

1 **Modelling evapotranspiration in a spring wheat from thermal**
2 **radiometry: Crop coefficients and E/T partitioning**

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20 **Abstract**

21 Wheat is one of the crops occupying the largest areas in the world (218 million ha in
22 2013). Understanding the land-atmosphere energy exchanges over these croplands
23 becomes important not only for agronomy but also for climatic and meteorological
24 aspects.

25 This study continues previous work on the estimation of actual evapotranspiration and
26 the assessment of crop coefficients of sorghum, sunflower, or canola. Two variations of
27 a simple two-source energy balance (STSEB) approach were used in combination with
28 land surface temperature measurements to calculate hourly and daily values of surface
29 fluxes and actual evapotranspiration (ET). An experiment was carried out during the
30 spring season of 2014 in Las Tiesas experimental farm in Barrax, Spain. Soil and
31 canopy temperature components together with meteorological variables and biophysical
32 parameters were measured from planting to senescence. Comparison to lysimeter
33 measurements showed calculation errors of $\pm 0.11 \text{ mm h}^{-1}$ and $\pm 0.8 \text{ mm d}^{-1}$ for hourly
34 and daily ET values, respectively, whereas an underestimation no greater than 4%
35 resulted from the entire campaign. Partition between soil and canopy components
36 yielded a ratio of evaporation (E) to transpiration (T) of 36% to 64%, respectively, for
37 the total growing season. Dual crop coefficients were also calculated and compared to
38 those proposed by FAO56.

39 Although separate E and T measurements were not available, similar results between
40 the STSEB and FAO 56 models demonstrate the utility of the STSEB for investigating
41 management strategies aimed at increasing crop water use efficiency.

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43 *Keywords:* Radiometric temperature, evapotranspiration, crop coefficient, two-source
44 energy balance, spring wheat.

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46 **1 Introduction**

47 Better management of water resources becomes critical for sustainable development as
48 a consequence of increasing global water demand and severity of droughts. Nowadays,
49 crop irrigation remains the main source of water consumption. This work focuses on

50 wheat, which is one of the most important crops worldwide, covering a total area of 218
51 million ha in 2013. In the European Union (EU) more than 25 million ha were
52 cultivated in the year 2013 with a production of 143.3 million tons, approximately 20%
53 of world production. Spain is the fifth producing country within the EU, with an area of
54 2.1 million ha and a production of 7.6 million tons (FAO 2014). Wheat area in Spain
55 has increased almost 20% in the past 4 years. Castilla y León is the Spanish region with
56 the largest surface area of wheat (around 780,000 ha), while Castilla- La Mancha holds
57 second place with nearly 320,000 ha (MAGRAMA 2014). In this framework,
58 understanding the land-atmosphere energy exchanges over wheat crop becomes
59 important not only for agronomy but also for climatic and meteorological aspects.

60 The most common approach widely used for calculating the soil water balance and
61 estimating crop water requirement is the FAO-56 method (Allen et al. 1998). According
62 to FAO-56, crop actual evapotranspiration (ET) is estimated by the combination of a
63 reference evapotranspiration (ET_o) and crop coefficients. There are two different FAO-
64 56 approaches: single and dual crop coefficients. The single crop coefficient approach is
65 used to express both plant transpiration and soil evaporation combined into a single crop
66 coefficient (K_c). The dual crop coefficient approach uses two coefficients to separate the
67 respective contribution of plant transpiration (K_{cb}) and soil evaporation (K_e), each by
68 individual values (Allen et al. 1998). This dual crop coefficient technique can improve
69 the accuracy of ET estimation although it requires calibration of the coefficients. This
70 technique has been widely applied and explored under a variety of climatic conditions
71 worldwide (Hunsaker et al. 2005; Williams and Ayars 2005; López-Urrea et al. 2009,
72 2102, 2014; Campos et al. 2010; Howell et al. 2012; Zhang et al. 2013; Ghamarnia et al.
73 2014). All these authors agree that crop coefficient values taken from literature may
74 serve as a starting point for irrigation scheduling, but corrections to these initial values

75 become necessary to adjust to local conditions since considerable errors may occur due
76 to their empirical nature. With this aim, many authors have shown the possibility of
77 using remote sensing measurements to estimate crop water requirements and then
78 improve irrigation scheduling and water productivity. Focusing on wheat, López-Urrea
79 et al. (2009) determined crop coefficient of this crop in the semi-arid climatic conditions
80 of Central Spain, using a weighing lysimeter. These authors showed good agreement
81 with the values proposed by FAO-56 and published by other authors. Gontia and Tiwari
82 (2010) generated monthly crop coefficient maps of wheat croplands in India from
83 vegetation indexes information, and used those to estimate ET maps. Zhao et al. (2013)
84 adopted the dual crop coefficient approach to simulate the soil water balance in winter
85 wheat in the North China Plain (NCP), and tested the SIMDualKc model. Gao et al.
86 (2014) calibrated this model in the same Chinese region with data from a winter wheat
87 but with subsurface drip irrigation. Shahrokhnia and Sepaskhah (2013) used weighing
88 lysimeters to evaluate and calibrate the values proposed by FAO for the daily crop
89 coefficient and ET of wheat in the Fars province, Iran. Yang et al. (2014) used a
90 complementary relationship model coupled with an Evaporative Fraction (EF) approach
91 to estimate ET of winter wheat in the NCP, based on meteorological data and a high
92 resolution IKONOS image. Farg et al. (2012) estimated crop coefficients for wheat in
93 the south Nile Delta of Egypt using vegetation indices derived from SPOT-4 satellite
94 data. Zhang et al. (2015) used MODIS data with an energy-balance ET model (EBEM)
95 to estimate daily evapotranspiration in the NCP, and the results were compared to
96 lysimeter measurements.

97 The combination of two-source energy balance with local radiometric temperatures has
98 been shown to effectively estimate actual evapotranspiration values under a variety of
99 crops and environmental conditions (French et al. 2007; Sánchez et al. 2008, 2011;

100 Colaizzi et al. 2012; Kustas et al. 2012). The main limitation to the operational
101 application of this technique at a regional scale is the retrieval of land surface
102 temperature from satellite data with the sufficient spatial and temporal resolutions;
103 especially in those agricultural areas composed of cropped fields smaller than 1 ha.
104 Nowadays none of the operating satellites offer the combination of spatial and temporal
105 resolution of thermal infrared (TIR) bands needed for these applications. However,
106 significant progress is being made in disaggregation techniques for downscaling
107 information of TIR bands using higher resolution visible/near infrared (VIS/NIR) bands
108 (Agam et al. 2007; Bindhu et al. 2013; Gao et al. 2012). This is expected to bring the
109 opportunity to use some operating satellites such as SPOT, DEIMOS, or FORMOSAT,
110 and others coming soon, such as the promising SENTINEL-2, which do not include TIR
111 bands but will offer high resolution VIS/NIR images (10-20 m). In a recent paper,
112 Sánchez et al. (2014) applied this technique to separate evaporation (E) and
113 transpiration (T) components and those were used to predict dual crop coefficients for
114 sunflower and canola crops. A new experiment was carried out in the spring growing
115 season of 2014 in a wheat field located in a semi-arid region of Central Spain. The
116 methodology and experimental setup were similar to those already described in Sánchez
117 et al. (2014), so the aim of this work is presenting the new results for a wheat crop and
118 reinforcing the potential of thermal infrared measurements as an alternative technique to
119 FAO-56 for the evaluation and partitioning of ET into E and T components. This can be
120 also considered a useful tool for the local adjustment of the FAO-56 crop coefficients.

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125 **2. Materials and methods**

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127 This experiment was carried out in “Las Tiesas” experimental farm (2° 5′W, 39° 3′N,
128 695 m a.s.l) located in the semi-arid, Temperate Mediterranean province of Albacete
129 (Central Spain) from February to June 2014. The study site is a 100 m x 100 m field
130 with a weighing lysimeter (2.7 m long, 2.3 m wide and 1.7 m deep) installed in the
131 center of the plot characterized by a resolution of 0.04 mm equivalent water depth.
132 Weighing lysimeters are presently the most accurate method to measure ET (Howell et
133 al., 1995). The soil is classified as *Petrocalcic Calcixerepts*. Average soil depth of the
134 experimental plot is 40 cm, and is limited by the development of a more or less
135 fragmented petrocalcic horizon. Texture is silty-clay-loam, with 13% sand, 49% silt and
136 38% clay, with a basic pH (8.1). The soil is low in organic matter (1.48%) and nitrogen
137 (0.10%), and has a high content of active limestone (12.5%). For a more comprehensive
138 description of the site and technical features of the lysimeter see López-Urrea et al.
139 (2006) and Sánchez et al. (2011).

140 Wheat (*Triticum aestivum* L. cv. ‘Califa’) was sowed on February 4 in rows 15 cm apart
141 with a seed population of 550 seeds m⁻² (Fig.1). Measurements started on 12 February
142 (DOY 43) and lasted to 30 June (DOY 181). Efforts were made to keep the crop inside
143 the lysimeter at the same growth rate and plant population as the crop outside to
144 minimize edge effects. The whole plot has a permanent sprinkler irrigation system with
145 sprinklers placed on a grid of 15 m x 12.5 m that provide a precipitation rate of 8.6 mm
146 h⁻¹. During the experiment wheat was irrigated, avoiding water stress conditions at
147 anytime. Fractional vegetation cover (P_v), and crop height were measured weekly, and
148 then modeled for the entire experiment, to monitor crop development (Fig. 2). The
149 fractional vegetation cover (P_v) was determined using a supervised classification

150 technique of digital photographic images with the maximum probability algorithm
151 (Calera et al. 2001), in order to assign the current classes of green vegetation and soil in
152 the image, based on the classic methodology for calculating green plant cover
153 developed by Cihlar et al. (1987). Digital photographs acquired weekly over the
154 lysimeter area were always taken at solar noon and vertically from an approximate
155 height of 2 m above ground. Supervised classification of these digital images was later
156 carried out with the help of the ENVI® computer program. Crop height (h) was
157 measured also weekly, in plant samples from three separate areas, as the distance
158 between ground level and the peak of the plant. Best fitting values for both P_v and h
159 data series were used to reproduce their curves for the entire experiment.

160 Three Apogee SI-121 Thermal Infrared Radiometers (IRT) (Apogee Instruments, Logan
161 UT, USA) were used in this experiment. These are broad band thermal instruments (8-
162 14 μm) with an accuracy of ± 0.2 °C, a 18° field of view, and a valid temperature range
163 from -30 to 65°C. One was placed at a height of 2 m over the lysimeter spot, looking at
164 the surface with nadir view and measuring the composite target temperature (T_R). A
165 second radiometer was placed at a height of 20 cm directly pointing to the soil between
166 rows (Fig. 1) to measure soil temperature data (T_s). Canopy temperature (T_c) values
167 were inferred from T_R and T_s , using P_v information, as described in Sánchez et al.
168 (2014). This experimental setup avoids limitations in obtaining T_c using IRTs with a
169 near-horizontal view, especially for low values of P_v .

170 All temperatures were corrected for emissivity and atmospheric effects. At this point,
171 downwelling sky radiance was calculated from sky brightness temperature values
172 measured by a third Apogee radiometer pointing at the sky with an angle of 53°. Values
173 of $\epsilon_c = 0.987 \pm 0.005$ and $\epsilon_s = 0.960 \pm 0.013$ were used for this study (Rubio et al. 2003).

174 Air temperature (T_a) and relative humidity (H_r) were measured using a HMP50 probe
175 (Vaisala Inc., Helsinki, Finland). Wind speed (u) was measured by an anemometer
176 (model A100R, VectorInstruments Ltd., UK). Solar irradiance (S) (model CM14, Kipp
177 & Zonen Delft, Holland) and incoming long-wave radiance (L_{sky}) (model CG2, Kipp &
178 Zonen Delft, Holland) were also measured. Net radiation (R_n) was measured by a NR-
179 Lite sensor (Kipp & Zonen, Delft, The Netherlands) mounted over the lysimeter spot.
180 Soil moisture (SM) was monitored using a capacitance sensor (10HS ECH₂O, Decagon
181 Devices Inc., Pullman, WA) at 10cm depth. All data were stored every 15 min, using a
182 CR-1000 datalogger (Campbell Scientific Inc., Logan, USA), and averaged at hourly
183 scale. Table 1 lists a summary of the mean values of these variables and parameters for
184 the entire experiment.

185 In this work a Simplified version of the Two-Source Energy Balance (STSEB) (Sánchez
186 et al. 2008) was applied to estimate total and separate soil and canopy energy fluxes
187 using the radiometric temperatures, biophysical information, and meteorological data as
188 inputs. A summary of the different equations, parameters and methodological procedure
189 of the STSEB model is included in the Appendix. The reader is referred to Sánchez et
190 al. (2008) and (2011) for a more comprehensive description. This approach was
191 conceived to be applied when the radiometric temperatures of both soil and canopy are
192 known, or at least one of them together with the composite temperature T_R . However,
193 application of STSEB is also possible when only T_R is available, upon the inclusion of
194 some assumptions as part of the approach, for example an initial calculation of canopy
195 transpiration using the Priestley-Taylor equation (Priestley and Taylor, 1972). A scheme
196 of this formulation of the STSEB- T_R model is included in the Appendix. A test of this
197 version of the model (STSEB- T_R) was carried out, and results were compared to the
198 pure STSEB approach.

199 Agreement between modeled and measured values of the surface energy fluxes are
200 analyzed in this paper in terms of the parameters of the linear regression adjustment
201 (slope, intercept and determination coefficient, r^2), the root mean squared error (RMSE),
202 and the mean bias error (MBE) (Willmott 1982).

203

204 **3 Results and discussion**

205 3.1 Comparison between STSEB and STSEB-T_R

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207 Results of the different terms of the energy balance equation were obtained and
208 averaged at an hourly scale, applying both the original STSEB and the modified
209 STSEB-T_R formulations (see Appendix). Figure 3 shows the comparison between the
210 two version outcomes. Differences between the two formulations are negligible in terms
211 of net radiation (R_n) and soil heat fluxes (G), with RMSE values lower than 5 W m^{-2} .
212 Some discrepancies arise in terms of the sensible heat flux (H), with a RMSE= 20 W m^{-2} .
213 This absolute error is maintained in ET estimates. However, the non-water-stressed
214 status of this wheat experiment mask this deviation in ET since H is a minor term
215 compared to R_n under these conditions. Nevertheless, a slight underestimation of ET is
216 observed with the STSEB-T_R approach, more evident for large ET values. These results
217 give confidence to the application of the STSEB-T_R scheme in those scenarios where
218 only the composite target temperature is available and non-water-stressed conditions are
219 prevalent. Further adjustments in the Priestley-Taylor approach would be required under
220 different surface and environmental conditions (Colaizzi et al. 2012).

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222 3.2 Modeled wheat evapotranspiration

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224 An accurate estimate of the net radiation is critical for obtaining accurate LE values.
225 Figure 4a shows the comparison between modeled and observed values of R_n . A RMSE
226 value of $\pm 35 \text{ Wm}^{-2}$, corresponding to an average relative error of $\pm 10\%$ was observed
227 for both the original STSEB and the STSEB- T_R calculations. These results are very
228 close to the value of $\pm 7\%$ obtained in Zhang et al. (2015) over wheat. Colaizzi et al.
229 (2012) applied the original TSEB approach, using separate measurements of T_s and T_c ,
230 to an irrigated cotton crop and observed a very similar RMSE of $\pm 30 \text{ Wm}^{-2}$ in the
231 retrieval of R_n . Very good agreement was observed also by these authors when
232 comparing TSEB and a modified TSEB- T_R formulation (Colaizzi et al. 2012), in terms
233 of R_n estimates.

234 Hourly values of ET, ranging between -0.2 and 1.2 mm h^{-1} , were compared to lysimeter
235 measurements (Fig. 4b). Using the original STSEB model, a root mean square error of
236 $\pm 0.11 \text{ mm h}^{-1}$ was obtained, and the bias was negligible. Similar RMSE= $\pm 0.11 \text{ mm h}^{-1}$,
237 with an underestimation of -0.03 mm h^{-1} and a slightly larger scatter, resulted from the
238 application of the STSEB- T_R approach. These results are an improvement over Sánchez
239 et al. (2011) and (2014), where RMSE values close to $\pm 0.20 \text{ mm h}^{-1}$ for sunflower and
240 canola, and $\pm 0.14 \text{ mm h}^{-1}$ for sorghum, were observed.

241 The original STSEB approach will be used hereafter for the rest of the analysis since, as
242 shown above, it seems to reproduce slightly better results than the STSEB- T_R in this
243 work.

244 The evolution of the daily ET (ET_d) values, modeled and measured, are shown in Fig.
245 5a. Average ET_d value remained below 3 mm d^{-1} until the end of March, peaked $9-10$
246 mm d^{-1} between middle May and middle June and declined afterwards during the grain
247 filling through physiological maturity period. In general, lysimeter ET_d values are well
248 captured by the STSEB model estimates for the entire wheat growing season, except

249 very few days when some rain events occurred and the lysimeter measure had to be
250 recalculated. Following these precipitation events, and very few other weight and
251 calibration verifications, the lysimeter mass data were interpolated using measurements
252 made immediately prior to and immediately following dates that required adjustments.
253 As shown in Figure 5b, discrepancies were within $\pm 1.0 \text{ mm d}^{-1}$ for more than 85% of
254 the dataset.

255 Quantitative analysis of the comparison between modeled and observed daily ET (ET_d)
256 shows an average underestimation of 0.18 mm d^{-1} with a RMSE value of $\pm 0.8 \text{ mm d}^{-1}$,
257 and a determination coefficient (r^2) of 0.903 (Fig. 6). Results are again in agreement
258 with those obtained in Sánchez et al. (2011) and (2014), where RMSE values of ± 1.0
259 mm d^{-1} were observed for sorghum, sunflower and canola, and very close to the
260 $RMSE = \pm 1.1 \text{ mm d}^{-1}$ shown by Colaizzi et al. (2012) in irrigated cotton fields also using
261 weighing lysimeters. These authors pointed out an underestimation of the TSEB early in
262 the season and an overestimation later on, when using direct T_s and T_c measurements.
263 Note that these direct T_c and T_s measurements consider the contribution of the entire
264 canopy and soil, respectively, accounting for sunlit and shaded portions, and this
265 proportion varies with time of day and canopy structure. Also, some experimental
266 limitations arise when measuring T_c using IRTs with near-horizontal view for low
267 vegetation cover conditions (Colaizzi et al. 2012), resulting in an overestimation of the
268 canopy temperature that yields a subsequent underestimation of ET. Colaizzi et al.
269 (2012) postulated that overestimates of E could be due to model assumptions and T_s
270 measurements not accounting for the whole interrow portion. Late season ET
271 overestimates were also reported by French et al. (2007) for wheat, and they attributed
272 this to leaf senescence. This behavior in the discrepancies is not observed in Figure 5b.
273 Focusing on wheat, Zhang et al. (2013) compared ET values predicted by their

274 simulation model with those obtained from eddy-covariance measurements. Values of
275 $RMSE=\pm 0.6 \text{ mm d}^{-1}$ and r^2 of 0.92 were observed by these authors in a winter wheat. A
276 similar error of $RMSE=\pm 0.4 \text{ mm d}^{-1}$, was shown by Gao et al. (2014) as a result of the
277 comparison between simulations by the adjusted dual crop coefficients and results
278 applying a water balance method. Yang et al. (2014) estimated daily ET using the
279 evaporative fraction method coupled with the daily net radiation, with an overall
280 estimation error of $RMSE=\pm 0.7 \text{ mm d}^{-1}$ with a determination coefficient of 0.937. A
281 daily average deviation of $\pm 0.9 \text{ mm d}^{-1}$ was obtained by Zhang et al. (2015) when
282 comparing lysimeter measurements with estimations using an energy balance model
283 together with MODIS data. In one of the very few ground-validated, ET studies at fine
284 spatial scale for wheat, French et al. (2007) used airborne image observations as inputs
285 in the TSEB model to calculate ET with accuracy to within $\pm 1.3 \text{ mm d}^{-1}$ for the full
286 season, when compared to independent soil water depletion observations.
287 The total seasonal evapotranspiration predicted by the STSEB model (500 mm) was less
288 than 4% lower than that measured in the lysimeter (520 mm) (see Fig. 7). Note that this
289 agreement is particularly good for the initial stage ($DOY < 90$), when bare soil and low
290 vegetation coverage conditions are traditionally a challenge for both energy and water
291 balance models (Colaizzi et al. 2012; Shahrokhnia and Sepaskhah 2013).

292

293 3.3 Evaporation/Transpiration partitioning

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295 The E and T values calculated with the STSEB model using data from the present study
296 are shown in Fig. 7.. Soil E was clearly dominant for vegetation cover fractions below
297 0.2 ($DOY < 90$). The ratio T/E increased very fast, and T became the major contribution
298 to ET after then. The total seasonal E resulted in 180 mm, with about half of this

299 amount concentrated before DOY 90. Cumulative T value was 320 mm. This means
300 36% of the seasonal wheat ET corresponds to soil evaporation. This modeled value is in
301 agreement with former studies relative to wheat. López-Urrea et al. (2009) obtained a
302 seasonal evaporation component amounting to 24% (135 mm) of the total ET. Zhang et
303 al. (2013) observed soil evaporation for winter wheat averaged 28% during the full crop
304 season, whereas it represented near 80% for the initial stage and decreased to 5-6%
305 during the mid-season period. Sun et al. (2006) reported 30 to 35% for non-stressed to
306 mild-stressed winter wheat, and Sadras and Rodriguez (2010) reported 22-34% in
307 Australia. Using micro-lysimeters, Shahrokhnia and Sepaskhah (2013) estimated that
308 soil evaporation was about 30% of the total wheat ET. A lower ratio of 19% was
309 obtained for the seasonal E/ET of a winter wheat with a drip irrigation system (Gao et
310 al. 2014). These findings should prompt further field studies of E and T partitioning for
311 different irrigation systems and management strategies.

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313 3.4 Crop coefficients

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315 Figure 8a plots the curve of K_c calculated as the ratio of the lysimeter measured, and
316 STSEB predictions, with the reference evapotranspiration (ET_0) calculated with the
317 FAO-56 Penman-Monteith equation (Allen et al. 1998). K_c values are presented as 5-
318 day averages to avoid the scatter produced by irrigation events. The average K_c data
319 obtained from lysimeter measurements for each stage were: K_{c-ini} : 0.80, K_{c-mid} : 1.18 and
320 K_{c-end} : 0.41, whereas the average K_c values obtained from STSEB calculations were: K_{c-}
321 ini : 0.82, K_{c-mid} : 1.14 and K_{c-end} : 0.59. López-Urrea et al. (2009) reported similar
322 behavior of K_c in a similar experiment over wheat in the same area using also lysimeter
323 measurements. These authors reported wheat K_c values of K_{c-mid} : 1.20 and K_{c-end} : 0.15.

324 The K_{c_mid} matched our measurements, whereas that difference in the K_{c_end} is due to the
325 higher values of evapotranspiration at the end of this growth stage in our measurements,
326 consequence of the relatively high value of $P_v=0.23$ still present in DOY 180. Other
327 authors obtained K_c values of 0.30-0.45 for K_{c_ini} , of 1.10-1.20 for K_{c_mid} , and K_{c_end} in
328 the range of 0.25-0.45 (Gontia and Tiwari 2010; Kjaersgaard et al. 2008; Howell et al.
329 2006; Allen et al. 1998). These K_{c_mid} data are similar to our averaged K_{c_mid} and small
330 variations can be due to differences in: the planting date, lengths of growth stages,
331 wheat varieties, cultural practices and climatic conditions. Differences in the K_{c_ini} and
332 K_{c_end} can be due to the higher values of evaporation during these two stages in our
333 measurements. Shahrokhnia and Sepashkah (2013) estimated values of 0.77, 1.35, and
334 0.26 for K_{c_ini} , K_{c_mid} , and K_{c_end} , respectively. Average K_{c_ini} basically matched our
335 measurements and K_{c_end} was lower than our estimation, whereas our values of K_{c_mid}
336 were lower than those reported by these authors. These discrepancies could be due to
337 different wheat variety and climatic conditions as well as to eventual deviations in the
338 reference ET calculations.

339 As stated by López-Urrea et al. (2009), soil evaporation component (E) can be
340 significant when sprinkler system is used for irrigation or frequent rain events occur.
341 This is the case of our study. Note the high values of K_{c_ini} observed (Fig. 8a) for the
342 initial stage of the wheat growing, with P_v values lower than 0.2.

343 Dual crop coefficients K_e and K_{cb} were calculated as the ratios E/ET_0 and T/ET_0 ,
344 respectively. Figure 8b shows the comparison between results obtained and values
345 proposed by FAO-56, all 5-day averaged. Relatively large values of K_e were obtained
346 for establishment and the beginning of development stages due to frequent irrigations
347 while the vegetation cover was low. During reproduction K_{cb} increased rapidly and
348 peaked to 1.10 during the ripening stage. The average K_{cb} data obtained from STSEB

349 calculations for each stage resulted in: $K_{cb_ini}= 0.05$, $K_{cb_mid}= 1.10$ and $K_{cb_end}= 0.19$.
350 Modeled K_{cb} values were smaller than FAO-56 predictions. In terms of K_e , FAO-56
351 underestimated modeled values, particularly at the initial growth stage. Note that the K_e
352 coefficient is greatly affected by irrigation strategy, soil type, canopy coverage, and
353 local weather conditions.

354 Zhang et al. (2013) estimated initial, mid-season and end K_{cb} values for wheat of 0.25,
355 1.15 and 0.30, respectively. Similar values were obtained by Shahrokhnia and
356 Sepaskhah (2013), ranging between 0.18-0.27, 1.11-1.16, and 0.11-0.14 for initial, mid-,
357 and end-season stages, respectively. Gao et al. (2014) also obtained K_{cb} values ranging
358 0.22-0.27, 1.02-1.10, and 0.25-0.43, for initial mid-, and end-season stages,
359 respectively, in subsurface drip irrigated wheat. All these reported K_{cb_mid} and K_{cb_end}
360 values are in agreement with our estimates, whereas those observed K_{cb_ini} values from
361 previous studies are clearly larger than our predicted average K_{cb_ini} . Differences at this
362 point are likely due to a higher canopy cover during the initial growth stage in the
363 studies reported in the literature.

364

365 **4 Conclusions**

366 Results in this paper reinforce the potential of the techniques based on the combination
367 of surface energy balance with radiometric temperatures for irrigation scheduling or
368 water management under a variety of crops and surface conditions.

369 In this work we focused on a spring wheat crop located in a semiarid region of central
370 Spain. Comparison between model estimates and lysimeter measurements showed a
371 RMSE value of $\pm 0.8 \text{ mm d}^{-1}$, in agreement with previous results using the same
372 technique over sorghum, sunflower or canola. Furthermore, this error is maintained for
373 more than 80% of the 130 days of the experiment duration, and equally for all

374 vegetation cover conditions. Accuracy improves when cumulative ET values are
375 calculated. A deviation no greater than 4% (20 mm) is observed for the prediction of the
376 total 520 mm measured for the full wheat growing season.

377 Partition of ET into E and T components resulted in 36% of the total ET corresponding
378 to the soil evaporation, although most of it was concentrated in the initial phase
379 ($P_v < 0.4$). A proper implementation of the STSEB approach might become a useful tool
380 at this point when facing strategies to increase crop water use efficiency through a
381 feasible monitoring of the soil evaporation/transpiration partitioning.

382 Crop coefficient and dual crop coefficients were also computed. Results are in
383 agreement with those K_c obtained from the lysimeter measurements, and the K_{cb} , and K_e
384 values shown by other authors for wheat. This technique could be used for the local
385 adjustment of the FAO56 K_c values, as an alternative in those fields where weighing
386 lysimeters are not available.

387 The main limitation for the operational application of the energy balance modeling at a
388 crop field scale is the coarse spatial resolution of the thermal data provided by the
389 orbiting satellites. Recent advances in downscaling TIR information from low-medium
390 spatial resolution sensors, using VIS/NIR medium-high spatial resolution sensors, bring
391 the opportunity to the operational application of the technique presented from satellite
392 data. With this aim, a modified STSEB- T_R approach was presented. This version was
393 conceived to be applied using the composite target temperature T_R as the unique
394 radiometric temperature input. Results using this new formulation match those using the
395 original STSEB model, under the conditions of the present study. Further work is
396 required, including evaporation and transpiration measurements under different field
397 and environmental conditions, before extracting any firm conclusion at this point.

398

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401 Competitiveness (projects CGL2013-46862-C2-1/2-P, CGL2011-30433-C02-02, and
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404 logistic support in the instrumentation maintenance of Laura Martinez and Juan A. de la
405 Vara.

406

407 **Appendix.**

408 The original formulation of the Simplified Two-Source Energy Balance model (STSEB)
409 (Sánchez et al. 2008) used the measured temperature of both soil (T_s) and canopy (T_c)
410 components to calculate the different terms of the energy balance equation:

411
$$R_n = H + ET + G \quad (A1)$$

412 where R_n is the net radiation flux ($W m^{-2}$), H is the sensible heat flux ($W m^{-2}$), ET is the
413 latent heat flux ($W m^{-2}$), and G is the soil heat flux ($W m^{-2}$).

414 According to the STSEB approach, the sum of the soil and canopy contributions (values
415 per unit area of component) to the total sensible heat flux, H_s and H_c , respectively, are
416 weighted by their respective partial areas as follows:

417
$$H = P_v H_c + (1 - P_v) H_s \quad (A2)$$

418 where P_v is the vegetation cover fraction at nadir. In equation (A2), H_s and H_c are
419 expressed as:

420
$$H_c = \rho C_p \frac{T_c - T_a}{r_a^h} \quad (A3a)$$

421
$$H_s = \rho C_p \frac{T_s - T_a}{r_a^a + r_a^s} \quad (A3b)$$

422 where ρC_p is the volumetric heat capacity of air ($J K^{-1} m^{-3}$), T_a is the air temperature at a
423 reference height (h), r_a^h is the aerodynamic resistance to heat transfer between the
424 canopy and the reference height at which the atmospheric data are measured ($s m^{-1}$), r_a^a
425 is the aerodynamic resistance to heat transfer between the point $z_{0M}+d$ (z_{0M} : canopy
426 roughness length for momentum, d : displacement height) and the reference height ($s m^{-1}$)

427 ¹), r_a^s is the aerodynamic resistance to heat flow in the boundary layer immediately
 428 above the soil surface ($s\ m^{-1}$). A summary of the expressions to estimate these
 429 resistances can be found in Sánchez et al. (2008). Equations (A3a) and (A3b) are taken
 430 from the parallel configuration of the TSEB model (Norman et al., 1995; Li et al.,
 431 2005), modified to take into account the distinction between r_a^h and r_a^a (Sánchez et al.
 432 2008).

433 The partitioning of the net radiation flux, R_n , between the soil and canopy is proposed as
 434 follows:

$$435 \quad R_n = P_v R_{nc} + (1 - P_v) R_{ns} \quad (A4)$$

436 where R_{nc} and R_{ns} are the contributions (values per unit area of component) of the
 437 canopy and soil, respectively, to the total net radiation flux. They are estimated by
 438 establishing a balance between the long-wave and the short-wave radiation separately
 439 for each component:

$$440 \quad R_{nc} = (1 - \alpha_c)S + \epsilon_c L_{sky} - \epsilon_c \sigma T_c^4 \quad (A5a)$$

$$441 \quad R_{ns} = (1 - \alpha_s)S + \epsilon_s L_{sky} - \epsilon_s \sigma T_s^4 \quad (A5b)$$

442 where S is the solar global radiation ($W\ m^{-2}$), α_s and α_c are soil and canopy albedos,
 443 respectively, σ is the Stefan-Boltzmann constant, and L_{sky} is the incident long-wave
 444 radiation ($W\ m^{-2}$).

445 A similar expression is used to combine the soil and canopy contributions, ET_s and ET_c ,
 446 respectively, to the total latent heat flux:

$$447 \quad ET = P_v ET_c + (1 - P_v) ET_s \quad (A6)$$

448 According to this framework, a complete and independent energy balance between the
 449 atmosphere and each component of the surface is established, from the assumption that
 450 all the fluxes act vertically. In this way, the component fluxes to the total latent heat
 451 flux can be written as:

$$452 \quad ET_c = R_{nc} - H_c \quad (A7a)$$

$$453 \quad ET_s = R_{ns} - H_s - \frac{G}{(1 - P_v)} \quad (A7b)$$

454 Finally, G can be estimated as a fraction (C_G) of the soil contribution to the net radiation
 455 (Choudhury et al. 1987):

$$456 \quad G = C_G (1 - P_v) R_{ns} \quad (A8)$$

457 where C_G can vary in a range of 0.2-0.5 depending on the soil type and moisture. A
 458 value of $C_G=0.35$ was used in this work.

459 When the composed target temperature (T_R) is the only measurement available, the
460 original formulation of the STSEB needs the inclusion of additional assumptions to
461 calculate, for example, an initial estimate of canopy latent heat flux. In this STSEB- T_R
462 approach, the Priestley-Taylor equation was used:

$$463 \quad ET_c = f_g \alpha \left[\frac{\Delta}{\Delta + \gamma} \right] R_{nc} \quad (A9)$$

464 where f_g is the fraction of the vegetation that is green, Δ is the slope of the water vapour
465 saturation curve, α is the Priestley-Taylor (PT) parameter (Priestley and Taylor, 1972),
466 and γ is the psychrometric constant. A value of $\alpha=1.26$ was assumed in this study,
467 according to the non-water-stressed conditions over this wheat field (French et al.
468 2007). Note that this value might need adjustment under water-stressed conditions.

469 An initial value of T_c is extracted by solving the equation resulting from the
470 combination of (A5a), (A7a), and (A9). Then, the corresponding value of T_s can be
471 calculated from the equation (Sánchez et al. 2008):

$$472 \quad \epsilon T_R^4 = P_v \epsilon_c T_c^4 + (1 - P_v) \epsilon_s T_s^4 \quad (A10)$$

473 where ϵ_c , and ϵ_s , are the canopy and soil emissivities, respectively, ϵ is the effective
474 surface emissivity. Once T_c and T_s values are estimated, equations (A2)-(A8) can be
475 applied.

476

477

478 **Conflicts of interest**

479 The authors declare no conflict of interest

480

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612 Table 1. Mean values of the meteorological variables: air temperature (T_a), relative
613 humidity (H_r), wind speed (u), solar irradiance (S), reference evapotranspiration
614 (ET_0), soil moisture at -10 cm (SM), and cumulated precipitation ($Prec.$) and
615 irrigation ($Irr.$), at the wheat plot for the entire experiment.

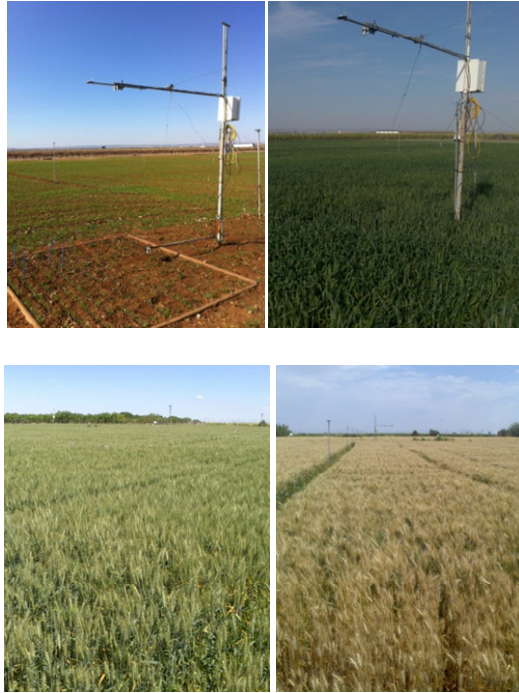
	T_a	H_r	u	S	SM	$Prec.$	$Irr.$	ET_0
	(°C)	(%)	($m\ s^{-1}$)	($W\ m^{-2}$)	($m^3\ m^{-3}$)	(mm)	(mm)	($mm\ d^{-1}$)
February*	7.3	60	4.2	134	0.28	8	16	1.9
March	8.8	66	3.9	196	0.28	2	70	2.9
April	13.8	69	3.0	255	0.27	37	46	4.2
May	15.9	60	2.6	302	0.28	5	183	5.3
June	20.1	59	2.4	305	0.25	43	119	5.6

616 * Starting 12 February.

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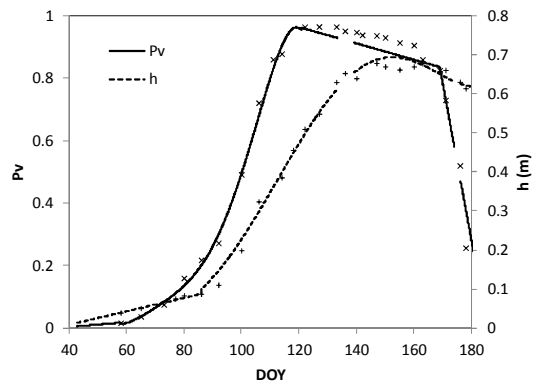
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621 **Fig. 1** Experimental setup over the lysimeter for DOYs 55 and 129 (top), and view of
 622 the wheat field conditions for DOYs 153 and 174 (bottom)

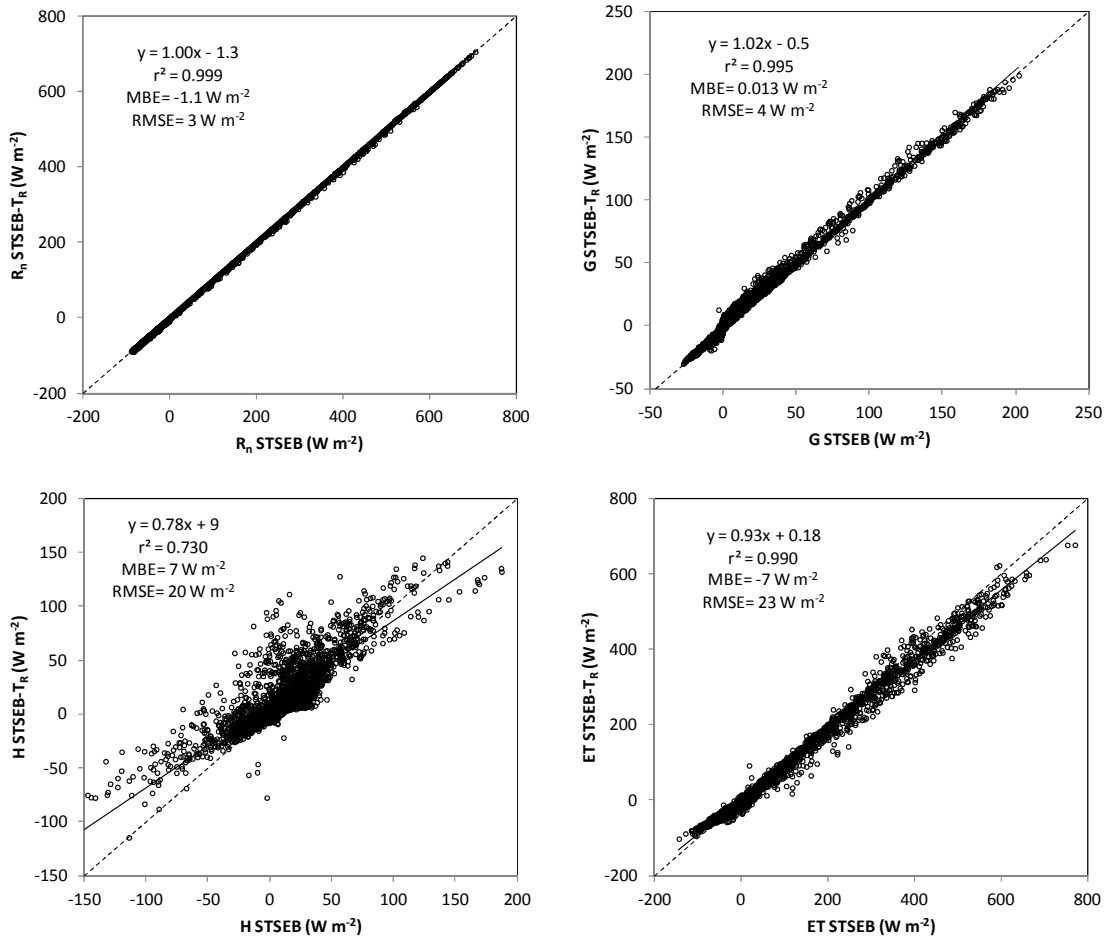
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625 **Fig. 2** The 2014 wheat season phenology showing fractional vegetation cover (P_v) and
 626 the canopy height (h). Marks correspond to measured values and lines represent
 627 modeled behavior

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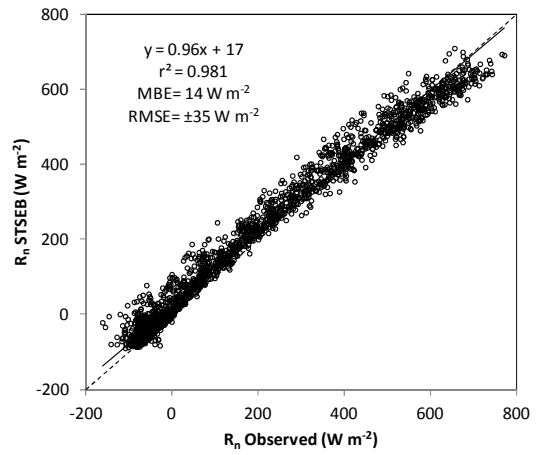
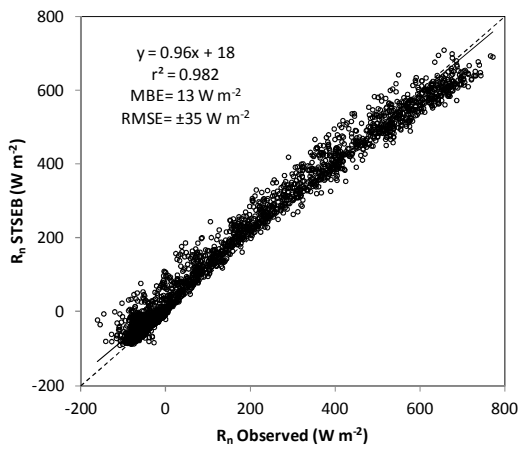
630 **Fig. 3** Comparison of hourly estimates of the different terms of the surface energy
 631 balance (R_n, G, H, and ET), using the original STSEB approach and the modified
 632 STSEB-T_R formulation.

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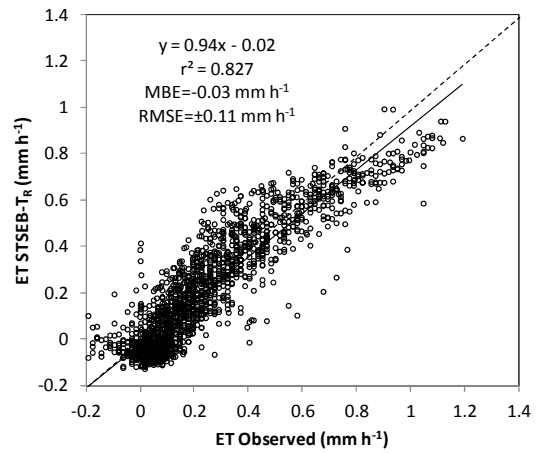
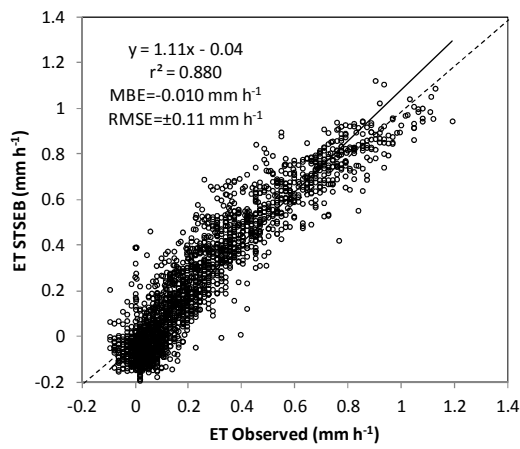
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(a)

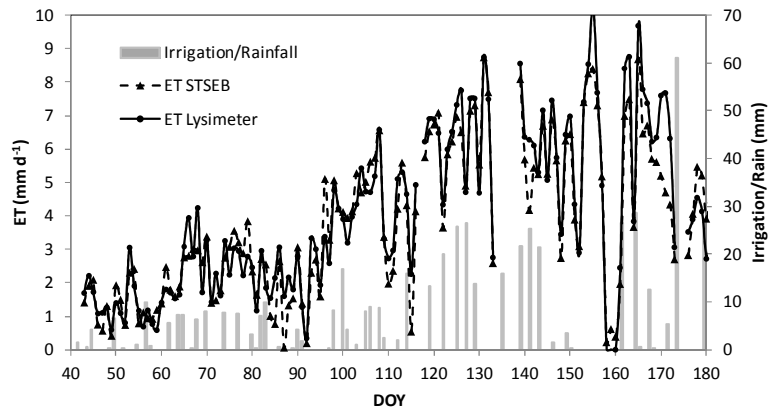


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(b)

641 **Fig. 4** Calculated vs. ground-measured hourly variables using the original STSEB
 642 approach and the modified STSEB- T_R formulation: (a) net radiation, (b)
 643 evapotranspiration

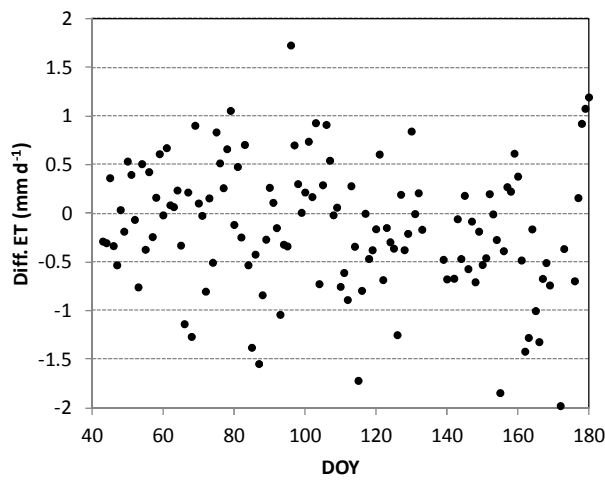
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(a)



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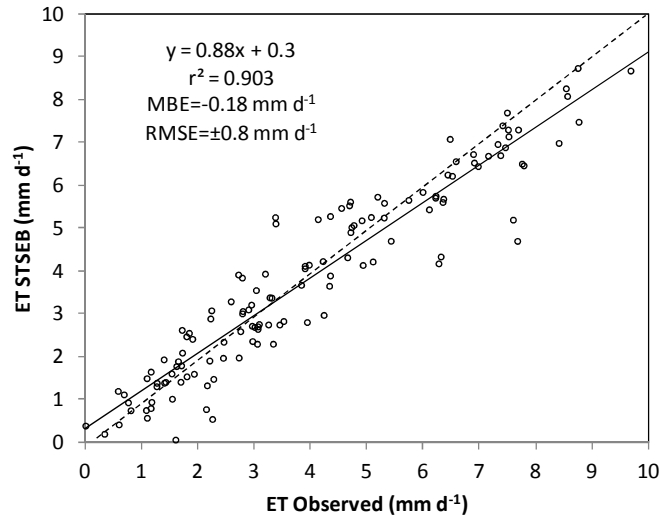
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(b)

652 **Fig. 5** (a) Evolution of modeled and observed daily ET values for the wheat season.
 653 Irrigation and rainfall amounts are also included. (b) Daily ET discrepancy (modeled
 654 ET- observed ET) over the growing season

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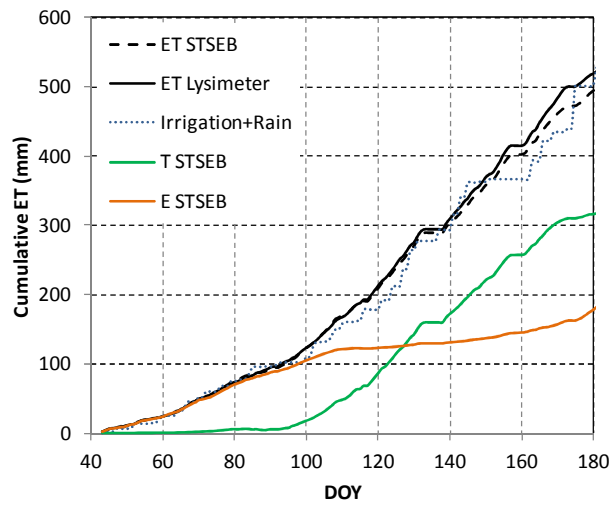


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659 **Fig. 6** Comparison of daily ET estimates with lysimeter measurements

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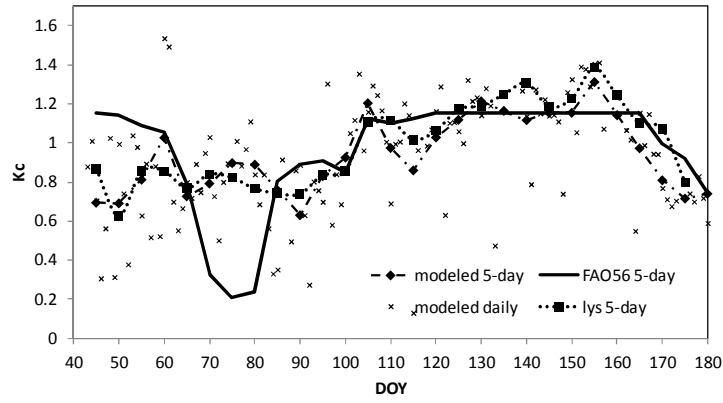
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663 **Fig. 7** Cumulative values of predicted ET, E, and T values, for the whole wheat season,
 664 together with observed ET and irrigation+rain amount

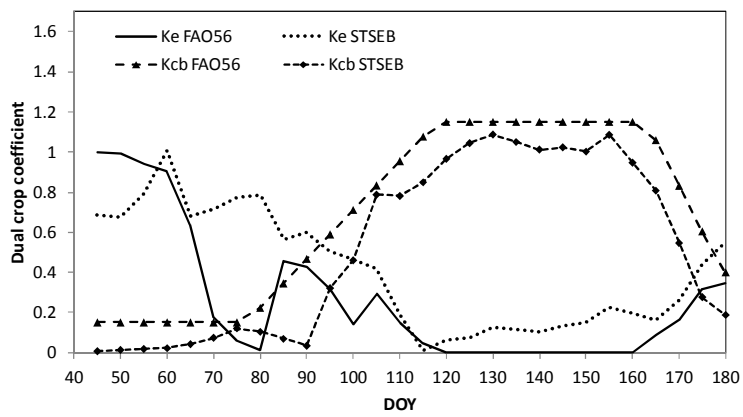
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(a)



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(b)

671 **Fig. 8** Comparison of modeled values of crop coefficients with those calculated from
672 lysimeter measurements and proposed by FAO56: (a) K_c , (b) K_e and K_{cb}

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