0	.0	.0	.01	50.0	66.0	5.0	.4	0.	0.	0.	0.	0.	.45
N410E3.005	.1	.0	.0	.0	.01	50.0	58.0	5.0	.2	0.	0.	0.	0.	0.	.38
N410E3.006	.1	.0	.0	.0	.01	50.0	50.0	5.0	.3	0.	0.	0.	0.	0.	.36
N410E3.007	.1	.0	.0	.0	-.01	50.0	42.0	5.0	.2	0.	0.	0.	0.	0.	.23
N410E3.008	.2	.0	.0	.0	.03	50.0	33.0	5.0	.4	0.	0.	0.	0.	0.	.70
N410E3.009	1.1	36.7	36.7	39.5	.14	50.0	17.0	5.0	2.9	0.	0.	320.	0.	0.	3.26
N410E3.010	1.0	.0	41.0	.0	.25	50.0	.0	5.0	2.6	0.	0.	357.	0.	0.	5.90
N410E4.004	.1	.0	.0	.0	.00	50.0	66.0	5.0	.4	0.	0.	0.	0.	0.	.43
N410E4.005	.0	.0	.0	.0	-.02	50.0	58.0	5.0	.1	0.	0.	0.	0.	0.	.05
N410E4.006	.1	.0	.0	.0	.01	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.22
N410E4.007	.2	.0	.0	.0	.02	50.0	42.0	5.0	.5	0.	0.	0.	0.	0.	.66
N410E4.008	.6	.0	38.7	.0	.00	50.0	33.0	5.0	1.5	0.	0.	337.	0.	0.	.11
N410E4.009	1.0	.0	27.4	.0	.14	50.0	17.0	5.0	2.6	0.	0.	239.	0.	0.	3.32
N410E4.010	.9	.0	15.4	.0	.27	50.0	.0	5.0	2.4	0.	0.	135.	0.	0.	6.30

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410E5.004	.2	.0	.0	.0	.00	50.0	66.0	5.0	.5	0.	0.	0.	0.	0.	.43
N410E5.005	.1	.0	.0	.0	-.03	50.0	58.0	5.0	.2	0.	0.	0.	0.	0.	.02
N410E5.006	.1	.0	.0	.0	-.02	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.07
N410E5.007	.1	.0	.0	.0	-.02	50.0	42.0	5.0	.4	0.	0.	0.	0.	0.	.17
N410E5.008	.4	.0	26.3	.0	-.01	50.0	33.0	5.0	1.2	0.	0.	229.	0.	0.	.16
N410E5.009	1.2	39.5	40.1	40.2	.10	50.0	17.0	5.0	3.1	0.	0.	350.	0.	0.	2.60
N410E5.010	1.0	.0	40.1	.0	.24	50.0	.0	5.0	2.5	0.	0.	350.	0.	0.	5.62
N410F1.004	.3	.0	22.2	.0	.01	50.0	66.0	11.0	.7	0.	0.	194.	0.	0.	.90
N410F1.005	.1	.0	.0	.0	.01	50.0	58.0	11.0	.3	0.	0.	0.	0.	0.	.40
N410F1.006	.1	.0	.0	.0	.00	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.12
N410F1.007	.1	.0	.0	.0	-.01	50.0	42.0	11.0	.2	0.	0.	0.	0.	0.	.20
N410F1.008	.7	.0	23.5	.0	-.02	50.0	33.0	11.0	1.9	0.	0.	205.	0.	0.	.13
N410F1.009	1.0	32.2	32.2	32.2	.14	50.0	17.0	11.0	2.7	0.	0.	281.	0.	0.	3.32
N410F1.010	.9	.0	30.3	.0	.19	50.0	.0	11.0	2.4	0.	0.	265.	0.	0.	4.58
N410F2.004	.2	.0	.0	.0	.05	50.0	66.0	11.0	.4	0.	0.	0.	0.	0.	1.30
N410F2.005	.1	.0	.0	.0	.02	50.0	58.0	11.0	.3	0.	0.	0.	0.	0.	.58
N410F2.006	.1	.0	.0	.0	.03	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.65
N410F2.007	.1	.0	.0	.0	-.01	50.0	42.0	11.0	.3	0.	0.	0.	0.	0.	.20
N410F2.008	.9	.0	33.6	.0	-.02	50.0	33.0	11.0	2.3	0.	0.	293.	0.	0.	.14
N410F2.009	1.6	20.9	31.7	41.0	.17	50.0	17.0	11.0	4.2	0.	0.	276.	0.	0.	3.90
N410F2.010	1.3	36.8	37.0	38.3	.24	50.0	.0	11.0	3.4	0.	0.	323.	0.	0.	5.60
N410F3.004	.1	.0	.0	.0	-.02	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.09
N410F3.005	.1	.0	.0	.0	.00	50.0	58.0	11.0	.1	0.	0.	0.	0.	0.	.24
N410F3.006	.1	.0	.0	.0	.02	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.46
N410F3.007	.2	.0	34.6	.0	.04	50.0	42.0	11.0	.6	0.	0.	302.	0.	0.	.97
N410F3.008	1.0	.0	39.7	.0	.02	50.0	33.0	11.0	2.5	0.	0.	346.	0.	0.	.65
N410F3.009	1.6	33.5	33.7	40.5	.17	50.0	17.0	11.0	4.1	0.	0.	294.	0.	0.	4.01
N410F3.010	1.1	36.4	36.5	40.4	.20	50.0	.0	11.0	3.0	0.	0.	318.	0.	0.	4.61
N410F4.004	.1	.0	.0	.0	-.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.13
N410F4.005	.1	.0	.0	.0	.00	50.0	58.0	11.0	.3	0.	0.	0.	0.	0.	.19
N410F4.006	.1	.0	.0	.0	.00	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.28
N410F4.007	.1	.0	.0	.0	.02	50.0	42.0	11.0	.4	0.	0.	0.	0.	0.	.68
N410F4.008	.4	.0	49.2	.0	.02	50.0	33.0	11.0	1.1	0.	0.	429.	0.	0.	.86
N410F4.009	1.3	38.7	38.7	38.8	.16	50.0	17.0	11.0	3.3	0.	0.	338.	0.	0.	3.80
N410F4.010	1.4	25.7	25.7	28.7	.21	50.0	.0	11.0	3.7	0.	0.	224.	0.	0.	4.96
N410F5.004	.0	.0	.0	.0	-.02	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.13
N410F5.005	.1	.0	.0	.0	.00	50.0	58.0	11.0	.2	0.	0.	0.	0.	0.	.06
N410F5.006	.1	.0	.0	.0	.02	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.49
N410F5.007	.1	.0	.0	.0	.00	50.0	42.0	11.0	.2	0.	0.	0.	0.	0.	.29
N410F5.008	.6	.0	48.6	.0	.02	50.0	33.0	11.0	1.7	0.	0.	424.	0.	0.	.58
N410F5.009	1.3	22.6	22.6	36.4	.15	50.0	17.0	11.0	3.3	0.	0.	197.	0.	0.	3.57
N410F5.010	1.0	.0	33.6	.0	.19	50.0	.0	11.0	2.5	0.	0.	293.	0.	0.	4.38

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410G1.004	.1	.0	.0	.0	.01	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.35
N410G1.005	.1	.0	.0	.0	.01	50.0	58.0	17.0	.2	0.	0.	0.	0.	0.	.32
N410G1.006	.1	.0	.0	.0	.01	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.26
N410G1.007	.2	.0	.0	.0	.02	50.0	42.0	17.0	.4	0.	0.	0.	0.	0.	.63
N410G1.008	1.1	38.4	38.4	38.4	.01	50.0	33.0	17.0	2.9	0.	0.	335.	0.	0.	.48
N410G1.009	1.4	23.2	36.9	36.9	.09	50.0	17.0	17.0	3.7	0.	0.	321.	0.	0.	2.33
N410G1.010	1.1	33.1	33.2	33.2	.14	50.0	.0	17.0	3.0	0.	0.	289.	0.	0.	3.31
N410G2.004	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.13
N410G2.005	.1	.0	.0	.0	.00	50.0	58.0	17.0	.2	0.	0.	0.	0.	0.	.11
N410G2.006	.1	.0	.0	.0	.01	50.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.29
N410G2.007	.1	.0	.0	.0	-.01	50.0	42.0	17.0	.2	0.	0.	0.	0.	0.	.18
N410G2.008	1.1	36.3	36.3	36.3	.02	50.0	33.0	17.0	2.8	0.	0.	316.	0.	0.	.45
N410G2.009	1.5	22.7	31.6	36.5	.11	50.0	17.0	17.0	4.1	0.	0.	275.	0.	0.	2.65
N410G2.010	1.1	32.7	32.7	40.4	.10	50.0	.0	17.0	3.0	0.	0.	285.	0.	0.	2.59
N410G3.004	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.12
N410G3.005	.1	.0	.0	.0	.00	50.0	58.0	17.0	.1	0.	0.	0.	0.	0.	.14
N410G3.006	.1	.0	.0	.0	.01	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.41
N410G3.007	.1	.0	.0	.0	.02	50.0	42.0	17.0	.4	0.	0.	0.	0.	0.	.52
N410G3.008	.8	.0	21.3	.0	.00	50.0	33.0	17.0	2.0	0.	0.	186.	0.	0.	.16
N410G3.009	1.3	14.7	26.6	37.9	.12	50.0	17.0	17.0	3.4	0.	0.	232.	0.	0.	3.08
N410G3.010	1.3	13.4	13.4	40.1	.10	50.0	.0	17.0	3.5	0.	0.	116.	0.	0.	2.64
N410G4.004	.1	.0	.0	.0	-.02	50.0	66.0	17.0	.4	0.	0.	0.	0.	0.	.09
N410G4.005	.1	.0	.0	.0	-.01	50.0	58.0	17.0	.1	0.	0.	0.	0.	0.	.07
N410G4.006	.1	.0	.0	.0	-.01	50.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.09
N410G4.007	.1	.0	.0	.0	-.01	50.0	42.0	17.0	.3	0.	0.	0.	0.	0.	.27
N410G4.008	.5	.0	16.9	.0	.01	50.0	33.0	17.0	1.4	0.	0.	147.	0.	0.	.51
N410G4.009	1.7	23.7	35.0	35.1	.13	50.0	17.0	17.0	4.5	0.	0.	305.	0.	0.	3.19
N410G4.010	1.3	27.3	27.3	29.4	.15	50.0	.0	17.0	3.4	0.	0.	238.	0.	0.	3.50
N410G5.004	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.21
N410G5.005	.1	.0	.0	.0	.00	50.0	58.0	17.0	.1	0.	0.	0.	0.	0.	.20
N410G5.006	.0	.0	.0	.0	-.03	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.06
N410G5.007	.1	.0	.0	.0	.01	50.0	42.0	17.0	.3	0.	0.	0.	0.	0.	.39
N410G5.008	.6	.0	52.7	.0	.00	50.0	33.0	17.0	1.7	0.	0.	460.	0.	0.	.07
N410G5.009	1.3	29.8	37.4	39.3	.12	50.0	17.0	17.0	3.5	0.	0.	326.	0.	0.	2.92
N410G5.010	1.3	30.3	30.3	30.4	.12	50.0	.0	17.0	3.4	0.	0.	264.	0.	0.	2.90
N410H2.004	1.0	.0	31.4	.0	.23	50.0	.0	1.0	2.6	0.	0.	274.	0.	0.	5.61
N410H2.005	1.1	38.0	41.1	41.2	.30	50.0	-17.0	1.0	2.9	0.	0.	358.	0.	0.	6.92
N410H2.006	1.1	34.2	35.9	36.2	.21	50.0	-33.0	1.0	2.9	0.	0.	313.	0.	0.	4.89
N410H2.007	.9	.0	40.2	.0	.16	50.0	-42.0	1.0	2.5	0.	0.	351.	0.	0.	3.90
N410H2.008	.7	.0	38.7	.0	.11	50.0	-50.0	1.0	2.0	0.	0.	337.	0.	0.	2.56
N410H2.009	.5	.0	42.4	.0	.07	50.0	-58.0	1.0	1.4	0.	0.	369.	0.	0.	1.63
N410H2.010	.3	.0	42.6	.0	.04	50.0	-66.0	1.0	.7	0.	0.	372.	0.	0.	1.02

FALCON 4: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410H3.004	1.0	40.9	40.9	41.0	.27	50.0	.0	1.0	2.7	0.	0.	357.	0.	0.	6.33
N410H3.005	1.0	35.6	35.6	35.7	.29	50.0	-17.0	1.0	2.7	0.	0.	311.	0.	0.	6.82
N410H3.006	1.1	36.5	36.5	36.5	.22	50.0	-33.0	1.0	2.8	0.	0.	318.	0.	0.	5.12
N410H3.007	1.0	.0	32.3	.0	.15	50.0	-42.0	1.0	2.6	0.	0.	281.	0.	0.	3.73
N410H3.008	.7	.0	32.4	.0	.09	50.0	-50.0	1.0	2.0	0.	0.	283.	0.	0.	2.24
N410H3.009	.9	.0	42.5	.0	.03	50.0	-58.0	1.0	2.3	0.	0.	371.	0.	0.	1.00
N410H3.010	.3	.0	28.4	.0	.02	50.0	-66.0	1.0	.8	0.	0.	247.	0.	0.	.67
N410H4.004	.8	.0	27.1	.0	.25	50.0	.0	1.0	2.3	0.	0.	237.	0.	0.	5.85
N410H4.005	.9	.0	30.5	.0	.29	50.0	-17.0	1.0	2.5	0.	0.	266.	0.	0.	6.84
N410H4.006	1.0	.0	33.3	.0	.23	50.0	-33.0	1.0	2.6	0.	0.	290.	0.	0.	5.33
N410H4.007	1.0	.0	40.3	.0	.16	50.0	-42.0	1.0	2.6	0.	0.	351.	0.	0.	3.88
N410H4.008	.8	.0	36.0	.0	.09	50.0	-50.0	1.0	2.2	0.	0.	314.	0.	0.	2.15
N410H4.009	.6	.0	36.1	.0	.05	50.0	-58.0	1.0	1.6	0.	0.	315.	0.	0.	1.32
N410H4.010	.3	.0	23.8	.0	.02	50.0	-66.0	1.0	.8	0.	0.	207.	0.	0.	.65
N410H5.004	1.0	.0	32.0	.0	.28	50.0	.0	1.0	2.5	0.	0.	279.	0.	0.	6.48
N410H5.005	1.1	39.3	39.4	39.5	.27	50.0	-17.0	1.0	2.8	0.	0.	343.	0.	0.	6.44
N410H5.006	1.2	26.0	39.7	39.8	.20	50.0	-33.0	1.0	3.3	0.	0.	346.	0.	0.	4.64
N410H5.007	1.0	39.7	39.7	39.7	.17	50.0	-42.0	1.0	2.8	0.	0.	346.	0.	0.	3.97
N410H5.008	.8	.0	39.2	.0	.09	50.0	-50.0	1.0	2.2	0.	0.	342.	0.	0.	2.15
N410H5.009	.5	.0	31.1	.0	.04	50.0	-58.0	1.0	1.3	0.	0.	271.	0.	0.	1.00
N410H5.010	.3	.0	40.9	.0	.02	50.0	-66.0	1.0	.8	0.	0.	357.	0.	0.	.39
N410I1.004	1.1	35.7	36.1	40.1	.24	50.0	.0	5.0	2.8	0.	0.	315.	0.	0.	5.66
N410I1.005	1.3	34.7	38.2	38.2	.22	50.0	-17.0	5.0	3.5	0.	0.	333.	0.	0.	5.16
N410I1.006	1.2	24.2	38.0	38.7	.17	50.0	-33.0	5.0	3.1	0.	0.	332.	0.	0.	3.91
N410I1.007	.9	.0	34.9	.0	.08	50.0	-42.0	5.0	2.4	0.	0.	304.	0.	0.	1.99
N410I1.008	1.0	.0	36.1	.0	.03	50.0	-50.0	5.0	2.6	0.	0.	315.	0.	0.	.78
N410I1.009	.6	.0	36.9	.0	.03	50.0	-58.0	5.0	1.7	0.	0.	322.	0.	0.	.72
N410I1.010	.4	.0	47.1	.0	.01	50.0	-66.0	5.0	1.2	0.	0.	411.	0.	0.	.28
N410I2.004	1.0	.0	42.1	.0	.26	50.0	.0	5.0	2.6	0.	0.	367.	0.	0.	6.04
N410I2.005	1.0	37.2	37.2	37.3	.27	50.0	-17.0	5.0	2.7	0.	0.	325.	0.	0.	6.23
N410I2.006	1.1	28.8	29.0	42.1	.21	50.0	-33.0	5.0	3.0	0.	0.	253.	0.	0.	5.07
N410I2.007	1.0	.0	33.7	.0	.11	50.0	-42.0	5.0	2.6	0.	0.	294.	0.	0.	2.67
N410I2.008	1.0	.0	33.4	.0	.07	50.0	-50.0	5.0	2.6	0.	0.	291.	0.	0.	1.76
N410I2.009	.9	.0	33.5	.0	.03	50.0	-58.0	5.0	2.4	0.	0.	292.	0.	0.	.88
N410I2.010	.3	.0	34.0	.0	.04	50.0	-66.0	5.0	.8	0.	0.	296.	0.	0.	.93
N410I3.004	1.1	36.4	36.5	37.8	.28	50.0	.0	5.0	3.0	0.	0.	318.	0.	0.	6.54
N410I3.005	1.2	20.7	36.3	38.5	.27	50.0	-17.0	5.0	3.3	0.	0.	316.	0.	0.	6.44
N410I3.006	1.1	27.9	27.9	47.0	.21	50.0	-33.0	5.0	2.8	0.	0.	243.	0.	0.	4.83
N410I3.007	1.0	.0	42.3	.0	.10	50.0	-42.0	5.0	2.6	0.	0.	369.	0.	0.	2.62
N410I3.008	.8	.0	20.8	.0	.08	50.0	-50.0	5.0	2.2	0.	0.	181.	0.	0.	1.88
N410I3.009	.6	.0	43.2	.0	.05	50.0	-58.0	5.0	1.7	0.	0.	377.	0.	0.	1.15
N410I3.010	.3	.0	41.0	.0	.03	50.0	-66.0	5.0	.8	0.	0.	357.	0.	0.	.88

FALCON 4: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410I4.004	.8	.0	29.6	.0	.26	50.0	.0	5.0	2.2	0.	0.	258.	0.	0.	6.07
N410I4.005	1.0	.0	21.8	.0	.26	50.0	-17.0	5.0	2.6	0.	0.	190.	0.	0.	6.20
N410I4.006	1.1	24.4	24.4	46.6	.22	50.0	-33.0	5.0	2.8	0.	0.	213.	0.	0.	5:09
N410I4.007	1.0	32.8	32.8	32.8	.10	50.0	-42.0	5.0	2.7	0.	0.	286.	0.	0.	2.65
N410I4.008	.9	.0	31.9	.0	.07	50.0	-50.0	5.0	2.3	0.	0.	278.	0.	0.	1.80
N410I4.009	.7	.0	51.1	.0	.03	50.0	-58.0	5.0	1.8	0.	0.	445.	0.	0.	.88
N410I4.010	.4	.0	44.0	.0	.02	50.0	-66.0	5.0	1.1	0.	0.	384.	0.	0.	.63
N410I5.004	1.1	28.3	38.4	41.3	.30	50.0	.0	5.0	2.9	0.	0.	335.	0.	0.	6.95
N410I5.005	1.3	38.1	41.8	41.9	.28	50.0	-17.0	5.0	3.4	0.	0.	364.	0.	0.	6.47
N410I5.006	1.1	38.8	41.6	41.6	.15	50.0	-33.0	5.0	3.0	0.	0.	362.	0.	0.	3.59
N410I5.007	1.0	40.0	40.0	40.0	.06	50.0	-42.0	5.0	2.7	0.	0.	349.	0.	0.	1.78
N410I5.008	.6	.0	40.1	.0	.05	50.0	-50.0	5.0	1.5	0.	0.	350.	0.	0.	1.28
N410I5.009	.5	.0	38.1	.0	.04	50.0	-58.0	5.0	1.4	0.	0.	332.	0.	0.	.93
N410I5.010	.1	.0	.0	.0	.03	50.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.67
N410J1.004	1.0	.0	42.6	.0	.22	50.0	.0	11.0	2.5	0.	0.	371.	0.	0.	5.12
N410J1.005	1.0	.0	41.7	.0	.23	50.0	-17.0	11.0	2.6	0.	0.	364.	0.	0.	5.44
N410J1.006	1.3	32.1	32.2	42.8	.20	50.0	-33.0	11.0	3.5	0.	0.	280.	0.	0.	4.74
N410J1.007	1.1	39.2	42.6	42.7	.07	50.0	-42.0	11.0	2.8	0.	0.	372.	0.	0.	1.98
N410J1.008	.8	.0	38.9	.0	.04	50.0	-50.0	11.0	2.0	0.	0.	339.	0.	0.	1.01
N410J1.009	.5	.0	53.6	.0	.02	50.0	-58.0	11.0	1.3	0.	0.	467.	0.	0.	.55
N410J1.010	.2	.0	.0	.0	.03	50.0	-66.0	11.0	.5	0.	0.	0.	0.	0.	.68
N410J2.004	1.0	48.6	48.6	48.7	.21	50.0	.0	11.0	2.7	0.	0.	424.	0.	0.	5.01
N410J2.005	1.3	35.7	42.2	49.1	.24	50.0	-17.0	11.0	3.4	0.	0.	368.	0.	0.	5.66
N410J2.006	1.2	38.6	39.0	44.5	.19	50.0	-33.0	11.0	3.2	0.	0.	340.	0.	0.	4.54
N410J2.007	1.2	38.6	38.7	46.6	.07	50.0	-42.0	11.0	3.1	0.	0.	337.	0.	0.	2.22
N410J2.008	.9	.0	38.7	.0	.02	50.0	-50.0	11.0	2.3	0.	0.	337.	0.	0.	.90
N410J2.009	.8	.0	41.9	.0	.02	50.0	-58.0	11.0	2.1	0.	0.	365.	0.	0.	.67
N410J2.010	.3	.0	18.3	.0	.03	50.0	-66.0	11.0	.9	0.	0.	159.	0.	0.	.81
N410J3.004	1.3	24.6	31.5	39.6	.21	50.0	.0	11.0	3.6	0.	0.	274.	0.	0.	4.93
N410J3.005	1.3	32.4	37.0	41.7	.25	50.0	-17.0	11.0	3.3	0.	0.	323.	0.	0.	5.88
N410J3.006	1.5	32.2	37.2	42.7	.19	50.0	-33.0	11.0	3.9	0.	0.	325.	0.	0.	4.64
N410J3.007	1.5	40.1	40.1	40.4	.09	50.0	-42.0	11.0	3.9	0.	0.	350.	0.	0.	2.32
N410J3.008	.6	.0	36.9	.0	.00	50.0	-50.0	11.0	1.6	0.	0.	321.	0.	0.	.61
N410J3.009	.7	.0	46.6	.0	.01	50.0	-58.0	11.0	1.8	0.	0.	406.	0.	0.	.37
N410J3.010	.4	.0	46.5	.0	-.02	50.0	-66.0	11.0	1.0	0.	0.	406.	0.	0.	.05
N410J4.004	1.1	32.7	32.8	36.6	.24	50.0	.0	11.0	3.0	0.	0.	286.	0.	0.	5.58
N410J4.005	1.0	34.0	40.5	40.6	.21	50.0	-17.0	11.0	2.7	0.	0.	353.	0.	0.	5.09
N410J4.006	1.5	32.3	38.9	39.0	.19	50.0	-33.0	11.0	3.9	0.	0.	339.	0.	0.	4.39
N410J4.007	1.1	38.9	38.9	39.0	.09	50.0	-42.0	11.0	2.8	0.	0.	339.	0.	0.	2.30
N410J4.008	.7	.0	36.3	.0	.02	50.0	-50.0	11.0	2.0	0.	0.	317.	0.	0.	.74
N410J4.009	.4	.0	53.9	.0	.03	50.0	-58.0	11.0	1.2	0.	0.	470.	0.	0.	.69
N410J4.010	.3	.0	54.0	.0	.02	50.0	-66.0	11.0	.7	0.	0.	471.	0.	0.	.44

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410J5.004	1.4	14.0	26.0	33.0	.21	50.0	.0	11.0	3.6	0.	0.	227.	0.	0.	5.05
N410J5.005	1.0	39.7	39.7	39.8	.21	50.0	-17.0	11.0	2.8	0.	0.	346.	0.	0.	4.96
N410J5.006	1.0	34.3	34.3	34.3	.20	50.0	-33.0	11.0	2.8	0.	0.	299.	0.	0.	4.72
N410J5.007	1.3	38.5	39.9	44.1	.13	50.0	-42.0	11.0	3.4	0.	0.	348.	0.	0.	3.08
N410J5.008	1.0	.0	30.9	.0	.04	50.0	-50.0	11.0	2.6	0.	0.	269.	0.	0.	.99
N410J5.009	.8	.0	43.6	.0	.03	50.0	-58.0	11.0	2.2	0.	0.	380.	0.	0.	.70
N410J5.010	.3	.0	58.5	.0	.00	50.0	-66.0	11.0	.7	0.	0.	510.	0.	0.	.26
N410K1.004	1.0	22.2	33.5	33.5	.12	50.0	.0	17.0	2.8	0.	0.	292.	0.	0.	2.94
N410K1.005	1.6	22.8	39.1	39.1	.14	50.0	-17.0	17.0	4.1	0.	0.	341.	0.	0.	3.49
N410K1.006	1.2	32.1	36.5	36.5	.13	50.0	-33.0	17.0	3.1	0.	0.	318.	0.	0.	3.19
N410K1.007	1.1	31.7	37.0	37.0	.06	50.0	-42.0	17.0	2.8	0.	0.	322.	0.	0.	1.83
N410K1.008	.7	.0	13.8	.0	.00	50.0	-50.0	17.0	1.9	0.	0.	120.	0.	0.	.46
N410K1.009	.3	.0	17.3	.0	-.01	50.0	-58.0	17.0	.9	0.	0.	151.	0.	0.	.16
N410K1.010	.1	.0	.0	.0	-.02	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.05
N410K2.004	1.2	32.8	32.8	39.9	.10	50.0	.0	17.0	3.2	0.	0.	286.	0.	0.	2.72
N410K2.005	1.0	43.7	43.7	43.7	.15	50.0	-17.0	17.0	2.8	0.	0.	381.	0.	0.	3.77
N410K2.006	1.1	27.0	31.5	32.7	.10	50.0	-33.0	17.0	2.8	0.	0.	274.	0.	0.	2.68
N410K2.007	1.0	.0	26.8	.0	.02	50.0	-42.0	17.0	2.6	0.	0.	233.	0.	0.	1.19
N410K2.008	.9	.0	46.1	.0	-.02	50.0	-50.0	17.0	2.4	0.	0.	402.	0.	0.	.29
N410K2.009	.2	.0	26.1	.0	.00	50.0	-58.0	17.0	.6	0.	0.	228.	0.	0.	.10
N410K2.010	.2	.0	41.9	.0	.00	50.0	-66.0	17.0	.6	0.	0.	365.	0.	0.	.20
N410K3.004	1.4	34.0	38.4	42.4	.11	50.0	.0	17.0	3.6	0.	0.	334.	0.	0.	2.86
N410K3.005	1.5	28.5	38.6	42.1	.18	50.0	-17.0	17.0	4.0	0.	0.	337.	0.	0.	4.28
N410K3.006	1.1	23.7	40.1	40.9	.12	50.0	-33.0	17.0	3.0	0.	0.	350.	0.	0.	3.01
N410K3.007	1.3	23.8	24.2	42.1	.06	50.0	-42.0	17.0	3.3	0.	0.	211.	0.	0.	1.86
N410K3.008	.7	.0	37.2	.0	-.01	50.0	-50.0	17.0	1.9	0.	0.	324.	0.	0.	.30
N410K3.009	.3	.0	19.2	.0	.00	50.0	-58.0	17.0	.7	0.	0.	167.	0.	0.	.19
N410K3.010	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.19
N410K4.004	1.6	35.8	37.8	38.2	.13	50.0	.0	17.0	4.2	0.	0.	330.	0.	0.	3.22
N410K4.005	1.0	26.9	26.9	26.9	.16	50.0	-17.0	17.0	2.7	0.	0.	234.	0.	0.	4.02
N410K4.006	1.2	27.8	27.9	39.9	.08	50.0	-33.0	17.0	3.1	0.	0.	243.	0.	0.	2.33
N410K4.007	.9	.0	40.1	.0	.01	50.0	-42.0	17.0	2.4	0.	0.	350.	0.	0.	1.10
N410K4.008	.6	.0	33.4	.0	-.01	50.0	-50.0	17.0	1.5	0.	0.	291.	0.	0.	.13
N410K4.009	.4	.0	54.5	.0	.00	50.0	-58.0	17.0	1.1	0.	0.	475.	0.	0.	.11
N410K4.010	.0	.0	.0	.0	-.01	50.0	-66.0	17.0	.1	0.	0.	0.	0.	0.	.08
N410K5.004	1.3	34.4	37.8	46.6	.13	50.0	.0	17.0	3.4	0.	0.	329.	0.	0.	3.30
N410K5.005	1.4	33.2	33.5	36.3	.18	50.0	-17.0	17.0	3.6	0.	0.	292.	0.	0.	4.23
N410K5.006	1.1	33.3	33.3	33.3	.11	50.0	-33.0	17.0	2.9	0.	0.	290.	0.	0.	2.88
N410K5.007	1.0	26.1	26.1	36.4	.03	50.0	-42.0	17.0	2.7	0.	0.	227.	0.	0.	1.31
N410K5.008	.6	.0	37.7	.0	.00	50.0	-50.0	17.0	1.6	0.	0.	328.	0.	0.	.27
N410K5.009	.3	.0	39.1	.0	-.01	50.0	-58.0	17.0	.8	0.	0.	341.	0.	0.	.18
N410K5.010	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.24

FALCON 4: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410L1.004	.1	.0	.0	.0	-.01	150.0	80.0	1.0	.2	0.	0.	0.	0.	0.	.17
N410L1.005	.1	.0	.0	.0	-.02	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.06
N410L1.006	.0	.0	.0	.0	-.03	150.0	56.0	1.0	.1	0.	0.	0.	0.	0.	.05
N410L1.007	.1	.0	.0	.0	-.04	150.0	28.0	1.0	.4	0.	0.	0.	0.	0.	.15
N410L1.008	.2	.0	.0	.0	-.04	150.0	25.0	1.0	.4	0.	0.	0.	0.	0.	.05
N410L1.009	.3	.0	36.6	.0	.03	150.0	17.0	1.0	.9	0.	0.	319.	0.	0.	.89
N410L1.010	.6	.0	41.2	.0	.15	150.0	.0	1.0	1.7	0.	0.	359.	0.	0.	3.46
N410L2.004	.1	.0	.0	.0	-.04	150.0	80.0	1.0	.2	0.	0.	0.	0.	0.	.02
N410L2.005	.0	.0	.0	.0	-.04	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.01
N410L2.006	.1	.0	.0	.0	.00	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.08
N410L2.007	.3	.0	47.0	.0	.04	150.0	28.0	1.0	.8	0.	0.	410.	0.	0.	1.11
N410L2.008	.3	.0	35.3	.0	.01	150.0	25.0	1.0	.9	0.	0.	308.	0.	0.	.25
N410L2.009	.5	.0	43.3	.0	.07	150.0	17.0	1.0	1.2	0.	0.	377.	0.	0.	1.74
N410L2.010	.6	.0	30.2	.0	.14	150.0	.0	1.0	1.5	0.	0.	263.	0.	0.	3.36
N410L3.004	.1	.0	.0	.0	.01	150.0	80.0	1.0	.3	0.	0.	0.	0.	0.	.39
N410L3.005	.1	.0	.0	.0	.00	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.18
N410L3.006	.1	.0	.0	.0	.01	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.56
N410L3.007	.2	.0	31.6	.0	.00	150.0	28.0	1.0	.7	0.	0.	276.	0.	0.	.54
N410L3.008	.3	.0	42.9	.0	.05	150.0	25.0	1.0	.9	0.	0.	374.	0.	0.	1.09
N410L3.009	.6	.0	42.7	.0	.08	150.0	17.0	1.0	1.6	0.	0.	372.	0.	0.	2.03
N410L3.010	.6	.0	41.8	.0	.15	150.0	.0	1.0	1.6	0.	0.	364.	0.	0.	3.60
N410L4.004	.1	.0	.0	.0	.01	150.0	80.0	1.0	.4	0.	0.	0.	0.	0.	.43
N410L4.005	.1	.0	.0	.0	.00	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.29
N410L4.006	.1	.0	.0	.0	.03	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.80
N410L4.007	.3	.0	35.8	.0	.06	150.0	28.0	1.0	.9	0.	0.	312.	0.	0.	1.55
N410L4.008	.3	.0	43.4	.0	.04	150.0	25.0	1.0	.9	0.	0.	378.	0.	0.	1.09
N410L4.009	.5	.0	44.2	.0	.07	150.0	17.0	1.0	1.4	0.	0.	386.	0.	0.	1.61
N410L4.010	.5	.0	38.6	.0	.12	150.0	.0	1.0	1.4	0.	0.	337.	0.	0.	3.02
N410L5.004	.1	.0	.0	.0	.00	150.0	80.0	1.0	.3	0.	0.	0.	0.	0.	.35
N410L5.005	.1	.0	.0	.0	.01	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.30
N410L5.006	.1	.0	.0	.0	.03	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.69
N410L5.007	.2	.0	.0	.0	.01	150.0	28.0	1.0	.4	0.	0.	0.	0.	0.	.61
N410L5.008	.3	.0	45.3	.0	.04	150.0	25.0	1.0	.9	0.	0.	395.	0.	0.	.99
N410L5.009	.5	.0	41.8	.0	.07	150.0	17.0	1.0	1.2	0.	0.	365.	0.	0.	1.80
N410L5.010	.7	.0	43.8	.0	.17	150.0	.0	1.0	1.9	0.	0.	382.	0.	0.	4.03
N410M1.004	.1	.0	.0	.0	.01	150.0	80.0	5.0	.2	0.	0.	0.	0.	0.	.39
N410M1.005	.1	.0	.0	.0	.00	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.11
N410M1.006	.1	.0	.0	.0	.00	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.33
N410M1.007	.3	.0	24.3	.0	-.01	150.0	28.0	5.0	.7	0.	0.	212.	0.	0.	.33
N410M1.008	.3	.0	49.9	.0	.02	150.0	25.0	5.0	.7	0.	0.	435.	0.	0.	.43
N410M1.009	.5	.0	42.8	.0	.04	150.0	17.0	5.0	1.2	0.	0.	374.	0.	0.	1.13
N410M1.010	.5	.0	44.7	.0	.12	150.0	.0	5.0	1.4	0.	0.	389.	0.	0.	2.94

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410M2.004	.1	.0	.0	.0	-.01	150.0	80.0	5.0	.2	0.	0.	0.	0.	0.	.09
N410M2.005	.1	.0	.0	.0	.00	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.21
N410M2.006	.1	.0	.0	.0	.02	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.51
N410M2.007	.3	.0	15.8	.0	.04	150.0	28.0	5.0	.7	0.	0.	138.	0.	0.	1.02
N410M2.008	.3	.0	27.2	.0	.01	150.0	25.0	5.0	.8	0.	0.	237.	0.	0.	.40
N410M2.009	.4	.0	36.8	.0	.03	150.0	17.0	5.0	1.2	0.	0.	321.	0.	0.	.90
N410M2.010	.7	.0	46.2	.0	.15	150.0	.0	5.0	1.8	0.	0.	403.	0.	0.	3.63
N410M3.004	.1	.0	.0	.0	.01	150.0	80.0	5.0	.3	0.	0.	0.	0.	0.	.41
N410M3.005	.1	.0	.0	.0	.01	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.37
N410M3.006	.1	.0	.0	.0	.00	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.25
N410M3.007	.4	.0	38.8	.0	.05	150.0	28.0	5.0	1.2	0.	0.	338.	0.	0.	1.15
N410M3.008	.3	.0	38.3	.0	.01	150.0	25.0	5.0	.9	0.	0.	334.	0.	0.	.52
N410M3.009	.5	.0	35.0	.0	.04	150.0	17.0	5.0	1.4	0.	0.	305.	0.	0.	1.15
N410M3.010	.7	.0	36.2	.0	.10	150.0	.0	5.0	1.8	0.	0.	316.	0.	0.	2.45
N410M4.004	.1	.0	.0	.0	-.01	150.0	80.0	5.0	.2	0.	0.	0.	0.	0.	.20
N410M4.005	.1	.0	.0	.0	-.02	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.01
N410M4.006	.1	.0	.0	.0	-.02	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.07
N410M4.007	.2	.0	44.7	.0	.01	150.0	28.0	5.0	.6	0.	0.	390.	0.	0.	.48
N410M4.008	.4	.0	37.5	.0	-.02	150.0	25.0	5.0	1.2	0.	0.	327.	0.	0.	.14
N410M4.009	.4	.0	35.3	.0	.02	150.0	17.0	5.0	.9	0.	0.	308.	0.	0.	.77
N410M4.010	.7	.0	41.6	.0	.12	150.0	.0	5.0	1.8	0.	0.	362.	0.	0.	2.83
N410M5.004	.1	.0	.0	.0	-.01	150.0	80.0	5.0	.2	0.	0.	0.	0.	0.	.12
N410M5.005	.1	.0	.0	.0	-.01	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.10
N410M5.006	.1	.0	.0	.0	.01	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.15
N410M5.007	.3	.0	40.5	.0	-.02	150.0	28.0	5.0	.8	0.	0.	353.	0.	0.	.26
N410M5.008	.2	.0	.0	.0	.01	150.0	25.0	5.0	.5	0.	0.	0.	0.	0.	.29
N410M5.009	.5	.0	39.5	.0	.03	150.0	17.0	5.0	1.3	0.	0.	344.	0.	0.	.73
N410M5.010	.5	.0	38.5	.0	.09	150.0	.0	5.0	1.4	0.	0.	336.	0.	0.	2.26
N410N1.004	.1	.0	.0	.0	.01	150.0	80.0	11.0	.2	0.	0.	0.	0.	0.	.26
N410N1.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.24
N410N1.006	.1	.0	.0	.0	.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.30
N410N1.007	.4	.0	37.9	.0	.01	150.0	28.0	11.0	1.1	0.	0.	330.	0.	0.	.48
N410N1.008	.4	.0	30.9	.0	.04	150.0	25.0	11.0	1.1	0.	0.	270.	0.	0.	.88
N410N1.009	.5	.0	37.8	.0	.03	150.0	17.0	11.0	1.4	0.	0.	330.	0.	0.	.92
N410N1.010	.5	.0	40.2	.0	.09	150.0	.0	11.0	1.4	0.	0.	351.	0.	0.	2.21
N410N2.004	.1	.0	.0	.0	.00	150.0	80.0	11.0	.3	0.	0.	0.	0.	0.	.11
N410N2.005	.0	.0	.0	.0	-.02	150.0	75.0	11.0	.0	0.	0.	0.	0.	0.	.06
N410N2.006	.1	.0	.0	.0	-.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.09
N410N2.007	.3	.0	34.0	.0	-.01	150.0	28.0	11.0	.7	0.	0.	297.	0.	0.	.27
N410N2.008	.3	.0	39.4	.0	.00	150.0	25.0	11.0	.8	0.	0.	344.	0.	0.	.28
N410N2.009	.4	.0	29.7	.0	.04	150.0	17.0	11.0	1.2	0.	0.	259.	0.	0.	1.06
N410N2.010	.6	.0	38.3	.0	.12	150.0	.0	11.0	1.5	0.	0.	334.	0.	0.	2.90

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410N3.004	.1	.0	.0	.0	.02	150.0	80.0	11.0	.2	0.	0.	0.	0.	0.	.54
N410N3.005	.1	.0	.0	.0	.04	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.93
N410N3.006	.1	.0	.0	.0	.01	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.33
N410N3.007	.4	.0	31.2	.0	-.01	150.0	28.0	11.0	1.0	0.	0.	272.	0.	0.	.22
N410N3.008	.4	.0	43.6	.0	-.02	150.0	25.0	11.0	1.0	0.	0.	380.	0.	0.	.21
N410N3.009	.4	.0	39.1	.0	.02	150.0	17.0	11.0	1.2	0.	0.	341.	0.	0.	.76
N410N3.010	.6	.0	34.2	.0	.09	150.0	.0	11.0	1.5	0.	0.	298.	0.	0.	2.30
N410N4.004	.1	.0	.0	.0	.00	150.0	80.0	11.0	.2	0.	0.	0.	0.	0.	.18
N410N4.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.15
N410N4.006	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.09
N410N4.007	.2	.0	40.6	.0	.00	150.0	28.0	11.0	.6	0.	0.	354.	0.	0.	.31
N410N4.008	.3	.0	35.1	.0	.01	150.0	25.0	11.0	.9	0.	0.	306.	0.	0.	.27
N410N4.009	.5	.0	40.5	.0	.02	150.0	17.0	11.0	1.2	0.	0.	353.	0.	0.	.65
N410N4.010	.7	.0	37.8	.0	.12	150.0	.0	11.0	1.8	0.	0.	330.	0.	0.	2.77
N410N5.004	.1	.0	.0	.0	.00	150.0	80.0	11.0	.2	0.	0.	0.	0.	0.	.19
N410N5.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.12
N410N5.006	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.07
N410N5.007	.4	.0	39.9	.0	.03	150.0	28.0	11.0	1.1	0.	0.	348.	0.	0.	.74
N410N5.008	.4	.0	39.1	.0	.03	150.0	25.0	11.0	1.2	0.	0.	341.	0.	0.	.65
N410N5.009	.5	.0	32.3	.0	.04	150.0	17.0	11.0	1.3	0.	0.	281.	0.	0.	.96
N410N5.010	.5	.0	46.4	.0	.08	150.0	.0	11.0	1.4	0.	0.	404.	0.	0.	1.99
N41001.004	.0	.0	.0	.0	-.04	150.0	80.0	17.0	.1	0.	0.	0.	0.	0.	.01
N41001.005	.1	.0	.0	.0	-.03	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.02
N41001.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.19
N41001.007	.3	.0	41.4	.0	.02	150.0	28.0	17.0	.7	0.	0.	361.	0.	0.	.57
N41001.008	.4	.0	41.4	.0	.02	150.0	25.0	17.0	1.1	0.	0.	361.	0.	0.	.55
N41001.009	.5	.0	33.4	.0	.03	150.0	17.0	17.0	1.3	0.	0.	291.	0.	0.	.82
N41001.010	.7	.0	33.7	.0	.09	150.0	.0	17.0	1.8	0.	0.	294.	0.	0.	2.10
N41002.004	.1	.0	.0	.0	.01	150.0	80.0	17.0	.1	0.	0.	0.	0.	0.	.31
N41002.005	.1	.0	.0	.0	.00	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.00
N41002.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.06
N41002.007	.3	.0	20.5	.0	.02	150.0	28.0	17.0	.7	0.	0.	178.	0.	0.	.52
N41002.008	.2	.0	45.7	.0	.01	150.0	25.0	17.0	.6	0.	0.	399.	0.	0.	.17
N41002.009	.4	.0	22.3	.0	.03	150.0	17.0	17.0	1.1	0.	0.	194.	0.	0.	.68
N41002.010	.6	.0	41.2	.0	.11	150.0	.0	17.0	1.7	0.	0.	359.	0.	0.	2.62
N41003.004	.1	.0	.0	.0	.00	150.0	80.0	17.0	.1	0.	0.	0.	0.	0.	.23
N41003.005	.0	.0	.0	.0	-.01	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.16
N41003.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.16
N41003.007	.3	.0	36.6	.0	.03	150.0	28.0	17.0	.8	0.	0.	319.	0.	0.	.80
N41003.008	.2	.0	26.5	.0	.02	150.0	25.0	17.0	.5	0.	0.	231.	0.	0.	.49
N41003.009	.5	.0	46.9	.0	.03	150.0	17.0	17.0	1.4	0.	0.	409.	0.	0.	.80
N41003.010	.6	.0	30.8	.0	.09	150.0	.0	17.0	1.7	0.	0.	269.	0.	0.	2.06

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N41004.004	.1	.0	.0	.0	.00	150.0	80.0	17.0	.1	0.	0.	0.	0.	0.	.22
N41004.005	.1	.0	.0	.0	.02	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.45
N41004.006	.1	.0	.0	.0	.01	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.34
N41004.007	.3	.0	35.7	.0	.02	150.0	28.0	17.0	.8	0.	0.	311.	0.	0.	.73
N41004.008	.3	.0	45.8	.0	.03	150.0	25.0	17.0	.9	0.	0.	400.	0.	0.	.86
N41004.009	.6	.0	36.4	.0	.04	150.0	17.0	17.0	1.6	0.	0.	317.	0.	0.	.92
N41004.010	.6	.0	27.5	.0	.06	150.0	.0	17.0	1.6	0.	0.	240.	0.	0.	1.52
N41005.004	.1	.0	.0	.0	.00	150.0	80.0	17.0	.2	0.	0.	0.	0.	0.	.21
N41005.005	.1	.0	.0	.0	.01	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.21
N41005.006	.1	.0	.0	.0	.01	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.49
N41005.007	.3	.0	42.4	.0	.01	150.0	28.0	17.0	.8	0.	0.	370.	0.	0.	.43
N41005.008	.3	.0	34.7	.0	.01	150.0	25.0	17.0	.9	0.	0.	302.	0.	0.	.19
N41005.009	.5	.0	34.3	.0	.03	150.0	17.0	17.0	1.4	0.	0.	299.	0.	0.	.82
N41005.010	.5	.0	34.5	.0	.08	150.0	.0	17.0	1.4	0.	0.	301.	0.	0.	1.96
N410P1.004	.7	.0	42.3	.0	.17	150.0	.0	1.0	1.8	0.	0.	369.	0.	0.	4.05
N410P1.005	.6	.0	41.8	.0	.13	150.0	-17.0	1.0	1.6	0.	0.	364.	0.	0.	3.12
N410P1.006	.7	.0	41.9	.0	.14	150.0	-25.0	1.0	1.8	0.	0.	365.	0.	0.	3.39
N410P1.007	.6	.0	38.4	.0	.13	150.0	-28.0	1.0	1.6	0.	0.	335.	0.	0.	3.41
N410P1.008	.6	.0	44.2	.0	.17	150.0	-56.0	1.0	1.6	0.	0.	386.	0.	0.	3.99
N410P1.009	.5	.0	40.9	.0	.09	150.0	-75.0	1.0	1.3	0.	0.	357.	0.	0.	2.17
N410P1.010	.6	.0	33.3	.0	.09	150.0	-80.0	1.0	1.6	0.	0.	290.	0.	0.	2.26
N410P2.004	.5	.0	35.8	.0	.14	150.0	.0	1.0	1.3	0.	0.	312.	0.	0.	3.35
N410P2.005	.6	.0	37.6	.0	.15	150.0	-17.0	1.0	1.5	0.	0.	328.	0.	0.	3.65
N410P2.006	.8	.0	31.8	.0	.18	150.0	-25.0	1.0	2.0	0.	0.	277.	0.	0.	4.29
N410P2.007	.6	.0	31.9	.0	.13	150.0	-28.0	1.0	1.7	0.	0.	278.	0.	0.	3.36
N410P2.008	.7	.0	42.2	.0	.17	150.0	-56.0	1.0	1.9	0.	0.	368.	0.	0.	4.09
N410P2.009	.5	.0	30.2	.0	.11	150.0	-75.0	1.0	1.5	0.	0.	263.	0.	0.	2.54
N410P2.010	.5	.0	35.1	.0	.09	150.0	-80.0	1.0	1.3	0.	0.	306.	0.	0.	2.27
N410P3.004	.6	.0	31.7	.0	.15	150.0	.0	1.0	1.6	0.	0.	276.	0.	0.	3.56
N410P3.005	.6	.0	41.2	.0	.17	150.0	-17.0	1.0	1.6	0.	0.	359.	0.	0.	4.04
N410P3.006	.7	.0	37.1	.0	.20	150.0	-25.0	1.0	1.8	0.	0.	323.	0.	0.	4.58
N410P3.007	.6	.0	22.8	.0	.17	150.0	-28.0	1.0	1.6	0.	0.	199.	0.	0.	4.15
N410P3.008	.5	.0	33.0	.0	.12	150.0	-56.0	1.0	1.3	0.	0.	287.	0.	0.	2.90
N410P3.009	.5	.0	37.4	.0	.07	150.0	-75.0	1.0	1.4	0.	0.	326.	0.	0.	1.87
N410P3.010	.4	.0	35.6	.0	.04	150.0	-80.0	1.0	1.0	0.	0.	311.	0.	0.	1.36
N410P4.004	.6	.0	38.5	.0	.17	150.0	.0	1.0	1.6	0.	0.	336.	0.	0.	4.02
N410P4.005	.6	.0	38.7	.0	.18	150.0	-17.0	1.0	1.6	0.	0.	338.	0.	0.	4.28
N410P4.006	.8	.0	39.7	.0	.21	150.0	-25.0	1.0	2.2	0.	0.	346.	0.	0.	5.03
N410P4.007	.7	.0	40.0	.0	.15	150.0	-28.0	1.0	2.0	0.	0.	349.	0.	0.	3.86
N410P4.008	.6	.0	37.7	.0	.15	150.0	-56.0	1.0	1.5	0.	0.	328.	0.	0.	3.54
N410P4.009	.4	.0	40.7	.0	.09	150.0	-75.0	1.0	1.1	0.	0.	355.	0.	0.	2.17
N410P4.010	.4	.0	41.1	.0	.05	150.0	-80.0	1.0	1.0	0.	0.	358.	0.	0.	1.20

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410P5.004	.5	.0	31.3	.0	.13	150.0	.0	1.0	1.4	0.	0.	273.	0.	0.	3.38
N410P5.005	.6	.0	43.5	.0	.16	150.0	-17.0	1.0	1.7	0.	0.	380.	0.	0.	3.68
N410P5.006	.8	.0	43.3	.0	.19	150.0	-25.0	1.0	2.1	0.	0.	378.	0.	0.	4.36
N410P5.007	.6	.0	37.7	.0	.19	150.0	-28.0	1.0	1.7	0.	0.	328.	0.	0.	4.50
N410P5.008	.6	.0	40.2	.0	.16	150.0	-56.0	1.0	1.5	0.	0.	350.	0.	0.	3.68
N410P5.009	.7	.0	41.1	.0	.10	150.0	-75.0	1.0	1.8	0.	0.	358.	0.	0.	2.50
N410P5.010	.5	.0	40.3	.0	.09	150.0	-80.0	1.0	1.3	0.	0.	351.	0.	0.	2.21
N410Q1.004	.7	.0	39.6	.0	.15	150.0	.0	5.0	1.8	0.	0.	345.	0.	0.	3.47
N410Q1.005	.7	.0	38.6	.0	.15	150.0	-17.0	5.0	1.8	0.	0.	337.	0.	0.	3.52
N410Q1.006	.8	.0	38.8	.0	.18	150.0	-25.0	5.0	2.1	0.	0.	338.	0.	0.	4.19
N410Q1.007	.7	.0	32.4	.0	.16	150.0	-28.0	5.0	1.9	0.	0.	283.	0.	0.	3.90
N410Q1.008	.7	.0	37.3	.0	.15	150.0	-56.0	5.0	1.9	0.	0.	325.	0.	0.	3.58
N410Q1.009	.6	.0	42.4	.0	.05	150.0	-75.0	5.0	1.6	0.	0.	370.	0.	0.	1.44
N410Q1.010	.5	.0	42.1	.0	.05	150.0	-80.0	5.0	1.3	0.	0.	367.	0.	0.	1.36
N410Q2.004	.6	.0	28.6	.0	.13	150.0	.0	5.0	1.6	0.	0.	250.	0.	0.	3.08
N410Q2.005	.7	.0	42.7	.0	.18	150.0	-17.0	5.0	1.9	0.	0.	372.	0.	0.	4.19
N410Q2.006	.8	.0	42.7	.0	.18	150.0	-25.0	5.0	2.0	0.	0.	372.	0.	0.	4.32
N410Q2.007	.7	.0	40.5	.0	.17	150.0	-28.0	5.0	1.8	0.	0.	353.	0.	0.	4.15
N410Q2.008	.6	.0	35.9	.0	.12	150.0	-56.0	5.0	1.6	0.	0.	313.	0.	0.	2.86
N410Q2.009	.5	.0	46.4	.0	.05	150.0	-75.0	5.0	1.3	0.	0.	405.	0.	0.	1.40
N410Q2.010	.5	.0	46.7	.0	.04	150.0	-80.0	5.0	1.3	0.	0.	407.	0.	0.	1.19
N410Q3.004	.6	.0	35.4	.0	.14	150.0	.0	5.0	1.7	0.	0.	309.	0.	0.	3.41
N410Q3.005	.7	.0	49.3	.0	.15	150.0	-17.0	5.0	1.8	0.	0.	430.	0.	0.	3.54
N410Q3.006	.7	.0	35.6	.0	.17	150.0	-25.0	5.0	1.8	0.	0.	311.	0.	0.	4.06
N410Q3.007	.8	.0	35.7	.0	.18	150.0	-28.0	5.0	2.0	0.	0.	311.	0.	0.	4.29
N410Q3.008	.6	.0	34.1	.0	.13	150.0	-56.0	5.0	1.7	0.	0.	297.	0.	0.	3.17
N410Q3.009	.5	.0	34.0	.0	.09	150.0	-75.0	5.0	1.4	0.	0.	296.	0.	0.	2.07
N410Q3.010	.5	.0	33.9	.0	.08	150.0	-80.0	5.0	1.3	0.	0.	296.	0.	0.	1.85
N410Q4.004	.6	.0	33.3	.0	.12	150.0	.0	5.0	1.5	0.	0.	290.	0.	0.	2.93
N410Q4.005	.6	.0	42.9	.0	.14	150.0	-17.0	5.0	1.6	0.	0.	374.	0.	0.	3.19
N410Q4.006	.7	.0	42.7	.0	.15	150.0	-25.0	5.0	1.8	0.	0.	373.	0.	0.	3.57
N410Q4.007	.6	.0	31.6	.0	.13	150.0	-28.0	5.0	1.6	0.	0.	275.	0.	0.	3.22
N410Q4.008	.7	.0	42.0	.0	.14	150.0	-56.0	5.0	1.9	0.	0.	366.	0.	0.	3.36
N410Q4.009	.7	.0	39.5	.0	.10	150.0	-75.0	5.0	1.8	0.	0.	344.	0.	0.	2.34
N410Q4.010	.7	.0	39.7	.0	.08	150.0	-80.0	5.0	1.8	0.	0.	346.	0.	0.	2.04
N410Q5.004	.6	.0	42.6	.0	.13	150.0	.0	5.0	1.7	0.	0.	372.	0.	0.	3.04
N410Q5.005	.8	.0	42.5	.0	.15	150.0	-17.0	5.0	2.1	0.	0.	370.	0.	0.	3.48
N410Q5.006	.8	.0	40.8	.0	.19	150.0	-25.0	5.0	2.2	0.	0.	356.	0.	0.	4.56
N410Q5.007	.9	.0	41.9	.0	.17	150.0	-28.0	5.0	2.3	0.	0.	365.	0.	0.	4.17
N410Q5.008	.7	.0	38.9	.0	.13	150.0	-56.0	5.0	1.9	0.	0.	339.	0.	0.	3.18
N410Q5.009	.6	.0	43.2	.0	.07	150.0	-75.0	5.0	1.6	0.	0.	377.	0.	0.	1.61
N410Q5.010	.6	.0	43.1	.0	.05	150.0	-80.0	5.0	1.5	0.	0.	376.	0.	0.	1.23

FALCON 4: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410R1.004	.6	.0	38.3	.0	.12	150.0	.0	11.0	1.5	0.	0.	334.	0.	0.	2.96
N410R1.005	.7	.0	43.2	.0	.11	150.0	-17.0	11.0	1.8	0.	0.	377.	0.	0.	2.53
N410R1.006	.7	.0	41.7	.0	.13	150.0	-25.0	11.0	1.9	0.	0.	363.	0.	0.	3.16
N410R1.007	.7	.0	44.0	.0	.11	150.0	-28.0	11.0	1.8	0.	0.	383.	0.	0.	2.68
N410R1.008	.7	.0	44.2	.0	.08	150.0	-56.0	11.0	1.9	0.	0.	386.	0.	0.	2.09
N410R1.009	.6	.0	44.2	.0	.03	150.0	-75.0	11.0	1.7	0.	0.	385.	0.	0.	.91
N410R1.010	.7	.0	44.3	.0	.04	150.0	-80.0	11.0	1.8	0.	0.	386.	0.	0.	1.02
N410R2.004	.6	.0	40.5	.0	.13	150.0	.0	11.0	1.7	0.	0.	353.	0.	0.	3.02
N410R2.005	.7	.0	33.6	.0	.12	150.0	-17.0	11.0	1.8	0.	0.	293.	0.	0.	2.79
N410R2.006	.7	.0	31.5	.0	.12	150.0	-25.0	11.0	1.9	0.	0.	274.	0.	0.	2.78
N410R2.007	.7	.0	31.8	.0	.11	150.0	-28.0	11.0	1.8	0.	0.	277.	0.	0.	2.84
N410R2.008	.6	.0	38.0	.0	.08	150.0	-56.0	11.0	1.5	0.	0.	331.	0.	0.	2.04
N410R2.009	.5	.0	38.7	.0	.06	150.0	-75.0	11.0	1.5	0.	0.	337.	0.	0.	1.51
N410R2.010	.4	.0	41.6	.0	.04	150.0	-80.0	11.0	1.1	0.	0.	363.	0.	0.	1.18
N410R3.004	.6	.0	41.9	.0	.11	150.0	.0	11.0	1.5	0.	0.	365.	0.	0.	2.56
N410R3.005	.6	.0	34.9	.0	.10	150.0	-17.0	11.0	1.5	0.	0.	305.	0.	0.	2.52
N410R3.006	.6	.0	41.8	.0	.11	150.0	-25.0	11.0	1.6	0.	0.	364.	0.	0.	2.75
N410R3.007	.6	.0	34.9	.0	.11	150.0	-28.0	11.0	1.7	0.	0.	304.	0.	0.	2.80
N410R3.008	.6	.0	39.8	.0	.09	150.0	-56.0	11.0	1.5	0.	0.	347.	0.	0.	2.08
N410R3.009	.4	.0	26.3	.0	.03	150.0	-75.0	11.0	1.2	0.	0.	230.	0.	0.	.87
N410R3.010	.3	.0	59.1	.0	.01	150.0	-80.0	11.0	.8	0.	0.	515.	0.	0.	.45
N410R4.004	.7	.0	40.5	.0	.11	150.0	.0	11.0	1.9	0.	0.	353.	0.	0.	2.57
N410R4.005	.7	.0	46.4	.0	.13	150.0	-17.0	11.0	1.8	0.	0.	405.	0.	0.	3.07
N410R4.006	.8	.0	37.7	.0	.12	150.0	-25.0	11.0	2.0	0.	0.	328.	0.	0.	2.87
N410R4.007	.7	.0	37.9	.0	.13	150.0	-28.0	11.0	1.9	0.	0.	330.	0.	0.	3.25
N410R4.008	.6	.0	37.2	.0	.08	150.0	-56.0	11.0	1.6	0.	0.	324.	0.	0.	1.98
N410R4.009	.7	.0	31.3	.0	.06	150.0	-75.0	11.0	1.7	0.	0.	273.	0.	0.	1.50
N410R4.010	.6	.0	37.8	.0	.06	150.0	-80.0	11.0	1.6	0.	0.	329.	0.	0.	1.44
N410R5.004	.6	.0	43.9	.0	.10	150.0	.0	11.0	1.6	0.	0.	383.	0.	0.	2.32
N410R5.005	.6	.0	34.1	.0	.12	150.0	-17.0	11.0	1.6	0.	0.	297.	0.	0.	2.81
N410R5.006	.8	.0	39.4	.0	.14	150.0	-25.0	11.0	2.0	0.	0.	343.	0.	0.	3.38
N410R5.007	.7	.0	40.3	.0	.13	150.0	-28.0	11.0	1.9	0.	0.	352.	0.	0.	3.11
N410R5.008	.7	.0	45.6	.0	.10	150.0	-56.0	11.0	1.8	0.	0.	398.	0.	0.	2.38
N410R5.009	.6	.0	34.3	.0	.07	150.0	-75.0	11.0	1.7	0.	0.	299.	0.	0.	1.78
N410R5.010	.5	.0	33.9	.0	.07	150.0	-80.0	11.0	1.5	0.	0.	296.	0.	0.	1.62
N410S1.004	.5	.0	29.1	.0	.08	150.0	.0	17.0	1.3	0.	0.	254.	0.	0.	1.95
N410S1.005	.7	.0	41.3	.0	.09	150.0	-17.0	17.0	1.7	0.	0.	360.	0.	0.	2.21
N410S1.006	.7	.0	35.0	.0	.08	150.0	-25.0	17.0	1.8	0.	0.	305.	0.	0.	1.95
N410S1.007	.7	.0	38.8	.0	.06	150.0	-28.0	17.0	1.7	0.	0.	338.	0.	0.	1.69
N410S1.008	.7	.0	34.9	.0	.05	150.0	-56.0	17.0	1.9	0.	0.	304.	0.	0.	1.29
N410S1.009	.4	.0	34.2	.0	.02	150.0	-75.0	17.0	1.1	0.	0.	298.	0.	0.	.53
N410S1.010	.3	.0	48.5	.0	.01	150.0	-80.0	17.0	.9	0.	0.	423.	0.	0.	.44

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410S2.004	.7	.0	41.8	.0	.09	150.0	.0	17.0	1.8	0.	0.	364.	0.	0.	2.19
N410S2.005	.7	.0	40.1	.0	.10	150.0	-17.0	17.0	1.9	0.	0.	350.	0.	0.	2.40
N410S2.006	.8	.0	44.9	.0	.12	150.0	-25.0	17.0	2.1	0.	0.	391.	0.	0.	2.77
N410S2.007	.7	.0	45.0	.0	.10	150.0	-28.0	17.0	1.9	0.	0.	392.	0.	0.	2.62
N410S2.008	.8	.0	44.7	.0	.06	150.0	-56.0	17.0	2.0	0.	0.	389.	0.	0.	1.37
N410S2.009	.5	.0	52.7	.0	.01	150.0	-75.0	17.0	1.2	0.	0.	459.	0.	0.	.38
N410S2.010	.3	.0	34.4	.0	.01	150.0	-80.0	17.0	.7	0.	0.	300.	0.	0.	.29
N410S3.004	.6	.0	42.5	.0	.10	150.0	.0	17.0	1.6	0.	0.	371.	0.	0.	2.35
N410S3.005	.6	.0	40.7	.0	.09	150.0	-17.0	17.0	1.7	0.	0.	355.	0.	0.	2.24
N410S3.006	.7	.0	39.9	.0	.05	150.0	-25.0	17.0	1.8	0.	0.	348.	0.	0.	1.59
N410S3.007	.8	.0	39.6	.0	.05	150.0	-28.0	17.0	2.2	0.	0.	345.	0.	0.	1.76
N410S3.008	.7	.0	39.7	.0	.05	150.0	-56.0	17.0	1.9	0.	0.	346.	0.	0.	1.35
N410S3.009	.4	.0	40.4	.0	.03	150.0	-75.0	17.0	1.1	0.	0.	352.	0.	0.	.73
N410S3.010	.3	.0	51.2	.0	.04	150.0	-80.0	17.0	.9	0.	0.	447.	0.	0.	.90
N410S4.004	.5	.0	36.4	.0	.08	150.0	.0	17.0	1.5	0.	0.	318.	0.	0.	1.99
N410S4.005	.5	.0	43.0	.0	.08	150.0	-17.0	17.0	1.5	0.	0.	375.	0.	0.	1.99
N410S4.006	.6	.0	32.2	.0	.07	150.0	-25.0	17.0	1.5	0.	0.	280.	0.	0.	1.95
N410S4.007	.7	.0	32.3	.0	.07	150.0	-28.0	17.0	1.9	0.	0.	282.	0.	0.	2.03
N410S4.008	.5	.0	36.2	.0	.06	150.0	-56.0	17.0	1.4	0.	0.	315.	0.	0.	1.46
N410S4.009	.6	.0	36.4	.0	.04	150.0	-75.0	17.0	1.7	0.	0.	318.	0.	0.	1.06
N410S4.010	.6	.0	36.4	.0	.05	150.0	-80.0	17.0	1.6	0.	0.	318.	0.	0.	1.23
N410S5.004	.6	.0	40.2	.0	.09	150.0	.0	17.0	1.6	0.	0.	351.	0.	0.	2.14
N410S5.005	.5	.0	38.6	.0	.08	150.0	-17.0	17.0	1.4	0.	0.	336.	0.	0.	2.02
N410S5.006	.7	.0	38.4	.0	.10	150.0	-25.0	17.0	1.7	0.	0.	335.	0.	0.	2.39
N410S5.007	.7	.0	38.4	.0	.09	150.0	-28.0	17.0	1.8	0.	0.	335.	0.	0.	2.38
N410S5.008	.6	.0	29.3	.0	.06	150.0	-56.0	17.0	1.6	0.	0.	255.	0.	0.	1.52
N410S5.009	.4	.0	32.7	.0	.02	150.0	-75.0	17.0	1.0	0.	0.	285.	0.	0.	.60
N410S5.010	.4	.0	42.7	.0	.01	150.0	-80.0	17.0	.9	0.	0.	372.	0.	0.	.53
N410T1.004	.2	.0	.0	.0	.04	250.0	28.0	1.0	.5	0.	0.	0.	0.	0.	1.08
N410T1.005	.2	.0	44.4	.0	.00	250.0	17.0	1.0	.7	0.	0.	387.	0.	0.	.31
N410T1.006	.5	.0	46.3	.0	.09	250.0	.0	1.0	1.3	0.	0.	403.	0.	0.	2.27
N410T1.007	.6	.0	45.7	.0	.12	250.0	-25.0	1.0	1.5	0.	0.	399.	0.	0.	2.98
N410T1.008	.6	.0	45.7	.0	.13	250.0	-33.0	1.0	1.5	0.	0.	398.	0.	0.	3.12
N410T1.009	.6	.0	44.4	.0	.15	250.0	-50.0	1.0	1.7	0.	0.	387.	0.	0.	3.59
N410T1.010	.6	.0	45.7	.0	.18	250.0	-58.0	1.0	1.6	0.	0.	398.	0.	0.	4.30
N410T2.004	.1	.0	.0	.0	-.04	250.0	28.0	1.0	.2	0.	0.	0.	0.	0.	.09
N410T2.005	.3	.0	43.6	.0	.01	250.0	17.0	1.0	.8	0.	0.	380.	0.	0.	.52
N410T2.006	.5	.0	45.3	.0	.10	250.0	.0	1.0	1.4	0.	0.	395.	0.	0.	2.47
N410T2.007	.5	.0	40.3	.0	.15	250.0	-25.0	1.0	1.3	0.	0.	351.	0.	0.	3.59
N410T2.008	.5	.0	40.1	.0	.16	250.0	-33.0	1.0	1.4	0.	0.	350.	0.	0.	3.77
N410T2.009	.6	.0	40.1	.0	.15	250.0	-50.0	1.0	1.5	0.	0.	349.	0.	0.	3.64
N410T2.010	.5	.0	40.3	.0	.13	250.0	-58.0	1.0	1.3	0.	0.	352.	0.	0.	2.98

FALCON 4: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410T3.004	.1	.0	.0	.0	.00	250.0	28.0	1.0	.2	0.	0.	0.	0.	0.	.24
N410T3.005	.2	.0	40.4	.0	.03	250.0	17.0	1.0	.6	0.	0.	352.	0.	0.	.74
N410T3.006	.5	.0	40.3	.0	.13	250.0	.0	1.0	1.4	0.	0.	351.	0.	0.	3.10
N410T3.007	.6	.0	46.1	.0	.14	250.0	-25.0	1.0	1.5	0.	0.	402.	0.	0.	3.33
N410T3.008	.6	.0	41.0	.0	.17	250.0	-33.0	1.0	1.5	0.	0.	358.	0.	0.	3.92
N410T3.009	.6	.0	47.0	.0	.17	250.0	-50.0	1.0	1.5	0.	0.	410.	0.	0.	3.89
N410T3.010	.5	.0	50.1	.0	.13	250.0	-58.0	1.0	1.3	0.	0.	437.	0.	0.	3.11
N410T4.004	.1	.0	.0	.0	.01	250.0	28.0	1.0	.3	0.	0.	0.	0.	0.	.41
N410T4.005	.2	.0	52.3	.0	.02	250.0	17.0	1.0	.6	0.	0.	456.	0.	0.	.59
N410T4.006	.5	.0	49.4	.0	.12	250.0	.0	1.0	1.4	0.	0.	431.	0.	0.	2.92
N410T4.007	.5	.0	50.8	.0	.12	250.0	-25.0	1.0	1.3	0.	0.	443.	0.	0.	2.93
N410T4.008	.5	.0	46.7	.0	.11	250.0	-33.0	1.0	1.3	0.	0.	407.	0.	0.	2.72
N410T4.009	.6	.0	47.6	.0	.15	250.0	-50.0	1.0	1.5	0.	0.	415.	0.	0.	3.43
N410T4.010	.4	.0	45.1	.0	.09	250.0	-58.0	1.0	1.1	0.	0.	393.	0.	0.	2.30
N410T5.004	.1	.0	.0	.0	-.02	250.0	28.0	1.0	.4	0.	0.	0.	0.	0.	.12
N410T5.005	.2	.0	.0	.0	.00	250.0	17.0	1.0	.5	0.	0.	0.	0.	0.	.31
N410T5.006	.4	.0	35.4	.0	.06	250.0	.0	1.0	1.0	0.	0.	309.	0.	0.	1.62
N410T5.007	.4	.0	45.6	.0	.07	250.0	-25.0	1.0	1.1	0.	0.	397.	0.	0.	2.04
N410T5.008	.4	.0	38.4	.0	.11	250.0	-33.0	1.0	1.2	0.	0.	335.	0.	0.	2.55
N410T5.009	.4	.0	49.3	.0	.10	250.0	-50.0	1.0	1.2	0.	0.	430.	0.	0.	2.54
N410T5.010	.4	.0	39.4	.0	.12	250.0	-58.0	1.0	1.0	0.	0.	344.	0.	0.	2.82
N410U1.004	.1	.0	.0	.0	-.01	250.0	28.0	5.0	.3	0.	0.	0.	0.	0.	.12
N410U1.005	.3	.0	46.9	.0	.01	250.0	17.0	5.0	.8	0.	0.	409.	0.	0.	.38
N410U1.006	.6	.0	42.5	.0	.08	250.0	.0	5.0	1.5	0.	0.	370.	0.	0.	1.99
N410U1.007	.4	.0	41.8	.0	.07	250.0	-25.0	5.0	1.0	0.	0.	365.	0.	0.	1.77
N410U1.008	.4	.0	40.9	.0	.09	250.0	-33.0	5.0	1.1	0.	0.	357.	0.	0.	2.04
N410U1.009	.5	.0	46.6	.0	.13	250.0	-50.0	5.0	1.4	0.	0.	406.	0.	0.	3.09
N410U1.010	.5	.0	39.3	.0	.13	250.0	-58.0	5.0	1.3	0.	0.	343.	0.	0.	3.03
N410U2.004	.4	.0	52.7	.0	.03	250.0	28.0	5.0	1.1	0.	0.	459.	0.	0.	.76
N410U2.005	.4	.0	43.1	.0	.04	250.0	17.0	5.0	1.2	0.	0.	376.	0.	0.	.98
N410U2.006	.6	.0	46.1	.0	.11	250.0	.0	5.0	1.5	0.	0.	402.	0.	0.	2.52
N410U2.007	.5	.0	41.8	.0	.13	250.0	-25.0	5.0	1.5	0.	0.	364.	0.	0.	3.17
N410U2.008	.5	.0	29.3	.0	.12	250.0	-33.0	5.0	1.4	0.	0.	255.	0.	0.	2.93
N410U2.009	.6	.0	43.4	.0	.15	250.0	-50.0	5.0	1.7	0.	0.	378.	0.	0.	3.52
N410U2.010	.5	.0	29.3	.0	.13	250.0	-58.0	5.0	1.3	0.	0.	255.	0.	0.	3.16
N410U3.004	.3	.0	39.9	.0	.01	250.0	28.0	5.0	.9	0.	0.	348.	0.	0.	.29
N410U3.005	.4	.0	35.9	.0	.06	250.0	17.0	5.0	1.2	0.	0.	313.	0.	0.	1.38
N410U3.006	.5	.0	33.3	.0	.13	250.0	.0	5.0	1.5	0.	0.	290.	0.	0.	3.03
N410U3.007	.6	.0	48.8	.0	.09	250.0	-25.0	5.0	1.5	0.	0.	426.	0.	0.	2.22
N410U3.008	.6	.0	47.2	.0	.14	250.0	-33.0	5.0	1.5	0.	0.	412.	0.	0.	3.35
N410U3.009	.6	.0	46.7	.0	.12	250.0	-50.0	5.0	1.7	0.	0.	407.	0.	0.	2.80
N410U3.010	.6	.0	43.3	.0	.12	250.0	-58.0	5.0	1.6	0.	0.	377.	0.	0.	2.92

FALCON 4: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410U4.004	.1	.0	.0	.0	.01	250.0	28.0	5.0	.3	0.	0.	0.	0.	0.	.34
N410U4.005	.2	.0	40.9	.0	.04	250.0	17.0	5.0	.6	0.	0.	357.	0.	0.	.96
N410U4.006	.5	.0	37.6	.0	.07	250.0	.0	5.0	1.3	0.	0.	327.	0.	0.	1.87
N410U4.007	.5	.0	36.3	.0	.12	250.0	-25.0	5.0	1.3	0.	0.	316.	0.	0.	2.83
N410U4.008	.5	.0	36.3	.0	.11	250.0	-33.0	5.0	1.2	0.	0.	316.	0.	0.	2.63
N410U4.009	.5	.0	48.5	.0	.14	250.0	-50.0	5.0	1.5	0.	0.	423.	0.	0.	3.35
N410U4.010	.5	.0	42.6	.0	.13	250.0	-58.0	5.0	1.3	0.	0.	371.	0.	0.	3.10
N410U5.004	.1	.0	.0	.0	.01	250.0	28.0	5.0	.3	0.	0.	0.	0.	0.	.35
N410U5.005	.2	.0	46.0	.0	.00	250.0	17.0	5.0	.6	0.	0.	401.	0.	0.	.22
N410U5.006	.5	.0	43.7	.0	.07	250.0	.0	5.0	1.3	0.	0.	381.	0.	0.	1.67
N410U5.007	.5	.0	44.1	.0	.11	250.0	-25.0	5.0	1.4	0.	0.	384.	0.	0.	2.65
N410U5.008	.6	.0	43.3	.0	.15	250.0	-33.0	5.0	1.7	0.	0.	378.	0.	0.	3.56
N410U5.009	.7	.0	47.3	.0	.13	250.0	-50.0	5.0	1.8	0.	0.	413.	0.	0.	3.13
N410U5.010	.5	.0	47.0	.0	.10	250.0	-58.0	5.0	1.3	0.	0.	409.	0.	0.	2.34
N410V1.004	.2	.0	.0	.0	.00	250.0	28.0	11.0	.5	0.	0.	0.	0.	0.	.25
N410V1.005	.3	.0	30.1	.0	.03	250.0	17.0	11.0	.9	0.	0.	262.	0.	0.	.82
N410V1.006	.5	.0	31.2	.0	.08	250.0	.0	11.0	1.4	0.	0.	272.	0.	0.	1.92
N410V1.007	.5	.0	48.0	.0	.07	250.0	-25.0	11.0	1.3	0.	0.	419.	0.	0.	1.94
N410V1.008	.5	.0	44.2	.0	.10	250.0	-33.0	11.0	1.3	0.	0.	385.	0.	0.	2.48
N410V1.009	.6	.0	44.0	.0	.08	250.0	-50.0	11.0	1.6	0.	0.	384.	0.	0.	2.00
N410V1.010	.5	.0	34.4	.0	.07	250.0	-58.0	11.0	1.3	0.	0.	300.	0.	0.	1.65
N410V2.004	.2	.0	.0	.0	-.01	250.0	28.0	11.0	.5	0.	0.	0.	0.	0.	.14
N410V2.005	.5	.0	46.1	.0	.03	250.0	17.0	11.0	1.2	0.	0.	402.	0.	0.	.66
N410V2.006	.6	.0	46.1	.0	.06	250.0	.0	11.0	1.5	0.	0.	402.	0.	0.	1.49
N410V2.007	.5	.0	45.0	.0	.10	250.0	-25.0	11.0	1.5	0.	0.	392.	0.	0.	2.54
N410V2.008	.5	.0	36.0	.0	.10	250.0	-33.0	11.0	1.3	0.	0.	314.	0.	0.	2.48
N410V2.009	.6	.0	35.5	.0	.12	250.0	-50.0	11.0	1.5	0.	0.	309.	0.	0.	2.83
N410V2.010	.5	.0	34.6	.0	.10	250.0	-58.0	11.0	1.4	0.	0.	301.	0.	0.	2.33
N410V3.004	.2	.0	32.4	.0	-.01	250.0	28.0	11.0	.6	0.	0.	282.	0.	0.	.20
N410V3.005	.4	.0	33.0	.0	.02	250.0	17.0	11.0	1.0	0.	0.	287.	0.	0.	.58
N410V3.006	.5	.0	36.4	.0	.09	250.0	.0	11.0	1.4	0.	0.	317.	0.	0.	2.14
N410V3.007	.7	.0	42.5	.0	.12	250.0	-25.0	11.0	1.7	0.	0.	371.	0.	0.	2.86
N410V3.008	.6	.0	43.4	.0	.11	250.0	-33.0	11.0	1.5	0.	0.	379.	0.	0.	2.65
N410V3.009	.5	.0	43.4	.0	.11	250.0	-50.0	11.0	1.4	0.	0.	378.	0.	0.	2.56
N410V3.010	.5	.0	46.4	.0	.10	250.0	-58.0	11.0	1.4	0.	0.	405.	0.	0.	2.42
N410V4.004	.1	.0	.0	.0	-.03	250.0	28.0	11.0	.3	0.	0.	0.	0.	0.	.07
N410V4.005	.3	.0	38.6	.0	.01	250.0	17.0	11.0	.8	0.	0.	336.	0.	0.	.47
N410V4.006	.5	.0	29.8	.0	.08	250.0	.0	11.0	1.3	0.	0.	259.	0.	0.	1.91
N410V4.007	.6	.0	33.3	.0	.14	250.0	-25.0	11.0	1.7	0.	0.	290.	0.	0.	3.23
N410V4.008	.5	.0	33.4	.0	.13	250.0	-33.0	11.0	1.4	0.	0.	291.	0.	0.	3.12
N410V4.009	.5	.0	42.6	.0	.09	250.0	-50.0	11.0	1.3	0.	0.	371.	0.	0.	2.18
N410V4.010	.4	.0	28.6	.0	.07	250.0	-58.0	11.0	1.1	0.	0.	249.	0.	0.	1.64

FALCON 4: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N410V5.004	.3	.0	43.0	.0	.01	250.0	28.0	11.0	.9	0.	0.	375.	0.	0.	.43
N410V5.005	.5	.0	50.3	.0	.04	250.0	17.0	11.0	1.2	0.	0.	439.	0.	0.	1.00
N410V5.006	.5	.0	44.4	.0	.06	250.0	.0	11.0	1.4	0.	0.	387.	0.	0.	1.51
N410V5.007	.5	.0	45.5	.0	.07	250.0	-25.0	11.0	1.3	0.	0.	396.	0.	0.	1.97
N410V5.008	.6	.0	45.4	.0	.13	250.0	-33.0	11.0	1.5	0.	0.	395.	0.	0.	3.00
N410V5.009	.6	.0	38.7	.0	.09	250.0	-50.0	11.0	1.5	0.	0.	337.	0.	0.	2.24
N410V5.010	.6	.0	46.6	.0	.06	250.0	-58.0	11.0	1.5	0.	0.	406.	0.	0.	1.54
N410W1.004	.1	.0	.0	.0	.00	250.0	28.0	17.0	.4	0.	0.	0.	0.	0.	.27
N410W1.005	.2	.0	45.4	.0	.01	250.0	17.0	17.0	.7	0.	0.	396.	0.	0.	.37
N410W1.006	.4	.0	42.2	.0	.03	250.0	.0	17.0	1.0	0.	0.	368.	0.	0.	.78
N410W1.007	.5	.0	46.0	.0	.08	250.0	-25.0	17.0	1.4	0.	0.	401.	0.	0.	2.02
N410W1.008	.5	.0	41.5	.0	.06	250.0	-33.0	17.0	1.3	0.	0.	362.	0.	0.	1.44
N410W1.009	.5	.0	41.3	.0	.07	250.0	-50.0	17.0	1.3	0.	0.	360.	0.	0.	1.75
N410W1.010	.5	.0	42.9	.0	.06	250.0	-58.0	17.0	1.4	0.	0.	374.	0.	0.	1.51
N410W2.004	.1	.0	.0	.0	.03	250.0	28.0	17.0	.4	0.	0.	0.	0.	0.	.91
N410W2.005	.1	.0	.0	.0	.01	250.0	17.0	17.0	.4	0.	0.	0.	0.	0.	.28
N410W2.006	.4	.0	29.7	.0	.00	250.0	.0	17.0	1.0	0.	0.	259.	0.	0.	.42
N410W2.007	.3	.0	31.3	.0	.05	250.0	-25.0	17.0	.9	0.	0.	273.	0.	0.	1.41
N410W2.008	.4	.0	33.4	.0	.08	250.0	-33.0	17.0	1.0	0.	0.	291.	0.	0.	1.87
N410W2.009	.5	.0	39.6	.0	.07	250.0	-50.0	17.0	1.4	0.	0.	345.	0.	0.	1.76
N410W2.010	.5	.0	39.5	.0	.06	250.0	-58.0	17.0	1.3	0.	0.	344.	0.	0.	1.55
N410W3.004	.1	.0	.0	.0	-.02	250.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.10
N410W3.005	.1	.0	.0	.0	.00	250.0	17.0	17.0	.3	0.	0.	0.	0.	0.	.23
N410W3.006	.3	.0	40.7	.0	.02	250.0	.0	17.0	.9	0.	0.	355.	0.	0.	.70
N410W3.007	.4	.0	43.4	.0	.06	250.0	-25.0	17.0	1.1	0.	0.	378.	0.	0.	1.52
N410W3.008	.5	.0	38.2	.0	.07	250.0	-33.0	17.0	1.2	0.	0.	333.	0.	0.	1.70
N410W3.009	.5	.0	34.4	.0	.06	250.0	-50.0	17.0	1.4	0.	0.	300.	0.	0.	1.53
N410W3.010	.4	.0	34.2	.0	.06	250.0	-58.0	17.0	1.1	0.	0.	298.	0.	0.	1.46
N410W4.004	.3	.0	39.9	.0	.01	250.0	28.0	17.0	.7	0.	0.	348.	0.	0.	.49
N410W4.005	.4	.0	43.0	.0	.02	250.0	17.0	17.0	1.1	0.	0.	375.	0.	0.	.60
N410W4.006	.4	.0	42.8	.0	.04	250.0	.0	17.0	1.2	0.	0.	373.	0.	0.	.89
N410W4.007	.5	.0	47.1	.0	.06	250.0	-25.0	17.0	1.4	0.	0.	410.	0.	0.	1.51
N410W4.008	.5	.0	49.9	.0	.07	250.0	-33.0	17.0	1.4	0.	0.	435.	0.	0.	1.83
N410W4.009	.5	.0	43.4	.0	.07	250.0	-50.0	17.0	1.4	0.	0.	379.	0.	0.	1.71
N410W4.010	.4	.0	41.0	.0	.06	250.0	-58.0	17.0	1.2	0.	0.	357.	0.	0.	1.52
N410W5.004	.1	.0	.0	.0	.00	250.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.35
N410W5.005	.4	.0	27.3	.0	.02	250.0	17.0	17.0	1.0	0.	0.	238.	0.	0.	.61
N410W5.006	.4	.0	27.2	.0	.04	250.0	.0	17.0	1.0	0.	0.	237.	0.	0.	.90
N410W5.007	.5	.0	45.2	.0	.08	250.0	-25.0	17.0	1.3	0.	0.	394.	0.	0.	1.87
N410W5.008	.4	.0	37.2	.0	.08	250.0	-33.0	17.0	1.2	0.	0.	324.	0.	0.	1.87
N410W5.009	.6	.0	36.2	.0	.07	250.0	-50.0	17.0	1.6	0.	0.	315.	0.	0.	1.83
N410W5.010	.5	.0	37.5	.0	.06	250.0	-58.0	17.0	1.3	0.	0.	327.	0.	0.	1.57

FALCON 4: LSR = 150, GAS = ARGON

	MODEL CONDITIONS								PROTOTYPE CONDITIONS						
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N415A1.009	.2	.0	.0	.0	.02	-62.0	30.0	2.0	.5	0.	0.	0.	0.	0.	.52
N415A1.008	13.5	3.2	29.3	65.8	1.91	-62.0	20.0	2.0	29.7	35.	64.	313.	438.	651.	50.14
N415A1.007	17.1	2.0	24.8	51.4	2.94	-62.0	10.0	2.0	35.7	22.	27.	265.	404.	457.	73.82
N415A1.006	18.9	1.2	19.6	68.4	3.91	-62.0	.0	2.0	38.7	13.	22.	210.	404.	459.	95.78
N415A1.005	18.6	.6	27.5	70.4	3.29	-62.0	-10.0	2.0	38.2	19.	23.	294.	590.	749.	82.62
N415A1.004	19.1	1.0	27.0	50.8	2.02	-62.0	-20.0	2.0	38.9	16.	17.	288.	417.	529.	51.30
N415A2.009	.4	.0	30.1	.0	.03	-62.0	30.0	2.0	1.2	0.	0.	321.	0.	0.	.88
N415A2.008	16.0	.7	21.6	67.7	2.65	-62.0	20.0	2.0	34.1	33.	65.	230.	480.	484.	67.86
N415A2.007	20.3	1.6	30.5	68.7	3.46	-62.0	10.0	2.0	40.8	19.	36.	326.	420.	576.	84.95
N415A2.006	20.4	1.7	27.1	62.3	4.51	-62.0	.0	2.0	40.9	19.	23.	290.	454.	492.	108.16
N415A2.005	18.5	.8	26.6	65.9	4.09	-62.0	-10.0	2.0	38.0	10.	25.	284.	613.	704.	100.66
N415A2.004	20.6	1.7	24.0	69.9	3.19	-62.0	-20.0	2.0	41.2	51.	54.	256.	388.	747.	77.61
N415A3.009	.1	.0	.0	.0	-.04	-62.0	30.0	2.0	.2	0.	0.	0.	0.	0.	.01
N415A3.008	14.5	.5	18.8	68.1	2.38	-62.0	20.0	2.0	31.5	6.	12.	200.	498.	727.	61.40
N415A3.007	19.1	1.2	20.2	63.6	3.41	-62.0	10.0	2.0	38.9	13.	14.	215.	382.	470.	83.93
N415A3.006	19.2	1.4	10.6	62.2	4.10	-62.0	.0	2.0	39.1	16.	19.	113.	512.	535.	99.45
N415A3.005	16.7	.6	17.0	70.1	3.17	-62.0	-10.0	2.0	35.1	6.	23.	182.	493.	748.	80.43
N415A3.004	17.9	.4	27.2	69.9	2.00	-62.0	-20.0	2.0	37.1	9.	14.	290.	508.	706.	51.21
N415A4.009	.9	.0	32.5	.0	.05	-62.0	30.0	2.0	2.4	0.	0.	347.	0.	0.	1.48
N415A4.008	17.5	.4	17.1	69.4	2.94	-62.0	20.0	2.0	36.5	4.	4.	183.	661.	669.	73.75
N415A4.007	20.6	2.0	23.0	68.1	4.35	-62.0	10.0	2.0	41.2	22.	26.	245.	492.	622.	105.41
N415A4.006	23.4	1.4	29.1	65.3	5.31	-62.0	.0	2.0	45.2	17.	20.	311.	465.	693.	124.43
N415A4.005	20.3	.5	23.0	70.4	4.79	-62.0	-10.0	2.0	40.8	6.	18.	246.	644.	742.	115.52
N415A4.004	24.4	.6	29.5	66.2	3.79	-62.0	-20.0	2.0	46.5	6.	16.	315.	705.	705.	90.67
N415A5.009	.2	.0	.0	.0	-.01	-62.0	30.0	2.0	.5	0.	0.	0.	0.	0.	.07
N415A5.008	15.9	.7	21.6	70.0	2.44	-62.0	20.0	2.0	33.9	8.	37.	230.	399.	735.	63.38
N415A5.007	16.8	.5	22.3	54.7	3.42	-62.0	10.0	2.0	35.3	6.	7.	238.	446.	529.	84.82
N415A5.006	18.9	.8	21.1	68.9	4.40	-62.0	.0	2.0	38.6	14.	17.	225.	513.	591.	106.99
N415A5.005	16.3	.7	25.0	70.4	3.82	-62.0	-10.0	2.0	34.5	17.	21.	267.	729.	745.	95.07
N415A5.004	19.6	.2	29.1	66.6	1.85	-62.0	-20.0	2.0	39.8	7.	57.	310.	590.	711.	50.47
N415B1.009	.2	.0	.0	.0	.01	-32.0	30.0	1.0	.5	0.	0.	0.	0.	0.	.41
N415B1.008	15.3	.9	16.4	70.3	3.33	-32.0	20.0	1.0	32.8	11.	34.	176.	591.	593.	83.71
N415B1.007	27.4	.1	7.3	38.4	1.39	-32.0	10.0	1.0	50.6	1.	1.	77.	341.	357.	35.31
N415B1.006	21.2	.5	22.2	49.2	1.57	-32.0	.0	1.0	42.1	14.	68.	237.	325.	411.	40.13
N415B1.005	32.9	.2	21.5	57.4	6.89	-32.0	-10.0	1.0	57.0	2.	2.	230.	434.	522.	147.76
N415B1.004	17.2	.7	14.4	64.0	1.31	-32.0	-20.0	1.0	35.9	7.	23.	154.	384.	534.	34.84
N415B2.009	.1	.0	.0	.0	.02	-32.0	30.0	1.0	.3	0.	0.	0.	0.	0.	.54
N415B2.008	17.1	1.3	25.6	63.9	3.15	-32.0	20.0	1.0	35.7	15.	16.	273.	424.	680.	80.06
N415B2.007	32.3	.1	28.9	42.2	1.31	-32.0	10.0	1.0	56.3	1.	1.	309.	344.	429.	33.22
N415B2.006	23.4	.4	21.6	51.4	1.39	-32.0	.0	1.0	45.2	4.	20.	231.	360.	402.	35.72
N415B2.005	30.3	.2	23.9	68.4	6.71	-32.0	-10.0	1.0	54.0	2.	2.	255.	462.	511.	147.55
N415B2.004	14.5	.4	29.1	68.1	1.14	-32.0	-20.0	1.0	31.4	4.	4.	310.	351.	503.	30.71

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N415B3.009	.2	.0	.0	.0	.01	-32.0	30.0	1.0	.5	0.	0.	0.	0.	0.	.45
N415B3.008	14.2	.7	23.7	70.4	3.26	-32.0	20.0	1.0	30.9	11.	44.	253.	435.	750.	82.88
N415B3.007	29.1	.1	15.1	40.5	1.14	-32.0	10.0	1.0	52.5	1.	1.	161.	329.	379.	29.63
N415B3.006	23.1	.4	29.6	46.8	1.04	-32.0	.0	1.0	44.8	5.	128.	316.	319.	389.	27.26
N415B3.005	32.7	.1	21.0	60.9	5.53	-32.0	-10.0	1.0	56.7	2.	2.	224.	453.	489.	125.30
N415B3.004	13.6	.5	24.7	65.1	.99	-32.0	-20.0	1.0	29.9	6.	43.	264.	345.	426.	27.06
N415B4.009	.1	.0	.0	.0	.00	-32.0	30.0	1.0	.2	0.	0.	0.	0.	0.	.28
N415B4.008	16.0	1.2	29.1	67.6	3.13	-32.0	20.0	1.0	34.0	15.	48.	310.	605.	721.	79.52
N415B4.007	33.2	.1	24.5	43.0	1.68	-32.0	10.0	1.0	57.3	1.	1.	261.	363.	384.	41.48
N415B4.006	25.1	.5	10.3	49.3	1.92	-32.0	.0	1.0	47.5	20.	20.	109.	378.	471.	47.31
N415B4.005	30.8	.2	25.9	69.8	6.06	-32.0	-10.0	1.0	54.6	2.	2.	277.	390.	612.	132.89
N415B4.004	14.8	.5	6.4	51.3	1.34	-32.0	-20.0	1.0	31.9	6.	32.	69.	375.	412.	36.47
N415B5.009	.2	.0	19.3	.0	.04	-32.0	30.0	1.0	.6	0.	0.	206.	0.	0.	1.17
N415B5.008	17.7	1.0	26.0	67.9	3.64	-32.0	20.0	1.0	36.8	12.	46.	277.	611.	632.	90.88
N415B5.007	28.4	.1	26.3	44.8	1.74	-32.0	10.0	1.0	51.8	1.	1.	281.	371.	398.	43.90
N415B5.006	27.3	.5	27.4	66.0	2.78	-32.0	.0	1.0	50.3	6.	6.	292.	391.	514.	66.66
N415B5.005	32.6	.1	27.6	69.1	7.10	-32.0	-10.0	1.0	56.6	1.	2.	295.	389.	530.	151.34
N415B5.004	17.9	.4	18.8	64.1	1.71	-32.0	-20.0	1.0	37.0	5.	5.	200.	354.	682.	44.77
N415C1.009	.2	.0	.0	.0	-.02	-2.0	30.0	1.0	.5	0.	0.	0.	0.	0.	.10
N415C1.008	1.7	2.5	25.6	25.8	.21	-2.0	20.0	1.0	4.4	0.	0.	273.	0.	0.	6.02
N415C1.007	2.8	2.2	2.3	37.3	.33	-2.0	10.0	1.0	7.2	24.	0.	24.	0.	271.	9.40
N415C1.006	1.6	5.2	23.6	37.3	.28	-2.0	.0	1.0	4.2	0.	0.	252.	0.	0.	8.06
N415C1.005	2.2	15.2	23.7	34.4	.22	-2.0	-10.0	1.0	5.8	252.	0.	253.	0.	271.	6.42
N415C1.004	1.3	18.8	34.3	35.3	.27	-2.0	-20.0	1.0	3.3	0.	0.	366.	0.	0.	7.62
N415C2.009	.2	.0	18.2	.0	.01	-2.0	30.0	1.0	.6	0.	0.	195.	0.	0.	.43
N415C2.008	1.8	8.4	30.4	56.8	.32	-2.0	20.0	1.0	4.7	0.	0.	324.	0.	0.	9.28
N415C2.007	2.8	6.4	29.9	32.5	.33	-2.0	10.0	1.0	7.3	198.	0.	319.	0.	323.	9.29
N415C2.006	2.3	2.0	30.0	34.6	.29	-2.0	.0	1.0	5.9	320.	0.	321.	0.	322.	8.19
N415C2.005	2.4	16.1	29.9	34.7	.25	-2.0	-10.0	1.0	6.1	305.	0.	319.	0.	320.	7.21
N415C2.004	1.5	25.6	30.3	31.8	.26	-2.0	-20.0	1.0	4.0	0.	0.	324.	0.	0.	7.51
N415C3.009	.1	.0	.0	.0	-.03	-2.0	30.0	1.0	.2	0.	0.	0.	0.	0.	.05
N415C3.008	1.7	6.1	23.0	28.7	.25	-2.0	20.0	1.0	4.5	0.	0.	246.	0.	0.	7.18
N415C3.007	2.2	6.0	22.5	32.1	.24	-2.0	10.0	1.0	5.8	238.	0.	240.	0.	241.	7.04
N415C3.006	1.9	11.2	27.0	33.6	.29	-2.0	.0	1.0	4.8	0.	0.	288.	0.	0.	8.17
N415C3.005	1.5	16.8	23.7	32.2	.19	-2.0	-10.0	1.0	3.9	0.	0.	253.	0.	0.	5.55
N415C3.004	1.1	20.1	20.1	32.7	.23	-2.0	-20.0	1.0	2.9	0.	0.	215.	0.	0.	6.52
N415C4.009	.3	.0	30.7	.0	.02	-2.0	30.0	1.0	.8	0.	0.	328.	0.	0.	.57
N415C4.008	2.2	15.0	29.1	61.9	.30	-2.0	20.0	1.0	5.8	310.	0.	310.	0.	311.	8.56
N415C4.007	2.0	7.6	31.4	35.9	.31	-2.0	10.0	1.0	5.2	255.	0.	335.	0.	335.	8.95
N415C4.006	2.5	9.0	30.5	35.9	.32	-2.0	.0	1.0	6.4	324.	0.	326.	0.	327.	9.14
N415C4.005	2.3	9.1	28.8	39.5	.25	-2.0	-10.0	1.0	5.9	307.	0.	308.	0.	308.	7.19
N415C4.004	1.4	25.1	29.3	31.4	.28	-2.0	-20.0	1.0	3.7	0.	0.	313.	0.	0.	8.05

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N415C5.009	.2	.0	.0	.0	-.01	-2.0	30.0	1.0	.5	0.	0.	0.	0.	0.	.21
N415C5.008	2.2	6.0	29.4	50.8	.33	-2.0	20.0	1.0	5.6	189.	0.	314.	0.	365.	9.65
N415C5.007	2.0	8.6	18.2	35.4	.30	-2.0	10.0	1.0	5.2	194.	0.	194.	0.	312.	8.64
N415C5.006	2.5	12.9	26.2	35.2	.31	-2.0	.0	1.0	6.4	279.	0.	280.	0.	281.	8.80
N415C5.005	1.9	10.6	20.3	35.3	.27	-2.0	-10.0	1.0	4.9	0.	0.	217.	0.	0.	7.68
N415C5.004	1.3	18.0	27.0	35.0	.31	-2.0	-20.0	1.0	3.4	0.	0.	288.	0.	0.	8.84
F415D1.005	.1	.0	.0	.0	-.01	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.13
F415D1.006	.1	.0	.0	.0	.01	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.51
F415D1.007	.1	.0	.0	.0	.00	50.0	33.0	1.0	.3	0.	0.	0.	0.	0.	.42
F415D1.008	.8	.0	30.5	.0	.07	50.0	16.5	1.0	2.2	0.	0.	326.	0.	0.	2.18
F415D1.009	.7	.0	30.3	.0	.13	50.0	.0	1.0	1.9	0.	0.	324.	0.	0.	3.77
F415D1.010	.6	.0	29.2	.0	.12	50.0	-33.0	1.0	1.5	0.	0.	312.	0.	0.	3.63
F415D1.011	.6	.0	27.1	.0	.13	50.0	-50.0	1.0	1.7	0.	0.	290.	0.	0.	3.88
F415D1.012	.6	.0	28.1	.0	.12	50.0	-66.0	1.0	1.7	0.	0.	300.	0.	0.	3.50
F415D2.005	.1	.0	.0	.0	-.03	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.03
F415D2.006	.1	.0	.0	.0	-.04	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.13
F415D2.007	.1	.0	.0	.0	-.03	50.0	33.0	1.0	.2	0.	0.	0.	0.	0.	.10
F415D2.008	.7	.0	31.5	.0	-.05	50.0	16.5	1.0	1.8	0.	0.	336.	0.	0.	.41
F415D2.009	.7	.0	30.3	.0	.10	50.0	.0	1.0	1.8	0.	0.	324.	0.	0.	2.97
F415D2.010	.7	.0	32.3	.0	.13	50.0	-33.0	1.0	1.7	0.	0.	345.	0.	0.	3.79
F415D2.011	.8	.0	24.6	.0	.12	50.0	-50.0	1.0	2.0	0.	0.	263.	0.	0.	3.84
F415D2.012	.7	.0	31.3	.0	.10	50.0	-66.0	1.0	1.8	0.	0.	334.	0.	0.	3.01
F415D3.005	.1	.0	.0	.0	-.03	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.07
F415D3.006	.1	.0	.0	.0	-.04	50.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.07
F415D3.007	.1	.0	.0	.0	-.03	50.0	33.0	1.0	.2	0.	0.	0.	0.	0.	.14
F415D3.008	.6	.0	26.9	.0	.03	50.0	16.5	1.0	1.6	0.	0.	287.	0.	0.	1.12
F415D3.009	.9	.0	17.4	.0	.12	50.0	.0	1.0	2.3	0.	0.	186.	0.	0.	3.63
F415D3.010	.7	.0	25.7	.0	.13	50.0	-33.0	1.0	1.8	0.	0.	274.	0.	0.	3.89
F415D3.011	.7	.0	31.8	.0	.11	50.0	-50.0	1.0	1.8	0.	0.	340.	0.	0.	3.36
F415D3.012	.6	.0	15.7	.0	.12	50.0	-66.0	1.0	1.5	0.	0.	167.	0.	0.	3.41
F415D4.005	.1	.0	.0	.0	-.03	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.09
F415D4.006	.1	.0	.0	.0	-.01	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.25
F415D4.007	.1	.0	.0	.0	-.03	50.0	33.0	1.0	.2	0.	0.	0.	0.	0.	.16
F415D4.008	.5	.0	16.8	.0	-.01	50.0	16.5	1.0	1.2	0.	0.	179.	0.	0.	.61
F415D4.009	.9	.0	12.6	.0	.10	50.0	.0	1.0	2.5	0.	0.	134.	0.	0.	3.02
F415D4.010	.7	.0	33.5	.0	.15	50.0	-33.0	1.0	1.9	0.	0.	358.	0.	0.	4.31
F415D4.011	.6	.0	22.0	.0	.12	50.0	-50.0	1.0	1.7	0.	0.	235.	0.	0.	3.55
F415D4.012	.8	.0	33.3	.0	.10	50.0	-66.0	1.0	2.1	0.	0.	356.	0.	0.	2.89
F415D5.005	.2	.0	.0	.0	.03	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.99
F415D5.006	.1	.0	.0	.0	-.01	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.36
F415D5.007	.2	.0	.0	.0	.02	50.0	33.0	1.0	.4	0.	0.	0.	0.	0.	.84
F415D5.008	.6	.0	28.9	.0	.05	50.0	16.5	1.0	1.7	0.	0.	308.	0.	0.	1.61

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F415D5.009	.7	.0	31.7	.0	.11	50.0	.0	1.0	1.9	0.	0.	338.	0.	0.	3.60
F415D5.010	.7	.0	33.6	.0	.11	50.0	-33.0	1.0	1.9	0.	0.	358.	0.	0.	3.54
F415D5.011	.6	.0	27.9	.0	.05	50.0	-50.0	1.0	1.7	0.	0.	298.	0.	0.	2.46
F415D5.012	.6	.0	20.3	.0	.08	50.0	-66.0	1.0	1.5	0.	0.	217.	0.	0.	2.32
F415E1.005	.1	.0	.0	.0	-.02	50.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.14
F415E1.006	.1	.0	.0	.0	.00	50.0	50.0	5.0	.3	0.	0.	0.	0.	0.	.33
F415E1.007	.4	.0	23.2	.0	.00	50.0	33.0	5.0	1.2	0.	0.	248.	0.	0.	.42
F415E1.008	1.0	17.8	17.8	17.8	.07	50.0	16.5	5.0	2.7	0.	0.	190.	0.	0.	2.30
F415E1.009	1.0	22.5	22.5	22.5	.13	50.0	.0	5.0	2.8	0.	0.	240.	0.	0.	3.67
F415E1.010	.8	.0	23.1	.0	.14	50.0	-33.0	5.0	2.3	0.	0.	247.	0.	0.	4.11
F415E1.011	.9	.0	32.8	.0	.08	50.0	-50.0	5.0	2.3	0.	0.	350.	0.	0.	2.35
F415E1.012	.6	.0	33.1	.0	.04	50.0	-66.0	5.0	1.7	0.	0.	353.	0.	0.	1.23
F415E2.005	.1	.0	.0	.0	-.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.42
F415E2.006	.1	.0	.0	.0	.01	50.0	50.0	5.0	.4	0.	0.	0.	0.	0.	.65
F415E2.007	.3	.0	12.6	.0	.02	50.0	33.0	5.0	.8	0.	0.	134.	0.	0.	.82
F415E2.008	1.1	17.9	17.9	30.3	.06	50.0	16.5	5.0	3.0	0.	0.	191.	0.	0.	1.98
F415E2.009	1.0	17.0	17.0	17.0	.16	50.0	.0	5.0	2.7	0.	0.	181.	0.	0.	4.57
F415E2.010	.8	.0	23.2	.0	.12	50.0	-33.0	5.0	2.1	0.	0.	247.	0.	0.	3.44
F415E2.011	.7	.0	23.1	.0	.07	50.0	-50.0	5.0	1.9	0.	0.	247.	0.	0.	2.09
F415E2.012	.4	.0	36.6	.0	.02	50.0	-66.0	5.0	1.1	0.	0.	391.	0.	0.	.78
F415E3.005	.1	.0	.0	.0	.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.76
F415E3.006	.1	.0	.0	.0	.00	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.28
F415E3.007	.8	.0	18.6	.0	.00	50.0	33.0	5.0	2.0	0.	0.	199.	0.	0.	.34
F415E3.008	1.1	30.7	30.7	30.8	.06	50.0	16.5	5.0	2.8	0.	0.	328.	0.	0.	2.05
F415E3.009	1.1	31.2	31.2	31.2	.13	50.0	.0	5.0	2.9	0.	0.	333.	0.	0.	3.67
F415E3.010	.7	.0	21.5	.0	.10	50.0	-33.0	5.0	2.0	0.	0.	229.	0.	0.	3.04
F415E3.011	1.0	.0	26.3	.0	.03	50.0	-50.0	5.0	2.5	0.	0.	281.	0.	0.	1.16
F415E3.012	.8	.0	31.2	.0	.01	50.0	-66.0	5.0	2.1	0.	0.	333.	0.	0.	.56
F415E4.005	.0	.0	.0	.0	.00	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.23
F415E4.006	.2	.0	.0	.0	.04	50.0	50.0	5.0	.5	0.	0.	0.	0.	0.	1.33
F415E4.007	.7	.0	22.6	.0	.05	50.0	33.0	5.0	1.8	0.	0.	242.	0.	0.	1.62
F415E4.008	.8	.0	6.8	.0	.10	50.0	16.5	5.0	2.2	0.	0.	73.	0.	0.	2.84
F415E4.009	.8	.0	18.5	.0	.16	50.0	.0	5.0	2.2	0.	0.	198.	0.	0.	4.67
F415E4.010	.9	.0	25.6	.0	.11	50.0	-33.0	5.0	2.5	0.	0.	273.	0.	0.	3.36
F415E4.011	.8	.0	29.1	.0	.05	50.0	-50.0	5.0	2.1	0.	0.	310.	0.	0.	1.41
F415E4.012	.4	.0	35.9	.0	.02	50.0	-66.0	5.0	1.1	0.	0.	383.	0.	0.	.68
F415E5.005	.1	.0	.0	.0	.01	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.45
F415E5.006	.1	.0	.0	.0	.01	50.0	50.0	5.0	.3	0.	0.	0.	0.	0.	.56
F415E5.007	.5	.0	21.2	.0	.02	50.0	33.0	5.0	1.4	0.	0.	227.	0.	0.	.74
F415E5.008	.9	.0	23.5	.0	.05	50.0	16.5	5.0	2.4	0.	0.	250.	0.	0.	1.63
F415E5.009	.8	.0	18.7	.0	.13	50.0	.0	5.0	2.2	0.	0.	200.	0.	0.	3.92
F415E5.010	.8	.0	25.7	.0	.11	50.0	-33.0	5.0	2.1	0.	0.	275.	0.	0.	3.31

FALCON 4: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F415E5.011	.8	.0	30.9	.0	.03	50.0	-50.0	5.0	2.2	0.	0.	329.	0.	0.	1.11
F415E5.012	.5	.0	37.9	.0	.02	50.0	-66.0	5.0	1.4	0.	0.	405.	0.	0.	.73
F415F1.005	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.26
F415F1.006	.1	.0	.0	.0	.00	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.43
F415F1.007	.6	.0	13.8	.0	-.02	50.0	33.0	11.0	1.6	0.	0.	148.	0.	0.	.12
F415F1.008	1.1	21.5	21.5	21.5	.05	50.0	16.5	11.0	3.0	0.	0.	230.	0.	0.	1.68
F415F1.009	.9	.0	19.5	.0	.12	50.0	.0	11.0	2.3	0.	0.	209.	0.	0.	3.42
F415F1.010	.7	.0	15.9	.0	.09	50.0	-33.0	11.0	1.9	0.	0.	170.	0.	0.	2.86
F415F1.011	.6	.0	23.7	.0	.02	50.0	-50.0	11.0	1.7	0.	0.	253.	0.	0.	.99
F415F1.012	.5	.0	38.5	.0	.00	50.0	-66.0	11.0	1.4	0.	0.	411.	0.	0.	.17
F415F2.005	.1	.0	.0	.0	-.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.08
F415F2.006	.1	.0	.0	.0	-.01	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.09
F415F2.007	.3	.0	5.4	.0	-.01	50.0	33.0	11.0	.8	0.	0.	57.	0.	0.	.18
F415F2.008	1.0	.0	24.6	.0	.03	50.0	16.5	11.0	2.6	0.	0.	262.	0.	0.	1.60
F415F2.009	1.0	.0	16.7	.0	.11	50.0	.0	11.0	2.6	0.	0.	178.	0.	0.	3.29
F415F2.010	.7	.0	25.7	.0	.10	50.0	-33.0	11.0	1.9	0.	0.	275.	0.	0.	3.06
F415F2.011	.7	.0	28.7	.0	.05	50.0	-50.0	11.0	2.0	0.	0.	307.	0.	0.	1.53
F415F2.012	.5	.0	21.9	.0	.00	50.0	-66.0	11.0	1.5	0.	0.	234.	0.	0.	.39
F415F3.005	.1	.0	.0	.0	-.02	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.08
F415F3.006	.1	.0	.0	.0	-.02	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.09
F415F3.007	.7	.0	29.7	.0	-.02	50.0	33.0	11.0	2.0	0.	0.	317.	0.	0.	.11
F415F3.008	1.6	20.4	23.8	24.0	.05	50.0	16.5	11.0	4.2	0.	0.	254.	0.	0.	1.68
F415F3.009	1.0	26.2	26.2	26.2	.17	50.0	.0	11.0	2.8	0.	0.	280.	0.	0.	5.01
F415F3.010	.8	.0	34.1	.0	.11	50.0	-33.0	11.0	2.2	0.	0.	364.	0.	0.	3.38
F415F3.011	.8	.0	36.5	.0	.03	50.0	-50.0	11.0	2.1	0.	0.	389.	0.	0.	.99
F415F3.012	.2	.0	41.9	.0	.00	50.0	-66.0	11.0	.6	0.	0.	447.	0.	0.	.24
F415F4.005	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.38
F415F4.006	.1	.0	.0	.0	.02	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.64
F415F4.007	.5	.0	34.3	.0	.01	50.0	33.0	11.0	1.2	0.	0.	366.	0.	0.	.40
F415F4.008	1.2	14.1	24.7	24.8	.08	50.0	16.5	11.0	3.2	0.	0.	264.	0.	0.	2.40
F415F4.009	1.3	24.8	24.9	24.9	.13	50.0	.0	11.0	3.4	0.	0.	265.	0.	0.	3.90
F415F4.010	.9	.0	27.8	.0	.10	50.0	-33.0	11.0	2.3	0.	0.	297.	0.	0.	3.01
F415F4.011	.8	.0	33.3	.0	.02	50.0	-50.0	11.0	2.2	0.	0.	356.	0.	0.	.99
F415F4.012	.6	.0	34.2	.0	.01	50.0	-66.0	11.0	1.7	0.	0.	365.	0.	0.	.65
F415F5.005	.1	.0	.0	.0	.00	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.36
F415F5.006	.2	.0	.0	.0	.01	50.0	50.0	11.0	.4	0.	0.	0.	0.	0.	.58
F415F5.007	1.0	29.2	29.2	29.2	.01	50.0	33.0	11.0	2.8	0.	0.	312.	0.	0.	.42
F415F5.008	1.9	22.7	22.7	23.1	.06	50.0	16.5	11.0	5.0	0.	0.	242.	0.	0.	2.15
F415F5.009	.9	.0	31.7	.0	.13	50.0	.0	11.0	2.5	0.	0.	338.	0.	0.	3.76
F415F5.010	.8	.0	21.1	.0	.12	50.0	-33.0	11.0	2.1	0.	0.	225.	0.	0.	3.52
F415F5.011	.8	.0	29.1	.0	.06	50.0	-50.0	11.0	2.2	0.	0.	310.	0.	0.	1.74
F415F5.012	.8	.0	18.4	.0	.03	50.0	-66.0	11.0	2.0	0.	0.	197.	0.	0.	.98

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F415G1.005	.1	.0	.0	.0	.03	50.0	66.0	17.0	.4	0.	0.	0.	0.	0.	.88
F415G1.006	.1	.0	.0	.0	.04	50.0	50.0	17.0	.4	0.	0.	0.	0.	0.	1.06
F415G1.007	.7	.0	17.8	.0	.02	50.0	33.0	17.0	1.9	0.	0.	190.	0.	0.	.58
F415G1.008	1.3	15.3	15.3	15.3	.07	50.0	16.5	17.0	3.4	0.	0.	163.	0.	0.	2.22
F415G1.009	1.1	30.2	30.2	30.2	.07	50.0	.0	17.0	2.8	0.	0.	322.	0.	0.	2.31
F415G1.010	.9	.0	32.6	.0	.08	50.0	-33.0	17.0	2.5	0.	0.	348.	0.	0.	2.41
F415G1.011	.6	.0	35.6	.0	.02	50.0	-50.0	17.0	1.6	0.	0.	380.	0.	0.	.79
F415G1.012	.3	.0	35.9	.0	.00	50.0	-66.0	17.0	.7	0.	0.	384.	0.	0.	.20
F415G2.005	.1	.0	.0	.0	.03	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.81
F415G2.006	.1	.0	.0	.0	.03	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.85
F415G2.007	.8	.0	36.6	.0	.02	50.0	33.0	17.0	2.0	0.	0.	391.	0.	0.	.74
F415G2.008	1.2	26.9	30.6	30.7	.10	50.0	16.5	17.0	3.2	0.	0.	327.	0.	0.	2.90
F415G2.009	.9	.0	30.6	.0	.08	50.0	.0	17.0	2.4	0.	0.	327.	0.	0.	2.55
F415G2.010	.8	.0	22.5	.0	.10	50.0	-33.0	17.0	2.2	0.	0.	241.	0.	0.	2.93
F415G2.011	.8	.0	35.5	.0	.04	50.0	-50.0	17.0	2.1	0.	0.	379.	0.	0.	1.08
F415G2.012	.3	.0	34.8	.0	.02	50.0	-66.0	17.0	.9	0.	0.	372.	0.	0.	.50
F415G3.005	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.15
F415G3.006	.1	.0	.0	.0	.00	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.31
F415G3.007	.6	.0	16.6	.0	.00	50.0	33.0	17.0	1.5	0.	0.	178.	0.	0.	.25
F415G3.008	1.1	9.5	9.5	23.3	.05	50.0	16.5	17.0	3.0	0.	0.	101.	0.	0.	1.84
F415G3.009	1.1	25.8	25.8	25.8	.05	50.0	.0	17.0	2.9	0.	0.	275.	0.	0.	1.88
F415G3.010	1.0	12.0	12.0	12.0	.08	50.0	-33.0	17.0	2.8	0.	0.	128.	0.	0.	2.53
F415G3.011	.8	.0	34.0	.0	.02	50.0	-50.0	17.0	2.1	0.	0.	363.	0.	0.	.82
F415G3.012	.6	.0	33.8	.0	.02	50.0	-66.0	17.0	1.5	0.	0.	361.	0.	0.	.46
F415G4.005	.1	.0	.0	.0	.02	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.48
F415G4.006	.2	.0	.0	.0	.03	50.0	50.0	17.0	.4	0.	0.	0.	0.	0.	.95
F415G4.007	1.1	16.3	16.3	16.3	.02	50.0	33.0	17.0	3.0	0.	0.	174.	0.	0.	.68
F415G4.008	1.2	26.8	26.8	26.8	.06	50.0	16.5	17.0	3.3	0.	0.	286.	0.	0.	2.08
F415G4.009	1.3	14.9	28.7	28.7	.09	50.0	.0	17.0	3.4	0.	0.	306.	0.	0.	2.82
F415G4.010	.9	.0	14.9	.0	.07	50.0	-33.0	17.0	2.5	0.	0.	159.	0.	0.	2.18
F415G4.011	.8	.0	23.4	.0	-.03	50.0	-50.0	17.0	2.2	0.	0.	249.	0.	0.	.25
F415G4.012	.2	.0	42.3	.0	-.03	50.0	-66.0	17.0	.6	0.	0.	452.	0.	0.	.02
F415G5.005	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.04
F415G5.006	.1	.0	.0	.0	-.01	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.08
F415G5.007	.9	.0	23.1	.0	.00	50.0	33.0	17.0	2.3	0.	0.	247.	0.	0.	.24
F415G5.008	.9	.0	20.0	.0	.08	50.0	16.6	17.0	2.4	0.	0.	214.	0.	0.	2.56
F415G5.009	.9	.0	22.1	.0	.08	50.0	.0	17.0	2.4	0.	0.	236.	0.	0.	2.58
F415G5.010	.9	.0	17.1	.0	.08	50.0	-33.0	17.0	2.3	0.	0.	183.	0.	0.	2.65

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F415J1.005	.1	.0	.0	.0	-.01	150.0	100.0	11.0	.1	0.	0.	0.	0.	0.	.11
F415J1.006	.1	.0	.0	.0	.00	150.0	84.0	11.0	.2	0.	0.	0.	0.	0.	.25
F415J1.007	.1	.0	.0	.0	.00	150.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.27
F415K1.005	.1	.0	.0	.0	-.01	150.0	100.0	17.0	.2	0.	0.	0.	0.	0.	.07
F415K1.006	.1	.0	.0	.0	-.01	150.0	84.0	17.0	.1	0.	0.	0.	0.	0.	.05
F415K1.007	.1	.0	.0	.0	.00	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.19
F415K1.008	.1	.0	.0	.0	-.01	150.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.17
F415K1.009	.1	.0	.0	.0	-.01	150.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.07
F415K1.010	.1	.0	.0	.0	-.01	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.05
F415K1.011	.1	.0	.0	.0	-.06	150.0	.0	17.0	.3	0.	0.	0.	0.	0.	.01
F415K1.012	.5	.0	16.2	.0	.03	150.0	-25.0	17.0	1.3	0.	0.	173.	0.	0.	1.21
F415K2.005	.1	.0	.0	.0	-.01	150.0	100.0	17.0	.1	0.	0.	0.	0.	0.	.04
F415K2.006	.1	.0	.0	.0	-.01	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.08
F415K2.007	.1	.0	.0	.0	.00	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.26
F415K2.008	.1	.0	.0	.0	.00	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.32
F415K2.009	.1	.0	.0	.0	.00	150.0	28.0	17.0	.3	0.	0.	0.	0.	0.	.19
F415K2.010	.1	.0	.0	.0	.00	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.20
F415K2.011	.6	.0	30.0	.0	-.01	150.0	.0	17.0	1.5	0.	0.	320.	0.	0.	.37
F415K2.012	.4	.0	34.9	.0	.05	150.0	-25.0	17.0	1.2	0.	0.	373.	0.	0.	1.55
F415K3.005	.0	.0	.0	.0	-.01	150.0	100.0	17.0	.1	0.	0.	0.	0.	0.	.02
F415K3.006	.1	.0	.0	.0	.02	150.0	84.0	17.0	.3	0.	0.	0.	0.	0.	.48
F415K3.007	.1	.0	.0	.0	.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.34
F415K3.008	.1	.0	.0	.0	-.02	150.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.14
F415K3.009	.1	.0	.0	.0	-.02	150.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.08
F415K3.010	.1	.0	.0	.0	-.02	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.06
F415K3.011	.3	.0	35.0	.0	.03	150.0	.0	17.0	.9	0.	0.	374.	0.	0.	.78
F415K3.012	.6	.0	20.2	.0	.06	150.0	-25.0	17.0	1.6	0.	0.	216.	0.	0.	1.88
F415K4.005	.1	.0	.0	.0	.01	150.0	100.0	17.0	.2	0.	0.	0.	0.	0.	.32
F415K4.006	.1	.0	.0	.0	.00	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.25
F415K4.007	.1	.0	.0	.0	.00	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.20
F415K4.008	.1	.0	.0	.0	.00	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.35
F415K4.009	.1	.0	.0	.0	.00	150.0	28.0	17.0	.3	0.	0.	0.	0.	0.	.46
F415K4.010	.1	.0	.0	.0	.00	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.29
F415K4.011	.4	.0	28.5	.0	.01	150.0	.0	17.0	1.1	0.	0.	304.	0.	0.	.40
F415K4.012	.4	.0	19.1	.0	.03	150.0	-25.0	17.0	1.1	0.	0.	204.	0.	0.	1.21
F415K5.005	.1	.0	.0	.0	-.02	150.0	100.0	17.0	.1	0.	0.	0.	0.	0.	.01
F415K5.006	.1	.0	.0	.0	.00	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.19
F415K5.007	.1	.0	.0	.0	-.03	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.00
F415K5.008	.1	.0	.0	.0	-.02	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.15
F415K5.009	.1	.0	.0	.0	.00	150.0	28.0	17.0	.3	0.	0.	0.	0.	0.	.20
F415K5.010	.1	.0	.0	.0	-.01	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.10
F415K5.011	.3	.0	28.4	.0	-.01	150.0	.0	17.0	.8	0.	0.	303.	0.	0.	.08

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F415K5.012	.6	.0	23.7	.0	.04	150.0	-25.0	17.0	1.5	0.	0.	253.	0.	0.	1.33
F415L1.005	.1	.0	.0	.0	-.01	150.0	25.0	1.0	.2	0.	0.	0.	0.	0.	.29
F415L1.006	.3	.0	36.7	.0	.02	150.0	.0	1.0	.7	0.	0.	392.	0.	0.	.80
F415L1.007	.4	.0	35.2	.0	.08	150.0	-25.0	1.0	1.1	0.	0.	376.	0.	0.	2.39
F415L1.008	.5	.0	19.8	.0	.08	150.0	-28.0	1.0	1.3	0.	0.	212.	0.	0.	2.36
F415L1.009	.4	.0	35.6	.0	.08	150.0	-56.0	1.0	1.0	0.	0.	380.	0.	0.	2.43
F415L1.010	.4	.0	35.4	.0	.07	150.0	-75.0	1.0	1.0	0.	0.	378.	0.	0.	2.14
F415L1.011	.5	.0	31.5	.0	.08	150.0	-84.0	1.0	1.2	0.	0.	336.	0.	0.	2.43
F415L1.012	.4	.0	34.4	.0	.03	150.0	-100.0	1.0	1.0	0.	0.	368.	0.	0.	1.19
F415L2.005	.0	.0	.0	.0	-.01	150.0	25.0	1.0	.1	0.	0.	0.	0.	0.	.15
F415L2.006	.3	.0	27.3	.0	.05	150.0	.0	1.0	.9	0.	0.	292.	0.	0.	1.35
F415L2.007	.4	.0	27.4	.0	.06	150.0	-25.0	1.0	1.0	0.	0.	293.	0.	0.	1.99
F415L2.008	.4	.0	22.6	.0	.04	150.0	-28.0	1.0	1.1	0.	0.	241.	0.	0.	1.76
F415L2.009	.4	.0	23.9	.0	.06	150.0	-56.0	1.0	1.0	0.	0.	256.	0.	0.	1.82
F415L2.010	.4	.0	22.6	.0	.06	150.0	-75.0	1.0	1.2	0.	0.	242.	0.	0.	1.79
F415L2.011	.4	.0	31.4	.0	.06	150.0	-84.0	1.0	1.2	0.	0.	336.	0.	0.	2.06
F415L2.012	.3	.0	31.7	.0	.03	150.0	-100.0	1.0	.9	0.	0.	339.	0.	0.	1.25
F415L3.005	.2	.0	11.6	.0	.03	150.0	25.0	1.0	.6	0.	0.	123.	0.	0.	.83
F415L3.006	.4	.0	21.4	.0	.05	150.0	.0	1.0	1.0	0.	0.	228.	0.	0.	1.54
F415L3.007	.3	.0	26.0	.0	.05	150.0	-25.0	1.0	.9	0.	0.	278.	0.	0.	1.69
F415L3.008	.4	.0	21.5	.0	.05	150.0	-28.0	1.0	1.1	0.	0.	230.	0.	0.	1.89
F415L3.009	.4	.0	24.7	.0	.08	150.0	-56.0	1.0	1.0	0.	0.	264.	0.	0.	2.30
F415L3.010	.3	.0	32.1	.0	.05	150.0	-75.0	1.0	.9	0.	0.	343.	0.	0.	1.55
F415L3.011	.3	.0	26.0	.0	.07	150.0	-84.0	1.0	.9	0.	0.	278.	0.	0.	2.13
F415L3.012	.3	.0	17.7	.0	.05	150.0	-100.0	1.0	.7	0.	0.	189.	0.	0.	1.69
F415L4.005	.1	.0	.0	.0	.02	150.0	25.0	1.0	.3	0.	0.	0.	0.	0.	.69
F415L4.006	.3	.0	13.8	.0	.05	150.0	.0	1.0	.7	0.	0.	147.	0.	0.	1.39
F415L4.007	.3	.0	16.1	.0	.06	150.0	-25.0	1.0	.9	0.	0.	172.	0.	0.	1.88
F415L4.008	.5	.0	28.7	.0	.07	150.0	-28.0	1.0	1.3	0.	0.	306.	0.	0.	2.24
F415L4.009	.4	.0	28.7	.0	.07	150.0	-56.0	1.0	1.1	0.	0.	306.	0.	0.	1.96
F415L4.010	.4	.0	30.7	.0	.08	150.0	-75.0	1.0	1.1	0.	0.	328.	0.	0.	2.24
F415L4.011	.4	.0	28.6	.0	.06	150.0	-84.0	1.0	1.1	0.	0.	306.	0.	0.	1.92
F415L4.012	.4	.0	30.7	.0	.08	150.0	-100.0	1.0	1.0	0.	0.	328.	0.	0.	2.36
F415L5.005	.1	.0	.0	.0	-.01	150.0	25.0	1.0	.3	0.	0.	0.	0.	0.	.23
F415L5.006	.3	.0	23.1	.0	.03	150.0	.0	1.0	.7	0.	0.	246.	0.	0.	1.01
F415L5.007	.3	.0	26.4	.0	.06	150.0	-25.0	1.0	.9	0.	0.	282.	0.	0.	1.82
F415L5.008	.5	.0	28.4	.0	.09	150.0	-28.0	1.0	1.3	0.	0.	303.	0.	0.	2.84
F415L5.009	.4	.0	33.1	.0	.09	150.0	-56.0	1.0	1.1	0.	0.	353.	0.	0.	2.51
F415L5.010	.3	.0	27.2	.0	.07	150.0	-75.0	1.0	.9	0.	0.	290.	0.	0.	2.04
F415L5.011	.4	.0	35.9	.0	.11	150.0	-84.0	1.0	1.2	0.	0.	383.	0.	0.	3.03
F415L5.012	.4	.0	25.6	.0	.10	150.0	-100.0	1.0	1.0	0.	0.	274.	0.	0.	2.91
F415M1.005	.1	.0	.0	.0	.02	150.0	25.0	5.0	.3	0.	0.	0.	0.	0.	.60

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F415M1.006	.4	.0	17.8	.0	.01	150.0	.0	5.0	1.1	0.	0.	190.	0.	0.	.55
F415M1.007	.5	.0	18.9	.0	.06	150.0	-25.0	5.0	1.3	0.	0.	202.	0.	0.	1.77
F415M1.008	.5	.0	19.0	.0	.06	150.0	-28.0	5.0	1.3	0.	0.	203.	0.	0.	1.81
F415M1.009	.4	.0	31.6	.0	.06	150.0	-56.0	5.0	1.1	0.	0.	337.	0.	0.	1.75
F415M1.010	.4	.0	33.9	.0	.05	150.0	-75.0	5.0	1.2	0.	0.	362.	0.	0.	1.41
F415M1.011	.4	.0	33.8	.0	.03	150.0	-84.0	5.0	1.0	0.	0.	361.	0.	0.	1.10
F415M1.012	.4	.0	27.2	.0	.05	150.0	-100.0	5.0	1.0	0.	0.	291.	0.	0.	1.43
F415M2.005	.1	.0	.0	.0	-.01	150.0	25.0	5.0	.2	0.	0.	0.	0.	0.	.07
F415M2.006	.4	.0	22.1	.0	.04	150.0	.0	5.0	1.0	0.	0.	236.	0.	0.	1.07
F415M2.007	.4	.0	16.2	.0	.07	150.0	-25.0	5.0	1.1	0.	0.	172.	0.	0.	2.19
F415M2.008	.5	.0	28.7	.0	.08	150.0	-28.0	5.0	1.4	0.	0.	306.	0.	0.	2.47
F415M2.009	.4	.0	29.0	.0	.07	150.0	-56.0	5.0	1.2	0.	0.	310.	0.	0.	2.04
F415M2.010	.4	.0	23.8	.0	.06	150.0	-75.0	5.0	1.1	0.	0.	254.	0.	0.	1.86
F415M2.011	.4	.0	28.5	.0	.07	150.0	-84.0	5.0	1.1	0.	0.	304.	0.	0.	2.12
F415M2.012	.4	.0	28.8	.0	.07	150.0	-100.0	5.0	1.2	0.	0.	307.	0.	0.	2.01
F415M3.005	.2	.0	35.1	.0	.04	150.0	25.0	5.0	.6	0.	0.	375.	0.	0.	1.14
F415M3.006	.3	.0	19.3	.0	.02	150.0	.0	5.0	.8	0.	0.	206.	0.	0.	.73
F415M3.007	.4	.0	34.2	.0	.07	150.0	-25.0	5.0	1.2	0.	0.	365.	0.	0.	2.09
F415M3.008	.5	.0	28.7	.0	.08	150.0	-28.0	5.0	1.4	0.	0.	306.	0.	0.	2.38
F415M3.009	.5	.0	27.3	.0	.04	150.0	-56.0	5.0	1.3	0.	0.	291.	0.	0.	1.35
F415M3.010	.4	.0	28.6	.0	.04	150.0	-75.0	5.0	1.1	0.	0.	305.	0.	0.	1.23
F415M3.011	.3	.0	28.7	.0	.01	150.0	-84.0	5.0	.9	0.	0.	306.	0.	0.	.78
F415M3.012	.5	.0	29.0	.0	.08	150.0	-100.0	5.0	1.2	0.	0.	310.	0.	0.	2.23
F415M4.005	.1	.0	.0	.0	.00	150.0	25.0	5.0	.2	0.	0.	0.	0.	0.	.14
F415M4.006	.4	.0	28.0	.0	.03	150.0	.0	5.0	1.1	0.	0.	299.	0.	0.	.88
F415M4.007	.4	.0	27.3	.0	.08	150.0	-25.0	5.0	1.2	0.	0.	291.	0.	0.	2.35
F415M4.008	.5	.0	29.7	.0	.08	150.0	-28.0	5.0	1.3	0.	0.	318.	0.	0.	2.41
F415M4.009	.4	.0	28.2	.0	.09	150.0	-56.0	5.0	1.2	0.	0.	301.	0.	0.	2.75
F415M4.010	.4	.0	30.4	.0	.08	150.0	-75.0	5.0	1.1	0.	0.	324.	0.	0.	2.43
F415M4.011	.5	.0	18.4	.0	.11	150.0	-84.0	5.0	1.3	0.	0.	197.	0.	0.	3.07
F415M4.012	.5	.0	37.3	.0	.10	150.0	-100.0	5.0	1.2	0.	0.	398.	0.	0.	2.84
F415M5.005	.1	.0	.0	.0	.00	150.0	25.0	5.0	.2	0.	0.	0.	0.	0.	.28
F415M5.006	.4	.0	21.7	.0	.03	150.0	.0	5.0	1.0	0.	0.	231.	0.	0.	.87
F415M5.007	.4	.0	32.7	.0	.05	150.0	-25.0	5.0	1.0	0.	0.	349.	0.	0.	1.47
F415M5.008	.5	.0	20.5	.0	.07	150.0	-28.0	5.0	1.3	0.	0.	219.	0.	0.	2.20
F415M5.009	.4	.0	19.3	.0	.06	150.0	-56.0	5.0	.9	0.	0.	206.	0.	0.	1.94
F415M5.010	.4	.0	29.0	.0	.05	150.0	-75.0	5.0	1.0	0.	0.	310.	0.	0.	1.59
F415M5.011	.4	.0	31.1	.0	.03	150.0	-84.0	5.0	1.2	0.	0.	332.	0.	0.	1.25
F415M5.012	.4	.0	29.4	.0	.04	150.0	-100.0	5.0	1.0	0.	0.	313.	0.	0.	1.37
F415N1.005	.1	.0	.0	.0	.00	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.06
F415N1.006	.2	.0	16.5	.0	.00	150.0	.0	11.0	.6	0.	0.	176.	0.	0.	.28
F415N1.007	.6	.0	31.1	.0	.06	150.0	-25.0	11.0	1.5	0.	0.	332.	0.	0.	1.73

FALCON 4: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F415N1.008	.6	.0	30.6	.0	.07	150.0	-28.0	11.0	1.6	0.	0.	327.	0.	0.	2.03
F415N1.009	.7	.0	27.7	.0	.06	150.0	-56.0	11.0	1.9	0.	0.	296.	0.	0.	1.81
F415N1.010	.5	.0	30.4	.0	.05	150.0	-75.0	11.0	1.3	0.	0.	324.	0.	0.	1.54
F415N1.011	.5	.0	29.8	.0	.06	150.0	-84.0	11.0	1.2	0.	0.	318.	0.	0.	1.84
F415N1.012	.4	.0	33.0	.0	.05	150.0	-100.0	11.0	1.0	0.	0.	353.	0.	0.	1.47
F415N2.005	.1	.0	.0	.0	.00	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.18
F415N2.006	.3	.0	24.0	.0	.00	150.0	.0	11.0	.8	0.	0.	256.	0.	0.	.25
F415N2.007	.4	.0	33.3	.0	.03	150.0	-25.0	11.0	1.2	0.	0.	356.	0.	0.	1.11
F415N2.008	.5	.0	15.5	.0	.05	150.0	-28.0	11.0	1.3	0.	0.	165.	0.	0.	1.49
F415N2.009	.5	.0	27.9	.0	.06	150.0	-56.0	11.0	1.2	0.	0.	298.	0.	0.	1.75
F415N2.010	.4	.0	12.8	.0	.04	150.0	-75.0	11.0	1.0	0.	0.	137.	0.	0.	1.31
F415N2.011	.4	.0	34.5	.0	.04	150.0	-84.0	11.0	1.1	0.	0.	369.	0.	0.	1.30
F415N2.012	.5	.0	29.4	.0	.04	150.0	-100.0	11.0	1.2	0.	0.	314.	0.	0.	1.20
F415N3.005	.1	.0	.0	.0	.00	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.13
F415N3.006	.3	.0	19.0	.0	.00	150.0	.0	11.0	.9	0.	0.	203.	0.	0.	.40
F415N3.007	.3	.0	13.7	.0	.03	150.0	-25.0	11.0	.9	0.	0.	146.	0.	0.	1.18
F415N3.008	.5	.0	21.2	.0	.04	150.0	-28.0	11.0	1.3	0.	0.	226.	0.	0.	1.35
F415N3.009	.4	.0	24.6	.0	.04	150.0	-56.0	11.0	1.0	0.	0.	262.	0.	0.	1.31
F415N3.010	.5	.0	22.8	.0	.03	150.0	-75.0	11.0	1.3	0.	0.	244.	0.	0.	1.09
F415N3.011	.4	.0	22.8	.0	.03	150.0	-84.0	11.0	1.1	0.	0.	243.	0.	0.	1.11
F415N3.012	.4	.0	28.5	.0	.04	150.0	-100.0	11.0	1.0	0.	0.	305.	0.	0.	1.34
F415N4.005	.1	.0	.0	.0	.00	150.0	25.0	11.0	.3	0.	0.	0.	0.	0.	.07
F415N4.006	.4	.0	13.4	.0	.00	150.0	.0	11.0	1.2	0.	0.	143.	0.	0.	.35
F415N4.007	.4	.0	25.9	.0	.03	150.0	-25.0	11.0	1.0	0.	0.	277.	0.	0.	1.13
F415N4.008	.4	.0	33.4	.0	.03	150.0	-28.0	11.0	1.1	0.	0.	356.	0.	0.	1.16
F415N4.009	.4	.0	27.7	.0	.06	150.0	-56.0	11.0	1.1	0.	0.	296.	0.	0.	1.89
F415N4.010	.6	.0	24.9	.0	.05	150.0	-75.0	11.0	1.7	0.	0.	265.	0.	0.	1.53
F415N4.011	.5	.0	27.6	.0	.03	150.0	-84.0	11.0	1.3	0.	0.	295.	0.	0.	1.14
F415N4.012	.4	.0	19.4	.0	.04	150.0	-100.0	11.0	1.1	0.	0.	207.	0.	0.	1.39
F415N5.005	.1	.0	.0	.0	.02	150.0	25.0	11.0	.3	0.	0.	0.	0.	0.	.50
F415N5.006	.4	.0	20.1	.0	.01	150.0	.0	11.0	1.2	0.	0.	214.	0.	0.	.52
F415N5.007	.6	.0	5.6	.0	.05	150.0	-25.0	11.0	1.6	0.	0.	60.	0.	0.	1.67
F415N5.008	.6	.0	19.8	.0	.06	150.0	-28.0	11.0	1.5	0.	0.	211.	0.	0.	1.99
F415N5.009	.7	.0	21.5	.0	.07	150.0	-56.0	11.0	1.8	0.	0.	229.	0.	0.	2.20
F415N5.010	.5	.0	32.3	.0	.06	150.0	-75.0	11.0	1.3	0.	0.	344.	0.	0.	1.91
F415N5.011	.5	.0	22.8	.0	.04	150.0	-84.0	11.0	1.4	0.	0.	243.	0.	0.	1.33
F415N5.012	.6	.0	22.9	.0	.04	150.0	-100.0	11.0	1.6	0.	0.	244.	0.	0.	1.26
F41501.005	.1	.0	.0	.0	.00	150.0	25.0	17.0	.1	0.	0.	0.	0.	0.	.13
F41501.006	.5	.0	8.8	.0	.01	150.0	.0	17.0	1.3	0.	0.	94.	0.	0.	.45
F41501.007	.6	.0	9.1	.0	.06	150.0	-25.0	17.0	1.6	0.	0.	97.	0.	0.	1.65
F41501.008	.5	.0	19.3	.0	.05	150.0	-28.0	17.0	1.3	0.	0.	206.	0.	0.	1.59
F41501.009	.5	.0	30.4	.0	.03	150.0	-56.0	17.0	1.2	0.	0.	325.	0.	0.	1.10

FALCON 4: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F41501.010	.4	.0	26.9	.0	.03	150.0	-75.0	17.0	1.1	0.	0.	287.	0.	0.	1.00
F41501.011	.6	.0	26.8	.0	.03	150.0	-84.0	17.0	1.5	0.	0.	286.	0.	0.	1.06
F41501.012	.7	.0	28.5	.0	.04	150.0	-100.0	17.0	1.7	0.	0.	304.	0.	0.	1.18
F41502.005	.1	.0	.0	.0	.01	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.40
F41502.006	.4	.0	24.3	.0	.02	150.0	.0	17.0	1.1	0.	0.	259.	0.	0.	.66
F41502.007	.6	.0	31.5	.0	.04	150.0	-25.0	17.0	1.6	0.	0.	336.	0.	0.	1.49
F41502.008	.7	.0	28.8	.0	.06	150.0	-28.0	17.0	1.9	0.	0.	308.	0.	0.	1.90
F41502.009	.7	.0	32.4	.0	.06	150.0	-56.0	17.0	1.9	0.	0.	346.	0.	0.	1.74
F41502.010	.5	.0	27.2	.0	.05	150.0	-75.0	17.0	1.4	0.	0.	291.	0.	0.	1.59
F41502.011	.6	.0	26.6	.0	.04	150.0	-84.0	17.0	1.6	0.	0.	284.	0.	0.	1.45
F41502.012	.5	.0	18.7	.0	.02	150.0	-100.0	17.0	1.4	0.	0.	200.	0.	0.	1.05
F41503.005	.1	.0	.0	.0	.00	150.0	25.0	17.0	.1	0.	0.	0.	0.	0.	.11
F41503.006	.4	.0	17.3	.0	-.01	150.0	.0	17.0	1.0	0.	0.	185.	0.	0.	.16
F41503.007	.5	.0	29.7	.0	.02	150.0	-25.0	17.0	1.4	0.	0.	318.	0.	0.	.98
F41503.008	.6	.0	15.7	.0	.01	150.0	-28.0	17.0	1.7	0.	0.	168.	0.	0.	.94
F41503.009	.5	.0	24.8	.0	.00	150.0	-56.0	17.0	1.4	0.	0.	264.	0.	0.	.76
F41503.010	.3	.0	23.6	.0	-.02	150.0	-75.0	17.0	.8	0.	0.	252.	0.	0.	.43
F41503.011	.4	.0	28.8	.0	-.02	150.0	-84.0	17.0	1.0	0.	0.	308.	0.	0.	.47
F41503.012	.4	.0	29.8	.0	.00	150.0	-100.0	17.0	1.1	0.	0.	318.	0.	0.	.69
F41504.005	.1	.0	.0	.0	.00	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.14
F41504.006	.4	.0	30.0	.0	.00	150.0	.0	17.0	1.1	0.	0.	320.	0.	0.	.21
F41504.007	.5	.0	31.0	.0	.07	150.0	-25.0	17.0	1.3	0.	0.	331.	0.	0.	1.92
F41504.008	.6	.0	26.3	.0	.06	150.0	-28.0	17.0	1.5	0.	0.	280.	0.	0.	1.86
F41504.009	.7	.0	22.4	.0	.04	150.0	-56.0	17.0	1.8	0.	0.	239.	0.	0.	1.42
F41504.010	.5	.0	31.4	.0	.03	150.0	-75.0	17.0	1.3	0.	0.	335.	0.	0.	.89
F41504.011	.5	.0	30.8	.0	.05	150.0	-84.0	17.0	1.4	0.	0.	329.	0.	0.	1.41
F41504.012	.5	.0	31.0	.0	.03	150.0	-100.0	17.0	1.3	0.	0.	331.	0.	0.	.95
F41505.005	.1	.0	.0	.0	.01	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.45
F41505.006	.6	.0	27.3	.0	.01	150.0	.0	17.0	1.6	0.	0.	291.	0.	0.	.36
F41505.007	.6	.0	28.5	.0	.04	150.0	-25.0	17.0	1.5	0.	0.	304.	0.	0.	1.37
F41505.008	.6	.0	28.6	.0	.05	150.0	-28.0	17.0	1.5	0.	0.	306.	0.	0.	1.59
F41505.009	.5	.0	33.8	.0	.04	150.0	-56.0	17.0	1.4	0.	0.	361.	0.	0.	1.29
F41505.010	.4	.0	33.3	.0	.03	150.0	-75.0	17.0	1.0	0.	0.	355.	0.	0.	1.02
F41505.011	.5	.0	32.9	.0	.04	150.0	-84.0	17.0	1.4	0.	0.	351.	0.	0.	1.15
F41505.012	.5	.0	34.6	.0	.03	150.0	-100.0	17.0	1.4	0.	0.	370.	0.	0.	.93

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N420A1.009	.3	.0	19.6	.0	.02	-62.0	30.0	2.0	.8	0.	0.	242.	0.	0.	.70
N420A1.008	13.4	.3	9.3	59.2	1.76	-62.0	20.0	2.0	29.5	58.	91.	115.	385.	724.	52.50
N420A1.007	16.1	1.5	19.4	40.9	2.25	-62.0	10.0	2.0	34.1	20.	23.	239.	413.	457.	66.22
N420A1.006	20.2	.3	11.8	43.2	3.58	-62.0	.0	2.0	40.6	14.	14.	146.	409.	463.	100.50
N420A1.005	11.7	.2	18.9	57.0	1.21	-62.0	-20.0	2.0	26.3	3.	74.	233.	358.	702.	37.39
N420A1.004	2.6	14.0	21.8	29.1	.13	-62.0	-30.0	2.0	6.6	266.	0.	268.	0.	327.	4.46
N420A2.009	.6	.0	10.7	.0	.02	-62.0	30.0	2.0	1.5	0.	0.	132.	0.	0.	.58
N420A2.008	13.9	2.9	22.6	60.3	1.65	-62.0	20.0	2.0	30.4	51.	67.	278.	412.	743.	50.22
N420A2.007	17.4	1.4	15.1	42.4	2.46	-62.0	10.0	2.0	36.3	20.	21.	186.	425.	464.	71.24
N420A2.006	21.8	.5	23.9	60.1	3.92	-62.0	.0	2.0	43.0	15.	16.	295.	434.	502.	108.84
N420A2.005	11.8	.3	24.8	55.1	1.26	-62.0	-20.0	2.0	26.5	32.	34.	306.	406.	641.	38.91
N420A2.004	2.3	7.9	25.7	31.6	.14	-62.0	-30.0	2.0	5.9	236.	0.	317.	0.	317.	4.71
N420A3.009	.3	.0	31.4	.0	.00	-62.0	30.0	2.0	.8	0.	0.	387.	0.	0.	.26
N420A3.008	13.4	1.4	18.9	50.9	1.37	-62.0	20.0	2.0	29.5	64.	76.	233.	381.	563.	42.64
N420A3.007	17.0	2.0	16.1	42.6	2.21	-62.0	10.0	2.0	35.6	29.	30.	199.	405.	442.	65.39
N420A3.006	21.0	.8	12.3	42.1	3.52	-62.0	.0	2.0	41.8	10.	25.	152.	428.	453.	98.99
N420A3.005	14.4	.2	19.7	59.7	1.14	-62.0	-20.0	2.0	31.3	8.	111.	242.	407.	409.	36.33
N420A3.004	1.7	14.5	24.3	29.3	.13	-62.0	-30.0	2.0	4.4	0.	0.	300.	0.	0.	4.52
N420A4.009	.2	.0	24.9	.0	.00	-62.0	30.0	2.0	.7	0.	0.	307.	0.	0.	.15
N420A4.008	14.2	.2	21.3	54.9	1.74	-62.0	20.0	2.0	30.9	3.	25.	263.	402.	660.	52.59
N420A4.007	16.0	1.1	17.1	44.7	1.78	-62.0	10.0	2.0	34.0	21.	24.	210.	455.	461.	52.72
N420A4.006	21.2	.9	16.7	45.2	3.76	-62.0	.0	2.0	42.1	13.	20.	206.	444.	469.	105.10
N420A4.005	11.0	.2	9.7	61.8	1.01	-62.0	-20.0	2.0	25.1	3.	9.	119.	347.	599.	31.50
N420A4.004	2.0	5.3	12.7	27.0	.15	-62.0	-30.0	2.0	5.3	157.	0.	157.	0.	157.	4.92
N420A5.009	.2	.0	24.5	.0	-.01	-62.0	30.0	2.0	.6	0.	0.	301.	0.	0.	.11
N420A5.008	15.7	2.0	20.6	58.2	1.88	-62.0	20.0	2.0	33.6	25.	27.	253.	492.	684.	56.47
N420A5.007	16.8	1.6	24.1	48.1	2.23	-62.0	10.0	2.0	35.3	22.	26.	297.	391.	477.	65.52
N420A5.006	20.1	.6	24.6	51.2	3.81	-62.0	.0	2.0	40.4	15.	21.	304.	437.	528.	106.28
N420A5.005	14.4	1.5	11.1	61.7	1.49	-62.0	-20.0	2.0	31.2	20.	75.	137.	410.	754.	45.55
N420A5.004	2.7	11.5	25.8	30.1	.16	-62.0	-30.0	2.0	6.9	248.	0.	318.	0.	351.	5.46
N420B1.009	.1	.0	.0	.0	.00	-32.0	30.0	1.0	.2	0.	0.	0.	0.	0.	.21
N420B1.008	22.4	.2	26.1	61.5	4.97	-32.0	20.0	1.0	43.8	2.	2.	322.	492.	710.	136.15
N420B1.007	28.0	.1	5.3	41.5	3.25	-32.0	10.0	1.0	51.3	1.	1.	65.	395.	397.	88.50
N420B1.006	16.9	.1	25.5	35.1	.87	-32.0	.0	1.0	35.5	2.	2.	315.	322.	388.	27.32
N420B1.005	20.1	.6	17.1	40.6	2.57	-32.0	-20.0	1.0	40.5	62.	65.	210.	392.	440.	72.56
N420B1.004	1.0	23.3	23.3	25.9	.10	-32.0	-30.0	1.0	2.7	0.	0.	287.	0.	0.	3.56
N420B2.009	.2	.0	29.0	.0	.03	-32.0	30.0	1.0	.6	0.	0.	357.	0.	0.	.89
N420B2.008	20.6	.1	20.7	60.6	4.77	-32.0	20.0	1.0	41.2	1.	2.	255.	515.	703.	130.84
N420B2.007	30.7	.1	17.0	54.0	3.33	-32.0	10.0	1.0	54.5	1.	1.	209.	363.	437.	89.61
N420B2.006	15.1	.1	19.8	55.2	.88	-32.0	.0	1.0	32.5	1.	1.	244.	318.	332.	27.65
N420B2.005	22.7	.2	18.5	37.3	2.26	-32.0	-20.0	1.0	44.2	3.	16.	228.	374.	386.	64.87
N420B2.004	1.2	18.5	25.3	26.0	.12	-32.0	-30.0	1.0	3.3	0.	0.	312.	0.	0.	4.07

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N420B3.009	.2	.0	24.3	.0	.01	-32.0	30.0	1.0	.5	0.	0.	300.	0.	0.	.61
N420B3.008	21.9	.1	17.1	60.2	4.54	-32.0	20.0	1.0	43.2	2.	2.	211.	413.	565.	123.19
N420B3.007	27.6	.1	16.6	43.3	3.04	-32.0	10.0	1.0	50.8	1.	1.	205.	359.	379.	82.72
N420B3.006	12.4	.1	6.6	35.0	1.02	-32.0	.0	1.0	27.7	1.	2.	81.	325.	340.	31.68
N420B3.005	21.8	.1	26.4	56.3	2.47	-32.0	-20.0	1.0	43.0	2.	31.	326.	380.	455.	70.15
N420B3.004	1.5	19.3	21.9	22.1	.10	-32.0	-30.0	1.0	4.0	0.	0.	270.	0.	0.	3.55
N420B4.009	.2	.0	.0	.0	-.12	-32.0	30.0	1.0	.5	0.	0.	0.	0.	0.	.04
N420B4.008	19.6	.1	3.8	54.5	4.40	-32.0	20.0	1.0	39.8	2.	2.	47.	445.	671.	121.52
N420B4.007	31.7	.1	11.1	36.5	3.03	-32.0	10.0	1.0	55.7	1.	1.	136.	409.	413.	81.56
N420B4.006	13.2	.1	24.6	33.6	.75	-32.0	.0	1.0	29.2	1.	1.	303.	312.	353.	23.68
N420B4.005	18.4	.2	8.1	40.4	1.70	-32.0	-20.0	1.0	37.9	13.	21.	99.	346.	373.	50.52
N420B4.004	1.1	22.5	27.6	27.7	.08	-32.0	-30.0	1.0	2.9	0.	0.	340.	0.	0.	2.73
N420B5.009	.1	.0	.0	.0	-.02	-32.0	30.0	1.0	.2	0.	0.	0.	0.	0.	.04
N420B5.008	19.5	.1	25.1	61.1	4.41	-32.0	20.0	1.0	39.6	2.	2.	310.	470.	721.	122.56
N420B5.007	31.1	.1	22.3	47.7	2.93	-32.0	10.0	1.0	54.9	1.	1.	275.	404.	427.	80.22
N420B5.006	13.0	.1	24.6	35.8	.96	-32.0	.0	1.0	28.8	1.	2.	304.	313.	359.	29.88
N420B5.005	23.2	.1	23.3	50.5	2.73	-32.0	-20.0	1.0	44.9	3.	40.	287.	377.	466.	76.69
N420B5.004	1.1	11.0	27.5	27.6	.12	-32.0	-30.0	1.0	3.0	0.	0.	339.	0.	0.	4.04
N420C1.009	.2	.0	.0	.0	.03	-2.0	30.0	1.0	.5	0.	0.	0.	0.	0.	.95
N420C1.008	5.0	2.3	24.2	48.8	.52	-2.0	20.0	1.0	12.4	140.	296.	298.	301.	378.	17.15
N420C1.007	2.8	.3	21.8	29.9	.31	-2.0	10.0	1.0	7.1	4.	0.	269.	0.	340.	10.19
N420C1.006	3.7	.4	27.1	31.9	.35	-2.0	.0	1.0	9.5	163.	0.	334.	0.	341.	11.46
N420C1.005	1.8	12.6	24.1	25.3	.27	-2.0	-20.0	1.0	4.6	0.	0.	297.	0.	0.	8.95
N420C1.004	2.0	12.2	12.2	21.7	.17	-2.0	-30.0	1.0	5.1	151.	0.	151.	0.	151.	5.66
N420C2.009	.3	.0	33.1	.0	.02	-2.0	30.0	1.0	.8	0.	0.	408.	0.	0.	.68
N420C2.008	7.2	.1	24.2	47.9	.60	-2.0	20.0	1.0	17.3	21.	246.	298.	308.	472.	19.99
N420C2.007	3.0	1.3	22.5	31.1	.32	-2.0	10.0	1.0	7.6	210.	0.	278.	0.	283.	10.63
N420C2.006	2.6	1.0	17.1	30.2	.30	-2.0	.0	1.0	6.6	210.	0.	211.	0.	212.	9.96
N420C2.005	2.0	9.5	19.8	27.2	.29	-2.0	-20.0	1.0	5.2	244.	0.	244.	0.	246.	9.65
N420C2.004	1.8	14.5	27.0	30.1	.19	-2.0	-30.0	1.0	4.6	0.	0.	333.	0.	0.	6.31
N420C3.009	.3	.0	23.9	.0	.03	-2.0	30.0	1.0	.9	0.	0.	294.	0.	0.	1.12
N420C3.008	5.0	.1	21.0	60.7	.65	-2.0	20.0	1.0	12.4	15.	233.	259.	268.	432.	21.15
N420C3.007	4.5	.3	.4	31.8	.35	-2.0	10.0	1.0	11.4	4.	4.	5.	5.	318.	11.36
N420C3.006	3.0	.5	10.1	32.0	.35	-2.0	.0	1.0	7.6	57.	0.	124.	0.	319.	11.46
N420C3.005	1.5	4.8	5.0	30.0	.31	-2.0	-20.0	1.0	3.9	0.	0.	62.	0.	0.	10.26
N420C3.004	1.8	10.9	15.3	30.7	.16	-2.0	-30.0	1.0	4.7	0.	0.	189.	0.	0.	5.49
N420C4.009	.2	.0	29.2	.0	.02	-2.0	30.0	1.0	.7	0.	0.	360.	0.	0.	.74
N420C4.008	7.9	1.5	26.4	55.5	.62	-2.0	20.0	1.0	18.9	89.	90.	325.	333.	506.	20.22
N420C4.007	2.4	1.6	25.9	30.5	.34	-2.0	10.0	1.0	6.2	139.	0.	319.	0.	332.	11.34
N420C4.006	2.4	.5	26.6	32.6	.36	-2.0	.0	1.0	6.3	109.	0.	328.	0.	330.	11.67
N420C4.005	2.4	8.9	26.6	29.5	.32	-2.0	-20.0	1.0	6.3	267.	0.	328.	0.	330.	10.53
N420C4.004	2.8	13.3	13.3	30.1	.19	-2.0	-30.0	1.0	7.2	164.	0.	164.	0.	189.	6.26

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS: PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS: POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N420C5.009	.1	.0	.0	.0	-.01	-2.0	30.0	1.0	.2	0.	0.	0.	0.	0.	.21
N420C5.008	11.2	.5	13.5	61.7	.52	-2.0	20.0	1.0	25.5	116.	162.	166.	175.	386.	18.32
N420C5.007	6.2	.5	13.6	30.0	.34	-2.0	10.0	1.0	15.1	7.	167.	168.	170.	328.	11.00
N420C5.006	3.5	.4	13.7	29.8	.32	-2.0	.0	1.0	8.9	5.	0.	168.	0.	330.	10.43
N420C5.005	2.2	6.3	6.6	28.3	.29	-2.0	-20.0	1.0	5.8	80.	0.	81.	0.	83.	9.74
N420C5.004	1.8	8.0	13.0	27.3	.15	-2.0	-30.0	1.0	4.7	0.	0.	160.	0.	0.	5.16
F420D1.005	.1	.0	.0	.0	.00	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.29
F420D1.006	.1	.0	.0	.0	.01	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.65
F420D1.007	.1	.0	.0	.0	-.03	50.0	42.0	1.0	.3	0.	0.	0.	0.	0.	.10
F420D1.008	.2	.0	47.6	.0	-.01	50.0	33.0	1.0	.7	0.	0.	587.	0.	0.	.54
F420D1.009	1.1	18.6	18.6	18.7	.09	50.0	.0	1.0	2.8	0.	0.	229.	0.	0.	3.29
F420D1.010	.7	.0	23.2	.0	.12	50.0	-33.0	1.0	1.9	0.	0.	286.	0.	0.	3.89
F420D1.011	.7	.0	20.9	.0	.10	50.0	-50.0	1.0	1.8	0.	0.	257.	0.	0.	3.41
F420D1.012	.5	.0	16.0	.0	.08	50.0	-66.0	1.0	1.4	0.	0.	197.	0.	0.	2.86
F420D2.005	.1	.0	.0	.0	-.01	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.19
F420D2.006	.1	.0	.0	.0	.00	50.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.37
F420D2.007	.1	.0	.0	.0	-.01	50.0	42.0	1.0	.3	0.	0.	0.	0.	0.	.19
F420D2.008	.2	.0	29.3	.0	-.02	50.0	33.0	1.0	.7	0.	0.	362.	0.	0.	.37
F420D2.009	1.1	25.3	25.3	25.3	.08	50.0	.0	1.0	2.8	0.	0.	312.	0.	0.	2.78
F420D2.010	.6	.0	23.6	.0	.10	50.0	-33.0	1.0	1.6	0.	0.	290.	0.	0.	3.41
F420D2.011	.7	.0	25.4	.0	.10	50.0	-50.0	1.0	1.9	0.	0.	313.	0.	0.	3.32
F420D2.012	.6	.0	22.4	.0	.08	50.0	-66.0	1.0	1.6	0.	0.	276.	0.	0.	2.72
F420D3.005	.1	.0	.0	.0	.00	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.36
F420D3.006	.1	.0	.0	.0	-.03	50.0	50.0	1.0	.2	0.	0.	0.	0.	0.	.07
F420D3.007	.1	.0	.0	.0	-.02	50.0	42.0	1.0	.3	0.	0.	0.	0.	0.	.17
F420D3.008	.2	.0	65.1	.0	-.01	50.0	33.0	1.0	.7	0.	0.	803.	0.	0.	.54
F420D3.009	.9	.0	9.0	.0	.09	50.0	.0	1.0	2.5	0.	0.	111.	0.	0.	3.20
F420D3.010	.7	.0	20.0	.0	.11	50.0	-33.0	1.0	1.9	0.	0.	247.	0.	0.	3.77
F420D3.011	.6	.0	21.5	.0	.08	50.0	-50.0	1.0	1.6	0.	0.	265.	0.	0.	3.02
F420D3.012	.5	.0	27.2	.0	.07	50.0	-66.0	1.0	1.3	0.	0.	335.	0.	0.	2.57
F420D4.005	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.26
F420D4.006	.1	.0	.0	.0	.00	50.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.26
F420D4.007	.1	.0	.0	.0	-.01	50.0	42.0	1.0	.2	0.	0.	0.	0.	0.	.18
F420D4.008	.3	.0	36.3	.0	.00	50.0	33.0	1.0	.8	0.	0.	448.	0.	0.	.67
F420D4.009	.9	.0	24.8	.0	.08	50.0	.0	1.0	2.3	0.	0.	306.	0.	0.	2.75
F420D4.010	.6	.0	7.3	.0	.12	50.0	-33.0	1.0	1.6	0.	0.	89.	0.	0.	4.05
F420D4.011	.6	.0	21.8	.0	.10	50.0	-50.0	1.0	1.5	0.	0.	269.	0.	0.	3.31
F420D4.012	.5	.0	19.0	.0	.08	50.0	-66.0	1.0	1.4	0.	0.	234.	0.	0.	2.81
F420D5.005	.1	.0	.0	.0	.01	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.59
F420D5.006	.2	.0	.0	.0	.02	50.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.84
F420D5.007	.1	.0	.0	.0	.03	50.0	42.0	1.0	.4	0.	0.	0.	0.	0.	1.15
F420D5.008	.2	.0	12.1	.0	-.01	50.0	33.0	1.0	.6	0.	0.	149.	0.	0.	.47

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F420D5.009	.8	.0	21.8	.0	.09	50.0	.0	1.0	2.0	0.	0.	268.	0.	0.	2.96
F420D5.010	.7	.0	26.3	.0	.12	50.0	-33.0	1.0	1.9	0.	0.	324.	0.	0.	4.10
F420D5.011	.6	.0	25.3	.0	.09	50.0	-50.0	1.0	1.6	0.	0.	312.	0.	0.	2.92
F420D5.012	.5	.0	25.6	.0	.08	50.0	-66.0	1.0	1.3	0.	0.	316.	0.	0.	2.68
F420E1.005	.1	.0	.0	.0	.01	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.50
F420E1.006	.1	.0	.0	.0	.01	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.34
F420E1.007	.2	.0	.0	.0	.02	50.0	42.0	5.0	.5	0.	0.	0.	0.	0.	.77
F420E1.008	.3	.0	45.0	.0	.01	50.0	33.0	5.0	.7	0.	0.	554.	0.	0.	.76
F420E1.009	1.1	11.4	11.4	11.4	.12	50.0	.0	5.0	2.9	0.	0.	140.	0.	0.	3.96
F420E1.010	1.1	23.4	23.4	23.5	.11	50.0	-33.0	5.0	2.8	0.	0.	289.	0.	0.	3.91
F420E1.011	.9	.0	17.5	.0	.11	50.0	-50.0	5.0	2.3	0.	0.	216.	0.	0.	3.77
F420E1.012	.5	.0	15.7	.0	.07	50.0	-66.0	5.0	1.4	0.	0.	193.	0.	0.	2.38
F420E2.005	.1	.0	.0	.0	.01	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.39
F420E2.006	.1	.0	.0	.0	.00	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.31
F420E2.007	.1	.0	.0	.0	-.03	50.0	42.0	5.0	.2	0.	0.	0.	0.	0.	.12
F420E2.008	.2	.0	38.3	.0	-.01	50.0	33.0	5.0	.6	0.	0.	472.	0.	0.	.53
F420E2.009	1.0	5.5	5.5	12.2	.09	50.0	.0	5.0	2.8	0.	0.	68.	0.	0.	3.00
F420E2.010	.7	.0	13.1	.0	.10	50.0	-33.0	5.0	1.9	0.	0.	162.	0.	0.	3.56
F420E2.011	.6	.0	5.5	.0	.06	50.0	-50.0	5.0	1.6	0.	0.	68.	0.	0.	2.52
F420E2.012	.5	.0	20.2	.0	.04	50.0	-66.0	5.0	1.3	0.	0.	249.	0.	0.	1.90
F420E3.005	.1	.0	.0	.0	.03	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.98
F420E3.006	.2	.0	.0	.0	.02	50.0	50.0	5.0	.5	0.	0.	0.	0.	0.	.85
F420E3.007	.1	.0	.0	.0	.01	50.0	42.0	5.0	.4	0.	0.	0.	0.	0.	.63
F420E3.008	.3	.0	35.6	.0	.01	50.0	33.0	5.0	.8	0.	0.	439.	0.	0.	1.04
F420E3.009	1.2	20.2	20.2	20.2	.13	50.0	.0	5.0	3.1	0.	0.	249.	0.	0.	4.34
F420E3.010	.9	.0	23.5	.0	.14	50.0	-33.0	5.0	2.5	0.	0.	290.	0.	0.	4.69
F420E3.011	1.1	24.2	24.2	24.3	.15	50.0	-50.0	5.0	3.0	0.	0.	299.	0.	0.	4.97
F420E3.012	.8	.0	17.7	.0	.11	50.0	-66.0	5.0	2.1	0.	0.	218.	0.	0.	3.60
F420E4.005	.1	.0	.0	.0	.00	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.33
F420E4.006	.1	.0	.0	.0	-.02	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.12
F420E4.007	.1	.0	.0	.0	-.02	50.0	42.0	5.0	.2	0.	0.	0.	0.	0.	.13
F420E4.008	.2	.0	50.3	.0	-.02	50.0	33.0	5.0	.6	0.	0.	620.	0.	0.	.46
F420E4.009	1.0	23.5	23.5	23.5	.12	50.0	.0	5.0	2.7	0.	0.	289.	0.	0.	3.94
F420E4.010	1.1	18.3	18.3	18.3	.11	50.0	-33.0	5.0	2.8	0.	0.	225.	0.	0.	3.90
F420E4.011	.9	.0	19.3	.0	.10	50.0	-50.0	5.0	2.4	0.	0.	238.	0.	0.	3.39
F420E4.012	.7	.0	14.6	.0	.09	50.0	-66.0	5.0	1.8	0.	0.	180.	0.	0.	3.04
F420E5.005	.1	.0	.0	.0	-.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.14
F420E5.006	.1	.0	.0	.0	.00	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.30
F420E5.007	.1	.0	.0	.0	.01	50.0	42.0	5.0	.3	0.	0.	0.	0.	0.	.42
F420E5.008	.2	.0	30.9	.0	.01	50.0	33.0	5.0	.7	0.	0.	381.	0.	0.	.72
F420E5.009	1.0	22.5	22.5	22.6	.09	50.0	.0	5.0	2.7	0.	0.	278.	0.	0.	3.12
F420E5.010	.9	.0	20.8	.0	.11	50.0	-33.0	5.0	2.3	0.	0.	256.	0.	0.	3.65

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F420E5.011	.7	.0	21.2	.0	.09	50.0	-50.0	5.0	1.9	0.	0.	262.	0.	0.	3.05
F420E5.012	1.0	12.6	12.6	12.7	.06	50.0	-66.0	5.0	2.8	0.	0.	156.	0.	0.	2.26
F420F1.005	.1	.0	.0	.0	.00	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.29
F420F1.006	.1	.0	.0	.0	.00	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.15
F420F1.007	.1	.0	.0	.0	-.03	50.0	42.0	11.0	.2	0.	0.	0.	0.	0.	.00
F420F1.008	.2	.0	55.2	.0	-.02	50.0	33.0	11.0	.6	0.	0.	680.	0.	0.	.30
F420F1.009	1.8	16.8	17.1	25.7	.11	50.0	.0	11.0	4.6	0.	0.	211.	0.	0.	3.69
F420F1.010	1.3	13.2	21.2	21.2	.11	50.0	-33.0	11.0	3.4	0.	0.	261.	0.	0.	3.66
F420F1.011	.8	.0	9.9	.0	.08	50.0	-50.0	11.0	2.2	0.	0.	122.	0.	0.	2.83
F420F1.012	.5	.0	15.0	.0	.00	50.0	-66.0	11.0	1.4	0.	0.	185.	0.	0.	1.15
F420F2.005	.1	.0	.0	.0	.00	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.09
F420F2.006	.1	.0	.0	.0	.01	50.0	50.0	11.0	.3	0.	0.	0.	0.	0.	.54
F420F2.007	.0	.0	.0	.0	.01	50.0	42.0	11.0	.1	0.	0.	0.	0.	0.	.63
F420F2.008	.2	.0	2.5	.0	.01	50.0	33.0	11.0	.6	0.	0.	31.	0.	0.	.67
F420F2.009	1.4	2.7	21.5	24.5	.12	50.0	.0	11.0	3.6	0.	0.	265.	0.	0.	4.06
F420F2.010	.9	.0	21.4	.0	.12	50.0	-33.0	11.0	2.4	0.	0.	263.	0.	0.	4.09
F420F2.011	1.1	10.6	10.7	10.7	.12	50.0	-50.0	11.0	2.9	0.	0.	132.	0.	0.	3.98
F420F2.012	.8	.0	25.1	.0	.07	50.0	-66.0	11.0	2.3	0.	0.	309.	0.	0.	2.46
F420F3.005	.1	.0	.0	.0	-.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.10
F420F3.006	.1	.0	.0	.0	.00	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.17
F420F3.007	.1	.0	.0	.0	.00	50.0	42.0	11.0	.2	0.	0.	0.	0.	0.	.27
F420F3.008	.2	.0	.0	.0	-.01	50.0	33.0	11.0	.5	0.	0.	0.	0.	0.	.38
F420F3.009	1.4	3.3	20.8	24.9	.10	50.0	.0	11.0	3.6	0.	0.	256.	0.	0.	3.58
F420F3.010	1.1	18.0	18.0	18.1	.11	50.0	-33.0	11.0	3.0	0.	0.	222.	0.	0.	3.64
F420F3.011	.9	.0	22.1	.0	.09	50.0	-50.0	11.0	2.5	0.	0.	273.	0.	0.	3.03
F420F3.012	.8	.0	24.8	.0	.06	50.0	-66.0	11.0	2.2	0.	0.	306.	0.	0.	2.11
F420F4.005	.1	.0	.0	.0	.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.27
F420F4.006	.1	.0	.0	.0	.00	50.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.19
F420F4.007	.1	.0	.0	.0	.01	50.0	42.0	11.0	.3	0.	0.	0.	0.	0.	.57
F420F4.008	.2	.0	40.5	.0	.00	50.0	33.0	11.0	.7	0.	0.	499.	0.	0.	.62
F420F4.009	1.3	6.0	6.0	25.6	.11	50.0	.0	11.0	3.4	0.	0.	74.	0.	0.	3.71
F420F4.010	.9	.0	22.7	.0	.11	50.0	-33.0	11.0	2.4	0.	0.	280.	0.	0.	3.67
F420F4.011	1.1	26.5	27.4	27.5	.10	50.0	-50.0	11.0	2.8	0.	0.	337.	0.	0.	3.45
F420F4.012	.9	.0	28.9	.0	.08	50.0	-66.0	11.0	2.3	0.	0.	356.	0.	0.	2.57
F420F5.005	.1	.0	.0	.0	-.01	50.0	66.0	11.0	.3	0.	0.	0.	0.	0.	.18
F420F5.006	.0	.0	.0	.0	-.01	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.19
F420F5.007	.1	.0	.0	.0	.00	50.0	42.0	11.0	.2	0.	0.	0.	0.	0.	.07
F420F5.008	.3	.0	24.1	.0	-.01	50.0	33.0	11.0	.7	0.	0.	297.	0.	0.	.49
F420F5.009	1.3	7.2	18.3	25.4	.11	50.0	.0	11.0	3.5	0.	0.	225.	0.	0.	3.72
F420F5.010	.8	.0	9.9	.0	.10	50.0	-33.0	11.0	2.1	0.	0.	122.	0.	0.	3.46
F420F5.011	.9	.0	24.7	.0	.08	50.0	-50.0	11.0	2.4	0.	0.	305.	0.	0.	2.77
F420F5.012	.7	.0	19.5	.0	.06	50.0	-66.0	11.0	1.9	0.	0.	240.	0.	0.	1.98

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F420G1.005	.1	.0	.0	.0	.00	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.24
F420G1.006	.1	.0	.0	.0	.01	50.0	50.0	17.0	.4	0.	0.	0.	0.	0.	.42
F420G1.007	.1	.0	.0	.0	.01	50.0	42.0	17.0	.3	0.	0.	0.	0.	0.	.48
F420G1.008	.2	.0	.0	.0	-.01	50.0	33.0	17.0	.5	0.	0.	0.	0.	0.	.46
F420G1.009	1.3	10.0	20.8	24.7	.09	50.0	.0	17.0	3.5	0.	0.	257.	0.	0.	3.22
F420G1.010	1.5	19.6	19.6	19.7	.04	50.0	-33.0	17.0	4.0	0.	0.	242.	0.	0.	1.59
F420G1.011	1.0	19.9	19.9	20.2	.04	50.0	-50.0	17.0	2.8	0.	0.	245.	0.	0.	1.59
F420G1.012	.7	.0	19.0	.0	.04	50.0	-66.0	17.0	1.8	0.	0.	234.	0.	0.	1.32
F420G2.005	.1	.0	.0	.0	.00	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.31
F420G2.006	.1	.0	.0	.0	.00	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.26
F420G2.007	.1	.0	.0	.0	-.01	50.0	42.0	17.0	.2	0.	0.	0.	0.	0.	.08
F420G2.008	.3	.0	44.8	.0	.00	50.0	33.0	17.0	.7	0.	0.	552.	0.	0.	.63
F420G2.009	1.8	2.6	25.0	27.7	.12	50.0	.0	17.0	4.8	0.	0.	308.	0.	0.	4.06
F420G2.010	1.3	12.9	23.9	24.0	.06	50.0	-33.0	17.0	3.4	0.	0.	295.	0.	0.	2.27
F420G2.011	1.1	25.5	25.5	26.5	.07	50.0	-50.0	17.0	2.8	0.	0.	314.	0.	0.	2.42
F420G2.012	.6	.0	16.5	.0	.04	50.0	-66.0	17.0	1.7	0.	0.	203.	0.	0.	1.42
F420G3.005	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.17
F420G3.006	.1	.0	.0	.0	.00	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.23
F420G3.007	.1	.0	.0	.0	.00	50.0	42.0	17.0	.4	0.	0.	0.	0.	0.	.34
F420G3.008	.2	.0	21.8	.0	-.01	50.0	33.0	17.0	.6	0.	0.	268.	0.	0.	.43
F420G3.009	1.8	1.9	8.5	26.0	.07	50.0	.0	17.0	4.7	0.	0.	105.	0.	0.	2.74
F420G3.010	.8	.0	22.8	.0	.03	50.0	-33.0	17.0	2.1	0.	0.	281.	0.	0.	1.31
F420G3.011	1.0	24.3	24.3	24.4	.02	50.0	-50.0	17.0	2.7	0.	0.	299.	0.	0.	1.47
F420G3.012	.6	.0	20.3	.0	.03	50.0	-66.0	17.0	1.7	0.	0.	251.	0.	0.	1.15
F420G4.005	.1	.0	.0	.0	-.02	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.02
F420G4.006	.1	.0	.0	.0	-.02	50.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.02
F420G4.007	.1	.0	.0	.0	-.03	50.0	42.0	17.0	.1	0.	0.	0.	0.	0.	.03
F420G4.008	.2	.0	.0	.0	-.03	50.0	33.0	17.0	.4	0.	0.	0.	0.	0.	.21
F420G4.009	1.7	7.5	15.5	27.5	.05	50.0	.0	17.0	4.4	0.	0.	191.	0.	0.	2.37
F420G4.010	1.0	.0	2.2	.0	.02	50.0	-33.0	17.0	2.6	0.	0.	27.	0.	0.	1.26
F420G4.011	.8	.0	18.0	.0	.02	50.0	-50.0	17.0	2.1	0.	0.	222.	0.	0.	1.26
F420G4.012	.6	.0	12.9	.0	.02	50.0	-66.0	17.0	1.6	0.	0.	158.	0.	0.	1.12
F420G5.005	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.15
F420G5.006	.1	.0	.0	.0	-.01	50.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.16
F420G5.007	.1	.0	.0	.0	-.01	50.0	42.0	17.0	.2	0.	0.	0.	0.	0.	.10
F420G5.008	.2	.0	36.3	.0	.00	50.0	33.0	17.0	.6	0.	0.	447.	0.	0.	.53
F420G5.009	1.6	2.8	25.9	27.8	.08	50.0	.0	17.0	4.3	0.	0.	319.	0.	0.	2.89
F420G5.010	1.3	18.8	18.9	18.9	.04	50.0	-33.0	17.0	3.5	0.	0.	233.	0.	0.	1.67
F420G5.011	1.1	19.0	19.1	24.5	.01	50.0	-50.0	17.0	2.9	0.	0.	235.	0.	0.	1.25
F420G5.012	.9	.0	19.1	.0	.01	50.0	-66.0	17.0	2.4	0.	0.	235.	0.	0.	.78
F420H1.005	.1	.0	.0	.0	.00	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.16
F420H1.006	.1	.0	.0	.0	.02	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.75

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F420H1.007	.2	.0	.0	.0	.03	150.0	25.0	1.0	.5	0.	0.	0.	0.	0.	1.02
F420H1.008	.3	.0	35.8	.0	.02	150.0	.0	1.0	.7	0.	0.	441.	0.	0.	1.04
F420H1.009	.4	.0	30.9	.0	.07	150.0	-25.0	1.0	1.1	0.	0.	381.	0.	0.	2.39
F420H1.010	.4	.0	24.8	.0	.10	150.0	-56.0	1.0	1.2	0.	0.	306.	0.	0.	3.24
F420H1.011	.4	.0	31.2	.0	.10	150.0	-75.0	1.0	1.2	0.	0.	384.	0.	0.	3.19
F420H1.012	.4	.0	25.1	.0	.08	150.0	-100.0	1.0	1.0	0.	0.	309.	0.	0.	2.57
F420H2.005	.0	.0	.0	.0	-.02	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.04
F420H2.006	.1	.0	.0	.0	.01	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.55
F420H2.007	.1	.0	.0	.0	-.01	150.0	25.0	1.0	.3	0.	0.	0.	0.	0.	.21
F420H2.008	.2	.0	11.9	.0	.00	150.0	.0	1.0	.6	0.	0.	147.	0.	0.	.61
F420H2.009	.4	.0	22.2	.0	.03	150.0	-25.0	1.0	1.1	0.	0.	274.	0.	0.	1.38
F420H2.010	.6	.0	26.7	.0	.08	150.0	-56.0	1.0	1.5	0.	0.	329.	0.	0.	2.68
F420H2.011	.7	.0	27.6	.0	.10	150.0	-75.0	1.0	1.8	0.	0.	340.	0.	0.	3.58
F420H2.012	.4	.0	28.4	.0	.04	150.0	-100.0	1.0	1.0	0.	0.	350.	0.	0.	1.81
F420H3.005	.1	.0	.0	.0	-.01	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.10
F420H3.006	.1	.0	.0	.0	.00	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.18
F420H3.007	.1	.0	.0	.0	-.02	150.0	25.0	1.0	.3	0.	0.	0.	0.	0.	.18
F420H3.008	.2	.0	.0	.0	.00	150.0	.0	1.0	.5	0.	0.	0.	0.	0.	.68
F420H3.009	.6	.0	24.5	.0	.07	150.0	-25.0	1.0	1.6	0.	0.	302.	0.	0.	2.27
F420H3.010	.5	.0	18.4	.0	.10	150.0	-56.0	1.0	1.3	0.	0.	226.	0.	0.	3.33
F420H3.011	.5	.0	28.6	.0	.10	150.0	-75.0	1.0	1.3	0.	0.	352.	0.	0.	3.25
F420H3.012	.4	.0	32.1	.0	.05	150.0	-100.0	1.0	.9	0.	0.	395.	0.	0.	1.75
F420H4.005	.1	.0	.0	.0	.01	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.42
F420H4.006	.1	.0	.0	.0	-.02	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.10
F420H4.007	.2	.0	.0	.0	.02	150.0	25.0	1.0	.4	0.	0.	0.	0.	0.	.65
F420H4.008	.2	.0	.0	.0	.00	150.0	.0	1.0	.5	0.	0.	0.	0.	0.	.47
F420H4.009	.4	.0	17.5	.0	.07	150.0	-25.0	1.0	1.1	0.	0.	216.	0.	0.	2.31
F420H4.010	.5	.0	30.2	.0	.09	150.0	-56.0	1.0	1.4	0.	0.	373.	0.	0.	3.20
F420H4.011	.4	.0	30.0	.0	.07	150.0	-75.0	1.0	1.2	0.	0.	370.	0.	0.	2.46
F420H4.012	.5	.0	29.9	.0	.08	150.0	-100.0	1.0	1.3	0.	0.	369.	0.	0.	2.84
F420H5.005	.1	.0	.0	.0	-.01	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.13
F420H5.006	.1	.0	.0	.0	-.01	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.19
F420H5.007	.1	.0	.0	.0	.00	150.0	25.0	1.0	.2	0.	0.	0.	0.	0.	.26
F420H5.008	.2	.0	.0	.0	.02	150.0	.0	1.0	.5	0.	0.	0.	0.	0.	.81
F420H5.009	.5	.0	17.9	.0	.06	150.0	-25.0	1.0	1.4	0.	0.	221.	0.	0.	2.03
F420H5.010	.5	.0	25.2	.0	.12	150.0	-56.0	1.0	1.4	0.	0.	311.	0.	0.	3.99
F420H5.011	.6	.0	27.1	.0	.14	150.0	-75.0	1.0	1.6	0.	0.	334.	0.	0.	4.77
F420H5.012	.5	.0	23.3	.0	.10	150.0	-100.0	1.0	1.3	0.	0.	287.	0.	0.	3.41
F420I1.005	.1	.0	.0	.0	.02	150.0	75.0	5.0	.4	0.	0.	0.	0.	0.	.57
F420I1.006	.1	.0	.0	.0	-.01	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.17
F420I1.007	.1	.0	.0	.0	-.01	150.0	25.0	5.0	.4	0.	0.	0.	0.	0.	.14
F420I1.008	.2	.0	7.9	.0	.00	150.0	.0	5.0	.7	0.	0.	97.	0.	0.	.61

FALCON 4: LSR = 200, GAS = ARGON

MODEL CONDITIONS									PROTOTYPE CONDITIONS						
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F420I1.009	.6	.0	28.4	.0	.05	150.0	-25.0	5.0	1.5	0.	0.	350.	0.	0.	1.79
F420I1.010	.5	.0	29.0	.0	.08	150.0	-56.0	5.0	1.4	0.	0.	357.	0.	0.	2.73
F420I1.011	.5	.0	21.7	.0	.08	150.0	-75.0	5.0	1.4	0.	0.	267.	0.	0.	2.73
F420I1.012	.4	.0	27.9	.0	.03	150.0	-100.0	5.0	1.0	0.	0.	344.	0.	0.	1.21
F420I2.005	.1	.0	.0	.0	.01	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.46
F420I2.006	.1	.0	.0	.0	.00	150.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.36
F420I2.007	.1	.0	.0	.0	-.04	150.0	25.0	5.0	.2	0.	0.	0.	0.	0.	.01
F420I2.008	.3	.0	24.8	.0	.00	150.0	.0	5.0	.8	0.	0.	305.	0.	0.	.59
F420I2.009	.6	.0	22.8	.0	.03	150.0	-25.0	5.0	1.5	0.	0.	281.	0.	0.	1.31
F420I2.010	.5	.0	31.2	.0	.07	150.0	-56.0	5.0	1.3	0.	0.	385.	0.	0.	2.54
F420I2.011	.5	.0	26.0	.0	.04	150.0	-75.0	5.0	1.3	0.	0.	320.	0.	0.	1.64
F420I2.012	.4	.0	28.3	.0	-.01	150.0	-100.0	5.0	1.0	0.	0.	348.	0.	0.	.62
F420I3.005	.1	.0	.0	.0	.01	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.38
F420I3.006	.1	.0	.0	.0	.00	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.20
F420I3.007	.2	.0	.0	.0	.01	150.0	25.0	5.0	.4	0.	0.	0.	0.	0.	.56
F420I3.008	.4	.0	28.5	.0	.02	150.0	.0	5.0	1.1	0.	0.	351.	0.	0.	1.11
F420I3.009	.4	.0	25.1	.0	.04	150.0	-25.0	5.0	1.1	0.	0.	309.	0.	0.	1.60
F420I3.010	.4	.0	33.1	.0	.07	150.0	-56.0	5.0	1.1	0.	0.	408.	0.	0.	2.39
F420I3.011	.5	.0	29.9	.0	.07	150.0	-75.0	5.0	1.4	0.	0.	368.	0.	0.	2.27
F420I3.012	.4	.0	25.8	.0	.04	150.0	-100.0	5.0	1.0	0.	0.	318.	0.	0.	1.42
F420I4.005	.1	.0	.0	.0	-.01	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.34
F420I4.006	.1	.0	.0	.0	-.01	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.16
F420I4.007	.1	.0	.0	.0	.00	150.0	25.0	5.0	.4	0.	0.	0.	0.	0.	.34
F420I4.008	.4	.0	27.5	.0	.03	150.0	.0	5.0	1.1	0.	0.	339.	0.	0.	1.20
F420I4.009	.5	.0	24.5	.0	.06	150.0	-25.0	5.0	1.4	0.	0.	302.	0.	0.	2.13
F420I4.010	.4	.0	18.9	.0	.06	150.0	-56.0	5.0	1.0	0.	0.	233.	0.	0.	2.30
F420I4.011	.5	.0	18.2	.0	.05	150.0	-75.0	5.0	1.2	0.	0.	224.	0.	0.	1.82
F420I4.012	.3	.0	31.3	.0	.01	150.0	-100.0	5.0	.8	0.	0.	386.	0.	0.	.84
F420I5.005	.1	.0	.0	.0	.01	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.45
F420I5.006	.1	.0	.0	.0	.01	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.40
F420I5.007	.2	.0	.0	.0	-.01	150.0	25.0	5.0	.4	0.	0.	0.	0.	0.	.23
F420I5.008	.4	.0	10.8	.0	.00	150.0	.0	5.0	1.0	0.	0.	133.	0.	0.	.59
F420I5.009	.6	.0	15.6	.0	.09	150.0	-25.0	5.0	1.5	0.	0.	192.	0.	0.	2.94
F420I5.010	.6	.0	24.5	.0	.09	150.0	-56.0	5.0	1.7	0.	0.	302.	0.	0.	3.09
F420I5.011	.7	.0	22.4	.0	.12	150.0	-75.0	5.0	1.8	0.	0.	276.	0.	0.	3.89
F420I5.012	.4	.0	25.8	.0	.06	150.0	-100.0	5.0	1.1	0.	0.	319.	0.	0.	2.06
F420J1.005	.1	.0	.0	.0	-.01	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.10
F420J1.006	.1	.0	.0	.0	.00	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.12
F420J1.007	.1	.0	.0	.0	-.02	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.05
F420J1.008	.2	.0	2.1	.0	-.01	150.0	.0	11.0	.6	0.	0.	26.	0.	0.	.37
F420J1.009	.6	.0	29.3	.0	.03	150.0	-25.0	11.0	1.7	0.	0.	361.	0.	0.	1.35
F420J1.010	.5	.0	26.5	.0	.07	150.0	-56.0	11.0	1.3	0.	0.	326.	0.	0.	2.30

FALCON 4: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F420J1.011	.7	.0	26.9	.0	.06	150.0	-75.0	11.0	1.8	0.	0.	331.	0.	0.	2.19
F420J1.012	.4	.0	22.1	.0	.03	150.0	-100.0	11.0	1.1	0.	0.	272.	0.	0.	1.16
F420J2.005	.1	.0	.0	.0	-.01	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	:04
F420J2.006	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.11
F420J2.007	.1	.0	.0	.0	-.02	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.14
F420J2.008	.8	.0	26.8	.0	-.02	150.0	.0	11.0	2.2	0.	0.	330.	0.	0.	.37
F420J2.009	.7	.0	25.5	.0	.02	150.0	-25.0	11.0	1.8	0.	0.	314.	0.	0.	.96
F420J2.010	.4	.0	26.3	.0	.05	150.0	-56.0	11.0	1.2	0.	0.	324.	0.	0.	1.89
F420J2.011	.5	.0	24.5	.0	.02	150.0	-75.0	11.0	1.5	0.	0.	302.	0.	0.	1.21
F420J2.012	.4	.0	23.3	.0	.02	150.0	-100.0	11.0	1.1	0.	0.	287.	0.	0.	1.18
F420J3.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.24
F420J3.006	.1	.0	.0	.0	.00	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.29
F420J3.007	.1	.0	.0	.0	.00	150.0	25.0	11.0	.3	0.	0.	0.	0.	0.	.40
F420J3.008	.5	.0	22.5	.0	.00	150.0	.0	11.0	1.4	0.	0.	277.	0.	0.	.65
F420J3.009	.6	.0	26.3	.0	.05	150.0	-25.0	11.0	1.5	0.	0.	324.	0.	0.	1.85
F420J3.010	.4	.0	3.1	.0	.06	150.0	-56.0	11.0	1.2	0.	0.	39.	0.	0.	2.11
F420J3.011	.5	.0	27.1	.0	.04	150.0	-75.0	11.0	1.4	0.	0.	334.	0.	0.	1.64
F420J3.012	.4	.0	25.8	.0	.04	150.0	-100.0	11.0	1.1	0.	0.	318.	0.	0.	1.45
F420J4.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.13
F420J4.006	.1	.0	.0	.0	-.02	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.10
F420J4.007	.1	.0	.0	.0	-.02	150.0	25.0	11.0	.3	0.	0.	0.	0.	0.	.11
F420J4.008	.2	.0	10.6	.0	-.01	150.0	.0	11.0	.6	0.	0.	130.	0.	0.	.37
F420J4.009	.5	.0	20.8	.0	.02	150.0	-25.0	11.0	1.4	0.	0.	256.	0.	0.	.98
F420J4.010	.5	.0	12.8	.0	.05	150.0	-56.0	11.0	1.2	0.	0.	158.	0.	0.	1.86
F420J4.011	.6	.0	17.3	.0	.04	150.0	-75.0	11.0	1.5	0.	0.	214.	0.	0.	1.63
F420J4.012	.4	.0	14.5	.0	.02	150.0	-100.0	11.0	1.0	0.	0.	179.	0.	0.	.89
F420J5.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.19
F420J5.006	.1	.0	.0	.0	.00	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.33
F420J5.007	.1	.0	.0	.0	.00	150.0	25.0	11.0	.2	0.	0.	0.	0.	0.	.28
F420J5.008	.4	.0	24.2	.0	-.01	150.0	.0	11.0	1.0	0.	0.	298.	0.	0.	.41
F420J5.009	.8	.0	24.8	.0	.05	150.0	-25.0	11.0	2.1	0.	0.	306.	0.	0.	1.81
F420J5.010	.4	.0	4.6	.0	.09	150.0	-56.0	11.0	1.2	0.	0.	57.	0.	0.	2.93
F420J5.011	.5	.0	18.3	.0	.04	150.0	-75.0	11.0	1.4	0.	0.	225.	0.	0.	1.70
F420J5.012	.3	.0	14.4	.0	.00	150.0	-100.0	11.0	.9	0.	0.	178.	0.	0.	.73
F420K1.005	.1	.0	.0	.0	-.02	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.07
F420K1.006	.1	.0	.0	.0	-.02	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.11
F420K1.007	.1	.0	.0	.0	.00	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.27
F420K1.008	.5	.0	9.4	.0	-.03	150.0	.0	17.0	1.2	0.	0.	116.	0.	0.	.23
F420K1.009	.6	.0	21.2	.0	.01	150.0	-25.0	17.0	1.7	0.	0.	261.	0.	0.	.84
F420K1.010	.6	.0	23.0	.0	.04	150.0	-56.0	17.0	1.5	0.	0.	284.	0.	0.	1.61
F420K1.011	.6	.0	23.0	.0	.03	150.0	-75.0	17.0	1.6	0.	0.	284.	0.	0.	1.18
F420K1.012	.3	.0	21.9	.0	.00	150.0	-100.0	17.0	.8	0.	0.	270.	0.	0.	.46

FALCON 4: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F420K2.005	.1	.0	.0	.0	.01	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.45
F420K2.006	.1	.0	.0	.0	.01	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.50
F420K2.007	.1	.0	.0	.0	.00	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.20
F420K2.008	.6	.0	18.5	.0	.00	150.0	.0	17.0	1.5	0.	0.	229.	0.	0.	.56
F420K2.009	.6	.0	21.8	.0	.05	150.0	-25.0	17.0	1.6	0.	0.	269.	0.	0.	1.63
F420K2.010	.5	.0	26.5	.0	.06	150.0	-56.0	17.0	1.3	0.	0.	326.	0.	0.	2.21
F420K2.011	.6	.0	23.7	.0	.07	150.0	-75.0	17.0	1.5	0.	0.	292.	0.	0.	2.38
F420K2.012	.4	.0	20.3	.0	.04	150.0	-100.0	17.0	1.1	0.	0.	250.	0.	0.	1.22
F420K3.005	.1	.0	.0	.0	.00	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.27
F420K3.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.22
F420K3.007	.1	.0	.0	.0	.00	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.30
F420K3.008	.5	.0	24.7	.0	.00	150.0	.0	17.0	1.3	0.	0.	304.	0.	0.	.58
F420K3.009	.4	.0	28.5	.0	.02	150.0	-25.0	17.0	1.1	0.	0.	351.	0.	0.	.93
F420K3.010	.5	.0	26.1	.0	.04	150.0	-56.0	17.0	1.3	0.	0.	321.	0.	0.	1.48
F420K3.011	.5	.0	29.0	.0	.03	150.0	-75.0	17.0	1.2	0.	0.	358.	0.	0.	1.33
F420K3.012	.3	.0	17.8	.0	.01	150.0	-100.0	17.0	.8	0.	0.	220.	0.	0.	.55
F420K4.005	.1	.0	.0	.0	-.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.08
F420K4.006	.1	.0	.0	.0	-.02	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.02
F420K4.007	.1	.0	.0	.0	-.01	150.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.14
F420K4.008	.6	.0	10.2	.0	.00	150.0	.0	17.0	1.5	0.	0.	126.	0.	0.	.64
F420K4.009	.5	.0	4.4	.0	.02	150.0	-25.0	17.0	1.3	0.	0.	54.	0.	0.	.98
F420K4.010	.5	.0	19.8	.0	.04	150.0	-56.0	17.0	1.3	0.	0.	244.	0.	0.	1.49
F420K4.011	.5	.0	19.5	.0	.04	150.0	-75.0	17.0	1.4	0.	0.	240.	0.	0.	1.66
F420K4.012	.4	.0	29.1	.0	.00	150.0	-100.0	17.0	.9	0.	0.	359.	0.	0.	.50
F420K5.005	.1	.0	.0	.0	.00	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.27
F420K5.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.10
F420K5.007	.1	.0	.0	.0	.00	150.0	25.0	17.0	.4	0.	0.	0.	0.	0.	.32
F420K5.008	.8	.0	26.0	.0	.00	150.0	.0	17.0	2.1	0.	0.	320.	0.	0.	.63
F420K5.009	.6	.0	4.9	.0	.04	150.0	-25.0	17.0	1.5	0.	0.	61.	0.	0.	1.37
F420K5.010	.5	.0	28.4	.0	.05	150.0	-56.0	17.0	1.3	0.	0.	350.	0.	0.	1.78
F420K5.011	.5	.0	29.1	.0	.04	150.0	-75.0	17.0	1.3	0.	0.	359.	0.	0.	1.59
F420K5.012	.5	.0	26.3	.0	.01	150.0	-100.0	17.0	1.3	0.	0.	324.	0.	0.	.78

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510A1.004	1.3	13.5	13.5	13.6	.02	-62.0	40.0	2.0	3.5	0.	0.	118.	0.	0.	.62
N510A1.005	2.8	10.1	15.5	41.4	.17	-62.0	30.0	2.0	7.2	105.	0.	135.	0.	137.	3.92
N510A1.006	27.4	2.2	9.8	84.6	8.33	-62.0	20.0	2.0	50.5	19.	20.	86.	588.	665.	157.77
N510A1.007	24.0	3.1	9.7	87.4	8.01	-62.0	10.0	2.0	46.0	27.	28.	84.	600.	696.	153.51
N510A1.008	22.7	2.2	11.3	84.1	8.02	-62.0	.0	2.0	44.2	20.	24.	98.	569.	732.	153.04
N510A1.009	22.0	2.1	14.5	83.1	7.11	-62.0	-10.0	2.0	43.2	18.	43.	126.	558.	723.	138.56
N510A1.010	28.4	1.4	9.1	84.7	8.20	-62.0	-20.0	2.0	51.8	13.	14.	79.	548.	646.	155.38
N510A2.004	.7	.0	17.6	.0	.06	-62.0	40.0	2.0	2.0	0.	0.	153.	0.	0.	1.40
N510A2.005	2.3	10.7	10.7	51.7	.19	-62.0	30.0	2.0	6.0	93.	0.	93.	0.	301.	4.38
N510A2.006	29.9	2.1	10.8	88.2	9.59	-62.0	20.0	2.0	53.6	18.	33.	94.	587.	683.	175.54
N510A2.007	26.3	2.8	12.0	90.8	9.63	-62.0	10.0	2.0	49.1	25.	25.	105.	642.	759.	178.80
N510A2.008	26.8	2.6	13.9	86.9	9.00	-62.0	.0	2.0	49.7	27.	39.	121.	611.	714.	166.68
N510A2.009	24.0	2.1	14.1	90.2	8.78	-62.0	-10.0	2.0	46.1	18.	39.	123.	636.	775.	164.86
N510A2.010	27.7	1.2	10.5	80.7	9.04	-62.0	-20.0	2.0	50.9	11.	13.	92.	564.	698.	168.32
N510A3.004	.9	.0	10.4	.0	.01	-62.0	40.0	2.0	2.5	0.	0.	90.	0.	0.	.43
N510A3.005	1.9	13.8	18.1	25.9	.09	-62.0	30.0	2.0	4.9	0.	0.	158.	0.	0.	2.42
N510A3.006	25.8	2.0	14.1	90.2	9.63	-62.0	20.0	2.0	48.5	18.	37.	123.	676.	679.	177.91
N510A3.007	25.3	1.9	13.8	87.3	9.07	-62.0	10.0	2.0	47.7	17.	31.	120.	604.	720.	170.22
N510A3.008	27.9	1.6	10.9	85.1	9.10	-62.0	.0	2.0	51.1	14.	36.	95.	598.	665.	169.12
N510A3.009	25.6	1.7	12.2	89.4	8.30	-62.0	-10.0	2.0	48.3	15.	19.	107.	650.	715.	157.19
N510A3.010	31.3	1.2	10.6	87.2	9.44	-62.0	-20.0	2.0	55.2	10.	10.	93.	671.	751.	175.92
N510A4.004	.3	.0	8.9	.0	.02	-62.0	40.0	2.0	.8	0.	0.	77.	0.	0.	.70
N510A4.005	2.3	10.3	16.3	16.8	.07	-62.0	30.0	2.0	6.1	142.	0.	142.	0.	142.	1.78
N510A4.006	27.2	2.3	8.5	91.1	9.63	-62.0	20.0	2.0	50.2	21.	25.	74.	659.	773.	179.08
N510A4.007	26.7	2.9	10.8	91.1	9.21	-62.0	10.0	2.0	49.7	25.	30.	94.	639.	785.	173.05
N510A4.008	26.1	2.9	11.2	85.9	9.38	-62.0	.0	2.0	48.8	25.	26.	98.	589.	683.	174.59
N510A4.009	26.4	1.6	12.6	91.3	8.01	-62.0	-10.0	2.0	49.2	14.	26.	110.	597.	675.	152.77
N510A4.010	27.6	1.2	10.2	88.1	9.82	-62.0	-20.0	2.0	50.8	11.	12.	89.	631.	722.	183.98
N510A5.004	1.1	20.6	20.6	20.7	.04	-62.0	40.0	2.0	2.8	0.	0.	180.	0.	0.	.96
N510A5.005	1.8	8.4	14.6	62.0	.12	-62.0	30.0	2.0	4.7	0.	0.	127.	0.	0.	2.91
N510A5.006	25.7	2.1	13.0	90.1	10.38	-62.0	20.0	2.0	48.3	18.	18.	113.	682.	754.	191.22
N510A5.007	25.4	2.7	11.7	90.7	9.89	-62.0	10.0	2.0	48.0	24.	24.	102.	641.	743.	184.00
N510A5.008	26.9	2.2	12.5	88.2	10.11	-62.0	.0	2.0	49.9	19.	24.	109.	638.	736.	186.38
N510A5.009	26.9	2.2	12.8	85.9	8.75	-62.0	-10.0	2.0	49.9	20.	26.	111.	638.	728.	164.77
N510A5.010	31.8	1.4	10.8	85.8	10.40	-62.0	-20.0	2.0	55.8	12.	13.	94.	704.	743.	192.92
N510B1.004	.7	.0	17.6	.0	.09	-32.0	40.0	1.0	1.9	0.	0.	153.	0.	0.	2.30
N510B1.005	2.3	12.3	16.3	37.4	.13	-32.0	30.0	1.0	6.0	142.	0.	142.	0.	142.	3.32
N510B1.006	33.2	.8	11.1	90.2	9.16	-32.0	20.0	1.0	57.3	7.	8.	97.	545.	696.	163.72
N510B1.007	51.1	.5	8.7	88.4	10.60	-32.0	10.0	1.0	73.9	4.	5.	76.	533.	686.	173.82
N510B1.008	31.3	.9	11.4	77.5	9.21	-32.0	.0	1.0	55.1	9.	11.	99.	586.	659.	166.98
N510B1.009	61.2	.8	10.2	90.6	12.36	-32.0	-10.0	1.0	81.0	7.	11.	89.	720.	789.	204.85
N510B1.010	49.2	1.4	10.0	77.7	10.40	-32.0	-20.0	1.0	72.4	12.	13.	87.	639.	677.	177.47

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510B2.004	.8	.0	16.1	.0	.06	-32.0	40.0	1.0	2.0	0.	0.	140.	0.	0.	1.40
N510B2.005	1.7	12.9	49.4	49.9	.16	-32.0	30.0	1.0	4.4	0.	0.	431.	0.	0.	3.85
N510B2.006	33.7	.9	9.2	91.7	10.23	-32.0	20.0	1.0	57.8	8.	10.	80.	588.	645.	180.37
N510B2.007	54.1	.5	10.2	75.3	11.24	-32.0	10.0	1.0	76.1	4.	5.	89.	570.	594.	184.13
N510B2.008	32.7	.7	13.8	86.4	10.20	-32.0	.0	1.0	56.8	6.	11.	120.	634.	677.	181.98
N510B2.009	57.3	.8	10.3	91.2	13.08	-32.0	-10.0	1.0	78.4	8.	8.	90.	624.	781.	220.02
N510B2.010	50.2	1.4	9.9	82.9	10.97	-32.0	-20.0	1.0	73.2	13.	15.	86.	581.	628.	186.62
N510B3.004	.8	.0	17.0	.0	.05	-32.0	40.0	1.0	2.1	0.	0.	148.	0.	0.	1.18
N510B3.005	1.0	.0	13.3	.0	.10	-32.0	30.0	1.0	2.6	0.	0.	116.	0.	0.	2.65
N510B3.006	33.4	.7	9.9	86.4	11.04	-32.0	20.0	1.0	57.6	6.	10.	86.	582.	726.	197.85
N510B3.007	53.5	.4	10.4	88.3	12.25	-32.0	10.0	1.0	75.6	4.	4.	91.	672.	673.	202.61
N510B3.008	32.6	.9	11.6	91.4	10.78	-32.0	.0	1.0	56.7	8.	11.	101.	630.	796.	191.66
N510B3.009	59.5	.7	9.9	83.5	12.66	-32.0	-10.0	1.0	79.9	6.	7.	86.	583.	674.	212.33
N510B3.010	48.2	1.8	10.4	88.4	11.19	-32.0	-20.0	1.0	71.6	16.	16.	91.	600.	648.	193.54
N510B4.004	.2	.0	19.6	.0	.00	-32.0	40.0	1.0	.6	0.	0.	171.	0.	0.	.37
N510B4.005	1.1	15.0	15.0	15.6	.16	-32.0	30.0	1.0	2.9	0.	0.	131.	0.	0.	3.66
N510B4.006	33.7	.7	10.3	84.5	9.75	-32.0	20.0	1.0	57.9	6.	7.	90.	541.	583.	173.24
N510B4.007	55.3	.5	10.5	85.4	10.72	-32.0	10.0	1.0	76.9	4.	5.	92.	549.	652.	177.15
N510B4.008	32.9	.3	11.4	89.3	10.11	-32.0	.0	1.0	57.0	9.	10.	99.	512.	741.	180.48
N510B4.009	62.2	1.0	10.2	88.4	12.43	-32.0	-10.0	1.0	81.6	9.	12.	89.	558.	793.	207.90
N510B4.010	52.2	1.6	9.8	87.1	10.50	-32.0	-20.0	1.0	74.7	15.	15.	85.	541.	666.	180.90
N510B5.004	.5	.0	18.2	.0	.01	-32.0	40.0	1.0	1.3	0.	0.	158.	0.	0.	.60
N510B5.005	1.3	13.8	15.7	18.2	.14	-32.0	30.0	1.0	3.4	0.	0.	137.	0.	0.	3.32
N510B5.006	35.2	1.0	10.9	85.1	8.90	-32.0	20.0	1.0	59.4	9.	16.	95.	564.	608.	160.02
N510B5.007	52.4	.4	10.0	80.1	9.96	-32.0	10.0	1.0	74.9	4.	5.	87.	565.	636.	164.12
N510B5.008	32.9	.7	10.6	76.8	8.09	-32.0	.0	1.0	57.0	6.	7.	92.	418.	668.	146.36
N510B5.009	56.8	.9	9.1	90.1	11.82	-32.0	-10.0	1.0	78.0	10.	12.	79.	610.	749.	200.54
N510B5.010	50.3	1.6	9.6	86.7	9.26	-32.0	-20.0	1.0	73.2	15.	15.	84.	464.	618.	158.96
N510C1.004	.3	.0	29.9	.0	.00	-2.0	40.0	1.0	.9	0.	0.	261.	0.	0.	.53
N510C1.005	.6	.0	12.6	.0	.08	-2.0	30.0	1.0	1.5	0.	0.	110.	0.	0.	2.01
N510C1.006	19.4	1.7	21.4	61.6	3.97	-2.0	20.0	1.0	39.4	15.	30.	187.	340.	399.	79.56
N510C1.007	18.9	.9	17.7	76.6	3.00	-2.0	10.0	1.0	38.7	12.	14.	154.	308.	501.	61.05
N510C1.008	23.6	1.5	15.0	52.7	3.32	-2.0	.0	1.0	45.5	14.	28.	131.	309.	326.	65.31
N510C1.009	23.2	2.1	19.7	59.9	5.23	-2.0	-10.0	1.0	44.9	19.	35.	172.	409.	461.	99.37
N510C1.010	19.8	3.8	13.1	75.8	6.24	-2.0	-20.0	1.0	40.0	34.	42.	114.	539.	553.	120.81
N510C2.004	1.2	16.1	17.0	18.8	.14	-2.0	40.0	1.0	3.2	0.	0.	148.	0.	0.	3.26
N510C2.005	5.3	9.8	9.9	18.2	.13	-2.0	30.0	1.0	13.2	85.	85.	86.	86.	87.	3.22
N510C2.006	17.1	1.9	18.7	55.7	2.82	-2.0	20.0	1.0	35.8	20.	27.	163.	303.	329.	57.87
N510C2.007	14.1	2.4	10.8	55.0	1.64	-2.0	10.0	1.0	30.8	21.	21.	94.	283.	333.	34.77
N510C2.008	22.2	2.6	12.1	54.0	2.02	-2.0	.0	1.0	43.5	23.	29.	105.	287.	288.	41.05
N510C2.009	25.2	2.4	15.4	54.3	3.91	-2.0	-10.0	1.0	47.6	21.	34.	134.	329.	331.	74.25
N510C2.010	22.7	3.9	16.2	65.6	4.82	-2.0	-20.0	1.0	44.3	39.	42.	141.	354.	471.	94.10

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510C3.004	.6	.0	35.2	.0	.08	-2.0	40.0	1.0	1.7	0.	0.	307.	0.	0.	2.05
N510C3.005	4.3	11.9	12.2	33.4	.13	-2.0	30.0	1.0	10.7	104.	106.	106.	107.	107.	3.21
N510C3.006	22.3	2.6	16.7	61.8	4.21	-2.0	20.0	1.0	43.6	24.	26.	146.	397.	400.	83.34
N510C3.007	24.0	2.9	15.9	61.3	2.76	-2.0	10.0	1.0	46.1	25.	27.	139.	274.	277.	55.11
N510C3.008	27.2	2.1	16.0	53.6	3.00	-2.0	.0	1.0	50.3	19.	30.	139.	275.	277.	57.40
N510C3.009	24.3	2.3	13.6	57.0	4.85	-2.0	-10.0	1.0	46.5	40.	42.	118.	388.	389.	91.19
N510C3.010	23.8	5.0	17.3	70.3	6.07	-2.0	-20.0	1.0	45.8	44.	45.	151.	423.	596.	117.91
N510C4.004	.2	.0	.0	.0	.02	-2.0	40.0	1.0	.5	0.	0.	0.	0.	0.	.70
N510C4.005	.5	.0	22.3	.0	.07	-2.0	30.0	1.0	1.4	0.	0.	194.	0.	0.	1.73
N510C4.006	19.6	1.9	15.8	68.4	3.66	-2.0	20.0	1.0	39.7	18.	19.	138.	376.	592.	73.59
N510C4.007	21.1	1.6	15.2	67.3	2.27	-2.0	10.0	1.0	42.0	14.	19.	133.	367.	368.	46.20
N510C4.008	28.0	2.3	14.9	56.7	2.34	-2.0	.0	1.0	51.2	21.	24.	130.	148.	269.	45.33
N510C4.009	24.9	2.9	15.1	66.1	3.69	-2.0	-10.0	1.0	47.2	26.	30.	132.	302.	401.	70.73
N510C4.010	23.9	4.6	15.3	69.6	5.47	-2.0	-20.0	1.0	46.0	41.	53.	133.	411.	525.	106.43
N510C5.004	.8	.0	17.4	.0	.11	-2.0	40.0	1.0	2.2	0.	0.	152.	0.	0.	2.60
N510C5.005	1.0	.0	15.3	.0	.11	-2.0	30.0	1.0	2.6	0.	0.	133.	0.	0.	2.75
N510C5.006	21.3	1.7	16.1	46.7	4.41	-2.0	20.0	1.0	42.3	15.	15.	140.	352.	355.	85.63
N510C5.007	27.2	2.3	15.6	49.1	3.46	-2.0	10.0	1.0	50.3	21.	30.	136.	274.	319.	66.06
N510C5.008	28.1	2.5	14.4	58.5	4.71	-2.0	.0	1.0	51.4	27.	27.	125.	273.	318.	85.36
N510C5.009	29.6	3.1	14.6	58.9	5.97	-2.0	-10.0	1.0	53.2	27.	27.	127.	512.	513.	107.04
N510C5.010	26.7	4.7	20.5	66.9	6.48	-2.0	-20.0	1.0	49.6	42.	42.	179.	459.	557.	121.50
N510D1.004	.1	.0	.0	.0	.03	50.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.77
N510D1.005	.1	.0	.0	.0	-.03	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.04
N510D1.006	.4	.0	20.5	.0	.05	50.0	56.0	1.0	1.2	0.	0.	178.	0.	0.	1.26
N510D1.007	.9	.0	12.5	.0	.15	50.0	44.0	1.0	2.3	0.	0.	109.	0.	0.	3.46
N510D1.008	1.4	7.4	13.4	13.5	.17	50.0	33.0	1.0	3.7	0.	0.	117.	0.	0.	3.95
N510D1.009	1.8	6.3	12.7	17.0	.36	50.0	22.0	1.0	4.8	0.	0.	111.	0.	0.	8.40
N510D1.010	1.9	7.5	8.6	25.3	.52	50.0	.0	1.0	5.0	0.	0.	75.	0.	0.	12.22
N510D2.004	.1	.0	.0	.0	.02	50.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.61
N510D2.005	.1	.0	.0	.0	-.02	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.14
N510D2.006	.2	.0	28.6	.0	.04	50.0	56.0	1.0	.7	0.	0.	250.	0.	0.	1.00
N510D2.007	1.0	.0	10.7	.0	.07	50.0	44.0	1.0	2.6	0.	0.	93.	0.	0.	2.01
N510D2.008	2.5	10.0	12.6	14.3	.21	50.0	33.0	1.0	6.5	88.	0.	110.	0.	112.	4.86
N510D2.009	2.6	6.1	11.5	24.9	.37	50.0	22.0	1.0	6.8	93.	0.	100.	0.	130.	8.57
N510D2.010	2.1	6.9	13.4	15.5	.46	50.0	.0	1.0	5.4	115.	0.	117.	0.	117.	10.79
N510D3.004	.1	.0	.0	.0	.02	50.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.82
N510D3.005	.0	.0	.0	.0	-.03	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.09
N510D3.006	.2	.0	.0	.0	.02	50.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.65
N510D3.007	.8	.0	14.6	.0	.07	50.0	44.0	1.0	2.0	0.	0.	127.	0.	0.	1.90
N510D3.008	1.7	10.0	13.5	14.3	.16	50.0	33.0	1.0	4.4	0.	0.	118.	0.	0.	3.73
N510D3.009	2.0	6.7	13.9	27.2	.29	50.0	22.0	1.0	5.2	104.	0.	121.	0.	121.	6.88
N510D3.010	2.5	9.6	14.3	16.5	.46	50.0	.0	1.0	6.4	120.	0.	124.	0.	135.	10.79

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510D4.004	.1	.0	.0	.0	.02	50.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.69
N510D4.005	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.30
N510D4.006	.1	.0	.0	.0	.02	50.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.64
N510D4.007	.7	.0	23.6	.0	.06	50.0	44.0	1.0	1.9	0.	0.	206.	0.	0.	1.71
N510D4.008	1.8	11.1	13.6	21.9	.16	50.0	33.0	1.0	4.8	0.	0.	118.	0.	0.	3.86
N510D4.009	2.2	5.5	11.4	21.6	.26	50.0	22.0	1.0	5.6	76.	0.	100.	0.	118.	6.25
N510D4.010	2.1	7.5	12.3	17.9	.46	50.0	.0	1.0	5.5	107.	0.	107.	0.	109.	10.71
N510D5.004	.1	.0	.0	.0	.01	50.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.53
N510D5.005	.1	.0	.0	.0	.03	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.84
N510D5.006	.1	.0	.0	.0	.02	50.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.54
N510D5.007	.5	.0	19.8	.0	.11	50.0	44.0	1.0	1.4	0.	0.	172.	0.	0.	2.59
N510D5.008	1.1	13.6	13.6	13.7	.08	50.0	33.0	1.0	3.0	0.	0.	119.	0.	0.	1.95
N510D5.009	2.2	10.2	11.8	21.2	.20	50.0	22.0	1.0	5.8	103.	0.	103.	0.	107.	4.70
N510D5.010	1.9	8.4	15.0	22.0	.46	50.0	.0	1.0	4.9	0.	0.	131.	0.	0.	10.83
N510E1.004	.1	.0	.0	.0	-.02	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.09
N510E1.005	.2	.0	.0	.0	.01	50.0	66.0	5.0	.5	0.	0.	0.	0.	0.	.43
N510E1.006	.5	.0	19.3	.0	.04	50.0	56.0	5.0	1.3	0.	0.	168.	0.	0.	.99
N510E1.007	.8	.0	13.1	.0	.03	50.0	44.0	5.0	2.1	0.	0.	114.	0.	0.	1.10
N510E1.008	1.7	7.9	13.8	14.6	.14	50.0	33.0	5.0	4.4	0.	0.	120.	0.	0.	3.27
N510E1.009	2.4	7.3	13.7	24.6	.33	50.0	22.0	5.0	6.2	93.	0.	120.	0.	121.	7.83
N510E1.010	2.1	9.1	13.1	21.6	.43	50.0	.0	5.0	5.6	110.	0.	114.	0.	115.	10.09
N510E2.004	.1	.0	.0	.0	-.02	50.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.09
N510E2.005	.1	.0	.0	.0	.02	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.48
N510E2.006	.3	.0	26.6	.0	.00	50.0	56.0	5.0	.8	0.	0.	232.	0.	0.	.26
N510E2.007	.4	.0	13.7	.0	.04	50.0	44.0	5.0	1.0	0.	0.	119.	0.	0.	1.11
N510E2.008	1.5	9.7	9.7	9.9	.09	50.0	33.0	5.0	4.0	0.	0.	85.	0.	0.	2.27
N510E2.009	1.8	5.7	13.9	14.5	.31	50.0	22.0	5.0	4.6	0.	0.	121.	0.	0.	7.30
N510E2.010	2.1	7.4	11.9	24.6	.45	50.0	.0	5.0	5.4	103.	0.	103.	0.	104.	10.60
N510E3.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.40
N510E3.005	.1	.0	.0	.0	.01	50.0	66.0	5.0	.4	0.	0.	0.	0.	0.	.44
N510E3.006	.3	.0	34.0	.0	.02	50.0	56.0	5.0	.8	0.	0.	296.	0.	0.	.52
N510E3.007	.6	.0	25.3	.0	.04	50.0	44.0	5.0	1.5	0.	0.	220.	0.	0.	.92
N510E3.008	2.0	8.0	11.0	13.5	.11	50.0	33.0	5.0	5.2	96.	0.	96.	0.	96.	2.78
N510E3.009	2.4	4.3	6.6	40.6	.33	50.0	22.0	5.0	6.2	58.	0.	58.	0.	120.	7.86
N510E3.010	2.1	8.4	15.6	18.7	.45	50.0	.0	5.0	5.4	135.	0.	136.	0.	136.	10.52
N510E4.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.37
N510E4.005	.1	.0	.0	.0	.00	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.06
N510E4.006	.5	.0	42.6	.0	.05	50.0	56.0	5.0	1.2	0.	0.	371.	0.	0.	1.13
N510E4.007	.6	.0	23.4	.0	.08	50.0	44.0	5.0	1.6	0.	0.	204.	0.	0.	1.90
N510E4.008	1.2	8.0	14.0	14.4	.11	50.0	33.0	5.0	3.2	0.	0.	122.	0.	0.	2.74
N510E4.009	1.8	7.5	13.3	36.2	.37	50.0	22.0	5.0	4.8	0.	0.	116.	0.	0.	8.60
N510E4.010	1.7	7.5	12.8	25.9	.43	50.0	.0	5.0	4.5	0.	0.	112.	0.	0.	10.02

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS: PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PROTOTYPE CONDITIONS: PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510E5.004	.1	.0	.0	.0	.01	50.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.47
N510E5.005	.2	.0	.0	.0	.02	50.0	66.0	5.0	.4	0.	0.	0.	0.	0.	.50
N510E5.006	.3	.0	23.3	.0	.05	50.0	56.0	5.0	.7	0.	0.	203.	0.	0.	1.20
N510E5.007	.7	.0	13.6	.0	.02	50.0	44.0	5.0	1.9	0.	0.	118.	0.	0.	.86
N510E5.008	1.4	6.3	11.9	12.7	.06	50.0	33.0	5.0	3.6	0.	0.	104.	0.	0.	1.90
N510E5.009	1.9	6.9	12.1	15.1	.31	50.0	22.0	5.0	5.1	105.	0.	105.	0.	107.	7.40
N510E5.010	1.5	9.0	16.0	21.6	.41	50.0	.0	5.0	3.9	0.	0.	139.	0.	0.	9.54
N510F1.004	.1	.0	.0	.0	.00	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.20
N510F1.005	.1	.0	.0	.0	.02	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.67
N510F1.006	.1	.0	.0	.0	.00	50.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.34
N510F1.007	.2	.0	.0	.0	.02	50.0	44.0	11.0	.5	0.	0.	0.	0.	0.	.71
N510F1.008	.6	.0	55.2	.0	.04	50.0	33.0	11.0	1.5	0.	0.	481.	0.	0.	.91
N510F1.009	1.7	6.1	6.9	19.1	.15	50.0	22.0	11.0	4.3	0.	0.	60.	0.	0.	3.67
N510F1.010	1.8	8.9	14.3	14.7	.35	50.0	.0	11.0	4.8	0.	0.	124.	0.	0.	8.18
N510F2.004	.1	.0	.0	.0	-.01	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.12
N510F2.005	.0	.0	.0	.0	.01	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.38
N510F2.006	.1	.0	.0	.0	-.02	50.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.04
N510F2.007	.1	.0	.0	.0	-.04	50.0	44.0	11.0	.4	0.	0.	0.	0.	0.	.06
N510F2.008	.6	.0	35.0	.0	-.03	50.0	33.0	11.0	1.5	0.	0.	305.	0.	0.	.24
N510F2.009	2.2	4.5	8.0	12.5	.12	50.0	22.0	11.0	5.7	69.	0.	69.	0.	108.	3.36
N510F2.010	2.0	9.5	12.9	14.7	.32	50.0	.0	11.0	5.1	113.	0.	113.	0.	113.	7.53
N510F3.004	.1	.0	.0	.0	-.02	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.07
N510F3.005	.1	.0	.0	.0	-.02	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.12
N510F3.006	.1	.0	.0	.0	.01	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.39
N510F3.007	.1	.0	.0	.0	.00	50.0	44.0	11.0	.3	0.	0.	0.	0.	0.	.15
N510F3.008	.7	.0	35.3	.0	.04	50.0	33.0	11.0	1.9	0.	0.	308.	0.	0.	1.00
N510F3.009	1.4	5.2	9.3	22.5	.15	50.0	22.0	11.0	3.6	0.	0.	81.	0.	0.	3.62
N510F3.010	1.3	10.9	11.0	14.8	.20	50.0	.0	11.0	3.5	0.	0.	96.	0.	0.	5.28
N510F4.004	.1	.0	.0	.0	-.02	50.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.10
N510F4.005	.1	.0	.0	.0	-.01	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.15
N510F4.006	.1	.0	.0	.0	.01	50.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.44
N510F4.007	.5	.0	10.5	.0	.00	50.0	44.0	11.0	1.4	0.	0.	91.	0.	0.	.41
N510F4.008	.7	.0	37.2	.0	.01	50.0	33.0	11.0	1.9	0.	0.	325.	0.	0.	.63
N510F4.009	1.9	13.8	13.9	14.4	.12	50.0	22.0	11.0	4.8	0.	0.	121.	0.	0.	3.14
N510F4.010	1.1	11.2	15.8	15.8	.23	50.0	.0	11.0	3.0	0.	0.	137.	0.	0.	5.55
N510F5.004	.1	.0	.0	.0	-.02	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.06
N510F5.005	.1	.0	.0	.0	-.02	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.06
N510F5.006	.1	.0	.0	.0	-.01	50.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.10
N510F5.007	.2	.0	.0	.0	.01	50.0	44.0	11.0	.5	0.	0.	0.	0.	0.	.28
N510F5.008	.8	.0	28.7	.0	.03	50.0	33.0	11.0	2.0	0.	0.	251.	0.	0.	.79
N510F5.009	1.2	7.3	7.3	12.2	.14	50.0	22.0	11.0	3.1	0.	0.	64.	0.	0.	3.44
N510F5.010	1.1	10.7	13.0	14.6	.25	50.0	.0	11.0	3.0	0.	0.	114.	0.	0.	5.85

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510G1.004	.0	.0	.0	.0	-.04	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.02
N510G1.005	.0	.0	.0	.0	-.04	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.01
N510G1.006	.1	.0	.0	.0	-.03	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.05
N510G1.007	.1	.0	.0	.0	-.02	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.11
N510G1.008	.5	.0	43.6	.0	-.02	50.0	33.0	17.0	1.2	0.	0.	380.	0.	0.	.16
N510G1.009	1.7	12.4	12.4	38.7	.05	50.0	22.0	17.0	4.4	0.	0.	108.	0.	0.	1.87
N510G1.010	1.3	11.2	14.3	14.3	.10	50.0	.0	17.0	3.4	0.	0.	125.	0.	0.	2.90
N510G2.004	.1	.0	.0	.0	-.01	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.01
N510G2.005	.1	.0	.0	.0	.01	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.34
N510G2.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.05
N510G2.007	.1	.0	.0	.0	-.02	50.0	44.0	17.0	.2	0.	0.	0.	0.	0.	.12
N510G2.008	.5	.0	39.4	.0	.00	50.0	33.0	17.0	1.4	0.	0.	344.	0.	0.	.22
N510G2.009	1.0	.0	25.3	.0	.05	50.0	22.0	17.0	2.5	0.	0.	221.	0.	0.	1.72
N510G2.010	1.9	8.2	13.6	16.6	.13	50.0	.0	17.0	5.0	0.	0.	118.	0.	0.	3.24
N510G3.004	.1	.0	.0	.0	-.03	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.04
N510G3.005	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.17
N510G3.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.03
N510G3.007	.0	.0	.0	.0	.01	50.0	44.0	17.0	.1	0.	0.	0.	0.	0.	.45
N510G3.008	.6	.0	49.3	.0	.00	50.0	33.0	17.0	1.7	0.	0.	430.	0.	0.	.44
N510G3.009	1.0	.0	23.4	.0	.07	50.0	22.0	17.0	2.6	0.	0.	204.	0.	0.	1.89
N510G3.010	1.8	6.7	6.7	22.2	.13	50.0	.0	17.0	4.7	0.	0.	59.	0.	0.	3.32
N510G4.004	.1	.0	.0	.0	-.01	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.03
N510G4.005	.1	.0	.0	.0	.00	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.05
N510G4.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.17
N510G4.007	.1	.0	.0	.0	.00	50.0	44.0	17.0	.3	0.	0.	0.	0.	0.	.02
N510G4.008	.9	.0	38.3	.0	.00	50.0	33.0	17.0	2.3	0.	0.	334.	0.	0.	.15
N510G4.009	1.2	5.3	5.3	5.3	.03	50.0	22.0	17.0	3.2	0.	0.	46.	0.	0.	1.34
N510G4.010	1.2	9.6	12.3	12.3	.09	50.0	.0	17.0	3.1	0.	0.	107.	0.	0.	2.72
N510G5.004	.1	.0	.0	.0	.00	50.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.12
N510G5.005	.1	.0	.0	.0	.01	50.0	66.0	17.0	.2	0.	0.	0.	0.	0.	.38
N510G5.006	.1	.0	.0	.0	.00	50.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.39
N510G5.007	.1	.0	.0	.0	.01	50.0	44.0	17.0	.1	0.	0.	0.	0.	0.	.46
N510G5.008	.3	.0	70.9	.0	.00	50.0	33.0	17.0	.9	0.	0.	618.	0.	0.	.23
N510G5.009	1.2	20.2	20.3	20.3	.01	50.0	22.0	17.0	3.1	0.	0.	177.	0.	0.	1.10
N510G5.010	1.2	8.9	15.8	15.8	.11	50.0	.0	17.0	3.2	0.	0.	138.	0.	0.	2.75
N510H1.004	1.5	11.4	12.3	17.5	.35	50.0	.0	1.0	4.0	0.	0.	107.	0.	0.	8.35
N510H1.005	2.0	10.7	10.8	26.2	.35	50.0	-22.0	1.0	5.2	94.	0.	94.	0.	95.	8.19
N510H1.006	1.2	16.4	16.5	19.1	.22	50.0	-33.0	1.0	3.1	0.	0.	143.	0.	0.	5.17
N510H1.007	1.2	15.8	15.8	15.9	.10	50.0	-44.0	1.0	3.3	0.	0.	137.	0.	0.	2.76
N510H1.008	.4	.0	28.9	.0	.08	50.0	-56.0	1.0	1.0	0.	0.	252.	0.	0.	1.99
N510H1.009	.3	.0	29.9	.0	.03	50.0	-66.0	1.0	.8	0.	0.	260.	0.	0.	.92
N510H1.010	.1	.0	.0	.0	.03	50.0	-75.0	1.0	.4	0.	0.	0.	0.	0.	.68

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510H2.004	1.9	7.9	12.6	18.9	.38	50.0	.0	1.0	4.9	0.	0.	110.	0.	0.	8.93
N510H2.005	1.3	21.2	21.5	23.8	.35	50.0	-22.0	1.0	3.3	0.	0.	187.	0.	0.	8.24
N510H2.006	1.1	17.1	17.2	17.3	.24	50.0	-33.0	1.0	2.8	0.	0.	150.	0.	0.	5.77
N510H2.007	.8	.0	22.1	.0	.15	50.0	-44.0	1.0	2.0	0.	0.	193.	0.	0.	3.55
N510H2.008	.7	.0	19.5	.0	.08	50.0	-56.0	1.0	1.9	0.	0.	170.	0.	0.	2.04
N510H2.009	.5	.0	26.0	.0	.04	50.0	-66.0	1.0	1.4	0.	0.	227.	0.	0.	1.17
N510H2.010	.3	.0	20.4	.0	.00	50.0	-75.0	1.0	.8	0.	0.	178.	0.	0.	.63
N510H3.004	1.7	10.6	13.1	18.4	.40	50.0	.0	1.0	4.5	0.	0.	115.	0.	0.	9.33
N510H3.005	1.3	15.8	16.7	32.3	.29	50.0	-22.0	1.0	3.5	0.	0.	146.	0.	0.	6.81
N510H3.006	1.4	11.0	11.2	17.1	.20	50.0	-33.0	1.0	3.6	0.	0.	98.	0.	0.	4.93
N510H3.007	.8	.0	16.3	.0	.12	50.0	-44.0	1.0	2.2	0.	0.	142.	0.	0.	2.93
N510H3.008	.6	.0	21.1	.0	.05	50.0	-56.0	1.0	1.6	0.	0.	184.	0.	0.	1.29
N510H3.009	.2	.0	24.1	.0	.05	50.0	-66.0	1.0	.6	0.	0.	210.	0.	0.	1.18
N510H3.010	.1	.0	.0	.0	.01	50.0	-75.0	1.0	.4	0.	0.	0.	0.	0.	.46
N510H4.004	1.7	12.1	15.9	28.0	.41	50.0	.0	1.0	4.6	0.	0.	139.	0.	0.	9.56
N510H4.005	1.0	22.4	22.4	22.6	.28	50.0	-22.0	1.0	2.8	0.	0.	196.	0.	0.	6.62
N510H4.006	1.6	13.8	13.9	31.4	.21	50.0	-33.0	1.0	4.2	0.	0.	121.	0.	0.	5.03
N510H4.007	.9	.0	23.5	.0	.14	50.0	-44.0	1.0	2.5	0.	0.	205.	0.	0.	3.28
N510H4.008	.4	.0	20.2	.0	.08	50.0	-56.0	1.0	1.2	0.	0.	176.	0.	0.	1.89
N510H4.009	.3	.0	22.3	.0	.06	50.0	-66.0	1.0	.7	0.	0.	195.	0.	0.	1.52
N510H4.010	.1	.0	.0	.0	.03	50.0	-75.0	1.0	.3	0.	0.	0.	0.	0.	.76
N510H5.004	2.0	12.7	13.3	21.9	.42	50.0	.0	1.0	5.3	116.	0.	116.	0.	116.	9.86
N510H5.005	1.3	12.8	29.0	29.0	.33	50.0	-22.0	1.0	3.4	0.	0.	252.	0.	0.	7.68
N510H5.006	1.2	13.8	14.5	14.6	.24	50.0	-33.0	1.0	3.3	0.	0.	126.	0.	0.	5.65
N510H5.007	.8	.0	25.0	.0	.18	50.0	-44.0	1.0	2.2	0.	0.	218.	0.	0.	4.15
N510H5.008	.5	.0	17.9	.0	.08	50.0	-56.0	1.0	1.3	0.	0.	156.	0.	0.	2.05
N510H5.009	.3	.0	23.8	.0	.03	50.0	-66.0	1.0	.7	0.	0.	208.	0.	0.	.84
N510H5.010	.2	.0	.0	.0	.05	50.0	-75.0	1.0	.4	0.	0.	0.	0.	0.	1.18
N510I1.004	1.6	9.5	12.7	25.1	.46	50.0	.0	5.0	4.2	0.	0.	111.	0.	0.	10.84
N510I1.005	1.2	10.2	10.2	25.9	.26	50.0	-22.0	5.0	3.2	0.	0.	89.	0.	0.	6.11
N510I1.006	.9	.0	10.2	.0	.12	50.0	-33.0	5.0	2.4	0.	0.	89.	0.	0.	2.92
N510I1.007	.6	.0	16.0	.0	.08	50.0	-44.0	5.0	1.7	0.	0.	139.	0.	0.	1.85
N510I1.008	.3	.0	24.9	.0	.02	50.0	-56.0	5.0	.7	0.	0.	217.	0.	0.	.69
N510I1.009	.2	.0	.0	.0	.00	50.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.35
N510I1.010	.0	.0	.0	.0	-.02	50.0	-75.0	5.0	.1	0.	0.	0.	0.	0.	.13
N510I2.004	1.8	9.1	9.2	24.6	.43	50.0	.0	5.0	4.7	0.	0.	80.	0.	0.	10.08
N510I2.005	1.5	12.8	20.8	21.4	.26	50.0	-22.0	5.0	3.9	0.	0.	182.	0.	0.	6.29
N510I2.006	1.1	20.1	20.1	20.4	.13	50.0	-33.0	5.0	2.8	0.	0.	175.	0.	0.	3.13
N510I2.007	.9	.0	16.3	.0	.08	50.0	-44.0	5.0	2.4	0.	0.	142.	0.	0.	1.88
N510I2.008	.5	.0	20.3	.0	.05	50.0	-56.0	5.0	1.3	0.	0.	177.	0.	0.	1.21
N510I2.009	.3	.0	23.6	.0	.05	50.0	-66.0	5.0	.8	0.	0.	206.	0.	0.	1.26
N510I2.010	.1	.0	.0	.0	.03	50.0	-75.0	5.0	.3	0.	0.	0.	0.	0.	.69

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510I3.004	1.5	7.8	13.0	20.0	.39	50.0	.0	5.0	4.1	0.	0.	113.	0.	0.	9.15
N510I3.005	1.3	15.0	15.1	35.0	.32	50.0	-22.0	5.0	3.4	0.	0.	132.	0.	0.	7.51
N510I3.006	.9	.0	13.2	.0	.17	50.0	-33.0	5.0	2.4	0.	0.	115.	0.	0.	3.96
N510I3.007	.9	.0	17.5	.0	.06	50.0	-44.0	5.0	2.4	0.	0.	152.	0.	0.	1.62
N510I3.008	.4	.0	20.5	.0	.03	50.0	-56.0	5.0	.9	0.	0.	179.	0.	0.	.96
N510I3.009	.2	.0	23.8	.0	-.03	50.0	-66.0	5.0	.6	0.	0.	207.	0.	0.	.12
N510I3.010	.1	.0	.0	.0	-.01	50.0	-75.0	5.0	.2	0.	0.	0.	0.	0.	.11
N510I4.004	1.6	11.6	11.7	29.1	.41	50.0	.0	5.0	4.3	0.	0.	102.	0.	0.	9.57
N510I4.005	1.2	13.1	17.5	38.7	.29	50.0	-22.0	5.0	3.2	0.	0.	152.	0.	0.	6.72
N510I4.006	1.2	10.3	10.3	17.3	.12	50.0	-33.0	5.0	3.1	0.	0.	90.	0.	0.	2.93
N510I4.007	.6	.0	16.8	.0	.04	50.0	-44.0	5.0	1.5	0.	0.	147.	0.	0.	1.09
N510I4.008	.3	.0	21.0	.0	.02	50.0	-56.0	5.0	.7	0.	0.	183.	0.	0.	.79
N510I4.009	.1	.0	.0	.0	.01	50.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.39
N510I4.010	.1	.0	.0	.0	.00	50.0	-75.0	5.0	.2	0.	0.	0.	0.	0.	.15
N510I5.004	1.8	9.2	9.4	22.2	.44	50.0	.0	5.0	4.7	0.	0.	82.	0.	0.	10.30
N510I5.005	1.3	13.8	14.0	20.2	.33	50.0	-22.0	5.0	3.3	0.	0.	122.	0.	0.	7.73
N510I5.006	1.3	13.6	14.0	17.5	.19	50.0	-33.0	5.0	3.5	0.	0.	122.	0.	0.	4.52
N510I5.007	.5	.0	9.2	.0	.09	50.0	-44.0	5.0	1.3	0.	0.	80.	0.	0.	2.23
N510I5.008	.5	.0	24.2	.0	.05	50.0	-56.0	5.0	1.3	0.	0.	211.	0.	0.	1.24
N510I5.009	.4	.0	18.9	.0	.03	50.0	-66.0	5.0	1.1	0.	0.	164.	0.	0.	.86
N510I5.010	.1	.0	.0	.0	-.01	50.0	-75.0	5.0	.2	0.	0.	0.	0.	0.	.11
N510J1.004	1.5	12.3	13.1	21.3	.27	50.0	.0	11.0	3.9	0.	0.	114.	0.	0.	6.56
N510J1.005	1.5	11.0	11.0	20.9	.20	50.0	-22.0	11.0	3.9	0.	0.	96.	0.	0.	4.78
N510J1.006	1.2	10.8	10.8	10.9	.08	50.0	-33.0	11.0	3.3	0.	0.	94.	0.	0.	2.06
N510J1.007	.4	.0	66.4	.0	.10	50.0	-44.0	11.0	1.2	0.	0.	579.	0.	0.	2.28
N510J1.008	.3	.0	44.5	.0	.06	50.0	-56.0	11.0	.8	0.	0.	388.	0.	0.	1.49
N510J1.009	.2	.0	.0	.0	.04	50.0	-66.0	11.0	.5	0.	0.	0.	0.	0.	.86
N510J1.010	.1	.0	.0	.0	.03	50.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.66
N510J2.004	1.5	7.1	11.9	17.4	.30	50.0	.0	11.0	3.9	0.	0.	103.	0.	0.	7.26
N510J2.005	1.2	14.4	21.5	38.4	.24	50.0	-22.0	11.0	3.2	0.	0.	187.	0.	0.	5.93
N510J2.006	1.4	21.7	21.7	51.0	.17	50.0	-33.0	11.0	3.7	0.	0.	189.	0.	0.	4.00
N510J2.007	1.4	37.7	37.9	38.0	.12	50.0	-44.0	11.0	3.7	0.	0.	330.	0.	0.	2.88
N510J2.008	.5	.0	28.0	.0	.10	50.0	-56.0	11.0	1.4	0.	0.	244.	0.	0.	2.41
N510J2.009	.5	.0	29.8	.0	.09	50.0	-66.0	11.0	1.4	0.	0.	259.	0.	0.	2.19
N510J2.010	.4	.0	31.5	.0	.08	50.0	-75.0	11.0	1.1	0.	0.	275.	0.	0.	1.86
N510J3.004	1.6	6.8	11.2	26.5	.31	50.0	.0	11.0	4.2	0.	0.	98.	0.	0.	7.43
N510J3.005	1.9	11.7	21.8	33.0	.14	50.0	-22.0	11.0	4.9	0.	0.	190.	0.	0.	3.75
N510J3.006	.7	.0	55.4	.0	.02	50.0	-33.0	11.0	1.9	0.	0.	483.	0.	0.	.98
N510J3.007	.5	.0	23.1	.0	.01	50.0	-44.0	11.0	1.4	0.	0.	201.	0.	0.	.58
N510J3.008	.1	.0	.0	.0	-.01	50.0	-56.0	11.0	.4	0.	0.	0.	0.	0.	.09
N510J3.009	.1	.0	.0	.0	-.03	50.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.06
N510J3.010	.1	.0	.0	.0	.01	50.0	-75.0	11.0	.2	0.	0.	0.	0.	0.	.45

FALCON 5: LSR = 100, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510J4.004	1.4	11.9	14.6	22.5	.29	50.0	.0	11.0	3.7	0.	0.	127.	0.	0.	6.84
N510J4.005	1.3	15.5	26.7	41.5	.20	50.0	-22.0	11.0	3.3	0.	0.	233.	0.	0.	5.09
N510J4.006	1.2	17.4	17.4	17.5	.13	50.0	-33.0	11.0	3.2	0.	0.	152.	0.	0.	3.16
N510J4.007	.7	.0	54.1	.0	.04	50.0	-44.0	11.0	1.9	0.	0.	471.	0.	0.	.89
N510J4.008	.4	.0	53.3	.0	.05	50.0	-56.0	11.0	1.2	0.	0.	465.	0.	0.	1.24
N510J4.009	.5	.0	29.9	.0	.03	50.0	-66.0	11.0	1.2	0.	0.	261.	0.	0.	.79
N510J4.010	.2	.0	30.5	.0	.00	50.0	-75.0	11.0	.6	0.	0.	266.	0.	0.	.32
N510J5.004	1.2	10.3	12.0	19.7	.27	50.0	.0	11.0	3.1	0.	0.	104.	0.	0.	6.39
N510J5.005	1.4	8.5	18.9	21.4	.20	50.0	-22.0	11.0	3.7	0.	0.	165.	0.	0.	4.87
N510J5.006	1.0	48.0	48.0	48.0	.07	50.0	-33.0	11.0	2.7	0.	0.	419.	0.	0.	1.88
N510J5.007	1.1	18.3	18.4	18.4	.02	50.0	-44.0	11.0	3.0	0.	0.	160.	0.	0.	.79
N510J5.008	.4	.0	39.7	.0	.01	50.0	-56.0	11.0	1.0	0.	0.	346.	0.	0.	.60
N510J5.009	.2	.0	.0	.0	.01	50.0	-66.0	11.0	.5	0.	0.	0.	0.	0.	.39
N510J5.010	.1	.0	.0	.0	-.03	50.0	-75.0	11.0	.4	0.	0.	0.	0.	0.	.07
N510K1.004	1.4	11.1	12.4	15.3	.12	50.0	.0	17.0	3.6	0.	0.	108.	0.	0.	3.72
N510K1.005	1.5	17.0	42.0	42.2	.09	50.0	-22.0	17.0	3.9	0.	0.	366.	0.	0.	2.68
N510K1.006	1.2	7.8	7.8	7.8	.04	50.0	-33.0	17.0	3.1	0.	0.	68.	0.	0.	1.28
N510K1.007	.9	.0	32.2	.0	.02	50.0	-44.0	17.0	2.3	0.	0.	280.	0.	0.	.77
N510K1.008	.5	.0	26.9	.0	.02	50.0	-56.0	17.0	1.3	0.	0.	235.	0.	0.	.35
N510K1.009	.2	.0	34.5	.0	.00	50.0	-66.0	17.0	.6	0.	0.	301.	0.	0.	.33
N510K1.010	.4	.0	21.1	.0	.00	50.0	-75.0	17.0	1.0	0.	0.	184.	0.	0.	.75
N510K2.004	1.7	7.9	9.9	39.4	.15	50.0	.0	17.0	4.5	0.	0.	86.	0.	0.	4.22
N510K2.005	1.1	55.0	55.0	55.0	.04	50.0	-22.0	17.0	2.9	0.	0.	480.	0.	0.	1.99
N510K2.006	.6	.0	88.0	.0	-.02	50.0	-33.0	17.0	1.6	0.	0.	767.	0.	0.	.70
N510K2.007	.5	.0	29.1	.0	.02	50.0	-44.0	17.0	1.4	0.	0.	253.	0.	0.	.55
N510K2.008	.3	.0	75.6	.0	.00	50.0	-56.0	17.0	.8	0.	0.	660.	0.	0.	.20
N510K2.009	.1	.0	.0	.0	-.01	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.31
N510K2.010	.1	.0	.0	.0	-.01	50.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.21
N510K3.004	1.4	10.1	10.1	12.4	.06	50.0	.0	17.0	3.6	0.	0.	88.	0.	0.	2.66
N510K3.005	.9	.0	40.2	.0	.07	50.0	-22.0	17.0	2.4	0.	0.	351.	0.	0.	2.31
N510K3.006	.8	.0	61.1	.0	.04	50.0	-33.0	17.0	2.0	0.	0.	533.	0.	0.	.86
N510K3.007	.5	.0	21.2	.0	.01	50.0	-44.0	17.0	1.3	0.	0.	185.	0.	0.	.65
N510K3.008	.3	.0	43.2	.0	.00	50.0	-56.0	17.0	.8	0.	0.	377.	0.	0.	.40
N510K3.009	.1	.0	.0	.0	.04	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	1.00
N510K3.010	.1	.0	.0	.0	.05	50.0	-75.0	17.0	.3	0.	0.	0.	0.	0.	1.23
N510K4.004	1.4	6.1	14.5	25.7	.19	50.0	.0	17.0	3.7	0.	0.	126.	0.	0.	4.79
N510K4.005	1.1	18.2	33.6	33.7	.07	50.0	-22.0	17.0	3.0	0.	0.	293.	0.	0.	2.14
N510K4.006	.8	.0	31.9	.0	.03	50.0	-33.0	17.0	2.2	0.	0.	278.	0.	0.	.99
N510K4.007	.5	.0	10.0	.0	.01	50.0	-44.0	17.0	1.4	0.	0.	87.	0.	0.	.59
N510K4.008	.3	.0	78.5	.0	.01	50.0	-56.0	17.0	.8	0.	0.	685.	0.	0.	.44
N510K4.009	.2	.0	.0	.0	-.01	50.0	-66.0	17.0	.5	0.	0.	0.	0.	0.	.23
N510K4.010	.1	.0	.0	.0	.01	50.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.46

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510K5.004	1.3	7.1	7.1	39.1	.18	50.0	.0	17.0	3.3	0.	0.	62.	0.	0.	4.58
N510K5.005	1.1	20.1	20.1	20.2	.07	50.0	-22.0	17.0	3.0	0.	0.	175.	0.	0.	2.33
N510K5.006	.8	.0	8.3	.0	.02	50.0	-33.0	17.0	2.2	0.	0.	73.	0.	0.	.70
N510K5.007	.3	.0	99.2	.0	.00	50.0	-44.0	17.0	.8	0.	0.	865.	0.	0.	.27
N510K5.008	.2	.0	15.9	.0	.02	50.0	-56.0	17.0	.6	0.	0.	138.	0.	0.	.38
N510K5.009	.2	.0	31.9	.0	.02	50.0	-66.0	17.0	.6	0.	0.	278.	0.	0.	.73
N510K5.010	.1	.0	.0	.0	-.01	50.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.18
N510L1.004	.1	.0	.0	.0	-.04	150.0	84.0	1.0	.3	0.	0.	0.	0.	0.	.11
N510L1.005	.1	.0	.0	.0	.00	150.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.40
N510L1.006	.8	.0	15.1	.0	.06	150.0	56.0	1.0	2.1	0.	0.	131.	0.	0.	1.58
N510L1.007	1.0	.0	19.1	.0	.19	150.0	50.0	1.0	2.6	0.	0.	166.	0.	0.	4.56
N510L1.008	1.3	18.4	18.6	19.2	.19	150.0	33.0	1.0	3.4	0.	0.	162.	0.	0.	4.47
N510L1.009	1.4	17.3	18.5	19.8	.21	150.0	28.0	1.0	3.7	0.	0.	161.	0.	0.	5.01
N510L1.010	1.0	.0	17.5	.0	.25	150.0	.0	1.0	2.6	0.	0.	153.	0.	0.	5.87
N510L2.004	.1	.0	.0	.0	.00	150.0	84.0	1.0	.4	0.	0.	0.	0.	0.	.39
N510L2.005	.2	.0	.0	.0	.07	150.0	75.0	1.0	.4	0.	0.	0.	0.	0.	1.57
N510L2.006	.9	.0	17.7	.0	.10	150.0	56.0	1.0	2.3	0.	0.	154.	0.	0.	2.70
N510L2.007	1.1	16.7	17.5	19.3	.17	150.0	50.0	1.0	3.0	0.	0.	153.	0.	0.	4.13
N510L2.008	1.3	16.4	17.5	17.9	.25	150.0	33.0	1.0	3.3	0.	0.	152.	0.	0.	5.86
N510L2.009	1.3	15.8	17.5	17.5	.27	150.0	28.0	1.0	3.5	0.	0.	152.	0.	0.	6.39
N510L2.010	1.3	16.2	16.3	16.5	.30	150.0	.0	1.0	3.5	0.	0.	142.	0.	0.	7.08
N510L3.004	.2	.0	.0	.0	.03	150.0	84.0	1.0	.4	0.	0.	0.	0.	0.	1.00
N510L3.005	.1	.0	.0	.0	-.04	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.14
N510L3.006	.7	.0	17.2	.0	.10	150.0	56.0	1.0	2.0	0.	0.	150.	0.	0.	2.51
N510L3.007	1.1	17.6	17.9	19.6	.18	150.0	50.0	1.0	2.9	0.	0.	156.	0.	0.	4.42
N510L3.008	1.0	.0	17.1	.0	.19	150.0	33.0	1.0	2.6	0.	0.	149.	0.	0.	4.47
N510L3.009	1.0	17.0	17.0	17.0	.27	150.0	28.0	1.0	2.8	0.	0.	148.	0.	0.	6.27
N510L3.010	.9	.0	16.9	.0	.31	150.0	.0	1.0	2.4	0.	0.	147.	0.	0.	7.36
N510L4.004	.1	.0	.0	.0	-.01	150.0	84.0	1.0	.3	0.	0.	0.	0.	0.	.41
N510L4.005	.1	.0	.0	.0	-.03	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.01
N510L4.006	1.3	17.9	19.7	19.9	.14	150.0	56.0	1.0	3.4	0.	0.	172.	0.	0.	3.37
N510L4.007	1.3	17.8	19.1	21.4	.17	150.0	50.0	1.0	3.6	0.	0.	166.	0.	0.	4.25
N510L4.008	1.2	15.9	16.1	18.6	.21	150.0	33.0	1.0	3.3	0.	0.	141.	0.	0.	5.00
N510L4.009	1.7	13.3	16.0	21.5	.27	150.0	28.0	1.0	4.4	0.	0.	140.	0.	0.	6.43
N510L4.010	1.2	17.0	17.5	17.9	.28	150.0	.0	1.0	3.1	0.	0.	152.	0.	0.	6.52
N510L5.004	.1	.0	.0	.0	-.02	150.0	84.0	1.0	.3	0.	0.	0.	0.	0.	.27
N510L5.005	.3	.0	25.4	.0	.06	150.0	75.0	1.0	.7	0.	0.	222.	0.	0.	1.40
N510L5.006	1.0	.0	18.6	.0	.11	150.0	56.0	1.0	2.6	0.	0.	162.	0.	0.	2.74
N510L5.007	1.1	17.0	18.7	19.6	.18	150.0	50.0	1.0	3.0	0.	0.	163.	0.	0.	4.26
N510L5.008	1.2	15.3	16.9	17.0	.23	150.0	33.0	1.0	3.1	0.	0.	147.	0.	0.	5.50
N510L5.009	1.0	15.4	15.4	15.5	.26	150.0	28.0	1.0	2.8	0.	0.	134.	0.	0.	6.19
N510L5.010	1.1	17.2	17.5	17.6	.32	150.0	.0	1.0	2.9	0.	0.	152.	0.	0.	7.44

FALCON 5: LSR = 100, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510M1.004	.1	.0	.0	.0	.04	150.0	84.0	5.0	.4	0.	0.	0.	0.	0.	1.09
N510M1.005	.1	.0	.0	.0	.02	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.64
N510M1.006	.1	.0	.0	.0	.02	150.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.63
N510M1.007	.5	.0	21.3	.0	.05	150.0	50.0	5.0	1.3	0.	0.	185.	0.	0.	1.15
N510M1.008	.9	.0	17.0	.0	.09	150.0	33.0	5.0	2.5	0.	0.	148.	0.	0.	2.26
N510M1.009	1.2	16.9	16.9	18.1	.14	150.0	28.0	5.0	3.1	0.	0.	148.	0.	0.	3.35
N510M1.010	.8	.0	19.5	.0	.15	150.0	.0	5.0	2.2	0.	0.	170.	0.	0.	3.79
N510M2.004	.1	.0	.0	.0	.01	150.0	84.0	5.0	.3	0.	0.	0.	0.	0.	.45
N510M2.005	.1	.0	.0	.0	-.02	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.04
N510M2.006	.4	.0	19.5	.0	.05	150.0	56.0	5.0	1.1	0.	0.	170.	0.	0.	1.24
N510M2.007	.9	.0	19.0	.0	.06	150.0	50.0	5.0	2.5	0.	0.	165.	0.	0.	1.42
N510M2.008	1.0	16.1	16.1	16.2	.10	150.0	33.0	5.0	2.7	0.	0.	141.	0.	0.	2.25
N510M2.009	1.0	16.5	16.5	16.5	.13	150.0	28.0	5.0	2.8	0.	0.	143.	0.	0.	3.05
N510M2.010	1.1	17.3	17.3	20.2	.20	150.0	.0	5.0	2.9	0.	0.	151.	0.	0.	4.68
N510M3.004	.1	.0	.0	.0	-.01	150.0	84.0	5.0	.2	0.	0.	0.	0.	0.	.23
N510M3.005	.1	.0	.0	.0	.01	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.54
N510M3.006	.1	.0	.0	.0	-.02	150.0	56.0	5.0	.4	0.	0.	0.	0.	0.	.12
N510M3.007	.3	.0	17.2	.0	.01	150.0	50.0	5.0	.8	0.	0.	150.	0.	0.	.51
N510M3.008	1.1	17.6	17.6	19.6	.08	150.0	33.0	5.0	2.8	0.	0.	154.	0.	0.	2.01
N510M3.009	1.2	16.9	17.8	18.4	.12	150.0	28.0	5.0	3.2	0.	0.	156.	0.	0.	2.99
N510M3.010	.8	.0	22.0	.0	.22	150.0	.0	5.0	2.3	0.	0.	192.	0.	0.	5.13
N510M4.004	.1	.0	.0	.0	.04	150.0	84.0	5.0	.4	0.	0.	0.	0.	0.	1.09
N510M4.005	.1	.0	.0	.0	.04	150.0	75.0	5.0	.3	0.	0.	0.	0.	0.	.91
N510M4.006	.3	.0	24.8	.0	.05	150.0	56.0	5.0	.9	0.	0.	217.	0.	0.	1.29
N510M4.007	1.2	18.9	18.9	19.1	.07	150.0	50.0	5.0	3.1	0.	0.	165.	0.	0.	1.78
N510M4.008	1.0	.0	18.2	.0	.12	150.0	33.0	5.0	2.6	0.	0.	159.	0.	0.	2.89
N510M4.009	1.2	16.8	16.9	17.8	.12	150.0	28.0	5.0	3.2	0.	0.	148.	0.	0.	2.97
N510M4.010	.8	.0	13.9	.0	.23	150.0	.0	5.0	2.1	0.	0.	121.	0.	0.	5.46
N510M5.004	.2	.0	.0	.0	.03	150.0	84.0	5.0	.4	0.	0.	0.	0.	0.	.83
N510M5.005	.2	.0	.0	.0	.03	150.0	75.0	5.0	.5	0.	0.	0.	0.	0.	.85
N510M5.006	1.1	19.4	19.5	19.5	.05	150.0	56.0	5.0	3.0	0.	0.	170.	0.	0.	1.29
N510M5.007	1.1	18.6	18.7	19.3	.01	150.0	50.0	5.0	3.0	0.	0.	163.	0.	0.	1.01
N510M5.008	1.0	15.8	15.8	16.0	.07	150.0	33.0	5.0	2.8	0.	0.	138.	0.	0.	1.79
N510M5.009	1.1	15.4	17.2	17.6	.10	150.0	28.0	5.0	3.0	0.	0.	150.	0.	0.	2.58
N510M5.010	.7	.0	16.5	.0	.16	150.0	.0	5.0	1.9	0.	0.	144.	0.	0.	3.95
N510N1.004	.1	.0	.0	.0	.00	150.0	84.0	11.0	.2	0.	0.	0.	0.	0.	.39
N510N1.005	.1	.0	.0	.0	.02	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.56
N510N1.006	.1	.0	.0	.0	.00	150.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.12
N510N1.007	.2	.0	15.3	.0	.00	150.0	50.0	11.0	.6	0.	0.	133.	0.	0.	.32
N510N1.008	.9	.0	19.5	.0	.02	150.0	33.0	11.0	2.5	0.	0.	170.	0.	0.	1.00
N510N1.009	.9	.0	17.8	.0	-.02	150.0	28.0	11.0	2.3	0.	0.	155.	0.	0.	.78
N510N1.010	.9	.0	18.2	.0	.06	150.0	.0	11.0	2.4	0.	0.	158.	0.	0.	2.00

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510N2.004	.1	.0	.0	.0	.04	150.0	84.0	11.0	.3	0.	0.	0.	0.	0.	1.00
N510N2.005	.1	.0	.0	.0	.04	150.0	75.0	11.0	.3	0.	0.	0.	0.	0.	1.05
N510N2.006	.3	.0	18.6	.0	.00	150.0	56.0	11.0	.7	0.	0.	162.	0.	0.	.05
N510N2.007	.9	.0	18.1	.0	-.01	150.0	50.0	11.0	2.4	0.	0.	158.	0.	0.	.21
N510N2.008	.9	.0	17.5	.0	.03	150.0	33.0	11.0	2.3	0.	0.	153.	0.	0.	.95
N510N2.009	.5	.0	17.4	.0	-.05	150.0	28.0	11.0	1.4	0.	0.	152.	0.	0.	.27
N510N2.010	.6	.0	25.8	.0	.06	150.0	.0	11.0	1.6	0.	0.	225.	0.	0.	1.94
N510N3.004	.1	.0	.0	.0	.01	150.0	84.0	11.0	.2	0.	0.	0.	0.	0.	.25
N510N3.005	.1	.0	.0	.0	.05	150.0	75.0	11.0	.3	0.	0.	0.	0.	0.	1.20
N510N3.006	.2	.0	.0	.0	.03	150.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.80
N510N3.007	.2	.0	11.7	.0	.01	150.0	50.0	11.0	.6	0.	0.	102.	0.	0.	.28
N510N3.008	1.1	12.3	12.4	18.4	.06	150.0	33.0	11.0	2.9	0.	0.	108.	0.	0.	1.56
N510N3.009	.7	.0	21.2	.0	.06	150.0	28.0	11.0	2.0	0.	0.	185.	0.	0.	1.45
N510N3.010	.6	.0	33.2	.0	.09	150.0	.0	11.0	1.7	0.	0.	290.	0.	0.	2.39
N510N4.004	.0	.0	.0	.0	-.03	150.0	84.0	11.0	.0	0.	0.	0.	0.	0.	.10
N510N4.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.00
N510N4.006	.4	.0	20.0	.0	.01	150.0	56.0	11.0	1.1	0.	0.	174.	0.	0.	.56
N510N4.007	.3	.0	19.5	.0	-.01	150.0	50.0	11.0	.9	0.	0.	170.	0.	0.	.22
N510N4.008	.8	.0	14.1	.0	.07	150.0	33.0	11.0	2.1	0.	0.	123.	0.	0.	1.71
N510N4.009	.6	.0	12.0	.0	.08	150.0	28.0	11.0	1.5	0.	0.	105.	0.	0.	2.03
N510N4.010	.8	.0	13.4	.0	.10	150.0	.0	11.0	2.0	0.	0.	116.	0.	0.	2.46
N510N5.004	.1	.0	.0	.0	.01	150.0	84.0	11.0	.3	0.	0.	0.	0.	0.	.41
N510N5.005	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.15
N510N5.006	.1	.0	.0	.0	.02	150.0	56.0	11.0	.3	0.	0.	0.	0.	0.	.61
N510N5.007	.6	.0	16.2	.0	.02	150.0	50.0	11.0	1.7	0.	0.	141.	0.	0.	.75
N510N5.008	.8	.0	15.5	.0	.03	150.0	33.0	11.0	2.1	0.	0.	135.	0.	0.	.87
N510N5.009	.7	.0	16.4	.0	.01	150.0	28.0	11.0	1.9	0.	0.	143.	0.	0.	.67
N510N5.010	1.0	.0	17.8	.0	.16	150.0	.0	11.0	2.6	0.	0.	156.	0.	0.	3.84
N51001.004	.1	.0	.0	.0	.02	150.0	84.0	17.0	.3	0.	0.	0.	0.	0.	.56
N51001.005	.1	.0	.0	.0	.02	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.54
N51001.006	.2	.0	20.4	.0	.03	150.0	56.0	17.0	.6	0.	0.	178.	0.	0.	.83
N51001.007	.8	.0	19.7	.0	.03	150.0	50.0	17.0	2.1	0.	0.	171.	0.	0.	.80
N51001.008	.5	.0	16.5	.0	.03	150.0	33.0	17.0	1.2	0.	0.	144.	0.	0.	.86
N51001.009	.3	.0	15.5	.0	-.04	150.0	28.0	17.0	.9	0.	0.	135.	0.	0.	.40
N51001.010	.6	.0	30.2	.0	.03	150.0	.0	17.0	1.5	0.	0.	263.	0.	0.	1.62
N51002.004	.1	.0	.0	.0	.05	150.0	84.0	17.0	.4	0.	0.	0.	0.	0.	1.11
N51002.005	.1	.0	.0	.0	.04	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	1.02
N51002.006	.1	.0	.0	.0	.04	150.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.87
N51002.007	.1	.0	.0	.0	-.02	150.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.09
N51002.008	.4	.0	10.8	.0	-.01	150.0	33.0	17.0	1.0	0.	0.	94.	0.	0.	.36
N51002.009	.8	.0	16.7	.0	.10	150.0	28.0	17.0	2.2	0.	0.	145.	0.	0.	2.50
N51002.010	.5	.0	24.4	.0	.01	150.0	.0	17.0	1.4	0.	0.	212.	0.	0.	.88

FALCON 5: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N51003.004	.1	.0	.0	.0	-.02	150.0	84.0	17.0	.1	0.	0.	0.	0.	0.	.08
N51003.005	.1	.0	.0	.0	-.02	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.04
N51003.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.4	0.	0.	0.	0.	0.	.29
N51003.007	.1	.0	.0	.0	.03	150.0	50.0	17.0	.4	0.	0.	0.	0.	0.	.87
N51003.008	.5	.0	18.5	.0	.05	150.0	33.0	17.0	1.3	0.	0.	161.	0.	0.	1.21
N51003.009	.4	.0	18.5	.0	-.02	150.0	28.0	17.0	1.0	0.	0.	162.	0.	0.	.31
N51003.010	.6	.0	22.0	.0	-.01	150.0	.0	17.0	1.7	0.	0.	192.	0.	0.	.81
N51004.004	.1	.0	.0	.0	.01	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.39
N51004.005	.1	.0	.0	.0	.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.17
N51004.006	.1	.0	.0	.0	.03	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.82
N51004.007	.1	.0	.0	.0	.01	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.45
N51004.008	.3	.0	16.8	.0	.02	150.0	33.0	17.0	.9	0.	0.	146.	0.	0.	.51
N51004.009	.4	.0	15.5	.0	.03	150.0	28.0	17.0	1.1	0.	0.	135.	0.	0.	.87
N51004.010	.6	.0	27.7	.0	.05	150.0	.0	17.0	1.6	0.	0.	241.	0.	0.	1.39
N51005.004	.1	.0	.0	.0	.00	150.0	84.0	17.0	.1	0.	0.	0.	0.	0.	.30
N51005.005	.1	.0	.0	.0	.00	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.06
N51005.006	.1	.0	.0	.0	.00	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.26
N51005.007	.7	.0	17.2	.0	-.01	150.0	50.0	17.0	1.8	0.	0.	150.	0.	0.	.23
N51005.008	.8	.0	16.1	.0	.03	150.0	33.0	17.0	2.1	0.	0.	140.	0.	0.	.84
N51005.009	.6	.0	10.7	.0	.04	150.0	28.0	17.0	1.5	0.	0.	93.	0.	0.	1.08
N51005.010	.8	.0	13.2	.0	.01	150.0	.0	17.0	2.2	0.	0.	115.	0.	0.	.86
N510P1.004	.8	.0	20.5	.0	.29	150.0	.0	1.0	2.2	0.	0.	179.	0.	0.	6.95
N510P1.005	.7	.0	17.3	.0	.21	150.0	-28.0	1.0	1.9	0.	0.	151.	0.	0.	5.13
N510P1.006	.8	.0	18.3	.0	.21	150.0	-33.0	1.0	2.0	0.	0.	160.	0.	0.	5.18
N510P1.007	.8	.0	25.5	.0	.26	150.0	-50.0	1.0	2.1	0.	0.	223.	0.	0.	6.21
N510P1.008	.7	.0	25.6	.0	.21	150.0	-56.0	1.0	1.8	0.	0.	223.	0.	0.	4.91
N510P1.009	.6	.0	28.6	.0	.14	150.0	-75.0	1.0	1.5	0.	0.	250.	0.	0.	3.36
N510P1.010	.4	.0	28.9	.0	.00	150.0	-84.0	1.0	1.1	0.	0.	252.	0.	0.	.68
N510P2.004	1.0	20.0	20.0	20.2	.28	150.0	.0	1.0	2.7	0.	0.	174.	0.	0.	6.65
N510P2.005	.9	.0	19.8	.0	.31	150.0	-28.0	1.0	2.5	0.	0.	173.	0.	0.	7.32
N510P2.006	.9	.0	20.2	.0	.27	150.0	-33.0	1.0	2.4	0.	0.	176.	0.	0.	6.49
N510P2.007	.9	.0	23.6	.0	.21	150.0	-50.0	1.0	2.5	0.	0.	206.	0.	0.	5.12
N510P2.008	.8	.0	23.5	.0	.21	150.0	-56.0	1.0	2.1	0.	0.	204.	0.	0.	5.03
N510P2.009	.6	.0	33.1	.0	.15	150.0	-75.0	1.0	1.6	0.	0.	288.	0.	0.	3.52
N510P2.010	.5	.0	32.1	.0	.15	150.0	-84.0	1.0	1.2	0.	0.	280.	0.	0.	3.56
N510P3.004	.9	.0	18.4	.0	.28	150.0	.0	1.0	2.3	0.	0.	160.	0.	0.	6.66
N510P3.005	.8	.0	20.3	.0	.26	150.0	-28.0	1.0	2.1	0.	0.	177.	0.	0.	6.25
N510P3.006	.8	.0	20.1	.0	.25	150.0	-33.0	1.0	2.2	0.	0.	176.	0.	0.	5.94
N510P3.007	.9	.0	24.2	.0	.30	150.0	-50.0	1.0	2.3	0.	0.	211.	0.	0.	6.97
N510P3.008	.7	.0	21.7	.0	.18	150.0	-56.0	1.0	1.8	0.	0.	189.	0.	0.	4.32
N510P3.009	.7	.0	23.3	.0	.17	150.0	-75.0	1.0	1.8	0.	0.	203.	0.	0.	3.91
N510P3.010	.5	.0	25.8	.0	.15	150.0	-84.0	1.0	1.4	0.	0.	225.	0.	0.	3.66

FALCON 5: LSR = 100, GAS = ARGON

	MODEL CONDITIONS								PROTOTYPE CONDITIONS						
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510P4.004	.9	.0	18.6	.0	.23	150.0	.0	1.0	2.5	0.	0.	162.	0.	0.	5.50
N510P4.005	1.0	.0	21.5	.0	.28	150.0	-28.0	1.0	2.6	0.	0.	187.	0.	0.	6.65
N510P4.006	1.0	.0	18.4	.0	.31	150.0	-33.0	1.0	2.6	0.	0.	161.	0.	0.	7.21
N510P4.007	.8	.0	21.7	.0	.22	150.0	-50.0	1.0	2.2	0.	0.	190.	0.	0.	5.39
N510P4.008	.6	.0	19.3	.0	.21	150.0	-56.0	1.0	1.7	0.	0.	168.	0.	0.	5.02
N510P4.009	.5	.0	16.4	.0	.08	150.0	-75.0	1.0	1.3	0.	0.	143.	0.	0.	2.05
N510P4.010	.5	.0	26.8	.0	.13	150.0	-84.0	1.0	1.2	0.	0.	233.	0.	0.	3.14
N510P5.004	.9	.0	16.5	.0	.29	150.0	.0	1.0	2.5	0.	0.	144.	0.	0.	6.90
N510P5.005	1.0	.0	20.8	.0	.23	150.0	-28.0	1.0	2.6	0.	0.	181.	0.	0.	5.59
N510P5.006	.9	.0	22.4	.0	.25	150.0	-33.0	1.0	2.3	0.	0.	195.	0.	0.	5.95
N510P5.007	.9	.0	21.6	.0	.19	150.0	-50.0	1.0	2.5	0.	0.	188.	0.	0.	4.65
N510P5.008	.7	.0	22.0	.0	.15	150.0	-56.0	1.0	1.8	0.	0.	192.	0.	0.	3.55
N510P5.009	.6	.0	22.4	.0	.11	150.0	-75.0	1.0	1.7	0.	0.	195.	0.	0.	2.82
N510P5.010	.5	.0	25.6	.0	.12	150.0	-84.0	1.0	1.2	0.	0.	224.	0.	0.	3.06
N510Q1.004	1.2	18.9	19.0	19.1	.24	150.0	.0	5.0	3.2	0.	0.	165.	0.	0.	5.59
N510Q1.005	.9	.0	17.5	.0	.25	150.0	-28.0	5.0	2.4	0.	0.	153.	0.	0.	5.81
N510Q1.006	1.1	18.7	18.7	18.8	.27	150.0	-33.0	5.0	2.8	0.	0.	163.	0.	0.	6.28
N510Q1.007	.9	.0	19.3	.0	.17	150.0	-50.0	5.0	2.3	0.	0.	168.	0.	0.	4.04
N510Q1.008	.8	.0	19.6	.0	.08	150.0	-56.0	5.0	2.1	0.	0.	170.	0.	0.	2.08
N510Q1.009	.6	.0	21.4	.0	.07	150.0	-75.0	5.0	1.7	0.	0.	187.	0.	0.	1.82
N510Q1.010	.5	.0	21.9	.0	.09	150.0	-84.0	5.0	1.2	0.	0.	191.	0.	0.	2.26
N510Q2.004	.9	.0	20.1	.0	.22	150.0	.0	5.0	2.4	0.	0.	175.	0.	0.	5.25
N510Q2.005	.8	.0	19.1	.0	.19	150.0	-28.0	5.0	2.1	0.	0.	166.	0.	0.	4.64
N510Q2.006	.7	.0	19.4	.0	.21	150.0	-33.0	5.0	1.9	0.	0.	169.	0.	0.	4.98
N510Q2.007	.6	.0	41.0	.0	.14	150.0	-50.0	5.0	1.7	0.	0.	357.	0.	0.	3.50
N510Q2.008	.6	.0	34.0	.0	.14	150.0	-56.0	5.0	1.7	0.	0.	296.	0.	0.	3.44
N510Q2.009	.5	.0	35.0	.0	.09	150.0	-75.0	5.0	1.3	0.	0.	305.	0.	0.	2.35
N510Q2.010	.4	.0	37.0	.0	.06	150.0	-84.0	5.0	1.1	0.	0.	323.	0.	0.	1.59
N510Q3.004	.7	.0	16.0	.0	.21	150.0	.0	5.0	1.8	0.	0.	140.	0.	0.	4.92
N510Q3.005	.7	.0	17.3	.0	.17	150.0	-28.0	5.0	1.9	0.	0.	151.	0.	0.	4.27
N510Q3.006	.8	.0	22.0	.0	.16	150.0	-33.0	5.0	2.0	0.	0.	192.	0.	0.	3.85
N510Q3.007	.7	.0	17.4	.0	.13	150.0	-50.0	5.0	1.9	0.	0.	152.	0.	0.	3.17
N510Q3.008	.7	.0	17.4	.0	.11	150.0	-56.0	5.0	1.8	0.	0.	152.	0.	0.	2.65
N510Q3.009	.5	.0	34.9	.0	.08	150.0	-75.0	5.0	1.4	0.	0.	304.	0.	0.	1.89
N510Q3.010	.4	.0	23.6	.0	.05	150.0	-84.0	5.0	1.0	0.	0.	206.	0.	0.	1.38
N510Q4.004	.8	.0	13.8	.0	.18	150.0	.0	5.0	2.1	0.	0.	120.	0.	0.	4.54
N510Q4.005	.9	.0	19.1	.0	.20	150.0	-28.0	5.0	2.4	0.	0.	167.	0.	0.	4.87
N510Q4.006	1.0	.0	19.2	.0	.18	150.0	-33.0	5.0	2.6	0.	0.	168.	0.	0.	4.41
N510Q4.007	.8	.0	19.1	.0	.14	150.0	-50.0	5.0	2.2	0.	0.	167.	0.	0.	3.43
N510Q4.008	.8	.0	21.4	.0	.11	150.0	-56.0	5.0	2.2	0.	0.	187.	0.	0.	2.84
N510Q4.009	.7	.0	22.3	.0	.14	150.0	-75.0	5.0	1.9	0.	0.	194.	0.	0.	3.40
N510Q4.010	.4	.0	21.2	.0	.08	150.0	-84.0	5.0	1.0	0.	0.	185.	0.	0.	1.89

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510Q5.004	.8	.0	15.0	.0	.16	150.0	.0	5.0	2.0	0.	0.	131.	0.	0.	3.94
N510Q5.005	1.0	.0	17.0	.0	.28	150.0	-28.0	5.0	2.6	0.	0.	148.	0.	0.	6.50
N510Q5.006	1.0	.0	17.4	.0	.27	150.0	-33.0	5.0	2.6	0.	0.	152.	0.	0.	6.36
N510Q5.007	1.0	26.1	26.1	26.2	.24	150.0	-50.0	5.0	2.7	0.	0.	227.	0.	0.	5.70
N510Q5.008	.8	.0	25.4	.0	.16	150.0	-56.0	5.0	2.2	0.	0.	221.	0.	0.	3.68
N510Q5.009	.7	.0	24.9	.0	.11	150.0	-75.0	5.0	1.8	0.	0.	217.	0.	0.	2.65
N510Q5.010	.5	.0	25.2	.0	.09	150.0	-84.0	5.0	1.3	0.	0.	220.	0.	0.	2.10
N510R1.004	.7	.0	24.2	.0	.10	150.0	.0	11.0	2.0	0.	0.	211.	0.	0.	2.73
N510R1.005	.7	.0	27.8	.0	.10	150.0	-28.0	11.0	1.8	0.	0.	242.	0.	0.	2.59
N510R1.006	.7	.0	19.4	.0	.11	150.0	-33.0	11.0	1.8	0.	0.	169.	0.	0.	2.58
N510R1.007	.6	.0	19.6	.0	.03	150.0	-50.0	11.0	1.7	0.	0.	171.	0.	0.	1.10
N510R1.008	.5	.0	20.7	.0	.03	150.0	-56.0	11.0	1.2	0.	0.	180.	0.	0.	.92
N510R1.009	.3	.0	21.3	.0	.04	150.0	-75.0	11.0	.8	0.	0.	186.	0.	0.	.99
N510R1.010	.3	.0	22.5	.0	.03	150.0	-84.0	11.0	.8	0.	0.	196.	0.	0.	.66
N510R2.004	.7	.0	25.2	.0	.13	150.0	.0	11.0	2.0	0.	0.	219.	0.	0.	3.42
N510R2.005	.9	.0	17.8	.0	.11	150.0	-28.0	11.0	2.3	0.	0.	155.	0.	0.	2.73
N510R2.006	1.0	.0	19.7	.0	.09	150.0	-33.0	11.0	2.5	0.	0.	172.	0.	0.	2.45
N510R2.007	.6	.0	21.2	.0	.00	150.0	-50.0	11.0	1.7	0.	0.	185.	0.	0.	.68
N510R2.008	.4	.0	20.9	.0	.01	150.0	-56.0	11.0	1.2	0.	0.	183.	0.	0.	.60
N510R2.009	.4	.0	24.3	.0	.04	150.0	-75.0	11.0	1.0	0.	0.	211.	0.	0.	1.10
N510R2.010	.4	.0	25.0	.0	.08	150.0	-84.0	11.0	.9	0.	0.	218.	0.	0.	1.80
N510R3.004	.8	.0	24.5	.0	.14	150.0	.0	11.0	2.2	0.	0.	213.	0.	0.	3.52
N510R3.005	.8	.0	26.4	.0	.11	150.0	-28.0	11.0	2.0	0.	0.	230.	0.	0.	2.85
N510R3.006	.8	.0	19.5	.0	.11	150.0	-33.0	11.0	2.2	0.	0.	170.	0.	0.	2.75
N510R3.007	.6	.0	30.2	.0	.07	150.0	-50.0	11.0	1.6	0.	0.	264.	0.	0.	1.70
N510R3.008	.7	.0	34.2	.0	.07	150.0	-56.0	11.0	1.8	0.	0.	298.	0.	0.	1.53
N510R3.009	.4	.0	34.6	.0	.05	150.0	-75.0	11.0	1.0	0.	0.	302.	0.	0.	1.21
N510R3.010	.3	.0	37.2	.0	.06	150.0	-84.0	11.0	.9	0.	0.	325.	0.	0.	1.45
N510R4.004	.7	.0	18.2	.0	.13	150.0	.0	11.0	1.9	0.	0.	159.	0.	0.	3.25
N510R4.005	.7	.0	19.0	.0	.11	150.0	-28.0	11.0	1.8	0.	0.	166.	0.	0.	2.86
N510R4.006	.8	.0	20.9	.0	.11	150.0	-33.0	11.0	2.2	0.	0.	182.	0.	0.	2.89
N510R4.007	.7	.0	21.0	.0	.03	150.0	-50.0	11.0	2.0	0.	0.	183.	0.	0.	1.17
N510R4.008	.6	.0	20.8	.0	.00	150.0	-56.0	11.0	1.6	0.	0.	181.	0.	0.	.45
N510R4.009	.3	.0	27.3	.0	.04	150.0	-75.0	11.0	.9	0.	0.	238.	0.	0.	1.11
N510R4.010	.5	.0	26.0	.0	.09	150.0	-84.0	11.0	1.4	0.	0.	227.	0.	0.	2.05
N510R5.004	.7	.0	20.0	.0	.15	150.0	.0	11.0	1.9	0.	0.	174.	0.	0.	3.67
N510R5.005	.9	.0	19.8	.0	.11	150.0	-28.0	11.0	2.3	0.	0.	173.	0.	0.	2.78
N510R5.006	1.0	.0	19.4	.0	.12	150.0	-33.0	11.0	2.6	0.	0.	169.	0.	0.	2.93
N510R5.007	.8	.0	21.5	.0	.09	150.0	-50.0	11.0	2.1	0.	0.	187.	0.	0.	2.08
N510R5.008	.6	.0	21.4	.0	.04	150.0	-56.0	11.0	1.7	0.	0.	186.	0.	0.	1.22
N510R5.009	.4	.0	33.0	.0	.09	150.0	-75.0	11.0	1.1	0.	0.	288.	0.	0.	2.13
N510R5.010	.4	.0	26.4	.0	.09	150.0	-84.0	11.0	1.0	0.	0.	230.	0.	0.	2.10

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510S1.004	.6	.0	31.8	.0	.08	150.0	.0	17.0	1.7	0.	0.	277.	0.	0.	2.29
N510S1.005	.4	.0	21.2	.0	-.04	150.0	-28.0	17.0	1.2	0.	0.	185.	0.	0.	.29
N510S1.006	.3	.0	26.8	.0	-.04	150.0	-33.0	17.0	.8	0.	0.	234.	0.	0.	.23
N510S1.007	.2	.0	.0	.0	-.05	150.0	-50.0	17.0	.5	0.	0.	0.	0.	0.	.07
N510S1.008	.1	.0	.0	.0	-.03	150.0	-56.0	17.0	.3	0.	0.	0.	0.	0.	.11
N510S1.009	.1	.0	.0	.0	-.02	150.0	-75.0	17.0	.2	0.	0.	0.	0.	0.	.13
N510S1.010	.1	.0	.0	.0	.02	150.0	-84.0	17.0	.2	0.	0.	0.	0.	0.	.48
N510S2.004	.6	.0	17.4	.0	.09	150.0	.0	17.0	1.6	0.	0.	151.	0.	0.	2.49
N510S2.005	.7	.0	22.1	.0	.08	150.0	-28.0	17.0	1.9	0.	0.	193.	0.	0.	1.88
N510S2.006	.6	.0	18.8	.0	.07	150.0	-33.0	17.0	1.6	0.	0.	164.	0.	0.	1.82
N510S2.007	.3	.0	30.8	.0	.01	150.0	-50.0	17.0	.7	0.	0.	269.	0.	0.	.49
N510S2.008	.3	.0	20.8	.0	.00	150.0	-56.0	17.0	.8	0.	0.	181.	0.	0.	.28
N510S2.009	.1	.0	.0	.0	.02	150.0	-75.0	17.0	.4	0.	0.	0.	0.	0.	.55
N510S2.010	.1	.0	.0	.0	.01	150.0	-84.0	17.0	.2	0.	0.	0.	0.	0.	.37
N510S3.004	.6	.0	30.0	.0	.06	150.0	.0	17.0	1.6	0.	0.	262.	0.	0.	1.98
N510S3.005	.3	.0	17.9	.0	.04	150.0	-28.0	17.0	.9	0.	0.	156.	0.	0.	1.07
N510S3.006	.4	.0	13.9	.0	.03	150.0	-33.0	17.0	1.2	0.	0.	121.	0.	0.	.73
N510S3.007	.4	.0	23.6	.0	.04	150.0	-50.0	17.0	1.0	0.	0.	206.	0.	0.	.94
N510S3.008	.2	.0	.0	.0	.02	150.0	-56.0	17.0	.5	0.	0.	0.	0.	0.	.50
N510S3.009	.1	.0	.0	.0	-.02	150.0	-75.0	17.0	.3	0.	0.	0.	0.	0.	.14
N510S3.010	.0	.0	.0	.0	.00	150.0	-84.0	17.0	.1	0.	0.	0.	0.	0.	.17
N510S4.004	.6	.0	22.0	.0	.06	150.0	.0	17.0	1.6	0.	0.	192.	0.	0.	1.98
N510S4.005	.4	.0	19.2	.0	.03	150.0	-28.0	17.0	1.1	0.	0.	167.	0.	0.	.70
N510S4.006	.5	.0	19.5	.0	.04	150.0	-33.0	17.0	1.4	0.	0.	170.	0.	0.	1.13
N510S4.007	.5	.0	19.5	.0	.08	150.0	-50.0	17.0	1.3	0.	0.	170.	0.	0.	1.78
N510S4.008	.3	.0	22.0	.0	.04	150.0	-56.0	17.0	.9	0.	0.	191.	0.	0.	.97
N510S4.009	.3	.0	20.9	.0	.03	150.0	-75.0	17.0	.8	0.	0.	182.	0.	0.	.87
N510S4.010	.1	.0	.0	.0	.02	150.0	-84.0	17.0	.2	0.	0.	0.	0.	0.	.56
N510S5.004	.8	.0	26.4	.0	.08	150.0	.0	17.0	2.1	0.	0.	230.	0.	0.	2.27
N510S5.005	.4	.0	28.9	.0	.01	150.0	-28.0	17.0	1.1	0.	0.	252.	0.	0.	.60
N510S5.006	.5	.0	25.1	.0	.02	150.0	-33.0	17.0	1.3	0.	0.	219.	0.	0.	.60
N510S5.007	.2	.0	.0	.0	.01	150.0	-50.0	17.0	.5	0.	0.	0.	0.	0.	.47
N510S5.008	.1	.0	.0	.0	-.01	150.0	-56.0	17.0	.3	0.	0.	0.	0.	0.	.20
N510S5.009	.1	.0	.0	.0	.01	150.0	-75.0	17.0	.3	0.	0.	0.	0.	0.	.34
N510S5.010	.0	.0	.0	.0	-.01	150.0	-84.0	17.0	.1	0.	0.	0.	0.	0.	.18
N510T1.004	.6	.0	21.8	.0	.09	250.0	75.0	1.0	1.6	0.	0.	190.	0.	0.	2.33
N510T1.005	.5	.0	19.9	.0	.10	250.0	66.0	1.0	1.4	0.	0.	174.	0.	0.	2.56
N510T1.006	.5	.0	35.5	.0	.13	250.0	56.0	1.0	1.3	0.	0.	310.	0.	0.	3.16
N510T1.007	.5	.0	19.2	.0	.15	250.0	44.0	1.0	1.3	0.	0.	167.	0.	0.	3.66
N510T1.008	.5	.0	25.8	.0	.19	250.0	33.0	1.0	1.5	0.	0.	225.	0.	0.	4.42
N510T1.009	.5	.0	19.8	.0	.20	250.0	22.0	1.0	1.4	0.	0.	173.	0.	0.	4.62
N510T1.010	.5	.0	26.5	.0	.17	250.0	.0	1.0	1.4	0.	0.	231.	0.	0.	4.05

FALCON 5: LSR = 100, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510T2.004	.1	.0	.0	.0	-.02	250.0	75.0	1.0	.3	0.	0.	0.	0.	0.	.17
N510T2.005	.1	.0	.0	.0	-.03	250.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.09
N510T2.006	.2	.0	.0	.0	-.02	250.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.23
N510T2.007	.5	.0	24.3	.0	.09	250.0	44.0	1.0	1.5	0.	0.	212.	0.	0.	2.24
N510T2.008	.6	.0	22.4	.0	.13	250.0	33.0	1.0	1.6	0.	0.	195.	0.	0.	3.09
N510T2.009	.8	.0	19.3	.0	.15	250.0	22.0	1.0	2.1	0.	0.	168.	0.	0.	3.66
N510T2.010	.6	.0	22.5	.0	.12	250.0	.0	1.0	1.7	0.	0.	196.	0.	0.	3.29
N510T3.004	.5	.0	23.2	.0	.05	250.0	75.0	1.0	1.3	0.	0.	202.	0.	0.	1.35
N510T3.005	.5	.0	22.8	.0	.17	250.0	66.0	1.0	1.5	0.	0.	199.	0.	0.	4.11
N510T3.006	.5	.0	22.8	.0	.19	250.0	56.0	1.0	1.2	0.	0.	199.	0.	0.	4.55
N510T3.007	.5	.0	31.6	.0	.23	250.0	44.0	1.0	1.4	0.	0.	275.	0.	0.	5.34
N510T3.008	.7	.0	22.9	.0	.17	250.0	33.0	1.0	1.8	0.	0.	199.	0.	0.	4.10
N510T3.009	.5	.0	38.9	.0	.23	250.0	22.0	1.0	1.5	0.	0.	339.	0.	0.	5.41
N510T3.010	.4	.0	30.6	.0	.19	250.0	.0	1.0	1.1	0.	0.	266.	0.	0.	4.41
N510T4.004	.4	.0	27.3	.0	.08	250.0	75.0	1.0	1.2	0.	0.	238.	0.	0.	2.11
N510T4.005	.6	.0	24.5	.0	.12	250.0	66.0	1.0	1.7	0.	0.	213.	0.	0.	2.89
N510T4.006	.7	.0	23.3	.0	.20	250.0	56.0	1.0	1.8	0.	0.	203.	0.	0.	4.72
N510T4.007	.6	.0	24.2	.0	.16	250.0	44.0	1.0	1.7	0.	0.	211.	0.	0.	3.97
N510T4.008	.6	.0	23.1	.0	.18	250.0	33.0	1.0	1.6	0.	0.	201.	0.	0.	4.17
N510T4.009	.7	.0	20.7	.0	.20	250.0	22.0	1.0	1.8	0.	0.	181.	0.	0.	4.73
N510T4.010	.5	.0	18.1	.0	.19	250.0	.0	1.0	1.3	0.	0.	158.	0.	0.	4.52
N510T5.004	.4	.0	23.9	.0	.02	250.0	75.0	1.0	1.0	0.	0.	208.	0.	0.	.92
N510T5.005	.6	.0	20.7	.0	.12	250.0	66.0	1.0	1.5	0.	0.	180.	0.	0.	2.78
N510T5.006	.6	.0	20.6	.0	.14	250.0	56.0	1.0	1.7	0.	0.	180.	0.	0.	3.53
N510T5.007	.6	.0	20.8	.0	.12	250.0	44.0	1.0	1.5	0.	0.	181.	0.	0.	3.01
N510T5.008	.6	.0	20.2	.0	.17	250.0	33.0	1.0	1.7	0.	0.	176.	0.	0.	3.93
N510T5.009	.6	.0	20.0	.0	.23	250.0	22.0	1.0	1.6	0.	0.	174.	0.	0.	5.48
N510T5.010	.4	.0	22.8	.0	.09	250.0	.0	1.0	1.1	0.	0.	198.	0.	0.	2.49
N510U1.004	.4	.0	24.1	.0	.06	250.0	75.0	5.0	1.2	0.	0.	210.	0.	0.	1.54
N510U1.005	.6	.0	22.3	.0	.06	250.0	66.0	5.0	1.7	0.	0.	194.	0.	0.	1.58
N510U1.006	.6	.0	22.1	.0	.08	250.0	56.0	5.0	1.6	0.	0.	193.	0.	0.	1.94
N510U1.007	.6	.0	19.1	.0	.11	250.0	44.0	5.0	1.7	0.	0.	166.	0.	0.	2.66
N510U1.008	.6	.0	22.8	.0	.11	250.0	33.0	5.0	1.5	0.	0.	199.	0.	0.	2.76
N510U1.009	.6	.0	18.6	.0	.12	250.0	22.0	5.0	1.7	0.	0.	162.	0.	0.	2.89
N510U1.010	.7	.0	18.1	.0	.13	250.0	.0	5.0	1.9	0.	0.	158.	0.	0.	3.07
N510U2.004	.4	.0	22.5	.0	.06	250.0	75.0	5.0	1.0	0.	0.	196.	0.	0.	1.63
N510U2.005	.5	.0	20.5	.0	.07	250.0	66.0	5.0	1.4	0.	0.	179.	0.	0.	1.79
N510U2.006	.4	.0	18.6	.0	.06	250.0	56.0	5.0	1.1	0.	0.	162.	0.	0.	1.59
N510U2.007	.6	.0	21.1	.0	.09	250.0	44.0	5.0	1.5	0.	0.	184.	0.	0.	2.20
N510U2.008	.5	.0	18.8	.0	.14	250.0	33.0	5.0	1.3	0.	0.	164.	0.	0.	3.29
N510U2.009	.8	.0	20.7	.0	.17	250.0	22.0	5.0	2.1	0.	0.	180.	0.	0.	3.95
N510U2.010	.5	.0	20.7	.0	.14	250.0	.0	5.0	1.4	0.	0.	181.	0.	0.	3.26

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510U3.004	.6	.0	26.0	.0	.10	250.0	75.0	5.0	1.6	0.	0.	227.	0.	0.	2.48
N510U3.005	.5	.0	24.6	.0	.10	250.0	66.0	5.0	1.5	0.	0.	214.	0.	0.	2.30
N510U3.006	.6	.0	20.0	.0	.09	250.0	56.0	5.0	1.6	0.	0.	174.	0.	0.	2.22
N510U3.007	.6	.0	17.0	.0	.12	250.0	44.0	5.0	1.7	0.	0.	148.	0.	0.	2.91
N510U3.008	.7	.0	20.9	.0	.16	250.0	33.0	5.0	1.8	0.	0.	182.	0.	0.	3.78
N510U3.009	.6	.0	16.9	.0	.16	250.0	22.0	5.0	1.6	0.	0.	148.	0.	0.	3.88
N510U3.010	.6	.0	30.1	.0	.16	250.0	.0	5.0	1.5	0.	0.	262.	0.	0.	3.80
N510U4.004	.6	.0	20.0	.0	.10	250.0	75.0	5.0	1.7	0.	0.	175.	0.	0.	2.40
N510U4.005	.6	.0	19.7	.0	.11	250.0	66.0	5.0	1.6	0.	0.	172.	0.	0.	2.49
N510U4.006	.7	.0	21.1	.0	.13	250.0	56.0	5.0	1.8	0.	0.	184.	0.	0.	2.99
N510U4.007	.6	.0	24.2	.0	.12	250.0	44.0	5.0	1.7	0.	0.	211.	0.	0.	2.93
N510U4.008	.7	.0	19.1	.0	.14	250.0	33.0	5.0	1.8	0.	0.	167.	0.	0.	3.36
N510U4.009	.6	.0	19.9	.0	.19	250.0	22.0	5.0	1.7	0.	0.	174.	0.	0.	4.40
N510U4.010	.6	.0	25.3	.0	.17	250.0	.0	5.0	1.6	0.	0.	220.	0.	0.	3.98
N510U5.004	.9	.0	20.4	.0	.11	250.0	75.0	5.0	2.5	0.	0.	178.	0.	0.	2.64
N510U5.005	.7	.0	20.2	.0	.10	250.0	66.0	5.0	1.9	0.	0.	176.	0.	0.	2.40
N510U5.006	.6	.0	20.1	.0	.07	250.0	56.0	5.0	1.7	0.	0.	175.	0.	0.	1.91
N510U5.007	.6	.0	19.8	.0	.11	250.0	44.0	5.0	1.6	0.	0.	173.	0.	0.	2.67
N510U5.008	.6	.0	20.2	.0	.13	250.0	33.0	5.0	1.7	0.	0.	176.	0.	0.	3.08
N510U5.009	.6	.0	20.1	.0	.16	250.0	22.0	5.0	1.7	0.	0.	176.	0.	0.	3.87
N510U5.010	.8	.0	20.5	.0	.15	250.0	.0	5.0	2.0	0.	0.	178.	0.	0.	3.62
N510V1.004	.5	.0	20.0	.0	.02	250.0	75.0	11.0	1.4	0.	0.	175.	0.	0.	.82
N510V1.005	.6	.0	20.1	.0	.03	250.0	66.0	11.0	1.5	0.	0.	175.	0.	0.	.90
N510V1.006	.4	.0	19.2	.0	.05	250.0	56.0	11.0	1.1	0.	0.	167.	0.	0.	1.08
N510V1.007	.4	.0	18.4	.0	.04	250.0	44.0	11.0	1.1	0.	0.	161.	0.	0.	1.10
N510V1.008	.5	.0	20.0	.0	.03	250.0	33.0	11.0	1.3	0.	0.	175.	0.	0.	1.12
N510V1.009	.5	.0	19.9	.0	.05	250.0	22.0	11.0	1.4	0.	0.	173.	0.	0.	1.49
N510V1.010	.4	.0	18.3	.0	.07	250.0	.0	11.0	1.2	0.	0.	160.	0.	0.	1.86
N510V2.004	.5	.0	22.7	.0	.03	250.0	75.0	11.0	1.3	0.	0.	198.	0.	0.	.96
N510V2.005	.4	.0	32.5	.0	.06	250.0	66.0	11.0	1.1	0.	0.	283.	0.	0.	1.45
N510V2.006	.6	.0	19.3	.0	.05	250.0	56.0	11.0	1.6	0.	0.	168.	0.	0.	1.24
N510V2.007	.6	.0	19.4	.0	.03	250.0	44.0	11.0	1.7	0.	0.	169.	0.	0.	.68
N510V2.008	.4	.0	27.7	.0	.03	250.0	33.0	11.0	1.2	0.	0.	242.	0.	0.	1.05
N510V2.009	.5	.0	27.8	.0	.08	250.0	22.0	11.0	1.4	0.	0.	242.	0.	0.	1.94
N510V2.010	.6	.0	16.5	.0	.08	250.0	.0	11.0	1.5	0.	0.	144.	0.	0.	2.14
N510V3.004	.4	.0	24.6	.0	.01	250.0	75.0	11.0	1.0	0.	0.	214.	0.	0.	.49
N510V3.005	.4	.0	20.9	.0	.02	250.0	66.0	11.0	1.2	0.	0.	182.	0.	0.	.44
N510V3.006	.5	.0	22.0	.0	.03	250.0	56.0	11.0	1.3	0.	0.	192.	0.	0.	.78
N510V3.007	.4	.0	18.8	.0	.03	250.0	44.0	11.0	1.1	0.	0.	164.	0.	0.	.84
N510V3.008	.4	.0	18.6	.0	.03	250.0	33.0	11.0	1.0	0.	0.	162.	0.	0.	.94
N510V3.009	.5	.0	30.7	.0	.03	250.0	22.0	11.0	1.4	0.	0.	267.	0.	0.	1.03
N510V3.010	.5	.0	32.8	.0	.06	250.0	.0	11.0	1.3	0.	0.	286.	0.	0.	1.80

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510V4.004	.5	.0	21.5	.0	.04	250.0	75.0	11.0	1.3	0.	0.	188.	0.	0.	1.11
N510V4.005	.5	.0	20.9	.0	.05	250.0	66.0	11.0	1.4	0.	0.	182.	0.	0.	1.31
N510V4.006	.5	.0	19.2	.0	.07	250.0	56.0	11.0	1.2	0.	0.	168.	0.	0.	1.65
N510V4.007	.5	.0	19.7	.0	.05	250.0	44.0	11.0	1.4	0.	0.	171.	0.	0.	1.12
N510V4.008	.4	.0	16.6	.0	.08	250.0	33.0	11.0	1.1	0.	0.	145.	0.	0.	1.99
N510V4.009	.5	.0	19.8	.0	.09	250.0	22.0	11.0	1.4	0.	0.	173.	0.	0.	2.21
N510V4.010	.5	.0	24.6	.0	.08	250.0	.0	11.0	1.5	0.	0.	214.	0.	0.	2.14
N510V5.004	.5	.0	20.5	.0	.03	250.0	75.0	11.0	1.3	0.	0.	179.	0.	0.	.70
N510V5.005	.3	.0	29.6	.0	.01	250.0	66.0	11.0	.9	0.	0.	258.	0.	0.	.40
N510V5.006	.4	.0	15.9	.0	.02	250.0	56.0	11.0	1.0	0.	0.	138.	0.	0.	.64
N510V5.007	.4	.0	17.8	.0	.00	250.0	44.0	11.0	1.2	0.	0.	156.	0.	0.	.45
N510V5.008	.4	.0	29.7	.0	.03	250.0	33.0	11.0	1.2	0.	0.	259.	0.	0.	1.01
N510V5.009	.5	.0	26.5	.0	.04	250.0	22.0	11.0	1.4	0.	0.	231.	0.	0.	1.17
N510V5.010	.5	.0	35.1	.0	.04	250.0	.0	11.0	1.3	0.	0.	306.	0.	0.	1.32
N510W1.004	.1	.0	.0	.0	-.06	250.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.02
N510W1.005	.0	.0	.0	.0	-.05	250.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.04
N510W1.006	.3	.0	40.5	.0	-.03	250.0	56.0	17.0	.7	0.	0.	353.	0.	0.	.14
N510W1.007	.6	.0	20.6	.0	.01	250.0	44.0	17.0	1.6	0.	0.	180.	0.	0.	.62
N510W1.008	.3	.0	20.6	.0	.00	250.0	33.0	17.0	.9	0.	0.	179.	0.	0.	.52
N510W1.009	.2	.0	40.3	.0	.00	250.0	22.0	17.0	.7	0.	0.	352.	0.	0.	.48
N510W1.010	.3	.0	33.5	.0	-.02	250.0	.0	17.0	.8	0.	0.	292.	0.	0.	.57
N510W2.004	.3	.0	23.4	.0	.00	250.0	75.0	17.0	.8	0.	0.	204.	0.	0.	.29
N510W2.005	.4	.0	23.2	.0	-.01	250.0	66.0	17.0	1.0	0.	0.	203.	0.	0.	.24
N510W2.006	.4	.0	20.7	.0	.02	250.0	56.0	17.0	1.1	0.	0.	181.	0.	0.	.57
N510W2.007	.4	.0	19.2	.0	.01	250.0	44.0	17.0	1.0	0.	0.	167.	0.	0.	.47
N510W2.008	.3	.0	21.0	.0	.01	250.0	33.0	17.0	.8	0.	0.	183.	0.	0.	.30
N510W2.009	.4	.0	28.0	.0	-.02	250.0	22.0	17.0	1.0	0.	0.	244.	0.	0.	.31
N510W2.010	.3	.0	39.3	.0	-.03	250.0	.0	17.0	.8	0.	0.	342.	0.	0.	.54
N510W3.004	.2	.0	23.6	.0	.00	250.0	75.0	17.0	.6	0.	0.	206.	0.	0.	.33
N510W3.005	.2	.0	22.3	.0	.01	250.0	66.0	17.0	.6	0.	0.	195.	0.	0.	.25
N510W3.006	.3	.0	22.4	.0	.02	250.0	56.0	17.0	.9	0.	0.	195.	0.	0.	.75
N510W3.007	.2	.0	14.7	.0	.02	250.0	44.0	17.0	.6	0.	0.	128.	0.	0.	.68
N510W3.008	.3	.0	14.8	.0	.02	250.0	33.0	17.0	.8	0.	0.	129.	0.	0.	.48
N510W3.009	.4	.0	49.0	.0	.00	250.0	22.0	17.0	1.1	0.	0.	427.	0.	0.	.56
N510W3.010	.3	.0	50.0	.0	-.02	250.0	.0	17.0	.8	0.	0.	436.	0.	0.	.55
N510W4.004	.5	.0	22.2	.0	.00	250.0	75.0	17.0	1.4	0.	0.	194.	0.	0.	.46
N510W4.005	.6	.0	19.8	.0	.02	250.0	66.0	17.0	1.5	0.	0.	173.	0.	0.	.58
N510W4.006	.3	.0	17.3	.0	.02	250.0	56.0	17.0	.8	0.	0.	151.	0.	0.	.48
N510W4.007	.4	.0	17.9	.0	.01	250.0	44.0	17.0	1.0	0.	0.	156.	0.	0.	.37
N510W4.008	.2	.0	.0	.0	.02	250.0	33.0	17.0	.5	0.	0.	0.	0.	0.	.49
N510W4.009	.4	.0	16.6	.0	.03	250.0	22.0	17.0	1.0	0.	0.	145.	0.	0.	1.01
N510W4.010	.5	.0	30.6	.0	.00	250.0	.0	17.0	1.3	0.	0.	267.	0.	0.	.79

FALCON 5: LSR = 100, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N510W5.004	.3	.0	21.1	.0	.01	250.0	75.0	17.0	.8	0.	0.	184.	0.	0.	.28
N510W5.005	.2	.0	25.8	.0	.01	250.0	66.0	17.0	.6	0.	0.	225.	0.	0.	.23
N510W5.006	.3	.0	24.9	.0	.02	250.0	56.0	17.0	.8	0.	0.	217.	0.	0.	.37
N510W5.007	.4	.0	18.4	.0	.01	250.0	44.0	17.0	1.1	0.	0.	160.	0.	0.	.48
N510W5.008	.3	.0	20.0	.0	.01	250.0	33.0	17.0	.9	0.	0.	174.	0.	0.	.31
N510W5.009	.4	.0	20.3	.0	.01	250.0	22.0	17.0	1.0	0.	0.	177.	0.	0.	.62
N510W5.010	.5	.0	30.0	.0	-.01	250.0	.0	17.0	1.2	0.	0.	262.	0.	0.	.67

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N515A1.009	3.2	5.7	10.9	48.2	.20	-62.0	30.0	2.0	8.2	91.	0.	117.	0.	218.	6.73
N515A1.008	23.5	.6	9.0	119.1	5.31	-62.0	20.0	2.0	45.4	19.	19.	96.	456.	971.	126.34
N515A1.007	24.5	.6	8.4	109.2	5.40	-62.0	10.0	2.0	46.7	11.	18.	90.	494.	787.	132.06
N515A1.006	21.9	1.3	7.6	103.5	5.93	-62.0	.0	2.0	43.1	15.	24.	81.	534.	871.	143.82
N515A1.005	20.9	2.4	8.6	102.1	5.12	-62.0	-10.0	2.0	41.6	30.	35.	92.	446.	801.	125.50
N515A1.004	20.0	3.0	8.7	97.1	4.80	-62.0	-20.0	2.0	40.4	33.	33.	93.	461.	788.	117.12
N515A2.009	3.2	6.0	9.5	56.5	.39	-62.0	30.0	2.0	8.3	82.	0.	102.	0.	381.	11.26
N515A2.008	23.8	1.0	10.9	104.2	6.06	-62.0	20.0	2.0	45.8	15.	16.	117.	486.	1112.	141.82
N515A2.007	23.6	.8	9.2	119.8	5.76	-62.0	10.0	2.0	45.5	9.	20.	98.	553.	964.	140.36
N515A2.006	23.6	1.3	9.6	118.8	6.63	-62.0	.0	2.0	45.5	14.	15.	103.	536.	934.	158.43
N515A2.005	24.2	2.1	9.4	119.4	5.73	-62.0	-10.0	2.0	46.3	23.	24.	100.	629.	1205.	139.84
N515A2.004	23.9	3.2	9.9	117.9	5.40	-62.0	-20.0	2.0	45.9	35.	36.	105.	477.	1256.	129.78
N515A3.009	3.4	5.6	15.9	46.2	.28	-62.0	30.0	2.0	8.8	94.	0.	170.	0.	349.	8.65
N515A3.008	27.0	.6	9.4	117.7	6.76	-62.0	20.0	2.0	50.0	11.	13.	100.	566.	946.	158.12
N515A3.007	27.4	.4	8.5	118.5	6.45	-62.0	10.0	2.0	50.4	5.	20.	91.	633.	907.	154.23
N515A3.006	25.8	1.0	8.2	115.8	7.04	-62.0	.0	2.0	48.5	11.	18.	87.	612.	1197.	166.16
N515A3.005	23.3	1.8	9.0	97.2	5.39	-62.0	-10.0	2.0	45.1	21.	23.	96.	506.	795.	132.69
N515A3.004	23.9	2.0	8.8	110.2	6.19	-62.0	-20.0	2.0	46.0	22.	23.	94.	608.	998.	147.29
N515A4.009	2.4	6.4	26.4	55.1	.40	-62.0	30.0	2.0	6.3	105.	0.	282.	0.	382.	11.42
N515A4.008	25.9	.8	9.3	120.2	7.52	-62.0	20.0	2.0	48.6	9.	15.	100.	783.	790.	172.36
N515A4.007	27.4	.6	8.9	101.9	6.83	-62.0	10.0	2.0	50.4	6.	6.	95.	659.	876.	162.60
N515A4.006	24.8	1.1	8.6	114.2	7.49	-62.0	.0	2.0	47.1	13.	15.	92.	647.	916.	175.94
N515A4.005	22.9	1.9	8.6	105.2	6.20	-62.0	-10.0	2.0	44.5	21.	23.	92.	598.	924.	149.63
N515A4.004	24.2	1.2	9.9	116.5	6.58	-62.0	-20.0	2.0	46.3	17.	38.	106.	570.	970.	153.73
N515A5.009	3.3	5.1	7.0	50.6	.33	-62.0	30.0	2.0	8.4	74.	0.	75.	0.	265.	9.82
N515A5.008	26.3	.8	9.6	117.8	6.78	-62.0	20.0	2.0	49.1	9.	16.	102.	603.	791.	156.74
N515A5.007	27.6	.4	9.1	117.9	6.54	-62.0	10.0	2.0	50.7	4.	15.	97.	546.	1200.	156.70
N515A5.006	24.8	1.2	8.6	119.8	6.80	-62.0	.0	2.0	47.1	13.	16.	92.	557.	1099.	161.23
N515A5.005	23.2	2.0	10.0	111.8	5.98	-62.0	-10.0	2.0	45.0	24.	28.	107.	556.	806.	144.88
N515A5.004	25.4	3.1	8.7	119.6	6.11	-62.0	-20.0	2.0	47.9	33.	36.	93.	568.	1187.	144.45
N515B1.009	2.5	7.2	10.0	28.6	.25	-32.0	30.0	1.0	6.4	77.	0.	107.	0.	152.	7.33
N515B1.008	24.7	1.4	9.5	107.1	5.27	-32.0	20.0	1.0	46.9	15.	16.	102.	415.	859.	126.06
N515B1.007	33.0	.1	7.8	119.7	6.32	-32.0	10.0	1.0	57.1	1.	1.	83.	478.	856.	148.87
N515B1.006	31.0	.2	8.4	100.9	5.72	-32.0	.0	1.0	54.9	2.	2.	90.	502.	567.	131.63
N515B1.005	28.7	.2	8.4	73.3	3.58	-32.0	-10.0	1.0	52.1	2.	2.	90.	257.	466.	83.17
N515B1.004	32.8	.7	8.4	111.5	5.13	-32.0	-20.0	1.0	56.9	7.	8.	90.	548.	899.	121.72
N515B2.009	2.8	8.8	11.5	39.5	.33	-32.0	30.0	1.0	7.3	119.	0.	123.	0.	127.	9.41
N515B2.008	26.6	1.1	9.0	76.5	4.77	-32.0	20.0	1.0	49.4	12.	26.	96.	449.	767.	116.23
N515B2.007	32.7	.1	8.5	118.0	5.91	-32.0	10.0	1.0	56.8	1.	2.	91.	470.	783.	136.70
N515B2.006	31.7	.2	7.2	112.3	5.63	-32.0	.0	1.0	55.6	2.	2.	77.	433.	792.	128.79
N515B2.005	31.9	.1	7.8	100.9	3.49	-32.0	-10.0	1.0	55.9	1.	2.	83.	329.	439.	81.52
N515B2.004	32.5	.5	8.3	87.6	5.26	-32.0	-20.0	1.0	56.6	6.	7.	89.	441.	792.	124.06

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N515B3.009	2.9	7.5	10.1	19.2	.25	-32.0	30.0	1.0	7.4	107.	0.	108.	0.	147.	7.48
N515B3.008	25.5	1.2	10.0	113.8	5.48	-32.0	20.0	1.0	48.1	14.	15.	106.	549.	740.	132.72
N515B3.007	34.2	.1	7.5	103.6	6.55	-32.0	10.0	1.0	58.4	1.	1.	80.	620.	870.	153.79
N515B3.006	31.1	.2	8.5	78.7	6.60	-32.0	.0	1.0	54.9	2.	2.	91.	474.	810.	151.53
N515B3.005	30.9	.1	8.1	88.9	4.52	-32.0	-10.0	1.0	54.7	1.	6.	86.	442.	705.	104.44
N515B3.004	35.0	.5	8.2	95.4	5.18	-32.0	-20.0	1.0	59.3	5.	12.	88.	536.	736.	121.63
N515B4.009	1.9	9.0	10.3	36.5	.34	-32.0	30.0	1.0	4.9	0.	0.	110.	0.	0.	9.73
N515B4.008	28.1	1.3	9.9	101.0	6.17	-32.0	20.0	1.0	51.4	17.	18.	105.	574.	755.	144.20
N515B4.007	33.8	.1	8.0	90.3	6.43	-32.0	10.0	1.0	58.0	1.	1.	85.	513.	703.	147.95
N515B4.006	32.4	.2	7.2	92.5	6.20	-32.0	.0	1.0	56.4	2.	2.	77.	487.	829.	141.95
N515B4.005	31.7	.1	8.4	81.1	4.16	-32.0	-10.0	1.0	55.6	1.	5.	89.	359.	434.	94.19
N515B4.004	32.8	.8	8.5	81.8	5.53	-32.0	-20.0	1.0	56.9	10.	13.	91.	417.	872.	127.46
N515B5.009	1.9	8.3	13.6	39.1	.35	-32.0	30.0	1.0	5.1	145.	0.	145.	0.	146.	10.02
N515B5.008	26.9	1.3	8.9	87.4	5.25	-32.0	20.0	1.0	49.8	16.	20.	95.	480.	727.	129.37
N515B5.007	35.4	.1	8.4	108.5	7.02	-32.0	10.0	1.0	59.7	1.	1.	90.	626.	1068.	162.96
N515B5.006	32.5	.2	8.0	97.5	6.54	-32.0	.0	1.0	56.6	2.	2.	85.	520.	648.	149.92
N515B5.005	35.7	.1	8.3	79.5	4.01	-32.0	-10.0	1.0	60.0	1.	2.	88.	419.	637.	93.07
N515B5.004	32.8	.4	8.3	103.9	5.44	-32.0	-20.0	1.0	56.9	4.	6.	89.	520.	783.	128.66
N515C1.009	2.2	9.4	19.9	39.2	.22	-2.0	30.0	1.0	5.6	120.	0.	212.	0.	213.	6.50
N515C1.008	13.9	2.5	9.1	89.9	3.47	-2.0	20.0	1.0	30.3	30.	31.	97.	472.	937.	90.53
N515C1.007	14.6	2.6	10.1	85.0	1.79	-2.0	10.0	1.0	31.5	30.	32.	108.	361.	651.	46.52
N515C1.006	17.2	2.1	9.5	74.1	1.52	-2.0	.0	1.0	36.0	23.	26.	102.	186.	552.	39.65
N515C1.005	13.8	2.0	9.9	74.1	1.35	-2.0	-10.0	1.0	30.2	28.	30.	105.	193.	222.	35.72
N515C1.004	16.3	2.8	9.9	79.7	1.99	-2.0	-20.0	1.0	34.5	38.	53.	105.	260.	558.	51.96
N515C2.009	2.5	8.2	28.5	37.8	.36	-2.0	30.0	1.0	6.5	150.	0.	304.	0.	305.	10.27
N515C2.008	18.6	.1	14.6	91.6	4.98	-2.0	20.0	1.0	38.2	16.	32.	156.	581.	977.	124.47
N515C2.007	20.3	1.5	14.7	90.0	2.93	-2.0	10.0	1.0	40.7	17.	22.	156.	710.	937.	72.35
N515C2.006	20.5	1.0	14.9	78.3	2.74	-2.0	.0	1.0	41.0	18.	24.	159.	282.	381.	67.19
N515C2.005	18.9	1.4	11.0	87.4	2.63	-2.0	-10.0	1.0	38.6	17.	18.	117.	273.	931.	64.66
N515C2.004	16.3	1.7	15.2	87.6	3.44	-2.0	-20.0	1.0	34.4	19.	42.	162.	470.	862.	86.05
N515C3.009	3.2	10.0	15.0	38.8	.34	-2.0	30.0	1.0	8.1	160.	0.	160.	0.	161.	9.74
N515C3.008	18.8	.1	10.5	91.4	4.77	-2.0	20.0	1.0	38.5	13.	26.	112.	677.	962.	118.72
N515C3.007	22.0	1.0	9.9	89.1	2.29	-2.0	10.0	1.0	43.3	25.	30.	105.	468.	526.	58.32
N515C3.006	21.8	2.4	9.4	52.1	1.86	-2.0	.0	1.0	42.9	32.	35.	101.	248.	462.	46.78
N515C3.005	24.8	2.2	9.4	88.1	2.00	-2.0	-10.0	1.0	47.1	27.	28.	101.	296.	938.	49.86
N515C3.004	23.4	3.2	9.5	91.2	2.80	-2.0	-20.0	1.0	45.3	37.	41.	102.	306.	656.	70.47
N515C4.009	3.0	5.8	5.9	47.9	.45	-2.0	30.0	1.0	7.7	62.	0.	63.	0.	360.	12.89
N515C4.008	21.6	.1	14.0	89.7	5.85	-2.0	20.0	1.0	42.8	7.	20.	149.	621.	748.	139.71
N515C4.007	22.0	1.6	12.7	37.1	3.03	-2.0	10.0	1.0	43.2	18.	25.	135.	395.	396.	87.43
N515C4.006	22.7	2.0	12.7	72.9	3.20	-2.0	.0	1.0	44.3	23.	27.	135.	357.	448.	75.49
N515C4.005	21.8	1.8	12.6	80.4	3.11	-2.0	-10.0	1.0	42.9	26.	32.	134.	352.	388.	74.61
N515C4.004	20.3	2.1	15.9	87.3	4.06	-2.0	-20.0	1.0	40.8	33.	35.	169.	367.	776.	99.64

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N515C5.009	3.7	3.9	16.9	40.9	.27	-2.0	30.0	1.0	9.3	42.	0.	180.	0.	181.	8.46
N515C5.008	20.3	.1	12.4	90.2	4.73	-2.0	20.0	1.0	40.8	16.	28.	132.	526.	883.	116.69
N515C5.007	22.2	2.4	12.6	78.2	3.59	-2.0	10.0	1.0	43.6	27.	27.	134.	412.	612.	85.37
N515C5.006	20.8	2.1	10.9	76.1	2.99	-2.0	.0	1.0	41.6	23.	24.	117.	345.	597.	72.69
N515C5.005	20.4	2.3	12.6	77.9	2.84	-2.0	-10.0	1.0	40.9	32.	46.	135.	338.	830.	69.96
N515C5.004	19.0	2.6	12.7	90.7	3.41	-2.0	-20.0	1.0	38.7	30.	53.	136.	444.	645.	84.47
F515D1.007	.1	.0	.0	.0	.00	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.26
F515D1.008	.5	.0	41.3	.0	.03	50.0	50.0	1.0	1.3	0.	0.	441.	0.	0.	.83
F515D1.009	.9	.0	19.6	.0	.02	50.0	33.0	1.0	2.3	0.	0.	209.	0.	0.	.80
F515D1.010	.9	.0	12.7	.0	.21	50.0	.0	1.0	2.4	0.	0.	135.	0.	0.	6.02
F515D1.011	1.5	10.3	10.5	31.8	.26	50.0	-33.0	1.0	3.9	0.	0.	112.	0.	0.	7.31
F515D1.012	.8	.0	23.0	.0	.07	50.0	-50.0	1.0	2.2	0.	0.	245.	0.	0.	2.28
F515D2.007	1.7	37.8	37.8	37.8	.01	50.0	66.0	1.0	4.4	0.	0.	403.	0.	0.	.52
F515D2.008	.1	.0	.0	.0	.01	50.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.52
F515D2.009	.8	.0	13.5	.0	.03	50.0	33.0	1.0	2.1	0.	0.	144.	0.	0.	.98
F515D2.010	.8	.0	20.7	.0	.18	50.0	.0	1.0	2.1	0.	0.	221.	0.	0.	5.09
F515D2.011	1.5	7.9	13.0	29.1	.30	50.0	-33.0	1.0	4.0	0.	0.	139.	0.	0.	8.52
F515D2.012	.8	.0	14.9	.0	.00	50.0	-50.0	1.0	2.1	0.	0.	159.	0.	0.	1.19
F515D3.007	.2	.0	.0	.0	.02	50.0	66.0	1.0	.5	0.	0.	0.	0.	0.	.90
F515D3.008	.3	.0	22.6	.0	.01	50.0	50.0	1.0	.9	0.	0.	241.	0.	0.	.55
F515D3.009	.5	.0	21.9	.0	.01	50.0	33.0	1.0	1.3	0.	0.	234.	0.	0.	.56
F515D3.010	.9	.0	22.8	.0	.20	50.0	.0	1.0	2.5	0.	0.	244.	0.	0.	5.84
F515D3.011	1.7	7.4	7.8	25.8	.14	50.0	-33.0	1.0	4.5	0.	0.	84.	0.	0.	4.04
F515D3.012	1.6	7.9	8.0	8.0	.11	50.0	-50.0	1.0	4.3	0.	0.	85.	0.	0.	3.13
F515D4.007	.2	.0	.0	.0	-.01	50.0	66.0	1.0	.5	0.	0.	0.	0.	0.	.28
F515D4.008	.1	.0	.0	.0	-.03	50.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.12
F515D4.009	.5	.0	16.5	.0	.03	50.0	33.0	1.0	1.5	0.	0.	176.	0.	0.	1.06
F515D4.010	1.2	22.4	22.7	23.0	.20	50.0	.0	1.0	3.3	0.	0.	242.	0.	0.	5.88
F515D4.011	1.4	8.7	18.4	27.9	.18	50.0	-33.0	1.0	3.6	0.	0.	196.	0.	0.	5.19
F515D4.012	1.1	18.8	18.9	19.2	.16	50.0	-50.0	1.0	2.8	0.	0.	201.	0.	0.	4.64
F515D5.007	.3	.0	21.4	.0	.01	50.0	66.0	1.0	.7	0.	0.	228.	0.	0.	.49
F515D5.008	1.3	20.4	20.5	20.8	.05	50.0	50.0	1.0	3.4	0.	0.	219.	0.	0.	1.77
F515D5.009	1.2	17.7	19.9	19.9	.10	50.0	33.0	1.0	3.3	0.	0.	212.	0.	0.	2.99
F515D5.010	1.1	21.6	21.6	21.8	.21	50.0	.0	1.0	2.8	0.	0.	230.	0.	0.	6.11
F515D5.011	1.1	18.1	18.1	18.2	.17	50.0	-33.0	1.0	2.8	0.	0.	194.	0.	0.	4.75
F515D5.012	.8	.0	28.0	.0	.08	50.0	-50.0	1.0	2.1	0.	0.	299.	0.	0.	2.52
F515E1.007	.6	.0	17.8	.0	-.02	50.0	66.0	5.0	1.7	0.	0.	190.	0.	0.	.16
F515E1.008	1.2	21.1	21.2	21.4	.05	50.0	50.0	5.0	3.1	0.	0.	226.	0.	0.	1.43
F515E1.009	1.6	11.9	12.8	21.2	.08	50.0	33.0	5.0	4.2	0.	0.	137.	0.	0.	2.51
F515E1.010	.9	.0	27.0	.0	.16	50.0	.0	5.0	2.4	0.	0.	288.	0.	0.	4.60
F515E1.011	1.5	6.4	7.2	7.5	.09	50.0	-33.0	5.0	3.9	0.	0.	77.	0.	0.	3.15
F515E1.012	1.0	.0	12.3	.0	.05	50.0	-50.0	5.0	2.6	0.	0.	132.	0.	0.	1.51

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F515E2.007	.2	.0	.0	.0	-.01	50.0	66.0	5.0	.4	0.	0.	0.	0.	0.	.21
F515E2.008	.6	.0	23.1	.0	.01	50.0	50.0	5.0	1.7	0.	0.	247.	0.	0.	.56
F515E2.009	1.6	16.1	16.2	22.6	.09	50.0	33.0	5.0	4.2	0.	0.	172.	0.	0.	2.75
F515E2.010	.9	.0	23.9	.0	.20	50.0	.0	5.0	2.3	0.	0.	255.	0.	0.	5.82
F515E2.011	1.8	6.0	6.0	6.6	.06	50.0	-33.0	5.0	4.7	0.	0.	64.	0.	0.	2.07
F515E2.012	1.3	6.4	6.5	6.8	.00	50.0	-50.0	5.0	3.4	0.	0.	69.	0.	0.	.57
F515E3.007	.2	.0	.0	.0	.02	50.0	66.0	5.0	.5	0.	0.	0.	0.	0.	.65
F515E3.008	.1	.0	.0	.0	-.01	50.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.07
F515E3.009	1.1	11.1	11.1	11.2	.03	50.0	33.0	5.0	3.0	0.	0.	119.	0.	0.	1.13
F515E3.010	1.1	17.7	17.7	18.0	.19	50.0	.0	5.0	3.0	0.	0.	189.	0.	0.	5.37
F515E3.011	1.3	16.8	19.7	20.0	.05	50.0	-33.0	5.0	3.5	0.	0.	210.	0.	0.	2.15
F515E3.012	.8	.0	9.2	.0	.01	50.0	-50.0	5.0	2.2	0.	0.	99.	0.	0.	.83
F515E4.007	.1	.0	.0	.0	-.04	50.0	66.0	5.0	.3	0.	0.	0.	0.	0.	.07
F515E4.008	.2	.0	54.9	.0	.00	50.0	50.0	5.0	.6	0.	0.	587.	0.	0.	.36
F515E4.009	1.5	21.5	22.9	23.0	.00	50.0	33.0	5.0	4.1	0.	0.	244.	0.	0.	.56
F515E4.010	1.2	10.8	10.9	22.7	.20	50.0	.0	5.0	3.1	0.	0.	116.	0.	0.	5.71
F515E4.011	2.0	9.5	23.8	27.4	.16	50.0	-33.0	5.0	5.2	254.	0.	254.	0.	254.	4.81
F515E4.012	1.1	14.3	14.3	14.5	.11	50.0	-50.0	5.0	2.9	0.	0.	152.	0.	0.	3.16
F515E5.007	.1	.0	.0	.0	-.04	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.03
F515E5.008	.2	.0	25.8	.0	.06	50.0	50.0	5.0	.6	0.	0.	275.	0.	0.	1.60
F515E5.009	.7	.0	51.0	.0	-.16	50.0	33.0	5.0	1.8	0.	0.	545.	0.	0.	2.41
F515E5.010	.9	.0	29.6	.0	.16	50.0	.0	5.0	2.5	0.	0.	316.	0.	0.	4.74
F515E5.011	1.2	10.8	10.8	27.3	.16	50.0	-33.0	5.0	3.1	0.	0.	115.	0.	0.	4.65
F515E5.012	1.1	5.2	22.7	22.7	.10	50.0	-50.0	5.0	2.9	0.	0.	242.	0.	0.	2.81
F515F1.007	.2	.0	.0	.0	.00	50.0	66.0	11.0	.4	0.	0.	0.	0.	0.	.25
F515F1.008	.3	.0	44.0	.0	.01	50.0	50.0	11.0	.9	0.	0.	469.	0.	0.	.43
F515F1.009	1.3	11.1	11.1	11.2	.03	50.0	33.0	11.0	3.5	0.	0.	119.	0.	0.	1.12
F515F1.010	1.3	6.2	20.0	26.5	.17	50.0	.0	11.0	3.5	0.	0.	213.	0.	0.	5.45
F515F1.011	1.3	5.5	27.1	28.4	.12	50.0	-33.0	11.0	3.4	0.	0.	290.	0.	0.	3.55
F515F1.012	.9	.0	26.7	.0	.05	50.0	-50.0	11.0	2.3	0.	0.	285.	0.	0.	1.40
F515F2.007	.1	.0	.0	.0	-.05	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.00
F515F2.008	.7	.0	18.0	.0	-.04	50.0	50.0	11.0	1.9	0.	0.	192.	0.	0.	.14
F515F2.009	1.0	.0	13.6	.0	.03	50.0	33.0	11.0	2.6	0.	0.	146.	0.	0.	1.33
F515F2.010	1.4	10.4	26.6	32.1	.13	50.0	.0	11.0	3.6	0.	0.	284.	0.	0.	4.96
F515F2.011	1.3	16.4	16.6	20.8	.06	50.0	-33.0	11.0	3.5	0.	0.	177.	0.	0.	2.10
F515F2.012	.8	.0	7.8	.0	.10	50.0	-50.0	11.0	2.2	0.	0.	83.	0.	0.	2.94
F515F3.007	.2	.0	.0	.0	.02	50.0	66.0	11.0	.5	0.	0.	0.	0.	0.	.72
F515F3.008	1.1	21.2	21.3	21.3	.05	50.0	50.0	11.0	2.8	0.	0.	227.	0.	0.	1.39
F515F3.009	1.2	16.8	18.7	21.2	.11	50.0	33.0	11.0	3.2	0.	0.	200.	0.	0.	3.21
F515F3.010	1.6	3.9	20.5	42.0	.15	50.0	.0	11.0	4.1	0.	0.	219.	0.	0.	6.17
F515F3.011	1.3	11.8	11.8	20.9	.07	50.0	-33.0	11.0	3.5	0.	0.	126.	0.	0.	2.77
F515F3.012	1.1	16.2	16.3	16.4	.00	50.0	-50.0	11.0	2.8	0.	0.	174.	0.	0.	.54

FALCON 5: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F515F4.007	.1	.0	.0	.0	-.03	50.0	66.0	11.0	.2	0.	0.	0.	0.	0.	.04
F515F4.008	.7	.0	22.1	.0	.03	50.0	50.0	11.0	1.9	0.	0.	236.	0.	0.	.78
F515F4.009	.9	.0	14.2	.0	.06	50.0	33.0	11.0	2.4	0.	0.	152.	0.	0.	1.76
F515F4.010	1.1	31.3	31.3	31.4	.17	50.0	.0	11.0	3.0	0.	0.	334.	0.	0.	4.92
F515F4.011	1.4	18.1	26.9	39.4	.16	50.0	-33.0	11.0	3.6	0.	0.	287.	0.	0.	4.64
F515F4.012	1.3	19.2	19.2	19.3	-.03	50.0	-50.0	11.0	3.4	0.	0.	205.	0.	0.	.65
F515F5.007	.2	.0	.0	.0	.01	50.0	66.0	11.0	.4	0.	0.	0.	0.	0.	.34
F515F5.008	.3	.0	35.7	.0	.02	50.0	50.0	11.0	.8	0.	0.	381.	0.	0.	.79
F515F5.009	.7	.0	22.8	.0	.03	50.0	33.0	11.0	2.0	0.	0.	244.	0.	0.	1.19
F515F5.010	.9	.0	24.7	.0	.13	50.0	.0	11.0	2.3	0.	0.	264.	0.	0.	3.94
F515F5.011	1.3	9.3	17.0	30.6	.09	50.0	-33.0	11.0	3.4	0.	0.	182.	0.	0.	3.05
F515F5.012	1.0	25.5	25.5	25.6	.01	50.0	-50.0	11.0	2.7	0.	0.	272.	0.	0.	.64
F515G1.007	.2	.0	15.8	.0	.00	50.0	66.0	17.0	.6	0.	0.	169.	0.	0.	.21
F515G1.008	1.1	29.5	29.6	29.6	-.03	50.0	50.0	17.0	2.9	0.	0.	316.	0.	0.	.18
F515G1.009	1.4	18.7	18.8	25.6	.03	50.0	33.0	17.0	3.8	0.	0.	200.	0.	0.	1.24
F515G1.010	1.2	5.9	23.5	24.1	.14	50.0	.0	17.0	3.1	0.	0.	250.	0.	0.	4.19
F515G1.011	1.7	19.9	19.9	19.9	.00	50.0	-33.0	17.0	4.4	0.	0.	212.	0.	0.	.92
F515G1.012	.7	.0	33.4	.0	-.02	50.0	-50.0	17.0	1.8	0.	0.	357.	0.	0.	.16
F515G2.007	.1	.0	.0	.0	-.01	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.16
F515G2.008	.1	.0	.0	.0	.02	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.60
F515G2.009	1.1	18.3	30.0	30.1	.03	50.0	33.0	17.0	2.8	0.	0.	320.	0.	0.	.89
F515G2.010	1.1	22.6	22.6	22.8	.11	50.0	.0	17.0	2.8	0.	0.	241.	0.	0.	3.15
F515G2.011	1.3	7.1	7.2	9.5	.06	50.0	-33.0	17.0	3.4	0.	0.	77.	0.	0.	2.29
F515G2.012	1.0	.0	16.9	.0	.03	50.0	-50.0	17.0	2.6	0.	0.	181.	0.	0.	1.06
F515G3.007	.1	.0	.0	.0	.01	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.48
F515G3.008	.1	.0	.0	.0	.01	50.0	50.0	17.0	.2	0.	0.	0.	0.	0.	.37
F515G3.009	.9	.0	32.0	.0	.01	50.0	33.0	17.0	2.5	0.	0.	341.	0.	0.	.72
F515G3.010	.9	.0	17.6	.0	.04	50.0	.0	17.0	2.5	0.	0.	188.	0.	0.	1.61
F515G3.011	1.3	16.9	23.5	23.6	.08	50.0	-33.0	17.0	3.5	0.	0.	251.	0.	0.	2.99
F515G3.012	1.0	.0	25.7	.0	.06	50.0	-50.0	17.0	2.6	0.	0.	275.	0.	0.	1.71
F515G4.007	.1	.0	.0	.0	.01	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.44
F515G4.008	.1	.0	.0	.0	-.01	50.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.14
F515G4.009	1.2	14.0	14.0	14.1	.04	50.0	33.0	17.0	3.1	0.	0.	150.	0.	0.	1.19
F515G4.010	1.2	11.8	29.3	29.4	.14	50.0	.0	17.0	3.2	0.	0.	313.	0.	0.	4.27
F515G4.011	1.4	6.1	6.1	15.5	-.02	50.0	-33.0	17.0	3.6	0.	0.	65.	0.	0.	1.09
F515G4.012	.6	.0	41.5	.0	.01	50.0	-50.0	17.0	1.6	0.	0.	443.	0.	0.	.52
F515G5.007	.1	.0	.0	.0	.00	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.26
F515G5.008	.2	.0	38.3	.0	.03	50.0	50.0	17.0	.6	0.	0.	409.	0.	0.	.77
F515G5.009	.9	.0	26.6	.0	.00	50.0	33.0	17.0	2.4	0.	0.	284.	0.	0.	.68
F515G5.010	.9	.0	36.6	.0	.12	50.0	.0	17.0	2.3	0.	0.	391.	0.	0.	3.59
F515G5.011	1.2	16.1	18.1	27.3	.03	50.0	-33.0	17.0	3.2	0.	0.	193.	0.	0.	2.17
F515G5.012	1.1	27.9	27.9	28.0	.00	50.0	-50.0	17.0	2.9	0.	0.	298.	0.	0.	.51

FALCON 5: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F515H1.007	.1	.0	.0	.0	.04	150.0	84.0	1.0	.3	0.	0.	0.	0.	0.	1.05
F515H1.008	.1	.0	.0	.0	.01	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.47
F515H1.009	.1	.0	.0	.0	.03	150.0	56.0	1.0	.3	0.	0.	0.	0.	0.	.75
F515H1.010	.2	.0	.0	.0	.00	150.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.50
F515H1.011	.3	.0	22.8	.0	.04	150.0	28.0	1.0	.9	0.	0.	243.	0.	0.	1.23
F515H1.012	.4	.0	20.8	.0	.10	150.0	.0	1.0	1.1	0.	0.	222.	0.	0.	2.90
F515H2.007	.1	.0	.0	.0	.01	150.0	84.0	1.0	.2	0.	0.	0.	0.	0.	.44
F515H2.008	.1	.0	.0	.0	.00	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.28
F515H2.009	.1	.0	.0	.0	.02	150.0	56.0	1.0	.4	0.	0.	0.	0.	0.	.55
F515H2.010	.2	.0	.0	.0	.01	150.0	50.0	1.0	.5	0.	0.	0.	0.	0.	.66
F515H2.011	.6	.0	29.6	.0	.10	150.0	28.0	1.0	1.5	0.	0.	316.	0.	0.	2.96
F515H2.012	.6	.0	28.2	.0	.15	150.0	.0	1.0	1.6	0.	0.	301.	0.	0.	4.32
F515H3.007	.1	.0	.0	.0	.00	150.0	84.0	1.0	.3	0.	0.	0.	0.	0.	.24
F515H3.008	.1	.0	.0	.0	.03	150.0	75.0	1.0	.4	0.	0.	0.	0.	0.	.82
F515H3.009	.0	.0	.0	.0	-.03	150.0	56.0	1.0	.0	0.	0.	0.	0.	0.	.02
F515H3.010	.3	.0	60.6	.0	.01	150.0	50.0	1.0	.8	0.	0.	647.	0.	0.	.89
F515H3.011	.5	.0	22.3	.0	.08	150.0	28.0	1.0	1.3	0.	0.	238.	0.	0.	2.32
F515H3.012	.5	.0	23.9	.0	.08	150.0	.0	1.0	1.3	0.	0.	256.	0.	0.	2.30
F515H4.007	.0	.0	.0	.0	-.03	150.0	84.0	1.0	.1	0.	0.	0.	0.	0.	.06
F515H4.008	.1	.0	.0	.0	.02	150.0	75.0	1.0	.2	0.	0.	0.	0.	0.	.52
F515H4.009	.1	.0	.0	.0	.00	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.06
F515H4.010	.1	.0	.0	.0	.00	150.0	50.0	1.0	.3	0.	0.	0.	0.	0.	.40
F515H4.011	.4	.0	23.5	.0	.02	150.0	28.0	1.0	1.0	0.	0.	250.	0.	0.	.95
F515H4.012	.5	.0	25.8	.0	.12	150.0	.0	1.0	1.3	0.	0.	276.	0.	0.	3.47
F515H5.007	.1	.0	.0	.0	.00	150.0	84.0	1.0	.2	0.	0.	0.	0.	0.	.25
F515H5.008	.0	.0	.0	.0	-.01	150.0	75.0	1.0	.0	0.	0.	0.	0.	0.	.11
F515H5.009	.1	.0	.0	.0	.01	150.0	56.0	1.0	.2	0.	0.	0.	0.	0.	.41
F515H5.010	.2	.0	.0	.0	.02	150.0	50.0	1.0	.5	0.	0.	0.	0.	0.	.89
F515H5.011	.2	.0	27.3	.0	-.02	150.0	28.0	1.0	.5	0.	0.	291.	0.	0.	.29
F515H5.012	.4	.0	20.7	.0	.07	150.0	.0	1.0	1.0	0.	0.	221.	0.	0.	2.05
F515I1.007	1.1	43.8	43.8	43.8	.12	150.0	84.0	5.0	3.0	0.	0.	468.	0.	0.	4.51
F515I1.008	.1	.0	.0	.0	-.03	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.03
F515I1.009	.0	.0	.0	.0	-.02	150.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.01
F515I1.010	.1	.0	.0	.0	-.01	150.0	50.0	5.0	.4	0.	0.	0.	0.	0.	.18
F515I1.011	.4	.0	19.4	.0	.03	150.0	28.0	5.0	1.2	0.	0.	207.	0.	0.	1.01
F515I1.012	.5	.0	24.4	.0	.07	150.0	.0	5.0	1.4	0.	0.	261.	0.	0.	2.10
F515I2.007	.1	.0	.0	.0	-.07	150.0	84.0	5.0	.3	0.	0.	0.	0.	0.	.14
F515I2.008	.1	.0	.0	.0	.02	150.0	75.0	5.0	.4	0.	0.	0.	0.	0.	.55
F515I2.009	.1	.0	.0	.0	.01	150.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.26
F515I2.010	.2	.0	.0	.0	.03	150.0	50.0	5.0	.5	0.	0.	0.	0.	0.	.88
F515I2.011	.6	.0	16.8	.0	.02	150.0	28.0	5.0	1.5	0.	0.	180.	0.	0.	.79
F515I2.012	.3	.0	26.7	.0	-.03	150.0	.0	5.0	.8	0.	0.	285.	0.	0.	.38

FALCON 5: LSR = 150, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F515I3.007	.1	.0	.0	.0	.02	150.0	84.0	5.0	.3	0.	0.	0.	0.	0.	.50
F515I3.008	.1	.0	.0	.0	.00	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.23
F515I3.009	.1	.0	.0	.0	.01	150.0	56.0	5.0	.3	0.	0.	0.	0.	0.	.52
F515I3.010	.1	.0	.0	.0	.00	150.0	50.0	5.0	.3	0.	0.	0.	0.	0.	.20
F515I3.011	.5	.0	26.7	.0	.03	150.0	28.0	5.0	1.4	0.	0.	285.	0.	0.	1.17
F515I3.012	.6	.0	22.7	.0	.07	150.0	.0	5.0	1.7	0.	0.	242.	0.	0.	2.13
F515I4.007	.1	.0	.0	.0	-.01	150.0	84.0	5.0	.1	0.	0.	0.	0.	0.	.06
F515I4.008	.1	.0	.0	.0	.00	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.12
F515I4.009	.1	.0	.0	.0	-.01	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.12
F515I4.010	.2	.0	.0	.0	.00	150.0	50.0	5.0	.4	0.	0.	0.	0.	0.	.20
F515I4.011	.7	.0	23.9	.0	.04	150.0	28.0	5.0	1.8	0.	0.	255.	0.	0.	1.33
F515I4.012	.5	.0	26.2	.0	.06	150.0	.0	5.0	1.3	0.	0.	280.	0.	0.	1.79
F515I5.007	.1	.0	.0	.0	.01	150.0	84.0	5.0	.3	0.	0.	0.	0.	0.	.30
F515I5.008	.1	.0	.0	.0	-.02	150.0	75.0	5.0	.2	0.	0.	0.	0.	0.	.21
F515I5.009	.1	.0	.0	.0	.00	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.28
F515I5.010	.2	.0	53.0	.0	.01	150.0	50.0	5.0	.5	0.	0.	566.	0.	0.	.57
F515I5.011	.6	.0	20.9	.0	.05	150.0	28.0	5.0	1.6	0.	0.	223.	0.	0.	1.60
F515I5.012	.6	.0	23.9	.0	.09	150.0	.0	5.0	1.6	0.	0.	256.	0.	0.	2.56
F515J1.007	.1	.0	.0	.0	-.01	150.0	84.0	11.0	.3	0.	0.	0.	0.	0.	.32
F515J1.008	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.31
F515J1.009	.2	.0	.0	.0	.01	150.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.25
F515J1.010	.2	.0	.0	.0	.02	150.0	50.0	11.0	.4	0.	0.	0.	0.	0.	.72
F515J1.011	.4	.0	24.3	.0	.02	150.0	28.0	11.0	1.2	0.	0.	259.	0.	0.	.64
F515J1.012	.6	.0	31.7	.0	.09	150.0	.0	11.0	1.6	0.	0.	338.	0.	0.	2.93
F515J2.007	.1	.0	.0	.0	.02	150.0	84.0	11.0	.3	0.	0.	0.	0.	0.	.69
F515J2.008	.2	.0	.0	.0	.03	150.0	75.0	11.0	.5	0.	0.	0.	0.	0.	1.00
F515J2.009	.1	.0	.0	.0	.01	150.0	56.0	11.0	.4	0.	0.	0.	0.	0.	.27
F515J2.010	.2	.0	18.3	.0	.01	150.0	50.0	11.0	.6	0.	0.	196.	0.	0.	.36
F515J2.011	.4	.0	34.0	.0	.02	150.0	28.0	11.0	1.2	0.	0.	363.	0.	0.	.75
F515J2.012	1.0	24.3	24.4	24.4	.04	150.0	.0	11.0	2.7	0.	0.	260.	0.	0.	4.52
F515J3.007	.1	.0	.0	.0	.00	150.0	84.0	11.0	.4	0.	0.	0.	0.	0.	.46
F515J3.008	.0	.0	.0	.0	-.01	150.0	75.0	11.0	.0	0.	0.	0.	0.	0.	.03
F515J3.009	.1	.0	.0	.0	.02	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.51
F515J3.010	.2	.0	.0	.0	.00	150.0	50.0	11.0	.4	0.	0.	0.	0.	0.	.22
F515J3.011	.5	.0	36.6	.0	.03	150.0	28.0	11.0	1.4	0.	0.	391.	0.	0.	.90
F515J3.012	.5	.0	30.1	.0	.05	150.0	.0	11.0	1.3	0.	0.	321.	0.	0.	1.41
F515J4.007	.1	.0	.0	.0	.01	150.0	84.0	11.0	.3	0.	0.	0.	0.	0.	.29
F515J4.008	.1	.0	.0	.0	.02	150.0	75.0	11.0	.3	0.	0.	0.	0.	0.	.60
F515J4.009	.1	.0	.0	.0	.00	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.09
F515J4.010	.1	.0	.0	.0	-.02	150.0	50.0	11.0	.2	0.	0.	0.	0.	0.	.04
F515J4.011	.5	.0	31.0	.0	.02	150.0	28.0	11.0	1.4	0.	0.	331.	0.	0.	.81
F515J4.012	.5	.0	25.3	.0	.04	150.0	.0	11.0	1.2	0.	0.	270.	0.	0.	1.39

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F515J5.007	.1	.0	.0	.0	-.02	150.0	84.0	11.0	.2	0.	0.	0.	0.	0.	.06
F515J5.008	.1	.0	.0	.0	.00	150.0	75.0	11.0	.2	0.	0.	0.	0.	0.	.22
F515J5.009	.1	.0	.0	.0	.00	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.08
F515J5.010	.3	.0	27.3	.0	.02	150.0	50.0	11.0	.9	0.	0.	291.	0.	0.	.66
F515J5.011	.6	.0	23.4	.0	.04	150.0	28.0	11.0	1.5	0.	0.	249.	0.	0.	1.10
F515J5.012	.6	.0	16.5	.0	.05	150.0	.0	11.0	1.7	0.	0.	176.	0.	0.	1.49
F515K1.007	.1	.0	.0	.0	.02	150.0	84.0	17.0	.4	0.	0.	0.	0.	0.	.66
F515K1.008	.0	.0	.0	.0	-.02	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.06
F515K1.009	.1	.0	.0	.0	-.01	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.08
F515K1.010	.1	.0	.0	.0	.00	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.20
F515K1.011	.5	.0	24.4	.0	.00	150.0	28.0	17.0	1.2	0.	0.	261.	0.	0.	.39
F515K1.012	.6	.0	25.0	.0	.06	150.0	.0	17.0	1.6	0.	0.	267.	0.	0.	1.88
F515K2.007	.1	.0	.0	.0	.02	150.0	84.0	17.0	.4	0.	0.	0.	0.	0.	.52
F515K2.008	.1	.0	.0	.0	-.01	150.0	75.0	17.0	.2	0.	0.	0.	0.	0.	.09
F515K2.009	.0	.0	.0	.0	-.02	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.06
F515K2.010	.1	.0	.0	.0	.01	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.33
F515K2.011	.5	.0	16.4	.0	.02	150.0	28.0	17.0	1.2	0.	0.	175.	0.	0.	.68
F515K2.012	.4	.0	16.5	.0	-.03	150.0	.0	17.0	1.2	0.	0.	176.	0.	0.	.67
F515K3.007	.1	.0	.0	.0	-.01	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.07
F515K3.008	.1	.0	.0	.0	.00	150.0	75.0	17.0	.3	0.	0.	0.	0.	0.	.26
F515K3.009	.3	.0	32.1	.0	.00	150.0	56.0	17.0	.7	0.	0.	343.	0.	0.	.18
F515K3.010	.1	.0	.0	.0	-.01	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.10
F515K3.011	.2	.0	28.8	.0	-.10	150.0	28.0	17.0	.6	0.	0.	307.	0.	0.	.12
F515K3.012	.9	.0	27.4	.0	.26	150.0	.0	17.0	2.4	0.	0.	293.	0.	0.	7.49
F515K4.007	.1	.0	.0	.0	.01	150.0	84.0	17.0	.2	0.	0.	0.	0.	0.	.34
F515K4.008	.0	.0	.0	.0	-.02	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.04
F515K4.009	.0	.0	.0	.0	-.02	150.0	56.0	17.0	.0	0.	0.	0.	0.	0.	.05
F515K4.010	.1	.0	.0	.0	.00	150.0	50.0	17.0	.3	0.	0.	0.	0.	0.	.32
F515K4.011	.5	.0	35.6	.0	.04	150.0	28.0	17.0	1.2	0.	0.	380.	0.	0.	1.32
F515K4.012	.6	.0	26.7	.0	.07	150.0	.0	17.0	1.7	0.	0.	286.	0.	0.	2.12
F515K5.007	.0	.0	.0	.0	-.01	150.0	84.0	17.0	.1	0.	0.	0.	0.	0.	.03
F515K5.008	.2	.0	.0	.0	.04	150.0	75.0	17.0	.4	0.	0.	0.	0.	0.	1.02
F515K5.009	.1	.0	.0	.0	.02	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.49
F515K5.010	.3	.0	29.6	.0	.01	150.0	50.0	17.0	.8	0.	0.	316.	0.	0.	.33
F515K5.011	.4	.0	25.7	.0	.04	150.0	28.0	17.0	1.2	0.	0.	274.	0.	0.	1.25
F515K5.012	.7	.0	29.3	.0	.13	150.0	.0	17.0	2.0	0.	0.	313.	0.	0.	3.67
F515L1.007	.3	.0	14.7	.0	.05	150.0	.0	1.0	.7	0.	0.	156.	0.	0.	1.48
F515L1.008	.5	.0	17.0	.0	.07	150.0	-25.0	1.0	1.3	0.	0.	182.	0.	0.	2.17
F515L1.009	.5	.0	19.1	.0	.12	150.0	-50.0	1.0	1.4	0.	0.	204.	0.	0.	3.34
F515L1.010	.7	.0	20.1	.0	.11	150.0	-56.0	1.0	1.7	0.	0.	215.	0.	0.	3.17
F515L1.011	.6	.0	21.7	.0	.11	150.0	-75.0	1.0	1.6	0.	0.	232.	0.	0.	3.26
F515L1.012	.6	.0	25.1	.0	.08	150.0	-84.0	1.0	1.5	0.	0.	268.	0.	0.	2.37

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F515L2.007	.4	.0	25.3	.0	.08	150.0	.0	1.0	1.2	0.	0.	270.	0.	0.	2.45
F515L2.008	.5	.0	19.4	.0	.09	150.0	-25.0	1.0	1.3	0.	0.	207.	0.	0.	2.63
F515L2.009	.6	.0	21.0	.0	.09	150.0	-50.0	1.0	1.5	0.	0.	224.	0.	0.	2.60
F515L2.010	.6	.0	25.0	.0	.11	150.0	-56.0	1.0	1.7	0.	0.	266.	0.	0.	3.31
F515L2.011	.6	.0	26.8	.0	.11	150.0	-75.0	1.0	1.5	0.	0.	286.	0.	0.	3.34
F515L2.012	.6	.0	22.7	.0	.10	150.0	-84.0	1.0	1.5	0.	0.	242.	0.	0.	2.82
F515L3.007	.6	.0	22.3	.0	.11	150.0	.0	1.0	1.5	0.	0.	238.	0.	0.	3.10
F515L3.008	.6	.0	18.4	.0	.10	150.0	-25.0	1.0	1.5	0.	0.	196.	0.	0.	2.89
F515L3.009	.7	.0	22.7	.0	.10	150.0	-50.0	1.0	1.8	0.	0.	242.	0.	0.	2.93
F515L3.010	.6	.0	19.1	.0	.11	150.0	-56.0	1.0	1.7	0.	0.	204.	0.	0.	3.18
F515L3.011	.5	.0	22.5	.0	.10	150.0	-75.0	1.0	1.4	0.	0.	240.	0.	0.	3.00
F515L3.012	.4	.0	23.2	.0	.03	150.0	-84.0	1.0	1.0	0.	0.	248.	0.	0.	1.14
F515L4.007	.4	.0	19.6	.0	.06	150.0	.0	1.0	1.0	0.	0.	210.	0.	0.	1.88
F515L4.008	.4	.0	27.6	.0	.08	150.0	-25.0	1.0	1.1	0.	0.	294.	0.	0.	2.48
F515L4.009	.6	.0	20.1	.0	.11	150.0	-50.0	1.0	1.6	0.	0.	214.	0.	0.	3.15
F515L4.010	.7	.0	19.5	.0	.14	150.0	-56.0	1.0	1.8	0.	0.	208.	0.	0.	3.90
F515L4.011	.5	.0	27.4	.0	.11	150.0	-75.0	1.0	1.4	0.	0.	292.	0.	0.	3.11
F515L4.012	.5	.0	26.4	.0	.08	150.0	-84.0	1.0	1.3	0.	0.	282.	0.	0.	2.46
F515L5.007	.5	.0	22.0	.0	.06	150.0	.0	1.0	1.3	0.	0.	235.	0.	0.	1.75
F515L5.008	.6	.0	18.8	.0	.12	150.0	-25.0	1.0	1.5	0.	0.	201.	0.	0.	3.58
F515L5.009	.5	.0	23.1	.0	.09	150.0	-50.0	1.0	1.3	0.	0.	247.	0.	0.	2.63
F515L5.010	.6	.0	27.2	.0	.11	150.0	-56.0	1.0	1.7	0.	0.	291.	0.	0.	3.11
F515L5.011	.5	.0	27.8	.0	.09	150.0	-75.0	1.0	1.3	0.	0.	297.	0.	0.	2.70
F515L5.012	.5	.0	25.0	.0	.09	150.0	-84.0	1.0	1.3	0.	0.	267.	0.	0.	2.70
F515M1.007	.4	.0	15.7	.0	.07	150.0	.0	5.0	1.0	0.	0.	167.	0.	0.	2.06
F515M1.008	.6	.0	23.5	.0	.07	150.0	-25.0	5.0	1.5	0.	0.	251.	0.	0.	2.19
F515M1.009	.6	.0	11.1	.0	.10	150.0	-50.0	5.0	1.6	0.	0.	118.	0.	0.	2.86
F515M1.010	.8	.0	21.7	.0	.11	150.0	-56.0	5.0	2.0	0.	0.	231.	0.	0.	3.30
F515M1.011	.6	.0	19.8	.0	.08	150.0	-75.0	5.0	1.6	0.	0.	211.	0.	0.	2.39
F515M1.012	.5	.0	23.8	.0	.06	150.0	-84.0	5.0	1.4	0.	0.	254.	0.	0.	1.94
F515M2.007	.5	.0	22.7	.0	.08	150.0	.0	5.0	1.4	0.	0.	242.	0.	0.	2.43
F515M2.008	.6	.0	19.2	.0	.08	150.0	-25.0	5.0	1.5	0.	0.	205.	0.	0.	2.29
F515M2.009	.6	.0	18.0	.0	.09	150.0	-50.0	5.0	1.6	0.	0.	192.	0.	0.	2.55
F515M2.010	.6	.0	16.5	.0	.10	150.0	-56.0	5.0	1.6	0.	0.	176.	0.	0.	3.02
F515M2.011	.6	.0	20.3	.0	.10	150.0	-75.0	5.0	1.7	0.	0.	217.	0.	0.	2.88
F515M2.012	.6	.0	18.0	.0	.08	150.0	-84.0	5.0	1.5	0.	0.	192.	0.	0.	2.46
F515M3.007	.4	.0	16.5	.0	.05	150.0	.0	5.0	1.0	0.	0.	176.	0.	0.	1.49
F515M3.008	.6	.0	15.4	.0	.07	150.0	-25.0	5.0	1.6	0.	0.	164.	0.	0.	2.08
F515M3.009	.4	.0	14.7	.0	.08	150.0	-50.0	5.0	1.2	0.	0.	157.	0.	0.	2.33
F515M3.010	.5	.0	17.8	.0	.06	150.0	-56.0	5.0	1.4	0.	0.	190.	0.	0.	2.03
F515M3.011	.5	.0	28.6	.0	.08	150.0	-75.0	5.0	1.4	0.	0.	305.	0.	0.	2.53
F515M3.012	.6	.0	16.8	.0	.08	150.0	-84.0	5.0	1.5	0.	0.	179.	0.	0.	2.37

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F515M4.007	.5	.0	16.9	.0	.06	150.0	.0	5.0	1.4	0.	0.	181.	0.	0.	1.67
F515M4.008	.5	.0	21.9	.0	.07	150.0	-25.0	5.0	1.2	0.	0.	234.	0.	0.	2.07
F515M4.009	.6	.0	19.7	.0	.07	150.0	-50.0	5.0	1.5	0.	0.	210.	0.	0.	2.21
F515M4.010	.7	.0	20.0	.0	.07	150.0	-56.0	5.0	1.7	0.	0.	214.	0.	0.	2.46
F515M4.011	.6	.0	20.4	.0	.06	150.0	-75.0	5.0	1.5	0.	0.	218.	0.	0.	1.97
F515M4.012	.6	.0	20.5	.0	.05	150.0	-84.0	5.0	1.7	0.	0.	219.	0.	0.	1.71
F515M5.007	.6	.0	15.0	.0	.06	150.0	.0	5.0	1.5	0.	0.	160.	0.	0.	1.77
F515M5.008	.5	.0	25.3	.0	.08	150.0	-25.0	5.0	1.3	0.	0.	270.	0.	0.	2.44
F515M5.009	.6	.0	17.5	.0	.09	150.0	-50.0	5.0	1.6	0.	0.	187.	0.	0.	2.58
F515M5.010	.6	.0	26.1	.0	.11	150.0	-56.0	5.0	1.6	0.	0.	278.	0.	0.	3.17
F515M5.011	.6	.0	24.6	.0	.09	150.0	-75.0	5.0	1.6	0.	0.	263.	0.	0.	2.80
F515M5.012	.6	.0	12.9	.0	.09	150.0	-84.0	5.0	1.5	0.	0.	138.	0.	0.	2.50
F515N1.007	.5	.0	20.9	.0	.06	150.0	.0	11.0	1.4	0.	0.	223.	0.	0.	1.84
F515N1.008	.6	.0	16.5	.0	.10	150.0	-25.0	11.0	1.6	0.	0.	176.	0.	0.	2.77
F515N1.009	.5	.0	15.1	.0	.06	150.0	-50.0	11.0	1.3	0.	0.	161.	0.	0.	1.86
F515N1.010	.5	.0	22.6	.0	.07	150.0	-56.0	11.0	1.5	0.	0.	242.	0.	0.	2.08
F515N1.011	.6	.0	23.7	.0	.06	150.0	-75.0	11.0	1.6	0.	0.	253.	0.	0.	1.88
F515N1.012	.5	.0	27.8	.0	.03	150.0	-84.0	11.0	1.5	0.	0.	297.	0.	0.	1.06
F515N2.007	.4	.0	30.6	.0	.06	150.0	.0	11.0	1.1	0.	0.	326.	0.	0.	1.66
F515N2.008	.7	.0	25.1	.0	.09	150.0	-25.0	11.0	2.0	0.	0.	268.	0.	0.	2.49
F515N2.009	.7	.0	24.0	.0	.08	150.0	-50.0	11.0	2.0	0.	0.	256.	0.	0.	2.33
F515N2.010	.7	.0	23.9	.0	.04	150.0	-56.0	11.0	2.0	0.	0.	255.	0.	0.	1.57
F515N2.011	.7	.0	23.0	.0	.07	150.0	-75.0	11.0	1.8	0.	0.	245.	0.	0.	2.15
F515N2.012	.5	.0	21.7	.0	.06	150.0	-84.0	11.0	1.4	0.	0.	232.	0.	0.	1.82
F515N3.007	.4	.0	19.6	.0	.06	150.0	.0	11.0	1.1	0.	0.	209.	0.	0.	1.69
F515N3.008	.7	.0	25.5	.0	.06	150.0	-25.0	11.0	1.8	0.	0.	273.	0.	0.	1.91
F515N3.009	.5	.0	14.0	.0	.06	150.0	-50.0	11.0	1.4	0.	0.	150.	0.	0.	1.94
F515N3.010	.6	.0	19.1	.0	.04	150.0	-56.0	11.0	1.6	0.	0.	203.	0.	0.	1.52
F515N3.011	.7	.0	15.1	.0	.04	150.0	-75.0	11.0	1.9	0.	0.	161.	0.	0.	1.49
F515N3.012	.6	.0	22.0	.0	.03	150.0	-84.0	11.0	1.5	0.	0.	234.	0.	0.	1.09
F515N4.007	.4	.0	14.5	.0	.05	150.0	.0	11.0	1.1	0.	0.	155.	0.	0.	1.45
F515N4.008	.5	.0	22.7	.0	.06	150.0	-25.0	11.0	1.4	0.	0.	243.	0.	0.	1.84
F515N4.009	.6	.0	19.0	.0	.06	150.0	-50.0	11.0	1.6	0.	0.	203.	0.	0.	1.91
F515N4.010	.8	.0	26.7	.0	.09	150.0	-56.0	11.0	2.0	0.	0.	285.	0.	0.	2.74
F515N4.011	.6	.0	20.4	.0	.03	150.0	-75.0	11.0	1.5	0.	0.	217.	0.	0.	1.16
F515N4.012	.5	.0	18.6	.0	.02	150.0	-84.0	11.0	1.4	0.	0.	198.	0.	0.	.68
F515N5.007	.6	.0	22.7	.0	.08	150.0	.0	11.0	1.6	0.	0.	243.	0.	0.	2.22
F515N5.008	.6	.0	19.5	.0	.09	150.0	-25.0	11.0	1.6	0.	0.	208.	0.	0.	2.52
F515N5.009	.6	.0	22.4	.0	.07	150.0	-50.0	11.0	1.7	0.	0.	239.	0.	0.	2.17
F515N5.010	.7	.0	22.6	.0	.03	150.0	-56.0	11.0	1.9	0.	0.	241.	0.	0.	1.46
F515N5.011	.8	.0	22.9	.0	.07	150.0	-75.0	11.0	2.1	0.	0.	245.	0.	0.	2.05
F515N5.012	.5	.0	23.5	.0	.04	150.0	-84.0	11.0	1.2	0.	0.	251.	0.	0.	1.14

FALCON 5: LSR = 150, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F51501.007	.5	.0	25.6	.0	.04	150.0	.0	17.0	1.3	0.	0.	274.	0.	0.	1.21
F51501.008	.5	.0	24.3	.0	.06	150.0	-25.0	17.0	1.3	0.	0.	260.	0.	0.	1.88
F51501.009	.4	.0	21.9	.0	.02	150.0	-50.0	17.0	1.1	0.	0.	234.	0.	0.	.82
F51501.010	.4	.0	24.6	.0	.02	150.0	-56.0	17.0	1.1	0.	0.	262.	0.	0.	.87
F51501.011	.4	.0	26.8	.0	.01	150.0	-75.0	17.0	1.0	0.	0.	286.	0.	0.	.39
F51501.012	.2	.0	.0	.0	.01	150.0	-84.0	17.0	.5	0.	0.	0.	0.	0.	.31
F51502.007	.6	.0	11.4	.0	.08	150.0	.0	17.0	1.5	0.	0.	122.	0.	0.	2.30
F51502.008	.6	.0	33.6	.0	.04	150.0	-25.0	17.0	1.5	0.	0.	359.	0.	0.	1.38
F51502.009	.5	.0	34.1	.0	.03	150.0	-50.0	17.0	1.4	0.	0.	364.	0.	0.	.98
F51502.010	.4	.0	30.5	.0	.03	150.0	-56.0	17.0	1.2	0.	0.	325.	0.	0.	.85
F51502.011	.2	.0	34.6	.0	-.01	150.0	-75.0	17.0	.7	0.	0.	370.	0.	0.	.45
F51502.012	.2	.0	34.7	.0	-.01	150.0	-84.0	17.0	.5	0.	0.	370.	0.	0.	.16
F51503.007	.5	.0	25.3	.0	.05	150.0	.0	17.0	1.4	0.	0.	270.	0.	0.	1.45
F51503.008	.6	.0	18.6	.0	.04	150.0	-25.0	17.0	1.6	0.	0.	198.	0.	0.	1.46
F51503.009	.5	.0	16.6	.0	.02	150.0	-50.0	17.0	1.2	0.	0.	177.	0.	0.	.85
F51503.010	.5	.0	16.4	.0	.01	150.0	-56.0	17.0	1.2	0.	0.	175.	0.	0.	.72
F51503.011	.5	.0	17.0	.0	.01	150.0	-75.0	17.0	1.4	0.	0.	181.	0.	0.	.55
F51503.012	.5	.0	21.3	.0	.02	150.0	-84.0	17.0	1.2	0.	0.	227.	0.	0.	.59
F51504.007	.5	.0	16.8	.0	.06	150.0	.0	17.0	1.4	0.	0.	179.	0.	0.	1.72
F51504.008	.5	.0	23.4	.0	.02	150.0	-25.0	17.0	1.4	0.	0.	250.	0.	0.	.97
F51504.009	.5	.0	23.2	.0	.01	150.0	-50.0	17.0	1.3	0.	0.	247.	0.	0.	.67
F51504.010	.6	.0	17.8	.0	-.01	150.0	-56.0	17.0	1.7	0.	0.	190.	0.	0.	.88
F51504.011	.4	.0	23.6	.0	-.02	150.0	-75.0	17.0	1.0	0.	0.	252.	0.	0.	.25
F51504.012	.3	.0	6.7	.0	-.01	150.0	-84.0	17.0	.8	0.	0.	72.	0.	0.	.23
F51505.007	.4	.0	17.0	.0	.03	150.0	.0	17.0	1.1	0.	0.	181.	0.	0.	.95
F51505.008	.6	.0	27.4	.0	.05	150.0	-25.0	17.0	1.6	0.	0.	292.	0.	0.	1.40
F51505.009	.5	.0	26.5	.0	.03	150.0	-50.0	17.0	1.5	0.	0.	282.	0.	0.	1.12
F51505.010	.5	.0	24.2	.0	.04	150.0	-56.0	17.0	1.4	0.	0.	258.	0.	0.	1.36
F51505.011	.6	.0	20.2	.0	.02	150.0	-75.0	17.0	1.7	0.	0.	216.	0.	0.	.80
F51505.012	.6	.0	19.8	.0	.02	150.0	-84.0	17.0	1.5	0.	0.	211.	0.	0.	.61

FALCON 5: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N520A1.009	2.2	7.1	22.0	34.7	.24	-62.0	30.0	2.0	5.7	200.	0.	271.	0.	274.	8.18
N520A1.008	29.4	.8	7.5	101.2	5.22	-62.0	20.0	2.0	53.0	15.	18.	92.	404.	768.	138.24
N520A1.007	26.5	.9	8.2	121.1	5.61	-62.0	10.0	2.0	49.4	12.	17.	101.	619.	1217.	155,38
N520A1.006	27.4	1.0	8.0	85.5	4.99	-62.0	.0	2.0	50.5	15.	19.	99.	476.	710.	138.55
N520A1.005	28.5	1.5	8.8	63.4	4.62	-62.0	-20.0	2.0	51.9	23.	26.	108.	360.	549.	123.88
N520A1.004	.7	.0	23.1	.0	.03	-62.0	-30.0	2.0	1.8	0.	0.	285.	0.	0.	1.26
N520A2.009	1.9	13.9	31.1	31.2	.24	-62.0	30.0	2.0	5.0	0.	0.	384.	0.	0.	7.89
N520A2.008	30.4	1.2	8.0	119.3	6.65	-62.0	20.0	2.0	54.1	16.	18.	98.	556.	1057.	176.19
N520A2.007	28.7	.3	7.8	117.7	6.94	-62.0	10.0	2.0	52.1	10.	14.	96.	812.	1450.	190.81
N520A2.006	25.5	1.0	7.9	117.6	6.40	-62.0	.0	2.0	48.0	13.	25.	97.	571.	1178.	177.00
N520A2.005	26.5	1.1	7.9	77.9	5.76	-62.0	-20.0	2.0	49.3	15.	24.	98.	525.	633.	156.08
N520A2.004	.6	.0	23.5	.0	-.03	-62.0	-30.0	2.0	1.6	0.	0.	290.	0.	0.	.41
N520A3.009	2.6	8.5	13.8	42.4	.37	-62.0	30.0	2.0	6.6	157.	0.	171.	0.	304.	12.37
N520A3.008	32.0	1.0	7.7	118.2	6.43	-62.0	20.0	2.0	55.9	13.	18.	95.	444.	1057.	168.80
N520A3.007	26.8	1.1	8.6	119.8	6.38	-62.0	10.0	2.0	49.7	14.	17.	106.	646.	1264.	174.76
N520A3.006	28.0	1.0	7.9	109.6	6.23	-62.0	.0	2.0	51.3	14.	21.	97.	580.	890.	169.46
N520A3.005	31.5	1.3	7.9	98.0	5.52	-62.0	-20.0	2.0	55.4	21.	23.	97.	472.	617.	147.84
N520A3.004	.2	.0	34.4	.0	.02	-62.0	-30.0	2.0	.6	0.	0.	425.	0.	0.	1.15
N520A4.009	2.5	9.2	18.1	35.1	.22	-62.0	30.0	2.0	6.5	115.	0.	224.	0.	397.	7.83
N520A4.008	31.8	.7	7.7	85.7	5.54	-62.0	20.0	2.0	55.8	10.	12.	95.	436.	695.	150.99
N520A4.007	28.8	.3	7.7	119.2	6.72	-62.0	10.0	2.0	52.2	11.	15.	95.	684.	1285.	184.81
N520A4.006	29.1	1.2	8.1	86.1	5.33	-62.0	.0	2.0	52.6	16.	20.	100.	478.	783.	146.63
N520A4.005	29.2	2.2	7.7	59.0	5.10	-62.0	-20.0	2.0	52.7	28.	30.	95.	456.	560.	136.82
N520A4.004	.7	.0	13.2	.0	-.02	-62.0	-30.0	2.0	1.9	0.	0.	162.	0.	0.	.40
N520A5.009	2.2	10.2	22.5	31.8	.16	-62.0	30.0	2.0	5.8	277.	0.	277.	0.	363.	5.99
N520A5.008	33.0	.6	7.3	91.2	6.02	-62.0	20.0	2.0	57.1	12.	16.	90.	436.	888.	156.70
N520A5.007	28.6	.2	7.7	119.9	6.60	-62.0	10.0	2.0	51.9	11.	17.	95.	645.	1346.	180.73
N520A5.006	26.3	.9	7.8	103.4	5.95	-62.0	.0	2.0	49.1	14.	18.	96.	480.	911.	162.82
N520A5.005	30.2	1.0	7.7	89.0	5.06	-62.0	-20.0	2.0	53.9	18.	20.	95.	449.	552.	135.86
N520A5.004	.2	.0	20.7	.0	-.02	-62.0	-30.0	2.0	.7	0.	0.	255.	0.	0.	.28
N520B1.009	1.2	10.3	19.1	21.0	.16	-32.0	30.0	1.0	3.3	0.	0.	236.	0.	0.	5.30
N520B1.008	32.8	.3	7.3	64.6	4.59	-32.0	20.0	1.0	56.9	4.	20.	90.	374.	499.	120.29
N520B1.007	42.2	.1	7.2	85.9	6.28	-32.0	10.0	1.0	66.4	2.	2.	89.	349.	704.	156.06
N520B1.006	42.1	.1	7.4	77.2	5.80	-32.0	.0	1.0	66.3	2.	2.	92.	408.	619.	147.34
N520B1.005	31.4	.1	5.9	98.5	4.63	-32.0	-20.0	1.0	55.3	4.	4.	72.	347.	824.	122.41
N520B1.004	.2	.0	18.6	.0	.00	-32.0	-30.0	1.0	.6	0.	0.	229.	0.	0.	.85
N520B2.009	1.1	19.1	19.2	36.8	.22	-32.0	30.0	1.0	2.9	0.	0.	237.	0.	0.	7.28
N520B2.008	34.5	.4	6.9	79.7	5.15	-32.0	20.0	1.0	58.7	14.	21.	85.	403.	510.	135.51
N520B2.007	41.0	.1	7.2	100.5	6.62	-32.0	10.0	1.0	65.2	2.	2.	88.	475.	699.	165.68
N520B2.006	41.5	.1	6.9	70.2	5.98	-32.0	.0	1.0	65.8	2.	2.	85.	438.	645.	152.35
N520B2.005	33.7	.1	6.9	66.2	4.73	-32.0	-20.0	1.0	57.9	1.	10.	85.	389.	525.	125.23
N520B2.004	.6	.0	32.7	.0	.05	-32.0	-30.0	1.0	1.7	0.	0.	403.	0.	0.	1.93

FALCON 5: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N520B3.009	1.7	10.2	10.3	21.0	.19	-32.0	30.0	1.0	4.4	0.	0.	127.	0.	0.	6.35
N520B3.008	33.1	.4	8.2	73.7	4.98	-32.0	20.0	1.0	57.2	10.	19.	101.	402.	478.	130.71
N520B3.007	44.6	.1	7.4	86.1	6.49	-32.0	10.0	1.0	68.5	2.	2.	92.	449.	706.	160.54
N520B3.006	43.8	.1	6.9	74.7	6.11	-32.0	.0	1.0	67.8	1.	2.	85.	376.	567.	152.22
N520B3.005	32.0	.1	7.2	106.0	4.80	-32.0	-20.0	1.0	56.0	1.	1.	89.	392.	643.	126.65
N520B3.004	.8	.0	27.4	.0	.03	-32.0	-30.0	1.0	2.0	0.	0.	338.	0.	0.	1.57
N520B4.009	2.3	8.1	16.5	20.1	.10	-32.0	30.0	1.0	5.9	202.	0.	203.	0.	204.	4.68
N520B4.008	36.3	.4	7.3	56.4	4.71	-32.0	20.0	1.0	60.6	6.	24.	90.	409.	465.	123.58
N520B4.007	46.5	.1	7.1	69.7	6.57	-32.0	10.0	1.0	70.1	2.	2.	87.	540.	743.	164.10
N520B4.006	43.9	.1	7.3	80.6	6.03	-32.0	.0	1.0	67.9	2.	2.	90.	410.	611.	151.09
N520B4.005	35.9	.1	7.2	60.3	4.57	-32.0	-20.0	1.0	60.2	1.	10.	88.	416.	484.	120.63
N520B4.004	.4	.0	7.5	.0	.05	-32.0	-30.0	1.0	1.0	0.	0.	92.	0.	0.	1.95
N520B5.009	1.7	11.8	18.2	28.1	.16	-32.0	30.0	1.0	4.6	0.	0.	224.	0.	0.	5.63
N520B5.008	36.2	.6	8.1	61.9	5.17	-32.0	20.0	1.0	60.5	15.	21.	100.	386.	588.	132.73
N520B5.007	43.3	.1	5.6	82.7	7.02	-32.0	10.0	1.0	67.4	2.	2.	68.	484.	684.	173.13
N520B5.006	45.5	.1	7.2	72.0	6.31	-32.0	.0	1.0	69.3	2.	2.	89.	432.	675.	156.62
N520B5.005	34.5	.1	8.3	69.9	4.85	-32.0	-20.0	1.0	58.8	1.	1.	102.	403.	480.	126.43
N520B5.004	.4	.0	11.7	.0	-.01	-32.0	-30.0	1.0	1.1	0.	0.	144.	0.	0.	.53
N520C1.009	2.8	2.7	11.1	27.2	.19	-2.0	30.0	1.0	7.2	135.	0.	137.	0.	139.	6.45
N520C1.008	18.3	1.2	7.2	87.8	2.58	-2.0	20.0	1.0	37.7	38.	42.	89.	272.	468.	77.15
N520C1.007	15.0	2.4	10.8	83.3	2.38	-2.0	10.0	1.0	32.2	39.	58.	133.	348.	1024.	71.62
N520C1.006	21.7	.2	7.7	84.7	2.93	-2.0	.0	1.0	42.8	2.	47.	95.	343.	626.	85.39
N520C1.005	29.9	.2	5.8	74.0	3.16	-2.0	-20.0	1.0	53.5	3.	3.	72.	362.	486.	89.07
N520C1.004	1.6	20.1	20.2	20.3	.03	-2.0	-30.0	1.0	4.1	0.	0.	248.	0.	0.	1.41
N520C2.009	2.5	11.1	12.3	22.8	.19	-2.0	30.0	1.0	6.5	151.	0.	151.	0.	280.	6.56
N520C2.008	13.9	.1	10.8	89.9	2.72	-2.0	20.0	1.0	30.4	15.	34.	133.	333.	735.	81.87
N520C2.007	19.4	.3	10.0	87.9	2.23	-2.0	10.0	1.0	39.4	13.	54.	124.	375.	981.	66.39
N520C2.006	22.5	.1	9.7	81.9	2.80	-2.0	.0	1.0	43.9	2.	3.	119.	390.	413.	80.47
N520C2.005	32.6	.2	6.6	90.4	3.90	-2.0	-20.0	1.0	56.7	3.	3.	82.	416.	737.	106.19
N520C2.004	.8	.0	27.7	.0	.01	-2.0	-30.0	1.0	2.1	0.	0.	341.	0.	0.	.92
N520C3.009	1.8	3.4	22.7	36.8	.26	-2.0	30.0	1.0	4.8	0.	0.	280.	0.	0.	8.76
N520C3.008	16.4	.1	9.0	78.5	3.21	-2.0	20.0	1.0	34.7	19.	38.	111.	451.	965.	96.16
N520C3.007	21.8	.2	7.6	82.9	2.80	-2.0	10.0	1.0	43.0	19.	40.	93.	516.	822.	81.37
N520C3.006	26.0	.1	6.9	78.3	3.80	-2.0	.0	1.0	48.7	2.	2.	85.	321.	559.	103.09
N520C3.005	35.3	.3	6.7	50.4	4.33	-2.0	-20.0	1.0	59.6	4.	5.	82.	346.	477.	116.51
N520C3.004	.3	.0	20.2	.0	.02	-2.0	-30.0	1.0	.8	0.	0.	248.	0.	0.	.86
N520C4.009	2.1	2.1	18.4	35.6	.23	-2.0	30.0	1.0	5.5	227.	0.	227.	0.	229.	7.87
N520C4.008	17.0	.1	9.1	80.7	3.49	-2.0	20.0	1.0	35.7	9.	45.	113.	391.	822.	102.29
N520C4.007	21.5	.2	8.0	82.9	3.03	-2.0	10.0	1.0	42.5	37.	45.	98.	376.	959.	86.77
N520C4.006	30.9	.1	7.4	64.1	4.22	-2.0	.0	1.0	54.8	2.	2.	91.	354.	586.	111.92
N520C4.005	40.1	.2	7.2	85.1	4.94	-2.0	-20.0	1.0	64.4	3.	3.	89.	441.	556.	126.77
N520C4.004	1.5	10.6	10.7	10.8	.07	-2.0	-30.0	1.0	3.9	0.	0.	132.	0.	0.	2.53

FALCON 5: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
N520C5.009	2.2	12.0	22.4	35.3	.33	-2.0	30.0	1.0	5.8	177.	0.	276.	0.	277.	10.82
N520C5.008	16.3	.1	8.3	89.9	3.28	-2.0	20.0	1.0	34.4	9.	46.	102.	496.	837.	97.97
N520C5.007	18.9	.1	8.8	71.5	2.08	-2.0	10.0	1.0	38.7	2.	33.	108.	502.	518.	69.29
N520C5.006	27.6	.1	9.4	58.8	3.73	-2.0	.0	1.0	50.7	2.	2.	116.	412.	513.	105.54
N520C5.005	37.2	.2	7.2	61.4	4.22	-2.0	-20.0	1.0	61.6	4.	5.	89.	507.	751.	115.49
N520C5.004	1.0	42.4	42.4	42.5	.04	-2.0	-30.0	1.0	2.7	0.	0.	523.	0.	0.	1.32
F520D1.006	.2	.0	.0	.0	.02	50.0	66.0	1.0	.5	0.	0.	0.	0.	0.	.73
F520D1.007	.2	.0	.0	.0	.01	50.0	50.0	1.0	.5	0.	0.	0.	0.	0.	.50
F520D1.008	.5	.0	20.1	.0	.04	50.0	33.0	1.0	1.5	0.	0.	248.	0.	0.	1.41
F520D1.009	.9	.0	17.3	.0	.14	50.0	.0	1.0	2.3	0.	0.	213.	0.	0.	4.68
F520D1.010	1.1	15.6	15.7	15.9	.13	50.0	-33.0	1.0	3.0	0.	0.	194.	0.	0.	4.15
F520D1.011	1.1	15.5	16.9	17.0	.10	50.0	-50.0	1.0	2.9	0.	0.	208.	0.	0.	3.23
F520D1.012	.4	.0	17.8	.0	.04	50.0	-66.0	1.0	1.2	0.	0.	219.	0.	0.	1.34
F520D2.006	.6	.0	19.9	.0	.05	50.0	66.0	1.0	1.5	0.	0.	245.	0.	0.	1.52
F520D2.007	.4	.0	19.8	.0	.03	50.0	50.0	1.0	1.2	0.	0.	244.	0.	0.	1.10
F520D2.008	.8	.0	15.3	.0	.08	50.0	33.0	1.0	2.2	0.	0.	188.	0.	0.	2.79
F520D2.009	.7	.0	18.2	.0	.12	50.0	.0	1.0	1.8	0.	0.	224.	0.	0.	4.18
F520D2.010	.6	.0	13.7	.0	.02	50.0	-33.0	1.0	1.6	0.	0.	169.	0.	0.	.86
F520D2.011	.2	.0	38.0	.0	.02	50.0	-50.0	1.0	.6	0.	0.	469.	0.	0.	1.07
F520D2.012	.1	.0	.0	.0	-.01	50.0	-66.0	1.0	.2	0.	0.	0.	0.	0.	.18
F520D3.006	.2	.0	.0	.0	.02	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.78
F520D3.007	.8	.0	20.5	.0	.04	50.0	50.0	1.0	2.2	0.	0.	253.	0.	0.	1.57
F520D3.008	1.1	13.7	13.7	13.8	.06	50.0	33.0	1.0	3.0	0.	0.	169.	0.	0.	1.99
F520D3.009	.9	.0	17.4	.0	.15	50.0	.0	1.0	2.5	0.	0.	215.	0.	0.	4.88
F520D3.010	.8	.0	19.1	.0	.06	50.0	-33.0	1.0	2.0	0.	0.	235.	0.	0.	1.98
F520D3.011	.8	.0	22.8	.0	.02	50.0	-50.0	1.0	2.0	0.	0.	282.	0.	0.	1.07
F520D3.012	.1	.0	.0	.0	.01	50.0	-66.0	1.0	.4	0.	0.	0.	0.	0.	.49
F520D4.006	.1	.0	.0	.0	.03	50.0	66.0	1.0	.4	0.	0.	0.	0.	0.	.92
F520D4.007	.1	.0	.0	.0	.00	50.0	50.0	1.0	.4	0.	0.	0.	0.	0.	.35
F520D4.008	.9	.0	11.2	.0	.02	50.0	33.0	1.0	2.5	0.	0.	139.	0.	0.	.83
F520D4.009	1.1	15.7	15.7	16.6	.14	50.0	.0	1.0	2.8	0.	0.	194.	0.	0.	4.80
F520D4.010	1.6	10.0	10.2	11.3	.14	50.0	-33.0	1.0	4.2	0.	0.	125.	0.	0.	4.51
F520D4.011	.6	.0	20.9	.0	.06	50.0	-50.0	1.0	1.7	0.	0.	257.	0.	0.	2.22
F520D4.012	.4	.0	25.2	.0	.02	50.0	-66.0	1.0	1.2	0.	0.	311.	0.	0.	1.06
F520D5.006	.1	.0	.0	.0	.03	50.0	66.0	1.0	.3	0.	0.	0.	0.	0.	.98
F520D5.007	.4	.0	28.7	.0	.03	50.0	50.0	1.0	1.2	0.	0.	354.	0.	0.	1.13
F520D5.008	.9	.0	9.1	.0	.07	50.0	33.0	1.0	2.4	0.	0.	112.	0.	0.	2.47
F520D5.009	.9	.0	15.5	.0	.15	50.0	.0	1.0	2.5	0.	0.	190.	0.	0.	5.05
F520D5.010	.9	.0	4.1	.0	.06	50.0	-33.0	1.0	2.4	0.	0.	50.	0.	0.	1.96
F520D5.011	1.0	14.2	14.2	14.2	.10	50.0	-50.0	1.0	2.7	0.	0.	175.	0.	0.	3.37
F520D5.012	.1	.0	.0	.0	.03	50.0	-66.0	1.0	.4	0.	0.	0.	0.	0.	.97
F520E1.006	.5	.0	20.8	.0	.06	50.0	66.0	5.0	1.4	0.	0.	257.	0.	0.	2.09

FALCON 5: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F520E1.007	1.0	17.4	17.4	17.4	.05	50.0	50.0	5.0	2.7	0.	0.	214.	0.	0.	1.99
F520E1.008	1.4	11.2	11.4	14.8	.13	50.0	33.0	5.0	3.7	0.	0.	140.	0.	0.	4.35
F520E1.009	.8	.0	17.4	.0	.09	50.0	.0	5.0	2.2	0.	0.	214.	0.	0.	3,08
F520E1.010	.9	.0	17.1	.0	.02	50.0	-33.0	5.0	2.4	0.	0.	211.	0.	0.	1.06
F520E1.011	.6	.0	25.7	.0	.07	50.0	-50.0	5.0	1.7	0.	0.	317.	0.	0.	2.19
F520E1.012	.1	.0	.0	.0	.01	50.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.53
F520E2.006	.7	.0	20.0	.0	.07	50.0	66.0	5.0	1.8	0.	0.	247.	0.	0.	2.41
F520E2.007	1.0	.0	22.4	.0	.04	50.0	50.0	5.0	2.6	0.	0.	276.	0.	0.	1.85
F520E2.008	1.7	10.6	15.0	15.2	.11	50.0	33.0	5.0	4.4	0.	0.	185.	0.	0.	3.84
F520E2.009	1.4	8.6	8.7	8.7	.12	50.0	.0	5.0	3.7	0.	0.	107.	0.	0.	4.15
F520E2.010	1.2	12.9	12.9	13.1	.05	50.0	-33.0	5.0	3.2	0.	0.	159.	0.	0.	1.72
F520E2.011	.3	.0	32.5	.0	.03	50.0	-50.0	5.0	.9	0.	0.	401.	0.	0.	1.18
F520E2.012	.2	.0	37.0	.0	.00	50.0	-66.0	5.0	.6	0.	0.	456.	0.	0.	.60
F520E3.006	.2	.0	.0	.0	.03	50.0	66.0	5.0	.5	0.	0.	0.	0.	0.	.98
F520E3.007	.4	.0	29.8	.0	.06	50.0	50.0	5.0	1.2	0.	0.	367.	0.	0.	1.91
F520E3.008	1.1	5.8	13.6	13.7	.04	50.0	33.0	5.0	3.0	0.	0.	168.	0.	0.	1.48
F520E3.009	1.0	.0	12.6	.0	.16	50.0	.0	5.0	2.6	0.	0.	155.	0.	0.	5.26
F520E3.010	.8	.0	19.3	.0	.05	50.0	-33.0	5.0	2.3	0.	0.	238.	0.	0.	1.85
F520E3.011	.7	.0	13.7	.0	.00	50.0	-50.0	5.0	1.8	0.	0.	169.	0.	0.	.44
F520E3.012	.1	.0	.0	.0	.00	50.0	-66.0	5.0	.4	0.	0.	0.	0.	0.	.32
F520E4.006	.2	.0	.0	.0	-.01	50.0	66.0	5.0	.5	0.	0.	0.	0.	0.	.36
F520E4.007	.6	.0	12.3	.0	.06	50.0	50.0	5.0	1.7	0.	0.	151.	0.	0.	1.88
F520E4.008	1.0	.0	17.5	.0	.05	50.0	33.0	5.0	2.6	0.	0.	216.	0.	0.	1.80
F520E4.009	1.1	17.9	22.9	23.0	.13	50.0	.0	5.0	2.9	0.	0.	282.	0.	0.	4.35
F520E4.010	.9	.0	20.8	.0	.06	50.0	-33.0	5.0	2.4	0.	0.	256.	0.	0.	2.09
F520E4.011	1.2	19.9	20.0	20.1	.00	50.0	-50.0	5.0	3.2	0.	0.	247.	0.	0.	.65
F520E4.012	.4	.0	20.5	.0	.04	50.0	-66.0	5.0	1.0	0.	0.	252.	0.	0.	1.55
F520F1.006	.3	.0	24.2	.0	.00	50.0	66.0	11.0	.9	0.	0.	298.	0.	0.	.34
F520F1.007	.9	.0	24.4	.0	.03	50.0	50.0	11.0	2.3	0.	0.	300.	0.	0.	1.13
F520F1.008	1.0	9.8	9.8	9.9	.06	50.0	33.0	11.0	2.7	0.	0.	121.	0.	0.	2.11
F520F1.009	1.1	13.9	13.9	14.4	.12	50.0	.0	11.0	2.8	0.	0.	172.	0.	0.	4.13
F520F1.010	.7	.0	13.8	.0	.04	50.0	-33.0	11.0	1.9	0.	0.	171.	0.	0.	1.44
F520F1.011	.2	.0	.0	.0	.01	50.0	-50.0	11.0	.5	0.	0.	0.	0.	0.	.49
F520F1.012	.1	.0	.0	.0	-.01	50.0	-66.0	11.0	.3	0.	0.	0.	0.	0.	.25
F520F2.006	.5	.0	15.6	.0	.03	50.0	66.0	11.0	1.3	0.	0.	193.	0.	0.	.87
F520F2.007	1.0	.0	13.3	.0	.02	50.0	50.0	11.0	2.6	0.	0.	164.	0.	0.	1.05
F520F2.008	.9	.0	17.1	.0	.05	50.0	33.0	11.0	2.5	0.	0.	211.	0.	0.	2.06
F520F2.009	1.1	17.1	17.1	17.1	.13	50.0	.0	11.0	2.9	0.	0.	210.	0.	0.	4.31
F520F2.010	1.0	18.7	18.7	18.8	.05	50.0	-33.0	11.0	2.8	0.	0.	231.	0.	0.	1.66
F520F2.011	.6	.0	18.0	.0	.04	50.0	-50.0	11.0	1.5	0.	0.	222.	0.	0.	1.39
F520F2.012	.1	.0	.0	.0	-.02	50.0	-66.0	11.0	.2	0.	0.	0.	0.	0.	.13
F520F3.006	.6	.0	21.6	.0	.03	50.0	66.0	11.0	1.7	0.	0.	267.	0.	0.	1.09

FALCON 5: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F520F3.007	1.1	17.6	17.6	17.6	.05	50.0	50.0	11.0	3.0	0.	0.	217.	0.	0.	1.61
F520F3.008	1.5	9.0	9.2	20.3	.13	50.0	33.0	11.0	4.1	0.	0.	114.	0.	0.	4.26
F520F3.009	1.0	9.5	9.5	16.9	.11	50.0	.0	11.0	2.8	0.	0.	117.	0.	0.	3.81
F520F3.010	.8	.0	15.8	.0	.02	50.0	-33.0	11.0	2.2	0.	0.	194.	0.	0.	.81
F520F3.011	.3	.0	30.6	.0	.02	50.0	-50.0	11.0	.8	0.	0.	378.	0.	0.	.85
F520F3.012	.2	.0	32.4	.0	.05	50.0	-66.0	11.0	.6	0.	0.	399.	0.	0.	1.80
F520F4.006	.7	.0	20.7	.0	.00	50.0	66.0	11.0	1.9	0.	0.	255.	0.	0.	.39
F520F4.007	1.3	2.8	2.8	2.9	.02	50.0	50.0	11.0	3.4	0.	0.	35.	0.	0.	.93
F520F4.008	1.0	9.4	18.2	18.2	.09	50.0	33.0	11.0	2.8	0.	0.	224.	0.	0.	2.92
F520F4.009	1.0	.0	9.7	.0	.07	50.0	.0	11.0	2.6	0.	0.	119.	0.	0.	2.46
F520F4.010	1.5	16.6	18.1	18.2	.03	50.0	-33.0	11.0	4.0	0.	0.	224.	0.	0.	1.67
F520F4.011	.9	.0	15.7	.0	.01	50.0	-50.0	11.0	2.4	0.	0.	194.	0.	0.	.77
F520F4.012	.4	.0	18.3	.0	.01	50.0	-66.0	11.0	1.0	0.	0.	226.	0.	0.	.56
F520F5.006	.5	.0	18.3	.0	.01	50.0	66.0	11.0	1.4	0.	0.	225.	0.	0.	.47
F520F5.007	.8	.0	18.6	.0	.02	50.0	50.0	11.0	2.2	0.	0.	229.	0.	0.	.86
F520F5.008	1.1	17.5	17.9	18.7	.07	50.0	33.0	11.0	3.0	0.	0.	221.	0.	0.	2.63
F520F5.009	1.3	13.6	20.6	20.6	.13	50.0	.0	11.0	3.4	0.	0.	253.	0.	0.	4.48
F520F5.010	1.1	12.0	12.0	12.4	.03	50.0	-33.0	11.0	3.0	0.	0.	148.	0.	0.	1.47
F520F5.011	.3	.0	20.3	.0	.01	50.0	-50.0	11.0	.8	0.	0.	250.	0.	0.	.64
F520F5.012	.2	.0	.0	.0	.04	50.0	-66.0	11.0	.4	0.	0.	0.	0.	0.	1.22
F520G1.006	.2	.0	30.3	.0	-.02	50.0	66.0	17.0	.6	0.	0.	373.	0.	0.	.05
F520G1.007	.9	.0	12.5	.0	-.01	50.0	50.0	17.0	2.5	0.	0.	154.	0.	0.	.31
F520G1.008	1.1	10.5	10.6	10.6	.03	50.0	33.0	17.0	2.9	0.	0.	130.	0.	0.	1.57
F520G1.009	1.5	13.2	13.3	21.9	.06	50.0	.0	17.0	4.1	0.	0.	163.	0.	0.	2.34
F520G1.010	.9	.0	17.7	.0	.00	50.0	-33.0	17.0	2.5	0.	0.	219.	0.	0.	.63
F520G1.011	.1	.0	.0	.0	.00	50.0	-50.0	17.0	.4	0.	0.	0.	0.	0.	.46
F520G1.012	.2	.0	.0	.0	.01	50.0	-66.0	17.0	.5	0.	0.	0.	0.	0.	.61
F520G2.006	.3	.0	17.4	.0	.02	50.0	66.0	17.0	.8	0.	0.	214.	0.	0.	.72
F520G2.007	1.2	7.3	7.3	7.4	.02	50.0	50.0	17.0	3.1	0.	0.	90.	0.	0.	.69
F520G2.008	1.2	3.6	3.7	18.5	.04	50.0	33.0	17.0	3.3	0.	0.	46.	0.	0.	1.64
F520G2.009	1.1	12.5	12.5	14.4	.04	50.0	.0	17.0	3.0	0.	0.	154.	0.	0.	1.95
F520G2.010	.7	.0	18.0	.0	.01	50.0	-33.0	17.0	1.9	0.	0.	222.	0.	0.	.83
F520G2.011	.5	.0	23.2	.0	.01	50.0	-50.0	17.0	1.3	0.	0.	286.	0.	0.	.73
F520G2.012	.1	.0	.0	.0	.01	50.0	-66.0	17.0	.4	0.	0.	0.	0.	0.	.43
F520G3.006	.3	.0	36.3	.0	.03	50.0	66.0	17.0	.7	0.	0.	448.	0.	0.	1.01
F520G3.007	1.4	8.0	20.2	20.3	.03	50.0	50.0	17.0	3.7	0.	0.	249.	0.	0.	1.17
F520G3.008	1.3	9.1	13.1	19.9	.06	50.0	33.0	17.0	3.4	0.	0.	161.	0.	0.	1.98
F520G3.009	1.3	13.4	13.4	16.3	.08	50.0	.0	17.0	3.4	0.	0.	165.	0.	0.	2.80
F520G3.010	1.3	9.7	9.7	14.7	.04	50.0	-33.0	17.0	3.4	0.	0.	120.	0.	0.	1.47
F520G3.011	.8	.0	7.3	.0	.04	50.0	-50.0	17.0	2.2	0.	0.	90.	0.	0.	1.36
F520G3.012	.1	.0	.0	.0	-.01	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.13
F520G4.006	.1	.0	.0	.0	.00	50.0	66.0	17.0	.3	0.	0.	0.	0.	0.	.31

FALCON 5: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F520G4.007	.5	.0	8.4	.0	.02	50.0	50.0	17.0	1.4	0.	0.	104.	0.	0.	.79
F520G4.008	1.0	.0	18.7	.0	.05	50.0	33.0	17.0	2.5	0.	0.	230.	0.	0.	1.91
F520G4.009	1.1	10.5	10.5	14.2	.11	50.0	.0	17.0	2.9	0.	0.	129.	0.	0.	3.70
F520G4.010	1.4	6.0	6.1	19.2	.03	50.0	-33.0	17.0	3.7	0.	0.	75.	0.	0.	1.27
F520G4.011	1.0	.0	17.7	.0	.05	50.0	-50.0	17.0	2.6	0.	0.	218.	0.	0.	1.99
F520G4.012	.2	.0	30.2	.0	-.02	50.0	-66.0	17.0	.6	0.	0.	372.	0.	0.	.09
F520G5.006	.7	.0	2.5	.0	-.01	50.0	66.0	17.0	1.9	0.	0.	31.	0.	0.	.22
F520G5.007	1.5	15.9	16.0	16.0	.01	50.0	50.0	17.0	3.9	0.	0.	197.	0.	0.	.49
F520G5.008	1.1	15.7	15.7	15.8	.04	50.0	33.0	17.0	3.0	0.	0.	194.	0.	0.	1.49
F520G5.009	1.2	11.3	11.3	15.5	.08	50.0	.0	17.0	3.1	0.	0.	140.	0.	0.	3.12
F520G5.010	.8	.0	16.4	.0	-.01	50.0	-33.0	17.0	2.3	0.	0.	202.	0.	0.	.65
F520G5.011	1.2	9.2	9.2	16.0	-.01	50.0	-50.0	17.0	3.1	0.	0.	113.	0.	0.	.44
F520G5.012	.1	.0	.0	.0	-.01	50.0	-66.0	17.0	.3	0.	0.	0.	0.	0.	.14
F520H1.006	1.0	.0	44.2	.0	.32	150.0	84.0	1.0	2.6	0.	0.	545.	0.	0.	10.65
F520H1.007	.4	.0	15.1	.0	.06	150.0	56.0	1.0	1.2	0.	0.	186.	0.	0.	1.99
F520H1.008	.0	.0	.0	.0	-.17	150.0	28.0	1.0	.1	0.	0.	0.	0.	0.	.02
F520H1.009	.5	.0	20.3	.0	.04	150.0	.0	1.0	1.3	0.	0.	251.	0.	0.	1.79
F520H1.010	.5	.0	24.1	.0	.07	150.0	-28.0	1.0	1.3	0.	0.	297.	0.	0.	2.32
F520H1.011	.7	.0	23.1	.0	.10	150.0	-56.0	1.0	1.8	0.	0.	284.	0.	0.	3.32
F520H1.012	.3	.0	23.0	.0	.02	150.0	-84.0	1.0	.9	0.	0.	283.	0.	0.	.96
F520H2.006	.2	.0	.0	.0	-.19	150.0	84.0	1.0	.5	0.	0.	0.	0.	0.	.18
F520H2.007	.7	.0	17.6	.0	.06	150.0	56.0	1.0	1.8	0.	0.	217.	0.	0.	2.12
F520H2.008	.5	.0	19.6	.0	.02	150.0	28.0	1.0	1.4	0.	0.	241.	0.	0.	1.29
F520H2.009	1.0	7.2	7.2	7.2	-.28	150.0	.0	1.0	2.7	0.	0.	89.	0.	0.	2.55
F520H2.010	.4	.0	19.7	.0	.03	150.0	-28.0	1.0	1.1	0.	0.	242.	0.	0.	1.01
F520H2.011	.2	.0	.0	.0	.01	150.0	-56.0	1.0	.5	0.	0.	0.	0.	0.	.80
F520H2.012	.1	.0	.0	.0	.02	150.0	-84.0	1.0	.3	0.	0.	0.	0.	0.	.87
F520H3.006	.4	.0	17.7	.0	.00	150.0	84.0	1.0	1.2	0.	0.	219.	0.	0.	.62
F520H3.007	.5	.0	21.3	.0	.04	150.0	56.0	1.0	1.3	0.	0.	263.	0.	0.	1.48
F520I1.006	.1	.0	.0	.0	-.71	150.0	84.0	5.0	.4	0.	0.	0.	0.	0.	.18
F520I1.007	.2	.0	27.4	.0	.01	150.0	56.0	5.0	.6	0.	0.	338.	0.	0.	.57
F520I1.008	.3	.0	26.8	.0	.01	150.0	28.0	5.0	.8	0.	0.	330.	0.	0.	.60
F520I1.009	.5	.0	22.3	.0	.06	150.0	.0	5.0	1.3	0.	0.	275.	0.	0.	2.15
F520I1.010	.6	.0	14.9	.0	.08	150.0	-28.0	5.0	1.5	0.	0.	184.	0.	0.	2.54
F520I1.011	.7	.0	21.7	.0	.06	150.0	-56.0	5.0	1.9	0.	0.	267.	0.	0.	2.30
F520I1.012	.3	.0	22.1	.0	.05	150.0	-84.0	5.0	.8	0.	0.	272.	0.	0.	1.59
F520I2.006	.1	.0	.0	.0	-.09	150.0	84.0	5.0	.3	0.	0.	0.	0.	0.	.14
F520I2.007	.4	.0	13.4	.0	.00	150.0	56.0	5.0	1.2	0.	0.	165.	0.	0.	.74
F520I2.008	.6	.0	14.3	.0	.04	150.0	28.0	5.0	1.7	0.	0.	176.	0.	0.	1.73
F520I2.009	.8	.0	18.1	.0	.06	150.0	.0	5.0	2.2	0.	0.	224.	0.	0.	2.30
F520I2.010	.6	.0	15.5	.0	.05	150.0	-28.0	5.0	1.7	0.	0.	190.	0.	0.	1.98
F520I2.011	.7	.0	19.5	.0	.09	150.0	-56.0	5.0	1.8	0.	0.	240.	0.	0.	3.18

FALCON 5: LSR = 200, GAS = ARGON

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F520I2.012	.3	.0	22.6	.0	.01	150.0	-84.0	5.0	.7	0.	0.	278.	0.	0.	.57
F520I3.006	.1	.0	.0	.0	-.21	150.0	84.0	5.0	.2	0.	0.	0.	0.	0.	.00
F520I3.007	.3	.0	24.9	.0	.02	150.0	56.0	5.0	.8	0.	0.	307.	0.	0.	.89
F520I3.008	.5	.0	24.4	.0	.04	150.0	28.0	5.0	1.4	0.	0.	301.	0.	0.	1.63
F520I3.009	.6	.0	13.5	.0	.06	150.0	.0	5.0	1.5	0.	0.	166.	0.	0.	2.15
F520I3.010	.7	.0	19.3	.0	.06	150.0	-28.0	5.0	1.9	0.	0.	238.	0.	0.	1.95
F520I3.011	.6	.0	22.1	.0	.02	150.0	-56.0	5.0	1.7	0.	0.	273.	0.	0.	1.11
F520I3.012	.5	.0	22.8	.0	.04	150.0	-84.0	5.0	1.5	0.	0.	281.	0.	0.	1.29
F520I4.006	.4	.0	29.4	.0	.11	150.0	84.0	5.0	1.1	0.	0.	362.	0.	0.	3.65
F520I4.007	.3	.0	16.9	.0	-.03	150.0	56.0	5.0	.8	0.	0.	208.	0.	0.	.20
F520I4.008	.7	.0	20.6	.0	.08	150.0	28.0	5.0	2.0	0.	0.	254.	0.	0.	2.72
F520I4.009	.4	.0	14.7	.0	.06	150.0	.0	5.0	1.2	0.	0.	181.	0.	0.	2.24
F520I4.010	.6	.0	15.1	.0	.04	150.0	-28.0	5.0	1.5	0.	0.	187.	0.	0.	1.47
F520I4.011	.6	.0	14.6	.0	.05	150.0	-56.0	5.0	1.6	0.	0.	180.	0.	0.	1.85
F520I4.012	.2	.0	.0	.0	.00	150.0	-84.0	5.0	.5	0.	0.	0.	0.	0.	.33
F520I5.006	.0	.0	.0	.0	-.09	150.0	84.0	5.0	.0	0.	0.	0.	0.	0.	.00
F520I5.007	.6	.0	18.1	.0	.04	150.0	56.0	5.0	1.7	0.	0.	223.	0.	0.	1.59
F520I5.008	.5	.0	20.4	.0	.04	150.0	28.0	5.0	1.5	0.	0.	251.	0.	0.	1.53
F520I5.009	.6	.0	20.6	.0	.08	150.0	.0	5.0	1.7	0.	0.	254.	0.	0.	2.83
F520I5.010	.4	.0	13.5	.0	.07	150.0	-28.0	5.0	1.2	0.	0.	167.	0.	0.	2.30
F520I5.011	.5	.0	16.0	.0	.02	150.0	-56.0	5.0	1.3	0.	0.	197.	0.	0.	1.02
F520I5.012	.1	.0	.0	.0	-.02	150.0	-84.0	5.0	.2	0.	0.	0.	0.	0.	.12
F520J1.006	.3	.0	12.0	.0	-.03	150.0	84.0	11.0	.9	0.	0.	147.	0.	0.	.07
F520J1.007	.5	.0	12.0	.0	.04	150.0	56.0	11.0	1.4	0.	0.	148.	0.	0.	1.38
F520J1.008	.6	.0	15.1	.0	.03	150.0	28.0	11.0	1.6	0.	0.	186.	0.	0.	1.24
F520J1.009	.5	.0	14.5	.0	.04	150.0	.0	11.0	1.3	0.	0.	178.	0.	0.	1.55
F520J1.010	.5	.0	22.7	.0	.03	150.0	-28.0	11.0	1.4	0.	0.	280.	0.	0.	1.34
F520J1.011	.7	.0	20.0	.0	.05	150.0	-56.0	11.0	2.0	0.	0.	247.	0.	0.	1.90
F520J1.012	.2	.0	.0	.0	-.01	150.0	-84.0	11.0	.5	0.	0.	0.	0.	0.	.14
F520J1.006	.3	.0	12.0	.0	-.03	150.0	84.0	11.0	.9	0.	0.	147.	0.	0.	.07
F520J2.007	.3	.0	27.9	.0	.02	150.0	56.0	11.0	.8	0.	0.	344.	0.	0.	.83
F520J2.008	.4	.0	19.6	.0	.02	150.0	28.0	11.0	1.1	0.	0.	242.	0.	0.	.88
F520J2.009	.5	.0	14.3	.0	.03	150.0	.0	11.0	1.2	0.	0.	176.	0.	0.	1.40
F520J2.010	.8	.0	22.4	.0	.07	150.0	-28.0	11.0	2.1	0.	0.	276.	0.	0.	2.36
F520J2.011	.7	.0	15.3	.0	.07	150.0	-56.0	11.0	1.9	0.	0.	188.	0.	0.	2.27
F520J2.012	.4	.0	24.4	.0	.02	150.0	-84.0	11.0	1.2	0.	0.	301.	0.	0.	.80
F520J3.006	.0	.0	.0	.0	-.08	150.0	84.0	11.0	.0	0.	0.	0.	0.	0.	.00
F520J3.007	.3	.0	17.5	.0	.00	150.0	56.0	11.0	.9	0.	0.	216.	0.	0.	.58
F520J3.008	.6	.0	17.6	.0	.07	150.0	28.0	11.0	1.7	0.	0.	217.	0.	0.	2.39
F520J3.009	.4	.0	18.2	.0	.02	150.0	.0	11.0	1.1	0.	0.	225.	0.	0.	1.27
F520J3.010	.9	.0	20.0	.0	.18	150.0	-28.0	11.0	2.3	0.	0.	246.	0.	0.	6.10
F520J3.011	.6	.0	20.1	.0	.04	150.0	-56.0	11.0	1.5	0.	0.	248.	0.	0.	1.51

FALCON 5: LSR = 200, GAS = ARGON

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F520J3.012	.5	.0	20.4	.0	.03	150.0	-84.0	11.0	1.4	0.	0.	251.	0.	0.	1.11
F520J4.006	.2	.0	.0	.0	.02	150.0	84.0	11.0	.5	0.	0.	0.	0.	0.	.61
F520J4.007	.5	.0	4.8	.0	.00	150.0	56.0	11.0	1.4	0.	0.	59.	0.	0.	.31
F520J4.008	.4	.0	4.0	.0	.02	150.0	28.0	11.0	1.0	0.	0.	49.	0.	0.	1.08
F520J4.009	.6	.0	20.3	.0	.05	150.0	.0	11.0	1.6	0.	0.	250.	0.	0.	1.95
F520J4.010	.6	.0	20.3	.0	.04	150.0	-28.0	11.0	1.5	0.	0.	250.	0.	0.	1.46
F520J4.011	.7	.0	23.6	.0	.08	150.0	-56.0	11.0	1.9	0.	0.	291.	0.	0.	2.78
F520J4.012	.5	.0	19.7	.0	.04	150.0	-84.0	11.0	1.3	0.	0.	243.	0.	0.	1.23
F520J5.006	.4	.0	10.6	.0	.03	150.0	84.0	11.0	1.2	0.	0.	131.	0.	0.	2.28
F520J5.007	.4	.0	4.5	.0	-.01	150.0	56.0	11.0	1.1	0.	0.	56.	0.	0.	.25
F520J5.008	.3	.0	5.4	.0	-.02	150.0	28.0	11.0	.8	0.	0.	66.	0.	0.	.31
F520J5.009	.4	.0	12.6	.0	.02	150.0	.0	11.0	1.0	0.	0.	156.	0.	0.	.90
F520J5.010	.7	.0	14.9	.0	.08	150.0	-28.0	11.0	1.9	0.	0.	184.	0.	0.	2.71
F520J5.011	.9	.0	18.9	.0	.15	150.0	-56.0	11.0	2.5	0.	0.	232.	0.	0.	4.88
F520J5.012	.4	.0	17.5	.0	.04	150.0	-84.0	11.0	1.0	0.	0.	215.	0.	0.	1.42
F520K1.006	.1	.0	.0	.0	.02	150.0	84.0	17.0	.3	0.	0.	0.	0.	0.	.63
F520K1.007	.1	.0	.0	.0	.00	150.0	56.0	17.0	.3	0.	0.	0.	0.	0.	.44
F520K1.008	.3	.0	5.9	.0	-.02	150.0	28.0	17.0	.9	0.	0.	73.	0.	0.	.20
F520K1.009	.4	.0	17.2	.0	.03	150.0	.0	17.0	1.2	0.	0.	212.	0.	0.	1.18
F520K1.010	.6	.0	20.0	.0	.07	150.0	-28.0	17.0	1.6	0.	0.	247.	0.	0.	2.23
F520K1.011	.7	.0	18.5	.0	.07	150.0	-56.0	17.0	1.8	0.	0.	229.	0.	0.	2.62
F520K1.012	.5	.0	22.4	.0	.02	150.0	-84.0	17.0	1.4	0.	0.	276.	0.	0.	.87
F520K2.006	.2	.0	13.9	.0	.00	150.0	84.0	17.0	.6	0.	0.	171.	0.	0.	.24
F520K2.007	.7	.0	17.4	.0	-.01	150.0	56.0	17.0	1.9	0.	0.	215.	0.	0.	.28
F520K2.008	.7	.0	16.9	.0	.01	150.0	28.0	17.0	1.9	0.	0.	209.	0.	0.	.74
F520K2.009	.7	.0	18.2	.0	.04	150.0	.0	17.0	1.8	0.	0.	225.	0.	0.	1.65
F520K2.010	.6	.0	20.2	.0	.03	150.0	-28.0	17.0	1.5	0.	0.	248.	0.	0.	1.26
F520K2.011	.7	.0	23.4	.0	.00	150.0	-56.0	17.0	1.7	0.	0.	289.	0.	0.	.54
F520K2.012	.3	.0	19.6	.0	.01	150.0	-84.0	17.0	.8	0.	0.	241.	0.	0.	.39
F520K3.006	.2	.0	.0	.0	-.02	150.0	84.0	17.0	.5	0.	0.	0.	0.	0.	.04
F520K3.007	.7	.0	21.4	.0	.01	150.0	56.0	17.0	1.9	0.	0.	263.	0.	0.	.73
F520K3.008	.5	.0	16.6	.0	.07	150.0	28.0	17.0	1.4	0.	0.	205.	0.	0.	2.35
F520K3.009	.5	.0	18.0	.0	.03	150.0	.0	17.0	1.3	0.	0.	222.	0.	0.	1.41
F520K3.010	.5	.0	17.3	.0	.02	150.0	-28.0	17.0	1.3	0.	0.	213.	0.	0.	.98
F520K3.011	.2	.0	28.6	.0	-.01	150.0	-56.0	17.0	.6	0.	0.	353.	0.	0.	.33
F520K3.012	.3	.0	28.5	.0	.01	150.0	-84.0	17.0	.8	0.	0.	351.	0.	0.	.62
F520K4.006	.1	.0	.0	.0	-.01	150.0	84.0	17.0	.3	0.	0.	0.	0.	0.	.03
F520K4.007	.3	.0	36.7	.0	-.01	150.0	56.0	17.0	.9	0.	0.	453.	0.	0.	.23
F520K4.008	.4	.0	22.2	.0	.03	150.0	28.0	17.0	1.0	0.	0.	274.	0.	0.	1.07
F520K4.009	.5	.0	17.3	.0	.07	150.0	.0	17.0	1.3	0.	0.	214.	0.	0.	2.34
F520K4.010	.5	.0	20.1	.0	.04	150.0	-28.0	17.0	1.2	0.	0.	248.	0.	0.	1.45
F520K4.011	.4	.0	17.3	.0	.02	150.0	-56.0	17.0	1.0	0.	0.	213.	0.	0.	.96

FALCON 5: LSR = 200, GAS = ARGON

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
F520K4.012	.2	.0	.0	.0	-.01	150.0	-84.0	17.0	.5	0.	0.	0.	0.	0.	.14
F520K5.006	.4	.0	20.4	.0	.08	150.0	84.0	17.0	1.2	0.	0.	252.	0.	0.	2.54
F520K5.007	.5	.0	20.3	.0	.02	150.0	56.0	17.0	1.3	0.	0.	251.	0.	0.	.68
F520K5.008	.5	.0	22.8	.0	.04	150.0	28.0	17.0	1.4	0.	0.	281.	0.	0.	1.43
F520K5.009	.5	.0	15.9	.0	.04	150.0	.0	17.0	1.3	0.	0.	196.	0.	0.	1.66
F520K5.010	.4	.0	19.7	.0	.02	150.0	-28.0	17.0	1.1	0.	0.	243.	0.	0.	.85
F520K5.011	.4	.0	19.2	.0	.00	150.0	-56.0	17.0	1.2	0.	0.	237.	0.	0.	.47
F520K5.012	.2	.0	.0	.0	.00	150.0	-84.0	17.0	.5	0.	0.	0.	0.	0.	.36

FALCON 4: LSR = 150, GAS = FREON 12

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415A1.009	.4	.0	10.8	.0	-.19	-62.0	30.0	2.0	1.1	0.	0.	333.	0.	0.	.08
D415A1.008	21.5	2.5	10.1	22.1	1.02	-62.0	20.0	2.0	42.6	86.	94.	314.	493.	541.	81.40
D415A1.007	22.9	1.4	10.1	65.5	1.68	-62.0	10.0	2.0	44.5	68.	72.	314.	511.	668.	119.16
D415A1.006	22.1	1.0	10.1	103.0	1.83	-62.0	.0	2.0	43.4	47.	64.	312.	514.	1199.	128.31
D415A1.005	20.2	1.0	9.7	26.3	1.26	-62.0	-10.0	2.0	40.6	40.	51.	300.	450.	632.	93.66
D415A1.004	17.7	1.4	10.9	17.5	.87	-62.0	-20.0	2.0	36.8	44.	76.	337.	458.	459.	69.78
D415A2.009	.8	.0	7.1	.0	.03	-62.0	30.0	2.0	2.2	0.	0.	219.	0.	0.	2.24
D415A2.008	25.5	1.1	8.1	39.5	1.74	-62.0	20.0	2.0	48.1	40.	58.	252.	556.	671.	121.90
D415A2.007	21.6	1.1	8.5	61.5	2.15	-62.0	10.0	2.0	42.7	36.	38.	262.	547.	1771.	149.91
D415A2.006	24.7	.8	10.3	115.3	2.17	-62.0	.0	2.0	47.0	26.	29.	319.	556.	1503.	150.82
D415A2.005	21.2	.7	9.2	101.0	1.70	-62.0	-10.0	2.0	42.1	21.	23.	284.	869.	871.	120.75
D415A2.004	20.6	.5	6.4	116.4	1.51	-62.0	-20.0	2.0	41.2	18.	33.	197.	432.	763.	106.11
D415A3.009	.4	.0	14.1	.0	.02	-62.0	30.0	2.0	1.2	0.	0.	438.	0.	0.	1.50
D415A3.008	25.0	.3	9.6	109.5	2.02	-62.0	20.0	2.0	47.4	9.	17.	297.	622.	1790.	139.01
D415A3.007	23.7	.8	9.4	80.7	2.26	-62.0	10.0	2.0	45.6	25.	30.	291.	507.	1033.	155.18
D415A3.006	25.4	.5	9.6	118.4	2.30	-62.0	.0	2.0	47.9	19.	29.	296.	643.	1039.	158.64
D415A3.005	24.5	.6	9.8	113.6	1.66	-62.0	-10.0	2.0	46.8	27.	33.	303.	629.	1657.	118.52
D415A3.004	22.4	.6	8.8	105.5	1.41	-62.0	-20.0	2.0	43.8	19.	36.	273.	470.	1986.	100.70
D415A4.009	.9	.0	10.8	.0	-.01	-62.0	30.0	2.0	2.4	0.	0.	333.	0.	0.	.65
D415A4.008	28.8	.3	8.1	115.8	2.09	-62.0	20.0	2.0	52.2	10.	10.	251.	608.	2294.	144.20
D415A4.007	23.5	.5	10.2	102.4	2.52	-62.0	10.0	2.0	45.4	18.	28.	316.	603.	745.	173.06
D415A4.006	25.7	.6	9.8	115.1	2.51	-62.0	.0	2.0	48.3	18.	28.	305.	649.	1282.	171.92
D415A4.005	24.0	.4	8.2	86.5	1.77	-62.0	-10.0	2.0	46.0	14.	41.	254.	876.	1582.	125.85
D415A4.004	20.9	1.3	10.8	109.3	1.65	-62.0	-20.0	2.0	41.7	44.	49.	336.	1199.	3118.	114.55
D415A5.009	.9	.0	10.4	.0	.00	-62.0	30.0	2.0	2.4	0.	0.	321.	0.	0.	.81
D415A5.008	24.3	.3	11.0	119.7	2.10	-62.0	20.0	2.0	46.4	10.	10.	341.	656.	2687.	144.67
D415A5.007	26.8	.7	10.2	101.2	2.42	-62.0	10.0	2.0	49.8	23.	34.	315.	573.	1330.	165.98
D415A5.006	24.5	.5	10.3	120.1	2.30	-62.0	.0	2.0	46.7	20.	24.	318.	628.	1028.	159.89
D415A5.005	23.3	.5	10.2	114.8	1.72	-62.0	-10.0	2.0	45.1	23.	24.	315.	849.	1537.	122.58
D415A5.004	26.2	.5	10.6	95.5	1.50	-62.0	-20.0	2.0	48.9	15.	16.	327.	701.	1946.	105.23
D415B1.009	.5	.0	6.4	.0	.03	-32.0	30.0	1.0	1.2	0.	0.	198.	0.	0.	2.52
D415B1.008	22.8	.4	7.3	67.7	1.61	-32.0	20.0	1.0	44.4	13.	20.	225.	626.	780.	114.46
D415B1.007	26.1	.2	11.1	16.3	1.37	-32.0	10.0	1.0	48.8	8.	11.	344.	376.	403.	95.73
D415B1.006	29.8	.3	9.5	15.3	1.49	-32.0	.0	1.0	53.5	9.	17.	294.	388.	399.	100.31
D415B1.005	17.4	.2	8.2	18.2	.92	-32.0	-10.0	1.0	36.3	7.	28.	255.	391.	499.	69.31
D415B1.004	16.2	.3	7.9	55.8	.89	-32.0	-20.0	1.0	34.4	11.	28.	244.	408.	656.	67.16
D415B2.009	.7	.0	11.7	.0	.02	-32.0	30.0	1.0	1.9	0.	0.	363.	0.	0.	2.09
D415B2.008	23.9	.3	8.9	70.5	1.77	-32.0	20.0	1.0	45.9	9.	10.	276.	559.	1399.	124.57
D415B2.007	23.3	.2	9.1	16.5	1.42	-32.0	10.0	1.0	45.1	5.	12.	282.	390.	401.	97.95
D415B2.006	27.6	.3	4.5	15.6	1.39	-32.0	.0	1.0	50.7	13.	26.	139.	383.	397.	94.93
D415B2.005	22.5	.2	6.4	23.5	1.09	-32.0	-10.0	1.0	44.0	7.	12.	197.	408.	508.	78.89
D415B2.004	21.3	.3	6.7	77.8	1.03	-32.0	-20.0	1.0	42.3	19.	22.	207.	380.	723.	75.68

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415B3.009	.8	.0	6.2	.0	.02	-32.0	30.0	1.0	2.2	0.	0.	191.	0.	0.	1.50
D415B3.008	23.1	.3	9.1	70.1	1.60	-32.0	20.0	1.0	44.8	8.	12.	282.	611.	2169.	113.65
D415B3.007	23.8	.2	7.1	15.4	1.30	-32.0	10.0	1.0	45.8	5.	10.	221.	384.	425.	91.15
D415B3.006	26.3	.3	9.2	15.1	1.34	-32.0	.0	1.0	49.2	10.	11.	283.	366.	422.	91.19
D415B3.005	21.5	.3	6.8	19.3	1.11	-32.0	-10.0	1.0	42.5	8.	19.	210.	382.	436.	80.34
D415B3.004	18.4	.6	7.8	44.0	.97	-32.0	-20.0	1.0	37.9	19.	29.	241.	399.	1362.	72.21
D415B4.009	.6	.0	10.3	.0	.02	-32.0	30.0	1.0	1.5	0.	0.	318.	0.	0.	1.43
D415B4.008	24.2	.4	10.1	80.9	1.73	-32.0	20.0	1.0	46.3	11.	17.	313.	690.	2108.	121.81
D415B4.007	23.4	.2	8.2	18.2	1.41	-32.0	10.0	1.0	45.3	5.	7.	252.	365.	404.	97.88
D415B4.006	26.9	.3	5.0	15.4	1.17	-32.0	.0	1.0	49.8	10.	23.	154.	380.	429.	81.80
D415B4.005	22.7	.3	4.8	22.7	1.01	-32.0	-10.0	1.0	44.3	10.	11.	150.	353.	539.	74.27
D415B4.004	19.7	.4	5.1	84.2	1.00	-32.0	-20.0	1.0	39.8	14.	23.	157.	394.	626.	74.44
D415B5.009	.4	.0	9.1	.0	.00	-32.0	30.0	1.0	1.1	0.	0.	282.	0.	0.	.74
D415B5.008	25.7	.2	6.9	86.7	1.70	-32.0	20.0	1.0	48.3	9.	24.	214.	609.	1149.	119.81
D415B5.007	23.0	.2	8.4	16.5	1.35	-32.0	10.0	1.0	44.7	6.	7.	260.	396.	445.	94.30
D415B5.006	23.7	.3	6.5	16.5	1.22	-32.0	.0	1.0	45.6	10.	22.	201.	417.	428.	84.83
D415B5.005	23.2	.2	5.7	19.3	1.13	-32.0	-10.0	1.0	45.0	7.	28.	178.	386.	478.	81.59
D415B5.004	19.2	.3	4.9	49.1	.97	-32.0	-20.0	1.0	39.2	9.	27.	151.	448.	800.	72.63
D415C1.009	.7	.0	10.0	.0	.01	-2.0	30.0	1.0	1.8	0.	0.	308.	0.	0.	1.95
D415C1.008	3.1	4.3	7.6	12.5	.16	-2.0	20.0	1.0	8.1	162.	0.	234.	0.	275.	12.95
D415C1.007	2.4	4.1	9.1	12.4	.14	-2.0	10.0	1.0	6.1	218.	0.	280.	0.	281.	11.80
D415C1.006	2.6	3.6	8.7	12.3	.12	-2.0	.0	1.0	6.7	161.	0.	269.	0.	324.	10.54
D415C1.005	2.8	3.5	8.3	12.2	.14	-2.0	-10.0	1.0	7.2	157.	0.	256.	0.	301.	11.74
D415C1.004	3.0	4.2	9.7	12.3	.14	-2.0	-20.0	1.0	7.7	299.	0.	299.	0.	306.	12.12
D415C2.009	.8	.0	11.9	.0	.03	-2.0	30.0	1.0	2.1	0.	0.	369.	0.	0.	2.82
D415C2.008	6.1	2.6	8.0	12.7	.17	-2.0	20.0	1.0	15.0	215.	247.	247.	250.	334.	13.95
D415C2.007	2.6	3.5	8.5	11.9	.16	-2.0	10.0	1.0	6.8	213.	0.	264.	0.	318.	12.91
D415C2.006	2.7	4.4	8.4	12.5	.14	-2.0	.0	1.0	6.9	215.	0.	261.	0.	279.	11.25
D415C2.005	2.1	1.6	7.6	12.5	.15	-2.0	-10.0	1.0	5.5	235.	0.	235.	0.	281.	12.68
D415C2.004	1.6	2.8	10.3	12.1	.15	-2.0	-20.0	1.0	4.3	0.	0.	320.	0.	0.	12.30
D415C3.009	.7	.0	11.3	.0	.02	-2.0	30.0	1.0	1.8	0.	0.	350.	0.	0.	1.78
D415C3.008	2.9	3.2	9.0	12.6	.16	-2.0	20.0	1.0	7.4	120.	0.	279.	0.	331.	12.95
D415C3.007	2.3	.8	8.9	12.5	.14	-2.0	10.0	1.0	6.0	120.	0.	276.	0.	277.	11.80
D415C3.006	3.3	.8	10.4	12.5	.13	-2.0	.0	1.0	8.5	273.	0.	323.	0.	324.	10.82
D415C3.005	2.6	2.5	10.0	12.8	.14	-2.0	-10.0	1.0	6.6	122.	0.	311.	0.	331.	11.82
D415C3.004	2.4	3.5	10.1	12.6	.14	-2.0	-20.0	1.0	6.3	312.	0.	312.	0.	325.	11.55
D415C4.009	1.2	11.6	11.6	11.6	.03	-2.0	30.0	1.0	3.2	0.	0.	360.	0.	0.	2.28
D415C4.008	2.7	2.6	6.9	12.4	.15	-2.0	20.0	1.0	6.9	183.	0.	212.	0.	281.	12.61
D415C4.007	5.0	2.9	9.0	11.4	.14	-2.0	10.0	1.0	12.4	182.	277.	278.	279.	301.	11.91
D415C4.006	2.1	2.7	9.0	12.8	.13	-2.0	.0	1.0	5.5	141.	0.	278.	0.	308.	11.03
D415C4.005	2.3	2.8	10.2	12.8	.14	-2.0	-10.0	1.0	6.1	206.	0.	315.	0.	316.	11.56
D415C4.004	2.1	4.7	10.3	11.9	.14	-2.0	-20.0	1.0	5.6	165.	0.	318.	0.	324.	11.92

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415C5.009	.4	.0	9.8	.0	.01	-2.0	30.0	1.0	1.1	0.	0.	304.	0.	0.	1.38
D415C5.008	3.5	1.4	10.5	12.2	.15	-2.0	20.0	1.0	8.9	241.	0.	324.	0.	327.	12.48
D415C5.007	3.5	1.3	10.2	13.3	.15	-2.0	10.0	1.0	9.0	249.	0.	315.	0.	334.	12.10
D415C5.006	5.9	1.5	10.2	13.4	.13	-2.0	.0	1.0	14.5	155.	315.	315.	318.	337.	10.85
D415C5.005	6.0	1.4	10.2	12.7	.14	-2.0	-10.0	1.0	14.7	156.	317.	317.	319.	327.	11.92
D415C5.004	3.1	5.1	10.3	12.3	.14	-2.0	-20.0	1.0	8.0	242.	0.	320.	0.	331.	11.61
D415D1.009	.0	.0	.0	.0	.00	50.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.02
D415D1.008	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.12
D415D1.007	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.09
D415D1.006	.2	.0	.0	.0	.00	50.0	33.0	1.0	.4	0.	0.	0.	0.	0.	.23
D415D1.005	.6	.0	10.6	.0	.01	50.0	25.0	1.0	1.6	0.	0.	328.	0.	0.	.47
D415D1.004	.8	.0	10.7	.0	.07	50.0	.0	1.0	2.2	0.	0.	331.	0.	0.	6.05
D415D2.009	.0	.0	.0	.0	-.01	50.0	75.0	1.0	.0	0.	0.	0.	0.	0.	.01
D415D2.008	.0	.0	.0	.0	-.01	50.0	66.0	1.0	.0	0.	0.	0.	0.	0.	.00
D415D2.007	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.02
D415D2.006	.2	.0	4.4	.0	.00	50.0	33.0	1.0	.6	0.	0.	136.	0.	0.	.29
D415D2.005	.4	.0	8.1	.0	.00	50.0	25.0	1.0	1.1	0.	0.	251.	0.	0.	.50
D415D2.004	1.2	9.3	9.5	10.6	.08	50.0	.0	1.0	3.2	0.	0.	293.	0.	0.	6.75
D415D3.009	.0	.0	.0	.0	.00	50.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.06
D415D3.008	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.00
D415D3.007	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.25
D415D3.006	.1	.0	.0	.0	.00	50.0	33.0	1.0	.4	0.	0.	0.	0.	0.	.28
D415D3.005	.4	.0	11.3	.0	.01	50.0	25.0	1.0	1.0	0.	0.	349.	0.	0.	.55
D415D3.004	1.0	.0	7.4	.0	.07	50.0	.0	1.0	2.6	0.	0.	228.	0.	0.	6.23
D415D4.009	.0	.0	.0	.0	.00	50.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.18
D415D4.008	.0	.0	.0	.0	.00	50.0	66.0	1.0	.1	0.	0.	0.	0.	0.	.56
D415D4.007	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.18
D415D4.006	.2	.0	.0	.0	.00	50.0	33.0	1.0	.4	0.	0.	0.	0.	0.	.42
D415D4.005	.5	.0	8.8	.0	.01	50.0	25.0	1.0	1.4	0.	0.	272.	0.	0.	.60
D415D4.004	1.0	9.8	9.8	9.8	.08	50.0	.0	1.0	2.7	0.	0.	304.	0.	0.	6.50
D415D5.009	.0	.0	.0	.0	.00	50.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.13
D415D5.008	.1	.0	.0	.0	.00	50.0	66.0	1.0	.2	0.	0.	0.	0.	0.	.11
D415D5.007	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.08
D415D5.006	.1	.0	.0	.0	.00	50.0	33.0	1.0	.3	0.	0.	0.	0.	0.	.37
D415D5.005	.6	.0	9.8	.0	.01	50.0	25.0	1.0	1.6	0.	0.	304.	0.	0.	.72
D415D5.004	.9	.0	9.6	.0	.07	50.0	.0	1.0	2.5	0.	0.	298.	0.	0.	6.09
D415E1.009	.0	.0	.0	.0	.00	50.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.20
D415E1.008	.1	.0	.0	.0	.00	50.0	66.0	5.0	.1	0.	0.	0.	0.	0.	.44
D415E1.007	.0	.0	.0	.0	.00	50.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.08
D415E1.006	.3	.0	7.1	.0	.00	50.0	33.0	5.0	.8	0.	0.	219.	0.	0.	.49
D415E1.005	.4	.0	11.7	.0	.01	50.0	25.0	5.0	1.1	0.	0.	362.	0.	0.	.62
D415E1.004	1.0	.0	10.1	.0	.07	50.0	.0	5.0	2.6	0.	0.	312.	0.	0.	5.84

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415E2.009	.0	.0	.0	.0	.00	50.0	75.0	5.0	.0	0.	0.	0.	0.	0.	.10
D415E2.008	.0	.0	.0	.0	.00	50.0	66.0	5.0	.0	0.	0.	0.	0.	0.	.00
D415E2.007	.0	.0	.0	.0	.00	50.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.00
D415E2.006	.3	.0	16.0	.0	.00	50.0	33.0	5.0	.8	0.	0.	495.	0.	0.	.41
D415E2.005	.7	.0	11.6	.0	.01	50.0	25.0	5.0	1.8	0.	0.	359.	0.	0.	.56
D415E2.004	.9	.0	11.6	.0	.07	50.0	.0	5.0	2.4	0.	0.	359.	0.	0.	6.07
D415E3.009	.0	.0	.0	.0	.00	50.0	75.0	5.0	.0	0.	0.	0.	0.	0.	.07
D415E3.008	.0	.0	.0	.0	.00	50.0	66.0	5.0	.0	0.	0.	0.	0.	0.	.08
D415E3.007	.0	.0	.0	.0	.00	50.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.09
D415E3.006	.2	.0	13.3	.0	.00	50.0	33.0	5.0	.6	0.	0.	410.	0.	0.	.21
D415E3.005	.8	.0	11.0	.0	.00	50.0	25.0	5.0	2.2	0.	0.	340.	0.	0.	.58
D415E3.004	.9	.0	10.3	.0	.07	50.0	.0	5.0	2.5	0.	0.	318.	0.	0.	5.92
D415E4.009	.0	.0	.0	.0	.00	50.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.07
D415E4.008	.0	.0	.0	.0	.00	50.0	66.0	5.0	.0	0.	0.	0.	0.	0.	.00
D415E4.007	.0	.0	.0	.0	.00	50.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.02
D415E4.006	.4	.0	11.7	.0	.00	50.0	33.0	5.0	1.0	0.	0.	362.	0.	0.	.41
D415E4.005	.5	.0	8.6	.0	.01	50.0	25.0	5.0	1.4	0.	0.	267.	0.	0.	.57
D415E4.004	1.0	.0	10.6	.0	.08	50.0	.0	5.0	2.6	0.	0.	329.	0.	0.	6.59
D415E5.009	.0	.0	.0	.0	.00	50.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.07
D415E5.008	.1	.0	.0	.0	.00	50.0	66.0	5.0	.2	0.	0.	0.	0.	0.	.19
D415E5.007	.0	.0	.0	.0	.00	50.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.19
D415E5.006	.2	.0	10.8	.0	.00	50.0	33.0	5.0	.6	0.	0.	335.	0.	0.	.41
D415E5.005	.6	.0	8.2	.0	.01	50.0	25.0	5.0	1.5	0.	0.	254.	0.	0.	.80
D415E5.004	1.1	9.9	9.9	9.9	.07	50.0	.0	5.0	2.9	0.	0.	307.	0.	0.	6.21
D415F1.009	.0	.0	.0	.0	.00	50.0	75.0	11.0	.0	0.	0.	0.	0.	0.	.03
D415F1.008	.0	.0	.0	.0	.00	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.27
D415F1.007	.0	.0	.0	.0	.00	50.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.08
D415F1.006	.1	.0	.0	.0	.00	50.0	33.0	11.0	.3	0.	0.	0.	0.	0.	.09
D415F1.005	.6	.0	7.4	.0	.01	50.0	25.0	11.0	1.7	0.	0.	229.	0.	0.	.65
D415F1.004	.7	.0	8.2	.0	.05	50.0	.0	11.0	1.9	0.	0.	254.	0.	0.	4.10
D415F2.009	.0	.0	.0	.0	.00	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.21
D415F2.008	.0	.0	.0	.0	.00	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.08
D415F2.007	.0	.0	.0	.0	.00	50.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.01
D415F2.006	.2	.0	6.4	.0	.00	50.0	33.0	11.0	.6	0.	0.	199.	0.	0.	.18
D415F2.005	.5	.0	5.8	.0	.00	50.0	25.0	11.0	1.4	0.	0.	179.	0.	0.	.52
D415F2.004	.6	.0	6.7	.0	.03	50.0	.0	11.0	1.7	0.	0.	209.	0.	0.	2.57
D415F3.009	.0	.0	.0	.0	.00	50.0	75.0	11.0	.0	0.	0.	0.	0.	0.	.00
D415F3.008	.0	.0	.0	.0	.00	50.0	66.0	11.0	.0	0.	0.	0.	0.	0.	.00
D415F3.007	.0	.0	.0	.0	.00	50.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.00
D415F3.006	.2	.0	.0	.0	.00	50.0	33.0	11.0	.4	0.	0.	0.	0.	0.	.15
D415F3.005	.6	.0	6.7	.0	.00	50.0	25.0	11.0	1.6	0.	0.	207.	0.	0.	.54
D415F3.004	.6	.0	8.3	.0	.04	50.0	.0	11.0	1.5	0.	0.	256.	0.	0.	3.05

FALCON 4: LSR = 150, GAS = FREON 12

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415F4.009	.0	.0	.0	.0	.00	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.22
D415F4.008	.1	.0	.0	.0	.00	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.39
D415F4.007	.0	.0	.0	.0	.00	50.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.23
D415F4.006	.1	.0	.0	.0	.00	50.0	33.0	11.0	.4	0.	0.	0.	0.	0.	.12
D415F4.005	.5	.0	6.7	.0	.01	50.0	25.0	11.0	1.3	0.	0.	206.	0.	0.	.67
D415F4.004	.9	.0	10.9	.0	.04	50.0	.0	11.0	2.4	0.	0.	338.	0.	0.	3.14
D415F5.009	.0	.0	.0	.0	.00	50.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.00
D415F5.008	.0	.0	.0	.0	.00	50.0	66.0	11.0	.1	0.	0.	0.	0.	0.	.01
D415F5.007	.0	.0	.0	.0	.00	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.00
D415F5.006	.1	.0	.0	.0	.00	50.0	33.0	11.0	.3	0.	0.	0.	0.	0.	.17
D415F5.005	.6	.0	7.6	.0	.01	50.0	25.0	11.0	1.5	0.	0.	235.	0.	0.	.62
D415F5.004	1.2	10.7	10.7	10.7	.04	50.0	.0	11.0	3.3	0.	0.	332.	0.	0.	3.47
D415G1.009	.0	.0	.0	.0	.00	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.10
D415G1.008	.0	.0	.0	.0	.00	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.09
D415G1.007	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.11
D415G1.006	.5	.0	11.9	.0	.00	50.0	33.0	17.0	1.4	0.	0.	367.	0.	0.	.19
D415G1.005	.7	.0	10.0	.0	.00	50.0	25.0	17.0	1.8	0.	0.	310.	0.	0.	.24
D415G1.004	.8	.0	10.5	.0	.02	50.0	.0	17.0	2.2	0.	0.	326.	0.	0.	1.88
D415G2.009	.0	.0	.0	.0	.00	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.00
D415G2.008	.0	.0	.0	.0	-.01	50.0	66.0	17.0	.0	0.	0.	0.	0.	0.	.08
D415G2.007	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.14
D415G2.006	.2	.0	.0	.0	.00	50.0	33.0	17.0	.5	0.	0.	0.	0.	0.	.17
D415G2.005	.8	.0	11.2	.0	.00	50.0	25.0	17.0	2.0	0.	0.	346.	0.	0.	.24
D415G2.004	1.2	10.8	11.0	11.0	.03	50.0	.0	17.0	3.1	0.	0.	341.	0.	0.	2.89
D415G3.009	.0	.0	.0	.0	.00	50.0	75.0	17.0	.0	0.	0.	0.	0.	0.	.07
D415G3.008	.0	.0	.0	.0	.00	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.32
D415G3.007	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.04
D415G3.006	.2	.0	.0	.0	.00	50.0	33.0	17.0	.5	0.	0.	0.	0.	0.	.17
D415G3.005	.5	.0	8.8	.0	.00	50.0	25.0	17.0	1.3	0.	0.	273.	0.	0.	.22
D415G3.004	.9	.0	2.0	.0	.03	50.0	.0	17.0	2.5	0.	0.	63.	0.	0.	2.85
D415G4.009	.0	.0	.0	.0	.00	50.0	75.0	17.0	.0	0.	0.	0.	0.	0.	.01
D415G4.008	.0	.0	.0	.0	-.01	50.0	66.0	17.0	.1	0.	0.	0.	0.	0.	.05
D415G4.007	.0	.0	.0	.0	-.01	50.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.06
D415G4.006	.6	.0	7.1	.0	.00	50.0	33.0	17.0	1.5	0.	0.	218.	0.	0.	.06
D415G4.005	.9	.0	7.1	.0	.00	50.0	25.0	17.0	2.5	0.	0.	221.	0.	0.	.37
D415G4.004	.9	.0	5.4	.0	.03	50.0	.0	17.0	2.3	0.	0.	166.	0.	0.	2.73
D415G5.009	.0	.0	.0	.0	.00	50.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.02
D415G5.008	.0	.0	.0	.0	.00	50.0	66.0	17.0	.0	0.	0.	0.	0.	0.	.00
D415G5.007	.0	.0	.0	.0	.00	50.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.02
D415G5.006	.3	.0	15.7	.0	.00	50.0	33.0	17.0	.7	0.	0.	486.	0.	0.	.16
D415G5.005	.6	.0	9.8	.0	.01	50.0	25.0	17.0	1.6	0.	0.	304.	0.	0.	.67
D415G5.004	.9	.0	10.2	.0	.03	50.0	.0	17.0	2.5	0.	0.	315.	0.	0.	2.53

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415H1.009	1.0	.0	10.9	.0	.08	50.0	.0	1.0	2.6	0.	0.	337.	0.	0.	6.25
D415H1.008	.9	.0	8.8	.0	.08	50.0	-25.0	1.0	2.3	0.	0.	274.	0.	0.	6.28
D415H1.007	.8	.0	7.5	.0	.06	50.0	-33.0	1.0	2.2	0.	0.	232.	0.	0.	4.81
D415H1.006	.8	.0	10.1	.0	.04	50.0	-50.0	1.0	2.2	0.	0.	314.	0.	0.	3.47
D415H1.005	.4	.0	7.5	.0	.02	50.0	-66.0	1.0	1.2	0.	0.	233.	0.	0.	1.29
D415H1.004	.3	.0	7.1	.0	.00	50.0	-75.0	1.0	.7	0.	0.	220.	0.	0.	.32
D415H2.009	1.0	.0	8.6	.0	.08	50.0	.0	1.0	2.6	0.	0.	267.	0.	0.	6.30
D415H2.008	1.1	9.2	9.2	9.2	.08	50.0	-25.0	1.0	3.0	0.	0.	284.	0.	0.	6.55
D415H2.007	.9	.0	9.9	.0	.06	50.0	-33.0	1.0	2.4	0.	0.	307.	0.	0.	5.21
D415H2.006	.9	.0	9.9	.0	.03	50.0	-50.0	1.0	2.3	0.	0.	307.	0.	0.	3.01
D415H2.005	.7	.0	7.7	.0	.02	50.0	-66.0	1.0	1.8	0.	0.	240.	0.	0.	2.04
D415H2.004	.5	.0	7.8	.0	.01	50.0	-75.0	1.0	1.4	0.	0.	241.	0.	0.	1.21
D415H3.009	1.0	10.3	10.3	10.3	.08	50.0	.0	1.0	2.7	0.	0.	318.	0.	0.	6.77
D415H3.008	1.1	9.2	9.2	9.2	.09	50.0	-25.0	1.0	3.0	0.	0.	284.	0.	0.	7.37
D415H3.007	.9	.0	9.0	.0	.07	50.0	-33.0	1.0	2.3	0.	0.	280.	0.	0.	5.66
D415H3.006	.9	.0	9.1	.0	.04	50.0	-50.0	1.0	2.4	0.	0.	282.	0.	0.	3.25
D415H3.005	.7	.0	9.2	.0	.02	50.0	-66.0	1.0	2.0	0.	0.	283.	0.	0.	1.55
D415H3.004	.4	.0	9.3	.0	.00	50.0	-75.0	1.0	1.2	0.	0.	287.	0.	0.	.55
D415H4.009	1.0	.0	7.9	.0	.08	50.0	.0	1.0	2.5	0.	0.	245.	0.	0.	6.97
D415H4.008	1.2	7.6	9.1	9.3	.09	50.0	-25.0	1.0	3.2	0.	0.	282.	0.	0.	7.56
D415H4.007	.9	.0	9.4	.0	.07	50.0	-33.0	1.0	2.4	0.	0.	292.	0.	0.	6.04
D415H4.006	.8	.0	7.5	.0	.04	50.0	-50.0	1.0	2.1	0.	0.	231.	0.	0.	3.57
D415H4.005	.6	.0	9.8	.0	.03	50.0	-66.0	1.0	1.7	0.	0.	305.	0.	0.	2.20
D415H4.004	.4	.0	9.8	.0	.01	50.0	-75.0	1.0	1.1	0.	0.	305.	0.	0.	.81
D415H5.009	.9	.0	8.4	.0	.09	50.0	.0	1.0	2.5	0.	0.	260.	0.	0.	7.13
D415H5.008	.9	.0	9.2	.0	.08	50.0	-25.0	1.0	2.5	0.	0.	283.	0.	0.	6.98
D415H5.007	.8	.0	9.1	.0	.07	50.0	-33.0	1.0	2.1	0.	0.	282.	0.	0.	5.93
D415H5.006	.8	.0	11.3	.0	.04	50.0	-50.0	1.0	2.0	0.	0.	349.	0.	0.	3.63
D415H5.005	.6	.0	10.3	.0	.02	50.0	-66.0	1.0	1.6	0.	0.	319.	0.	0.	1.63
D415H5.004	.4	.0	10.7	.0	.01	50.0	-75.0	1.0	1.0	0.	0.	331.	0.	0.	.68
D415I1.009	1.0	11.0	11.0	11.0	.07	50.0	.0	5.0	2.7	0.	0.	340.	0.	0.	5.76
D415I1.008	1.0	11.1	11.1	11.1	.08	50.0	-25.0	5.0	2.7	0.	0.	343.	0.	0.	6.43
D415I1.007	.9	.0	8.3	.0	.06	50.0	-33.0	5.0	2.3	0.	0.	257.	0.	0.	5.21
D415I1.006	.8	.0	8.3	.0	.03	50.0	-50.0	5.0	2.1	0.	0.	257.	0.	0.	2.66
D415I1.005	.5	.0	9.7	.0	.02	50.0	-66.0	5.0	1.4	0.	0.	302.	0.	0.	1.35
D415I1.004	.5	.0	9.9	.0	.01	50.0	-75.0	5.0	1.3	0.	0.	307.	0.	0.	.67
D415I2.009	.9	.0	10.7	.0	.08	50.0	.0	5.0	2.4	0.	0.	333.	0.	0.	6.26
D415I2.008	1.1	9.1	9.1	10.6	.08	50.0	-25.0	5.0	2.8	0.	0.	282.	0.	0.	7.04
D415I2.007	1.0	.0	9.7	.0	.06	50.0	-33.0	5.0	2.6	0.	0.	302.	0.	0.	5.19
D415I2.006	.8	.0	9.0	.0	.02	50.0	-50.0	5.0	2.2	0.	0.	277.	0.	0.	2.18
D415I2.005	.5	.0	12.3	.0	.01	50.0	-66.0	5.0	1.4	0.	0.	380.	0.	0.	.86
D415I2.004	.4	.0	7.0	.0	.00	50.0	-75.0	5.0	1.1	0.	0.	216.	0.	0.	.31

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415I3.009	1.0	.0	9.2	.0	.08	50.0	.0	5.0	2.6	0.	0.	283.	0.	0.	6.76
D415I3.008	1.0	.0	8.2	.0	.09	50.0	-25.0	5.0	2.6	0.	0.	254.	0.	0.	7.23
D415I3.007	.9	.0	6.9	.0	.07	50.0	-33.0	5.0	2.5	0.	0.	215.	0.	0.	6.11
D415I3.006	.8	.0	11.7	.0	.03	50.0	-50.0	5.0	2.2	0.	0.	361.	0.	0.	2.94
D415I3.005	.6	.0	12.0	.0	.02	50.0	-66.0	5.0	1.6	0.	0.	371.	0.	0.	1.62
D415I3.004	.3	.0	6.1	.0	.01	50.0	-75.0	5.0	.9	0.	0.	189.	0.	0.	.65
D415I4.009	.9	.0	8.5	.0	.07	50.0	.0	5.0	2.3	0.	0.	263.	0.	0.	6.11
D415I4.008	1.0	.0	12.3	.0	.08	50.0	-25.0	5.0	2.6	0.	0.	380.	0.	0.	6.30
D415I4.007	.8	.0	12.1	.0	.06	50.0	-33.0	5.0	2.2	0.	0.	375.	0.	0.	5.11
D415I4.006	.8	.0	9.4	.0	.03	50.0	-50.0	5.0	2.0	0.	0.	290.	0.	0.	2.79
D415I4.005	.7	.0	12.2	.0	.02	50.0	-66.0	5.0	2.0	0.	0.	377.	0.	0.	1.43
D415I4.004	.5	.0	11.2	.0	.00	50.0	-75.0	5.0	1.3	0.	0.	346.	0.	0.	.30
D415I5.009	.9	.0	11.7	.0	.08	50.0	.0	5.0	2.5	0.	0.	362.	0.	0.	6.91
D415I5.008	1.5	10.9	11.7	11.7	.09	50.0	-25.0	5.0	4.0	0.	0.	362.	0.	0.	7.26
D415I5.007	1.0	.0	11.7	.0	.07	50.0	-33.0	5.0	2.6	0.	0.	361.	0.	0.	5.61
D415I5.006	.7	.0	6.8	.0	.03	50.0	-50.0	5.0	1.9	0.	0.	210.	0.	0.	2.80
D415I5.005	.5	.0	6.9	.0	.02	50.0	-66.0	5.0	1.4	0.	0.	213.	0.	0.	1.45
D415I5.004	.4	.0	5.2	.0	.01	50.0	-75.0	5.0	1.2	0.	0.	162.	0.	0.	.63
D415J1.009	1.2	5.9	6.0	6.0	.05	50.0	.0	11.0	3.1	0.	0.	184.	0.	0.	4.59
D415J1.008	.9	.0	11.2	.0	.06	50.0	-25.0	11.0	2.4	0.	0.	347.	0.	0.	5.36
D415J1.007	.8	.0	6.5	.0	.04	50.0	-33.0	11.0	2.2	0.	0.	200.	0.	0.	3.80
D415J1.006	.6	.0	6.8	.0	.01	50.0	-50.0	11.0	1.7	0.	0.	211.	0.	0.	1.16
D415J1.005	.4	.0	9.9	.0	.00	50.0	-66.0	11.0	1.0	0.	0.	307.	0.	0.	.32
D415J1.004	.2	.0	9.7	.0	.00	50.0	-75.0	11.0	.6	0.	0.	299.	0.	0.	.23
D415J2.009	1.0	10.8	10.8	10.8	.06	50.0	.0	11.0	2.7	0.	0.	333.	0.	0.	4.83
D415J2.008	1.1	10.3	10.4	10.4	.06	50.0	-25.0	11.0	2.9	0.	0.	321.	0.	0.	5.42
D415J2.007	.9	.0	7.2	.0	.05	50.0	-33.0	11.0	2.3	0.	0.	224.	0.	0.	4.36
D415J2.006	.6	.0	8.6	.0	.01	50.0	-50.0	11.0	1.6	0.	0.	265.	0.	0.	1.21
D415J2.005	.4	.0	12.0	.0	.00	50.0	-66.0	11.0	1.0	0.	0.	373.	0.	0.	.36
D415J2.004	.1	.0	.0	.0	.00	50.0	-75.0	11.0	.4	0.	0.	0.	0.	0.	.48
D415J3.009	1.1	9.8	9.8	9.8	.06	50.0	.0	11.0	3.0	0.	0.	303.	0.	0.	5.04
D415J3.008	1.0	9.4	9.4	9.4	.07	50.0	-25.0	11.0	2.8	0.	0.	290.	0.	0.	5.64
D415J3.007	.9	.0	9.5	.0	.05	50.0	-33.0	11.0	2.3	0.	0.	294.	0.	0.	4.36
D415J3.006	.7	.0	7.6	.0	.02	50.0	-50.0	11.0	1.9	0.	0.	236.	0.	0.	1.68
D415J3.005	.4	.0	9.3	.0	.01	50.0	-66.0	11.0	1.1	0.	0.	288.	0.	0.	.45
D415J3.004	.3	.0	9.3	.0	.00	50.0	-75.0	11.0	.7	0.	0.	288.	0.	0.	.11
D415J4.009	1.0	11.6	11.6	11.6	.06	50.0	.0	11.0	2.7	0.	0.	359.	0.	0.	4.91
D415J4.008	1.6	7.8	11.5	11.5	.07	50.0	-25.0	11.0	4.3	0.	0.	355.	0.	0.	6.03
D415J4.007	.9	.0	11.9	.0	.06	50.0	-33.0	11.0	2.3	0.	0.	367.	0.	0.	4.80
D415J4.006	.9	.0	8.4	.0	.02	50.0	-50.0	11.0	2.3	0.	0.	260.	0.	0.	1.99
D415J4.005	.5	.0	8.8	.0	.01	50.0	-66.0	11.0	1.3	0.	0.	271.	0.	0.	.70
D415J4.004	.2	.0	6.8	.0	.01	50.0	-75.0	11.0	.7	0.	0.	211.	0.	0.	.61

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415J5.009	.9	.0	9.9	.0	.06	50.0	.0	11.0	2.4	0.	0.	306.	0.	0.	4.81
D415J5.008	1.2	7.5	8.7	8.7	.07	50.0	-25.0	11.0	3.2	0.	0.	269.	0.	0.	5.84
D415J5.007	.9	.0	8.7	.0	.06	50.0	-33.0	11.0	2.4	0.	0.	268.	0.	0.	4.82
D415J5.006	.7	.0	9.8	.0	.01	50.0	-50.0	11.0	1.9	0.	0.	305.	0.	0.	1.46
D415J5.005	.3	.0	11.7	.0	.00	50.0	-66.0	11.0	.9	0.	0.	362.	0.	0.	.36
D415J5.004	.2	.0	.0	.0	.00	50.0	-75.0	11.0	.5	0.	0.	0.	0.	0.	.41
D415K1.009	.8	.0	10.9	.0	.03	50.0	.0	17.0	2.1	0.	0.	339.	0.	0.	2.29
D415K1.008	1.1	6.1	10.5	10.5	.05	50.0	-25.0	17.0	3.0	0.	0.	325.	0.	0.	3.98
D415K1.007	.9	.0	10.5	.0	.04	50.0	-33.0	17.0	2.4	0.	0.	326.	0.	0.	3.25
D415K1.006	.6	.0	7.7	.0	.01	50.0	-50.0	17.0	1.6	0.	0.	240.	0.	0.	.80
D415K1.005	.2	.0	.0	.0	.00	50.0	-66.0	17.0	.4	0.	0.	0.	0.	0.	.20
D415K1.004	.3	.0	7.9	.0	.00	50.0	-75.0	17.0	.7	0.	0.	244.	0.	0.	.22
D415K2.009	.9	.0	8.8	.0	.03	50.0	.0	17.0	2.4	0.	0.	272.	0.	0.	2.46
D415K2.008	1.1	8.0	8.5	10.8	.04	50.0	-25.0	17.0	2.9	0.	0.	264.	0.	0.	3.42
D415K2.007	.9	.0	11.4	.0	.03	50.0	-33.0	17.0	2.4	0.	0.	352.	0.	0.	2.99
D415K2.006	.7	.0	8.7	.0	.01	50.0	-50.0	17.0	1.7	0.	0.	271.	0.	0.	.83
D415K2.005	.2	.0	.0	.0	.00	50.0	-66.0	17.0	.5	0.	0.	0.	0.	0.	.04
D415K2.004	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.3	0.	0.	0.	0.	0.	.01
D415K3.009	1.0	9.4	9.4	9.5	.03	50.0	.0	17.0	2.8	0.	0.	292.	0.	0.	2.82
D415K3.008	.9	.0	9.2	.0	.04	50.0	-25.0	17.0	2.3	0.	0.	284.	0.	0.	3.76
D415K3.007	.8	.0	10.4	.0	.04	50.0	-33.0	17.0	2.1	0.	0.	323.	0.	0.	3.30
D415K3.006	.8	.0	8.9	.0	.01	50.0	-50.0	17.0	2.0	0.	0.	276.	0.	0.	1.03
D415K3.005	.2	.0	9.9	.0	.00	50.0	-66.0	17.0	.6	0.	0.	308.	0.	0.	.27
D415K3.004	.2	.0	.0	.0	.00	50.0	-75.0	17.0	.4	0.	0.	0.	0.	0.	.25
D415K4.009	.9	.0	8.8	.0	.03	50.0	.0	17.0	2.3	0.	0.	273.	0.	0.	2.88
D415K4.008	1.1	7.4	7.5	11.5	.06	50.0	-25.0	17.0	2.9	0.	0.	233.	0.	0.	4.89
D415K4.007	.9	.0	8.9	.0	.05	50.0	-33.0	17.0	2.3	0.	0.	276.	0.	0.	3.95
D415K4.006	.7	.0	12.0	.0	.01	50.0	-50.0	17.0	2.0	0.	0.	370.	0.	0.	.92
D415K4.005	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.4	0.	0.	0.	0.	0.	.39
D415K4.004	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.3	0.	0.	0.	0.	0.	.25
D415K5.009	.8	.0	9.1	.0	.03	50.0	.0	17.0	2.0	0.	0.	282.	0.	0.	2.38
D415K5.008	1.2	7.6	7.6	10.4	.05	50.0	-25.0	17.0	3.2	0.	0.	234.	0.	0.	4.41
D415K5.007	.9	.0	10.2	.0	.04	50.0	-33.0	17.0	2.3	0.	0.	315.	0.	0.	3.17
D415K5.006	.7	.0	12.0	.0	.00	50.0	-50.0	17.0	1.8	0.	0.	371.	0.	0.	.55
D415K5.005	.1	.0	.0	.0	.00	50.0	-66.0	17.0	.2	0.	0.	0.	0.	0.	.02
D415K5.004	.0	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.13
D415L1.009	.0	.0	.0	.0	.00	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.35
D415L1.008	.0	.0	.0	.0	.00	150.0	56.0	1.0	.0	0.	0.	0.	0.	0.	.06
D415L1.007	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.03
D415L1.006	.3	.0	12.2	.0	.00	150.0	28.0	1.0	.9	0.	0.	377.	0.	0.	.43
D415L1.005	.3	.0	11.8	.0	.01	150.0	25.0	1.0	.9	0.	0.	365.	0.	0.	.56
D415L1.004	.6	.0	13.3	.0	.04	150.0	.0	1.0	1.5	0.	0.	411.	0.	0.	3.35

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415L2.009	.0	.0	.0	.0	.00	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.06
D415L2.008	.0	.0	.0	.0	.00	150.0	56.0	1.0	.0	0.	0.	0.	0.	0.	.24
D415L2.007	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.31
D415L2.006	.4	.0	11.9	.0	.01	150.0	28.0	1.0	.9	0.	0.	368.	0.	0.	.59
D415L2.005	.3	.0	11.8	.0	.00	150.0	25.0	1.0	.9	0.	0.	366.	0.	0.	.38
D415L2.004	.6	.0	8.0	.0	.05	150.0	.0	1.0	1.5	0.	0.	248.	0.	0.	3.90
D415L3.009	.0	.0	.0	.0	.00	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.01
D415L3.008	.1	.0	.0	.0	.00	150.0	56.0	1.0	.1	0.	0.	0.	0.	0.	.18
D415L3.007	.1	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.28
D415L3.006	.2	.0	7.5	.0	.01	150.0	28.0	1.0	.6	0.	0.	231.	0.	0.	.73
D415L3.005	.3	.0	7.5	.0	.00	150.0	25.0	1.0	.8	0.	0.	233.	0.	0.	.47
D415L3.004	.6	.0	8.0	.0	.04	150.0	.0	1.0	1.5	0.	0.	248.	0.	0.	3.67
D415L4.009	.0	.0	.0	.0	.00	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.17
D415L4.008	.1	.0	.0	.0	.00	150.0	56.0	1.0	.1	0.	0.	0.	0.	0.	.20
D415L4.007	.0	.0	.0	.0	.00	150.0	50.0	1.0	.0	0.	0.	0.	0.	0.	.00
D415L4.006	.4	.0	12.0	.0	.01	150.0	28.0	1.0	1.1	0.	0.	370.	0.	0.	.69
D415L4.005	.3	.0	13.7	.0	.01	150.0	25.0	1.0	.9	0.	0.	425.	0.	0.	.77
D415L4.004	.6	.0	10.5	.0	.04	150.0	.0	1.0	1.5	0.	0.	325.	0.	0.	3.52
D415L5.009	.0	.0	.0	.0	.00	150.0	75.0	1.0	.1	0.	0.	0.	0.	0.	.29
D415L5.008	.0	.0	.0	.0	.00	150.0	56.0	1.0	.0	0.	0.	0.	0.	0.	.01
D415L5.007	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.29
D415L5.006	.4	.0	8.8	.0	.01	150.0	28.0	1.0	1.1	0.	0.	274.	0.	0.	.57
D415L5.005	.4	.0	10.6	.0	.01	150.0	25.0	1.0	1.0	0.	0.	329.	0.	0.	.45
D415L5.004	.6	.0	10.7	.0	.04	150.0	.0	1.0	1.5	0.	0.	330.	0.	0.	3.71
D415M1.009	.0	.0	.0	.0	.00	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.06
D415M1.008	.0	.0	.0	.0	.00	150.0	56.0	5.0	.0	0.	0.	0.	0.	0.	.00
D415M1.007	.0	.0	.0	.0	.00	150.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.03
D415M1.006	.3	.0	12.9	.0	.00	150.0	28.0	5.0	.7	0.	0.	400.	0.	0.	.34
D415M1.005	.4	.0	7.5	.0	.01	150.0	25.0	5.0	1.0	0.	0.	231.	0.	0.	.57
D415M1.004	.5	.0	12.3	.0	.03	150.0	.0	5.0	1.5	0.	0.	381.	0.	0.	2.79
D415M2.009	.0	.0	.0	.0	.00	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.04
D415M2.008	.0	.0	.0	.0	.00	150.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.08
D415M2.007	.0	.0	.0	.0	.00	150.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.00
D415M2.006	.3	.0	9.2	.0	.00	150.0	28.0	5.0	.9	0.	0.	286.	0.	0.	.35
D415M2.005	.4	.0	9.2	.0	.00	150.0	25.0	5.0	1.0	0.	0.	285.	0.	0.	.39
D415M2.004	.6	.0	10.1	.0	.04	150.0	.0	5.0	1.7	0.	0.	312.	0.	0.	3.23
D415M3.009	.0	.0	.0	.0	.00	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.21
D415M3.008	.1	.0	.0	.0	.00	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.49
D415M3.007	.0	.0	.0	.0	.00	150.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.03
D415M3.006	.4	.0	10.8	.0	.01	150.0	28.0	5.0	1.1	0.	0.	333.	0.	0.	.62
D415M3.005	.5	.0	10.7	.0	.01	150.0	25.0	5.0	1.4	0.	0.	333.	0.	0.	.44
D415M3.004	.7	.0	11.7	.0	.04	150.0	.0	5.0	1.8	0.	0.	362.	0.	0.	3.15

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS: PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	POSITION Y (M)	POSITION Z (M)	PROTOTYPE CONDITIONS: PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415M4.009	.0	.0	.0	.0	.00	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.10
D415M4.008	.1	.0	.0	.0	.00	150.0	56.0	5.0	.2	0.	0.	0.	0.	0.	.00
D415M4.007	.1	.0	.0	.0	.00	150.0	50.0	5.0	.2	0.	0.	0.	0.	0.	.03
D415M4.006	.4	.0	12.9	.0	.00	150.0	28.0	5.0	1.1	0.	0.	401.	0.	0.	.55
D415M4.005	.3	.0	12.9	.0	.01	150.0	25.0	5.0	.9	0.	0.	399.	0.	0.	.67
D415M4.004	.7	.0	11.5	.0	.03	150.0	.0	5.0	1.8	0.	0.	355.	0.	0.	3.01
D415M5.009	.0	.0	.0	.0	.00	150.0	75.0	5.0	.1	0.	0.	0.	0.	0.	.20
D415M5.008	.0	.0	.0	.0	.00	150.0	56.0	5.0	.1	0.	0.	0.	0.	0.	.48
D415M5.007	.0	.0	.0	.0	.00	150.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.24
D415M5.006	.4	.0	12.6	.0	.00	150.0	28.0	5.0	1.2	0.	0.	389.	0.	0.	.29
D415M5.005	.4	.0	9.5	.0	.01	150.0	25.0	5.0	1.0	0.	0.	294.	0.	0.	.59
D415M5.004	.7	.0	12.1	.0	.04	150.0	.0	5.0	1.8	0.	0.	375.	0.	0.	3.16
D415N1.009	.0	.0	.0	.0	.00	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.07
D415N1.008	.1	.0	.0	.0	.01	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.57
D415N1.007	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.28
D415N1.006	.4	.0	10.7	.0	.00	150.0	28.0	11.0	1.0	0.	0.	332.	0.	0.	.34
D415N1.005	.4	.0	10.7	.0	.01	150.0	25.0	11.0	1.1	0.	0.	331.	0.	0.	.52
D415N1.004	.5	.0	9.3	.0	.03	150.0	.0	11.0	1.4	0.	0.	289.	0.	0.	2.47
D415N2.009	.0	.0	.0	.0	.00	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.18
D415N2.008	.0	.0	.0	.0	.00	150.0	56.0	11.0	.0	0.	0.	0.	0.	0.	.02
D415N2.007	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.00
D415N2.006	.2	.0	.0	.0	.00	150.0	28.0	11.0	.5	0.	0.	0.	0.	0.	.22
D415N2.005	.1	.0	.0	.0	.00	150.0	25.0	11.0	.3	0.	0.	0.	0.	0.	.14
D415N2.004	.5	.0	12.5	.0	.03	150.0	.0	11.0	1.3	0.	0.	388.	0.	0.	2.27
D415N3.009	.0	.0	.0	.0	.00	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.02
D415N3.008	.1	.0	.0	.0	.00	150.0	56.0	11.0	.1	0.	0.	0.	0.	0.	.03
D415N3.007	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.05
D415N3.006	.3	.0	10.1	.0	.00	150.0	28.0	11.0	.8	0.	0.	313.	0.	0.	.29
D415N3.005	.3	.0	12.1	.0	.00	150.0	25.0	11.0	.9	0.	0.	374.	0.	0.	.31
D415N3.004	.6	.0	12.5	.0	.03	150.0	.0	11.0	1.7	0.	0.	387.	0.	0.	2.76
D415N4.009	.0	.0	.0	.0	.00	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.10
D415N4.008	.1	.0	.0	.0	.00	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.08
D415N4.007	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.09
D415N4.006	.3	.0	12.9	.0	.00	150.0	28.0	11.0	.8	0.	0.	401.	0.	0.	.38
D415N4.005	.3	.0	12.8	.0	.00	150.0	25.0	11.0	.8	0.	0.	397.	0.	0.	.24
D415N4.004	.5	.0	11.1	.0	.03	150.0	.0	11.0	1.4	0.	0.	343.	0.	0.	2.58
D415N5.009	.0	.0	.0	.0	.00	150.0	75.0	11.0	.1	0.	0.	0.	0.	0.	.00
D415N5.008	.1	.0	.0	.0	.00	150.0	56.0	11.0	.2	0.	0.	0.	0.	0.	.00
D415N5.007	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.46
D415N5.006	.2	.0	.0	.0	.00	150.0	28.0	11.0	.5	0.	0.	0.	0.	0.	.36
D415N5.005	.2	.0	.0	.0	.00	150.0	25.0	11.0	.4	0.	0.	0.	0.	0.	.28
D415N5.004	.6	.0	11.6	.0	.03	150.0	.0	11.0	1.7	0.	0.	359.	0.	0.	2.40

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D41501.009	.0	.0	.0	.0	.00	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.08
D41501.008	.0	.0	.0	.0	.00	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.07
D41501.007	.0	.0	.0	.0	.00	150.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.28
D41501.006	.2	.0	.0	.0	.00	150.0	28.0	17.0	.5	0.	0.	0.	0.	0.	.14
D41501.005	.2	.0	.0	.0	.00	150.0	25.0	17.0	.5	0.	0.	0.	0.	0.	.20
D41501.004	.5	.0	11.3	.0	.02	150.0	.0	17.0	1.3	0.	0.	350.	0.	0.	1.46
D41502.009	.0	.0	.0	.0	.00	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.08
D41502.008	.1	.0	.0	.0	.01	150.0	56.0	17.0	.1	0.	0.	0.	0.	0.	.61
D41502.007	.0	.0	.0	.0	.00	150.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.34
D41502.006	.1	.0	.0	.0	-.01	150.0	28.0	17.0	.3	0.	0.	0.	0.	0.	.04
D41502.005	.1	.0	.0	.0	.00	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.04
D41502.004	.5	.0	10.7	.0	.02	150.0	.0	17.0	1.3	0.	0.	332.	0.	0.	1.86
D41503.009	.0	.0	.0	.0	.01	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.54
D41503.008	.1	.0	.0	.0	.00	150.0	56.0	17.0	.2	0.	0.	0.	0.	0.	.08
D41503.007	.0	.0	.0	.0	.00	150.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.10
D41503.006	.1	.0	.0	.0	.00	150.0	28.0	17.0	.4	0.	0.	0.	0.	0.	.32
D41503.005	.1	.0	.0	.0	.00	150.0	25.0	17.0	.4	0.	0.	0.	0.	0.	.26
D41503.004	.6	.0	10.3	.0	.03	150.0	.0	17.0	1.6	0.	0.	319.	0.	0.	2.32
D41504.009	.0	.0	.0	.0	.00	150.0	75.0	17.0	.1	0.	0.	0.	0.	0.	.10
D41504.008	.0	.0	.0	.0	.00	150.0	56.0	17.0	.0	0.	0.	0.	0.	0.	.17
D41504.007	.0	.0	.0	.0	.00	150.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.03
D41504.006	.1	.0	.0	.0	.00	150.0	28.0	17.0	.2	0.	0.	0.	0.	0.	.27
D41504.005	.1	.0	.0	.0	.00	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.21
D41504.004	.6	.0	12.4	.0	.02	150.0	.0	17.0	1.5	0.	0.	384.	0.	0.	1.83
D41505.009	.0	.0	.0	.0	.00	150.0	75.0	17.0	.0	0.	0.	0.	0.	0.	.10
D41505.008	.0	.0	.0	.0	.00	150.0	56.0	17.0	.0	0.	0.	0.	0.	0.	.00
D41505.007	.0	.0	.0	.0	.00	150.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.12
D41505.006	.2	.0	.0	.0	.00	150.0	28.0	17.0	.5	0.	0.	0.	0.	0.	.11
D41505.005	.2	.0	10.9	.0	.00	150.0	25.0	17.0	.6	0.	0.	339.	0.	0.	.09
D41505.004	.4	.0	8.8	.0	.02	150.0	.0	17.0	1.1	0.	0.	272.	0.	0.	1.75
D415P1.009	.6	.0	11.1	.0	.04	150.0	.0	1.0	1.7	0.	0.	344.	0.	0.	3.48
D415P1.008	.7	.0	10.5	.0	.05	150.0	-25.0	1.0	1.8	0.	0.	324.	0.	0.	4.25
D415P1.007	.6	.0	12.2	.0	.05	150.0	-28.0	1.0	1.7	0.	0.	377.	0.	0.	3.81
D415P1.006	.6	.0	10.8	.0	.04	150.0	-50.0	1.0	1.6	0.	0.	335.	0.	0.	3.53
D415P1.005	.6	.0	10.8	.0	.04	150.0	-56.0	1.0	1.6	0.	0.	334.	0.	0.	3.25
D415P1.004	.5	.0	13.1	.0	.03	150.0	-75.0	1.0	1.5	0.	0.	404.	0.	0.	2.57
D415P2.009	.5	.0	10.5	.0	.04	150.0	.0	1.0	1.4	0.	0.	325.	0.	0.	3.60
D415P2.008	.6	.0	9.0	.0	.04	150.0	-25.0	1.0	1.6	0.	0.	278.	0.	0.	3.78
D415P2.007	.6	.0	9.0	.0	.05	150.0	-28.0	1.0	1.6	0.	0.	278.	0.	0.	3.90
D415P2.006	.6	.0	9.1	.0	.04	150.0	-50.0	1.0	1.5	0.	0.	280.	0.	0.	3.71
D415P2.005	.5	.0	9.2	.0	.04	150.0	-56.0	1.0	1.4	0.	0.	284.	0.	0.	3.49
D415P2.004	.5	.0	9.1	.0	.03	150.0	-75.0	1.0	1.5	0.	0.	282.	0.	0.	2.49

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415P3.009	.6	.0	12.0	.0	.05	150.0	.0	1.0	1.6	0.	0.	370.	0.	0.	3.92
D415P3.008	.6	.0	10.8	.0	.05	150.0	-25.0	1.0	1.6	0.	0.	334.	0.	0.	4.38
D415P3.007	.6	.0	8.4	.0	.05	150.0	-28.0	1.0	1.5	0.	0.	261.	0.	0.	4.28
D415P3.006	.6	.0	10.1	.0	.04	150.0	-50.0	1.0	1.6	0.	0.	313.	0.	0.	3.62
D415P3.005	.6	.0	8.8	.0	.05	150.0	-56.0	1.0	1.6	0.	0.	273.	0.	0.	3.77
D415P3.004	.5	.0	11.5	.0	.03	150.0	-75.0	1.0	1.5	0.	0.	356.	0.	0.	2.63
D415P4.009	.7	.0	11.7	.0	.05	150.0	.0	1.0	1.8	0.	0.	363.	0.	0.	3.93
D415P4.008	.6	.0	9.0	.0	.05	150.0	-25.0	1.0	1.7	0.	0.	279.	0.	0.	4.11
D415P4.007	.6	.0	11.2	.0	.05	150.0	-28.0	1.0	1.6	0.	0.	345.	0.	0.	3.99
D415P4.006	.6	.0	8.6	.0	.04	150.0	-50.0	1.0	1.6	0.	0.	267.	0.	0.	3.74
D415P4.005	.6	.0	11.1	.0	.04	150.0	-56.0	1.0	1.5	0.	0.	344.	0.	0.	3.38
D415P4.004	.6	.0	9.9	.0	.03	150.0	-75.0	1.0	1.6	0.	0.	307.	0.	0.	2.41
D415P5.009	.5	.0	9.4	.0	.05	150.0	.0	1.0	1.4	0.	0.	291.	0.	0.	3.89
D415P5.008	.6	.0	8.0	.0	.05	150.0	-25.0	1.0	1.7	0.	0.	247.	0.	0.	4.42
D415P5.007	.6	.0	8.2	.0	.05	150.0	-28.0	1.0	1.5	0.	0.	253.	0.	0.	4.05
D415P5.006	.6	.0	11.2	.0	.04	150.0	-50.0	1.0	1.7	0.	0.	348.	0.	0.	3.70
D415P5.005	.5	.0	11.2	.0	.04	150.0	-56.0	1.0	1.4	0.	0.	348.	0.	0.	3.47
D415P5.004	.6	.0	11.4	.0	.03	150.0	-75.0	1.0	1.6	0.	0.	352.	0.	0.	2.29
D415Q1.009	.6	.0	10.8	.0	.04	150.0	.0	5.0	1.5	0.	0.	335.	0.	0.	3.25
D415Q1.008	.6	.0	9.2	.0	.05	150.0	-25.0	5.0	1.6	0.	0.	284.	0.	0.	3.96
D415Q1.007	.6	.0	8.9	.0	.04	150.0	-28.0	5.0	1.5	0.	0.	275.	0.	0.	3.79
D415Q1.006	.6	.0	11.1	.0	.03	150.0	-50.0	5.0	1.6	0.	0.	344.	0.	0.	2.76
D415Q1.005	.5	.0	9.0	.0	.03	150.0	-56.0	5.0	1.4	0.	0.	280.	0.	0.	2.48
D415Q1.004	.6	.0	11.2	.0	.02	150.0	-75.0	5.0	1.6	0.	0.	345.	0.	0.	1.81
D415Q2.009	.6	.0	10.8	.0	.04	150.0	.0	5.0	1.5	0.	0.	335.	0.	0.	3.56
D415Q2.008	.7	.0	12.0	.0	.05	150.0	-25.0	5.0	2.0	0.	0.	370.	0.	0.	3.95
D415Q2.007	.6	.0	11.9	.0	.04	150.0	-28.0	5.0	1.7	0.	0.	370.	0.	0.	3.65
D415Q2.006	.7	.0	10.3	.0	.04	150.0	-50.0	5.0	1.7	0.	0.	318.	0.	0.	3.52
D415Q2.005	.7	.0	10.3	.0	.04	150.0	-56.0	5.0	1.8	0.	0.	320.	0.	0.	3.37
D415Q2.004	.6	.0	11.1	.0	.02	150.0	-75.0	5.0	1.5	0.	0.	344.	0.	0.	2.01
D415Q3.009	.6	.0	11.9	.0	.04	150.0	.0	5.0	1.6	0.	0.	368.	0.	0.	3.50
D415Q3.008	.7	.0	12.3	.0	.05	150.0	-25.0	5.0	2.0	0.	0.	381.	0.	0.	4.58
D415Q3.007	.7	.0	12.3	.0	.05	150.0	-28.0	5.0	1.9	0.	0.	382.	0.	0.	4.19
D415Q3.006	.6	.0	12.4	.0	.05	150.0	-50.0	5.0	1.7	0.	0.	383.	0.	0.	3.90
D415Q3.005	.5	.0	10.3	.0	.04	150.0	-56.0	5.0	1.4	0.	0.	320.	0.	0.	3.24
D415Q3.004	.5	.0	10.6	.0	.03	150.0	-75.0	5.0	1.4	0.	0.	329.	0.	0.	2.17
D415Q4.009	.6	.0	9.8	.0	.04	150.0	.0	5.0	1.5	0.	0.	303.	0.	0.	3.39
D415Q4.008	.5	.0	10.7	.0	.04	150.0	-25.0	5.0	1.5	0.	0.	331.	0.	0.	3.40
D415Q4.007	.6	.0	7.3	.0	.04	150.0	-28.0	5.0	1.5	0.	0.	227.	0.	0.	3.65
D415Q4.006	.6	.0	11.6	.0	.04	150.0	-50.0	5.0	1.5	0.	0.	358.	0.	0.	3.43
D415Q4.005	.6	.0	11.6	.0	.04	150.0	-56.0	5.0	1.6	0.	0.	358.	0.	0.	3.18
D415Q4.004	.4	.0	11.5	.0	.02	150.0	-75.0	5.0	1.1	0.	0.	356.	0.	0.	1.82

FALCON 4: LSR = 150, GAS = FREON 12

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415Q5.009	.6	.0	9.4	.0	.04	150.0	.0	5.0	1.6	0.	0.	292.	0.	0.	3.52
D415Q5.008	.7	.0	9.4	.0	.05	150.0	-25.0	5.0	1.8	0.	0.	291.	0.	0.	4.27
D415Q5.007	.6	.0	9.3	.0	.05	150.0	-28.0	5.0	1.7	0.	0.	289.	0.	0.	3.99
D415Q5.006	.5	.0	8.5	.0	.04	150.0	-50.0	5.0	1.4	0.	0.	262.	0.	0.	3.11
D415Q5.005	.6	.0	8.9	.0	.03	150.0	-56.0	5.0	1.6	0.	0.	276.	0.	0.	2.90
D415Q5.004	.6	.0	8.9	.0	.02	150.0	-75.0	5.0	1.6	0.	0.	277.	0.	0.	1.78
D415R1.009	.5	.0	9.2	.0	.03	150.0	.0	11.0	1.3	0.	0.	284.	0.	0.	2.49
D415R1.008	.6	.0	8.5	.0	.02	150.0	-25.0	11.0	1.5	0.	0.	263.	0.	0.	2.17
D415R1.007	.6	.0	8.6	.0	.03	150.0	-28.0	11.0	1.5	0.	0.	266.	0.	0.	2.27
D415R1.006	.6	.0	10.6	.0	.03	150.0	-50.0	11.0	1.5	0.	0.	329.	0.	0.	2.31
D415R1.005	.5	.0	10.7	.0	.02	150.0	-56.0	11.0	1.3	0.	0.	331.	0.	0.	1.97
D415R1.004	.4	.0	12.6	.0	.01	150.0	-75.0	11.0	1.1	0.	0.	389.	0.	0.	.85
D415R2.009	.6	.0	12.1	.0	.04	150.0	.0	11.0	1.5	0.	0.	375.	0.	0.	3.06
D415R2.008	.6	.0	6.6	.0	.04	150.0	-25.0	11.0	1.7	0.	0.	203.	0.	0.	3.02
D415R2.007	.6	.0	9.3	.0	.03	150.0	-28.0	11.0	1.6	0.	0.	288.	0.	0.	2.87
D415R2.006	.6	.0	8.8	.0	.03	150.0	-50.0	11.0	1.6	0.	0.	272.	0.	0.	2.61
D415R2.005	.6	.0	8.8	.0	.03	150.0	-56.0	11.0	1.6	0.	0.	272.	0.	0.	2.40
D415R2.004	.3	.0	8.1	.0	.01	150.0	-75.0	11.0	.9	0.	0.	250.	0.	0.	.88
D415R3.009	.5	.0	10.8	.0	.03	150.0	.0	11.0	1.3	0.	0.	336.	0.	0.	2.51
D415R3.008	.7	.0	9.1	.0	.03	150.0	-25.0	11.0	2.0	0.	0.	283.	0.	0.	2.83
D415R3.007	.6	.0	9.2	.0	.03	150.0	-28.0	11.0	1.6	0.	0.	283.	0.	0.	2.86
D415R3.006	.6	.0	10.4	.0	.03	150.0	-50.0	11.0	1.6	0.	0.	321.	0.	0.	2.82
D415R3.005	.5	.0	11.2	.0	.02	150.0	-56.0	11.0	1.4	0.	0.	346.	0.	0.	2.13
D415R3.004	.5	.0	8.1	.0	.01	150.0	-75.0	11.0	1.3	0.	0.	251.	0.	0.	1.12
D415R4.009	.5	.0	13.1	.0	.03	150.0	.0	11.0	1.3	0.	0.	404.	0.	0.	2.86
D415R4.008	.7	.0	10.3	.0	.04	150.0	-25.0	11.0	1.9	0.	0.	319.	0.	0.	3.39
D415R4.007	.5	.0	10.3	.0	.03	150.0	-28.0	11.0	1.4	0.	0.	318.	0.	0.	2.90
D415R4.006	.6	.0	11.0	.0	.03	150.0	-50.0	11.0	1.5	0.	0.	342.	0.	0.	2.57
D415R4.005	.5	.0	13.0	.0	.03	150.0	-56.0	11.0	1.5	0.	0.	401.	0.	0.	2.19
D415R4.004	.4	.0	11.7	.0	.01	150.0	-75.0	11.0	1.1	0.	0.	362.	0.	0.	1.08
D415R5.009	.6	.0	11.8	.0	.03	150.0	.0	11.0	1.6	0.	0.	364.	0.	0.	2.88
D415R5.008	.8	.0	10.4	.0	.04	150.0	-25.0	11.0	2.1	0.	0.	321.	0.	0.	3.23
D415R5.007	.6	.0	10.4	.0	.03	150.0	-28.0	11.0	1.7	0.	0.	321.	0.	0.	2.71
D415R5.006	.6	.0	12.2	.0	.03	150.0	-50.0	11.0	1.6	0.	0.	379.	0.	0.	2.73
D415R5.005	.6	.0	10.3	.0	.03	150.0	-56.0	11.0	1.5	0.	0.	318.	0.	0.	2.45
D415R5.004	.5	.0	10.3	.0	.01	150.0	-75.0	11.0	1.3	0.	0.	320.	0.	0.	1.16
D415S1.009	.4	.0	11.5	.0	.02	150.0	.0	17.0	1.1	0.	0.	357.	0.	0.	1.65
D415S1.008	.5	.0	11.1	.0	.01	150.0	-25.0	17.0	1.3	0.	0.	343.	0.	0.	1.29
D415S1.007	.5	.0	11.0	.0	.02	150.0	-28.0	17.0	1.3	0.	0.	342.	0.	0.	1.45
D415S1.006	.5	.0	7.4	.0	.02	150.0	-50.0	17.0	1.3	0.	0.	228.	0.	0.	1.76
D415S1.005	.4	.0	9.6	.0	.02	150.0	-56.0	17.0	1.2	0.	0.	296.	0.	0.	1.46
D415S1.004	.4	.0	8.1	.0	.01	150.0	-75.0	17.0	1.0	0.	0.	249.	0.	0.	.44

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415S2.009	.5	.0	12.0	.0	.02	150.0	.0	17.0	1.2	0.	0.	372.	0.	0.	1.31
D415S2.008	.6	.0	11.4	.0	.02	150.0	-25.0	17.0	1.5	0.	0.	352.	0.	0.	1.54
D415S2.007	.5	.0	7.1	.0	.01	150.0	-28.0	17.0	1.4	0.	0.	220.	0.	0.	1.38
D415S2.006	.5	.0	7.1	.0	.02	150.0	-50.0	17.0	1.4	0.	0.	218.	0.	0.	1.65
D415S2.005	.5	.0	9.3	.0	.02	150.0	-56.0	17.0	1.3	0.	0.	288.	0.	0.	1.40
D415S2.004	.4	.0	5.9	.0	.00	150.0	-75.0	17.0	1.0	0.	0.	183.	0.	0.	.46
D415S3.009	.5	.0	9.8	.0	.02	150.0	.0	17.0	1.3	0.	0.	303.	0.	0.	1.52
D415S3.008	.6	.0	9.4	.0	.01	150.0	-25.0	17.0	1.5	0.	0.	292.	0.	0.	1.47
D415S3.007	.5	.0	11.8	.0	.01	150.0	-28.0	17.0	1.4	0.	0.	367.	0.	0.	1.39
D415S3.006	.5	.0	10.5	.0	.01	150.0	-50.0	17.0	1.4	0.	0.	326.	0.	0.	1.48
D415S3.005	.4	.0	10.4	.0	.01	150.0	-56.0	17.0	1.2	0.	0.	322.	0.	0.	1.22
D415S3.004	.4	.0	7.5	.0	.00	150.0	-75.0	17.0	1.0	0.	0.	233.	0.	0.	.33
D415S4.009	.6	.0	10.0	.0	.02	150.0	.0	17.0	1.6	0.	0.	311.	0.	0.	2.07
D415S4.008	.6	.0	10.6	.0	.02	150.0	-25.0	17.0	1.5	0.	0.	328.	0.	0.	2.03
D415S4.007	.4	.0	9.6	.0	.02	150.0	-28.0	17.0	1.2	0.	0.	297.	0.	0.	1.77
D415S4.006	.5	.0	9.3	.0	.02	150.0	-50.0	17.0	1.3	0.	0.	288.	0.	0.	1.77
D415S4.005	.5	.0	9.6	.0	.02	150.0	-56.0	17.0	1.3	0.	0.	298.	0.	0.	1.59
D415S4.004	.4	.0	10.6	.0	.01	150.0	-75.0	17.0	1.0	0.	0.	327.	0.	0.	.69
D415S5.009	.5	.0	10.5	.0	.03	150.0	.0	17.0	1.3	0.	0.	325.	0.	0.	2.26
D415S5.008	.5	.0	7.0	.0	.03	150.0	-25.0	17.0	1.4	0.	0.	215.	0.	0.	2.23
D415S5.007	.4	.0	10.3	.0	.02	150.0	-28.0	17.0	1.2	0.	0.	319.	0.	0.	1.97
D415S5.006	.6	.0	6.9	.0	.02	150.0	-50.0	17.0	1.5	0.	0.	213.	0.	0.	2.15
D415S5.005	.5	.0	6.7	.0	.02	150.0	-56.0	17.0	1.3	0.	0.	206.	0.	0.	1.50
D415S5.004	.3	.0	10.6	.0	.01	150.0	-75.0	17.0	.8	0.	0.	327.	0.	0.	.62
D415T1.009	.4	.0	12.3	.0	.00	250.0	25.0	1.0	1.0	0.	0.	380.	0.	0.	.41
D415T1.008	.5	.0	11.7	.0	.03	250.0	.0	1.0	1.2	0.	0.	361.	0.	0.	2.73
D415T1.007	.5	.0	10.9	.0	.04	250.0	-25.0	1.0	1.4	0.	0.	337.	0.	0.	3.39
D415T1.006	.4	.0	10.8	.0	.03	250.0	-33.0	1.0	1.1	0.	0.	335.	0.	0.	2.77
D415T1.005	.5	.0	13.8	.0	.04	250.0	-50.0	1.0	1.3	0.	0.	427.	0.	0.	3.22
D415T1.004	.4	.0	11.2	.0	.03	250.0	-75.0	1.0	1.2	0.	0.	347.	0.	0.	2.87
D415T2.009	.3	.0	9.9	.0	.01	250.0	25.0	1.0	.8	0.	0.	306.	0.	0.	.66
D415T2.008	.4	.0	9.2	.0	.03	250.0	.0	1.0	1.2	0.	0.	286.	0.	0.	2.86
D415T2.007	.4	.0	8.7	.0	.04	250.0	-25.0	1.0	1.1	0.	0.	271.	0.	0.	3.03
D415T2.006	.5	.0	8.8	.0	.04	250.0	-33.0	1.0	1.2	0.	0.	272.	0.	0.	3.05
D415T2.005	.5	.0	8.8	.0	.04	250.0	-50.0	1.0	1.4	0.	0.	274.	0.	0.	3.28
D415T2.004	.5	.0	8.9	.0	.04	250.0	-75.0	1.0	1.3	0.	0.	274.	0.	0.	3.34
D415T3.009	.4	.0	11.0	.0	.01	250.0	25.0	1.0	1.0	0.	0.	340.	0.	0.	1.09
D415T3.008	.5	.0	9.1	.0	.04	250.0	.0	1.0	1.2	0.	0.	280.	0.	0.	2.95
D415T3.007	.4	.0	9.9	.0	.04	250.0	-25.0	1.0	1.2	0.	0.	306.	0.	0.	3.00
D415T3.006	.5	.0	13.4	.0	.04	250.0	-33.0	1.0	1.3	0.	0.	416.	0.	0.	3.23
D415T3.005	.5	.0	12.4	.0	.04	250.0	-50.0	1.0	1.3	0.	0.	385.	0.	0.	3.53
D415T3.004	.5	.0	11.8	.0	.03	250.0	-75.0	1.0	1.2	0.	0.	364.	0.	0.	2.86

FALCON 4: LSR = 150, GAS = FREON 12

MODEL CONDITIONS						PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415T4.009	.4	.0	12.2	.0	.02	250.0	25.0	1.0	1.1	0.	0.	378.	0.	0.	1.45
D415T4.008	.5	.0	11.9	.0	.04	250.0	.0	1.0	1.4	0.	0.	369.	0.	0.	3.06
D415T4.007	.5	.0	11.9	.0	.04	250.0	-25.0	1.0	1.3	0.	0.	368.	0.	0.	3.12
D415T4.006	.5	.0	12.0	.0	.04	250.0	-33.0	1.0	1.3	0.	0.	370.	0.	0.	3.23
D415T4.005	.4	.0	9.6	.0	.04	250.0	-50.0	1.0	1.2	0.	0.	298.	0.	0.	3.35
D415T4.004	.5	.0	9.8	.0	.04	250.0	-75.0	1.0	1.2	0.	0.	305.	0.	0.	3.28
D415T5.009	.4	.0	13.3	.0	.01	250.0	25.0	1.0	1.0	0.	0.	413.	0.	0.	.84
D415T5.008	.5	.0	13.2	.0	.04	250.0	.0	1.0	1.3	0.	0.	409.	0.	0.	3.00
D415T5.007	.4	.0	12.5	.0	.04	250.0	-25.0	1.0	1.2	0.	0.	387.	0.	0.	3.10
D415T5.006	.4	.0	8.0	.0	.04	250.0	-33.0	1.0	1.2	0.	0.	248.	0.	0.	3.18
D415T5.005	.4	.0	13.4	.0	.04	250.0	-50.0	1.0	1.2	0.	0.	415.	0.	0.	3.25
D415T5.004	.5	.0	12.0	.0	.04	250.0	-75.0	1.0	1.3	0.	0.	370.	0.	0.	3.25
D415U1.009	.4	.0	10.7	.0	.01	250.0	25.0	5.0	1.0	0.	0.	332.	0.	0.	.52
D415U1.008	.4	.0	9.6	.0	.02	250.0	.0	5.0	1.1	0.	0.	296.	0.	0.	1.84
D415U1.007	.4	.0	10.4	.0	.03	250.0	-25.0	5.0	1.1	0.	0.	323.	0.	0.	2.59
D415U1.006	.5	.0	11.4	.0	.03	250.0	-33.0	5.0	1.2	0.	0.	353.	0.	0.	2.61
D415U1.005	.5	.0	11.5	.0	.03	250.0	-50.0	5.0	1.2	0.	0.	356.	0.	0.	2.75
D415U1.004	.4	.0	11.6	.0	.03	250.0	-75.0	5.0	1.2	0.	0.	358.	0.	0.	2.31
D415U2.009	.3	.0	11.4	.0	.01	250.0	25.0	5.0	.9	0.	0.	353.	0.	0.	.67
D415U2.008	.6	.0	11.5	.0	.03	250.0	.0	5.0	1.5	0.	0.	355.	0.	0.	2.55
D415U2.007	.4	.0	11.4	.0	.03	250.0	-25.0	5.0	1.2	0.	0.	354.	0.	0.	2.62
D415U2.006	.5	.0	10.9	.0	.03	250.0	-33.0	5.0	1.4	0.	0.	337.	0.	0.	2.55
D415U2.005	.5	.0	10.8	.0	.03	250.0	-50.0	5.0	1.3	0.	0.	334.	0.	0.	2.88
D415U2.004	.5	.0	10.9	.0	.03	250.0	-75.0	5.0	1.3	0.	0.	339.	0.	0.	2.43
D415U3.009	.2	.0	11.4	.0	.00	250.0	25.0	5.0	.6	0.	0.	354.	0.	0.	.48
D415U3.008	.4	.0	10.7	.0	.02	250.0	.0	5.0	1.1	0.	0.	331.	0.	0.	1.87
D415U3.007	.4	.0	10.5	.0	.03	250.0	-25.0	5.0	1.1	0.	0.	326.	0.	0.	2.45
D415U3.006	.4	.0	10.6	.0	.02	250.0	-33.0	5.0	1.2	0.	0.	327.	0.	0.	2.20
D415U3.005	.5	.0	9.8	.0	.03	250.0	-50.0	5.0	1.3	0.	0.	305.	0.	0.	2.65
D415U3.004	.5	.0	8.8	.0	.03	250.0	-75.0	5.0	1.4	0.	0.	272.	0.	0.	2.69
D415U4.009	.4	.0	12.5	.0	.01	250.0	25.0	5.0	1.0	0.	0.	388.	0.	0.	.66
D415U4.008	.5	.0	9.9	.0	.04	250.0	.0	5.0	1.3	0.	0.	306.	0.	0.	3.11
D415U4.007	.5	.0	12.0	.0	.03	250.0	-25.0	5.0	1.4	0.	0.	372.	0.	0.	2.63
D415U4.006	.6	.0	12.0	.0	.03	250.0	-33.0	5.0	1.5	0.	0.	370.	0.	0.	2.90
D415U4.005	.5	.0	12.0	.0	.04	250.0	-50.0	5.0	1.3	0.	0.	371.	0.	0.	3.21
D415U4.004	.5	.0	10.0	.0	.03	250.0	-75.0	5.0	1.3	0.	0.	309.	0.	0.	2.61
D415U5.009	.3	.0	12.7	.0	.00	250.0	25.0	5.0	.8	0.	0.	393.	0.	0.	.23
D415U5.008	.5	.0	12.8	.0	.02	250.0	.0	5.0	1.3	0.	0.	395.	0.	0.	2.05
D415U5.007	.4	.0	12.8	.0	.03	250.0	-25.0	5.0	1.1	0.	0.	396.	0.	0.	2.30
D415U5.006	.5	.0	12.4	.0	.03	250.0	-33.0	5.0	1.3	0.	0.	385.	0.	0.	2.28
D415U5.005	.5	.0	9.5	.0	.03	250.0	-50.0	5.0	1.4	0.	0.	294.	0.	0.	2.80
D415U5.004	.4	.0	8.5	.0	.03	250.0	-75.0	5.0	1.2	0.	0.	262.	0.	0.	2.45

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415V1.009	.2	.0	.0	.0	.00	250.0	25.0	11.0	.5	0.	0.	0.	0.	0.	.25
D415V1.008	.3	.0	8.6	.0	.01	250.0	.0	11.0	.9	0.	0.	267.	0.	0.	1.11
D415V1.007	.3	.0	8.8	.0	.02	250.0	-25.0	11.0	.9	0.	0.	273.	0.	0.	1.60
D415V1.006	.4	.0	8.9	.0	.02	250.0	-33.0	11.0	1.0	0.	0.	274.	0.	0.	1.49
D415V1.005	.4	.0	11.1	.0	.02	250.0	-50.0	11.0	1.1	0.	0.	343.	0.	0.	1.92
D415V1.004	.4	.0	11.4	.0	.02	250.0	-75.0	11.0	1.0	0.	0.	352.	0.	0.	1.61
D415V2.009	.3	.0	11.4	.0	.00	250.0	25.0	11.0	.8	0.	0.	354.	0.	0.	.17
D415V2.008	.5	.0	11.3	.0	.02	250.0	.0	11.0	1.3	0.	0.	349.	0.	0.	1.36
D415V2.007	.5	.0	11.6	.0	.02	250.0	-25.0	11.0	1.4	0.	0.	358.	0.	0.	1.94
D415V2.006	.5	.0	11.4	.0	.02	250.0	-33.0	11.0	1.3	0.	0.	353.	0.	0.	1.98
D415V2.005	.4	.0	13.1	.0	.03	250.0	-50.0	11.0	1.2	0.	0.	405.	0.	0.	2.14
D415V2.004	.5	.0	10.5	.0	.02	250.0	-75.0	11.0	1.2	0.	0.	324.	0.	0.	1.74
D415V3.009	.3	.0	10.4	.0	.00	250.0	25.0	11.0	.9	0.	0.	323.	0.	0.	.41
D415V3.008	.4	.0	12.7	.0	.02	250.0	.0	11.0	1.2	0.	0.	392.	0.	0.	1.70
D415V3.007	.4	.0	12.2	.0	.02	250.0	-25.0	11.0	1.0	0.	0.	379.	0.	0.	1.85
D415V3.006	.5	.0	12.4	.0	.02	250.0	-33.0	11.0	1.3	0.	0.	384.	0.	0.	1.83
D415V3.005	.5	.0	12.3	.0	.03	250.0	-50.0	11.0	1.3	0.	0.	382.	0.	0.	2.12
D415V3.004	.4	.0	11.8	.0	.02	250.0	-75.0	11.0	1.2	0.	0.	366.	0.	0.	1.96
D415V4.009	.2	.0	11.1	.0	.00	250.0	25.0	11.0	.6	0.	0.	342.	0.	0.	.38
D415V4.008	.5	.0	12.9	.0	.02	250.0	.0	11.0	1.4	0.	0.	400.	0.	0.	1.98
D415V4.007	.5	.0	12.8	.0	.03	250.0	-25.0	11.0	1.4	0.	0.	396.	0.	0.	2.17
D415V4.006	.6	.0	9.7	.0	.02	250.0	-33.0	11.0	1.7	0.	0.	299.	0.	0.	1.95
D415V4.005	.5	.0	9.7	.0	.02	250.0	-50.0	11.0	1.4	0.	0.	299.	0.	0.	2.03
D415V4.004	.4	.0	10.0	.0	.02	250.0	-75.0	11.0	1.2	0.	0.	309.	0.	0.	1.48
D415V5.009	.2	.0	14.7	.0	.00	250.0	25.0	11.0	.6	0.	0.	455.	0.	0.	.37
D415V5.008	.4	.0	9.8	.0	.02	250.0	.0	11.0	1.2	0.	0.	303.	0.	0.	1.74
D415V5.007	.4	.0	13.5	.0	.03	250.0	-25.0	11.0	1.1	0.	0.	417.	0.	0.	2.31
D415V5.006	.5	.0	10.9	.0	.02	250.0	-33.0	11.0	1.4	0.	0.	338.	0.	0.	2.17
D415V5.005	.5	.0	10.8	.0	.03	250.0	-50.0	11.0	1.3	0.	0.	334.	0.	0.	2.43
D415V5.004	.5	.0	10.8	.0	.02	250.0	-75.0	11.0	1.3	0.	0.	335.	0.	0.	2.12
D415W1.009	.1	.0	.0	.0	.00	250.0	25.0	17.0	.2	0.	0.	0.	0.	0.	.05
D415W1.008	.3	.0	9.6	.0	.01	250.0	.0	17.0	.9	0.	0.	297.	0.	0.	.59
D415W1.007	.4	.0	8.6	.0	.02	250.0	-25.0	17.0	1.1	0.	0.	265.	0.	0.	1.57
D415W1.006	.4	.0	9.2	.0	.02	250.0	-33.0	17.0	1.2	0.	0.	284.	0.	0.	1.50
D415W1.005	.4	.0	9.2	.0	.02	250.0	-50.0	17.0	1.0	0.	0.	285.	0.	0.	1.56
D415W1.004	.4	.0	11.5	.0	.02	250.0	-75.0	17.0	1.0	0.	0.	357.	0.	0.	1.33
D415W2.009	.3	.0	11.5	.0	.01	250.0	25.0	17.0	.7	0.	0.	356.	0.	0.	.45
D415W2.008	.4	.0	11.4	.0	.01	250.0	.0	17.0	1.1	0.	0.	354.	0.	0.	1.25
D415W2.007	.3	.0	7.9	.0	.02	250.0	-25.0	17.0	.9	0.	0.	243.	0.	0.	1.38
D415W2.006	.4	.0	13.0	.0	.01	250.0	-33.0	17.0	1.0	0.	0.	403.	0.	0.	1.42
D415W2.005	.4	.0	11.1	.0	.02	250.0	-50.0	17.0	1.2	0.	0.	344.	0.	0.	1.40
D415W2.004	.4	.0	10.0	.0	.02	250.0	-75.0	17.0	1.1	0.	0.	310.	0.	0.	1.35

FALCON 4: LSR = 150, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D415W3.009	.1	.0	.0	.0	.00	250.0	25.0	17.0	.4	0.	0.	0.	0.	0.	.12
D415W3.008	.4	.0	8.9	.0	.01	250.0	.0	17.0	1.2	0.	0.	276.	0.	0.	1.04
D415W3.007	.3	.0	12.9	.0	.01	250.0	-25.0	17.0	.9	0.	0.	401.	0.	0.	1.19
D415W3.006	.3	.0	12.8	.0	.01	250.0	-33.0	17.0	.9	0.	0.	397.	0.	0.	.91
D415W3.005	.4	.0	13.3	.0	.02	250.0	-50.0	17.0	1.0	0.	0.	413.	0.	0.	1.42
D415W3.004	.5	.0	13.7	.0	.01	250.0	-75.0	17.0	1.3	0.	0.	425.	0.	0.	1.20
D415W4.009	.3	.0	12.4	.0	.00	250.0	25.0	17.0	.8	0.	0.	383.	0.	0.	.29
D415W4.008	.3	.0	12.0	.0	.01	250.0	.0	17.0	.9	0.	0.	370.	0.	0.	1.01
D415W4.007	.3	.0	12.2	.0	.01	250.0	-25.0	17.0	.9	0.	0.	379.	0.	0.	.99
D415W4.006	.3	.0	8.1	.0	.01	250.0	-33.0	17.0	.9	0.	0.	252.	0.	0.	1.17
D415W4.005	.4	.0	11.2	.0	.02	250.0	-50.0	17.0	1.2	0.	0.	346.	0.	0.	1.42
D415W4.004	.5	.0	11.3	.0	.02	250.0	-75.0	17.0	1.2	0.	0.	350.	0.	0.	1.44
D415W5.009	.2	.0	.0	.0	.00	250.0	25.0	17.0	.5	0.	0.	0.	0.	0.	.26
D415W5.008	.4	.0	11.4	.0	.02	250.0	.0	17.0	1.0	0.	0.	353.	0.	0.	1.49
D415W5.007	.3	.0	9.3	.0	.02	250.0	-25.0	17.0	.8	0.	0.	287.	0.	0.	1.38
D415W5.006	.4	.0	13.3	.0	.01	250.0	-33.0	17.0	1.1	0.	0.	412.	0.	0.	1.36
D415W5.005	.4	.0	10.5	.0	.02	250.0	-50.0	17.0	1.1	0.	0.	325.	0.	0.	1.71
D415W5.004	.4	.0	8.3	.0	.02	250.0	-75.0	17.0	1.0	0.	0.	257.	0.	0.	1.44

FALCON 4: LSR = 200, GAS = FREON 12

	MODEL CONDITIONS					PROTOTYPE CONDITIONS									
FILE NAME	PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420A1.009	.8	.0	6.5	.0	.00	-62.0	30.0	2.0	2.1	0.	0.	233.	0.	0.	.54
D420A1.008	19.7	.4	5.5	58.2	.75	-62.0	20.0	2.0	39.9	36.	57.	197.	382.	998.	65.44
D420A1.007	16.4	.6	6.4	24.0	.94	-62.0	10.0	2.0	34.6	24.	31.	229.	588.	589.	82.06
D420A1.006	17.1	.4	4.2	50.2	1.09	-62.0	.0	2.0	35.8	14.	32.	149.	469.	733.	92.98
D420A1.005	19.0	.4	6.3	61.0	.70	-62.0	-20.0	2.0	38.8	27.	29.	227.	425.	621.	62.16
D420A1.004	1.2	6.8	9.3	9.5	.05	-62.0	-30.0	2.0	3.2	0.	0.	332.	0.	0.	4.98
D420A2.009	.5	.0	11.0	.0	.00	-62.0	30.0	2.0	1.4	0.	0.	392.	0.	0.	.38
D420A2.008	20.7	.3	8.8	53.7	.96	-62.0	20.0	2.0	41.3	11.	29.	315.	497.	1093.	82.52
D420A2.007	19.6	.3	8.9	58.3	1.13	-62.0	10.0	2.0	39.8	21.	29.	320.	441.	843.	96.84
D420A2.006	21.8	.5	7.7	61.3	1.26	-62.0	.0	2.0	43.0	25.	29.	274.	605.	1236.	106.34
D420A2.005	24.0	.3	9.5	59.3	.92	-62.0	-20.0	2.0	46.0	12.	24.	338.	2119.	2119.	83.83
D420A2.004	1.4	5.3	5.4	9.2	.07	-62.0	-30.0	2.0	3.8	0.	0.	191.	0.	0.	6.78
D420A3.009	.7	.0	8.2	.0	.00	-62.0	30.0	2.0	1.7	0.	0.	293.	0.	0.	.60
D420A3.008	20.6	.5	8.9	58.7	1.06	-62.0	20.0	2.0	41.2	16.	17.	318.	714.	1985.	90.28
D420A3.007	18.5	.6	8.2	56.3	1.11	-62.0	10.0	2.0	38.0	21.	27.	294.	487.	1858.	94.71
D420A3.006	23.0	.4	8.5	55.3	1.45	-62.0	.0	2.0	44.7	16.	38.	303.	572.	863.	118.99
D420A3.005	19.7	.3	4.9	61.7	.99	-62.0	-20.0	2.0	39.8	15.	26.	177.	1456.	2149.	86.34
D420A3.004	1.8	2.7	9.0	10.4	.07	-62.0	-30.0	2.0	4.8	0.	0.	323.	0.	0.	6.88
D420A4.009	.3	.0	8.2	.0	.00	-62.0	30.0	2.0	.8	0.	0.	292.	0.	0.	.42
D420A4.008	22.2	.5	8.8	57.5	1.06	-62.0	20.0	2.0	43.6	20.	20.	313.	491.	1824.	89.81
D420A4.007	21.6	.4	8.3	45.0	1.08	-62.0	10.0	2.0	42.7	20.	20.	298.	567.	1429.	92.72
D420A4.006	20.3	.4	7.1	59.9	1.52	-62.0	.0	2.0	40.8	14.	28.	252.	534.	809.	123.96
D420A4.005	20.0	.1	9.5	61.7	1.12	-62.0	-20.0	2.0	40.4	2.	16.	341.	2014.	2085.	98.25
D420A4.004	1.5	3.6	10.2	11.3	.07	-62.0	-30.0	2.0	3.8	0.	0.	366.	0.	0.	7.26
D420A5.009	.6	.0	6.7	.0	.00	-62.0	30.0	2.0	1.5	0.	0.	239.	0.	0.	.35
D420A5.008	21.9	.1	8.3	61.6	1.05	-62.0	20.0	2.0	43.1	17.	17.	298.	636.	2062.	90.04
D420A5.007	18.6	.5	5.7	61.1	1.13	-62.0	10.0	2.0	38.2	19.	27.	205.	545.	896.	97.94
D420A5.006	23.2	.4	6.9	56.7	1.59	-62.0	.0	2.0	45.0	14.	38.	247.	651.	701.	127.12
D420A5.005	23.7	.0	7.7	60.5	1.02	-62.0	-20.0	2.0	45.6	9.	16.	276.	2106.	2165.	95.59
D420A5.004	1.6	6.6	8.2	10.8	.07	-62.0	-30.0	2.0	4.1	0.	0.	294.	0.	0.	7.06
D420B1.009	.4	.0	9.8	.0	.02	-32.0	30.0	1.0	1.1	0.	0.	349.	0.	0.	1.58
D420B1.008	20.5	.2	8.2	59.1	.53	-32.0	20.0	1.0	41.1	7.	11.	295.	502.	2112.	48.16
D420B1.007	17.3	.2	3.9	13.2	.31	-32.0	10.0	1.0	36.1	7.	7.	140.	326.	339.	27.78
D420B1.006	23.9	.2	8.6	58.6	.68	-32.0	.0	1.0	45.9	9.	18.	307.	380.	934.	57.93
D420B1.005	23.0	.4	6.9	52.7	1.10	-32.0	-20.0	1.0	44.7	18.	22.	247.	435.	595.	90.55
D420B1.004	.8	.0	8.4	.0	.04	-32.0	-30.0	1.0	2.2	0.	0.	299.	0.	0.	4.04
D420B2.009	.7	.0	9.2	.0	.02	-32.0	30.0	1.0	1.9	0.	0.	327.	0.	0.	1.68
D420B2.008	20.5	.2	5.2	52.7	.76	-32.0	20.0	1.0	41.1	7.	8.	187.	466.	1883.	65.31
D420B2.007	24.3	.2	6.2	11.6	.39	-32.0	10.0	1.0	46.5	5.	6.	222.	285.	331.	33.82
D420B2.006	25.2	.3	8.8	50.0	1.03	-32.0	.0	1.0	47.6	9.	10.	313.	544.	1591.	83.72
D420B2.005	26.6	.4	6.3	53.5	1.34	-32.0	-20.0	1.0	49.5	14.	20.	227.	471.	1666.	107.42
D420B2.004	1.3	10.2	10.2	10.3	.05	-32.0	-30.0	1.0	3.4	0.	0.	364.	0.	0.	4.92

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420B3.009	.4	.0	9.4	.0	.02	-32.0	30.0	1.0	1.1	0.	0.	335.	0.	0.	1.71
D420B3.008	20.1	.2	5.9	53.5	.63	-32.0	20.0	1.0	40.5	10.	10.	211.	794.	1914.	54.04
D420B3.007	23.7	.2	7.9	14.2	.38	-32.0	10.0	1.0	45.7	6.	6.	281.	326.	351.	33.08
D420B3.006	24.6	.2	7.7	60.8	.75	-32.0	.0	1.0	46.9	9.	10.	276.	445.	756.	62.60
D420B3.005	22.9	.6	7.3	55.5	1.24	-32.0	-20.0	1.0	44.6	24.	30.	260.	514.	516.	101.20
D420B3.004	.9	.0	5.2	.0	.05	-32.0	-30.0	1.0	2.4	0.	0.	187.	0.	0.	5.15
D420B4.009	.6	.0	9.0	.0	.01	-32.0	30.0	1.0	1.5	0.	0.	321.	0.	0.	1.08
D420B4.008	21.7	.1	4.9	59.9	.89	-32.0	20.0	1.0	42.8	5.	6.	175.	657.	1689.	74.07
D420B4.007	29.3	.1	8.8	13.9	.50	-32.0	10.0	1.0	52.8	5.	5.	314.	335.	370.	42.21
D420B4.006	28.5	.3	8.2	60.5	1.19	-32.0	.0	1.0	51.9	10.	11.	295.	436.	897.	94.70
D420B4.005	34.3	.5	6.9	59.8	1.39	-32.0	-20.0	1.0	58.5	17.	20.	246.	472.	2139.	110.00
D420B4.004	.7	.0	6.2	.0	.04	-32.0	-30.0	1.0	2.0	0.	0.	222.	0.	0.	4.17
D420B5.009	.6	.0	7.5	.0	.00	-32.0	30.0	1.0	1.5	0.	0.	267.	0.	0.	.68
D420B5.008	20.9	.2	6.3	45.2	.65	-32.0	20.0	1.0	41.6	8.	11.	225.	454.	1552.	55.15
D420B5.007	21.9	.2	4.6	11.6	.36	-32.0	10.0	1.0	43.1	6.	6.	164.	300.	382.	31.59
D420B5.006	23.1	.3	9.1	30.7	.90	-32.0	.0	1.0	44.8	10.	10.	324.	468.	593.	74.89
D420B5.005	23.0	.4	4.1	57.0	1.19	-32.0	-20.0	1.0	44.6	30.	35.	146.	392.	433.	96.56
D420B5.004	.8	.0	9.6	.0	.04	-32.0	-30.0	1.0	2.1	0.	0.	345.	0.	0.	4.26
D420C1.009	.3	.0	11.4	.0	.02	-2.0	30.0	1.0	.7	0.	0.	408.	0.	0.	1.56
D420C1.008	2.8	2.2	8.8	20.6	.13	-2.0	20.0	1.0	7.1	104.	0.	316.	0.	317.	13.11
D420C1.007	1.8	2.8	7.4	11.3	.12	-2.0	10.0	1.0	4.6	0.	0.	264.	0.	0.	11.86
D420C1.006	1.6	2.9	9.3	11.1	.12	-2.0	.0	1.0	4.1	0.	0.	332.	0.	0.	11.17
D420C1.005	1.6	4.8	8.4	10.1	.11	-2.0	-20.0	1.0	4.3	0.	0.	301.	0.	0.	10.76
D420C1.004	1.0	.0	7.2	.0	.05	-2.0	-30.0	1.0	2.6	0.	0.	256.	0.	0.	5.36
D420C2.009	.3	.0	7.3	.0	.01	-2.0	30.0	1.0	.9	0.	0.	261.	0.	0.	1.31
D420C2.008	2.4	.8	7.9	51.4	.14	-2.0	20.0	1.0	6.2	282.	0.	282.	0.	333.	13.45
D420C2.007	2.5	4.8	8.7	12.5	.11	-2.0	10.0	1.0	6.4	309.	0.	310.	0.	311.	10.86
D420C2.006	1.6	5.2	8.2	11.4	.10	-2.0	.0	1.0	4.3	0.	0.	293.	0.	0.	9.81
D420C2.005	1.8	4.3	5.0	10.2	.10	-2.0	-20.0	1.0	4.7	0.	0.	179.	0.	0.	9.58
D420C2.004	1.1	6.6	6.6	9.1	.05	-2.0	-30.0	1.0	3.0	0.	0.	234.	0.	0.	5.33
D420C3.009	.7	.0	9.3	.0	.01	-2.0	30.0	1.0	1.9	0.	0.	332.	0.	0.	1.06
D420C3.008	2.4	1.5	8.7	28.5	.11	-2.0	20.0	1.0	6.3	308.	0.	309.	0.	310.	10.93
D420C3.007	2.0	2.9	8.0	10.1	.11	-2.0	10.0	1.0	5.1	287.	0.	287.	0.	311.	10.77
D420C3.006	1.7	3.0	3.0	9.8	.10	-2.0	.0	1.0	4.5	0.	0.	108.	0.	0.	9.83
D420C3.005	3.1	.3	5.8	10.1	.11	-2.0	-20.0	1.0	8.0	206.	0.	207.	0.	209.	10.26
D420C3.004	1.0	.0	6.7	.0	.05	-2.0	-30.0	1.0	2.6	0.	0.	238.	0.	0.	4.97
D420C4.009	.5	.0	9.4	.0	.01	-2.0	30.0	1.0	1.4	0.	0.	336.	0.	0.	1.41
D420C4.008	3.1	.2	7.7	31.8	.12	-2.0	20.0	1.0	7.9	8.	0.	277.	0.	463.	11.71
D420C4.007	1.5	.3	5.4	10.2	.10	-2.0	10.0	1.0	4.0	0.	0.	192.	0.	0.	10.07
D420C4.006	1.7	.9	8.9	10.3	.10	-2.0	.0	1.0	4.5	0.	0.	318.	0.	0.	9.56
D420C4.005	1.9	.4	.4	10.1	.10	-2.0	-20.0	1.0	4.9	0.	0.	13.	0.	0.	9.45
D420C4.004	1.0	8.9	8.9	8.9	.06	-2.0	-30.0	1.0	2.7	0.	0.	317.	0.	0.	5.69

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420C5.009	.9	.0	9.1	.0	.01	-2.0	30.0	1.0	2.4	0.	0.	326.	0.	0.	1.41
D420C5.008	2.8	.5	21.8	30.8	.12	-2.0	20.0	1.0	7.3	91.	0.	779.	0.	779.	11.94
D420C5.007	1.8	.7	8.7	10.8	.11	-2.0	10.0	1.0	4.7	0.	0.	311.	0.	0.	10.76
D420C5.006	2.8	.2	8.3	10.9	.10	-2.0	.0	1.0	7.2	29.	0.	296.	0.	297.	10.01
D420C5.005	2.6	5.7	6.8	10.9	.11	-2.0	-20.0	1.0	6.7	243.	0.	244.	0.	314.	10.90
D420C5.004	1.0	3.9	3.9	7.9	.06	-2.0	-30.0	1.0	2.8	0.	0.	138.	0.	0.	5.53
D420D1.009	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.19
D420D1.008	.3	.0	11.1	.0	.00	50.0	25.0	1.0	.8	0.	0.	397.	0.	0.	.58
D420D1.007	.7	.0	8.5	.0	.05	50.0	.0	1.0	2.0	0.	0.	304.	0.	0.	4.95
D420D1.006	.6	.0	7.6	.0	.05	50.0	-25.0	1.0	1.7	0.	0.	271.	0.	0.	4.88
D420D1.005	.5	.0	7.7	.0	.02	50.0	-50.0	1.0	1.3	0.	0.	274.	0.	0.	2.17
D420D1.004	.2	.0	.0	.0	.00	50.0	-75.0	1.0	.5	0.	0.	0.	0.	0.	.25
D420D2.009	.0	.0	.0	.0	-.01	50.0	50.0	1.0	.0	0.	0.	0.	0.	0.	.00
D420D2.008	.4	.0	9.7	.0	.01	50.0	25.0	1.0	1.1	0.	0.	346.	0.	0.	1.18
D420D2.007	.6	.0	6.0	.0	.06	50.0	.0	1.0	1.7	0.	0.	213.	0.	0.	5.39
D420D2.006	.7	.0	6.7	.0	.06	50.0	-25.0	1.0	1.8	0.	0.	238.	0.	0.	5.34
D420D2.005	.6	.0	8.1	.0	.03	50.0	-50.0	1.0	1.6	0.	0.	289.	0.	0.	2.81
D420D2.004	.2	.0	6.1	.0	.00	50.0	-75.0	1.0	.7	0.	0.	219.	0.	0.	.24
D420D3.009	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.15
D420D3.008	.5	.0	8.1	.0	.01	50.0	25.0	1.0	1.3	0.	0.	290.	0.	0.	.99
D420D3.007	.7	.0	9.4	.0	.06	50.0	.0	1.0	1.9	0.	0.	338.	0.	0.	5.55
D420D3.006	.7	.0	8.2	.0	.05	50.0	-25.0	1.0	1.9	0.	0.	292.	0.	0.	5.18
D420D3.005	.6	.0	10.8	.0	.03	50.0	-50.0	1.0	1.6	0.	0.	385.	0.	0.	2.63
D420D3.004	.2	.0	.0	.0	.00	50.0	-75.0	1.0	.4	0.	0.	0.	0.	0.	.26
D420D4.009	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.30
D420D4.008	.4	.0	8.3	.0	.00	50.0	25.0	1.0	1.1	0.	0.	296.	0.	0.	.59
D420D4.007	.8	.0	8.1	.0	.05	50.0	.0	1.0	2.0	0.	0.	288.	0.	0.	5.28
D420D4.006	.8	.0	8.6	.0	.06	50.0	-25.0	1.0	2.1	0.	0.	307.	0.	0.	5.43
D420D4.005	.6	.0	10.5	.0	.03	50.0	-50.0	1.0	1.5	0.	0.	376.	0.	0.	2.74
D420D4.004	.2	.0	.0	.0	.00	50.0	-75.0	1.0	.4	0.	0.	0.	0.	0.	.38
D420D5.009	.0	.0	.0	.0	.00	50.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.16
D420D5.008	.5	.0	9.9	.0	.01	50.0	25.0	1.0	1.5	0.	0.	354.	0.	0.	1.28
D420D5.007	.7	.0	8.5	.0	.06	50.0	.0	1.0	1.8	0.	0.	302.	0.	0.	5.42
D420D5.006	.7	.0	8.5	.0	.05	50.0	-25.0	1.0	1.8	0.	0.	303.	0.	0.	5.14
D420D5.005	.8	.0	8.0	.0	.03	50.0	-50.0	1.0	2.0	0.	0.	287.	0.	0.	3.03
D420D5.004	.3	.0	9.3	.0	.01	50.0	-75.0	1.0	.8	0.	0.	332.	0.	0.	.53
D420E1.009	.0	.0	.0	.0	.00	50.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.11
D420E1.008	.5	.0	8.5	.0	.01	50.0	25.0	5.0	1.4	0.	0.	304.	0.	0.	1.02
D420E1.007	.6	.0	9.8	.0	.04	50.0	.0	5.0	1.6	0.	0.	351.	0.	0.	4.19
D420E1.006	.6	.0	8.0	.0	.05	50.0	-25.0	5.0	1.7	0.	0.	287.	0.	0.	4.62
D420E1.005	.5	.0	8.6	.0	.01	50.0	-50.0	5.0	1.4	0.	0.	309.	0.	0.	1.43
D420E1.004	.1	.0	.0	.0	.00	50.0	-75.0	5.0	.3	0.	0.	0.	0.	0.	.23

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420E2.009	.0	.0	.0	.0	.00	50.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.09
D420E2.008	.5	.0	8.0	.0	.00	50.0	25.0	5.0	1.5	0.	0.	287.	0.	0.	.70
D420E2.007	.6	.0	9.2	.0	.05	50.0	.0	5.0	1.7	0.	0.	330.	0.	0.	4.50
D420E2.006	.7	.0	8.8	.0	.05	50.0	-25.0	5.0	1.8	0.	0.	313.	0.	0.	4.90
D420E2.005	.5	.0	7.8	.0	.02	50.0	-50.0	5.0	1.4	0.	0.	280.	0.	0.	1.86
D420E2.004	.2	.0	.0	.0	.00	50.0	-75.0	5.0	.5	0.	0.	0.	0.	0.	.46
D420E3.009	.0	.0	.0	.0	.00	50.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.25
D420E3.008	.5	.0	10.4	.0	.01	50.0	25.0	5.0	1.4	0.	0.	371.	0.	0.	.66
D420E3.007	.9	.0	10.3	.0	.05	50.0	.0	5.0	2.5	0.	0.	368.	0.	0.	4.82
D420E3.006	.7	.0	4.5	.0	.05	50.0	-25.0	5.0	2.0	0.	0.	162.	0.	0.	5.24
D420E3.005	.6	.0	6.7	.0	.02	50.0	-50.0	5.0	1.7	0.	0.	239.	0.	0.	1.75
D420E3.004	.2	.0	.0	.0	.00	50.0	-75.0	5.0	.5	0.	0.	0.	0.	0.	.12
D420E4.009	.0	.0	.0	.0	.00	50.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.02
D420E4.008	.4	.0	11.5	.0	.01	50.0	25.0	5.0	1.2	0.	0.	410.	0.	0.	.95
D420E4.007	.6	.0	7.9	.0	.05	50.0	.0	5.0	1.7	0.	0.	281.	0.	0.	4.99
D420E4.006	.7	.0	7.8	.0	.05	50.0	-25.0	5.0	1.8	0.	0.	278.	0.	0.	5.02
D420E4.005	.5	.0	8.7	.0	.02	50.0	-50.0	5.0	1.3	0.	0.	310.	0.	0.	1.67
D420E4.004	.2	.0	8.9	.0	.00	50.0	-75.0	5.0	.6	0.	0.	319.	0.	0.	.09
D420E5.009	.1	.0	.0	.0	.00	50.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.09
D420E5.008	.6	.0	9.1	.0	.01	50.0	25.0	5.0	1.5	0.	0.	326.	0.	0.	1.35
D420E5.007	.7	.0	7.5	.0	.05	50.0	.0	5.0	1.8	0.	0.	268.	0.	0.	5.10
D420E5.006	.7	.0	8.1	.0	.06	50.0	-25.0	5.0	1.9	0.	0.	290.	0.	0.	5.38
D420E5.005	.6	.0	10.4	.0	.02	50.0	-50.0	5.0	1.5	0.	0.	370.	0.	0.	1.83
D420E5.004	.2	.0	.0	.0	.00	50.0	-75.0	5.0	.5	0.	0.	0.	0.	0.	.33
D420F1.009	.0	.0	.0	.0	.00	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.10
D420F1.008	.7	.0	6.6	.0	.01	50.0	25.0	11.0	1.9	0.	0.	237.	0.	0.	.84
D420F1.007	.6	.0	9.3	.0	.03	50.0	.0	11.0	1.6	0.	0.	332.	0.	0.	3.28
D420F1.006	.7	.0	5.6	.0	.04	50.0	-25.0	11.0	1.8	0.	0.	200.	0.	0.	3.74
D420F1.005	.4	.0	6.5	.0	.01	50.0	-50.0	11.0	1.2	0.	0.	233.	0.	0.	.96
D420F1.004	.3	.0	4.9	.0	.00	50.0	-75.0	11.0	.9	0.	0.	175.	0.	0.	.07
D420F2.009	.0	.0	.0	.0	.00	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.12
D420F2.008	.5	.0	5.9	.0	.00	50.0	25.0	11.0	1.5	0.	0.	209.	0.	0.	.63
D420F2.007	.7	.0	10.3	.0	.04	50.0	.0	11.0	1.8	0.	0.	367.	0.	0.	3.71
D420F2.006	.8	.0	8.7	.0	.05	50.0	-25.0	11.0	2.2	0.	0.	312.	0.	0.	4.71
D420F2.005	.5	.0	9.9	.0	.01	50.0	-50.0	11.0	1.2	0.	0.	352.	0.	0.	1.21
D420F2.004	.1	.0	.0	.0	.00	50.0	-75.0	11.0	.4	0.	0.	0.	0.	0.	.22
D420F3.009	.0	.0	.0	.0	.00	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.16
D420F3.008	.6	.0	5.4	.0	.01	50.0	25.0	11.0	1.5	0.	0.	192.	0.	0.	1.00
D420F3.007	.8	.0	10.7	.0	.04	50.0	.0	11.0	2.2	0.	0.	383.	0.	0.	3.57
D420F3.006	.8	.0	7.9	.0	.04	50.0	-25.0	11.0	2.1	0.	0.	281.	0.	0.	4.22
D420F3.005	.7	.0	7.7	.0	.01	50.0	-50.0	11.0	1.8	0.	0.	274.	0.	0.	1.31
D420F3.004	.3	.0	8.0	.0	.00	50.0	-75.0	11.0	.9	0.	0.	286.	0.	0.	.46

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420F4.009	.0	.0	.0	.0	.00	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.03
D420F4.008	.5	.0	10.7	.0	.01	50.0	25.0	11.0	1.4	0.	0.	383.	0.	0.	.69
D420F4.007	.5	.0	5.9	.0	.04	50.0	.0	11.0	1.5	0.	0.	211.	0.	0.	3.87
D420F4.006	.7	.0	9.0	.0	.05	50.0	-25.0	11.0	2.0	0.	0.	323.	0.	0.	4.57
D420F4.005	.5	.0	9.8	.0	.01	50.0	-50.0	11.0	1.2	0.	0.	349.	0.	0.	1.21
D420F4.004	.1	.0	.0	.0	.00	50.0	-75.0	11.0	.3	0.	0.	0.	0.	0.	.05
D420F5.009	.0	.0	.0	.0	.00	50.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.00
D420F5.008	.6	.0	9.6	.0	.01	50.0	25.0	11.0	1.5	0.	0.	342.	0.	0.	.68
D420F5.007	.6	.0	5.8	.0	.04	50.0	.0	11.0	1.7	0.	0.	206.	0.	0.	3.56
D420F5.006	.8	.0	7.2	.0	.04	50.0	-25.0	11.0	2.0	0.	0.	258.	0.	0.	4.32
D420F5.005	.7	.0	7.7	.0	.02	50.0	-50.0	11.0	1.8	0.	0.	274.	0.	0.	1.52
D420F5.004	.2	.0	4.9	.0	.00	50.0	-75.0	11.0	.6	0.	0.	175.	0.	0.	.19
D420G1.009	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.18
D420G1.008	.5	.0	11.1	.0	.01	50.0	25.0	17.0	1.3	0.	0.	398.	0.	0.	.73
D420G1.007	.7	.0	8.9	.0	.01	50.0	.0	17.0	1.8	0.	0.	320.	0.	0.	1.39
D420G1.006	.7	.0	9.7	.0	.03	50.0	-25.0	17.0	1.8	0.	0.	346.	0.	0.	3.16
D420G1.005	.6	.0	10.2	.0	.01	50.0	-50.0	17.0	1.5	0.	0.	363.	0.	0.	.88
D420G1.004	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.3	0.	0.	0.	0.	0.	.17
D420G2.009	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.03
D420G2.008	.7	.0	6.8	.0	.01	50.0	25.0	17.0	1.9	0.	0.	242.	0.	0.	1.16
D420G2.007	.6	.0	8.7	.0	.02	50.0	.0	17.0	1.6	0.	0.	312.	0.	0.	1.94
D420G2.006	.8	.0	9.8	.0	.03	50.0	-25.0	17.0	2.2	0.	0.	349.	0.	0.	3.43
D420G2.005	.5	.0	7.2	.0	.01	50.0	-50.0	17.0	1.4	0.	0.	258.	0.	0.	1.07
D420G2.004	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.3	0.	0.	0.	0.	0.	.34
D420G3.009	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.11
D420G3.008	.7	.0	7.9	.0	.01	50.0	25.0	17.0	1.7	0.	0.	281.	0.	0.	.81
D420G3.007	.6	.0	10.6	.0	.02	50.0	.0	17.0	1.7	0.	0.	378.	0.	0.	1.72
D420G3.006	.9	.0	9.4	.0	.03	50.0	-25.0	17.0	2.5	0.	0.	338.	0.	0.	3.45
D420G3.005	.6	.0	9.0	.0	.01	50.0	-50.0	17.0	1.6	0.	0.	321.	0.	0.	.87
D420G3.004	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.22
D420G4.009	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.05
D420G4.008	.7	.0	9.2	.0	.00	50.0	25.0	17.0	1.8	0.	0.	328.	0.	0.	.42
D420G4.007	.6	.0	8.0	.0	.02	50.0	.0	17.0	1.7	0.	0.	286.	0.	0.	1.71
D420G4.006	.8	.0	8.1	.0	.04	50.0	-25.0	17.0	2.2	0.	0.	290.	0.	0.	3.77
D420G4.005	.5	.0	5.2	.0	.01	50.0	-50.0	17.0	1.3	0.	0.	187.	0.	0.	.81
D420G4.004	.1	.0	.0	.0	.00	50.0	-75.0	17.0	.1	0.	0.	0.	0.	0.	.24
D420G5.009	.0	.0	.0	.0	.00	50.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.11
D420G5.008	.7	.0	6.8	.0	.00	50.0	25.0	17.0	1.9	0.	0.	243.	0.	0.	.63
D420G5.007	.6	.0	7.0	.0	.02	50.0	.0	17.0	1.5	0.	0.	250.	0.	0.	1.76
D420G5.006	.7	.0	6.2	.0	.03	50.0	-25.0	17.0	1.8	0.	0.	220.	0.	0.	3.26
D420G5.005	.5	.0	6.4	.0	.01	50.0	-50.0	17.0	1.3	0.	0.	230.	0.	0.	1.03
D420G5.004	.2	.0	.0	.0	.00	50.0	-75.0	17.0	.4	0.	0.	0.	0.	0.	.19

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420H1.009	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.25
D420H1.008	.3	.0	8.3	.0	.01	150.0	25.0	1.0	.8	0.	0.	298.	0.	0.	.82
D420H1.007	.4	.0	7.4	.0	.03	150.0	.0	1.0	1.1	0.	0.	265.	0.	0.	2.76
D420H1.006	.5	.0	7.7	.0	.03	150.0	-25.0	1.0	1.2	0.	0.	274.	0.	0.	3.07
D420H1.005	.4	.0	9.6	.0	.03	150.0	-50.0	1.0	1.2	0.	0.	343.	0.	0.	2.93
D420H1.004	.4	.0	9.5	.0	.02	150.0	-75.0	1.0	1.1	0.	0.	339.	0.	0.	1.98
D420H2.009	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.34
D420H2.008	.2	.0	7.8	.0	.00	150.0	25.0	1.0	.6	0.	0.	277.	0.	0.	.62
D420H2.007	.4	.0	10.3	.0	.03	150.0	.0	1.0	1.0	0.	0.	369.	0.	0.	2.78
D420H2.006	.4	.0	9.7	.0	.04	150.0	-25.0	1.0	1.0	0.	0.	348.	0.	0.	3.48
D420H2.005	.4	.0	9.4	.0	.03	150.0	-50.0	1.0	1.0	0.	0.	336.	0.	0.	2.88
D420H2.004	.4	.0	10.6	.0	.02	150.0	-75.0	1.0	1.0	0.	0.	379.	0.	0.	1.92
D420H3.009	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.22
D420H3.008	.5	.0	9.3	.0	.02	150.0	25.0	1.0	1.2	0.	0.	331.	0.	0.	1.51
D420H3.007	.4	.0	9.4	.0	.03	150.0	.0	1.0	1.2	0.	0.	336.	0.	0.	3.19
D420H3.006	.4	.0	8.5	.0	.03	150.0	-25.0	1.0	1.1	0.	0.	303.	0.	0.	3.13
D420H3.005	.4	.0	10.2	.0	.03	150.0	-50.0	1.0	1.1	0.	0.	364.	0.	0.	2.64
D420H3.004	.3	.0	8.1	.0	.02	150.0	-75.0	1.0	.9	0.	0.	289.	0.	0.	1.83
D420H4.009	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.20
D420H4.008	.3	.0	10.7	.0	.01	150.0	25.0	1.0	.8	0.	0.	383.	0.	0.	.78
D420H4.007	.5	.0	11.3	.0	.03	150.0	.0	1.0	1.2	0.	0.	403.	0.	0.	3.10
D420H4.006	.4	.0	8.9	.0	.03	150.0	-25.0	1.0	1.2	0.	0.	317.	0.	0.	3.37
D420H4.005	.5	.0	8.9	.0	.03	150.0	-50.0	1.0	1.3	0.	0.	317.	0.	0.	2.84
D420H4.004	.4	.0	9.2	.0	.02	150.0	-75.0	1.0	1.0	0.	0.	329.	0.	0.	2.14
D420H5.009	.0	.0	.0	.0	.00	150.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.20
D420H5.008	.3	.0	9.6	.0	.01	150.0	25.0	1.0	.8	0.	0.	342.	0.	0.	.86
D420H5.007	.4	.0	10.4	.0	.03	150.0	.0	1.0	1.2	0.	0.	372.	0.	0.	3.15
D420H5.006	.5	.0	9.9	.0	.04	150.0	-25.0	1.0	1.4	0.	0.	354.	0.	0.	3.42
D420H5.005	.5	.0	7.6	.0	.03	150.0	-50.0	1.0	1.2	0.	0.	271.	0.	0.	3.15
D420H5.004	.4	.0	9.1	.0	.02	150.0	-75.0	1.0	1.0	0.	0.	327.	0.	0.	2.26
D420I1.009	.0	.0	.0	.0	.00	150.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.05
D420I1.008	.2	.0	9.2	.0	.00	150.0	25.0	5.0	.6	0.	0.	329.	0.	0.	.44
D420I1.007	.4	.0	9.7	.0	.02	150.0	.0	5.0	1.2	0.	0.	345.	0.	0.	2.08
D420I1.006	.4	.0	10.4	.0	.02	150.0	-25.0	5.0	1.1	0.	0.	370.	0.	0.	2.35
D420I1.005	.4	.0	9.1	.0	.02	150.0	-50.0	5.0	1.0	0.	0.	324.	0.	0.	1.68
D420I1.004	.3	.0	7.8	.0	.01	150.0	-75.0	5.0	.9	0.	0.	279.	0.	0.	.93
D420I2.009	.0	.0	.0	.0	.00	150.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.00
D420I2.008	.2	.0	9.9	.0	.00	150.0	25.0	5.0	.6	0.	0.	354.	0.	0.	.35
D420I2.007	.4	.0	8.0	.0	.02	150.0	.0	5.0	1.1	0.	0.	287.	0.	0.	2.35
D420I2.006	.5	.0	9.5	.0	.03	150.0	-25.0	5.0	1.3	0.	0.	340.	0.	0.	2.83
D420I2.005	.4	.0	10.6	.0	.02	150.0	-50.0	5.0	1.1	0.	0.	379.	0.	0.	2.29
D420I2.004	.3	.0	10.5	.0	.01	150.0	-75.0	5.0	.9	0.	0.	376.	0.	0.	1.36

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420I3.009	.0	.0	.0	.0	.00	150.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.01
D420I3.008	.4	.0	9.8	.0	.00	150.0	25.0	5.0	1.1	0.	0.	351.	0.	0.	.26
D420I3.007	.4	.0	9.6	.0	.02	150.0	.0	5.0	1.0	0.	0.	342.	0.	0.	2.20
D420I3.006	.4	.0	8.6	.0	.03	150.0	-25.0	5.0	1.1	0.	0.	307.	0.	0.	2.73
D420I3.005	.4	.0	8.3	.0	.02	150.0	-50.0	5.0	1.0	0.	0.	295.	0.	0.	1.93
D420I3.004	.3	.0	7.5	.0	.01	150.0	-75.0	5.0	.9	0.	0.	268.	0.	0.	1.05
D420I4.009	.0	.0	.0	.0	.00	150.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.11
D420I4.008	.3	.0	12.1	.0	.01	150.0	25.0	5.0	.7	0.	0.	434.	0.	0.	.65
D420I4.007	.4	.0	7.1	.0	.03	150.0	.0	5.0	1.0	0.	0.	252.	0.	0.	2.65
D420I4.006	.5	.0	10.3	.0	.03	150.0	-25.0	5.0	1.3	0.	0.	370.	0.	0.	3.11
D420I4.005	.5	.0	10.6	.0	.03	150.0	-50.0	5.0	1.2	0.	0.	379.	0.	0.	2.52
D420I4.004	.4	.0	9.6	.0	.01	150.0	-75.0	5.0	1.0	0.	0.	343.	0.	0.	1.41
D420I5.009	.0	.0	.0	.0	.00	150.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.16
D420I5.008	.3	.0	9.2	.0	.00	150.0	25.0	5.0	.8	0.	0.	329.	0.	0.	.66
D420I5.007	.4	.0	11.2	.0	.03	150.0	.0	5.0	1.1	0.	0.	400.	0.	0.	2.48
D420I5.006	.5	.0	8.8	.0	.03	150.0	-25.0	5.0	1.3	0.	0.	315.	0.	0.	3.13
D420I5.005	.4	.0	10.4	.0	.02	150.0	-50.0	5.0	1.2	0.	0.	371.	0.	0.	2.20
D420I5.004	.4	.0	6.0	.0	.01	150.0	-75.0	5.0	1.2	0.	0.	215.	0.	0.	1.31
D420J1.009	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.26
D420J1.008	.2	.0	9.3	.0	.00	150.0	25.0	11.0	.6	0.	0.	332.	0.	0.	.20
D420J1.007	.3	.0	7.7	.0	.02	150.0	.0	11.0	.8	0.	0.	276.	0.	0.	1.53
D420J1.006	.4	.0	10.8	.0	.02	150.0	-25.0	11.0	1.0	0.	0.	385.	0.	0.	2.13
D420J1.005	.4	.0	10.4	.0	.02	150.0	-50.0	11.0	1.1	0.	0.	373.	0.	0.	1.64
D420J1.004	.3	.0	11.0	.0	.01	150.0	-75.0	11.0	.8	0.	0.	393.	0.	0.	.71
D420J2.009	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.01
D420J2.008	.3	.0	10.9	.0	.00	150.0	25.0	11.0	.9	0.	0.	390.	0.	0.	.13
D420J2.007	.4	.0	10.7	.0	.02	150.0	.0	11.0	1.0	0.	0.	381.	0.	0.	1.95
D420J2.006	.4	.0	6.4	.0	.02	150.0	-25.0	11.0	1.1	0.	0.	230.	0.	0.	2.20
D420J2.005	.4	.0	8.5	.0	.02	150.0	-50.0	11.0	1.2	0.	0.	304.	0.	0.	1.85
D420J2.004	.3	.0	8.9	.0	.01	150.0	-75.0	11.0	.7	0.	0.	317.	0.	0.	.90
D420J3.009	.0	.0	.0	.0	.00	150.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.18
D420J3.008	.2	.0	5.4	.0	.00	150.0	25.0	11.0	.6	0.	0.	193.	0.	0.	.30
D420J3.007	.4	.0	11.0	.0	.02	150.0	.0	11.0	1.1	0.	0.	392.	0.	0.	2.10
D420J3.006	.5	.0	11.3	.0	.02	150.0	-25.0	11.0	1.3	0.	0.	404.	0.	0.	2.36
D420J3.005	.4	.0	10.0	.0	.02	150.0	-50.0	11.0	1.1	0.	0.	358.	0.	0.	2.16
D420J3.004	.4	.0	10.0	.0	.01	150.0	-75.0	11.0	1.0	0.	0.	357.	0.	0.	.87
D420J4.009	.0	.0	.0	.0	.00	150.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.00
D420J4.008	.2	.0	10.2	.0	.01	150.0	25.0	11.0	.7	0.	0.	366.	0.	0.	.68
D420J4.007	.5	.0	10.4	.0	.02	150.0	.0	11.0	1.3	0.	0.	372.	0.	0.	1.96
D420J4.006	.5	.0	9.2	.0	.02	150.0	-25.0	11.0	1.3	0.	0.	327.	0.	0.	2.27
D420J4.005	.4	.0	9.8	.0	.01	150.0	-50.0	11.0	1.1	0.	0.	350.	0.	0.	1.53
D420J4.004	.4	.0	9.8	.0	.01	150.0	-75.0	11.0	.9	0.	0.	349.	0.	0.	.68

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420J5.009	.0	.0	.0	.0	.00	150.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.00
D420J5.008	.1	.0	.0	.0	.00	150.0	25.0	11.0	.4	0.	0.	0.	0.	0.	.59
D420J5.007	.4	.0	9.3	.0	.02	150.0	.0	11.0	1.1	0.	0.	334.	0.	0.	2.37
D420J5.006	.4	.0	6.6	.0	.02	150.0	-25.0	11.0	1.1	0.	0.	237.	0.	0.	2.17
D420J5.005	.4	.0	8.2	.0	.02	150.0	-50.0	11.0	1.1	0.	0.	292.	0.	0.	2.12
D420J5.004	.4	.0	8.8	.0	.01	150.0	-75.0	11.0	1.0	0.	0.	314.	0.	0.	.91
D420K1.009	.0	.0	.0	.0	.00	150.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.29
D420K1.008	.2	.0	.0	.0	.01	150.0	25.0	17.0	.4	0.	0.	0.	0.	0.	.66
D420K1.007	.3	.0	8.7	.0	.01	150.0	.0	17.0	.8	0.	0.	310.	0.	0.	1.16
D420K1.006	.5	.0	9.2	.0	.01	150.0	-25.0	17.0	1.4	0.	0.	329.	0.	0.	1.08
D420K1.005	.3	.0	9.7	.0	.01	150.0	-50.0	17.0	.9	0.	0.	346.	0.	0.	1.20
D420K1.004	.3	.0	7.9	.0	.01	150.0	-75.0	17.0	.7	0.	0.	282.	0.	0.	.55
D420K2.009	.0	.0	.0	.0	.00	150.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.15
D420K2.008	.1	.0	.0	.0	.00	150.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.13
D420K2.007	.3	.0	8.8	.0	.02	150.0	.0	17.0	.7	0.	0.	315.	0.	0.	1.59
D420K2.006	.4	.0	9.9	.0	.02	150.0	-25.0	17.0	1.0	0.	0.	353.	0.	0.	1.77
D420K2.005	.3	.0	9.1	.0	.01	150.0	-50.0	17.0	.8	0.	0.	324.	0.	0.	1.28
D420K2.004	.4	.0	9.0	.0	.00	150.0	-75.0	17.0	1.0	0.	0.	321.	0.	0.	.31
D420K3.009	.0	.0	.0	.0	.00	150.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.03
D420K3.008	.3	.0	12.8	.0	.00	150.0	25.0	17.0	.7	0.	0.	457.	0.	0.	.15
D420K3.007	.3	.0	9.0	.0	.01	150.0	.0	17.0	.8	0.	0.	322.	0.	0.	1.29
D420K3.006	.4	.0	9.1	.0	.02	150.0	-25.0	17.0	1.2	0.	0.	326.	0.	0.	1.60
D420K3.005	.3	.0	10.1	.0	.01	150.0	-50.0	17.0	.9	0.	0.	361.	0.	0.	1.40
D420K3.004	.3	.0	7.4	.0	.00	150.0	-75.0	17.0	.7	0.	0.	265.	0.	0.	.54
D420K4.009	.0	.0	.0	.0	.00	150.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.03
D420K4.008	.2	.0	.0	.0	.00	150.0	25.0	17.0	.5	0.	0.	0.	0.	0.	.12
D420K4.007	.3	.0	7.5	.0	.01	150.0	.0	17.0	.8	0.	0.	269.	0.	0.	1.21
D420K4.006	.4	.0	10.8	.0	.01	150.0	-25.0	17.0	1.1	0.	0.	385.	0.	0.	1.52
D420K4.005	.4	.0	10.2	.0	.01	150.0	-50.0	17.0	.9	0.	0.	364.	0.	0.	1.02
D420K4.004	.2	.0	7.9	.0	.00	150.0	-75.0	17.0	.6	0.	0.	283.	0.	0.	.29
D420K5.009	.0	.0	.0	.0	.00	150.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.36
D420K5.008	.2	.0	.0	.0	.00	150.0	25.0	17.0	.4	0.	0.	0.	0.	0.	.51
D420K5.007	.4	.0	8.4	.0	.01	150.0	.0	17.0	1.0	0.	0.	302.	0.	0.	1.26
D420K5.006	.4	.0	4.8	.0	.02	150.0	-25.0	17.0	1.0	0.	0.	172.	0.	0.	1.90
D420K5.005	.4	.0	10.1	.0	.02	150.0	-50.0	17.0	1.2	0.	0.	361.	0.	0.	1.59
D420K5.004	.3	.0	5.6	.0	.00	150.0	-75.0	17.0	.7	0.	0.	201.	0.	0.	.53
D420L1.009	.0	.0	.0	.0	.00	250.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.36
D420L1.008	.2	.0	.0	.0	.00	250.0	25.0	1.0	.4	0.	0.	0.	0.	0.	.61
D420L1.007	.3	.0	8.1	.0	.02	250.0	.0	1.0	.7	0.	0.	289.	0.	0.	1.79
D420L1.006	.4	.0	11.2	.0	.02	250.0	-25.0	1.0	1.0	0.	0.	399.	0.	0.	2.09
D420L1.005	.4	.0	11.2	.0	.02	250.0	-50.0	1.0	1.0	0.	0.	402.	0.	0.	2.23
D420L1.004	.3	.0	10.3	.0	.02	250.0	-75.0	1.0	.9	0.	0.	369.	0.	0.	1.96

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	POSITION X (M)	Y (M)	Z (M)	PROTOTYPE CONDITIONS PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420L2.009	.0	.0	.0	.0	.00	250.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.27
D420L2.008	.2	.0	.0	.0	.01	250.0	25.0	1.0	.5	0.	0.	0.	0.	0.	.72
D420L2.007	.4	.0	11.8	.0	.02	250.0	.0	1.0	1.0	0.	0.	422.	0.	0.	2.09
D420L2.006	.3	.0	7.9	.0	.02	250.0	-25.0	1.0	.9	0.	0.	281.	0.	0.	2.32
D420L2.005	.3	.0	9.5	.0	.03	250.0	-50.0	1.0	.9	0.	0.	339.	0.	0.	2.51
D420L2.004	.3	.0	8.6	.0	.03	250.0	-75.0	1.0	.9	0.	0.	307.	0.	0.	2.58
D420L3.009	.0	.0	.0	.0	.00	250.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.13
D420L3.008	.1	.0	.0	.0	.01	250.0	25.0	1.0	.4	0.	0.	0.	0.	0.	.63
D420L3.007	.3	.0	11.1	.0	.02	250.0	.0	1.0	.9	0.	0.	398.	0.	0.	2.08
D420L3.006	.4	.0	9.6	.0	.02	250.0	-25.0	1.0	1.0	0.	0.	343.	0.	0.	2.15
D420L3.005	.4	.0	11.4	.0	.03	250.0	-50.0	1.0	1.1	0.	0.	408.	0.	0.	2.87
D420L3.004	.4	.0	9.8	.0	.02	250.0	-75.0	1.0	1.0	0.	0.	352.	0.	0.	2.41
D420L4.009	.0	.0	.0	.0	.00	250.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.20
D420L4.008	.2	.0	.0	.0	.00	250.0	25.0	1.0	.4	0.	0.	0.	0.	0.	.30
D420L4.007	.3	.0	9.7	.0	.02	250.0	.0	1.0	.8	0.	0.	346.	0.	0.	1.81
D420L4.006	.3	.0	11.2	.0	.02	250.0	-25.0	1.0	.8	0.	0.	401.	0.	0.	2.13
D420L4.005	.4	.0	10.3	.0	.02	250.0	-50.0	1.0	1.0	0.	0.	368.	0.	0.	2.44
D420L4.004	.4	.0	9.8	.0	.02	250.0	-75.0	1.0	1.1	0.	0.	350.	0.	0.	1.96
D420L5.009	.0	.0	.0	.0	.00	250.0	50.0	1.0	.1	0.	0.	0.	0.	0.	.33
D420L5.008	.1	.0	.0	.0	.00	250.0	25.0	1.0	.3	0.	0.	0.	0.	0.	.26
D420L5.007	.3	.0	9.2	.0	.02	250.0	.0	1.0	.8	0.	0.	328.	0.	0.	1.60
D420L5.006	.4	.0	9.3	.0	.03	250.0	-25.0	1.0	1.0	0.	0.	331.	0.	0.	2.51
D420L5.005	.4	.0	9.0	.0	.03	250.0	-50.0	1.0	1.0	0.	0.	320.	0.	0.	2.48
D420L5.004	.4	.0	8.9	.0	.02	250.0	-75.0	1.0	1.0	0.	0.	319.	0.	0.	2.37
D420M1.009	.0	.0	.0	.0	.00	250.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.03
D420M1.008	.2	.0	8.8	.0	.00	250.0	25.0	5.0	.6	0.	0.	316.	0.	0.	.37
D420M1.007	.3	.0	10.3	.0	.02	250.0	.0	5.0	.7	0.	0.	369.	0.	0.	1.64
D420M1.006	.4	.0	10.8	.0	.02	250.0	-25.0	5.0	1.0	0.	0.	388.	0.	0.	2.24
D420M1.005	.3	.0	7.7	.0	.02	250.0	-50.0	5.0	.7	0.	0.	276.	0.	0.	1.99
D420M1.004	.2	.0	9.5	.0	.01	250.0	-75.0	5.0	.7	0.	0.	341.	0.	0.	1.43
D420M2.009	.0	.0	.0	.0	.00	250.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.10
D420M2.008	.2	.0	12.3	.0	.00	250.0	25.0	5.0	.6	0.	0.	438.	0.	0.	.52
D420M2.007	.4	.0	10.5	.0	.02	250.0	.0	5.0	1.0	0.	0.	376.	0.	0.	1.50
D420M2.006	.3	.0	9.2	.0	.02	250.0	-25.0	5.0	.8	0.	0.	329.	0.	0.	1.93
D420M2.005	.3	.0	9.3	.0	.02	250.0	-50.0	5.0	.9	0.	0.	334.	0.	0.	2.08
D420M2.004	.3	.0	8.3	.0	.02	250.0	-75.0	5.0	.9	0.	0.	295.	0.	0.	1.64
D420M3.009	.0	.0	.0	.0	.00	250.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.08
D420M3.008	.3	.0	10.3	.0	.01	250.0	25.0	5.0	.8	0.	0.	368.	0.	0.	.78
D420M3.007	.3	.0	10.2	.0	.02	250.0	.0	5.0	.8	0.	0.	365.	0.	0.	1.87
D420M3.006	.3	.0	10.0	.0	.02	250.0	-25.0	5.0	.8	0.	0.	356.	0.	0.	1.83
D420M3.005	.4	.0	10.5	.0	.02	250.0	-50.0	5.0	1.0	0.	0.	377.	0.	0.	2.42
D420M3.004	.4	.0	11.8	.0	.02	250.0	-75.0	5.0	1.0	0.	0.	422.	0.	0.	1.60

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D420M4.009	.0	.0	.0	.0	.00	250.0	50.0	5.0	.1	0.	0.	0.	0.	0.	.19
D420M4.008	.3	.0	8.4	.0	.00	250.0	25.0	5.0	.8	0.	0.	302.	0.	0.	.48
D420M4.007	.4	.0	11.1	.0	.01	250.0	.0	5.0	1.0	0.	0.	398.	0.	0.	1.54
D420M4.006	.3	.0	10.0	.0	.02	250.0	-25.0	5.0	.9	0.	0.	356.	0.	0.	1.88
D420M4.005	.4	.0	8.1	.0	.02	250.0	-50.0	5.0	1.0	0.	0.	288.	0.	0.	2.22
D420M4.004	.4	.0	10.4	.0	.02	250.0	-75.0	5.0	1.1	0.	0.	370.	0.	0.	1.91
D420M5.009	.0	.0	.0	.0	.00	250.0	50.0	5.0	.0	0.	0.	0.	0.	0.	.00
D420M5.008	.2	.0	8.6	.0	.00	250.0	25.0	5.0	.6	0.	0.	309.	0.	0.	.25
D420M5.007	.3	.0	8.6	.0	.01	250.0	.0	5.0	.7	0.	0.	308.	0.	0.	1.10
D420M5.006	.4	.0	11.8	.0	.02	250.0	-25.0	5.0	1.0	0.	0.	420.	0.	0.	1.92
D420M5.005	.3	.0	9.2	.0	.02	250.0	-50.0	5.0	.9	0.	0.	328.	0.	0.	2.08
D420M5.004	.4	.0	9.9	.0	.02	250.0	-75.0	5.0	1.0	0.	0.	354.	0.	0.	2.00
D420N1.009	.0	.0	.0	.0	.00	250.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.05
D420N1.008	.1	.0	.0	.0	.00	250.0	25.0	11.0	.4	0.	0.	0.	0.	0.	.21
D420N1.007	.3	.0	10.6	.0	.01	250.0	.0	11.0	.8	0.	0.	377.	0.	0.	1.13
D420N1.006	.3	.0	10.9	.0	.02	250.0	-25.0	11.0	.8	0.	0.	389.	0.	0.	1.61
D420N1.005	.3	.0	9.2	.0	.02	250.0	-50.0	11.0	.8	0.	0.	330.	0.	0.	1.59
D420N1.004	.3	.0	8.3	.0	.01	250.0	-75.0	11.0	.7	0.	0.	298.	0.	0.	1.33
D420N2.009	.0	.0	.0	.0	.01	250.0	50.0	11.0	.1	0.	0.	0.	0.	0.	.61
D420N2.008	.3	.0	10.8	.0	.01	250.0	25.0	11.0	.9	0.	0.	385.	0.	0.	.87
D420N2.007	.3	.0	9.6	.0	.01	250.0	.0	11.0	.8	0.	0.	342.	0.	0.	1.46
D420N2.006	.4	.0	8.7	.0	.02	250.0	-25.0	11.0	1.0	0.	0.	311.	0.	0.	2.16
D420N2.005	.3	.0	9.5	.0	.02	250.0	-50.0	11.0	.9	0.	0.	341.	0.	0.	2.12
D420N2.004	.3	.0	7.1	.0	.01	250.0	-75.0	11.0	.8	0.	0.	252.	0.	0.	1.43
D420N3.009	.0	.0	.0	.0	.00	250.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.22
D420N3.008	.2	.0	10.9	.0	.00	250.0	25.0	11.0	.6	0.	0.	389.	0.	0.	.23
D420N3.007	.3	.0	9.7	.0	.01	250.0	.0	11.0	.9	0.	0.	348.	0.	0.	1.20
D420N3.006	.3	.0	7.9	.0	.02	250.0	-25.0	11.0	.9	0.	0.	283.	0.	0.	1.65
D420N3.005	.3	.0	7.7	.0	.02	250.0	-50.0	11.0	.9	0.	0.	274.	0.	0.	1.69
D420N3.004	.3	.0	7.4	.0	.02	250.0	-75.0	11.0	.9	0.	0.	266.	0.	0.	1.63
D420N4.009	.0	.0	.0	.0	.00	250.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.00
D420N4.008	.2	.0	.0	.0	.00	250.0	25.0	11.0	.5	0.	0.	0.	0.	0.	.10
D420N4.007	.4	.0	10.2	.0	.01	250.0	.0	11.0	1.0	0.	0.	364.	0.	0.	1.17
D420N4.006	.4	.0	11.4	.0	.02	250.0	-25.0	11.0	1.1	0.	0.	407.	0.	0.	1.96
D420N4.005	.3	.0	7.0	.0	.02	250.0	-50.0	11.0	.8	0.	0.	250.	0.	0.	1.76
D420N4.004	.3	.0	8.5	.0	.01	250.0	-75.0	11.0	.7	0.	0.	302.	0.	0.	1.38
D420N5.009	.0	.0	.0	.0	.00	250.0	50.0	11.0	.0	0.	0.	0.	0.	0.	.00
D420N5.008	.2	.0	12.1	.0	.00	250.0	25.0	11.0	.5	0.	0.	432.	0.	0.	.39
D420N5.007	.2	.0	6.4	.0	.01	250.0	.0	11.0	.6	0.	0.	230.	0.	0.	1.09
D420N5.006	.4	.0	11.0	.0	.02	250.0	-25.0	11.0	1.0	0.	0.	395.	0.	0.	1.98
D420N5.005	.3	.0	10.7	.0	.02	250.0	-50.0	11.0	.8	0.	0.	382.	0.	0.	1.88
D420N5.004	.3	.0	9.3	.0	.01	250.0	-75.0	11.0	.8	0.	0.	334.	0.	0.	1.04

FALCON 4: LSR = 200, GAS = FREON 12

FILE NAME	MODEL CONDITIONS PEAK CONC. (%)	1% ARR. TIME (SEC)	PEAK TIME (SEC)	1% END TIME (SEC)	SUM (X-S)	PROTOTYPE CONDITIONS POSITION X (M)	Y (M)	Z (M)	PEAK CONC. (%)	5% ARR. TIME (SEC)	10% ARR. TIME (SEC)	PEAK TIME (SEC)	10% END TIME (SEC)	5% END TIME (SEC)	SUM (X-S)
D42001.009	.0	.0	.0	.0	.00	250.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.20
D42001.008	.3	.0	10.7	.0	.00	250.0	25.0	17.0	.8	0.	0.	384.	0.	0.	.34
D42001.007	.3	.0	8.6	.0	.01	250.0	.0	17.0	.7	0.	0.	308.	0.	0.	.90
D42001.006	.3	.0	11.2	.0	.01	250.0	-25.0	17.0	.9	0.	0.	400.	0.	0.	1.15
D42001.005	.3	.0	8.2	.0	.01	250.0	-50.0	17.0	.7	0.	0.	295.	0.	0.	1.31
D42001.004	.3	.0	7.8	.0	.01	250.0	-75.0	17.0	.7	0.	0.	280.	0.	0.	.72
D42002.009	.0	.0	.0	.0	.00	250.0	50.0	17.0	.1	0.	0.	0.	0.	0.	.19
D42002.008	.1	.0	.0	.0	.00	250.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.39
D42002.007	.3	.0	9.2	.0	.01	250.0	.0	17.0	.7	0.	0.	327.	0.	0.	1.00
D42002.006	.3	.0	8.2	.0	.02	250.0	-25.0	17.0	.8	0.	0.	292.	0.	0.	1.58
D42002.005	.3	.0	9.7	.0	.01	250.0	-50.0	17.0	.8	0.	0.	348.	0.	0.	1.27
D42002.004	.4	.0	10.5	.0	.01	250.0	-75.0	17.0	1.0	0.	0.	376.	0.	0.	1.18
D42003.009	.0	.0	.0	.0	.00	250.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.00
D42003.008	.1	.0	.0	.0	.00	250.0	25.0	17.0	.1	0.	0.	0.	0.	0.	.03
D42003.007	.3	.0	10.9	.0	.01	250.0	.0	17.0	.7	0.	0.	391.	0.	0.	.57
D42003.006	.3	.0	8.6	.0	.01	250.0	-25.0	17.0	.7	0.	0.	306.	0.	0.	1.10
D42003.005	.3	.0	9.6	.0	.01	250.0	-50.0	17.0	.8	0.	0.	344.	0.	0.	1.10
D42003.004	.3	.0	7.3	.0	.01	250.0	-75.0	17.0	.7	0.	0.	262.	0.	0.	.77
D42004.009	.0	.0	.0	.0	.00	250.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.02
D42004.008	.2	.0	.0	.0	.00	250.0	25.0	17.0	.4	0.	0.	0.	0.	0.	.14
D42004.007	.3	.0	11.3	.0	.01	250.0	.0	17.0	.7	0.	0.	404.	0.	0.	.85
D42004.006	.3	.0	9.7	.0	.01	250.0	-25.0	17.0	.8	0.	0.	347.	0.	0.	1.29
D42004.005	.3	.0	9.5	.0	.01	250.0	-50.0	17.0	.8	0.	0.	341.	0.	0.	1.44
D42004.004	.3	.0	9.3	.0	.01	250.0	-75.0	17.0	.9	0.	0.	333.	0.	0.	1.13
D42005.009	.0	.0	.0	.0	.00	250.0	50.0	17.0	.0	0.	0.	0.	0.	0.	.00
D42005.008	.1	.0	.0	.0	.00	250.0	25.0	17.0	.3	0.	0.	0.	0.	0.	.20
D42005.007	.2	.0	7.7	.0	.01	250.0	.0	17.0	.6	0.	0.	276.	0.	0.	.78
D42005.006	.3	.0	7.0	.0	.01	250.0	-25.0	17.0	.9	0.	0.	249.	0.	0.	1.27
D42005.005	.3	.0	6.8	.0	.01	250.0	-50.0	17.0	.8	0.	0.	242.	0.	0.	1.22
D42005.004	.3	.0	10.5	.0	.01	250.0	-75.0	17.0	.9	0.	0.	376.	0.	0.	1.06