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# The ATLAS-SPT Radio Survey of Cluster Galaxies

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The work presented in this thesis is, to the best of my knowledge and belief, original except as acknowledged in the text.

I hereby declare that I have not submitted this material, either in full or in part, for a degree at this or any other institution.

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Andrew Nicholas O'Brien February 05, 2019

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# Abstract

Galaxy clusters are the largest gravitationally bound objects in the Universe. The study of galaxy clusters can give insights into the large-scale structure of the Universe and provide constraints on the cosmological parameters that dictate the evolution of the Universe. Bent-tail radio sources are a class of Active Galactic Nuclei (AGN) where the jets or lobes have been distorted significantly due to the relative movement through a dense medium. This behaviour is expected to occur in galaxy clusters, especially those of high mass.

I have planned and carried out the observations for the ATLAS-SPT survey, a radio continuum survey of  $\sim 86 \text{ deg}^2$  using the Australia Telescope Compact Array at a central observing frequency of 2.1 GHz over a bandwidth of 2 GHz, with the telescope in an extended array configuration with a maximum baseline length of 6 km.

The calibrated dataset was imaged, deconvolved using a multi-frequency deconvolution algorithm, and corrected for wide-bandwidth primary beam effects to produce total intensity and spectral variation images for each pointing. The limited  $u, v$  coverage of the survey caused several imaging challenges; the most significant being a poorly behaved synthesised beam response pattern and sidelobes from moderately bright outlier sources producing image artefacts. I devised an imaging pipeline which minimised the outlier source artefacts by employing a two-stage imaging process: 1) each pointing was imaged well beyond the primary beam with a coarse pixel resolution to find bright outlying sources; 2) outlying sources with a brightness expected to produce a synthesised beam pattern above the thermal noise of the pointing were modelled and subtracted from the pointing dataset. After subtracting the outlying sources, imaging could proceed as normal.

Once each pointing was imaged, they were convolved with a Gaussian to produce a common angular resolution of  $8''$  and linearly mosaicked to produce two images of the entire field: one total intensity mosaic and a spectral index mosaic. Due to limitations in the mosaicking software, 9 overlapping mosaic tiles were produced and subsequently combined with a custom imaging script. The final combined total intensity mosaic contains approximately  $43\,000 \times 40\,000$  px and has a median rms noise level of approximately  $180 \mu\text{Jy}$ .



I have produced a radio source catalogue containing positions and flux densities of 6067 sources. 722 of these sources have sufficient signal-to-noise ratios to provide a reliable spectral index measurement which is also included in the catalogue. I conducted a completeness simulation which indicates that the catalogue is 100% complete at the  $1.3 \text{ mJy beam}^{-1}$  flux density level. This simulation was also used to estimate the flux density and positional accuracies. Due to noise fluctuations, flux densities of the faintest catalogued sources ( $\sim 0.36 \text{ mJy beam}^{-1}$ ) are boosted by  $\sim 30\%$ , and the boosting level falls below 5% for sources  $\geq 0.74 \text{ mJy beam}^{-1}$ . The extracted positions have a median offset of  $\ll 1''$  from their simulated input positions with a standard deviation of  $\sigma = 1.6''$  for the faintest sources, improving to  $\sigma = 0.5''$  for sources with flux densities  $\geq 1.3 \text{ mJy beam}^{-1}$ . The catalogue was also matched and compared with the ATCA-XXL survey which covered the inner  $25 \text{ deg}^2$  of the field to a greater sensitivity. The matched sources are shown to be in excellent flux density and positional agreement.

I constructed a Euclidean-normalised differential source count using the ATLAS-SPT catalogue, incorporating the necessary flux density corrections from the completeness simulation. The source counts agree well with others from the literature. The result confirms that the ATLAS-SPT survey is most sensitive to AGN and the steepening of the source counts clearly show the evolution of these sources. The source counts toward the catalogue sensitivity limit show the characteristic flattening, indicating the increased population of star-forming galaxies at those flux densities.

I have identified 50 bent-tail radio galaxy candidates from the ATLAS-SPT total intensity mosaic by visual inspection and cross-matched these sources with the deep  $3.6 \mu\text{m}$  *Spitzer*–South Pole Telescope Deep Field (SSDF) catalogue of the field. I then cross-matched the SSDF sources to both the Blanco Cosmology Survey (BCS) and Dark Energy Survey (DES) Science Verification catalogues and provide photometric redshift estimates for 17 bent-tail candidates. I then cross-matched these bent-tail candidates with redshifts to known cluster catalogues (546 in total). I found that only 4 are associated with known clusters. Recent models when applied to this dataset predict that  $\sim 7$  bent-tail sources should be associated with high-mass ( $M \geq 10^{15} M_{\odot}$ ) clusters such as those from the SPT SZ cluster catalogue. Instead I find only one. The lack of bent-tail sources within clusters may be explained by various effects such as projection, resolution, and AGN duty cycle. However, the lack of clusters found around bent-tail sources is more problematic and suggests that bent-tails may reside in cluster of lower mass than expected.

# List of Abbreviations

<b>AGN</b>	Active Galactic Nuclei
<b>ASKAP</b>	Australian Square Kilometre Array Pathfinder
<b>ATCA</b>	Australia Telescope Compact Array
<b>ATLAS</b>	Australia Telescope Large Area Survey
<b>ATNF</b>	Australia Telescope National Facility
<b>BCS</b>	Blanco Cosmology Survey
<b>CABB</b>	Compact Array Broad-band Backend
<b>CDFS</b>	<i>Chandra</i> Deep Field South
<b>CMB</b>	Cosmic Microwave Background
<b>CSIRO</b>	Australian Commonwealth Scientific and Industrial Research Organisation
<b>DES</b>	Dark Energy Survey
<b>EMU</b>	Evolutionary Map of the Universe
<b>FIRST</b>	Faint Images of the Radio Sky at Twenty centimetres
<b>FWHM</b>	full width at half maximum
<b>ICM</b>	intra-cluster medium
<b>IRAC</b>	Infrared Array Camera
<b>NVSS</b>	NRAO VLA Sky Survey
<b>OTF</b>	on-the-fly
<b>PSF</b>	point spread function
<b>PyBDSF</b>	Python Blob Detector and Source Finder

<b>RCS1</b>	first Red-Sequence Cluster Survey
<b>RFI</b>	Radio Frequency Interference
<b>SDSS</b>	Sloan Digital Sky Survey
<b>SNR</b>	signal-to-noise ratio
<b>SPIRE</b>	Spectral and Photometric Imaging Receiver
<b>SPT</b>	South Pole Telescope
<b>SSDF</b>	<i>Spitzer</i> –South Pole Telescope Deep Field
<b>SUMSS</b>	Sydney University Molonglo Sky Survey
<b>SWIRE</b>	<i>Spitzer</i> Wide-area InfraRed Extragalactic Survey
<b>SZ</b>	Sunyaev-Zel’dovich
<b>TAC</b>	Time Allocation Committee
<b>ToO</b>	Target of Opportunity
<b>VLA</b>	Very Large Array
<b>XMM</b>	X-ray Multi-Mirror Mission

# Chapter 1

## Introduction

### 1.1 Galaxy Clusters

Comprised of tens to thousands of galaxies, galaxy clusters are the largest gravitationally bound objects in the Universe. They form at intersections of sheets and filaments of the large-scale structure of the Universe where the dark matter is most concentrated. As well as containing galaxies, clusters also contain a cloud of diffuse superheated plasma often referred to as the intra-cluster medium (ICM), as well as concentrations of dark matter which make up most of their mass. The large-scale structure of clusters evolves very slowly over cosmic time, making them relics of the conditions of the early Universe. Therefore, studying galaxy clusters reveals important information on the history of galaxy and structure formation in dense environments. When studied over a range of cosmological distances, cluster studies can reveal the evolutionary timeline of the cosmos and explore the impact of environments of galaxy evolution.

The ICM is typically heated to between 10 to 100 MK. At these temperatures, the gas is ionised and free-moving electrons are decelerated as they pass other charged particles. This deceleration produces a photon in a process called *bremstrahlung*. The energy of the photon is proportional to the temperature of the plasma  $h\nu \sim kT$ , which for an ICM is within the X-ray regime.

Clusters can be detected at several wavelengths using various methods. Traditionally, X-ray observations of thermal emission from the ICM (Rosati et al., 1998; Romer et al., 2001; Pierre et al., 2004), or optical identifications of galaxies within the same proximity that also occupy the same colour-space (Gladders and Yee, 2005; Kodama et al., 2007; Wilson et al., 2008) have been used. Both of these methods are instrumentally limited to small areas or bright objects and are therefore biased to nearby clusters. The SZ effect is another method of cluster detection (described in Section 1.3) which is distance independent, however it may still be biased toward

high-mass clusters.

Radio observations have proved to be a valuable complementary means of detecting galaxy clusters (Blanton et al., 2000, 2003; Mao et al., 2009, 2010; Wing and Blanton, 2011; Norris et al., 2013; Dehghan et al., 2014). The ICM is detectable at radio wavelengths as diffuse synchrotron radiation; emission caused by the acceleration of relativistic charged particles due to magnetic fields. This shows that not only is the ICM a turbulent flurry of hot gases, but there exist magnetic fields and non-thermal relativistic particles. Furthermore, shocks produced by cluster-cluster mergers propagating through the ICM re-accelerate charged particles which emit diffuse radio emission along the cluster periphery. This emission, called a radio relic, is typically irregular and elongated along the shock front.

## 1.2 Bent-tail Radio Sources

In addition to the diffuse emission mechanisms mentioned in Section 1.1, radio observations are also able to detect galaxy clusters via the distortions of the relativistic jets from AGN (Blanton et al., 2000; Belsole et al., 2007; Venturi et al., 2007). The relative movement between the AGN hosts and ICM can cause the jets to become misaligned from their usual trajectory and bend in the direction of the ICM movement (Mao et al., 2010) much like a flag waving in the wind. In some cases, the distortions are so extreme that the jets curl backward and the radio galaxy appears to only have a single jet (until observations with sufficient resolution are able to resolve the individual jets). This method of cluster detection is unique in that it is able to detect clusters out to much greater distances than optical or X-ray, due to the sensitivity and resolution of modern radio interferometers (see Section 1.4). Additionally, since the detection is purely the synchrotron emission from AGN, it is free from dimming effects such as dust extinction which plagues observations at other wavelengths.

Since clusters have an increased probability of hosting radio sources (Burns et al., 1981; Valentijn and Bijleveld, 1983; Burns, 1990), using bent-lobe radio galaxies as a method of finding clusters could reveal high-redshift<sup>1</sup> clusters without the requirement for extremely deep observations. Using radio data from the Faint Images of the Radio Sky at Twenty centimetres (FIRST) survey (Becker et al., 1995) with optical data from the fourth data release of the Sloan Digital Sky Survey (SDSS) (Adelman-McCarthy et al., 2006), Wing and Blanton (2011) showed that extended, multicomponent radio sources are more often associated with clusters than single component sources (where a component is one part of the radio emission that can be adequately modelled with a 2D Gaussian; a point source is modelled with a single component).

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<sup>1</sup>In the context of this work, high-redshift sources are those beyond the typical detection limits of optical surveys, i.e.  $z > 0.5$ .

Bent-lobed radio sources were also found more often in clusters than sources with straight lobes.

Detections of radio haloes and relics require sensitive, short-baseline interferometric observations whereas detecting bent-tail sources require high spatial resolution to resolve the extended jets and lobes.

### 1.3 The Sunyaev-Zel'dovich Effect

The Sunyaev-Zel'dovich effect is an astrophysical phenomenon whereby photons from the Cosmic Microwave Background (CMB) are boosted to higher energies as they pass through an ICM in a form of inverse Compton scattering. As the CMB photons pass through the plasma, the energetic electrons in the gas collide with the photons resulting in a transference of energy from the electron to the photon. The increase in energy of the photon equates to an increased frequency and thus a shorter wavelength. This slight change in frequency (spectral shift) is detectable over the area of the ICM as an increase in intensity of higher frequency photons and a consequent decrease in intensity of lower frequency photons. An exaggerated model of the spectral shift and an example of an SZ effect detection are shown in Figure 1.1.

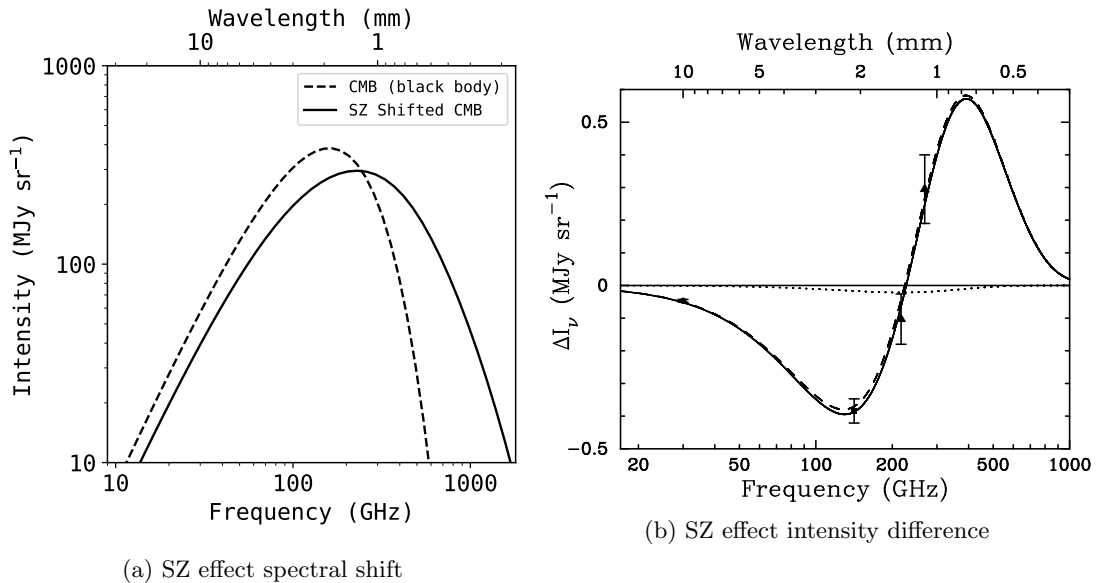


Figure 1.1: (a) An exaggerated model of the spectral shift of the CMB caused by the SZ effect. The expected CMB spectrum is plotted as a dashed line, and the observed shifted spectrum as the solid line. This plot represents the SZ effect that would be observed if the CMB photons passed through a medium 1000 times more massive than the average cluster. Figure by the author. (b) The difference in intensity observed with the SZ effect when compared to the expected CMB intensity. There is a noticeable decrease in intensity of lower frequency photons, and an increase in higher frequency photons. Figure from Carlstrom et al. (2002).

The amplitude of the distorted spectra caused by the SZ effect is proportional to the integrated electron pressure along the line of sight. Therefore, the SZ flux is a measurement of the total thermal energy of the ICM the CMB is passing through. This in turn is a robust

indicator of the mass of the cluster (Barbosa et al., 1995; Holder et al., 2001; Motl et al., 2005). Consequently, SZ surveys may be biased toward more massive clusters as their SZ signals are more easily detectable.

Since the SZ effect is the scattering of CMB photons and the CMB energy density increases with redshift, cosmic dimming effects are cancelled out. This results in the surface brightness of the SZ effect being nearly redshift independent, meaning that high redshift clusters are no more difficult to detect than those at low redshift. However, Lin et al. (2009) showed that SZ surveys may miss clusters that contain strong radio sources at high frequencies due to contamination of the SZ signal. This, combined with the tendency for high redshift clusters to contain AGN (Krick et al., 2009; Martini et al., 2009) predicts a possible bias toward lower redshift clusters in SZ surveys. A counter argument to this is presented by Gralla et al. (2011): they find no evolution in the radio source populations in FIRST that lie within clusters from the first Red-Sequence Cluster Survey (RCS1), meaning that the forecasted point source contamination of low-mass clusters at high redshift in SZ surveys is likely not as severe as originally predicted.

### 1.3.1 The South Pole Telescope (SPT)

The SPT, located in Antarctica, is a millimetre-wavelength radio telescope which has conducted a 2500 deg<sup>2</sup> survey of the Southern sky at 95, 150 and 220 GHz at  $\sim 1'$  resolution. These observing bands make it perfect for SZ effect detections. A 100 deg<sup>2</sup> subsection of this observation area, called the SPT deep field, was observed to a depth of  $\sqrt{2}$  (and eventually 3) times the rest of the field, approximately an rms of 37, 12 and 35  $\mu\text{K arcmin}^2$  at 95, 150 and 220 GHz, respectively. To date, this is the deepest millimetre-wavelength study of the sky, making this field truly unique.

The SPT deep field is among the largest and most intensely studied fields in the sky with extensive multi-wavelength coverage. Using the deep millimetre-wavelength data, the SPT deep field has yielded the best and most well characterised SZ selected galaxy cluster catalogue (Bleem et al., 2015b); has the deepest CMB weak lensing map in existence (Story et al., 2015); and is covered by large contiguous *Herschel*/Spectral and Photometric Imaging Receiver (SPIRE) (Holder et al., 2013), *Spitzer*/Infrared Array Camera (IRAC) (Ashby et al., 2014), and X-ray Multi-Mirror Mission (*XMM*) (Pierre et al., 2016) surveys. There exists optical photometry data for an area of  $\sim 35$  deg<sup>2</sup> within the field completed by the BCS (Bleem et al., 2015a; Desai et al., 2012). Additionally, the field was prioritised for the ongoing DES which has now released deep optical photometry for the entire area (Dark Energy Survey Collaboration et al., 2018). These data were publicly released shortly before this thesis was submitted and

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<sup>2</sup>The SPT maps are in units of CMB fluctuation temperature.

thus the analysis in Chapter 4 which makes use of the DES data uses an earlier subset of Dark Energy Survey Collaboration et al. (2018) release (see Section 4.2.4.2).

## 1.4 Radio Telescopes

Our knowledge about astrophysical processes is based on observations of the electromagnetic radiation they emit. A typical black-body source of radiation (one that absorbs all incoming radiation) radiates in all directions across all frequencies. The total luminosity  $L$  of such an object is a measurement of its total energy output per second in Watts (W). Since it is impossible to directly measure the total luminosity (as it would require an instrument that entirely encompasses the object and can measure all frequencies), telescopes measure the emission over a finite collecting area across a finite frequency range. This results in measuring the object flux  $S$ , which is the rate at which energy is detected over an area perpendicular to the direction of propagation. As this measurement occurs over a finite bandwidth it is expressed in units of flux per unit bandwidth  $S_\nu$ , called flux density. When integrated over the receiving bandwidth, the flux density is equal to the total observed flux i.e.  $S = \int S_\nu d\nu$ . Flux density is expressed in SI units as  $\text{W m}^{-2} \text{Hz}^{-1}$ , but due to the extremely low power of most astronomical radio emission the unit of Jansky (Jy) is typically used which is defined as  $1 \text{ Jy} = 1 \times 10^{-26} \text{ W m}^{-2} \text{Hz}^{-1}$ .

The electromagnetic radiation emitted by astrophysical processes are received on Earth and measured using instruments dependant on the frequency of radiation being observed. Radio telescopes differ from other telescopes as their observing frequency  $\nu$  is relatively low and so according to the Planck relation  $E = h\nu$ , radio photons have very little energy. The low energies of radio photons means that conventional telescopes which use methods such as photon counting with specialised detectors are not practical. Instead, radio telescopes make use of conductive antennas to intercept radio waves whose electric field oscillations induce voltage oscillations inside the antennas. These oscillations are then converted to a digital signal for processing.

Although all radio telescopes use antennas as a means for capturing the radio waves, the telescope design still varies greatly depending on the wavelength being observed. For centimetre wavelengths (the target wavelength used in this thesis) a paraboloid dish is usually used to collect incoming radio-frequency radiation and focus them into the radio receiver. Paraboloid dishes are used for their large effective area and ability to focus the incoming wavefronts without changing their path lengths, thus keeping the waves in phase. Both the sensitivity and resolution of the telescope improve proportionally with the size of the effective area of the dish.

As with optical telescopes, the use of a reflector introduces a diffraction pattern called an Airy disc which characterises the telescope response across the area of the dish assuming that



the incoming signal strength is uniform across the collecting area. This pattern consists of a main response in the centre followed by a series of concentric rings called sidelobes, each with decreasing intensity. This pattern dictates the resolution of the instrument, or more specifically, the minimum angular separation between two sources which can be resolved as distinct sources. Formally, the angular separation limit is defined by

$$\theta = 1.22 \frac{\lambda}{D}$$

where  $D$  is the diameter of the aperture. Additionally, the resolution of the telescope is often quoted as the full width at half maximum (FWHM) of the response pattern, approximately equal to

$$\theta_{\text{FWHM}} \approx 1.02 \frac{\lambda}{D}$$

Since the resolution of the telescope is dependant on the diameter of the aperture, it is desired to increase  $D$  to produce the highest resolution possible. However, this simultaneously decreases the field of view. In order to satisfy the conflicting requirements of high resolution and a large field of view, many single dishes are combined to form an interferometer.

### 1.4.1 Interferometers

Interferometry is the practice of superimposing electromagnetic waves in order to produce an interference pattern which can then be analysed. In radio astronomy, this technique involves correlating (multiplying and averaging) the signals from several radio telescopes in order to produce a signal with far greater resolution. The individual dishes are usually correlated in pairs with the distance between any two elements referred to as a baseline and represented by the vector  $\vec{b}$ . A simple two-element interferometer is shown in Figure 1.2. Note the output  $R$  of a two-element interferometer has much more intense sidelobes than the single-dish diffraction pattern mentioned in Section 1.4.

To improve the instrument response, more dishes can be added to the interferometer and their effect is illustrated in Figure 1.3. This shows that the synthesised beam of an interferometer (in this context, often called a telescope array) has a resolution of approximately  $\lambda/b$ , where  $b$  is the maximum baseline length. This enables extremely high resolution radio telescopes to be built using multiple smaller dishes over a large area.

The coordinate system of the correlator output  $R$  is three-dimensional and rectilinear expressed as quantities  $(u, v, w)$  in units of the observed wavelength, often called a visibility. The direction of  $w$  is set to the direction of observation (i.e. the unit vector  $\hat{s}$ ) and  $(u, v)$  are perpendicular to  $w$  with  $u$  being the projected easterly direction and  $v$  to the north. One typically

can ignore the  $w$  coordinate as it is set to 0 since  $\hat{s}$  is perpendicular to  $(u, v)$  (this is not the case for more complex interferometers). Radio astronomers commonly refer to this coordinate space as the  $u, v$  plane. Using the Van Cittert-Zernike theorem, a visibility  $V$  can be expressed in terms of the sky emission  $T$

$$V(u, v) = \iint T(l, m) e^{-i2\pi(ul+vm)} dl dm$$

where  $(l, m)$  are coordinates on a plane tangent to the sky. Since  $e^{ix} = \cos x + i \sin x$ , this integral can be simplified as a two-dimensional Fourier transform:

$$V(u, v) \xrightarrow{\mathcal{F}} T(l, m)$$

This unique property of radio interferometers allows astronomers to create sky brightness maps

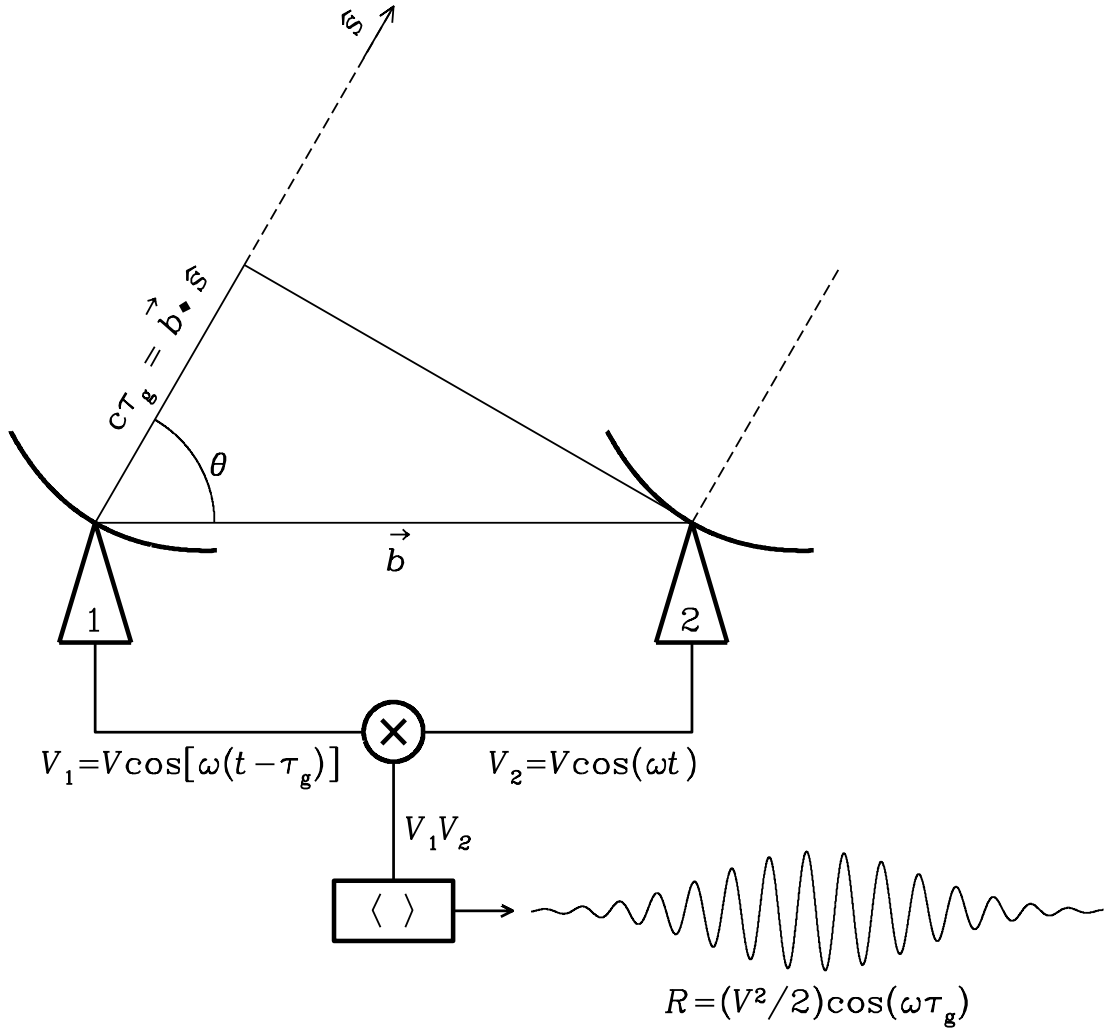


Figure 1.2: A simple two-element interferometer with baseline vector  $\vec{b}$  intercepting planar waves perpendicular to the the unit vector  $\hat{s}$  over a narrow frequency range centred at  $\nu = \omega/2\pi$ . The two antennae voltage outputs  $V_1$  and  $V_2$  have equal amplitudes but are offset by the geometric delay  $\tau_g$ .  $V_1$  and  $V_2$  are correlated to produce  $R$ . Image taken from Condon and Ransom (2016).

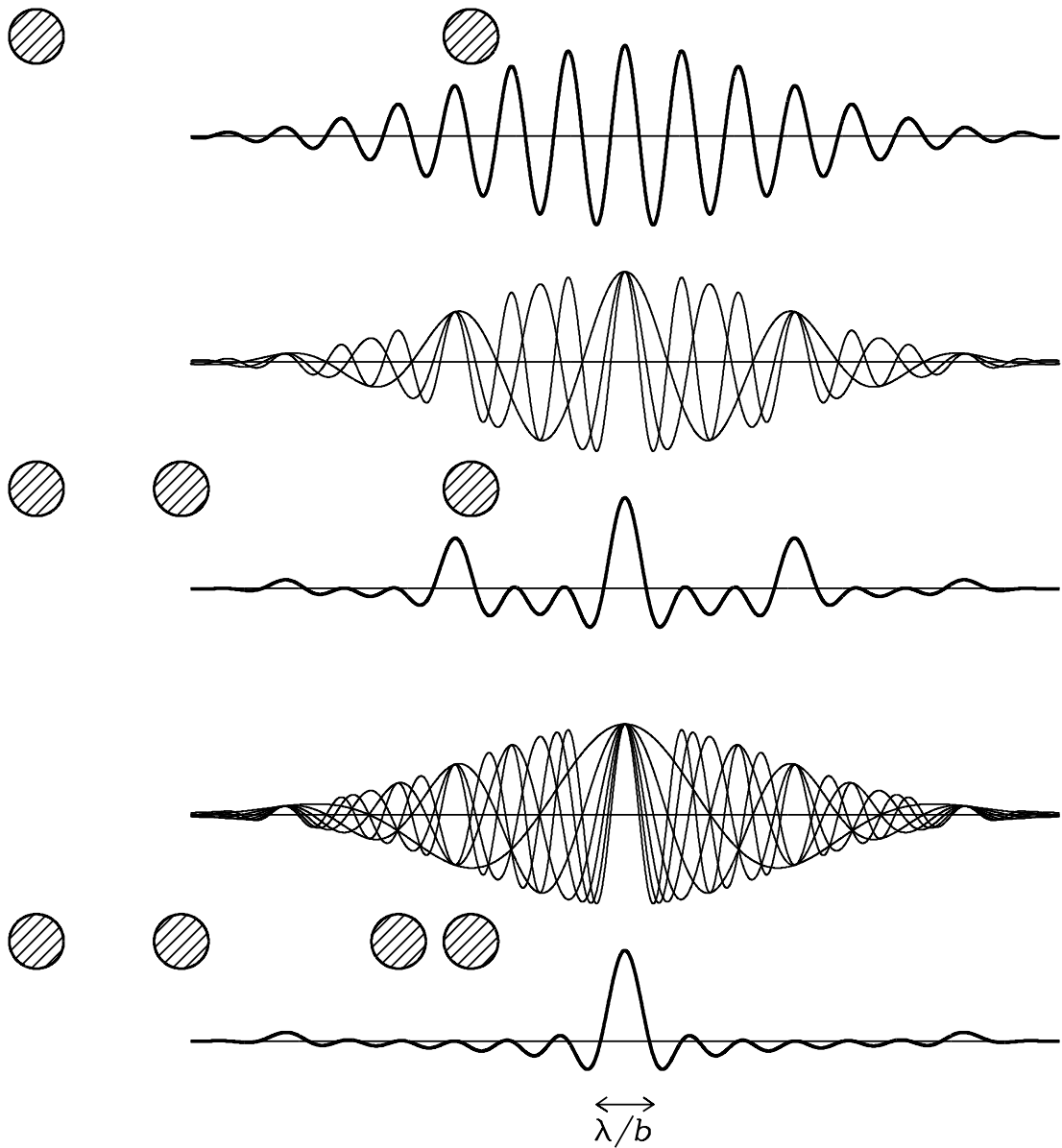


Figure 1.3: The effect of adding dishes to an interferometer and synthesising the correlated outputs from antenna pairs. The antenna positions are shown as hatched circles, the baseline correlations in the first and third plots with their synthesised beams plotted beneath. As shown, the main response of the synthesised beam is approximately Gaussian with a width (resolution) of  $\lambda/b$ . Image taken from Condon and Ransom (2016).

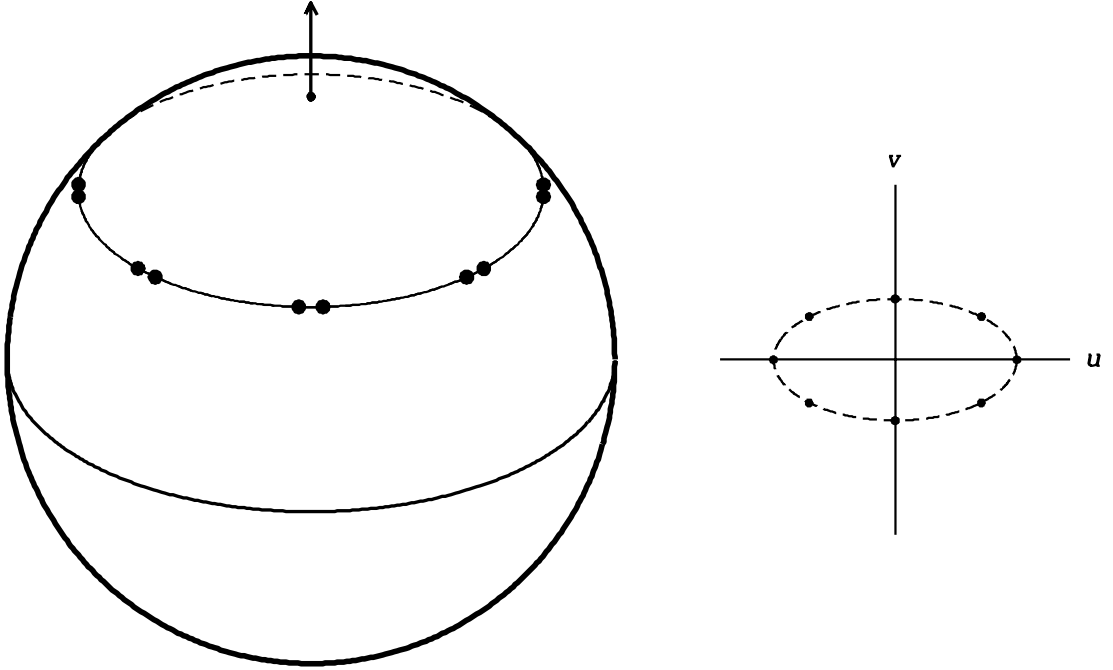


Figure 1.4: A two-element interferometer at a latitude of  $40^\circ$  as viewed from a distant source at a declination of  $\delta = 30^\circ$ . As the Earth rotates (counter-clockwise) the  $(u, v)$  coordinates of the observed visibilities (i.e. the projected baseline separation) are shown on the plot to the right of the diagram. Image taken from Condon and Ransom (2016).

by simply Fourier transforming the output of the correlator.

Individual dishes in a telescope array can be thought of as small sections of a much larger, imaginary dish with a diameter equal to the longest baseline. While the resolution of the telescope array is approximately equal to the synthesised beam FWHM of this imaginary dish, the effective collecting area is only equal to the sum of the collecting areas of the individual dishes. This results in the  $uv$ -plane being poorly sampled. It is impractical to have the dishes constantly move to vary the baseline orientations during observation to improve the  $uv$ -plane sample, so a method called Earth-rotation aperture synthesis is used.

Earth-rotation aperture synthesis uses the rotation of the Earth relative to the observed source to change the baseline orientations throughout an observation in order to properly sample the  $uv$ -plane. A simple two-element interferometer with the antennae arranged on an East-West line will trace out a complete ellipse within the  $uv$ -plane over a period of 12 hours. Only 12 hours is required to completely sample the  $uv$ -plane with an East-West array as each baseline with coordinates  $(u, v)$  can also be considered as a baseline with coordinates  $(-u, -v)$ . The maximum value of  $u$  is equal to the baseline length and the maximum value of  $v$  equal to  $u$  scaled by  $\cos \delta$  where  $\delta$  is the declination of the source. A diagram of a two-element interferometer using Earth-rotation synthesis is shown in Figure 1.4. Telescope arrays with multiple baselines will trace out a series of concentric ellipses. An example of an East-West radio telescope array is the ATCA, the instrument primarily used throughout this thesis.

## 1.4.2 The Australia Telescope Compact Array (ATCA)



Figure 1.5: The ATCA in a hybrid compact array configuration. Photographed by the author in 2013.

The radio data used in this thesis was obtained from the ATCA instrument located outside the rural town of Narrabri, New South Wales, Australia. ATCA is operated as a national research facility alongside the radio astronomy observatories Parkes and Mopra by the Australia Telescope National Facility (ATNF), a division of Australian Commonwealth Scientific and Industrial Research Organisation (CSIRO) Astronomy and Space Science.

ATCA consists of six 22 m diameter antennas that connect to a single correlator in order to behave as a single radio synthesis array. To allow the support of multiple array configurations, 5 of the dishes are situated on a 3 km railway track that runs East to West along a tangent to the surface of the Earth. There is also an additional 214 m track that runs North to South that intersects at approximately the centre of the main track to allow a new set of hybrid arrays of shorter baselines. The sixth antenna is fixed a further 3 km from the end of the western end of the main track. An antenna may only be placed in one of 45 predetermined locations where there are existing stations to provide power and data access points to the antennas. Once an antenna is moved to a station, four large hydraulic-driven feet extend down from the antenna base onto concrete station footholds. These feet slightly lift the antenna off the railway to ensure that they cannot be inadvertently moved during observations. Its position is then accurately measured to within fractions of a millimetre.

There are a total of 17 standard array configurations, offering a variety of different baseline lengths for various astronomical studies. In the most compact configuration, the minimum baseline achievable is 30 m, with a maximum baseline of 170 m<sup>3</sup>. In the larger configurations, the maximum possible baseline is from the beginning of the East-West track to the fixed sixth antenna, a total distance of 6 km. The reason for the different configurations is that there exists a tradeoff between the resolution and the *uv*-coverage of the data collected. Large array configurations provide superb resolution but consequently have large gaps in the *uv*-coverage, while compact configurations provide nearly full *uv*-coverage at the cost of poor resolution. As a result, observers often request observing time while the instrument is in different configurations and later combine the data to produce images that have both high resolution and good *uv*-coverage.

The antennas themselves consist of a dish with solid aluminium panels that reflect radio waves onto the sub-reflector that is suspended above the dish. This sub-reflector then concentrates the radio waves into a receiver located inside the antenna body. The antennas can physically support observations of up to 116 GHz, however the sixth antenna still has a number of older perforated aluminium panels and is therefore limited to 50 GHz. This is acceptable because the sixth antenna is not used for the higher frequency observations as they typically use compact hybrid arrays. Prior to 2009, the maximum available bandwidth was  $2 \times 128$  MHz and provided support for both continuum and spectral line surveys. Post 2009, the ATCA was upgraded to support a much wider bandwidth of up to  $2 \times 2$  GHz.

## 1.5 Research Aims and Significance

This thesis aims to complete the following major scientific objectives:

- Pioneer advanced imaging and source-finding techniques for large area radio surveys in preparation for the next generation of instruments.
- Using automated methods, produce a catalogue of radio sources at a central frequency of 2.1 GHz containing positions and flux densities for each source, and spectral indices where possible.
- Investigate the spatial correlation between bent-tail radio sources and SZ effect selected galaxy clusters.

To achieve these aims, I planned and carried out the observations of the ATLAS-SPT radio survey of the SPT deep-field. This field was selected in order to enable the pursuit of several

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<sup>3</sup>For compact array configurations, the 6th antenna is typically ignored when quoting the maximum baseline because baselines containing the 6th antenna sample far greater distances in the *uv*-plane compared to the other baselines. This creates a large gap in the *uv*-coverage which makes the imaging process difficult.

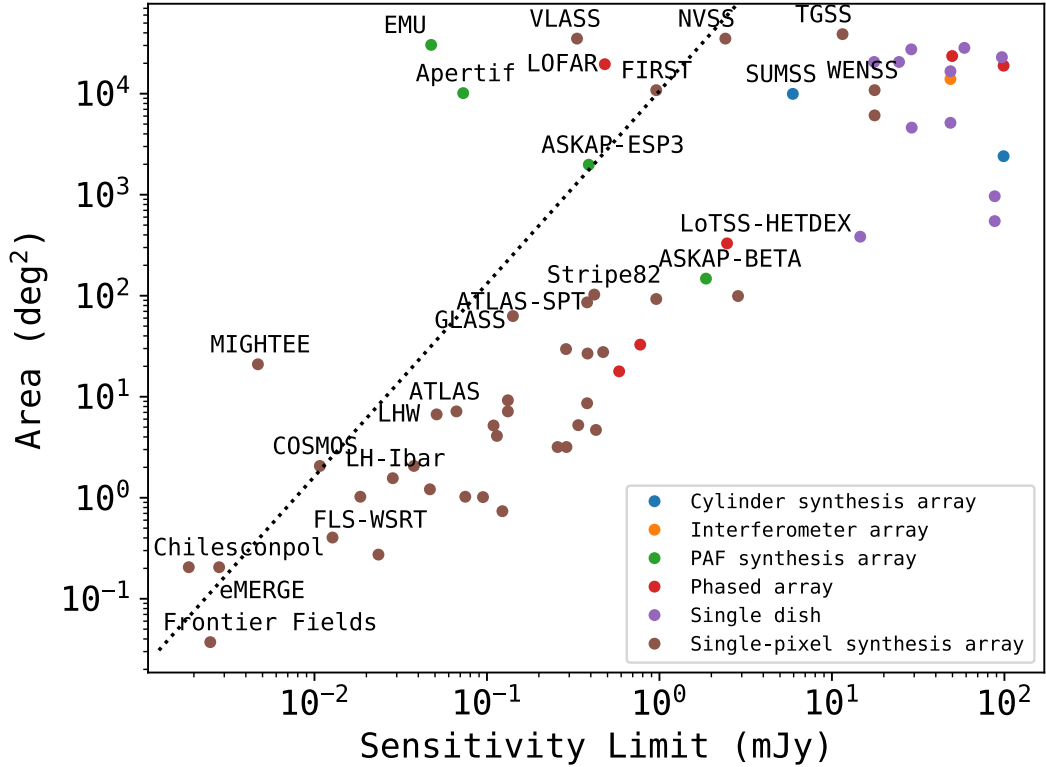


Figure 1.6: A comparison of existing and planned radio surveys in terms of sensitivity and sky area. The black dotted line shows the approximate limit within this space due to time award constraints. Figure recreated from Norris (2017).

major scientific goals including clusters of galaxies, AGN, large-scale structure, dusty star-forming galaxies and cosmology. The field has deep multi-wavelength coverage (as described in Section 1.3.1) yet very few radio observations exist. A survey at radio frequencies is the last piece of the multi-wavelength puzzle for this region of sky. Accurate positions provided in the radio source catalogue will enable the disentanglement of confused sources from other studies and provide accurate targets for follow-up observations with other instruments.

At  $\sim 86 \text{ deg}^2$ , the ATLAS-SPT survey is considered a large area survey in the context of other radio surveys conducted with a synthesis array consisting of single-pixel feeds (see Figure 1.6). The sensitivity is mostly limited by the data quality – observing and imaging difficulties described throughout Chapter 2 prevented the survey from reaching the target rms noise level of  $40 \mu\text{Jy beam}^{-1}$  which was estimated using a telescope sensitivity calculator. This follows the sensitivity discrepancy described by Heywood et al. (2016) who demonstrated the significant difference between thermal noise and effective noise of the Very Large Array (VLA) Stripe 82 survey due to various imaging effects such as incomplete deconvolution and calibration deficiencies. These effects are exacerbated by the limited  $u, v$  coverage of the ATLAS-SPT.

There are currently several next-generation radio telescopes being built around the world ca-

pable of conducting surveys of unprecedented size and depth on dramatically reduced timescales. In particular, the Australian Square Kilometre Array Pathfinder (ASKAP) (Johnston et al., 2008) in Western Australia will be able to observe  $\sim 30 \text{ deg}^2$  to an rms noise of  $\sim 10 \mu\text{Jy beam}^{-1}$  in 12 h. The Evolutionary Map of the Universe (EMU) (Norris et al., 2011) survey is a prioritised continuum survey planned for ASKAP that will map the entire visible sky ( $\sim 75\%$  of the full sky) at a wavelength of 20 cm. The survey is expected to produce a catalogue of approximately 70 million galaxies out to extremely large cosmological distances. One of the declared science goals for EMU is to use radio sources to trace galaxy clusters and large-scale structure. The low-frequency end of our survey bandwidth overlaps with EMU, but our effective frequency is significantly higher. The ATLAS-SPT survey will therefore serve as a pilot study for EMU as our field is both large and deep enough to act as a data complement for spectral index measurement and as a training set for photometric redshifts. Our survey will also contribute to the refinement of EMU by providing cross-identification of sources and piloting advanced imaging and source extraction techniques.

## 1.6 Outline

This thesis is organised into the following chapters and sections. Chapter 2 describes the data acquisition from planning the radio observations, the observations themselves, the data reduction and calibration method, and the imaging process. A description of the source finding process executed on the final image is given in Chapter 3 along with the full radio catalogue of sources, analysis of the completeness and accuracy of the catalogue, comparisons with another study, and radio source counts. In Chapter 4 I present original work submitted to the peer-reviewed journal *Monthly Notices of the Royal Astronomical Society* which has made use of the data products presented in this thesis. Finally, in Chapter 5 I give a conclusion and outline future work.



## Chapter 2

# Observations and Data

This chapter is based on work I presented at the conference *The many facets of extragalactic radio surveys: towards new scientific challenges* in Bologna, Italy on 20–23 October 2015 (O’Brien et al., 2016).

### 2.1 Observation Strategy

The ATLAS-SPT survey was conducted using the ATCA at a central frequency of 2.1 GHz with the correlator set to the standard Compact Array Broad-band Backend (CABB) continuum mode. This provides  $2048 \times 1$  MHz channels for a total bandwidth of approximately 2 GHz. To maximise resolution, the observations were conducted with long baseline configurations (6A and 6C) which consisted of baseline lengths between 153.1–6000.0 m and resulted in a synthesised beam full-width half-maximum of  $8''$ .

The target field was the SSDF, a  $\sim 86 \text{ deg}^2$  area of sky bounded by  $23 \text{ h} \leq \alpha \leq 24 \text{ h}$  and  $-60^\circ \leq \delta \leq -50^\circ$ . Since the field is much larger than the primary beam of the telescope (i.e. the effective field of view), the observation was conducted in mosaic mode.

#### 2.1.1 Pointing Arrangement

To ensure the entire field is sampled to a uniform depth, the antenna pointings were arranged in a hexagonal grid across the field. The spacing between pointing centres was chosen to conform to Nyquist sampling:

$$\theta_{\text{hex}} = \frac{\lambda}{D\sqrt{3}} \quad (2.1)$$

where  $\theta_{\text{hex}}$  is the hexagonal pointing spacing in radians,  $\lambda$  is the observing wavelength, and  $D$  is the antenna dish diameter. Since the primary beam size changes as a function of

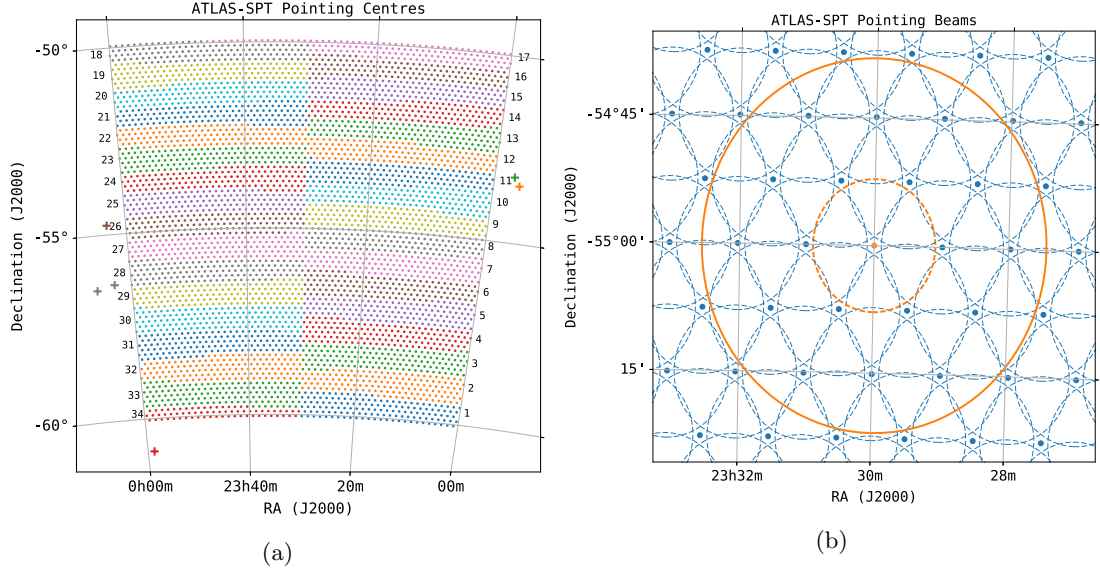


Figure 2.1: The antenna pointings used for the ATLAS-SPT survey. (a) shows the pointing centres coloured by block, with the block numbers given around the field boundary. Additional pointings centred on strong sources identified in SUMSS are drawn with + markers. (b) is a zoomed in area of the field showing the pointing centres and the ATCA primary beam FWHM at 3.1 GHz as a dashed circle. A single example of the primary beam FWHM at 1.1 GHz is shown as a solid orange circle.

observing frequency,  $\theta_{\text{hex}}$  was calculated using the upper-limit of the observing bandwidth, 3.1 GHz ( $\lambda = 9.67$  cm). Using Equation 2.1, the pointing centre spacing was calculated to be  $\sim 8.7'$ . However, this spacing does not account for the coordinate system geometry where the distance between meridians decreases toward the celestial poles. This is typically not an issue for small fields or, more accurately, fields that do not span a significant area in Declination. As the SSDF spans  $10^\circ$  in Declination, the on-sky horizontal spacing between pointings at the North of the field and to the South will differ by a factor of  $\sim 0.78$ . Thus, a correction was made to scale the horizontal spacings proportionally to  $\cos \delta$  to avoid oversampling at the Southern end of the field. The final pointing arrangement over the field consists of 4787 pointings and is shown alongside a subset of pointings showing the ATCA primary beam FWHM in Figure 2.1.

### 2.1.2 Calibration Requirements

Every radio-astronomy observation must undergo various calibration steps both before and after the observations. The specific calibration requirements are dependent on the observing frequency and the instrument, but most involve the observation of special sources called “calibrators”. It is critical for observers to understand these requirements while planning observation schedules as they can use a significant fraction of observing time. The calibration steps for centimetre-wavelength observations with the ATCA can be summarised into four parts: delay calibration, bandpass calibration, absolute flux calibration, and time-varying gains calibration.

Delay calibration refers to the measurement and correction of the signal delays from each antenna. Each antenna measures the incoming radio-wave and sends it to the correlator. Here, the signals from each pair of antennas (referred to as a “baseline”) is correlated by effectively multiplying the signals. For the signal from a source to correlate, they must arrive at each antenna simultaneously. The correlator automatically corrects for geometric delays, that is, the difference in arrival time at each antenna for a plane wavefront due to the physical location of each antenna. Other forms of time delay, such as the return path lengths and other instrumental delays must be measured and corrected before at the beginning of the observation to ensure the observed signals are correlated. Small, uncorrected delays manifest as inconsistent phases as a function of frequency. One can determine the required delay corrections by measuring the slope of the phases with respect to frequency. This is achieved by observing any strong ( $S \gtrsim 1$  Jy), unresolved source and issuing the `dcal` command to the correlator.

Bandpass calibration corrects for the inconsistent response of each antenna across the observing band. As with delay calibration, this can be corrected by observing a bright, unresolved source. However, since each channel needs to be corrected, the integration time on the bandpass calibrator source is typically longer in order to reach a sufficient signal-to-noise ratio per channel. For centimetre continuum observations, one typically requires a single 5 to 10 min scan. This can be at any time during the observation as the receivers are generally stable over the course of a typical 12 h observation while in continuum mode. The data collected on the bandpass calibrator is then used to correct the bandpasses after the observation.

Absolute flux density calibration translates the arbitrary gain scale that is measured by the telescope into an absolute flux density scale. For the ATCA, this is achieved by observing one of four well-known flux density calibrator sources then computing and applying a frequency-dependent correction factor. For ATCA centimetre observations, the recommended flux density calibrator is PKS 1934–638 as it has a known, stable flux density. The flux scale model for PKS 1934–638 is given in Reynolds (1994). As with the bandpass calibration, the absolute flux scale is applied after the observation.

Time-varying gains refers to the multitude of factors that affect how the telescope responds to incoming signals over the course of an observation. Examples include atmospheric and ionospheric phase and opacity, antenna dish distortions due to gravity, and incoming radiation from the ground. Since these effects are time-variable, they need to be monitored regularly to be corrected. The simplest way to monitor changes in the antenna gains over time is to regularly observe an unresolved source close to the target source(s). This calibrator source, referred to as the gain or phase calibrator, should have a stable flux throughout the observation. At centimetre-wavelengths, it is recommended to observe the phase calibrator once or twice per

hour during good atmospheric conditions. Similarly to the bandpass and absolute flux calibrations, the data are corrected after the observation by interpolating gain corrections between the phase calibrator samples.

Further detail on the calibration methods performed after the observations is given in Section 2.3.

### 2.1.3 Constructing the Schedule

#### 2.1.3.1 Distributing observing time

The total observing time awarded by the ATCA Time Allocation Committee (TAC) for the initial proposal was 241 h. The proposal made a commitment to trial the new ATCA on-the-fly (OTF) mosaic mode where the telescope integrates while continuously moving. This can significantly decrease the time lost to overheads such as slewing between pointings. However, given that the mode was largely untested, we were reluctant to risk such a large amount of observing time by using this mode for the entire project. Instead, we decided to use the first two observing days ( $2 \times 12$  h) to observe a subset of the field using OTF and use the remaining time to observe the entire field in the traditional ATCA mosaic mode. This will allow us to provide a quantitative evaluation on the accuracy of the OTF mode by comparing it to the data recorded using the traditional mosaic mode.

With the pointings arranged and the observing schedule released by the TAC, the next step was to determine how long to integrate on each pointing. This involved balancing the awarded observing time against  $u, v$  coverage, integration time, and calibration overheads. Calibration overheads are mostly constant, so the real trade-off is between the time of each individual scan and the total number of scans per pointing with shorter scans providing more  $u, v$  coverage at the cost of increased slewing overhead.

Since the calibration source requirements for the delay, bandpass and absolute flux density calibrators are almost the same (i.e. a bright, stable, unresolved source with known flux density; see Section 2.1.2), we were able to observe a single source to correct for these effects: PKS 1934-638. To monitor the time-varying gains, we used the phase calibrator PKS 2333-528 ( $S_{2.1\text{GHz}} = 1.766 \pm 0.014$  Jy) for the entire project as it is close to the field centre and thus  $\leq 5^\circ$  from each pointing. As a worst case, it would take the antennas 72 sec to slew from the furthest pointing to the phase calibrator if the antenna drive time was limited to movement only in the altitude direction (the ATCA antennas slew faster in azimuth compared to altitude).

The amount of time available to spend integrating on each pointing can be estimated using

the following equation:

$$N_{cuts}(N_p t_p + t_{slew,p}(N_p - 1)) = f_{cal} \frac{t_{obs} - t_{cal}}{f_{cal} + t_{cal}} \quad (2.2)$$

where  $N_{cuts}$  is the number of desired samples of the  $u, v$  plane per pointing;  $N_p$  is the number of pointings;  $t_p$  is the observing time spent on each pointing per sample in the  $u, v$  plane;  $t_{slew,p}$  is the time taken to slew between two pointings;  $f_{cal}$  is the the phase calibrator scan frequency, i.e. the amount of time to spend observing pointings before a phase calibrator scan is required;  $t_{obs}$  is the total observing time after accounting for telescope setup overheads (i.e. calibration steps, excluding phase calibration); and  $t_{cal}$  is the time required for a phase calibrator scan, including the slew to and from the calibrator.

For the ATLAS-SPT survey, all of these values, except  $t_p$ , are known or can be estimated. Experience from past surveys indicated that to obtain enough  $u, v$  coverage to map complex source structures and permit stable imaging (deconvolution is more likely to diverge when the data is poorly sampled in the  $u, v$  domain), a minimum of 6 equidistant samples within the  $u, v$  plane for each pointing would be necessary ( $N_{cuts} = 6$ ). The number of pointings given in Section 2.1.1 is  $N_p = 4787$  and the time to slew between each was estimated to be  $t_{slew,p} = 1.6$  sec. The ATCA online calibrator cycle time calculator<sup>1</sup> indicated that the rms of the uncorrected visibility phases would be no worse than  $2^\circ$  if the phase calibrator were to be scanned every 20 min. Thus, we set  $f_{cal} = 20$  min. Given that the chosen phase calibrator is bright, we can obtain a sufficient signal-to-noise ratio for calibration in 2 min. This, combined with the worst case slew time to the phase calibrator (72 sec as mentioned above), means that each phase calibrator scan will take  $t_{cal} = 4.4$  min. We estimated that the telescope setup, delay calibration and a 10 min scan of the bandpass/flux calibrator at the beginning of each observation day would take approximately 30 min. Given the 15 unique observing days, this leaves a total available observing time of  $t_{obs} = 209.5$  h. Solving Equation 2.2 for the integration time per pointing per cut gives 19.9 sec. Rounding down to the nearest multiple of available correlator cycle time intervals gives  $t_p = 18$  sec.

### 2.1.3.2 Pointing blocks

Since the ATLAS-SPT project consists of a large number of mosaic pointings, each with a small number of  $u, v$  plane samples, we required careful bookkeeping to record which pointings have been observed at given hour angles to ensure approximate equidistant  $u, v$  coverage. No matter the level of detail in the observation planning, unpredictable events such as Radio Frequency Interference (RFI) and Target of Opportunity (ToO) observations can result in significant ob-

<sup>1</sup><https://www.narrabri.atnf.csiro.au/calibrators/calcycle.html>

serving time losses and thus careful records were kept to ensure our  $u, v$  coverage requirements were met.

Recording the hour angle at which each pointing was observed is infeasible due to the large number of pointings and frequent switching between pointings. An alternative solution was devised where the pointings were grouped into “blocks” which would take approximately one sidereal hour to complete one  $u, v$  cut for each pointing. The number of pointings in a block was determined by:

$$t_p N_{p,b} + t_{slew,p}(N_{p,b} - 1) + 3t_{cal} = 3600 \text{ sec} \quad (2.3)$$

where  $N_{p,b}$  is the number of pointings per block. This resulted in  $\lfloor N_{p,b} \rfloor = 143$ , for a total of 34 blocks (33 blocks of 143 pointings, and one block of 68 pointings). The pointings were added to the block groups sequentially in alternating directions across RA so that when one row of pointings is complete, the antennas only need to slew up to the next pointing to start the next row. Furthermore, each block (with one exception) was restricted to span 0.5 h in RA because the field was not entirely above the horizon at the start of some observing days. This enabled the observation of at least half the blocks before the entire field had risen. The pointing blocks are illustrated in Figure 2.1a.

### 2.1.3.3 Exterior sources

Radio telescopes are sensitive to sources well beyond the effective limit of their primary beam. While the sensitivity drops off and approaches 0 away from the centre, a bright enough source can still produce sidelobes which affect the quality of the image. The impact of these exterior sources on the imaging process can be mitigated by modelling the source and subtracting that model from the visibility data prior to imaging. This effectiveness of this process is limited by the accuracy of the exterior source model.

Anticipating this problem, the exterior of the field was searched for nearby bright sources. Ideally, these sources would be identified in a survey at a similar frequency, but since ATLAS-SPT was the first of its kind for this field, we used the SUMSS catalogue (Mauch et al., 2003) to find sources with an extrapolated 2.1 GHz flux density of  $\geq 1$  Jy. Six candidate exterior sources were found and an extra pointing was placed centred on each source. This was to ensure an accurate model could be produced by imaging the potentially problematic sources at the phase centre where the telescope is most sensitive. These exterior source pointings were placed into their nearest block and are shown with plus markers in Figure 2.1a.

## 2.2 Observations

The main ATLAS-SPT observations took place on-site at the Paul Wild Observatory in Narrabri, NSW, Australia during the ATNF April 2013 observing semester between 19th May – 3rd June 2013. Most observations spanned long periods over unfavourable human hours which was mitigated by sharing the load amongst several observers. The specific observation periods are given in Table 2.1.

Observers were given a table of the pointing blocks and LST hour ranges along with the scheduled blocks for each observing period. Any issues resulting in the potential loss of data during the observation was marked on the table to allow the affected block to be rescheduled for the same LST on a later day. Time lost due RFI and a ToO were the most significant and required the resubmission of the project proposal to the TAC to recover the time in the next semester which was granted and observed between 6th February – 11th February 2014.

Day	Date	Start Time	Duration (h)	Array Config.
April 2013 Semester				
1	19 May 2013	00:30	13	6C
2	20 May 2013	00:30	13	6C
3	21 May 2013	00:30	14.5	6C
4	22 May 2013	00:00	15	6C
5	23 May 2013	00:00	15	6C
6	24 May 2013	00:00	15	6C
7	25 May 2013	00:00	15	6C
8	25 May 2013	23:30	15	6C
9	26 May 2013	23:30	15	6C
10	27 May 2013	23:30	15	6C
11	28 May 2013	23:30	15	6C
12	29 May 2013	23:30	15	6C
13	30 May 2013	23:30	15	6C
14	31 May 2013	23:30	15	6C
15	01 June 2013	23:30	15	6C
16	02 June 2013	23:00	14.5	6C
17	04 June 2013	00:00	8	6C
October 2013 Semester				
18	06 February 2014	09:30	11	6A
19	07 February 2014	11:30	3	6A
20	11 February 2014	16:00	3	6A
Total			260	

Table 2.1: The scheduled observing periods for the ATLAS-SPT. All dates and times are in Australian Eastern Standard Time (AEST; UTC+10). The additional 17h awarded in the October 2013 semester was to recover lost observing time in the previous semester.

## 2.3 Data Reduction and Calibration

Calibration (this section) and imaging (Section 2.4) were conducted using the ATNF version of the data reduction software MIRIAD (Sault et al., 1995). In this section, I outline the steps taken to calibrate the radio-continuum data. The inputs to the tasks used are shown in boxes. Input parameters that were left unset are omitted. All calibration steps were repeated for each observing day.

Raw telescope data was read in using the MIRIAD task `atlod`, with options set to automatically remove known persistent interference from both internal and external sources, discard the auto-correlation data from each antenna, and apply the online XY phase corrections.

```
Task:  atlod
in     = input.RPFITS
out    = output.uv
options = birdie,rfiflag,noauto,xycorr
```

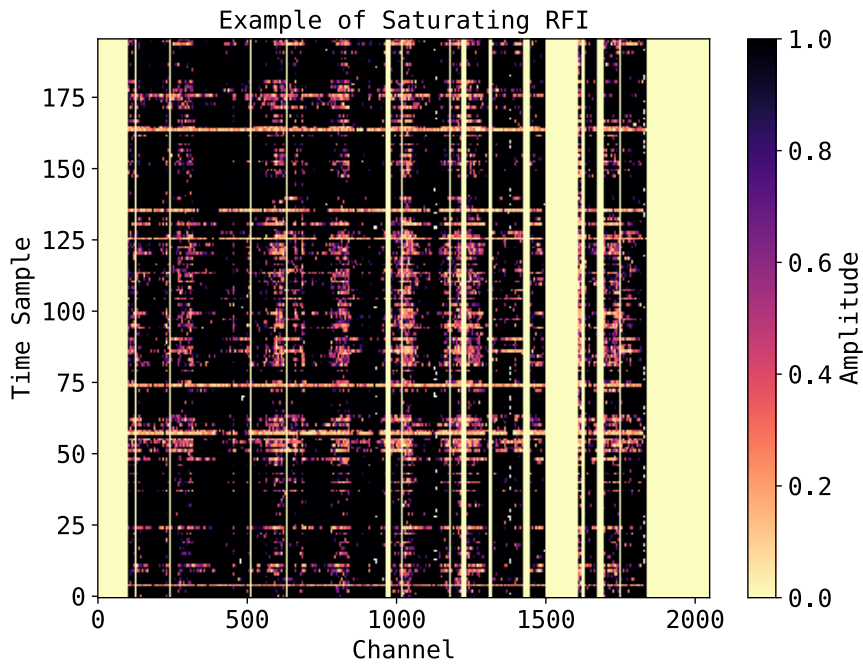
The data was then split into separate files for each source using `uvsplit`. Mosaic pointings were split using mosaic mode to keep each block together in a single file. The bandpass and flux density calibrator data were inspected first. Any obvious radio-frequency interference (RFI) was flagged using either `uvflag` or the interactive task `blflag`. Less obvious RFI, such as narrow-bandwidth intermittent RFI, was flagged using the task `pgflag` which implements the automated SumThreshold flagging method (Offringa et al., 2010). The flagging was repeated for all raw polarisations (XX, YY, XY, YX). This flagging strategy was sufficient to remove most RFI except in cases where it was so extreme that the receivers were saturated and no astronomical signals were recoverable. An example of this extreme RFI (sometimes referred to as “mid-week” RFI) is shown in Figure 2.2.

```
Task:  pgflag
vis    = 1934-638.2100
stokes = xx,yy,xy,yx
flagpar = 7,1,1,3,5,3,20
command = <b
options = nodisp
```

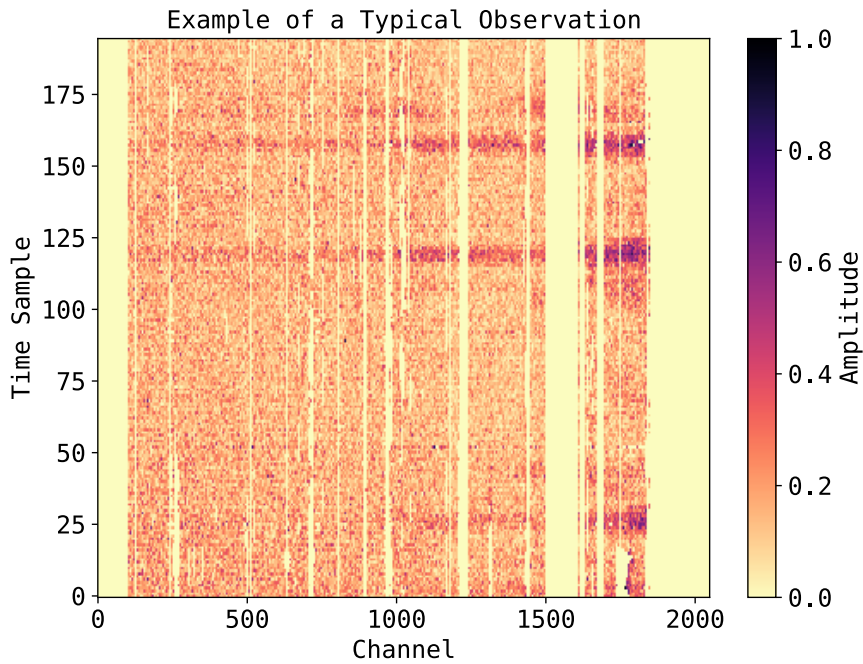
The bandpass function and an initial estimate of the antenna gain corrections were then calculated using the task `mfcal` on the bandpass calibrator using a solution interval of 0.1 min. Time-varying gain and instrumental polarisation leakage corrections were then calculated in



multi-frequency mode with 8 frequency bins with the task `gpcal`. These flagging and calibration steps were then repeated for the phase calibrator data, adding the `qusolve` option to `gpcal` to solve for the phase calibrator polarisation in addition to the instrumental leakage. The phase calibrator data was then corrected to the absolute flux density scale of PKS B1934-638 using `gpboot`. Finally, the calibration solutions from the phase calibrator were copied to the individual pointing data with `gpcopy` which were then also flagged using `pgflag`. Approximately 25% of the visibility data in each pointing was flagged due to RFI.



(a) An observation with saturating broadband interference. Note that the interference is spread across both time and frequency channels, saturating the signals from real sources. Real signals are not recoverable from this kind of interference. The colour scale is saturated beyond 1.0.



(b) A typical observation covering many pointings with all strong interference removed. The contiguous lines of zero amplitude are from previous flagging of some channels that are known to contain interference. The dark structures seen in this plot are from real sources.

Figure 2.2: A comparison between a typical ATLAS-SPT dataset and another affected by saturating broadband interference (“mid-week” RFI). Time is shown on the y-axis in units of correlator samples (each sample is a 9 s integration), with channels (analogous to frequency) on the x-axis. The intensity is mapped to the amplitude of the signal.

## 2.4 Imaging

The imaging process mostly follows standard MIRIAD practices for wide-bandwidth radio-continuum ATCA data, that is, the requirement to image each pointing individually before linearly mosaicking the pointings to form a final image of the field. As each imaging step except the final linear mosaic is to be run on each pointing individually, most of the imaging is an embarrassingly parallel process. This section contains details on the imaging process for individual pointings (Section 2.4.1), a summary of the parallel computing approaches used to speed up the individual imaging steps (Section 2.4.2), followed by details of the linear mosaicking which produced the final image of the ATLAS-SPT field (Section 2.4.3).

### 2.4.1 Individual Pointing Imaging

A Stokes  $I$  dirty map and a dirty beam (point spread function (PSF)) was created for each pointing using the task `invert` in multi-frequency synthesis (MFS) mode. A spectral dirty beam was also created so that spectral information was maintained during deconvolution as described in Sault and Conway (1999). Briggs robust weighting scheme was used with a parameter of  $-0.5$  to achieve a good compromise between resolution and sensitivity. An example of the PSF for a typical pointing is shown in Figure 2.3. Each map was gridded on the same pixel grid by defining a common reference pixel at the field centre ( $\alpha = 23^{\text{h}}30^{\text{m}}00^{\text{s}}$ ,  $\delta = -55^{\circ}00'00''$ ) where each pixel was  $0.86''$  in size.

Every radio source detected from the sky in the dirty maps are convolved with the PSF of the instrument. To remove this instrumental response, deconvolution is required. This process is also known as *cleaning* in reference to the CLEAN algorithm first described by Högbom (1974). The implementation of multi-frequency deconvolution in MIRIAD requires a guard band around the cleaning area such that only the inner third of an MFS image can be cleaned. This restriction is limited by the size of the dirty beam image; increasing the size of the dirty beam image increases the area of the dirty map which can be deconvolved by `mfclean`. Thus, the dirty beam was constructed to be twice the size of the dirty map with the option *double*, allowing the inner two-thirds to be deconvolved in the next step.

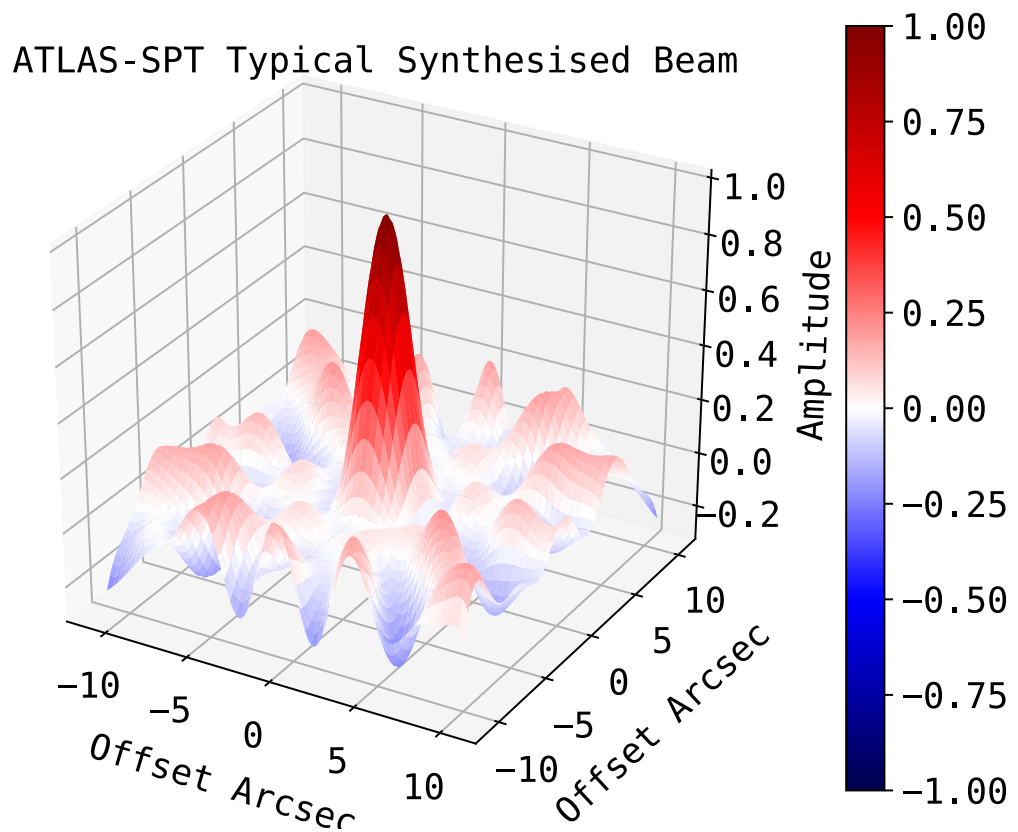


Figure 2.3: The synthesised beam (point-spread function) of a typical ATLAS-SPT pointing.

```

Task:   invert
vis     = spt1_1.uv
map     = spt1_1.map
beam    = spt1_1.beam
imsize  = 6028
cell    = 0.86
offset  = 23:30:00,-55:00:00
robust  = 0.5
stokes  = i
options = mfs,sdb,double,mosaic

```

The dirty maps were then deconvolved using the task `mfclean`. The sparse  $u, v$  coverage of each pointing (see Figure 2.4 for a typical example) made deconvolution difficult as severe artefacts from mJy-level sources beyond the edge of the primary beam were well above the level of thermal noise. These artefacts can be removed by including the source during deconvolution, but this was infeasible for these data as in many cases the sources were located well beyond the edge of the primary beam. Including these sources during deconvolution would require

imaging a much larger area which is computationally expensive. To address this problem, each pointing was imaged with a coarse resolution of  $4.3'' \text{ px}^{-1}$  so that deconvolution area extended to 5 times the size of the primary beam. The inner portion of the image corresponding to the sky-area that will be cleaned at full resolution (i.e. the region containing the sources of interest for the pointing) was masked and the approximate positions of strong sources beyond the primary beam area were detected using the task `imsad`. Small sub-images of 200 px square were then created for each strong outlier source at the full pixel resolution of  $0.86''$  which were then deconvolved. The models of the outlier sources were then subtracted from the pointing visibilities to remove the artefacts using `uvmodel`.

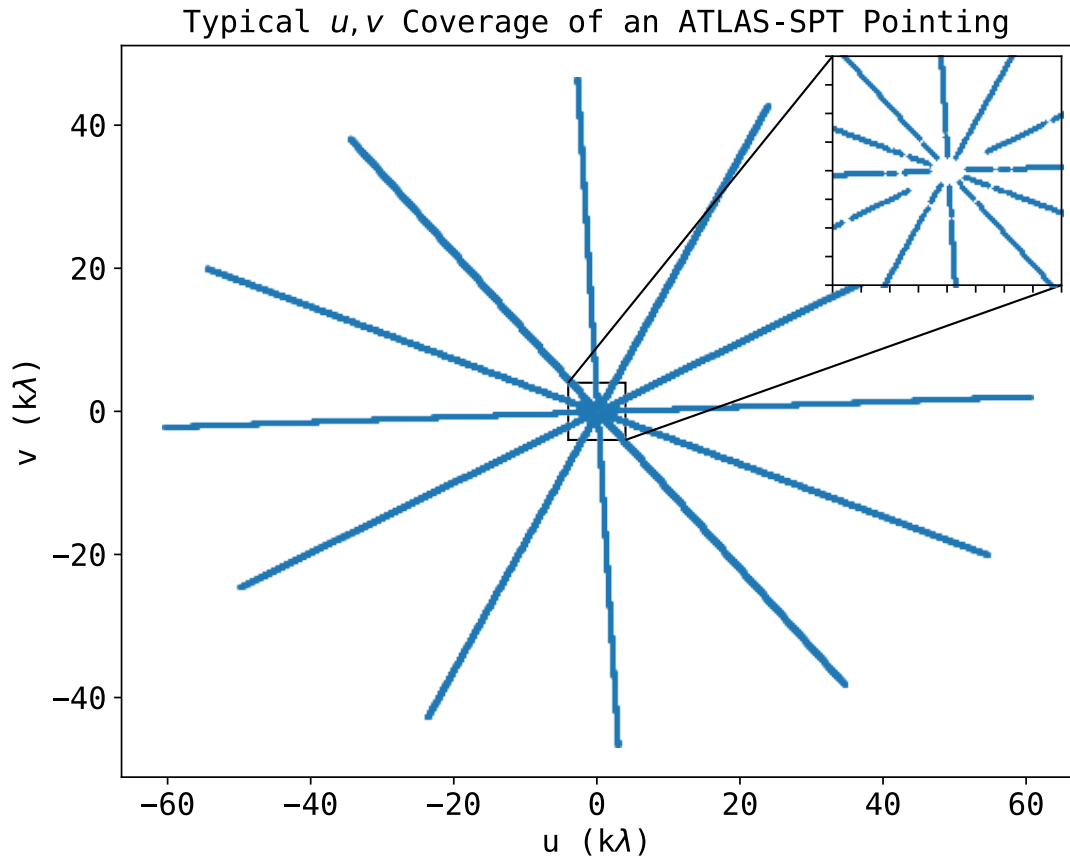


Figure 2.4: The  $u, v$  coverage for a typical ATLAS-SPT pointing. The inset shows a zoomed in region for  $u, v$  values  $-4$  to  $4 k\lambda$ . The missing data around  $(0,0)$  is due to the telescope configuration, whereas the small gaps seen in the inset is due to flagged data on short baselines which are more susceptible to RFI.

```
Task:  mfclean
map    = spt1_1.map
beam   = spt1_1.beam
out    = spt1_1.mfclean
cutoff = <20*rms>
niters = 5000
region = percentage(66)
```

```
Task:  uvmodel
vis    = spt1_1.uv
model  = spt1_1_outlier.mfclean
options = subtract,mfs
out    = spt1_1.uvmodel
```

With the outlying sources removed from the visibilities, the dirty maps were recreated and iteratively deconvolved until the maximum residual reached  $20\sigma$  (where  $\sigma$  is the rms of the image noise). The output clean models were then used to perform an iteration of phase self-calibration using the task `selfcal` with the gain solutions split across 8 frequency bins. The imaging and deconvolution was then repeated for each pointing twice more, cleaning down to maximum residuals of 10 then  $5\sigma$ , repeating the phase self-calibration with the  $10\sigma$  clean models for pointings that showed signs of significant phase errors.

```
Task:  selfcal
vis    = spt1_1.uv
model  = spt1_1.mfclean
interval = 1
nfbins = 8
options = phase
```

Using the task `restor`, the clean models for each pointing were then convolved with their respective dirty beams and subtracted from the dirty map to produce a residual image. The clean models were convolved with a Gaussian fit to their dirty beams (the restoring beam) and added back to the residual image to produce a restored map for each pointing.

```
Task:   restor
model   = spt1_1.mfclean
beam    = spt1_1.beam
map     = spt1_1.map
options = mfs
out     = spt1_1.restor
```

To prepare the restored maps for linear mosaicking, each was convolved with a Gaussian using the task `convol` to produce a map with a synthesised beam FWHM of 8". This beam size was chosen to fit the largest restoring beam for the field.

```
Task:   convol
map     = spt1_1.restor
fwhm    = 8
out     = spt1_1.convol
options = final
```

## 2.4.2 Parallel Computing

The parallel nature of the imaging made it ideal to be processed on a computing cluster. All pointings were imaged on the *Galaxy* supercomputer at the Pawsey Supercomputing Centre. With 472 compute nodes supported by a high-speed Lustre filesystem, *Galaxy* was able to image hundreds of pointings simultaneously, drastically reducing the amount of time required to image the entire ATLAS-SPT dataset. This was achieved by distributing the imaging tasks to compute nodes and sharing any input data with the Message Passing Interface (MPI) via the Python module `mpi4py`, an example of which is shown below.

## 2.4.3 Linear Mosaicking

To achieve the best possible sensitivity, the individual pointing images were linearly mosaicked together. Typically, this involves performing a weighted average of all the images to form a single output image where the weights are proportional to the primary beam attenuation.

The convolved maps were corrected for primary beam attenuation using a frequency-dependant primary beam model and mosaicked together using the task `linmos`. The maps were mosaicked as 9 smaller sub-mosaics of approximately 20,000 pixels across each coordinate axis as software limitations restricted the number of output pixels. Each sub-mosaic was constructed to overlap

```

1  import sys
2  from mpi4py import MPI
3
4  comm = MPI.COMM_WORLD
5
6  # following are specified when submitting the job
7  rank = comm.Get_rank()
8  size = comm.Get_size()
9
10 if rank == 0:
11     # distribute filenames to all nodes to avoid a potential I/O hit
12     # of all nodes reading the same file
13     with open(sys.argv[1], 'r') as fp:
14         all_files = fp.read().split('\n')[:-1]
15 else:
16     all_files = None
17
18 # evenly distribute filenames to nodes
19 all_files = comm.scatter(all_files, root=0)
20
21 # proceed with processing

```

Listing 1: An example of a Python script which distributes data efficiently between compute nodes using the Message Passing Interface (MPI) protocol. This method was used extensively throughout the processing of the ATLAS-SPT data.

by approximately one degree so that any given point inside the field boundary was covered to its maximum available sensitivity in at least one of the sub-mosaics (see Figure 2.5). A mosaic of the spectral information (i.e. the  $I\alpha$  image plane produced by `mfclean`) was also made by supplying the *alpha* option to `linmos`.

```

Task:  linmos

in     = @submosaic_1.in
out    = submosaic_1.linmos

bw     = 2

cutoff = 0.2

options = alpha

```

A final mosaic of the entire ATLAS-SPT field was created by trimming the attenuated edges of the sub-mosaics along the centre of the overlapping regions and concatenating the results into a single image. The trimming and concatenating was performed along RAs  $23^{\text{h}}$ ,  $23^{\text{h}}20^{\text{m}}$ ,  $23^{\text{h}}40^{\text{m}}$ , and  $24^{\text{h}}$ ; and Declinations  $-50^{\circ}$ ,  $-53^{\circ}20'$ ,  $-56^{\circ}40'$ , and  $-60^{\circ}$ .



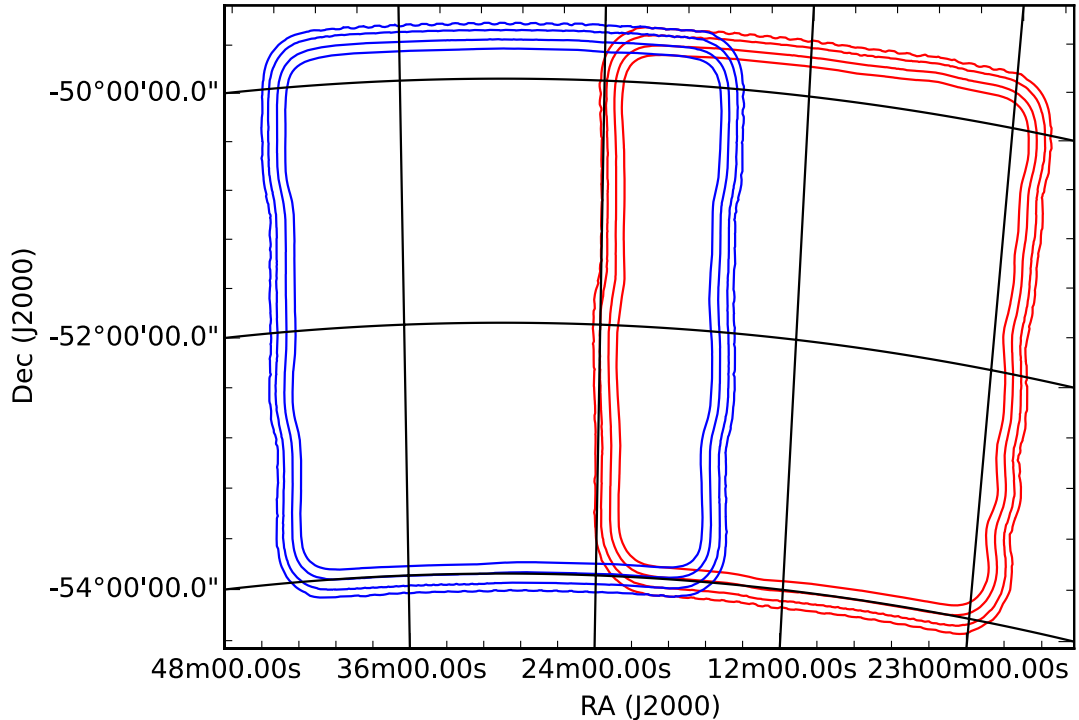


Figure 2.5: An example of the overlap between two of the 9 ATLAS-SPT sub-mosaics. The contour levels are drawn at  $3$ ,  $5$ ,  $10$  and  $20\sigma$ . A theoretical source near the edge of the left sub-mosaic will be in a position of degraded sensitivity due to primary beam attenuation. However, due to the overlap, this source would be located in an area of maximum sensitivity within the right sub-mosaic.

## 2.5 Image Analysis

In this section I characterise the final ATLAS-SPT mosaic. The full mosaic with two zoomed-in subfigures is shown in Figure 2.6. Since the mosaic is so large, barely any sources are visible in the full-size image, but numerous areas of increased noise are apparent. The first subfigure (from left to right) shows an example of a bright source which was difficult to deconvolve and its effect on the surrounding image area. The second subfigure shows an example of the complex sources resolvable with the ATLAS-SPT  $8''$  resolution.

The spatial rms of the mosaic was calculated using Python Blob Detector and Source Finder (PyBDSF) (see Chapter 3 for details). The mosaic has an average rms of  $208 \mu\text{Jy beam}^{-1}$  and a median rms of  $180 \mu\text{Jy beam}^{-1}$ . The distribution of the rms map pixel values is shown in Figure 2.7.

The rms of the mosaic is substantially higher than the original survey target of  $40 \mu\text{Jy beam}^{-1}$ . This is due to: (i) flagged data due to RFI contamination; (ii) calibration issues for pointings around strong sources, or complex sources that are difficult to model, exacerbated by the poor  $u, v$  coverage; (iii) residual beam sidelobes from incomplete deconvolution (to minimise clean bias. See Section 2.5.1). Future radio surveys should take these factors into account when

estimating the expected sensitivity and prioritise good  $u, v$  coverage to mitigate imaging issues.

The final angular resolution is  $8 \times 8''$  as determined by the common convolving Gaussian described in Section 2.4.1.

### 2.5.1 Clean Bias

Clean bias is the systematic suppression of source flux density caused by cleaning noise peaks (Condon et al., 1998). This occurs during deconvolution when clean components are placed on pixels where there are no real sources, causing flux to be removed from real sources elsewhere in the image as the beam response is subtracted. The amount of flux removed from the real source is proportional to the sidelobe amplitude which may be up to 0.2 in most ATLAS-SPT pointings (see Figure 2.3). The outcome is that flux is redistributed from real sources to noise. Clean bias can affect all sources nearly independent of flux density, but fainter sources are more affected. The underlying cause is high noise and synthesised beam sidelobe amplitudes. Due to the poor  $u, v$  coverage of each pointing, both factors exist in the ATLAS-SPT images.

One can test for clean bias by injecting simulated sources with known positions and flux densities into a visibility dataset and repeating the imaging process. The flux densities of the simulated sources are then measured and compared with their known input flux density. Clean bias was measured in the ATLAS-SPT image following the same methodology used in Franzen et al. (2015) which is summarised here.

Using `uvmodel`, 132 simulated point sources were added to the visibilities of a typical ATLAS-SPT pointing at random positions within the clean area (i.e. the inner 66% of the dirty map). The simulated source positions were chosen such that the separation between each source, either real or simulated, was at least  $1'$ . The flux density distribution of the simulated sources is given in Table 2.2 in units of the signal-to-noise ratio (SNR). The pointing was then imaged using the same method described in Section 2.4.1 and the simulated source flux densities were extracted using `imfit`. This simulation was repeated 30 times to improve statistics. The ratio of extracted flux density  $S_{\text{ext}}$  to injected flux density  $S_{\text{in}}$  was calculated for all sources in each simulation.

```
Task:   uvmodel
vis     = spt1_1.uv
options = add
flux    = <rms*SNR>
offset  = <dRA>, <dDEC>
out     = spt1_1.sim
```

```

Task:   imfit
in      = spt1_1.sim.restor
object  = point
spar    = <rms*SNR>,<dRA>,<dDEC>
fix     = x,y

```

SNR	$N$
100	1
50	1
30	2
20	3
16	5
12	10
10	10
9	15
8	15
7	15
6	15
5	40
Total	132

Table 2.2: The flux density distribution of simulated sources injected into the visibility data of a typical ATLAS-SPT pointing to test for clean bias in units of the SNR.

The initial results indicated that the pointings were severely affected by clean bias. Simulated sources with  $\text{SNR} = 5$  were bias low by as much as 30%. This result made it apparent that the PSF sidelobes were too significant to simply clean the primary beam area of each pointing to a cutoff of  $5\sigma$ .

One solution would be to clean to a more shallow depth, but this would result in a final image with degraded sensitivity as the image noise would have significant sidelobes. Instead, a catalogue of sources was produced using the clean bias affected image in order to repeat the imaging process while restricting deconvolution to the locations of these sources. Note that the source positions within the clean bias affected image are correct, but the flux densities are biased low. The clean bias analysis was repeated on the new image formed with restricted deconvolution and the results show that this approach significantly decreased the effect (see Figure 2.8).

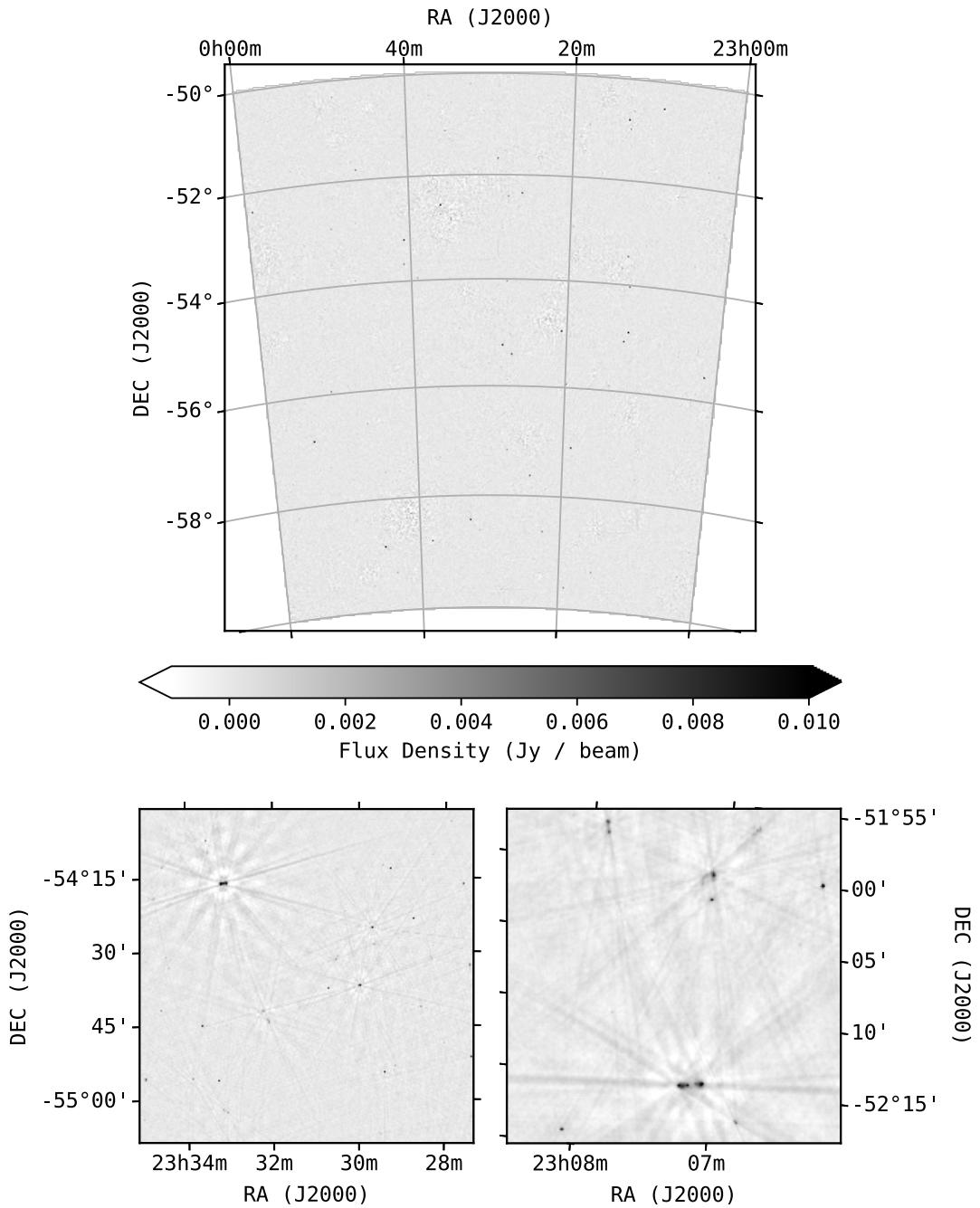


Figure 2.6: The ATLAS-SPT final mosaic with two zoomed-in subfigures. Note that due to the size of the mosaic, barely any sources are visible in the main figure. The purpose of including the mosaic is to show the full extent of the mosaic used in further analysis and also make apparent the varying noise due to strong or complex sources. The first subfigure (left to right) shows an example of increased noise caused by incomplete deconvolution of a bright source; the second subfigure shows examples of the complex source morphologies resolvable in the ATLAS-SPT mosaic.

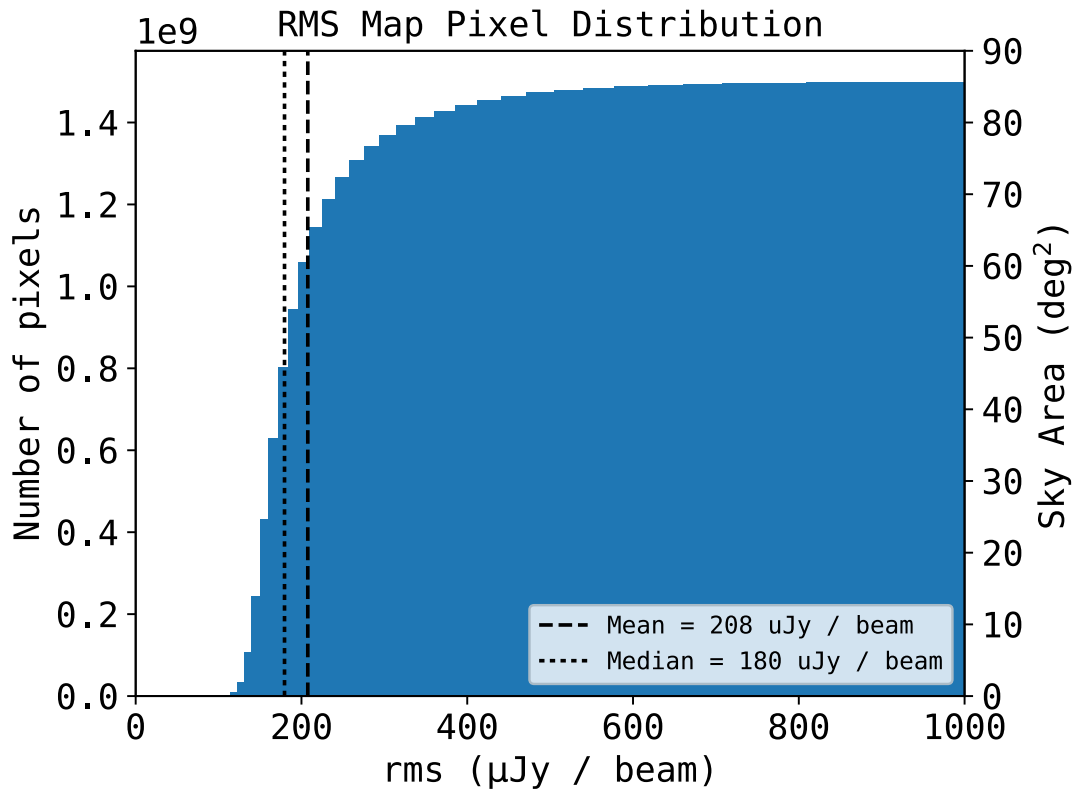


Figure 2.7: The cumulative histogram of pixel values for the rms map of the ATLAS-SPT mosaic as calculated by PyBDSF. The mean rms is shown with a vertical dashed line and the median rms is shown with a vertical dotted line. There are very few pixels that have values above  $1000 \mu\text{Jy beam}^{-1}$  and are not visible in the figure. These pixels are from areas of the mosaic where PyBDSF has increased the resolution of the rms map to capture artefacts around strong sources. The approximate sky area below a given rms value is shown on the right ordinate axis.

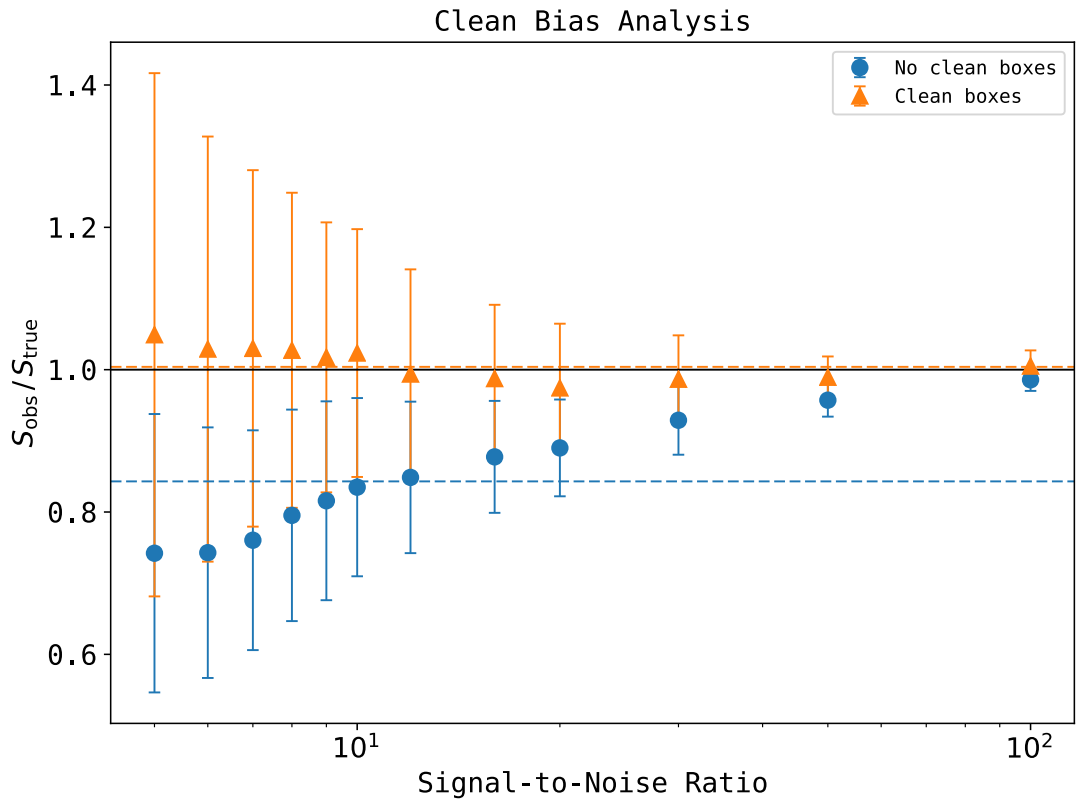


Figure 2.8: Results of the clean bias analysis. Each marker indicates the median ratio between the extracted and injected flux densities of the simulated sources defined in Table 2.2. The error bars indicate the standard deviation of the flux density ratios for all sources at each SNR value. The black solid line is drawn at  $y = 1$  and the dashed lines are the average of the median values. These results indicate that using clean boxes to restrict deconvolution to the locations of sources produces negligible clean bias in the final image.

## Chapter 3

# Radio Catalogues

This chapter is based on work in preparation for submission to *Monthly Notices of the Royal Astronomical Society*.

The final mosaic image described in Section 2.4 was processed using the source-finding software PyBDSF (Mohan and Rafferty, 2015). In this chapter, I give an overview of the functionality of PyBDSF, provide the output catalogue of radio sources from the ATLAS-SPT mosaic, assess the completeness and accuracy of the catalogue, compare the results to Butler et al. (2017), describe the extraction of spectral indices for each component and provide spectral indices for each catalogue source above a given reliability threshold, and present radio source counts for the survey area.

### 3.1 Source Extraction

Source extraction is the process of fitting Gaussian components to pixels of an image. This is appropriate as real sky emission in radio interferometric data is convolved with a Gaussian fit to the synthesised beam after the cleaning process (as described in Section 2.4). Here, I outline the basic methodology employed by PyBDSF to extract sources from an input image.

The input image is read in and some basic pixel value statistics are computed. For accurate source detections, the rms noise (analogous to sensitivity) across the image must be determined. PyBDSF estimates the spatial rms by computing the clipped rms within a sliding box that moves across the image. The size of this box may be automatically determined or defined by the user. For the ATLAS-SPT source extraction, I found that using an rms box size of 200 px stepped by 50 px produced the best results: smaller sizes produced an rms map that was too sensitive to real extended emission resulting in missed sources; and larger sizes resulted in noise variations due to image artefacts being smoothed out resulting in spurious detections. An option was also

enabled to increase the resolution of the rms map around bright sources to reduce the likelihood of the software misidentifying artefacts as sources.

With an rms map of the entire image produced, the software then locates all pixels above a given pixel threshold defined in units of rms, or  $\sigma$ . These pixels are then iteratively flood-filled to produce ‘islands’; a process whereby surrounding contiguous pixels are added to the island provided their values are greater than a given island threshold (which is less than the pixel threshold). Islands are merged as necessary. For the ATLAS-SPT source extraction, the pixel threshold was set to  $5\sigma$  and the island boundary threshold to  $3\sigma$ . These thresholds were chosen such that the output catalogue of sources would be highly complete.

The pixel islands are then fitted with multiple Gaussian components. The software estimates the initial number of components in the island based on the size of the island, the size of the synthesised beam (i.e. an unresolved source in the image), and the number of peaks in the island. The Gaussian components are fitted simultaneously using the Levenberg-Marquardt algorithm. Each component is checked against a list of flagging parameters to determine its viability (for example if it is much larger than the beam or the island). If any of the components within the island are flagged, the number of components is decreased by one and the fitting is attempted again. This process repeats until either no components are flagged or the island has no components in which case the entire island is disregarded. Approximately 4% of the originally detected islands were discarded, with the usual cause being that the island was placed around a strong artefact in which case all the putative components are flagged due to their unrealistic properties (e.g. highly eccentric components).

The final step is to group the Gaussian components into meaningful sources. There are a number of parameters which affect how this is performed, but I found that simply grouping components based on their island gave good results. However, this does mean that sources made up of disjoint components such as separated radio-doubles (sources consisting of two lobes) or radio-triples (sources consisting of a compact core and two lobes) are often classified as individual sources.

## 3.2 Radio Source Catalogue

The ATLAS-SPT radio source catalogue of sources is presented in Table 3.1. There are a total of 6067 sources formed from 7246 Gaussian components. Errors are fitting errors from Condon (1997), with calibration error estimates added in quadrature to  $\sigma_{\text{RA}}$ ,  $\sigma_{\text{DEC}}$ ,  $\sigma_S$ , and  $\sigma_{S_p}$  (see Section 3.2.1.3. The column names and descriptions are given below:

- SID: a unique number that identifies the source, starting from zero



- RA: the right ascension of the source in hours, minutes and seconds
- $\sigma_{\text{RA}}$ : the error on the right ascension of the source, in arcseconds
- DEC: the declination of the source (for the equinox of the image), in degrees, arcminutes and arcseconds.
- $\sigma_{\text{DEC}}$ : the 1- $\sigma$  error on the declination of the source, in arcseconds
- $S$ : the raw total integrated Stokes I flux density of the source at the reference frequency, in mJy
- $\sigma_S$ : the 1- $\sigma$  error on the total flux density of the source, in mJy
- $S_p$ : the raw peak Stokes I flux density per beam of the source, in mJy/beam
- $\sigma_{S_p}$ : the 1- $\sigma$  error on the peak flux density per beam of the source, in mJy/beam
- $\Theta_{\text{Maj}}$ : the FWHM of the deconvolved major axis of the source, in arcseconds
- $\sigma_{\Theta_{\text{Maj}}}$ : the 1- $\sigma$  error on the FWHM of the deconvolved major axis of the source, in arcseconds
- $\Theta_{\text{Min}}$ : the FWHM of the deconvolved minor axis of the source, in arcseconds
- $\sigma_{\Theta_{\text{Min}}}$ : the 1- $\sigma$  error on the FWHM of the deconvolved minor axis of the source, in arcseconds
- $\Theta_{\text{PA}}$ : the position angle of the deconvolved major axis of the source measured east of north, in degrees
- $\sigma_{\Theta_{\text{PA}}}$ : the 1- $\sigma$  error on the position angle of the deconvolved major axis of the source, in degrees
- $\sigma_{\text{rms}}$ : the average background rms value of the island surrounding the source, in mJy/beam
- $\alpha$ : the total integrated spectral index of the source
- Type: a character code that indicates the source structure. 'S' is a source consisting of a single Gaussian component; 'C' is a source consisting of a single Gaussian component from an island which contained other sources; 'M' is a source composed of multiple Gaussian components.

Table 3.1: The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
0	23 59 43.54	0.16	-50 10 08.64	0.17	11.406	0.720	10.277	0.603	3.67	0.19	1.52	0.17	114.52	6.20	0.206	-1.15	S
1	23 59 55.90	0.31	-50 48 39.03	0.34	3.694	0.410	2.957	0.274	4.80	0.69	3.42	0.68	142.86	54.71	0.211	–	S
2	23 59 47.41	0.14	-50 42 33.82	0.15	29.104	1.647	28.185	1.567	0.00	0.07	0.00	0.06	0.00	179.97	0.226	0.48	S
3	23 59 45.00	0.71	-50 44 19.95	0.79	2.928	0.366	1.542	0.244	9.69	1.92	6.02	1.47	133.55	30.05	0.211	–	S
4	23 59 46.08	0.19	-50 50 35.23	0.21	6.313	0.490	5.752	0.377	3.62	0.33	1.16	0.29	147.32	14.83	0.201	–	S
5	23 59 40.92	1.30	-50 51 02.41	2.09	6.728	0.409	0.970	0.162	30.41	5.26	12.57	2.23	146.80	9.71	0.181	–	S
6	23 59 33.45	0.37	-50 47 53.35	0.39	4.449	0.389	2.638	0.251	7.73	0.87	5.94	0.79	123.77	33.53	0.189	–	S
7	23 59 39.76	0.23	-51 00 39.66	0.26	28.535	1.628	7.715	0.494	11.62	0.50	10.34	0.42	77.67	13.68	0.253	–	M
8	23 59 48.49	0.96	-51 13 01.37	2.27	3.496	0.293	0.868	0.187	21.16	5.19	8.81	2.25	171.82	15.13	0.186	–	S
9	23 59 22.03	0.76	-50 33 00.69	1.02	2.547	0.319	1.216	0.215	10.99	2.37	6.44	1.70	150.12	28.22	0.189	–	S
10	23 59 28.93	0.81	-50 46 20.08	0.69	2.454	0.318	1.312	0.213	8.95	1.90	6.40	1.55	97.89	36.93	0.185	–	S
11	23 59 26.67	0.55	-50 46 40.72	2.17	3.301	0.450	0.982	0.201	0.00	5.21	0.00	0.71	0.00	12.73	0.193	–	M
12	23 59 33.90	0.56	-51 01 07.80	0.58	6.047	0.500	2.623	0.309	9.63	1.35	9.16	1.25	106.20	173.93	0.252	–	S
13	23 59 37.06	0.15	-51 06 41.64	0.17	14.081	0.852	12.282	0.709	3.88	0.16	2.36	0.15	147.19	8.11	0.208	-0.23	S
14	23 59 28.64	1.19	-50 59 35.41	1.01	2.696	0.342	1.140	0.235	11.48	2.88	7.81	2.20	107.01	38.12	0.211	–	S
15	23 58 57.53	0.80	-50 09 42.07	0.69	1.452	0.310	1.078	0.198	6.59	1.95	2.79	1.46	107.57	35.66	0.180	–	S
16	23 59 34.54	0.48	-51 16 16.99	0.57	3.148	0.375	1.962	0.247	7.19	1.24	5.53	1.11	14.49	41.64	0.206	–	S
17	23 59 26.74	1.04	-51 09 25.41	1.33	2.734	0.300	0.985	0.205	12.26	2.95	9.69	2.55	7.88	55.93	0.185	–	S
18	23 59 32.51	1.19	-51 21 04.54	1.39	2.963	0.324	1.009	0.223	12.15	3.25	10.70	2.78	3.10	119.74	0.203	–	S
19	23 59 35.21	0.66	-51 28 42.64	1.06	6.504	0.454	1.836	0.244	16.96	2.50	9.60	1.39	12.01	10.06	0.219	–	S
20	23 59 24.23	0.25	-51 11 56.16	0.23	4.493	0.411	3.886	0.292	4.32	0.49	1.72	0.41	94.64	15.24	0.193	–	S
21	23 59 36.88	0.71	-51 31 00.69	1.48	3.250	0.419	1.432	0.285	13.32	3.38	5.35	1.64	0.08	16.37	0.261	–	S
22	23 59 07.52	1.19	-50 59 30.32	0.97	4.927	0.349	1.303	0.191	20.41	3.35	8.32	1.40	117.84	7.80	0.181	–	S
23	23 59 22.66	0.24	-51 24 43.15	0.33	9.614	0.613	4.736	0.341	11.49	0.72	5.32	0.41	152.93	0.87	0.205	–	S
24	23 59 46.70	0.49	-52 02 13.11	0.61	2.804	0.488	2.167	0.313	5.49	1.32	3.27	1.16	171.09	48.81	0.276	–	S
25	23 58 37.39	0.14	-50 16 27.18	0.15	102.277	5.632	100.523	5.531	1.57	0.01	0.32	0.01	162.85	178.38	0.163	-0.42	S
26	23 58 46.62	0.14	-50 35 44.35	0.15	50.979	2.828	34.053	1.883	8.07	0.07	4.29	0.05	121.56	1.41	0.196	-1.00	M
27	23 59 25.60	0.69	-51 37 02.85	0.70	4.287	0.516	2.268	0.343	8.37	1.69	7.01	1.49	43.32	47.81	0.295	–	S
28	23 58 40.54	0.15	-50 32 49.53	0.16	20.348	1.168	18.388	1.031	3.71	0.10	1.38	0.09	130.45	0.44	0.195	-0.78	S
29	23 58 44.69	0.94	-50 42 16.49	0.93	2.074	0.264	0.958	0.179	9.38	2.34	8.42	2.01	104.34	128.70	0.158	–	S
30	23 58 53.64	0.72	-50 58 22.36	1.07	1.663	0.296	1.002	0.197	9.17	2.46	4.18	1.62	154.72	28.04	0.176	–	S
31	23 58 57.39	0.14	-51 06 07.14	0.15	66.154	3.654	65.743	3.621	0.00	0.02	0.00	0.02	0.00	4.10	0.194	-0.02	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
32	23 59 26.12	0.14	-51 55 54.10	0.15	142.924	7.979	130.214	7.208	3.48	0.06	1.34	0.05	157.29	178.00	0.798	-0.63	S
33	23 58 59.24	1.31	-51 15 32.37	1.08	3.294	0.302	1.017	0.198	14.30	3.15	10.40	2.42	102.14	35.08	0.182	-	S
34	23 59 56.20	0.14	-52 42 26.61	0.15	37.624	2.150	35.722	1.994	2.12	0.08	1.63	0.08	144.03	122.90	0.338	-0.60	S
35	23 59 33.39	0.17	-52 09 39.98	0.18	11.402	0.750	9.780	0.593	3.90	0.23	2.71	0.22	127.55	19.00	0.242	-0.08	S
36	23 59 57.15	0.92	-52 45 14.38	1.17	15.788	0.971	2.928	0.405	19.97	2.71	14.39	2.11	152.46	21.62	0.395	-	S
37	23 59 41.43	0.14	-52 25 23.94	0.15	71.406	3.962	69.240	3.820	1.84	0.04	0.96	0.04	149.06	4.97	0.302	-0.52	S
38	23 58 11.57	0.23	-50 09 58.27	0.22	14.268	0.858	6.178	0.382	11.73	0.52	3.93	0.24	33.46	3.56	0.175	-	M
39	23 59 32.97	0.44	-52 24 02.27	0.54	5.231	0.633	3.421	0.416	7.13	1.18	4.71	1.01	156.02	32.90	0.346	-	S
40	23 59 47.03	0.88	-52 47 12.85	1.61	17.841	1.057	2.630	0.374	25.80	3.71	14.44	2.08	172.83	10.25	0.398	-	S
41	23 58 26.22	0.59	-50 42 39.15	0.56	2.211	0.259	1.285	0.171	8.02	1.40	5.97	1.22	110.48	40.34	0.144	-	S
42	23 58 54.88	0.41	-51 30 05.94	0.32	9.116	0.637	4.902	0.323	13.98	1.08	0.00	0.32	140.60	4.49	0.178	-	M
43	23 59 30.31	0.15	-52 24 42.05	0.16	31.076	1.829	30.399	1.714	1.68	0.10	0.47	0.10	171.55	21.29	0.376	-0.21	S
44	23 58 07.23	0.23	-50 13 02.43	0.28	3.988	0.346	3.180	0.241	5.20	0.53	3.03	0.44	0.29	17.52	0.158	-	S
45	23 58 38.29	0.78	-51 04 43.62	1.05	1.392	0.322	0.963	0.209	7.46	2.40	3.37	1.78	151.90	41.46	0.190	-	S
46	23 59 45.60	0.74	-52 50 50.78	0.29	77.254	4.476	14.835	0.952	21.74	1.72	6.99	0.57	0.13	5.57	0.490	-	M
47	23 58 54.31	0.30	-51 34 49.36	0.35	4.383	0.412	3.072	0.274	6.23	0.72	4.46	0.65	163.98	30.19	0.202	-	S
48	23 59 58.79	0.24	-53 15 20.44	0.24	10.365	0.874	8.299	0.614	4.33	0.46	3.74	0.44	114.71	93.29	0.392	-	S
49	23 58 31.23	0.27	-51 04 44.00	0.40	6.202	0.449	3.316	0.272	10.15	0.86	5.26	0.54	163.24	5.16	0.188	-	S
50	23 59 48.60	0.14	-53 06 57.13	0.15	95.681	5.396	73.179	4.065	6.00	0.09	1.83	0.06	166.69	1.96	0.571	-1.16	M
51	23 59 48.31	0.51	-53 07 43.56	0.23	23.293	1.715	10.138	0.778	0.00	1.16	0.00	0.42	0.00	6.41	0.542	-	M
52	23 59 47.40	0.69	-53 09 51.43	2.26	19.221	1.366	2.819	0.474	18.80	5.32	4.44	1.56	87.36	17.35	0.447	-	M
53	23 58 30.19	0.83	-51 13 24.88	0.56	12.815	0.740	2.380	0.233	21.12	2.03	13.66	1.18	74.86	5.38	0.208	-	S
54	23 57 46.87	0.69	-50 02 24.59	0.95	3.342	0.286	1.243	0.179	13.26	2.27	8.38	1.45	20.82	16.76	0.156	-	S
55	23 59 12.17	0.33	-52 24 05.34	0.24	255.456	17.473	149.185	9.246	13.36	0.78	1.52	0.26	22.24	3.57	4.263	-	M
56	23 57 59.85	0.90	-50 30 38.69	0.99	2.269	0.266	0.987	0.180	10.92	2.33	7.98	2.02	133.16	50.68	0.159	-	S
57	23 58 02.99	0.32	-50 48 42.69	0.36	7.275	0.475	3.300	0.259	11.79	0.87	6.49	0.54	135.35	3.98	0.172	-	S
58	23 59 05.50	0.19	-52 33 37.25	0.26	22.151	1.364	11.088	0.663	11.38	0.53	2.63	0.22	60.98	3.31	0.259	-0.77	M
59	23 59 12.12	0.35	-52 43 39.32	0.43	4.535	0.548	3.414	0.360	5.74	0.92	3.45	0.77	177.98	27.50	0.292	-	S
60	23 57 32.03	0.30	-50 04 05.42	0.36	2.425	0.307	2.116	0.203	4.25	0.75	1.68	0.65	11.32	29.55	0.162	-	S
61	23 58 02.90	0.72	-50 59 24.27	0.70	1.540	0.304	1.112	0.196	6.28	1.74	3.85	1.51	117.45	54.54	0.176	-	S
62	23 59 59.64	0.50	-53 59 11.28	0.51	2.099	0.450	1.905	0.279	2.79	1.17	2.35	1.13	129.70	173.85	0.253	-	S
63	23 58 48.71	0.62	-52 17 49.48	0.68	2.688	0.474	1.897	0.308	5.73	1.57	4.75	1.40	21.97	93.38	0.272	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
64	23 58 17.44	0.61	-51 31 11.39	0.55	2.407	0.272	1.402	0.178	9.93	1.64	3.79	0.91	119.16	10.80	0.151	–	S
65	23 58 12.07	0.48	-51 23 32.03	0.59	4.599	0.359	1.950	0.216	10.60	1.28	8.56	1.14	176.32	34.83	0.173	–	S
66	23 58 41.35	0.56	-52 10 10.79	0.61	3.186	0.407	1.936	0.269	6.89	1.38	6.23	1.29	169.10	174.11	0.228	–	S
67	23 58 59.09	0.14	-52 43 06.89	0.15	33.001	1.889	31.069	1.737	2.34	0.08	1.66	0.08	91.59	14.71	0.305	-0.70	S
68	23 58 02.49	1.09	-51 17 02.81	0.91	2.180	0.300	1.061	0.203	11.68	2.88	5.27	1.61	116.10	19.70	0.182	–	S
69	23 59 55.34	0.30	-54 06 53.36	0.51	6.851	0.531	3.519	0.325	10.88	1.14	4.66	0.61	1.43	3.76	0.245	–	S
70	23 58 41.89	0.20	-52 23 16.59	0.18	17.355	1.197	11.119	0.686	0.00	0.35	0.00	0.22	0.00	5.50	0.311	–	M
71	23 58 03.56	0.54	-51 25 04.03	0.57	3.104	0.327	1.700	0.214	8.24	1.28	6.69	1.22	132.33	67.85	0.177	–	S
72	23 59 23.41	0.37	-53 29 52.77	0.44	17.566	1.235	7.721	0.704	10.68	0.99	7.65	0.79	148.60	14.79	0.519	–	S
73	23 59 38.52	3.11	-53 51 23.18	0.35	14.091	1.150	1.928	0.370	0.00	7.32	0.00	0.74	0.00	10.26	0.355	–	M
74	23 57 54.51	0.55	-51 15 20.56	0.42	5.124	0.412	2.466	0.252	11.54	1.37	5.56	0.76	107.48	6.70	0.200	–	S
75	23 59 20.55	0.64	-53 29 10.40	0.53	22.174	1.389	6.273	0.632	15.22	1.57	10.60	1.05	55.73	8.41	0.517	–	S
76	23 57 50.85	0.42	-51 11 15.01	0.43	2.670	0.337	1.966	0.221	5.35	0.96	4.48	0.91	108.15	90.61	0.182	–	S
77	23 57 36.54	1.15	-50 50 40.47	1.02	3.715	0.293	1.071	0.177	16.72	3.09	9.63	1.85	117.83	17.07	0.164	–	S
78	23 58 41.58	0.16	-52 38 21.28	0.17	17.150	1.058	13.600	0.805	4.71	0.21	3.56	0.19	104.80	11.41	0.284	-0.73	S
79	23 57 14.11	1.03	-50 15 32.41	0.85	2.438	0.268	1.053	0.179	12.24	2.74	6.58	1.49	54.20	16.25	0.160	–	S
80	23 57 43.63	0.37	-51 07 07.13	0.38	17.886	1.073	4.801	0.350	14.78	1.00	7.37	0.55	128.94	7.55	0.230	–	M
81	23 59 31.90	0.68	-53 53 13.30	0.58	3.788	0.519	2.303	0.343	7.34	1.54	5.56	1.33	78.41	46.74	0.295	–	S
82	23 58 29.17	0.42	-52 22 30.97	0.44	2.402	0.455	2.267	0.285	2.68	1.00	1.06	0.89	128.28	111.63	0.252	–	S
83	23 57 40.13	1.57	-51 06 42.88	1.41	4.267	0.357	1.059	0.227	16.78	3.89	12.04	3.00	113.06	38.22	0.219	–	S
84	23 59 45.29	0.77	-54 18 17.11	0.70	2.583	0.432	1.648	0.285	7.40	1.90	4.50	1.43	49.84	33.17	0.252	–	S
85	23 59 05.33	0.47	-53 23 30.06	0.42	8.368	0.777	4.726	0.501	8.60	1.11	5.61	0.86	109.86	18.47	0.396	–	S
86	23 58 10.04	0.15	-52 09 58.24	0.16	14.573	0.868	12.543	0.719	3.70	0.15	2.76	0.14	35.02	8.63	0.196	-0.50	S
87	23 57 23.07	0.74	-50 54 51.49	0.76	1.160	0.314	0.977	0.195	4.61	1.83	2.37	1.61	126.08	87.04	0.181	–	S
88	23 56 56.19	1.43	-50 12 13.70	1.02	2.054	0.262	0.818	0.181	12.09	3.40	8.20	2.34	78.78	33.23	0.165	–	S
89	23 59 36.53	0.16	-54 23 24.51	0.17	13.907	0.854	11.573	0.678	4.32	0.19	2.77	0.17	178.60	5.60	0.224	-1.08	S
90	23 59 32.84	0.25	-54 23 24.08	0.25	4.883	0.457	4.110	0.319	4.21	0.51	2.55	0.45	56.37	22.81	0.217	–	S
91	23 57 33.83	0.75	-51 24 16.63	0.82	1.949	0.276	1.077	0.185	8.96	1.99	5.84	1.61	134.13	39.83	0.162	–	S
92	23 57 36.52	0.35	-51 32 59.80	0.55	3.744	0.323	1.988	0.204	10.16	1.23	5.27	0.77	173.88	9.40	0.160	–	S
93	23 58 04.92	0.84	-52 18 17.56	0.61	2.844	0.441	1.801	0.288	9.03	2.14	2.36	1.10	58.07	13.95	0.257	–	S
94	23 59 12.62	0.97	-54 03 06.08	0.65	7.630	0.490	1.851	0.230	17.46	2.29	11.29	1.45	73.15	10.99	0.208	–	S
95	23 57 51.66	0.22	-52 02 16.03	0.25	4.577	0.419	4.015	0.299	3.84	0.46	2.00	0.41	21.28	22.84	0.196	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
96	23 57 29.62	0.57	-51 28 13.04	0.62	2.167	0.276	1.303	0.182	7.39	1.41	5.97	1.31	143.72	89.88	0.155	–	S
97	23 59 04.88	1.61	-53 55 49.80	1.82	5.074	0.375	1.038	0.218	20.93	4.99	11.53	2.62	33.55	17.68	0.224	–	S
98	23 58 05.80	1.28	-52 28 42.19	1.10	4.636	0.472	1.576	0.318	13.15	3.19	9.51	2.29	55.45	31.57	0.290	–	S
99	23 57 12.98	2.00	-51 04 28.15	1.28	5.618	0.355	0.890	0.160	26.27	5.08	13.14	2.45	104.71	13.18	0.173	–	S
100	23 57 27.96	0.95	-51 29 33.27	0.71	4.163	0.485	1.479	0.175	11.90	2.54	3.26	1.07	26.96	15.84	0.155	–	M
101	23 59 33.07	0.90	-54 37 13.18	1.27	2.991	0.350	1.207	0.238	12.88	3.06	6.87	1.87	150.35	22.08	0.215	–	S
102	23 58 48.59	0.14	-53 35 34.12	0.15	55.754	3.172	53.726	2.993	2.37	0.08	0.00	0.07	111.67	2.72	0.470	0.05	S
103	23 57 51.00	0.15	-52 08 15.17	0.16	15.645	0.915	15.173	0.854	1.68	0.10	1.12	0.10	31.47	122.13	0.179	-0.48	S
104	23 57 10.20	0.60	-51 02 58.57	0.72	2.069	0.296	1.273	0.196	7.43	1.57	5.59	1.45	165.67	65.88	0.170	–	S
105	23 59 57.60	0.65	-55 18 27.95	1.19	8.436	0.576	2.268	0.300	19.71	2.86	7.86	1.20	155.04	5.79	0.280	–	S
106	23 56 48.69	0.93	-50 30 34.57	1.30	3.105	0.319	1.127	0.214	13.57	3.11	8.42	1.99	20.30	24.07	0.194	–	S
107	23 57 19.47	0.63	-51 23 38.33	0.74	1.377	0.250	0.965	0.162	6.59	1.67	4.11	1.45	145.59	53.81	0.144	–	S
108	23 58 55.55	0.38	-53 56 40.45	0.38	4.309	0.428	2.877	0.281	7.31	0.96	3.71	0.66	41.15	10.81	0.218	–	S
109	23 56 52.40	0.48	-50 53 46.11	0.65	3.065	0.346	1.830	0.226	10.08	1.62	3.28	0.86	143.76	9.79	0.191	–	S
110	23 56 39.12	0.16	-50 32 02.53	0.19	13.390	0.806	9.702	0.573	7.16	0.26	2.72	0.17	166.12	179.14	0.197	-1.04	S
111	23 56 31.59	0.23	-50 19 25.55	0.48	7.355	0.494	3.526	0.278	13.46	1.07	3.85	0.43	1.37	0.44	0.192	–	S
112	23 59 08.70	0.16	-54 27 42.87	0.17	11.854	0.721	9.786	0.571	4.31	0.18	3.00	0.16	175.01	7.21	0.182	-0.32	S
113	23 58 00.30	0.27	-52 48 01.00	0.28	34.579	2.165	12.276	0.852	11.82	0.69	4.53	0.35	129.05	5.52	0.519	–	M
114	23 59 26.71	0.67	-54 54 51.23	0.71	2.052	0.526	1.730	0.328	3.91	1.64	2.96	1.53	155.63	173.96	0.302	–	S
115	23 58 06.49	0.15	-53 00 34.57	0.16	39.811	2.398	37.859	2.160	2.61	0.13	0.61	0.12	115.90	8.38	0.567	-0.76	S
116	23 58 21.00	0.20	-53 24 07.06	0.21	28.476	1.795	17.875	1.143	7.35	0.38	4.94	0.29	38.35	3.15	0.542	–	S
117	23 57 11.83	0.63	-51 35 16.59	0.77	2.057	0.287	1.199	0.190	8.28	1.74	5.62	1.47	151.64	44.23	0.165	–	S
118	23 57 01.61	0.14	-51 23 25.57	0.15	21.063	1.190	19.478	1.084	2.80	0.07	1.82	0.07	175.81	6.50	0.159	-0.45	S
119	23 59 05.66	0.75	-54 34 19.23	0.81	2.713	0.321	1.333	0.214	9.91	2.08	6.32	1.44	34.16	22.95	0.187	–	S
120	23 58 21.28	0.59	-53 29 59.89	0.74	3.287	0.715	2.585	0.454	5.36	1.66	2.87	1.39	173.11	54.05	0.411	–	S
121	23 56 57.51	0.68	-51 18 14.13	0.72	1.468	0.235	0.951	0.154	7.62	1.85	4.18	1.31	38.43	27.01	0.136	–	S
122	23 56 29.09	0.44	-50 35 08.99	0.71	4.031	0.448	2.297	0.293	9.84	1.61	4.50	0.98	165.99	13.94	0.247	–	S
123	23 56 45.39	0.47	-51 02 19.74	0.25	4.287	0.451	2.279	0.214	0.00	1.06	0.00	0.46	0.00	9.21	0.174	–	M
124	23 57 08.33	1.33	-51 42 41.43	0.97	4.298	0.342	1.178	0.209	15.60	3.13	11.15	2.22	86.85	25.92	0.195	–	S
125	23 56 17.07	0.65	-50 21 49.28	0.71	2.003	0.374	1.433	0.242	5.70	1.65	4.74	1.48	147.59	174.61	0.215	–	S
126	23 56 26.00	0.77	-50 41 32.04	0.60	3.176	0.501	2.043	0.329	7.82	1.84	4.25	1.31	98.33	27.69	0.290	–	S
127	23 56 18.30	0.72	-50 31 06.86	0.54	3.899	0.362	1.804	0.232	11.18	1.77	6.62	1.12	100.57	14.72	0.195	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
128	23 57 57.41	0.21	-53 15 07.06	0.21	27.544	1.989	21.319	1.423	5.64	0.39	2.95	0.31	116.33	7.22	0.767	–	S
129	23 56 56.22	0.52	-51 36 48.97	0.56	1.562	0.272	1.222	0.175	4.95	1.29	3.67	1.16	143.47	105.03	0.154	–	S
130	23 56 25.32	0.15	-50 45 09.45	0.16	15.261	0.915	13.546	0.777	3.37	0.14	2.47	0.14	123.94	17.75	0.213	-0.52	S
131	23 57 53.27	0.14	-53 11 13.72	0.15	1547.369	85.364	1526.092	84.023	0.00	0.02	0.00	0.02	0.00	178.52	3.837	0.30	S
132	23 56 10.31	0.16	-50 21 15.53	0.18	11.108	0.713	9.795	0.582	3.93	0.22	1.90	0.18	5.10	7.71	0.215	-1.20	S
133	23 59 35.06	0.52	-55 38 27.71	0.80	5.637	0.479	2.349	0.297	12.91	1.89	6.18	1.04	154.65	8.90	0.253	–	S
134	23 56 32.97	0.30	-51 05 06.76	0.33	3.263	0.363	2.675	0.243	4.38	0.66	3.28	0.65	11.22	54.52	0.186	–	S
135	23 56 17.11	1.70	-50 41 14.02	1.35	45.629	2.515	1.822	0.185	47.05	4.20	34.66	2.96	97.46	9.33	0.293	–	S
136	23 57 34.13	0.26	-52 49 20.44	0.31	12.804	1.002	8.260	0.654	6.98	0.63	5.00	0.52	11.28	14.94	0.438	–	S
137	23 56 34.14	0.34	-51 11 35.18	0.36	2.669	0.307	2.094	0.204	5.27	0.79	3.28	0.70	128.86	34.03	0.160	–	S
138	23 58 48.93	0.30	-54 44 18.16	0.32	6.230	0.646	4.863	0.434	4.89	0.66	3.59	0.62	151.99	43.34	0.325	–	S
139	23 57 43.79	0.35	-53 10 33.40	0.36	11.708	1.675	10.468	1.089	3.63	0.80	1.48	0.72	40.70	40.54	0.903	–	S
140	23 59 13.23	0.15	-55 22 42.15	0.16	14.377	0.863	13.055	0.747	3.14	0.13	1.85	0.13	139.21	9.47	0.201	-0.55	S
141	23 59 21.42	0.22	-55 36 57.61	0.31	20.871	1.303	9.236	0.591	12.66	0.71	3.02	0.29	111.17	4.08	0.302	–	M
142	23 59 02.24	1.13	-55 11 30.33	1.63	3.666	0.334	1.089	0.218	17.29	4.18	7.85	1.90	22.98	14.29	0.209	–	S
143	23 55 48.88	1.87	-50 04 55.73	1.47	6.994	0.409	0.791	0.132	26.05	4.51	20.52	3.36	84.37	25.06	0.155	–	S
144	23 59 23.15	0.39	-55 42 02.72	0.39	2.782	0.406	2.347	0.263	4.16	0.89	2.64	0.81	127.28	61.25	0.221	–	S
145	23 57 52.17	0.76	-53 33 41.10	0.78	4.026	0.773	2.688	0.507	5.77	1.84	5.60	1.73	42.81	174.28	0.452	–	S
146	23 56 45.04	0.81	-51 47 33.19	1.22	2.808	0.281	1.057	0.186	13.62	2.92	7.59	1.69	16.89	18.24	0.167	–	S
147	23 56 56.39	0.25	-52 08 31.11	0.28	3.562	0.328	2.869	0.227	4.43	0.52	3.57	0.51	0.54	55.87	0.156	–	S
148	23 57 33.87	0.60	-53 09 17.78	0.57	5.721	0.965	4.188	0.623	6.46	1.49	3.16	1.15	119.35	31.75	0.548	–	S
149	23 58 27.48	1.08	-54 29 49.60	1.72	4.051	0.301	0.916	0.175	19.06	4.08	11.16	2.34	11.25	17.89	0.173	–	S
150	23 59 33.30	0.45	-56 00 18.08	1.04	11.025	0.675	2.627	0.283	21.29	2.41	8.48	0.95	1.09	2.67	0.257	–	S
151	23 55 57.99	1.03	-50 29 49.14	1.17	2.654	0.385	1.220	0.266	9.41	2.80	8.50	2.35	18.44	145.43	0.237	–	S
152	23 56 49.19	0.18	-51 59 45.00	0.19	8.404	0.546	6.431	0.398	5.14	0.28	3.82	0.25	24.80	10.39	0.173	–	S
153	23 56 30.83	0.16	-51 32 08.42	0.18	8.916	0.564	7.748	0.458	4.46	0.21	1.49	0.17	159.38	3.33	0.163	-0.61	S
154	23 59 31.11	0.51	-56 01 11.21	0.76	11.199	0.707	3.150	0.326	17.08	1.85	8.79	0.94	17.65	4.07	0.276	–	S
155	23 59 56.96	0.48	-56 41 51.24	0.45	4.289	0.466	2.622	0.306	6.76	1.10	5.89	0.98	102.73	116.32	0.250	–	S
156	23 59 32.59	0.17	-56 12 00.06	0.18	18.930	1.151	13.814	0.789	10.94	0.30	0.00	0.12	125.82	1.84	0.213	-0.75	M
157	23 59 12.27	0.73	-55 46 09.97	0.79	1.283	0.355	1.065	0.221	4.47	1.93	2.61	1.59	145.52	99.27	0.205	–	S
158	23 56 24.28	1.01	-51 34 14.34	0.76	2.372	0.278	1.085	0.186	11.52	2.50	6.40	1.56	105.27	21.00	0.165	–	S
159	23 59 56.90	0.41	-56 44 52.58	0.48	2.639	0.392	2.069	0.254	5.08	1.07	3.00	0.90	8.03	35.16	0.217	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
160	23 55 42.85	0.18	-50 27 35.21	0.31	81.619	4.549	34.072	1.895	21.05	0.65	9.34	0.27	90.13	2.56	0.281	-0.78	M
161	23 56 35.16	0.85	-51 56 13.15	1.20	1.809	0.263	0.874	0.179	10.31	2.73	6.60	1.98	11.41	35.44	0.160	-	S
162	23 59 02.12	0.73	-55 38 06.02	0.71	2.052	0.362	1.374	0.236	7.82	1.93	3.15	1.30	126.80	24.39	0.211	-	S
163	23 59 40.45	0.57	-56 29 00.05	0.54	2.455	0.407	1.798	0.264	5.37	1.35	4.15	1.18	49.04	68.44	0.231	-	S
164	23 58 30.26	0.62	-54 56 08.34	1.13	40.858	2.550	8.920	1.116	19.99	2.61	11.02	1.42	176.96	7.96	1.045	-	S
165	23 55 50.57	0.32	-50 44 13.32	0.36	4.136	0.377	2.756	0.248	6.74	0.75	4.94	0.69	146.08	33.79	0.183	-	S
166	23 58 09.81	0.14	-54 30 01.29	0.15	20.169	1.153	18.786	1.050	2.29	0.08	2.05	0.08	26.48	121.68	0.182	-0.79	S
167	23 55 56.05	1.02	-50 56 23.26	1.25	2.211	0.323	1.008	0.223	10.60	2.84	7.46	2.40	149.69	58.85	0.199	-	S
168	23 56 03.25	0.15	-51 12 56.98	0.16	25.106	1.470	15.531	0.875	8.14	0.16	6.56	0.13	35.12	5.02	0.189	-0.06	M
169	23 58 39.46	1.44	-55 15 36.81	1.76	7.079	0.474	1.244	0.243	20.92	4.42	14.06	2.88	25.57	21.83	0.253	-	S
170	23 58 40.60	0.24	-55 17 40.04	0.24	6.093	0.540	5.107	0.382	4.07	0.45	2.93	0.43	103.90	39.71	0.249	-	S
171	23 59 02.14	0.89	-55 47 15.80	1.08	3.680	0.346	1.282	0.227	12.43	2.52	9.44	2.04	156.68	39.51	0.203	-	S
172	23 58 31.77	0.17	-55 07 23.38	0.17	21.593	1.318	16.751	0.988	5.48	0.22	2.85	0.17	70.36	0.97	0.340	-1.23	S
173	23 56 05.25	0.72	-51 17 49.66	0.87	0.951	0.257	0.774	0.161	5.27	1.97	2.36	1.68	148.48	66.36	0.149	-	S
174	23 55 41.00	1.44	-50 34 54.23	0.99	2.046	0.304	0.925	0.210	11.73	3.58	6.26	2.03	65.80	25.33	0.191	-	S
175	23 58 21.69	0.98	-54 56 08.46	0.94	177.186	9.923	14.893	1.342	23.92	2.40	19.90	2.07	137.50	35.49	1.063	-	M
176	23 56 03.89	0.41	-51 16 34.63	0.36	2.435	0.292	1.847	0.192	5.64	0.92	3.40	0.75	83.59	25.40	0.155	-	S
177	23 58 58.52	0.67	-55 45 33.35	0.82	3.495	0.373	1.633	0.245	10.76	2.06	6.16	1.29	24.90	16.24	0.213	-	S
178	23 56 07.89	0.92	-51 25 21.00	0.98	1.847	0.248	0.884	0.169	10.20	2.40	7.00	1.95	130.67	44.81	0.149	-	S
179	23 55 36.10	0.72	-50 28 41.01	0.86	1.732	0.514	1.497	0.316	4.57	1.94	1.62	1.69	147.69	78.11	0.296	-	S
180	23 57 45.19	0.14	-54 04 26.20	0.15	148.571	8.253	125.695	6.949	4.90	0.06	1.34	0.04	109.11	176.06	0.681	-0.58	S
181	23 55 31.18	0.78	-50 23 31.28	0.98	2.875	0.371	1.410	0.250	10.55	2.32	6.41	1.70	144.80	31.96	0.220	-	S
182	23 56 04.12	0.88	-51 24 12.60	1.56	2.047	0.228	0.758	0.155	14.91	3.64	6.98	1.93	159.42	19.66	0.143	-	S
183	23 55 32.10	0.17	-50 29 10.67	0.18	14.316	0.923	11.892	0.718	4.01	0.23	3.39	0.22	37.12	22.73	0.284	-1.05	S
184	23 58 35.00	0.86	-55 19 44.51	0.82	1.368	0.341	1.013	0.218	5.67	2.13	3.75	1.76	118.51	90.74	0.199	-	S
185	23 58 36.50	0.72	-55 24 40.09	0.57	3.713	0.386	1.831	0.253	10.22	1.71	6.05	1.21	109.20	19.25	0.215	-	S
186	23 56 49.87	0.22	-52 47 13.33	0.23	14.130	1.111	11.070	0.785	4.78	0.43	3.65	0.39	43.74	21.97	0.472	-	S
187	23 59 39.97	1.23	-56 49 35.73	1.24	5.315	0.367	1.138	0.196	18.34	3.27	12.38	2.39	130.99	23.89	0.192	-	S
188	23 58 52.69	0.59	-55 47 21.21	1.07	1.345	0.342	1.034	0.214	0.00	2.47	0.00	1.33	0.00	21.13	0.200	-	S
189	23 57 45.85	0.20	-54 14 04.73	0.21	6.386	0.487	5.233	0.355	3.90	0.35	3.65	0.35	131.34	174.31	0.199	-	S
190	23 58 00.99	0.60	-54 36 58.59	0.66	2.914	0.432	1.877	0.284	7.59	1.61	4.29	1.23	138.71	29.77	0.247	-	S
191	23 58 56.67	1.06	-55 56 08.65	0.77	12.641	0.728	1.873	0.216	22.32	2.41	16.21	1.82	83.91	13.76	0.215	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
192	23 57 41.63	0.64	-54 13 26.64	0.63	1.415	0.333	1.196	0.208	4.54	1.56	2.13	1.34	122.95	66.58	0.191	–	S
193	23 58 49.87	0.59	-55 51 55.43	0.69	3.533	0.369	1.756	0.241	9.57	1.68	6.35	1.21	23.90	20.23	0.205	–	S
194	23 58 20.29	1.70	-55 12 02.47	0.49	7.310	0.649	1.528	0.262	0.00	4.02	0.00	0.96	0.00	13.11	0.248	–	M
195	23 55 54.74	0.80	-51 24 51.79	1.44	1.955	0.253	0.843	0.174	12.69	3.28	6.33	1.87	1.94	22.52	0.157	–	S
196	23 56 43.19	0.46	-52 50 17.56	0.48	14.580	0.995	5.929	0.543	13.45	1.34	6.18	0.65	38.41	3.13	0.415	–	S
197	23 55 15.29	0.21	-50 23 00.88	0.25	68.260	3.819	20.785	1.166	26.09	0.57	8.50	0.17	48.25	1.47	0.230	-0.57	M
198	23 57 05.45	0.82	-53 28 16.08	1.02	4.192	0.557	2.033	0.377	10.32	2.51	6.25	1.68	24.87	25.99	0.334	–	S
199	23 55 11.65	0.79	-50 14 00.71	0.87	1.361	0.282	0.928	0.184	6.77	2.02	4.53	1.80	135.12	73.53	0.165	–	S
200	23 55 32.51	0.77	-50 55 04.41	0.75	6.412	0.520	2.292	0.318	11.24	1.79	10.77	1.71	62.92	67.65	0.273	–	S
201	23 59 06.13	0.50	-56 23 29.35	0.73	5.469	0.413	2.025	0.241	12.46	1.65	8.32	1.15	173.16	13.51	0.202	–	S
202	23 58 26.21	0.43	-55 32 02.44	0.65	6.875	0.502	2.665	0.287	12.46	1.48	7.68	0.95	178.37	9.40	0.232	–	S
203	23 55 20.16	0.15	-50 36 01.71	0.16	17.657	1.019	16.077	0.903	3.08	0.10	2.07	0.10	155.01	11.72	0.180	-0.30	S
204	23 56 08.60	1.01	-52 01 45.98	0.93	1.879	0.248	0.888	0.168	10.69	2.68	6.42	1.72	48.38	24.96	0.150	–	S
205	23 59 53.62	0.23	-57 27 01.38	0.27	5.339	0.426	3.865	0.289	6.20	0.54	3.20	0.41	10.79	6.61	0.186	–	S
206	23 57 45.61	0.28	-54 36 37.56	0.33	2.990	0.376	2.714	0.251	0.00	0.68	0.00	0.57	0.00	22.24	0.197	–	S
207	23 57 29.08	0.14	-54 16 14.45	0.15	26.477	1.504	24.716	1.377	3.15	0.08	0.00	0.07	107.77	179.78	0.218	-0.98	S
208	23 58 07.51	0.14	-55 12 57.32	0.15	33.059	1.852	31.940	1.769	1.71	0.05	1.27	0.05	111.27	114.66	0.203	-0.48	S
209	23 59 27.64	0.20	-56 59 57.06	0.22	5.877	0.442	4.690	0.319	4.33	0.36	3.57	0.35	1.41	29.64	0.178	–	S
210	23 57 42.39	0.57	-54 37 14.52	0.53	1.964	0.359	1.561	0.229	5.57	1.42	1.84	1.05	46.91	27.89	0.204	–	S
211	23 58 39.54	0.29	-55 59 44.02	0.30	5.344	0.515	4.104	0.348	5.51	0.66	2.90	0.52	36.34	13.73	0.252	–	S
212	23 56 11.99	0.80	-52 18 35.13	0.76	1.764	0.269	1.023	0.180	8.00	1.99	5.73	1.59	49.91	40.80	0.158	–	S
213	23 59 25.65	0.52	-57 00 28.89	0.73	2.574	0.296	1.377	0.195	8.98	1.66	5.68	1.20	175.67	21.42	0.167	–	S
214	23 55 41.71	0.62	-51 28 00.96	0.76	1.783	0.256	1.075	0.170	8.18	1.74	5.16	1.40	150.29	37.77	0.147	–	S
215	23 56 08.34	1.48	-52 14 07.73	2.09	4.822	0.312	0.733	0.150	22.62	4.72	16.27	3.59	173.26	33.67	0.163	–	S
216	23 57 05.69	0.21	-53 47 55.33	0.24	9.483	0.791	7.847	0.565	4.57	0.44	2.66	0.39	165.63	17.90	0.350	–	S
217	23 54 53.33	0.94	-50 00 35.32	0.42	15.989	0.952	2.505	0.240	14.41	2.21	3.44	0.82	5.86	10.98	0.196	–	M
218	23 56 48.65	0.32	-53 22 01.13	0.31	7.243	0.707	5.314	0.473	5.16	0.67	4.55	0.65	68.29	60.95	0.350	–	S
219	23 58 34.94	0.15	-55 59 29.26	0.16	26.617	1.552	19.486	1.102	5.46	0.14	1.18	0.10	5.33	3.22	0.255	-0.57	M
220	23 59 30.57	0.23	-57 12 11.64	0.29	3.986	0.357	3.157	0.246	5.69	0.57	1.63	0.42	169.16	6.80	0.167	–	S
221	23 55 16.59	0.86	-50 49 16.73	0.76	2.667	0.423	1.596	0.280	9.27	2.26	4.07	1.39	117.59	22.50	0.250	–	S
222	23 57 24.37	0.33	-54 21 04.88	0.38	3.316	0.393	2.601	0.260	5.16	0.81	3.17	0.71	159.80	31.90	0.207	–	S
223	23 57 26.27	0.57	-54 24 52.54	0.57	1.212	0.276	1.067	0.172	3.07	1.30	2.84	1.28	90.46	174.37	0.157	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
224	23 59 30.23	0.44	-57 14 00.00	0.58	1.336	0.285	1.205	0.177	0.00	1.31	0.00	0.98	0.00	28.03	0.161	-	S
225	23 58 59.62	1.55	-56 37 23.83	1.61	6.603	0.438	1.227	0.219	23.71	4.72	10.84	2.07	36.65	10.94	0.231	-	S
226	23 58 37.59	0.62	-56 10 56.49	0.73	2.483	0.305	1.345	0.202	8.71	1.75	5.78	1.30	22.09	25.60	0.174	-	S
227	23 56 53.72	0.79	-53 44 54.15	0.70	84.584	4.845	41.994	2.347	43.21	2.43	5.34	0.31	35.56	2.80	0.416	-0.84	M
228	23 55 13.61	0.54	-50 56 46.05	0.85	15.074	0.992	4.735	0.497	19.42	2.19	6.32	0.79	145.81	3.18	0.427	-	S
229	23 55 51.06	0.23	-51 59 55.72	0.44	8.868	0.546	3.586	0.268	14.38	0.96	5.82	0.44	176.20	0.42	0.173	-	S
230	23 55 27.94	1.50	-51 19 38.18	0.89	3.188	0.281	0.994	0.180	17.27	3.75	7.76	1.71	102.50	13.65	0.169	-	S
231	23 57 28.94	0.14	-54 37 37.40	0.15	25.717	1.459	24.163	1.346	2.22	0.07	1.84	0.07	168.70	116.95	0.208	-0.69	S
232	23 55 23.60	0.51	-51 14 06.09	0.50	2.964	0.329	1.796	0.216	8.09	1.28	5.13	0.99	121.79	24.81	0.178	-	S
233	23 55 26.22	0.71	-51 18 51.60	0.70	1.915	0.294	1.191	0.194	7.49	1.79	5.13	1.42	48.32	36.96	0.170	-	S
234	23 56 49.93	0.25	-53 40 16.17	0.19	13.325	0.985	10.507	0.705	0.00	0.48	0.00	0.25	0.00	179.97	0.393	-	S
235	23 55 48.04	0.72	-51 58 04.24	0.59	3.549	0.330	1.580	0.212	10.35	1.71	7.82	1.31	69.81	25.11	0.179	-	S
236	23 55 05.75	0.81	-50 42 16.06	0.96	1.810	0.313	1.064	0.209	8.27	2.19	5.57	1.88	145.04	58.60	0.186	-	S
237	23 57 16.01	0.55	-54 21 33.59	0.53	6.024	0.442	2.371	0.254	12.24	1.40	7.88	1.00	125.12	13.10	0.204	-	S
238	23 55 09.94	0.33	-50 56 25.24	0.41	40.574	2.391	10.137	0.694	17.82	1.05	6.63	0.43	120.65	4.81	0.414	-	M
239	23 54 53.25	0.72	-50 22 44.43	0.93	1.790	0.316	1.121	0.209	7.98	2.16	4.64	1.60	21.97	35.84	0.186	-	S
240	23 56 53.96	0.78	-53 52 35.81	0.32	16.160	1.061	6.870	0.448	20.18	1.88	0.00	0.36	157.34	4.44	0.242	-	M
241	23 58 54.81	0.88	-56 42 23.19	1.01	2.389	0.377	1.253	0.256	9.28	2.49	5.83	1.85	143.79	38.56	0.228	-	S
242	23 57 06.98	1.27	-54 13 48.18	0.99	17.215	1.016	2.005	0.247	20.15	3.33	11.35	1.74	26.54	16.78	0.221	-	M
243	23 54 40.99	0.60	-50 02 38.79	0.56	2.260	0.379	1.681	0.245	6.30	1.46	3.21	1.15	114.07	33.56	0.215	-	S
244	23 55 09.10	0.17	-50 57 10.18	0.19	15.527	1.114	14.128	0.886	3.30	0.27	1.78	0.25	150.43	22.46	0.417	-	S
245	23 56 29.85	0.61	-53 16 38.42	0.59	3.441	0.555	2.402	0.362	6.11	1.46	4.40	1.26	48.53	48.39	0.316	-	S
246	23 55 02.02	0.75	-50 45 31.41	0.87	1.998	0.347	1.235	0.231	7.09	2.02	5.87	1.73	177.76	131.48	0.204	-	S
247	23 57 00.90	0.39	-54 06 11.41	0.44	2.568	0.376	2.096	0.243	4.45	0.95	3.07	0.87	19.06	54.64	0.206	-	S
248	23 59 42.56	0.75	-57 46 23.92	0.62	2.355	0.308	1.311	0.205	8.63	1.75	5.48	1.37	108.67	32.27	0.178	-	S
249	23 58 13.80	1.10	-55 52 48.19	1.23	3.313	0.355	1.159	0.242	11.61	2.94	10.12	2.50	161.67	95.00	0.219	-	S
250	23 59 02.94	0.54	-56 59 49.57	0.80	1.493	0.277	1.060	0.179	6.96	1.83	2.54	1.22	0.62	23.77	0.160	-	S
251	23 57 05.56	0.83	-54 17 54.33	0.89	2.831	0.344	1.320	0.232	9.58	2.17	7.57	1.78	32.08	44.41	0.204	-	S
252	23 58 08.66	0.14	-55 51 23.97	0.15	32.361	1.823	33.169	1.838	0.00	0.05	0.00	0.05	0.00	7.48	0.228	0.02	S
253	23 57 04.66	0.34	-54 17 30.65	0.35	3.225	0.397	2.635	0.262	4.58	0.77	2.97	0.71	133.57	46.01	0.210	-	S
254	23 59 42.36	0.63	-57 51 52.70	0.68	2.369	0.351	1.464	0.232	7.26	1.64	5.10	1.35	143.88	45.50	0.202	-	S
255	23 56 05.87	0.24	-52 47 56.27	0.20	15.116	0.964	6.548	0.440	6.82	0.48	0.00	0.29	152.60	6.99	0.254	-	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
256	23 55 06.91	0.85	-51 04 47.31	0.84	1.368	0.323	0.992	0.208	5.55	2.12	4.56	1.79	106.68	156.87	0.189	–	S
257	23 57 42.93	0.25	-55 17 46.05	0.24	4.835	0.416	3.863	0.291	4.68	0.49	3.19	0.43	50.21	20.91	0.190	–	S
258	23 59 53.02	0.31	-58 07 26.97	0.32	6.293	0.583	4.390	0.388	5.32	0.68	5.03	0.62	163.68	110.97	0.284	–	S
259	23 59 23.12	0.52	-57 31 11.12	0.78	2.069	0.354	1.428	0.229	7.61	1.81	2.27	1.13	159.98	18.49	0.204	–	S
260	23 59 55.21	0.21	-58 10 48.19	0.20	8.218	0.604	6.568	0.438	5.21	0.36	2.47	0.30	119.30	6.97	0.237	–	S
261	23 57 39.83	1.17	-55 17 19.61	0.89	2.775	0.304	1.070	0.206	12.08	2.73	8.21	2.05	99.42	34.49	0.184	–	S
262	23 54 31.44	0.33	-50 11 26.61	0.96	7.529	0.581	2.124	0.216	14.69	2.24	0.00	0.66	90.91	8.70	0.181	–	M
263	23 54 41.73	0.14	-50 30 53.03	0.15	101.085	5.573	98.399	5.416	1.94	0.02	0.46	0.02	166.11	178.84	0.220	-0.43	S
264	23 59 03.05	0.23	-57 14 56.52	0.18	6.136	0.488	4.263	0.278	0.00	0.42	0.00	0.23	0.00	5.41	0.149	–	M
265	23 56 40.93	1.68	-53 57 24.84	1.09	23.980	1.429	2.860	0.275	29.29	4.52	8.03	1.26	144.15	10.52	0.226	–	M
266	23 54 33.39	0.23	-50 16 07.03	0.26	3.871	0.374	3.504	0.266	3.42	0.47	1.67	0.44	23.96	31.13	0.179	–	S
267	23 59 17.95	0.35	-57 36 00.81	0.36	3.287	0.357	2.387	0.236	5.18	0.80	4.50	0.72	148.00	90.39	0.185	–	S
268	23 56 24.76	0.83	-53 32 51.82	0.73	1.934	0.523	1.577	0.327	5.22	1.98	2.12	1.61	109.16	58.68	0.303	–	S
269	23 57 48.31	0.81	-55 38 39.57	1.07	4.356	0.336	1.282	0.200	14.71	2.51	10.18	1.83	156.59	23.00	0.181	–	S
270	23 57 17.75	0.16	-54 57 09.43	0.16	73.801	4.162	30.754	1.730	11.95	0.19	7.95	0.13	176.86	2.38	0.365	-0.63	M
271	23 57 09.75	0.27	-54 47 04.55	0.26	6.121	0.584	5.004	0.402	4.56	0.54	2.93	0.50	95.49	28.06	0.281	–	S
272	23 55 30.61	0.96	-52 10 49.23	0.77	2.731	0.274	1.139	0.179	12.44	2.49	6.79	1.39	54.77	15.19	0.159	–	S
273	23 55 21.33	0.49	-51 55 46.21	0.52	5.062	0.392	2.247	0.235	11.12	1.36	7.10	0.88	37.76	10.67	0.186	–	S
274	23 54 54.33	0.14	-51 08 08.30	0.15	247.091	13.634	243.412	13.403	0.00	0.02	0.00	0.02	0.00	1.86	0.636	-0.33	S
275	23 54 27.29	0.19	-50 18 05.99	0.20	6.637	0.471	5.594	0.357	3.86	0.30	3.20	0.29	46.61	29.12	0.175	–	S
276	23 55 20.80	0.66	-51 56 43.83	0.69	1.890	0.289	1.190	0.191	6.33	1.61	6.19	1.50	29.21	174.80	0.166	–	S
277	23 59 00.51	0.22	-57 23 34.95	0.17	7.436	0.559	4.432	0.284	0.00	0.40	0.00	0.20	0.00	4.25	0.145	–	M
278	23 58 34.47	1.04	-56 50 52.39	0.82	1.431	0.283	0.866	0.189	7.58	2.40	5.21	1.92	89.16	64.12	0.169	–	S
279	23 56 04.56	0.69	-53 12 16.70	1.07	3.774	0.386	1.538	0.255	12.16	2.43	7.48	1.62	179.27	22.18	0.225	–	S
280	23 58 02.02	0.79	-56 09 10.37	1.05	1.914	0.297	1.025	0.200	9.52	2.55	5.09	1.62	19.68	25.10	0.179	–	S
281	23 55 13.68	0.67	-51 47 56.45	0.69	0.937	0.280	0.878	0.169	2.27	1.61	1.95	1.52	93.43	174.83	0.160	–	S
282	23 55 56.70	0.21	-53 03 50.41	0.21	6.916	0.553	6.022	0.410	3.51	0.35	2.66	0.34	77.30	37.69	0.235	–	S
283	23 54 15.71	0.15	-50 02 05.36	0.16	21.280	1.230	16.769	0.952	5.37	0.15	3.07	0.12	114.07	0.60	0.224	-1.31	S
284	23 55 08.32	0.16	-51 43 05.05	0.17	8.364	0.533	7.248	0.431	3.71	0.20	2.70	0.19	162.93	21.77	0.158	-0.83	S
285	23 56 12.92	1.17	-53 34 27.39	1.07	3.446	0.457	1.461	0.316	10.20	2.81	8.59	2.39	58.40	68.58	0.283	–	S
286	23 59 07.20	0.17	-57 40 56.90	0.17	9.543	0.618	7.984	0.483	3.69	0.22	3.27	0.21	90.26	76.19	0.193	-1.23	S
287	23 57 16.77	0.58	-55 13 07.82	0.67	2.024	0.319	1.350	0.209	6.63	1.53	4.64	1.31	152.57	52.33	0.183	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
288	23 55 25.02	0.61	-52 15 30.87	0.90	1.082	0.250	0.840	0.158	6.91	2.10	0.00	1.31	155.68	26.11	0.145	–	S
289	23 56 11.54	0.49	-53 35 12.78	0.50	4.371	0.521	2.825	0.342	7.04	1.22	4.76	0.97	39.93	26.39	0.284	–	S
290	23 54 56.83	0.69	-51 27 15.72	0.67	1.275	0.259	0.956	0.166	5.04	1.68	4.37	1.45	72.46	133.32	0.149	–	S
291	23 57 55.31	0.15	-56 10 13.05	0.16	12.903	0.775	10.862	0.627	3.92	0.16	2.88	0.15	10.64	7.81	0.182	-0.76	S
292	23 59 06.22	1.32	-57 42 31.52	0.83	1.835	0.280	0.876	0.192	10.67	2.98	5.92	1.98	82.66	30.76	0.173	–	S
293	23 56 47.56	1.67	-54 33 07.34	1.08	2.894	0.297	0.964	0.200	16.43	4.24	6.76	1.83	58.68	14.93	0.191	–	S
294	23 55 51.18	0.79	-53 04 33.56	0.75	4.212	0.403	1.784	0.261	12.32	2.13	6.79	1.33	123.93	16.48	0.226	–	S
295	23 55 07.57	0.30	-51 49 16.52	0.37	4.722	0.355	2.621	0.220	8.37	0.78	6.25	0.63	12.08	16.57	0.154	–	S
296	23 57 55.63	0.67	-56 10 58.95	1.08	1.999	0.321	1.118	0.215	9.50	2.49	4.44	1.53	165.97	23.06	0.192	–	S
297	23 55 54.53	0.17	-53 11 54.63	0.18	9.717	0.660	9.038	0.547	2.55	0.21	1.87	0.21	121.85	141.04	0.225	-0.21	S
298	23 58 04.87	0.15	-56 27 20.89	0.15	94.115	5.233	52.377	2.898	9.62	0.10	1.47	0.05	17.44	0.79	0.318	-1.21	M
299	23 58 52.44	0.17	-57 31 38.01	0.18	6.747	0.453	5.644	0.349	4.18	0.25	2.66	0.23	163.34	10.32	0.153	–	S
300	23 59 05.67	0.29	-57 48 47.94	0.26	3.807	0.418	3.322	0.285	4.02	0.58	1.78	0.52	101.15	27.19	0.212	–	S
301	23 56 16.52	0.18	-53 53 01.56	0.19	9.663	0.673	8.270	0.519	3.31	0.27	3.31	0.26	65.03	174.61	0.242	–	S
302	23 55 34.08	0.48	-52 44 50.40	0.31	28.999	1.668	13.458	0.765	26.50	1.24	2.51	0.22	145.46	2.38	0.195	-0.74	M
303	23 59 24.08	1.06	-58 14 48.81	1.50	5.102	0.404	1.326	0.246	17.58	3.77	9.37	1.98	19.97	14.55	0.238	–	S
304	23 55 36.80	0.73	-52 52 20.60	0.50	4.178	0.452	2.215	0.296	9.96	1.75	5.13	1.05	70.79	13.87	0.252	–	S
305	23 56 21.26	0.42	-54 06 02.76	0.44	1.743	0.397	1.811	0.241	0.00	0.98	0.00	0.94	0.00	174.60	0.222	–	S
306	23 56 52.56	0.16	-54 55 51.78	0.17	18.854	1.204	16.608	0.985	3.26	0.19	2.58	0.19	9.45	24.47	0.358	-0.23	S
307	23 56 45.77	0.52	-54 46 51.11	0.50	3.115	0.490	2.335	0.318	4.95	1.22	4.28	1.08	55.60	108.33	0.275	–	S
308	23 55 03.89	0.14	-52 03 46.88	0.15	35.158	1.952	34.366	1.897	0.00	0.04	0.00	0.04	0.00	2.05	0.156	-0.50	S
309	23 59 34.36	0.82	-58 31 43.75	1.12	4.584	0.462	1.893	0.300	15.24	3.00	3.86	1.10	141.98	7.37	0.278	–	S
310	23 57 59.54	0.95	-56 33 25.82	1.85	7.098	0.467	1.336	0.229	23.12	4.38	11.04	2.01	6.81	11.02	0.238	–	S
311	23 56 25.17	0.68	-54 17 27.22	0.62	1.366	0.315	1.146	0.196	5.95	1.76	0.00	1.15	122.33	24.79	0.181	–	S
312	23 54 06.11	0.37	-50 16 09.61	0.17	37.680	2.146	19.377	1.091	20.96	0.81	1.85	0.18	178.12	2.10	0.234	-0.89	M
313	23 54 03.02	0.29	-50 10 29.32	0.32	4.489	0.424	3.359	0.286	5.25	0.62	4.36	0.62	168.99	176.58	0.206	–	S
314	23 56 37.37	0.45	-54 38 18.78	0.56	4.274	0.408	2.271	0.263	8.90	1.29	6.10	0.98	15.66	19.26	0.214	–	S
315	23 59 53.69	0.27	-58 58 28.96	0.29	2.991	0.376	2.833	0.252	2.47	0.59	0.71	0.54	12.22	56.14	0.196	–	S
316	23 59 44.67	0.33	-58 49 18.56	0.43	6.489	0.482	3.168	0.288	9.62	0.96	6.30	0.69	6.57	8.08	0.213	–	S
317	23 57 10.96	0.65	-55 30 25.10	0.67	3.097	0.371	1.654	0.247	7.64	1.54	7.27	1.49	170.70	174.42	0.211	–	S
318	23 55 53.51	0.60	-53 32 05.48	0.47	3.994	0.441	2.307	0.289	8.31	1.38	5.42	1.04	79.25	22.45	0.241	–	S
319	23 56 30.22	0.15	-54 30 26.31	0.16	15.013	0.897	14.028	0.799	2.86	0.13	0.85	0.12	30.14	5.32	0.204	1.08	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
320	23 56 40.22	1.25	-54 51 13.77	1.93	95.013	5.366	10.034	0.720	44.49	5.22	11.97	1.37	115.43	8.53	0.463	–	M
321	23 55 25.78	0.27	-52 46 58.46	0.27	3.678	0.385	3.246	0.266	3.40	0.53	2.41	0.52	61.98	51.51	0.192	–	S
322	23 55 18.91	0.20	-52 37 05.51	0.29	36.934	2.119	9.074	0.557	12.88	0.59	5.36	0.28	66.56	3.85	0.247	–	M
323	23 56 13.08	1.41	-54 07 18.62	0.57	28.464	1.666	3.640	0.313	28.41	3.30	11.69	1.29	177.48	9.63	0.241	–	M
324	23 56 27.82	1.22	-54 29 47.99	1.04	3.866	0.496	1.091	0.212	10.57	3.66	0.00	0.80	34.33	13.43	0.204	–	M
325	23 53 59.71	0.14	-50 14 58.23	0.15	105.961	5.845	96.830	5.332	3.77	0.03	0.00	0.02	1.89	176.36	0.262	-0.85	S
326	23 54 26.33	0.64	-51 05 03.62	0.75	2.087	0.304	1.274	0.201	8.60	1.85	4.52	1.31	138.53	26.83	0.176	–	S
327	23 54 26.06	0.30	-51 06 17.06	1.80	4.949	0.515	0.905	0.182	0.00	4.26	0.00	0.38	0.00	7.31	0.175	–	M
328	23 54 19.71	0.92	-50 52 56.31	0.71	2.427	0.421	1.498	0.279	7.85	2.16	4.90	1.61	77.76	36.53	0.248	–	S
329	23 56 14.17	0.18	-54 13 13.74	0.19	8.338	0.549	6.253	0.393	4.86	0.29	4.40	0.28	33.47	29.74	0.180	–	S
330	23 59 02.33	0.62	-58 06 09.28	0.80	2.653	0.318	1.387	0.211	10.09	1.96	4.89	1.21	147.33	15.84	0.184	–	S
331	23 56 38.49	0.25	-54 54 12.63	0.55	29.507	1.865	10.267	0.695	15.53	1.29	2.71	0.39	70.09	4.91	0.406	–	M
332	23 54 06.03	0.33	-50 34 30.01	0.67	38.134	2.180	10.979	0.649	25.11	1.65	5.89	0.42	106.38	4.02	0.238	-0.65	M
333	23 58 57.61	0.44	-58 03 02.74	0.38	5.508	0.487	3.063	0.312	7.87	0.95	6.20	0.86	80.92	35.25	0.242	–	S
334	23 55 45.97	0.68	-53 31 25.67	0.54	2.808	0.419	1.842	0.275	7.04	1.55	4.55	1.24	81.67	35.42	0.239	–	S
335	23 54 49.22	0.36	-51 54 19.44	0.37	4.686	0.360	2.490	0.222	7.92	0.80	7.39	0.77	44.58	44.84	0.161	–	S
336	23 55 20.21	0.15	-52 51 43.15	0.15	26.296	1.512	24.804	1.389	2.83	0.09	0.45	0.08	100.86	2.66	0.255	-0.47	S
337	23 58 16.30	0.58	-57 11 58.75	0.80	1.638	0.228	0.950	0.152	8.35	1.85	4.91	1.30	7.80	24.30	0.132	–	S
338	23 55 56.88	0.27	-53 51 27.04	0.30	7.251	0.589	4.853	0.389	6.57	0.61	4.76	0.54	147.02	22.23	0.264	–	S
339	23 58 09.29	0.29	-57 03 46.00	0.33	2.813	0.293	2.192	0.197	5.30	0.69	2.94	0.58	153.53	19.86	0.148	–	S
340	23 54 54.63	0.30	-52 09 50.53	0.31	3.973	0.397	3.090	0.268	5.36	0.67	3.28	0.58	125.75	25.21	0.197	–	S
341	23 59 11.27	0.31	-58 24 49.99	0.30	4.548	0.429	3.328	0.287	6.58	0.71	2.60	0.52	129.90	8.71	0.210	–	S
342	23 56 26.69	0.18	-54 44 19.75	0.19	8.473	0.633	7.859	0.501	2.79	0.27	1.47	0.26	38.17	25.08	0.249	–	S
343	23 55 19.94	0.39	-52 57 05.16	0.39	2.565	0.390	2.248	0.252	3.51	0.87	2.46	0.82	55.09	78.68	0.213	–	S
344	23 59 06.16	0.66	-58 21 49.74	0.64	2.956	0.466	1.904	0.307	6.03	1.51	5.64	1.46	110.73	84.03	0.268	–	S
345	23 59 04.22	0.24	-58 20 15.93	0.22	18.618	1.185	9.135	0.573	9.18	0.52	4.80	0.31	26.88	6.10	0.275	–	M
346	23 56 46.05	0.56	-55 16 42.60	0.53	3.951	0.343	1.821	0.216	8.89	1.30	8.40	1.17	69.09	106.24	0.176	–	S
347	23 55 55.46	1.67	-54 00 58.27	1.85	22.158	1.228	1.219	0.161	34.93	4.29	31.86	3.97	17.12	42.03	0.239	–	S
348	23 59 01.64	0.47	-58 20 59.27	0.33	14.987	1.054	11.485	0.686	20.96	1.25	0.00	0.22	26.19	2.57	0.268	-0.79	M
349	23 59 24.24	0.14	-58 47 16.54	0.15	37.818	2.114	36.282	2.008	1.77	0.05	1.44	0.05	67.33	117.12	0.219	-0.43	S
350	23 57 18.82	0.25	-56 06 12.37	0.29	3.958	0.351	3.016	0.240	5.37	0.57	3.35	0.48	2.37	16.34	0.164	–	S
351	23 53 56.22	0.33	-50 30 43.41	0.32	3.318	0.371	2.671	0.248	4.46	0.69	3.60	0.68	88.26	57.23	0.191	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
352	23 53 57.79	0.46	-50 34 05.10	0.45	4.238	0.452	2.687	0.296	7.80	1.14	4.69	0.86	120.17	20.58	0.239	–	S
353	23 55 12.15	0.22	-52 51 51.26	0.23	6.489	0.574	5.665	0.413	3.89	0.43	2.20	0.40	131.32	27.41	0.263	–	S
354	23 57 51.23	0.77	-56 54 53.52	0.84	1.935	0.248	0.961	0.167	8.38	2.01	7.52	1.71	7.78	85.89	0.146	–	S
355	23 55 10.21	0.31	-52 52 24.21	0.37	4.743	0.519	3.654	0.345	5.79	0.80	2.90	0.63	152.68	19.76	0.267	–	S
356	23 57 17.80	0.19	-56 13 56.37	0.20	12.497	0.778	8.258	0.511	9.26	0.40	0.00	0.19	131.16	177.83	0.226	–	S
357	23 55 50.18	1.10	-54 01 37.23	1.13	3.465	0.371	1.248	0.252	10.79	2.64	10.67	2.58	106.00	174.70	0.227	–	S
358	23 54 50.26	0.49	-52 22 12.00	0.46	3.620	0.328	1.915	0.210	8.26	1.13	7.05	1.00	64.96	36.11	0.167	–	S
359	23 59 14.77	0.21	-58 44 55.77	0.21	11.058	0.752	7.595	0.507	6.21	0.38	4.35	0.34	136.47	10.00	0.269	–	S
360	23 57 05.33	0.54	-55 56 17.73	0.63	1.352	0.257	1.048	0.165	5.09	1.44	3.32	1.23	8.59	58.02	0.147	–	S
361	23 54 41.25	0.44	-52 09 21.99	0.36	35.175	2.023	10.803	0.630	25.05	1.11	13.11	0.59	143.25	4.99	0.209	-0.29	M
362	23 59 31.07	0.17	-59 04 39.32	0.18	8.269	0.593	7.833	0.486	2.06	0.24	1.62	0.22	90.85	118.86	0.221	–	S
363	23 55 40.31	0.17	-53 48 48.90	0.18	10.745	0.731	9.762	0.595	2.66	0.22	2.46	0.22	108.15	174.74	0.251	–	S
364	23 54 47.12	0.59	-52 19 28.88	0.75	1.477	0.282	1.081	0.182	6.57	1.72	3.10	1.32	152.83	36.73	0.162	–	S
365	23 55 12.38	0.44	-53 03 44.45	0.43	2.304	0.416	2.084	0.263	3.52	1.01	1.45	0.93	112.98	65.00	0.231	–	S
366	23 57 55.85	0.19	-57 09 25.08	0.19	4.680	0.357	4.283	0.278	2.70	0.29	2.04	0.28	40.98	47.52	0.144	–	S
367	23 56 54.34	1.03	-55 45 11.38	0.74	3.646	0.329	1.314	0.211	12.97	2.38	8.44	1.69	96.34	23.42	0.187	–	S
368	23 58 01.08	0.93	-57 17 12.25	0.31	9.185	0.577	2.271	0.193	15.39	2.18	0.57	0.59	1.80	7.48	0.148	–	M
369	23 54 02.34	0.98	-51 00 59.04	0.62	3.131	0.306	1.320	0.199	12.50	2.36	6.80	1.34	93.44	15.25	0.175	–	S
370	23 58 00.60	0.14	-57 18 50.89	0.15	31.272	1.735	29.753	1.642	2.03	0.04	1.47	0.04	1.50	94.97	0.132	-0.25	S
371	23 55 35.78	0.68	-53 46 21.13	0.98	1.803	0.408	1.291	0.262	7.15	2.25	2.62	1.54	159.20	33.68	0.239	–	S
372	23 57 28.98	0.49	-56 36 08.14	0.56	2.472	0.348	1.683	0.228	6.07	1.27	4.72	1.11	2.03	53.23	0.195	–	S
373	23 57 53.50	0.69	-57 09 07.02	0.73	0.772	0.253	0.729	0.152	2.47	1.67	1.08	1.60	171.31	174.28	0.145	–	S
374	23 55 56.55	0.17	-54 21 46.82	0.18	7.149	0.497	6.566	0.404	2.68	0.23	2.09	0.23	158.04	148.57	0.177	–	S
375	23 55 10.92	1.01	-53 10 13.67	1.43	15.936	0.982	2.397	0.282	26.21	4.01	4.36	0.85	118.88	8.52	0.249	–	M
376	23 55 26.68	0.27	-53 35 41.54	0.38	8.310	0.632	4.016	0.294	9.90	0.88	1.69	0.41	111.13	7.13	0.194	–	M
377	23 54 22.89	0.48	-51 43 47.52	1.24	5.050	0.357	1.501	0.195	19.43	2.87	6.99	1.09	174.66	6.25	0.179	–	S
378	23 55 28.69	0.78	-53 40 14.43	0.71	2.551	0.349	1.401	0.233	8.15	1.82	6.49	1.61	103.72	67.56	0.203	–	S
379	23 58 37.55	0.16	-58 10 03.64	0.17	10.565	0.695	9.443	0.567	3.28	0.21	1.94	0.20	176.72	12.26	0.222	0.00	S
380	23 53 51.02	0.98	-50 47 57.37	1.50	2.341	0.274	0.896	0.188	14.37	3.60	6.99	2.01	151.45	22.52	0.172	–	S
381	23 54 24.60	0.71	-51 52 00.53	0.68	1.256	0.280	0.983	0.178	5.14	1.70	3.25	1.48	54.34	64.57	0.161	–	S
382	23 54 45.76	0.81	-52 31 04.17	0.66	3.606	0.308	1.389	0.192	11.68	1.92	8.84	1.45	68.33	24.45	0.165	–	S
383	23 53 32.55	0.41	-50 12 30.95	0.41	2.639	0.331	1.982	0.218	5.17	0.93	4.25	0.88	64.44	54.41	0.178	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
384	23 53 40.64	0.93	-50 29 35.65	0.84	3.083	0.349	1.374	0.234	11.46	2.41	7.05	1.64	117.01	25.85	0.206	–	S
385	23 56 38.88	0.26	-55 34 22.26	0.28	9.005	0.618	5.047	0.376	8.00	0.57	6.13	0.50	147.16	15.55	0.234	–	S
386	23 56 43.48	0.15	-55 43 08.34	0.16	15.965	0.934	13.941	0.790	3.28	0.12	2.78	0.12	156.54	113.88	0.186	-0.59	S
387	23 53 36.85	0.60	-50 26 51.02	0.72	14.607	0.833	2.501	0.234	20.71	1.67	15.84	1.36	150.39	17.13	0.205	–	S
388	23 56 35.81	0.89	-55 32 59.04	1.55	3.779	0.367	1.216	0.245	15.09	3.57	8.39	2.07	170.79	20.73	0.228	–	S
389	23 54 18.63	0.22	-51 48 44.21	0.31	5.015	0.423	3.748	0.288	6.77	0.63	2.18	0.41	0.42	6.13	0.192	–	S
390	23 53 58.76	0.15	-51 10 46.42	0.16	11.505	0.691	11.360	0.645	0.00	0.12	0.00	0.11	0.00	19.04	0.160	-0.61	S
391	23 58 09.14	1.42	-57 42 11.93	0.80	2.386	0.301	0.989	0.207	12.59	3.21	6.37	1.90	79.21	22.47	0.188	–	S
392	23 55 57.40	1.40	-54 36 26.70	0.34	3.051	0.470	1.011	0.206	0.00	3.30	0.00	0.65	0.00	13.64	0.199	–	M
393	23 59 56.86	0.55	-59 50 54.52	0.49	3.066	0.849	3.148	0.506	0.00	1.28	0.00	1.05	0.00	79.03	0.479	–	S
394	23 54 25.97	0.24	-52 03 39.12	0.26	3.770	0.330	3.032	0.231	4.27	0.48	3.76	0.48	22.36	69.54	0.152	–	S
395	23 53 35.87	1.32	-50 27 55.33	1.95	3.446	0.333	1.019	0.223	18.86	5.11	7.48	2.01	26.92	15.80	0.218	–	S
396	23 56 54.06	1.37	-56 02 52.67	1.09	3.206	0.287	0.949	0.187	15.24	3.33	9.62	2.29	112.28	27.18	0.174	–	S
397	23 55 08.76	0.51	-53 19 56.90	0.42	3.350	0.405	2.250	0.265	7.08	1.18	4.11	0.90	99.35	22.70	0.220	–	S
398	23 56 37.02	1.34	-55 39 46.87	0.98	5.324	0.358	1.122	0.183	18.03	3.10	13.06	2.29	73.20	24.11	0.178	–	S
399	23 57 51.80	0.15	-57 23 09.26	0.16	12.366	0.728	12.226	0.689	0.00	0.10	0.00	0.10	0.00	6.68	0.151	0.58	S
400	23 58 23.81	0.35	-58 04 48.81	0.37	3.090	0.399	2.498	0.262	4.19	0.83	3.41	0.74	171.32	75.12	0.213	–	S
401	23 55 14.96	0.35	-53 32 35.81	0.39	2.998	0.420	2.560	0.273	4.26	0.84	2.29	0.76	145.57	44.66	0.226	–	S
402	23 56 03.92	1.02	-54 52 58.34	1.03	5.118	0.448	1.783	0.282	15.84	3.08	6.43	1.32	39.44	9.80	0.260	–	S
403	23 58 30.69	0.78	-58 16 22.46	0.70	1.365	0.349	1.092	0.220	4.61	1.83	3.22	1.58	105.98	131.81	0.202	–	S
404	23 55 39.74	0.25	-54 16 56.24	0.28	3.891	0.335	2.904	0.228	5.25	0.54	4.10	0.51	171.07	34.22	0.154	–	S
405	23 55 39.93	0.14	-54 18 34.21	0.15	25.934	1.451	24.338	1.348	2.34	0.05	1.71	0.05	18.19	7.46	0.154	0.15	S
406	23 53 44.03	0.26	-50 54 42.67	0.34	3.993	0.384	3.070	0.259	6.93	0.76	1.05	0.47	149.05	7.13	0.188	–	S
407	23 53 22.72	0.83	-50 14 47.18	0.65	2.923	0.307	1.361	0.202	10.87	2.05	6.84	1.37	102.59	21.45	0.174	–	S
408	23 54 07.06	0.14	-51 42 59.19	0.15	65.795	3.656	55.386	3.054	4.65	0.04	0.61	0.03	47.13	1.22	0.214	-0.82	M
409	23 53 34.19	0.34	-50 39 04.82	0.47	4.078	0.386	2.558	0.251	9.02	1.10	3.57	0.65	149.77	8.85	0.195	–	S
410	23 54 59.25	0.35	-53 16 26.26	0.33	3.573	0.404	2.817	0.269	5.56	0.80	2.58	0.63	114.63	19.52	0.210	–	S
411	23 58 17.30	0.15	-58 08 17.42	0.17	33.732	1.962	23.817	1.344	7.40	0.17	2.97	0.11	88.28	2.72	0.302	-1.08	M
412	23 55 29.59	0.23	-54 10 33.93	0.24	5.853	0.442	4.281	0.304	4.99	0.43	4.76	0.42	125.65	174.77	0.182	–	S
413	23 53 49.58	0.30	-51 18 52.05	0.32	5.679	0.418	3.215	0.260	7.21	0.65	7.14	0.64	35.67	97.89	0.175	–	S
414	23 55 20.39	0.15	-54 01 12.53	0.16	17.406	1.013	15.528	0.877	2.93	0.11	2.66	0.11	23.40	121.06	0.193	-0.64	S
415	23 55 11.60	0.98	-53 48 06.07	0.71	8.918	0.782	1.987	0.255	16.82	2.70	1.58	0.74	140.76	9.19	0.230	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
416	23 53 35.23	0.14	-50 55 35.51	0.16	45.690	2.557	32.394	1.793	12.53	0.15	2.35	0.06	80.47	0.82	0.198	-0.59	M
417	23 55 09.18	0.31	-53 45 33.09	0.74	6.262	0.619	2.407	0.255	0.00	1.72	0.00	0.61	0.00	10.05	0.218	-	M
418	23 58 04.96	0.19	-58 01 26.16	0.31	9.991	0.713	5.263	0.358	0.00	0.65	0.00	0.29	0.00	5.22	0.211	-	M
419	23 57 48.89	0.27	-57 43 10.42	0.24	39.431	2.259	8.857	0.547	15.00	0.54	12.78	0.45	164.61	10.04	0.249	-	M
420	23 53 48.30	0.59	-51 23 34.42	0.68	2.108	0.268	1.231	0.177	8.77	1.67	5.09	1.22	138.74	26.34	0.152	-	S
421	23 57 32.67	0.32	-57 21 25.53	0.35	2.834	0.303	2.122	0.201	5.39	0.76	3.59	0.65	25.77	24.77	0.156	-	S
422	23 53 40.19	2.04	-51 09 20.73	1.20	6.883	0.417	0.978	0.163	29.02	5.19	13.43	2.25	104.11	11.16	0.182	-	S
423	23 56 42.51	0.90	-56 21 18.10	1.02	6.029	0.468	1.755	0.279	13.73	2.46	11.06	1.97	22.62	31.98	0.253	-	S
424	23 54 27.25	0.23	-52 38 20.66	0.23	6.819	0.499	4.866	0.341	5.37	0.42	4.90	0.41	57.45	38.16	0.199	-	S
425	23 54 05.26	0.43	-51 58 18.41	0.76	6.663	0.447	2.209	0.231	16.05	1.77	7.74	0.90	162.45	6.15	0.191	-	S
426	23 58 33.34	0.14	-58 42 00.40	0.15	53.772	2.984	51.324	2.832	2.13	0.04	1.14	0.04	49.17	91.30	0.230	-0.22	S
427	23 55 57.52	0.71	-55 06 49.82	0.89	2.114	0.350	1.261	0.233	7.77	2.06	5.29	1.62	9.37	43.36	0.206	-	S
428	23 58 14.53	0.48	-58 18 50.94	0.40	3.515	0.367	2.154	0.240	7.26	1.05	5.23	0.90	77.61	31.53	0.193	-	S
429	23 57 11.76	0.94	-56 56 21.76	1.60	2.604	0.264	0.840	0.178	14.75	3.70	8.44	2.20	170.94	22.58	0.166	-	S
430	23 58 56.21	0.14	-59 09 34.90	0.15	23.419	1.335	22.925	1.277	1.50	0.07	0.54	0.07	173.22	105.73	0.203	0.76	S
431	23 58 36.04	1.27	-58 45 41.70	0.88	3.080	0.317	1.107	0.213	13.37	2.94	7.85	1.98	103.25	25.08	0.193	-	S
432	23 57 59.97	0.90	-58 02 01.71	1.21	2.535	0.343	1.112	0.236	10.39	2.83	7.38	2.10	172.74	39.85	0.212	-	S
433	23 54 50.39	1.75	-53 26 00.20	1.24	23.624	1.386	2.046	0.255	29.69	4.68	12.68	1.83	26.39	13.01	0.229	-	M
434	23 58 03.29	0.16	-58 08 54.48	0.19	22.272	1.386	14.576	0.853	7.73	0.28	1.18	0.16	71.83	3.30	0.293	-1.15	M
435	23 53 44.50	0.68	-51 26 14.76	0.90	1.293	0.274	0.918	0.177	6.75	2.00	3.64	1.61	159.70	48.80	0.160	-	S
436	23 53 04.55	0.56	-50 07 32.45	0.74	3.684	0.347	1.695	0.224	10.52	1.68	7.45	1.28	15.89	25.81	0.188	-	S
437	23 57 23.61	0.30	-57 17 57.49	0.35	2.496	0.250	1.820	0.167	5.60	0.73	3.91	0.63	176.03	24.88	0.126	-	S
438	23 57 37.74	0.93	-57 37 18.31	1.18	3.559	0.338	1.232	0.222	14.29	2.98	7.71	1.76	145.13	17.87	0.202	-	S
439	23 53 21.64	0.91	-50 44 27.22	0.75	1.598	0.312	1.083	0.202	8.56	2.40	1.99	1.33	115.98	21.32	0.184	-	S
440	23 57 27.82	0.38	-57 32 42.73	1.19	30.535	1.815	20.010	1.153	29.57	2.80	7.89	0.75	92.07	6.23	0.342	-0.35	M
441	23 53 30.24	0.40	-51 04 07.11	0.48	2.702	0.312	1.836	0.205	6.94	1.07	4.34	0.88	149.64	29.09	0.167	-	S
442	23 54 59.14	0.48	-53 45 42.81	0.61	3.093	0.388	1.938	0.255	7.56	1.37	4.86	1.09	164.82	29.93	0.216	-	S
443	23 54 19.65	0.52	-52 39 07.03	0.73	11.695	0.681	2.550	0.233	21.04	1.85	10.62	0.87	24.69	3.06	0.195	-	S
444	23 54 00.93	0.18	-52 04 42.50	0.21	4.959	0.371	4.336	0.283	4.00	0.33	1.91	0.28	9.54	13.43	0.147	-	S
445	23 56 21.96	0.85	-55 59 00.15	0.81	1.047	0.264	0.785	0.168	5.49	2.11	3.52	1.71	45.67	72.39	0.154	-	S
446	23 53 14.72	1.49	-50 40 42.92	2.06	9.312	0.537	0.933	0.156	29.22	4.69	20.75	3.59	164.12	27.35	0.190	-	S
447	23 56 08.19	0.69	-55 46 45.81	0.88	1.870	0.277	1.046	0.186	8.35	2.05	5.69	1.57	9.79	37.12	0.163	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
448	23 56 16.17	0.57	-55 59 28.70	0.81	1.087	0.267	0.896	0.167	0.00	1.85	0.00	1.31	0.00	33.72	0.154	–	S
449	23 58 04.57	0.50	-58 26 48.11	0.42	2.573	0.326	1.777	0.214	6.56	1.11	3.90	0.92	109.26	28.51	0.179	–	S
450	23 55 27.62	0.91	-54 46 15.97	1.10	1.978	0.316	1.007	0.216	8.78	2.56	6.93	2.12	9.72	66.59	0.192	–	S
451	23 56 05.37	1.18	-55 44 47.52	1.00	2.287	0.250	0.846	0.170	11.33	2.76	9.49	2.34	74.18	69.94	0.153	–	S
452	23 53 50.89	0.82	-52 02 02.20	0.73	2.199	0.272	1.132	0.182	10.19	2.10	5.69	1.40	118.40	23.00	0.159	–	S
453	23 57 17.43	1.06	-57 28 31.07	1.55	2.672	0.264	0.819	0.178	14.14	3.60	9.70	2.49	176.78	31.18	0.166	–	S
454	23 54 29.28	0.15	-53 13 44.83	0.16	10.993	0.706	11.283	0.655	0.00	0.16	0.00	0.14	0.00	4.84	0.210	-0.13	S
455	23 56 10.24	0.73	-55 54 36.79	1.11	2.885	0.282	1.128	0.184	13.49	2.72	6.48	1.41	17.77	13.24	0.166	–	S
456	23 56 15.25	0.36	-56 03 15.94	0.48	2.441	0.275	1.649	0.181	7.23	1.08	3.57	0.78	160.55	15.36	0.147	–	S
457	23 57 30.64	0.28	-57 49 11.08	0.27	6.119	0.455	3.791	0.292	7.55	0.60	4.79	0.48	125.69	10.02	0.189	–	S
458	23 54 06.11	0.27	-52 35 07.72	0.29	4.219	0.341	2.873	0.227	5.75	0.57	5.38	0.55	11.14	99.93	0.152	–	S
459	23 57 08.28	0.90	-57 19 10.12	0.28	2.412	0.319	1.082	0.141	0.00	2.09	0.00	0.53	0.00	9.82	0.127	–	M
460	23 54 42.98	0.31	-53 42 22.87	0.29	3.756	0.400	3.061	0.270	4.75	0.67	2.67	0.57	60.99	23.18	0.202	–	S
461	23 56 32.02	1.30	-56 32 35.33	1.71	6.774	0.412	1.009	0.163	26.86	4.47	12.87	2.19	142.77	10.94	0.179	–	S
462	23 56 29.20	0.71	-56 27 25.78	0.69	1.102	0.314	0.974	0.193	3.06	1.62	2.67	1.59	52.67	174.57	0.180	–	S
463	23 55 17.26	0.93	-54 39 13.20	1.52	3.271	0.330	1.126	0.220	15.97	3.73	6.80	1.77	152.70	15.61	0.206	–	S
464	23 53 50.65	0.51	-52 10 23.51	0.90	2.817	0.285	1.333	0.185	12.06	2.12	5.18	1.08	9.76	11.33	0.160	–	S
465	23 54 06.25	0.17	-52 40 02.93	0.18	8.364	0.548	7.280	0.439	3.41	0.22	2.86	0.21	132.37	146.49	0.174	-0.67	S
466	23 58 30.32	0.88	-59 07 35.24	0.76	2.902	0.357	1.384	0.241	9.86	2.12	6.60	1.65	117.71	36.10	0.211	–	S
467	23 58 05.04	0.31	-58 37 33.40	0.30	2.984	0.397	2.758	0.262	2.69	0.67	1.74	0.60	71.87	102.02	0.210	–	S
468	23 57 23.99	0.56	-57 45 45.67	0.86	4.056	0.390	1.794	0.251	11.81	2.05	5.81	1.13	13.19	11.13	0.218	–	S
469	23 56 12.28	0.53	-56 07 45.45	0.56	4.009	0.335	1.802	0.208	9.96	1.35	7.59	1.07	32.65	21.36	0.169	–	S
470	23 53 14.47	1.32	-51 05 07.85	1.21	1.891	0.255	0.807	0.176	13.57	3.74	5.79	1.88	123.16	20.94	0.161	–	S
471	23 58 48.34	1.26	-59 33 20.77	1.01	13.374	0.892	5.048	0.359	24.45	3.72	1.87	0.66	135.74	7.23	0.228	–	M
472	23 55 11.27	0.25	-54 35 05.68	0.28	7.915	0.585	5.015	0.378	7.15	0.57	5.03	0.48	157.29	14.00	0.241	–	S
473	23 53 17.22	0.14	-51 12 14.36	0.15	24.436	1.404	23.742	1.327	2.13	0.09	0.00	0.08	13.57	6.63	0.235	0.40	S
474	23 55 32.15	0.16	-55 09 23.43	0.18	8.298	0.534	6.981	0.419	4.15	0.22	2.62	0.20	26.22	8.38	0.163	-0.39	S
475	23 54 16.83	0.34	-53 04 54.86	0.18	9.812	0.863	6.568	0.463	0.00	0.73	0.00	0.21	0.00	3.70	0.289	–	M
476	23 56 44.60	0.28	-56 57 38.71	0.27	3.766	0.335	2.803	0.227	5.50	0.59	3.65	0.51	51.69	18.47	0.158	–	S
477	23 58 23.02	1.37	-59 05 08.36	1.88	7.385	0.451	1.002	0.182	24.23	4.52	15.87	3.00	156.00	19.38	0.204	–	S
478	23 53 13.44	0.15	-51 11 34.10	0.16	30.683	1.776	18.909	1.070	6.92	0.16	5.06	0.13	46.00	4.92	0.252	-1.19	M
479	23 54 06.29	0.76	-52 50 09.35	0.79	1.452	0.299	1.039	0.192	7.15	2.12	2.30	1.35	38.91	26.58	0.174	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
480	23 57 26.99	0.31	-57 57 14.46	0.37	5.350	0.440	3.276	0.282	9.11	0.88	3.05	0.50	140.87	3.74	0.205	-	S
481	23 52 55.79	0.22	-50 37 03.66	0.31	9.479	0.596	4.825	0.333	11.37	0.66	4.97	0.35	156.65	1.35	0.189	-	S
482	23 58 12.03	0.71	-58 57 25.30	0.45	47.998	2.757	7.217	0.523	18.68	1.71	10.66	0.89	11.96	8.90	0.341	-	M
483	23 55 04.72	0.23	-54 33 40.70	0.26	5.657	0.485	4.528	0.339	4.68	0.48	3.22	0.43	12.78	22.81	0.220	-	S
484	23 53 29.79	0.16	-51 47 07.58	0.17	11.357	0.755	10.719	0.640	2.56	0.20	1.09	0.19	46.49	18.63	0.247	-0.39	S
485	23 53 09.01	0.27	-51 06 26.43	0.31	4.301	0.387	3.180	0.262	5.68	0.61	4.08	0.56	165.80	32.35	0.184	-	S
486	23 59 03.46	0.66	-59 58 46.68	0.39	58.430	3.559	10.530	0.858	25.09	1.68	5.97	0.40	20.98	3.70	0.633	-	M
487	23 53 51.42	0.71	-52 28 11.55	0.68	2.306	0.247	1.113	0.163	9.84	1.76	7.05	1.43	120.02	34.84	0.139	-	S
488	23 57 26.83	0.75	-58 00 56.28	0.67	1.777	0.321	1.183	0.210	6.27	1.78	4.90	1.50	106.42	106.06	0.187	-	S
489	23 52 41.27	0.64	-50 11 04.12	1.02	3.283	0.346	1.473	0.228	12.42	2.43	6.03	1.31	17.00	15.20	0.201	-	S
490	23 57 01.67	0.43	-57 29 14.80	0.45	1.978	0.319	1.649	0.204	4.82	1.06	1.83	0.87	138.17	31.98	0.177	-	S
491	23 54 16.13	1.42	-53 18 49.76	0.48	4.882	0.694	1.814	0.295	0.00	3.44	0.00	0.64	0.00	11.45	0.278	-	M
492	23 57 50.00	0.23	-58 35 33.61	0.24	5.181	0.436	4.133	0.306	4.14	0.45	3.73	0.42	5.39	56.66	0.195	-	S
493	23 58 00.80	0.25	-58 49 20.40	0.26	5.513	0.455	4.016	0.309	5.26	0.51	4.28	0.48	151.97	33.50	0.204	-	S
494	23 53 30.85	0.16	-52 00 03.79	0.17	10.467	0.669	9.921	0.581	2.45	0.18	1.06	0.16	54.42	17.30	0.198	-0.26	S
495	23 53 56.25	0.14	-52 50 31.86	0.15	23.723	1.349	23.571	1.312	0.00	0.07	0.00	0.06	0.00	0.31	0.199	0.06	S
496	23 52 37.46	0.58	-50 14 41.44	0.70	1.859	0.337	1.358	0.218	5.86	1.51	4.20	1.41	165.21	86.57	0.193	-	S
497	23 57 14.13	1.10	-57 55 20.39	1.03	4.313	0.489	1.543	0.215	12.23	3.47	0.00	0.60	131.48	10.00	0.198	-	M
498	23 56 22.95	0.62	-56 45 23.33	0.85	2.682	0.288	1.304	0.189	11.49	2.15	4.57	1.07	23.78	10.48	0.166	-	S
499	23 57 15.81	0.14	-57 58 32.26	0.15	61.000	3.371	59.469	3.276	1.68	0.03	0.50	0.03	6.60	90.49	0.189	-0.39	S
500	23 58 00.52	0.24	-58 56 41.84	0.21	8.213	0.727	7.202	0.524	4.53	0.44	0.00	0.36	104.89	8.82	0.334	-	S
501	23 58 18.51	0.38	-59 19 28.72	0.34	5.777	0.463	3.203	0.291	8.34	0.83	5.71	0.69	117.47	16.73	0.214	-	S
502	23 54 32.41	0.66	-53 57 42.76	0.94	1.590	0.306	1.048	0.201	7.51	2.13	3.91	1.55	172.53	36.04	0.180	-	S
503	23 53 26.94	1.74	-52 01 15.86	1.07	3.964	0.322	1.036	0.200	19.05	4.42	9.04	1.96	64.18	14.62	0.195	-	S
504	23 54 06.19	0.62	-53 15 07.55	0.59	2.615	0.367	1.646	0.242	6.61	1.46	5.76	1.33	61.21	80.08	0.208	-	S
505	23 52 58.20	0.91	-51 07 56.81	1.12	2.988	0.326	1.245	0.218	14.00	3.01	5.86	1.48	138.11	15.36	0.197	-	S
506	23 54 40.86	1.63	-54 16 46.17	1.04	2.091	0.218	0.685	0.148	15.04	3.93	8.26	2.19	66.64	22.19	0.138	-	S
507	23 53 52.19	0.40	-52 52 16.39	0.53	2.293	0.339	1.788	0.219	6.21	1.19	1.85	0.85	156.49	20.23	0.187	-	S
508	23 58 17.46	0.16	-59 22 08.09	0.17	11.005	0.720	9.880	0.591	3.31	0.20	1.87	0.19	109.44	14.45	0.227	-0.53	S
509	23 55 18.97	0.69	-55 18 18.17	0.68	1.780	0.280	1.153	0.183	8.37	1.87	3.15	1.17	127.96	19.74	0.162	-	S
510	23 54 48.71	0.18	-54 30 28.55	0.18	8.692	0.573	6.965	0.430	4.84	0.27	3.08	0.24	116.85	10.05	0.187	-	S
511	23 53 23.12	1.25	-51 59 30.44	0.40	15.031	0.872	1.938	0.221	24.18	2.95	5.58	0.78	167.01	7.69	0.194	-	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
512	23 54 57.89	0.22	-54 45 21.72	0.23	5.424	0.434	4.399	0.310	4.27	0.40	3.40	0.38	40.82	31.41	0.186	–	S
513	23 52 34.43	0.60	-50 23 40.71	1.68	13.031	0.744	1.732	0.201	33.89	3.91	12.28	1.37	173.24	4.70	0.218	–	S
514	23 55 24.80	1.37	-55 30 29.94	1.29	3.502	0.271	0.852	0.163	17.72	3.64	10.89	2.39	126.13	23.39	0.157	–	S
515	23 57 50.49	1.40	-58 51 47.55	0.99	3.365	0.314	1.065	0.206	15.55	3.37	8.02	1.97	111.62	18.96	0.192	–	S
516	23 58 44.26	0.87	-59 56 22.56	0.27	28.287	1.896	9.378	0.705	16.66	2.03	1.44	0.50	179.14	6.09	0.480	–	M
517	23 55 38.53	0.42	-55 52 52.40	0.43	7.949	0.524	3.017	0.274	10.31	0.94	10.06	0.93	165.95	174.30	0.203	–	S
518	23 53 06.06	0.33	-51 29 53.61	0.36	2.399	0.299	2.015	0.198	4.35	0.75	2.75	0.71	142.23	50.75	0.158	–	S
519	23 57 31.05	0.27	-58 30 34.32	0.25	14.491	0.905	5.730	0.385	9.76	0.64	3.68	0.34	137.93	6.12	0.222	–	M
520	23 52 30.35	0.89	-50 21 02.49	1.10	5.686	0.478	1.885	0.298	15.20	2.89	8.49	1.56	32.09	15.08	0.269	–	S
521	23 56 44.18	0.74	-57 29 39.07	0.93	2.193	0.282	1.065	0.190	9.26	2.16	6.93	1.71	175.09	40.83	0.167	–	S
522	23 54 11.24	0.15	-53 36 30.09	0.17	17.958	1.090	15.232	0.883	4.36	0.17	2.33	0.15	146.01	4.65	0.271	0.13	S
523	23 52 29.27	0.26	-50 22 13.06	0.32	9.649	0.677	5.506	0.417	9.01	0.71	5.20	0.46	25.38	5.83	0.266	–	S
524	23 56 24.32	1.07	-57 04 35.92	1.14	1.883	0.233	0.779	0.160	12.23	3.04	6.80	1.94	135.20	25.77	0.144	–	S
525	23 58 03.95	1.36	-59 14 41.79	1.22	5.519	0.382	1.139	0.204	18.30	3.39	12.69	2.55	123.18	27.71	0.202	–	S
526	23 55 53.60	0.93	-56 20 58.39	1.17	2.185	0.351	1.096	0.240	9.86	2.83	5.99	2.00	149.60	37.50	0.216	–	S
527	23 56 24.23	0.79	-57 05 13.23	1.08	1.332	0.241	0.784	0.160	9.40	2.67	3.56	1.54	148.68	22.82	0.145	–	S
528	23 54 19.87	0.29	-53 55 50.74	0.26	3.239	0.355	2.895	0.243	4.13	0.60	0.00	0.48	67.22	16.41	0.179	–	S
529	23 52 49.82	0.26	-51 13 26.05	0.27	2.970	0.341	2.807	0.234	2.89	0.54	0.00	0.51	121.90	40.98	0.173	–	S
530	23 55 50.13	0.14	-56 19 41.69	0.15	55.704	3.087	48.859	2.697	3.91	0.04	1.55	0.04	27.18	176.78	0.221	-0.87	S
531	23 52 36.84	0.68	-50 43 04.17	0.68	1.278	0.275	1.000	0.175	5.38	1.69	2.97	1.41	47.13	50.88	0.158	–	S
532	23 52 28.47	0.16	-50 31 25.50	0.19	46.893	2.643	26.247	1.462	16.85	0.30	6.24	0.12	110.97	1.40	0.230	-0.83	M
533	23 55 31.11	0.92	-55 54 13.88	1.99	4.213	0.460	1.120	0.191	13.84	5.02	0.00	1.09	62.77	15.78	0.181	–	M
534	23 57 08.09	0.25	-58 10 52.58	0.28	4.306	0.380	3.238	0.259	5.06	0.55	3.88	0.50	1.09	26.57	0.178	–	S
535	23 53 03.74	0.40	-51 42 26.90	0.39	3.825	0.673	3.638	0.425	2.45	0.90	0.81	0.83	63.64	99.65	0.370	–	S
536	23 57 42.08	0.35	-58 55 27.96	0.33	3.955	0.489	3.246	0.323	4.25	0.76	3.06	0.68	111.11	66.78	0.258	–	S
537	23 58 23.90	0.52	-59 47 30.98	0.46	12.551	0.824	4.660	0.423	15.03	1.41	5.61	0.61	42.70	1.43	0.330	–	S
538	23 57 27.79	1.04	-58 38 37.51	1.36	3.982	0.287	0.963	0.161	19.20	3.51	9.44	1.81	144.39	12.26	0.156	–	S
539	23 57 22.26	1.24	-58 34 24.09	0.91	7.547	0.468	1.375	0.199	19.39	2.79	14.13	2.17	73.29	22.28	0.197	–	S
540	23 55 23.16	0.17	-55 47 39.39	0.18	7.344	0.492	6.423	0.392	3.50	0.23	2.40	0.22	30.37	16.60	0.165	–	S
541	23 57 42.52	0.75	-59 00 03.87	1.12	7.802	0.552	2.111	0.302	17.13	2.76	8.98	1.43	17.06	9.47	0.280	–	S
542	23 53 02.97	0.32	-51 46 48.47	0.34	6.371	0.717	5.078	0.478	4.53	0.71	3.67	0.69	33.32	59.27	0.370	–	S
543	23 52 41.76	0.22	-51 06 10.83	0.25	6.628	0.468	4.447	0.311	6.38	0.45	5.12	0.41	3.70	24.42	0.179	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
544	23 53 05.49	0.24	-51 53 15.26	0.25	4.851	0.465	4.301	0.329	3.50	0.48	2.18	0.45	30.44	36.37	0.223	-	S
545	23 55 34.96	0.50	-56 07 49.84	0.56	2.455	0.304	1.526	0.200	6.81	1.28	5.54	1.12	15.02	49.69	0.169	-	S
546	23 57 41.91	0.87	-59 00 47.82	0.64	4.110	0.486	2.053	0.323	10.69	2.07	5.10	1.29	111.87	16.92	0.283	-	S
547	23 57 51.54	1.23	-59 13 08.16	1.21	4.973	0.389	1.243	0.236	14.23	3.05	12.89	2.66	139.24	120.04	0.224	-	S
548	23 55 42.89	0.99	-56 22 22.02	1.36	8.966	0.657	1.533	0.234	17.38	3.77	3.47	1.12	118.92	13.24	0.218	-	M
549	23 53 10.69	1.07	-52 06 18.13	1.01	2.528	0.242	0.989	0.156	15.79	3.25	4.74	1.14	43.67	8.75	0.145	-	S
550	23 52 24.79	1.10	-50 34 48.70	1.39	4.968	0.352	1.111	0.194	17.07	3.06	13.78	2.73	0.45	51.95	0.187	-	S
551	23 57 40.92	1.58	-59 01 28.74	0.66	6.385	0.631	1.399	0.279	0.00	3.91	0.00	0.82	0.00	14.36	0.269	-	M
552	23 55 12.03	1.22	-55 35 19.75	0.96	1.590	0.248	0.758	0.171	9.66	2.83	7.08	2.25	85.82	58.38	0.153	-	S
553	23 52 56.91	1.26	-51 45 27.97	0.64	123.653	6.907	21.745	1.276	52.37	3.24	11.21	0.64	20.14	4.08	0.446	-0.99	M
554	23 57 05.62	0.75	-58 21 27.86	1.21	4.591	0.338	1.287	0.193	17.16	2.94	8.46	1.45	14.55	9.77	0.180	-	S
555	23 55 09.79	0.75	-55 36 47.00	0.88	1.034	0.247	0.757	0.158	5.79	2.09	3.68	1.69	15.54	65.02	0.144	-	S
556	23 57 34.53	1.10	-59 00 34.65	0.72	7.093	0.549	2.286	0.324	17.22	2.71	6.48	1.20	112.94	7.62	0.297	-	S
557	23 56 57.97	0.22	-58 13 30.77	0.23	3.844	0.361	3.486	0.259	3.40	0.43	1.01	0.39	25.63	20.14	0.171	-	S
558	23 54 53.49	1.04	-55 14 24.06	1.11	2.032	0.255	0.872	0.174	12.21	2.99	6.43	1.83	133.58	24.03	0.157	-	S
559	23 56 00.31	0.16	-56 55 48.05	0.17	8.050	0.511	7.054	0.417	3.10	0.18	2.83	0.18	1.06	50.68	0.149	-0.48	S
560	23 54 07.17	1.00	-53 58 25.17	1.11	2.863	0.312	1.083	0.212	10.98	2.63	9.69	2.30	163.56	123.40	0.189	-	S
561	23 56 06.65	1.10	-57 05 31.54	1.75	2.676	0.230	0.695	0.148	16.84	4.12	10.16	2.46	7.05	22.45	0.143	-	S
562	23 57 44.25	0.66	-59 15 17.47	0.52	2.559	0.366	1.636	0.241	7.15	1.48	4.60	1.21	93.48	39.02	0.208	-	S
563	23 55 34.51	1.14	-56 21 37.56	1.19	3.666	0.363	1.220	0.243	13.45	3.06	9.21	2.28	134.91	35.10	0.222	-	S
564	23 52 34.92	0.87	-51 11 09.43	1.27	4.865	0.359	1.412	0.204	20.45	3.39	6.82	1.22	143.08	7.72	0.192	-	S
565	23 55 35.73	0.19	-56 24 45.77	0.17	16.709	1.065	10.144	0.602	7.94	0.32	0.00	0.16	159.45	3.27	0.225	-0.99	M
566	23 53 23.01	0.65	-52 43 38.87	0.86	1.012	0.273	0.845	0.170	5.15	1.94	1.24	1.51	9.73	48.94	0.158	-	S
567	23 55 23.85	0.71	-56 06 53.70	1.08	2.249	0.276	1.028	0.187	10.75	2.48	6.57	1.67	176.23	25.61	0.165	-	S
568	23 52 54.61	0.34	-51 51 27.29	0.37	2.673	0.475	2.733	0.299	0.00	0.79	0.00	0.74	0.00	106.25	0.260	-	S
569	23 56 13.18	0.69	-57 19 45.71	0.92	2.011	0.212	0.866	0.141	10.69	2.13	7.48	1.59	167.03	28.30	0.123	-	S
570	23 52 22.63	0.14	-50 51 14.92	0.15	43.226	2.435	30.988	1.718	7.34	0.09	0.00	0.05	146.92	1.24	0.215	-0.84	M
571	23 56 02.81	1.04	-57 08 01.88	1.00	1.440	0.309	0.571	0.132	0.00	3.36	0.00	0.33	0.00	8.24	0.129	-	M
572	23 52 39.78	0.14	-51 28 04.64	0.15	137.429	7.604	135.474	7.467	0.00	0.03	0.00	0.03	0.00	2.65	0.481	-0.41	S
573	23 56 23.31	2.10	-57 38 15.79	1.86	5.329	0.330	0.707	0.140	28.41	5.75	13.85	2.95	125.19	15.59	0.162	-	S
574	23 56 46.61	0.76	-58 10 37.30	0.66	1.310	0.293	0.992	0.187	5.29	1.79	3.58	1.48	99.87	90.70	0.170	-	S
575	23 52 53.67	0.43	-51 59 38.44	0.45	2.410	0.318	1.788	0.208	4.98	1.02	4.62	0.92	39.13	132.81	0.173	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
576	23 55 29.34	0.48	-56 27 24.19	0.31	15.191	0.983	4.957	0.357	13.86	1.15	5.10	0.50	152.08	6.58	0.231	–	M
577	23 56 59.24	0.15	-58 32 16.20	0.16	31.173	1.772	19.301	1.083	9.14	0.16	4.87	0.10	130.93	2.25	0.214	-0.85	M
578	23 55 12.40	1.37	-56 01 04.55	0.62	4.380	0.399	0.899	0.172	0.00	3.27	0.00	1.25	0.00	21.36	0.165	–	M
579	23 53 06.29	1.26	-52 27 32.65	1.05	1.646	0.209	0.707	0.142	12.96	3.45	5.74	1.67	50.43	17.99	0.130	–	S
580	23 55 16.56	0.55	-56 08 39.91	0.63	1.803	0.307	1.315	0.199	6.20	1.51	3.14	1.14	25.06	30.36	0.175	–	S
581	23 57 35.32	0.44	-59 25 13.37	2.53	41.901	2.370	2.895	0.318	49.17	5.96	7.75	0.94	81.36	7.04	0.275	–	M
582	23 56 53.41	1.14	-58 26 35.21	1.17	2.790	0.322	1.114	0.218	14.20	3.39	5.48	1.61	132.18	15.05	0.202	–	S
583	23 55 22.58	1.10	-56 20 33.01	1.20	2.655	0.302	0.978	0.208	10.91	2.90	9.88	2.49	168.52	120.97	0.188	–	S
584	23 53 26.47	0.82	-53 09 35.68	0.82	1.938	0.473	1.445	0.303	4.99	1.96	4.46	1.84	105.36	175.19	0.276	–	S
585	23 57 16.93	0.89	-58 59 21.08	1.08	3.485	0.452	1.544	0.309	10.03	2.61	7.44	1.97	13.94	39.37	0.276	–	S
586	23 51 51.85	0.19	-50 03 27.33	0.21	5.982	0.461	5.240	0.348	3.63	0.34	2.48	0.32	35.67	26.62	0.189	–	S
587	23 53 46.23	1.16	-53 48 13.87	1.44	10.365	0.745	2.545	0.414	20.98	4.00	8.47	1.55	32.18	9.64	0.409	–	S
588	23 56 50.18	0.51	-58 26 21.54	0.45	1.537	0.370	1.529	0.224	0.00	1.16	0.00	0.99	0.00	97.36	0.208	–	S
589	23 52 05.87	0.16	-50 35 05.87	0.17	9.409	0.593	8.660	0.506	2.93	0.17	1.87	0.17	136.95	22.94	0.169	-0.69	S
590	23 54 20.41	0.50	-54 47 36.20	0.93	3.913	0.327	1.526	0.201	13.93	2.15	6.42	1.10	167.49	9.61	0.175	–	S
591	23 57 44.28	0.25	-59 35 53.72	0.24	4.632	0.466	4.165	0.327	3.77	0.49	0.85	0.43	121.03	19.56	0.228	–	S
592	23 55 36.67	0.26	-56 51 20.91	0.27	34.030	1.919	8.811	0.537	17.42	0.64	10.59	0.37	41.34	4.09	0.232	–	M
593	23 53 40.10	0.71	-53 42 03.23	0.79	2.747	0.348	1.425	0.233	8.38	1.83	7.15	1.63	18.71	70.49	0.202	–	S
594	23 53 59.53	0.89	-54 17 20.55	0.92	1.129	0.224	0.700	0.149	6.56	2.20	6.01	2.00	31.72	171.07	0.133	–	S
595	23 52 08.02	0.16	-50 47 58.53	0.17	9.296	0.590	8.143	0.482	3.39	0.19	2.80	0.19	124.10	133.05	0.173	-0.17	S
596	23 53 40.95	1.76	-53 49 05.87	2.06	42.883	2.369	1.877	0.241	41.70	4.79	34.02	4.17	157.36	28.81	0.392	–	S
597	23 57 51.84	1.02	-59 49 43.33	0.92	2.416	0.433	1.334	0.294	7.69	2.50	6.34	2.00	50.97	95.44	0.262	–	S
598	23 55 23.92	0.28	-56 34 30.06	0.30	3.902	0.446	3.380	0.301	3.75	0.62	2.29	0.57	22.90	38.71	0.229	–	S
599	23 54 36.25	0.66	-55 22 09.53	0.92	1.385	0.258	0.895	0.170	7.51	2.12	4.08	1.52	5.77	34.58	0.152	–	S
600	23 57 48.80	0.69	-59 50 13.45	1.97	10.127	0.773	1.733	0.291	0.00	4.66	0.00	1.46	0.00	20.65	0.275	–	M
601	23 55 21.91	0.62	-56 34 57.89	0.79	7.070	0.492	2.226	0.265	15.25	2.01	8.39	1.11	25.30	8.19	0.229	–	S
602	23 51 52.65	0.42	-50 20 36.55	0.48	8.436	0.581	3.522	0.322	13.13	1.25	6.68	0.70	136.13	6.23	0.242	–	S
603	23 53 42.98	0.21	-53 55 14.10	0.23	7.982	0.578	5.869	0.402	5.62	0.41	4.01	0.36	164.82	16.40	0.225	–	S
604	23 56 22.75	0.64	-58 02 35.19	0.53	1.450	0.295	1.170	0.187	5.30	1.47	2.08	1.17	108.58	40.34	0.168	–	S
605	23 54 38.62	0.49	-55 31 01.84	0.41	2.266	0.282	1.580	0.185	6.38	1.08	4.07	0.90	96.62	31.34	0.154	–	S
606	23 55 30.96	0.63	-56 51 06.02	0.69	2.223	0.387	1.537	0.251	6.67	1.70	3.61	1.26	29.80	31.73	0.223	–	S
607	23 53 39.19	0.39	-53 54 57.32	0.41	14.090	0.835	4.416	0.344	16.28	1.09	8.16	0.58	132.17	2.13	0.238	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
608	23 52 55.10	0.26	-52 32 49.48	0.30	2.928	0.304	2.484	0.208	4.24	0.59	2.50	0.53	179.36	32.23	0.152	–	S
609	23 52 14.56	0.70	-51 12 20.72	1.04	2.415	0.281	1.129	0.187	12.21	2.53	5.54	1.40	150.15	17.32	0.166	–	S
610	23 57 16.17	0.18	-59 15 43.51	0.18	6.915	0.527	6.699	0.426	1.97	0.26	0.57	0.25	96.47	44.35	0.211	–	S
611	23 52 03.58	0.36	-50 51 40.47	0.43	3.727	0.338	2.250	0.219	8.08	0.96	5.30	0.76	150.72	21.29	0.167	–	S
612	23 53 13.37	0.27	-53 11 37.77	0.17	18.124	1.250	14.757	0.872	0.00	0.54	0.00	0.15	0.00	2.18	0.318	0.01	M
613	23 54 57.32	0.42	-56 04 58.66	0.48	1.700	0.302	1.486	0.191	4.47	1.10	0.09	0.89	145.99	32.42	0.168	–	S
614	23 54 43.80	0.17	-55 45 28.16	0.18	7.317	0.479	6.333	0.382	3.62	0.22	2.56	0.21	32.21	15.37	0.152	-0.12	S
615	23 57 12.16	0.41	-59 14 19.78	0.63	8.567	0.665	2.760	0.255	11.48	1.55	2.97	0.66	58.87	9.82	0.205	–	M
616	23 53 45.43	0.17	-54 12 00.91	0.19	9.201	0.603	7.287	0.450	5.12	0.27	3.03	0.23	137.77	7.66	0.194	–	S
617	23 54 37.06	1.00	-55 38 18.16	0.68	5.124	0.418	1.727	0.256	13.78	2.33	8.76	1.54	71.16	17.80	0.227	–	S
618	23 56 51.58	0.51	-58 50 02.79	0.47	2.575	0.289	1.550	0.190	6.71	1.17	6.03	1.04	65.45	119.25	0.157	–	S
619	23 55 02.93	0.22	-56 18 43.22	0.25	5.061	0.385	3.650	0.263	5.91	0.48	3.82	0.40	179.62	11.23	0.161	–	S
620	23 54 54.05	0.14	-56 05 43.47	0.15	47.836	2.648	45.419	2.504	2.66	0.03	0.00	0.03	162.76	177.87	0.174	-0.55	S
621	23 54 02.77	1.11	-54 43 53.70	1.57	2.851	0.268	0.864	0.177	16.65	3.93	8.27	2.09	148.02	19.25	0.167	–	S
622	23 54 48.35	0.60	-55 58 25.04	1.03	4.906	0.414	1.311	0.177	10.96	2.69	0.00	0.66	57.67	10.65	0.161	–	M
623	23 55 27.58	0.28	-56 57 37.58	0.31	3.941	0.336	2.673	0.222	6.30	0.65	4.48	0.55	12.87	17.23	0.156	–	S
624	23 52 47.54	0.96	-52 29 54.06	1.48	2.289	0.243	0.814	0.164	14.88	3.56	7.48	1.98	153.39	21.22	0.152	–	S
625	23 56 57.65	0.84	-59 00 53.03	0.96	2.147	0.374	1.215	0.252	7.48	2.32	6.18	1.86	174.38	78.10	0.224	–	S
626	23 55 19.56	0.30	-56 47 56.49	0.30	3.297	0.321	2.494	0.216	5.47	0.67	3.31	0.56	38.12	18.24	0.158	–	S
627	23 51 44.93	0.93	-50 24 29.22	0.66	2.832	0.400	1.565	0.267	9.60	2.27	5.09	1.42	97.15	23.10	0.235	–	S
628	23 52 09.23	1.09	-51 16 27.17	0.73	1.316	0.260	0.828	0.172	8.29	2.57	3.97	1.67	87.21	31.48	0.155	–	S
629	23 54 19.20	0.14	-55 15 43.37	0.15	21.792	1.229	21.449	1.190	1.74	0.06	0.00	0.06	127.63	5.57	0.158	0.50	S
630	23 54 32.79	0.37	-55 38 40.17	0.65	6.499	0.634	2.328	0.266	9.52	1.56	0.00	0.66	65.77	11.15	0.233	–	M
631	23 53 42.30	0.77	-54 13 28.80	0.75	1.521	0.310	1.059	0.201	5.69	1.82	4.92	1.69	104.73	175.14	0.181	–	S
632	23 52 16.45	0.67	-51 34 38.73	0.88	1.896	0.262	1.040	0.176	9.14	2.01	5.77	1.55	156.43	36.27	0.154	–	S
633	23 56 20.75	0.96	-58 18 34.05	0.88	3.600	0.423	0.826	0.187	0.00	2.94	0.00	0.72	0.00	15.17	0.181	–	M
634	23 51 54.90	0.66	-50 52 14.83	0.88	1.943	0.271	1.100	0.180	9.90	2.16	4.53	1.32	145.63	21.27	0.159	–	S
635	23 55 32.54	0.44	-57 12 34.20	0.48	3.755	0.307	1.841	0.190	10.22	1.19	5.95	0.82	137.20	11.24	0.150	–	S
636	23 53 12.59	0.52	-53 33 24.91	0.64	11.154	0.754	3.856	0.396	14.97	1.68	7.50	0.84	30.94	5.66	0.324	–	S
637	23 51 47.14	0.78	-50 36 49.47	0.54	1.302	0.306	1.091	0.190	0.00	1.87	0.00	1.19	0.00	26.43	0.176	–	S
638	23 52 52.94	0.49	-52 52 39.94	0.64	3.336	0.457	2.359	0.215	11.13	1.74	0.00	0.60	119.52	9.49	0.171	–	M
639	23 55 46.04	0.26	-57 33 17.63	0.35	3.292	0.291	2.280	0.193	7.15	0.74	2.89	0.50	168.74	6.95	0.139	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
640	23 55 29.79	0.44	-57 14 20.10	0.69	3.071	0.280	1.471	0.178	10.64	1.57	5.76	0.96	0.84	11.30	0.148	–	S
641	23 52 13.38	0.18	-51 39 48.83	0.19	8.707	0.593	7.211	0.451	4.39	0.28	3.01	0.25	119.30	16.86	0.206	–	S
642	23 54 52.84	0.58	-56 19 46.50	0.66	2.689	0.303	1.444	0.199	8.99	1.63	5.63	1.15	26.99	20.70	0.170	–	S
643	23 56 03.15	0.18	-58 01 52.92	0.19	4.722	0.360	4.278	0.278	3.55	0.30	0.96	0.27	139.81	12.19	0.145	–	S
644	23 53 26.81	0.45	-54 02 26.95	0.74	5.234	0.388	1.974	0.224	13.54	1.69	7.41	1.00	165.26	9.63	0.185	–	S
645	23 53 30.07	0.65	-54 08 08.25	0.71	2.901	0.292	1.397	0.190	11.61	1.93	5.21	1.07	133.82	12.34	0.163	–	S
646	23 53 11.80	0.15	-53 36 54.46	0.17	28.503	1.648	20.625	1.180	6.29	0.17	3.45	0.13	16.66	179.63	0.307	-1.04	S
647	23 51 58.16	0.15	-51 15 03.62	0.16	10.749	0.657	9.783	0.564	2.87	0.15	2.27	0.15	108.56	30.41	0.167	-0.00	S
648	23 53 54.72	0.37	-54 55 33.71	0.38	2.418	0.285	1.816	0.188	4.95	0.84	4.22	0.78	37.31	68.21	0.151	–	S
649	23 52 05.76	0.69	-51 39 35.42	0.52	1.889	0.334	1.408	0.215	6.73	1.64	2.18	1.10	102.22	24.32	0.191	–	S
650	23 56 39.90	0.36	-59 04 11.70	0.31	32.786	1.901	7.496	0.515	15.52	0.86	9.51	0.53	141.82	6.95	0.309	–	M
651	23 55 47.30	0.81	-57 53 26.67	0.70	1.203	0.252	0.860	0.163	6.85	2.00	2.85	1.42	119.16	34.29	0.147	–	S
652	23 52 41.89	0.65	-52 52 35.18	0.78	2.549	0.320	1.367	0.213	8.67	1.80	6.37	1.46	20.13	38.76	0.184	–	S
653	23 55 52.05	0.57	-58 00 18.35	0.79	1.885	0.256	1.095	0.169	8.95	1.91	4.05	1.16	17.15	16.77	0.148	–	S
654	23 53 57.77	0.88	-55 07 41.48	0.79	1.697	0.254	0.923	0.171	7.94	2.07	6.68	1.78	66.68	82.04	0.151	–	S
655	23 56 03.46	0.58	-58 16 12.12	0.62	1.201	0.263	0.991	0.166	4.27	1.49	2.87	1.25	153.17	92.62	0.150	–	S
656	23 54 49.93	0.77	-56 32 10.93	1.00	2.487	0.295	1.107	0.199	10.18	2.31	7.51	1.79	179.23	37.85	0.176	–	S
657	23 51 18.82	0.63	-50 03 22.08	0.55	2.309	0.367	1.626	0.239	6.31	1.47	4.25	1.23	89.99	42.09	0.208	–	S
658	23 54 48.44	0.62	-56 33 46.12	0.95	2.304	0.319	1.237	0.213	9.47	2.20	5.12	1.42	2.98	22.61	0.189	–	S
659	23 51 20.66	0.52	-50 17 49.64	0.92	104.315	5.806	12.827	0.794	37.68	2.13	22.48	1.17	89.64	6.46	0.364	–	M
660	23 53 43.69	0.78	-54 53 24.48	0.85	2.646	0.280	1.138	0.187	9.62	2.01	8.82	1.77	6.05	103.83	0.162	–	S
661	23 51 43.15	0.41	-51 05 25.56	0.54	2.248	0.290	1.578	0.190	6.74	1.18	3.90	0.93	176.00	28.61	0.159	–	S
662	23 57 07.34	0.17	-59 47 17.14	0.18	14.134	0.905	11.096	0.675	4.52	0.23	3.64	0.23	121.14	24.58	0.276	-1.13	S
663	23 52 34.67	0.65	-52 50 28.22	0.51	2.185	0.298	1.455	0.194	8.56	1.68	1.62	0.87	54.74	11.61	0.169	–	S
664	23 52 07.48	0.42	-52 00 41.09	0.45	2.195	0.333	1.797	0.215	5.00	1.03	2.52	0.89	138.30	39.06	0.183	–	S
665	23 52 08.89	0.16	-52 05 34.04	0.17	8.955	0.576	7.883	0.469	3.56	0.20	2.40	0.19	172.31	18.27	0.174	0.11	S
666	23 56 51.87	0.69	-59 32 32.32	0.61	1.544	0.313	1.159	0.201	5.21	1.63	3.74	1.34	56.51	81.04	0.180	–	S
667	23 54 40.81	0.85	-56 31 25.72	1.18	1.669	0.291	0.905	0.196	9.80	2.87	4.69	1.78	152.25	28.07	0.177	–	S
668	23 54 20.48	0.46	-56 00 12.57	0.50	2.004	0.282	1.448	0.184	5.56	1.14	4.28	1.01	158.42	64.56	0.156	–	S
669	23 52 14.16	0.25	-52 17 39.16	0.26	4.178	0.356	3.222	0.246	5.43	0.53	3.38	0.45	132.43	19.57	0.162	–	S
670	23 51 47.31	0.25	-51 22 37.64	0.31	3.310	0.336	2.753	0.230	5.10	0.64	1.94	0.50	161.57	17.02	0.167	–	S
671	23 51 46.23	0.81	-51 19 56.47	0.88	1.256	0.242	0.807	0.160	7.20	2.08	5.06	1.82	134.41	73.03	0.143	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
672	23 51 23.97	0.24	-50 33 13.10	0.25	4.611	0.427	4.001	0.302	3.36	0.47	3.09	0.44	123.75	175.61	0.201	-	S
673	23 51 26.37	0.85	-50 40 50.88	0.81	8.763	0.642	2.198	0.243	17.48	2.63	1.20	0.69	132.16	8.63	0.210	-	M
674	23 51 31.96	0.27	-50 52 51.42	0.29	3.382	0.362	2.928	0.247	3.37	0.58	3.11	0.55	1.37	175.59	0.182	-	S
675	23 52 02.66	0.19	-51 57 47.96	0.21	7.840	0.575	6.500	0.427	4.42	0.34	2.96	0.31	161.41	21.37	0.224	-	S
676	23 51 23.36	1.35	-50 36 05.77	1.53	6.819	0.448	1.218	0.220	18.56	3.45	16.84	3.27	25.01	78.48	0.225	-	S
677	23 54 40.36	0.51	-56 35 58.97	0.61	4.041	0.355	1.843	0.224	9.53	1.37	7.78	1.18	172.47	34.52	0.184	-	S
678	23 51 49.39	0.87	-51 32 16.14	1.33	1.932	0.276	0.890	0.189	11.14	3.01	6.66	2.04	6.49	33.44	0.170	-	S
679	23 56 06.35	0.74	-58 40 18.90	1.13	4.079	0.361	1.417	0.229	14.05	2.72	7.56	1.51	14.24	13.86	0.208	-	S
680	23 54 52.96	0.44	-56 59 16.68	0.51	1.859	0.304	1.481	0.195	4.78	1.14	3.08	0.99	165.91	52.95	0.170	-	S
681	23 53 42.86	0.52	-55 08 59.65	0.42	1.924	0.272	1.429	0.177	6.42	1.23	2.43	0.86	59.57	18.92	0.150	-	S
682	23 52 45.67	1.03	-53 31 48.46	1.00	2.558	0.330	1.131	0.226	10.08	2.57	8.03	2.11	46.27	52.41	0.201	-	S
683	23 55 28.84	0.85	-57 55 01.76	0.80	1.060	0.221	0.720	0.143	7.18	2.21	3.26	1.51	41.72	32.52	0.130	-	S
684	23 51 46.57	1.25	-51 37 44.55	1.19	1.814	0.260	0.811	0.179	12.55	3.51	5.85	1.94	125.32	24.48	0.163	-	S
685	23 53 27.48	0.77	-54 48 23.00	0.64	1.068	0.271	0.886	0.169	4.80	1.78	2.09	1.45	72.63	59.40	0.156	-	S
686	23 53 01.57	0.58	-54 03 34.21	0.76	2.145	0.309	1.306	0.205	7.83	1.71	5.04	1.34	167.39	35.99	0.178	-	S
687	23 51 10.79	2.20	-50 25 17.99	1.88	37.393	2.063	1.473	0.180	50.04	5.93	33.01	3.50	54.84	10.04	0.306	-	S
688	23 51 00.96	1.70	-50 03 14.08	1.48	5.360	0.366	0.985	0.194	20.53	4.30	14.69	3.10	112.39	30.83	0.199	-	S
689	23 55 36.26	0.17	-58 10 12.09	0.18	9.582	0.593	7.346	0.438	5.79	0.24	2.62	0.18	135.19	1.22	0.162	-0.84	S
690	23 55 46.68	0.59	-58 25 52.37	1.14	8.864	0.526	1.648	0.192	22.78	2.68	11.23	1.30	165.99	5.63	0.185	-	S
691	23 54 08.35	0.15	-56 04 06.77	0.16	48.940	2.722	23.861	1.330	10.01	0.13	8.23	0.11	175.84	3.52	0.217	-0.42	M
692	23 54 58.10	0.27	-57 22 15.41	0.36	6.711	0.440	3.109	0.243	10.36	0.77	6.63	0.54	164.82	5.67	0.160	-	S
693	23 51 04.85	0.48	-50 25 20.82	1.63	15.941	1.081	4.514	0.401	21.70	3.89	1.99	0.79	74.54	8.91	0.315	-	M
694	23 51 01.81	2.16	-50 17 31.89	1.78	16.719	0.967	1.738	0.289	35.51	6.14	16.06	2.64	119.52	11.66	0.358	-	S
695	23 52 24.18	0.83	-53 09 02.39	0.89	3.187	0.360	1.406	0.242	9.67	2.10	8.54	1.88	30.82	74.14	0.211	-	S
696	23 51 59.71	0.14	-52 21 35.45	0.15	71.430	3.940	68.845	3.790	2.11	0.02	0.85	0.02	127.47	179.48	0.170	-0.48	S
697	23 51 19.01	0.20	-50 56 46.17	0.20	8.600	0.576	6.375	0.408	5.40	0.34	4.25	0.29	88.94	14.82	0.197	-	S
698	23 53 36.37	2.27	-55 20 35.98	1.37	12.143	0.781	0.946	0.183	23.29	5.90	8.43	2.01	22.02	17.94	0.175	-	M
699	23 54 19.61	0.28	-56 30 24.56	0.27	3.196	0.356	2.822	0.242	3.52	0.58	2.09	0.54	60.64	42.43	0.181	-	S
700	23 53 51.74	1.06	-55 46 52.36	1.05	3.708	0.310	1.102	0.194	12.80	2.61	11.69	2.29	42.27	75.41	0.177	-	S
701	23 55 05.70	0.19	-57 41 24.11	0.20	5.456	0.406	4.606	0.303	3.76	0.32	3.00	0.31	125.23	46.98	0.161	-	S
702	23 54 56.03	1.48	-57 27 44.20	0.92	2.084	0.225	0.743	0.153	14.15	3.49	7.35	1.97	66.25	20.91	0.141	-	S
703	23 54 15.60	0.22	-56 28 01.16	0.24	16.074	0.947	5.217	0.342	7.83	0.44	6.59	0.39	99.58	26.50	0.187	-	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
704	23 54 05.86	0.26	-56 12 01.11	0.33	3.555	0.330	2.615	0.221	6.20	0.68	3.07	0.52	162.21	12.08	0.159	–	S
705	23 51 46.57	0.49	-52 00 55.31	0.62	2.986	0.336	1.716	0.221	8.38	1.39	5.69	1.13	159.01	32.41	0.185	–	S
706	23 54 24.54	0.73	-56 42 28.23	1.32	2.479	0.279	1.036	0.186	13.77	3.19	4.97	1.38	14.15	12.59	0.172	–	S
707	23 52 00.46	0.39	-52 33 33.51	0.47	2.721	0.291	1.762	0.191	6.97	1.03	4.97	0.86	14.79	29.45	0.153	–	S
708	23 51 18.18	0.32	-51 06 51.68	0.37	3.394	0.402	2.741	0.266	5.15	0.79	2.76	0.68	152.29	29.88	0.210	–	S
709	23 53 11.71	0.14	-54 48 23.18	0.15	23.386	1.319	21.422	1.191	2.67	0.07	2.15	0.07	17.81	11.61	0.171	0.00	S
710	23 56 08.96	0.64	-59 14 59.25	0.77	2.127	0.287	1.184	0.191	8.31	1.85	5.49	1.37	17.70	28.81	0.167	–	S
711	23 52 03.07	1.30	-52 43 28.32	1.37	1.744	0.211	0.660	0.145	14.62	3.92	6.66	2.02	131.49	21.66	0.135	–	S
712	23 56 39.83	0.21	-59 55 31.11	0.22	9.592	0.824	8.445	0.601	3.20	0.38	2.45	0.37	20.68	43.30	0.370	–	S
713	23 53 36.50	0.67	-55 32 21.20	0.83	1.701	0.292	1.071	0.193	7.29	1.92	4.89	1.55	162.16	48.52	0.171	–	S
714	23 52 40.29	0.51	-53 55 36.44	0.70	1.525	0.281	1.156	0.180	6.24	1.57	2.48	1.16	165.91	30.74	0.161	–	S
715	23 50 48.53	0.15	-50 13 01.73	0.16	18.045	1.087	16.848	0.963	3.12	0.15	0.00	0.12	60.65	4.49	0.258	-0.89	S
716	23 54 55.63	0.90	-57 38 28.05	1.59	2.280	0.238	0.765	0.162	14.52	3.71	7.86	2.07	179.05	21.01	0.151	–	S
717	23 53 37.98	0.76	-55 39 03.02	0.81	1.239	0.326	0.980	0.206	4.49	1.90	3.65	1.73	14.63	165.25	0.189	–	S
718	23 55 56.06	0.84	-59 03 15.85	1.35	3.564	0.343	1.198	0.226	14.07	3.20	8.04	1.86	7.45	18.73	0.209	–	S
719	23 52 59.06	0.31	-54 34 03.50	0.38	3.419	0.368	2.531	0.244	5.88	0.82	3.49	0.67	169.00	22.64	0.190	–	S
720	23 55 52.75	0.85	-58 59 33.88	0.86	1.717	0.323	1.047	0.215	6.72	2.19	5.76	1.80	29.00	100.54	0.192	–	S
721	23 54 23.56	0.57	-56 53 25.31	0.56	3.045	0.340	1.717	0.224	8.61	1.43	5.32	1.08	129.90	23.48	0.188	–	S
722	23 51 10.03	0.49	-51 03 37.92	0.49	2.122	0.340	1.692	0.218	5.98	1.27	1.65	0.91	125.59	23.71	0.189	–	S
723	23 51 55.34	0.24	-52 38 56.55	0.24	4.127	0.347	3.313	0.244	4.52	0.46	3.51	0.44	106.95	38.81	0.156	–	S
724	23 54 47.54	0.29	-57 32 48.57	0.40	3.874	0.304	2.182	0.191	8.89	0.87	4.85	0.58	168.47	7.28	0.138	–	S
725	23 56 05.68	0.84	-59 20 19.05	0.71	1.935	0.338	1.193	0.224	6.98	1.97	5.36	1.62	86.93	91.33	0.199	–	S
726	23 51 47.69	1.35	-52 26 53.83	1.10	3.969	0.279	0.912	0.152	19.54	3.55	10.95	2.01	116.71	16.25	0.147	–	S
727	23 53 22.66	0.18	-55 24 10.01	0.18	9.205	0.617	7.733	0.477	4.06	0.25	2.87	0.24	115.87	19.44	0.208	–	S
728	23 51 35.86	0.58	-52 05 53.64	0.68	2.153	0.296	1.321	0.196	7.29	1.53	5.61	1.34	20.81	52.08	0.168	–	S
729	23 53 05.31	0.25	-54 55 28.67	0.29	5.060	0.411	3.551	0.276	6.13	0.57	4.21	0.48	4.17	16.24	0.183	–	S
730	23 52 20.56	0.18	-53 35 08.38	0.20	8.001	0.572	6.677	0.430	4.41	0.32	2.59	0.27	16.76	12.20	0.215	–	S
731	23 54 17.10	0.59	-56 53 09.21	0.73	2.438	0.383	1.557	0.252	7.04	1.69	4.74	1.34	6.14	39.46	0.221	–	S
732	23 51 30.79	0.61	-52 01 50.05	2.18	7.378	0.534	1.297	0.198	21.10	5.23	0.00	0.85	73.21	10.57	0.185	–	M
733	23 51 58.34	0.50	-52 55 38.38	0.48	2.306	0.263	1.441	0.173	6.97	1.14	5.59	1.05	109.13	55.11	0.142	–	S
734	23 52 09.85	0.28	-53 19 07.53	0.16	42.736	2.426	23.259	1.303	0.00	0.58	0.00	0.14	0.00	1.78	0.249	-0.81	M
735	23 54 12.23	0.47	-56 49 28.26	0.48	2.894	0.517	2.442	0.328	4.23	1.14	2.32	0.98	35.59	52.69	0.289	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
736	23 54 46.03	0.36	-57 41 13.68	0.42	2.573	0.309	1.889	0.203	5.61	0.92	3.74	0.78	174.82	30.37	0.165	–	S
737	23 52 43.19	0.72	-54 23 30.71	1.16	2.571	0.316	1.158	0.214	11.35	2.65	6.46	1.69	175.71	24.40	0.191	–	S
738	23 51 47.63	0.94	-52 41 07.35	0.90	1.517	0.255	0.854	0.171	8.77	2.38	5.55	1.83	123.49	44.13	0.153	–	S
739	23 55 39.87	0.78	-59 00 17.83	0.64	1.744	0.300	1.144	0.196	7.75	1.89	3.42	1.30	118.14	26.39	0.175	–	S
740	23 54 29.17	0.24	-57 24 09.19	0.30	5.280	0.410	3.493	0.270	7.15	0.61	3.93	0.45	166.73	7.55	0.178	–	S
741	23 50 47.25	0.37	-50 39 45.76	0.29	6.899	0.575	4.351	0.373	7.92	0.84	4.45	0.56	90.44	9.76	0.267	–	S
742	23 52 37.42	0.65	-54 26 24.55	0.55	13.092	0.824	2.671	0.267	13.65	1.49	11.53	1.25	0.17	33.37	0.223	–	M
743	23 53 07.82	0.34	-55 18 41.86	0.37	3.463	0.341	2.340	0.225	6.07	0.79	4.99	0.74	156.58	52.33	0.172	–	S
744	23 55 10.35	0.84	-58 28 57.92	0.45	8.378	0.605	2.347	0.229	11.84	1.95	5.65	1.01	176.46	14.95	0.189	–	M
745	23 52 01.71	0.65	-53 19 37.38	0.78	1.616	0.426	1.388	0.262	5.62	1.93	0.00	1.29	143.19	31.50	0.245	–	S
746	23 50 54.96	0.16	-51 07 23.83	0.16	74.825	4.155	30.627	1.714	14.56	0.20	8.89	0.13	141.85	1.99	0.318	-1.03	M
747	23 53 59.19	0.15	-56 49 31.84	0.17	86.929	4.852	45.618	2.532	13.00	0.23	0.00	0.08	115.51	1.07	0.338	-0.86	M
748	23 55 33.21	0.78	-59 05 50.14	0.83	1.418	0.308	0.984	0.200	6.36	2.08	3.93	1.62	143.18	56.36	0.181	–	S
749	23 55 45.86	0.23	-59 24 24.38	0.22	6.478	0.461	4.493	0.312	5.53	0.41	4.85	0.39	70.45	51.67	0.178	–	S
750	23 52 41.37	0.53	-54 42 31.07	0.66	2.553	0.357	1.623	0.235	7.25	1.49	4.85	1.22	161.64	38.53	0.202	–	S
751	23 55 22.22	0.75	-58 54 17.74	0.78	4.308	0.348	1.484	0.212	10.94	1.89	10.65	1.65	177.06	104.27	0.184	–	S
752	23 50 44.70	0.44	-50 52 36.66	0.50	4.423	0.459	2.687	0.300	8.37	1.20	4.86	0.87	139.15	19.67	0.243	–	S
753	23 54 03.91	1.16	-57 01 45.42	1.01	1.572	0.245	0.752	0.169	9.36	2.80	7.15	2.21	55.44	60.50	0.151	–	S
754	23 53 03.10	0.14	-55 30 08.10	0.15	26.209	1.488	25.807	1.435	1.74	0.07	0.00	0.07	139.46	6.69	0.212	-0.13	S
755	23 53 05.94	0.78	-55 36 21.24	0.80	3.977	0.398	1.664	0.262	9.71	1.93	9.07	1.71	30.49	94.46	0.227	–	S
756	23 51 13.86	0.14	-52 08 40.10	0.16	19.805	1.130	17.181	0.962	4.80	0.11	0.00	0.08	11.75	178.62	0.176	-1.00	S
757	23 52 40.12	0.77	-54 53 15.84	0.52	1.605	0.272	1.110	0.177	7.33	1.75	3.01	1.18	89.47	24.61	0.157	–	S
758	23 50 22.83	0.26	-50 14 57.08	0.28	9.027	0.657	5.722	0.425	7.54	0.61	4.86	0.44	39.25	8.96	0.266	–	S
759	23 50 45.81	0.17	-51 07 20.03	0.18	13.091	0.885	11.653	0.711	3.86	0.25	1.69	0.21	161.47	11.16	0.300	–	S
760	23 50 53.09	0.48	-51 24 41.93	0.70	2.514	0.266	1.350	0.174	9.70	1.57	5.58	1.08	166.12	20.01	0.146	–	S
761	23 55 51.28	0.23	-59 44 03.91	0.24	6.036	0.476	4.523	0.329	4.92	0.44	4.04	0.42	167.86	27.65	0.204	–	S
762	23 53 13.79	0.63	-55 53 58.37	0.98	1.186	0.262	0.845	0.168	7.16	2.26	2.24	1.45	4.14	29.01	0.154	–	S
763	23 52 52.31	0.49	-55 20 04.58	0.40	2.126	0.324	1.714	0.209	5.80	1.14	1.09	0.82	110.81	20.18	0.179	–	S
764	23 53 20.32	0.16	-56 08 14.03	0.17	9.572	0.634	7.838	0.458	4.13	0.20	0.00	0.14	46.81	4.57	0.153	0.28	M
765	23 55 48.53	0.41	-59 43 24.63	0.38	3.006	0.390	2.304	0.255	4.76	0.92	3.83	0.80	57.99	76.95	0.210	–	S
766	23 50 42.41	0.51	-51 07 24.92	0.49	2.084	0.472	1.995	0.289	0.00	1.20	0.00	1.05	0.00	53.47	0.265	–	S
767	23 53 53.03	0.40	-57 00 44.51	0.40	3.051	0.317	1.985	0.208	6.41	0.92	5.18	0.83	134.30	55.16	0.165	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
768	23 54 26.02	0.22	-57 50 41.68	0.26	3.245	0.289	2.673	0.203	4.83	0.50	1.94	0.41	2.24	11.49	0.134	–	S
769	23 54 05.51	0.44	-57 20 04.61	0.72	2.578	0.351	1.644	0.229	8.35	1.64	3.03	0.98	174.03	14.65	0.199	–	S
770	23 52 46.33	0.36	-55 11 45.42	0.41	2.763	0.298	1.909	0.196	5.93	0.88	4.71	0.79	15.01	41.62	0.155	–	S
771	23 55 06.22	0.77	-58 48 55.58	0.76	3.184	0.337	1.400	0.223	9.18	1.81	8.52	1.73	145.13	154.39	0.193	–	S
772	23 51 06.48	0.15	-52 02 55.96	0.16	16.110	0.953	14.901	0.845	2.55	0.12	2.09	0.12	170.91	134.43	0.203	-0.61	S
773	23 51 58.16	0.16	-53 47 34.62	0.17	10.750	0.655	9.142	0.531	3.83	0.17	2.92	0.16	138.78	18.31	0.165	-0.81	S
774	23 51 25.98	0.26	-52 44 59.43	0.19	22.859	1.336	13.732	0.778	15.02	0.56	0.00	0.16	151.79	2.15	0.186	-0.72	M
775	23 55 05.08	0.42	-58 49 35.06	0.45	5.191	0.420	2.523	0.259	8.37	1.02	7.71	0.93	174.66	50.06	0.201	–	S
776	23 51 04.25	0.22	-51 59 55.85	0.25	5.957	0.443	4.265	0.302	5.77	0.46	4.48	0.41	11.67	22.82	0.179	–	S
777	23 51 12.42	0.57	-52 18 12.46	0.58	1.634	0.257	1.152	0.167	5.92	1.36	4.61	1.25	124.16	85.68	0.145	–	S
778	23 50 27.77	0.15	-50 42 47.06	0.17	97.888	5.504	39.912	2.241	12.11	0.22	7.47	0.14	110.81	2.48	0.450	-1.09	M
779	23 52 28.73	1.21	-54 49 07.65	1.26	4.523	0.301	0.975	0.152	21.13	3.67	10.37	1.71	38.93	10.92	0.150	–	S
780	23 50 56.26	0.40	-51 47 57.70	0.47	2.837	0.294	1.781	0.192	7.63	1.07	4.96	0.86	148.07	25.73	0.154	–	S
781	23 51 38.48	1.26	-53 15 45.32	1.18	1.731	0.244	0.781	0.167	12.73	3.65	5.03	1.70	44.41	18.85	0.154	–	S
782	23 52 38.96	0.46	-55 08 41.99	0.39	1.298	0.268	1.293	0.165	0.00	1.03	0.00	0.83	0.00	35.18	0.149	–	S
783	23 53 16.19	0.15	-56 14 22.43	0.16	9.200	0.565	8.754	0.504	2.10	0.14	1.43	0.14	152.94	124.98	0.146	-0.47	S
784	23 52 06.68	0.26	-54 12 45.94	0.29	3.930	0.374	3.154	0.257	4.72	0.56	3.20	0.51	159.54	31.87	0.181	–	S
785	23 52 47.95	0.68	-55 27 46.08	0.66	2.315	0.297	1.307	0.197	8.77	1.73	5.25	1.28	127.93	27.46	0.170	–	S
786	23 54 34.33	0.53	-58 15 08.08	0.60	1.096	0.264	0.992	0.163	3.56	1.40	0.72	1.16	162.48	66.76	0.150	–	S
787	23 52 50.73	0.17	-55 34 58.93	0.19	8.609	0.649	8.285	0.524	0.00	0.26	0.00	0.25	0.00	25.42	0.257	–	S
788	23 51 20.37	0.20	-52 48 20.34	0.18	19.319	1.122	8.234	0.487	11.01	0.34	6.01	0.21	6.36	3.72	0.180	–	M
789	23 54 43.77	0.64	-58 32 06.14	0.61	2.762	0.333	1.513	0.221	7.44	1.44	6.81	1.42	105.99	84.93	0.188	–	S
790	23 55 16.04	0.80	-59 19 18.63	0.81	1.151	0.284	0.853	0.182	4.78	1.88	4.43	1.86	4.95	174.82	0.166	–	S
791	23 50 14.10	0.38	-50 34 01.04	0.18	235.164	13.076	79.675	4.434	28.48	0.83	6.76	0.21	4.16	1.87	0.678	-0.96	M
792	23 52 01.85	1.07	-54 16 23.22	0.84	1.471	0.305	0.910	0.203	7.47	2.47	5.07	1.97	80.66	60.08	0.182	–	S
793	23 55 00.28	0.62	-59 01 35.42	0.67	2.046	0.364	1.426	0.236	6.34	1.64	3.86	1.30	144.87	43.16	0.210	–	S
794	23 51 11.09	0.20	-52 38 46.95	0.21	4.874	0.366	4.061	0.271	4.24	0.35	3.01	0.32	144.94	28.20	0.147	–	S
795	23 50 24.87	0.35	-50 58 30.30	0.43	3.461	0.358	2.371	0.236	7.42	0.98	3.61	0.69	147.26	15.41	0.184	–	S
796	23 55 30.71	0.14	-59 43 49.96	0.15	29.863	1.682	27.866	1.548	2.17	0.06	1.99	0.06	170.97	119.29	0.211	-0.65	S
797	23 54 56.11	0.95	-58 58 15.09	0.74	1.517	0.298	0.959	0.197	7.17	2.19	4.77	1.73	91.64	63.13	0.177	–	S
798	23 53 06.73	0.47	-56 13 26.51	0.49	2.337	0.286	1.544	0.188	6.81	1.19	4.42	0.94	36.16	26.47	0.157	–	S
799	23 50 48.68	0.56	-51 54 13.14	0.52	1.843	0.314	1.426	0.202	5.64	1.34	2.99	1.10	111.55	39.55	0.177	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
800	23 54 51.46	1.00	-58 52 53.83	1.14	4.334	0.367	1.279	0.232	12.97	2.73	11.24	2.28	165.87	56.52	0.213	–	S
801	23 53 27.00	0.27	-56 51 50.17	0.42	6.182	0.518	3.745	0.332	8.84	0.93	3.50	0.54	3.28	5.53	0.245	–	S
802	23 53 47.11	0.19	-57 22 49.86	0.22	20.962	1.245	11.610	0.714	11.01	0.43	2.74	0.20	140.50	178.19	0.305	–	S
803	23 52 59.04	0.36	-56 05 52.71	0.44	5.887	0.417	2.607	0.239	9.97	0.96	7.87	0.80	169.75	19.08	0.176	–	S
804	23 50 18.16	1.58	-50 51 06.72	1.09	4.844	0.384	1.267	0.234	18.58	4.14	9.55	1.94	61.10	15.47	0.226	–	S
805	23 52 39.79	0.14	-55 35 18.86	0.15	166.821	9.205	165.010	9.086	1.24	0.02	0.00	0.02	144.37	4.00	0.429	-0.29	S
806	23 54 50.08	0.23	-58 57 04.61	0.22	5.751	0.453	4.456	0.318	4.77	0.42	3.66	0.40	121.32	33.70	0.193	–	S
807	23 50 24.91	0.41	-51 11 13.73	0.38	2.570	0.301	1.886	0.198	6.59	1.01	3.01	0.72	117.04	17.93	0.160	–	S
808	23 53 43.77	0.89	-57 22 04.12	1.17	9.668	0.637	2.146	0.315	18.73	2.89	11.34	1.80	148.99	14.48	0.301	–	S
809	23 52 16.41	0.21	-54 56 34.82	0.18	6.001	0.523	4.800	0.313	0.00	0.37	0.00	0.21	0.00	5.67	0.169	–	M
810	23 52 34.42	1.78	-55 33 46.64	1.70	19.945	1.122	1.618	0.236	35.53	4.94	20.03	2.89	127.96	12.26	0.309	–	S
811	23 55 14.37	1.25	-59 34 12.08	0.83	1.795	0.262	0.866	0.178	11.49	2.97	4.85	1.67	109.49	21.27	0.162	–	S
812	23 53 03.40	0.60	-56 22 44.68	0.82	1.217	0.269	0.925	0.171	6.03	1.88	2.42	1.38	172.83	37.61	0.156	–	S
813	23 55 20.75	0.61	-59 44 59.48	0.44	2.396	0.402	1.822	0.259	6.00	1.34	2.47	1.02	78.69	28.36	0.227	–	S
814	23 51 28.63	0.56	-53 33 22.37	0.64	1.326	0.348	1.233	0.212	3.15	1.46	0.66	1.28	174.50	98.67	0.198	–	S
815	23 54 38.25	0.94	-58 49 08.09	0.94	5.141	0.377	1.398	0.215	13.66	2.34	11.97	2.00	33.55	45.59	0.196	–	S
816	23 53 31.22	0.41	-57 12 00.28	0.68	2.140	0.271	1.353	0.177	8.48	1.54	3.05	0.91	173.66	13.04	0.152	–	S
817	23 52 55.06	0.70	-56 13 35.27	1.39	2.440	0.262	0.944	0.175	14.02	3.25	6.19	1.58	2.17	15.47	0.161	–	S
818	23 55 17.42	0.25	-59 45 40.63	0.26	4.496	0.467	4.010	0.324	3.54	0.51	1.64	0.47	137.62	30.17	0.231	–	S
819	23 50 55.03	1.38	-52 32 20.09	1.36	4.165	0.275	0.795	0.136	20.47	3.86	13.39	2.37	43.79	19.09	0.138	–	S
820	23 53 20.54	0.72	-56 58 23.76	0.88	1.151	0.326	0.949	0.202	5.71	2.17	0.00	1.48	148.00	37.24	0.189	–	S
821	23 55 16.64	0.14	-59 48 34.35	0.15	127.847	7.057	84.358	4.646	7.81	0.04	1.25	0.02	97.41	0.50	0.247	-0.64	M
822	23 50 08.85	0.56	-50 54 26.56	0.48	4.278	0.384	2.132	0.245	9.14	1.30	7.31	1.06	83.50	28.28	0.198	–	S
823	23 53 21.92	0.79	-57 03 24.65	0.82	2.354	0.300	1.161	0.202	8.54	2.02	7.46	1.72	27.96	73.77	0.176	–	S
824	23 52 34.67	0.68	-55 46 43.58	0.69	2.065	0.330	1.314	0.218	6.83	1.71	5.14	1.43	38.95	54.27	0.191	–	S
825	23 50 36.71	0.33	-52 01 59.03	0.32	57.265	3.227	15.019	0.871	19.00	0.86	10.21	0.43	37.45	4.45	0.278	-1.05	M
826	23 53 31.09	0.52	-57 21 30.37	0.78	10.366	0.655	2.882	0.301	17.47	1.92	8.50	0.92	19.76	4.93	0.258	–	S
827	23 53 40.28	0.53	-57 37 55.74	0.45	2.882	0.343	1.302	0.151	8.15	1.49	0.00	0.48	136.67	8.90	0.133	–	M
828	23 52 27.00	0.70	-55 37 29.05	0.58	3.661	0.418	1.927	0.276	8.66	1.61	6.44	1.31	66.07	35.80	0.235	–	S
829	23 53 29.02	0.90	-57 21 02.27	1.42	3.130	0.404	1.276	0.279	12.14	3.32	6.97	2.06	166.49	27.43	0.254	–	S
830	23 53 01.98	1.87	-56 41 01.24	2.25	10.818	0.903	2.578	0.299	29.38	6.83	0.00	0.60	124.89	7.94	0.263	–	M
831	23 50 35.86	0.58	-52 05 07.96	0.61	1.801	0.413	1.560	0.257	3.54	1.42	2.86	1.31	132.83	175.78	0.235	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
832	23 54 37.02	0.55	-59 04 48.49	0.98	11.264	0.729	2.417	0.239	16.44	2.44	5.57	0.93	62.72	10.63	0.199	–	M
833	23 53 59.93	0.65	-58 09 52.82	0.66	1.899	0.252	1.088	0.167	7.43	1.62	6.09	1.37	31.12	55.49	0.144	–	S
834	23 51 07.78	0.19	-53 13 14.76	0.19	5.170	0.396	4.806	0.310	2.98	0.30	1.05	0.27	83.69	20.58	0.160	–	S
835	23 53 42.41	0.43	-57 44 52.58	0.46	2.356	0.296	1.656	0.194	6.40	1.08	3.73	0.87	140.50	26.17	0.161	–	S
836	23 51 36.58	0.19	-54 11 16.42	0.19	8.022	0.568	6.675	0.428	3.98	0.29	3.24	0.29	130.40	44.12	0.211	–	S
837	23 51 47.76	0.39	-54 35 52.67	0.24	139.750	7.788	39.481	2.213	31.04	0.95	5.51	0.18	20.78	1.63	0.427	-1.19	M
838	23 51 08.65	0.93	-53 18 22.35	0.82	1.918	0.265	0.967	0.179	9.44	2.25	6.63	1.80	112.81	44.80	0.158	–	S
839	23 52 50.98	0.99	-56 28 22.01	0.48	17.208	0.992	2.650	0.229	21.52	2.30	10.60	1.07	175.91	9.66	0.176	–	M
840	23 52 25.21	0.30	-55 45 37.87	0.31	3.618	0.372	2.806	0.250	4.73	0.66	3.84	0.62	148.86	65.41	0.187	–	S
841	23 53 08.60	0.15	-57 00 10.75	0.16	10.916	0.693	10.822	0.628	0.00	0.15	0.00	0.15	0.00	132.19	0.199	-0.20	S
842	23 50 47.14	0.71	-52 41 42.15	1.28	1.236	0.227	0.710	0.151	9.90	2.93	3.93	1.67	174.74	25.66	0.138	–	S
843	23 53 02.54	0.14	-56 53 39.85	0.15	24.152	1.391	23.135	1.295	0.00	0.09	0.00	0.08	0.00	0.84	0.240	-0.93	S
844	23 50 55.71	0.40	-53 01 43.69	0.68	4.132	0.365	2.033	0.230	11.66	1.58	4.90	0.83	162.03	8.78	0.189	–	S
845	23 54 26.28	0.53	-58 59 44.69	0.66	3.183	0.368	1.757	0.243	8.82	1.58	5.20	1.12	152.43	20.43	0.207	–	S
846	23 53 23.36	0.99	-57 27 18.87	1.04	2.687	0.273	0.972	0.183	10.97	2.57	9.97	2.18	24.12	81.13	0.164	–	S
847	23 53 19.72	0.26	-57 23 36.79	0.33	4.430	0.402	3.226	0.270	6.31	0.68	2.99	0.50	167.81	10.42	0.193	–	S
848	23 50 39.79	0.85	-52 32 46.19	1.42	2.908	0.243	0.854	0.152	16.42	3.29	9.28	1.95	165.05	19.95	0.141	–	S
849	23 53 09.88	0.65	-57 09 56.09	1.09	1.923	0.265	0.976	0.178	10.52	2.54	4.94	1.47	168.54	19.90	0.159	–	S
850	23 51 18.33	0.17	-53 56 42.50	0.18	6.895	0.456	5.844	0.357	4.07	0.24	2.68	0.22	164.80	14.81	0.149	–	S
851	23 51 57.34	0.64	-55 10 13.46	1.10	1.602	0.225	0.838	0.151	10.66	2.59	4.41	1.39	8.31	18.03	0.135	–	S
852	23 53 39.02	0.18	-57 59 11.08	0.19	6.034	0.417	5.078	0.319	3.90	0.27	2.87	0.25	153.04	21.31	0.148	–	S
853	23 54 05.87	0.14	-58 41 49.92	0.15	33.902	1.904	23.902	1.327	7.68	0.10	2.26	0.06	130.35	1.32	0.180	-1.02	M
854	23 52 46.55	0.19	-56 38 29.72	0.21	9.965	0.652	6.966	0.446	5.94	0.33	4.42	0.29	159.35	11.25	0.214	–	S
855	23 49 30.19	0.14	-50 04 35.92	0.15	34.546	1.946	30.764	1.711	3.75	0.08	1.73	0.07	29.85	0.66	0.246	-1.27	S
856	23 53 03.33	0.34	-57 08 21.65	0.33	4.087	0.343	2.516	0.221	7.76	0.79	4.70	0.61	128.90	13.09	0.161	–	S
857	23 54 39.41	0.56	-59 30 21.60	0.71	3.796	0.331	1.596	0.208	11.03	1.68	7.31	1.20	156.17	17.76	0.176	–	S
858	23 51 56.47	0.29	-55 14 49.72	0.29	3.433	0.312	2.516	0.210	5.32	0.60	4.33	0.57	125.13	53.73	0.149	–	S
859	23 52 12.61	0.65	-55 44 39.42	0.78	1.237	0.290	0.975	0.183	5.79	1.90	1.58	1.36	23.54	35.69	0.167	–	S
860	23 53 53.41	0.27	-58 28 58.07	0.37	9.246	0.714	4.396	0.321	10.30	0.86	3.38	0.43	112.35	7.35	0.210	–	M
861	23 50 37.10	0.29	-52 43 59.85	0.37	4.125	0.336	2.533	0.217	8.05	0.79	4.81	0.58	158.81	12.58	0.154	–	S
862	23 52 59.31	1.34	-57 06 14.12	0.46	6.383	0.476	1.431	0.181	18.17	3.23	0.00	0.72	161.87	8.72	0.163	–	M
863	23 54 07.78	0.20	-58 53 47.78	0.20	10.453	0.673	6.749	0.437	6.12	0.34	5.48	0.33	56.74	31.27	0.215	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
864	23 53 38.51	0.15	-58 10 52.43	0.16	12.590	0.734	11.602	0.654	2.61	0.10	1.89	0.10	18.44	13.23	0.141	-0.43	S
865	23 51 38.33	0.17	-54 52 55.41	0.17	21.181	1.243	12.387	0.713	8.04	0.23	5.80	0.19	136.02	7.05	0.211	-0.57	M
866	23 53 43.35	1.32	-58 20 53.20	1.15	5.189	0.485	1.343	0.206	13.87	4.03	0.00	0.74	134.62	11.35	0.193	-	M
867	23 53 21.62	1.04	-57 47 23.69	1.15	1.950	0.265	0.845	0.183	10.04	2.84	7.93	2.22	24.34	54.54	0.164	-	S
868	23 53 25.30	0.37	-57 55 22.55	0.50	5.402	0.396	2.445	0.232	11.58	1.18	5.80	0.69	150.31	6.13	0.177	-	S
869	23 53 19.74	0.44	-57 46 46.23	0.43	2.705	0.312	1.809	0.205	6.14	1.02	4.89	0.90	39.41	44.36	0.167	-	S
870	23 49 37.63	1.68	-50 45 20.05	1.12	14.644	0.920	1.910	0.269	24.57	4.54	6.46	1.32	144.57	12.58	0.247	-	M
871	23 50 44.44	0.37	-53 12 18.22	0.32	3.610	0.349	2.484	0.231	6.68	0.83	4.10	0.65	99.20	18.50	0.175	-	S
872	23 53 44.59	0.94	-58 26 20.82	0.91	1.315	0.280	0.846	0.184	7.71	2.52	3.66	1.68	39.99	34.36	0.167	-	S
873	23 52 06.08	0.19	-55 49 36.75	0.21	6.404	0.446	4.901	0.320	5.13	0.34	3.57	0.30	23.87	11.95	0.163	-	S
874	23 49 35.19	0.63	-50 40 51.89	0.70	1.176	0.409	1.225	0.240	0.00	1.61	0.00	1.42	0.00	87.07	0.233	-	S
875	23 53 49.26	0.57	-58 36 40.99	0.85	5.272	0.391	1.778	0.224	14.54	2.04	7.73	1.15	156.20	9.80	0.195	-	S
876	23 54 06.91	0.66	-59 03 24.38	0.74	3.107	0.387	1.655	0.257	8.86	1.84	5.66	1.32	26.60	25.09	0.223	-	S
877	23 51 38.03	0.65	-55 03 21.31	0.84	1.815	0.260	1.028	0.174	8.46	1.94	5.53	1.49	163.54	36.69	0.152	-	S
878	23 49 55.50	0.42	-51 35 12.95	0.45	3.104	0.272	1.690	0.174	7.98	0.98	7.01	0.94	137.02	95.88	0.135	-	S
879	23 49 25.43	0.39	-50 24 57.79	0.37	7.028	0.538	3.649	0.330	8.37	0.88	7.46	0.77	71.26	30.42	0.241	-	S
880	23 52 29.49	1.62	-56 36 18.90	0.98	2.968	0.307	0.958	0.209	14.65	3.70	8.62	2.33	83.93	27.33	0.194	-	S
881	23 51 23.36	0.51	-54 41 56.85	0.39	7.510	0.562	3.618	0.334	12.47	1.32	3.91	0.56	54.08	3.42	0.258	-	S
882	23 51 03.96	0.32	-54 12 30.09	0.73	43.288	2.520	20.989	1.207	27.97	1.79	1.43	0.27	64.75	2.92	0.353	-1.53	M
883	23 51 13.44	0.14	-54 25 54.19	0.15	80.854	4.500	43.679	2.418	8.91	0.09	4.03	0.05	148.17	1.15	0.274	-0.58	M
884	23 52 29.92	1.37	-56 42 09.81	0.97	2.011	0.294	0.924	0.202	12.36	3.42	5.02	1.78	114.11	21.40	0.185	-	S
885	23 50 11.05	0.91	-52 17 53.20	1.08	2.106	0.299	1.009	0.204	9.50	2.49	7.47	2.11	21.25	61.75	0.181	-	S
886	23 50 40.10	0.81	-53 20 47.00	1.04	2.256	0.319	1.120	0.217	9.52	2.36	6.80	1.92	163.85	50.40	0.191	-	S
887	23 50 58.39	0.44	-53 58 23.34	0.55	2.600	0.273	1.512	0.179	7.95	1.21	5.72	1.01	165.16	31.83	0.146	-	S
888	23 50 02.77	0.21	-52 02 46.75	0.24	7.581	0.544	5.418	0.373	6.84	0.47	3.32	0.34	149.71	6.44	0.211	-	S
889	23 54 28.16	0.72	-59 43 43.51	0.68	2.626	0.422	1.629	0.280	6.45	1.71	5.74	1.51	46.78	129.45	0.245	-	S
890	23 52 06.78	0.87	-56 06 12.49	1.23	1.522	0.260	0.821	0.175	10.69	3.09	3.86	1.62	148.48	21.71	0.160	-	S
891	23 49 28.74	0.23	-50 47 47.32	0.24	11.911	0.803	5.506	0.373	6.31	0.45	6.12	0.42	45.22	60.97	0.218	-	M
892	23 50 54.42	0.78	-53 56 29.86	0.86	1.186	0.286	0.876	0.183	5.23	2.01	4.34	1.79	5.24	164.73	0.167	-	S
893	23 52 09.89	1.41	-56 18 42.46	1.37	2.673	0.334	0.714	0.150	12.40	4.57	0.00	0.53	131.23	9.94	0.145	-	M
894	23 51 19.13	1.09	-54 47 51.58	1.42	5.778	0.614	2.320	0.255	18.09	4.11	0.00	0.75	48.78	9.75	0.221	-	M
895	23 50 47.91	0.73	-53 45 52.80	0.80	1.802	0.327	1.180	0.215	7.40	1.97	4.26	1.52	137.62	41.70	0.191	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
896	23 49 44.14	0.97	-51 29 02.93	0.97	2.569	0.301	1.098	0.204	11.00	2.46	8.03	2.00	124.76	46.01	0.180	–	S
897	23 53 08.18	0.25	-57 58 36.20	0.25	4.120	0.360	3.232	0.249	4.35	0.50	3.86	0.46	36.17	61.49	0.166	–	S
898	23 52 47.03	0.45	-57 25 18.73	1.02	3.045	0.288	1.337	0.184	13.86	2.39	3.98	0.94	167.72	7.46	0.164	–	S
899	23 53 49.23	0.27	-59 03 46.71	0.29	6.701	0.539	4.443	0.355	6.40	0.59	4.70	0.52	148.69	19.24	0.241	–	S
900	23 51 57.15	0.15	-56 07 57.16	0.16	14.589	0.848	13.070	0.738	3.26	0.11	2.01	0.10	10.16	5.96	0.161	-0.29	S
901	23 50 01.37	0.78	-52 20 51.48	0.96	1.668	0.232	0.856	0.157	9.55	2.24	6.38	1.76	150.87	42.56	0.138	–	S
902	23 50 21.67	0.93	-53 05 17.45	0.83	2.328	0.260	1.023	0.174	11.58	2.42	6.85	1.60	120.46	24.58	0.154	–	S
903	23 49 17.57	0.64	-50 40 18.10	0.66	3.552	0.436	1.978	0.289	7.56	1.55	7.12	1.44	52.81	101.93	0.247	–	S
904	23 50 18.74	0.76	-53 00 32.25	1.29	1.731	0.257	0.851	0.175	10.96	2.95	5.56	1.77	2.11	26.24	0.157	–	S
905	23 53 13.22	0.92	-58 13 51.88	1.10	1.693	0.249	0.864	0.167	11.70	2.98	3.58	1.40	139.22	15.88	0.153	–	S
906	23 50 08.75	0.65	-52 41 22.36	0.73	3.512	0.277	1.310	0.167	13.04	1.85	8.23	1.26	138.24	17.49	0.141	–	S
907	23 49 29.48	0.75	-51 13 39.57	0.82	1.902	0.448	1.447	0.285	6.20	2.01	2.77	1.57	134.47	48.06	0.260	–	S
908	23 52 09.98	0.66	-56 35 43.89	0.60	1.760	0.339	1.350	0.216	6.80	1.71	0.00	1.08	125.27	21.33	0.194	–	S
909	23 51 53.05	0.33	-56 06 33.33	0.45	2.672	0.319	1.973	0.209	6.34	0.98	2.72	0.71	170.43	16.62	0.170	–	S
910	23 51 19.28	0.32	-55 05 53.65	0.35	3.166	0.303	2.174	0.201	5.76	0.74	5.03	0.69	8.70	58.89	0.151	–	S
911	23 49 36.91	0.76	-51 38 23.84	0.80	2.539	0.263	1.155	0.173	11.82	2.18	6.25	1.31	131.47	18.00	0.150	–	S
912	23 49 34.42	0.61	-51 34 21.70	0.30	5.706	0.450	1.790	0.193	0.00	1.44	0.00	0.48	0.00	8.70	0.166	–	M
913	23 51 57.56	0.50	-56 21 22.79	0.76	1.907	0.241	1.093	0.159	8.91	1.75	4.60	1.13	3.08	18.84	0.137	–	S
914	23 52 23.66	1.30	-57 06 04.28	1.51	2.553	0.256	0.832	0.171	17.22	4.24	6.41	1.78	137.40	15.08	0.164	–	S
915	23 52 14.63	3.20	-56 51 55.69	0.86	6.178	0.429	0.756	0.161	22.38	7.72	0.00	1.06	162.75	13.53	0.156	–	M
916	23 54 00.45	1.19	-59 35 20.28	1.32	4.187	0.472	0.964	0.209	10.55	4.09	0.00	0.74	127.06	13.10	0.202	–	M
917	23 52 25.48	0.96	-57 12 20.30	0.95	4.330	0.307	1.139	0.169	15.92	2.59	10.71	1.73	39.78	17.76	0.155	–	S
918	23 51 10.31	1.06	-55 01 44.81	1.61	2.722	0.254	0.803	0.168	15.68	3.84	9.33	2.29	13.95	23.97	0.158	–	S
919	23 52 40.41	0.65	-57 38 10.59	0.80	1.639	0.247	0.967	0.165	7.65	1.87	5.38	1.46	7.40	40.57	0.144	–	S
920	23 51 55.29	0.35	-56 23 27.01	0.43	2.697	0.302	1.907	0.199	6.18	0.93	3.87	0.75	5.84	23.48	0.159	–	S
921	23 51 08.24	0.14	-54 59 17.98	0.15	64.405	3.555	61.095	3.365	2.16	0.02	1.53	0.02	157.42	2.85	0.173	-0.52	S
922	23 53 24.64	0.37	-58 46 45.71	0.32	2.798	0.378	2.425	0.247	4.29	0.78	1.46	0.67	107.62	29.62	0.202	–	S
923	23 51 57.11	0.58	-56 39 26.84	0.54	6.099	0.508	2.707	0.315	11.15	1.47	6.71	1.01	126.58	14.64	0.258	–	S
924	23 52 47.48	0.23	-57 57 13.91	0.22	4.476	0.363	3.595	0.257	4.52	0.42	3.18	0.39	48.65	22.45	0.158	–	S
925	23 53 40.88	0.14	-59 18 09.39	0.15	32.710	1.830	31.715	1.755	1.71	0.05	0.91	0.05	169.67	98.92	0.192	-0.46	S
926	23 51 42.94	0.30	-56 10 39.98	0.34	4.322	0.359	2.680	0.232	7.01	0.73	5.36	0.62	15.51	20.93	0.166	–	S
927	23 49 05.65	1.27	-50 44 39.07	1.85	4.716	0.369	1.120	0.224	21.17	4.74	9.62	2.22	146.02	17.30	0.222	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
928	23 51 19.65	0.49	-55 29 51.76	0.65	7.216	0.498	2.493	0.269	13.19	1.49	8.91	1.06	159.19	13.77	0.219	–	S
929	23 49 51.57	0.45	-52 32 11.31	0.54	2.387	0.286	1.544	0.188	6.86	1.17	5.14	1.04	177.51	46.73	0.156	–	S
930	23 50 01.94	1.05	-52 56 03.64	0.81	3.150	0.302	1.194	0.197	13.02	2.65	7.78	1.59	60.03	19.29	0.176	–	S
931	23 52 01.75	0.22	-56 46 48.56	0.16	17.870	1.085	11.781	0.675	0.00	0.40	0.00	0.14	0.00	2.12	0.189	-0.30	M
932	23 50 20.47	0.29	-53 36 59.95	0.32	12.584	0.870	6.569	0.515	9.16	0.74	6.22	0.53	32.14	8.89	0.340	–	S
933	23 53 22.80	0.14	-58 57 28.06	0.15	268.637	14.919	247.946	13.692	2.37	0.04	2.14	0.04	56.13	110.42	1.203	-0.56	S
934	23 53 13.25	0.72	-58 41 48.42	1.23	1.566	0.277	0.884	0.185	10.14	2.95	3.15	1.50	159.72	19.68	0.169	–	S
935	23 49 20.49	0.18	-51 32 29.49	0.20	7.309	0.508	6.068	0.384	4.47	0.30	2.89	0.27	147.50	17.23	0.183	–	S
936	23 52 46.81	1.17	-58 04 45.18	1.58	2.957	0.260	0.793	0.169	15.34	3.78	10.74	2.59	12.61	30.56	0.161	–	S
937	23 48 58.86	0.24	-50 39 28.80	0.25	5.344	0.480	4.504	0.339	3.62	0.48	3.48	0.45	54.49	127.89	0.223	–	S
938	23 49 43.23	1.04	-52 24 52.31	0.96	1.482	0.264	0.823	0.178	8.48	2.59	5.99	2.02	52.94	50.56	0.159	–	S
939	23 52 17.75	1.00	-57 24 00.68	1.40	16.803	0.934	1.324	0.144	34.40	3.44	20.89	2.02	18.99	7.00	0.177	–	S
940	23 52 49.13	1.67	-58 11 49.35	0.61	5.396	0.458	0.946	0.187	12.45	3.96	0.00	1.30	167.80	18.33	0.179	–	M
941	23 52 37.25	0.20	-57 54 47.63	0.21	8.810	0.632	5.494	0.349	7.57	0.43	0.00	0.22	132.09	4.41	0.175	–	M
942	23 51 36.80	0.25	-56 14 07.98	0.24	3.780	0.320	2.994	0.224	4.67	0.47	3.40	0.43	66.61	27.85	0.144	–	S
943	23 49 18.67	0.16	-51 35 38.22	0.17	8.838	0.568	7.883	0.468	3.07	0.20	2.62	0.19	4.68	149.87	0.172	-0.44	S
944	23 52 07.01	0.15	-57 08 36.79	0.16	9.838	0.597	8.544	0.494	3.81	0.16	2.15	0.14	164.13	6.07	0.148	-0.21	S
945	23 48 56.41	0.60	-50 43 13.39	0.59	4.901	0.428	2.184	0.270	9.74	1.40	8.63	1.33	108.95	62.88	0.223	–	S
946	23 49 26.70	0.83	-51 54 41.37	1.22	1.783	0.249	0.835	0.171	10.68	2.75	6.81	2.00	175.84	38.44	0.152	–	S
947	23 51 19.27	1.83	-55 46 54.84	0.36	4.684	0.430	0.995	0.188	0.00	4.29	0.00	0.77	0.00	12.05	0.180	–	M
948	23 49 11.51	1.17	-51 20 59.45	1.48	4.175	0.394	1.238	0.262	14.09	3.29	11.25	2.88	1.57	64.98	0.243	–	S
949	23 53 04.62	0.93	-58 43 14.42	0.81	2.072	0.283	1.027	0.192	9.32	2.24	6.55	1.77	118.76	47.71	0.169	–	S
950	23 50 39.38	0.20	-54 34 14.62	0.22	4.922	0.437	4.629	0.325	2.64	0.37	1.06	0.35	22.45	36.23	0.199	–	S
951	23 49 53.64	0.72	-52 59 23.53	0.83	1.679	0.316	1.106	0.208	6.43	1.92	5.23	1.68	3.21	110.79	0.185	–	S
952	23 51 52.75	0.94	-56 49 34.06	1.02	1.719	0.278	0.889	0.190	8.37	2.51	6.89	2.05	23.68	74.95	0.169	–	S
953	23 51 00.99	0.97	-55 22 16.34	0.86	31.642	1.754	2.711	0.254	30.37	2.44	22.28	1.75	52.04	8.65	0.282	–	S
954	23 49 34.40	0.36	-52 23 03.46	0.29	9.382	0.592	3.982	0.306	11.21	0.80	7.76	0.56	91.49	7.35	0.198	–	S
955	23 51 25.87	0.14	-56 07 47.00	0.15	18.017	1.031	17.032	0.952	2.18	0.08	1.58	0.08	33.54	16.80	0.166	-0.33	S
956	23 51 22.66	0.30	-56 02 47.17	0.39	2.050	0.282	1.811	0.184	0.00	0.85	0.00	0.61	0.00	15.96	0.152	–	S
957	23 51 57.59	0.40	-57 06 34.14	0.49	8.329	0.602	5.382	0.339	14.45	1.33	3.05	0.44	48.43	5.68	0.166	–	M
958	23 50 41.64	0.15	-54 48 02.69	0.16	12.120	0.736	10.895	0.628	2.81	0.15	2.55	0.14	66.14	144.23	0.182	-0.45	S
959	23 50 06.37	0.22	-53 40 30.40	0.21	127.040	7.106	30.431	1.754	17.53	0.48	7.84	0.21	33.10	2.30	0.525	-1.54	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
960	23 49 41.23	1.41	-52 43 59.42	0.83	1.916	0.213	0.737	0.144	13.66	3.39	7.00	1.79	73.68	19.94	0.132	–	S
961	23 52 04.86	0.51	-57 19 48.20	0.80	3.291	0.332	1.620	0.215	11.80	1.96	4.16	0.94	153.58	9.32	0.186	–	S
962	23 48 55.32	0.22	-50 59 12.83	0.24	6.381	0.555	5.534	0.400	3.68	0.42	2.73	0.41	178.30	54.74	0.252	–	S
963	23 49 18.18	0.77	-51 53 35.28	0.78	1.507	0.267	0.958	0.177	6.53	1.89	5.84	1.72	116.22	176.04	0.156	–	S
964	23 51 12.33	0.85	-55 49 44.67	0.97	1.755	0.258	0.914	0.174	9.74	2.51	5.41	1.61	31.44	26.52	0.155	–	S
965	23 51 28.83	0.55	-56 20 49.09	0.91	2.214	0.243	1.061	0.160	11.17	2.13	5.39	1.22	164.49	15.36	0.140	–	S
966	23 48 46.09	0.64	-50 39 34.80	0.58	2.969	0.368	1.740	0.243	7.66	1.47	6.15	1.30	97.60	49.42	0.206	–	S
967	23 52 02.81	0.20	-57 19 58.79	0.22	7.505	0.514	5.311	0.352	5.74	0.37	4.36	0.33	159.70	14.75	0.185	–	S
968	23 49 28.40	0.48	-52 20 43.10	0.48	2.741	0.300	1.683	0.197	7.23	1.17	5.60	0.98	48.99	34.88	0.161	–	S
969	23 52 44.27	0.19	-58 26 43.37	0.20	5.649	0.411	4.588	0.302	4.02	0.32	3.51	0.31	148.53	53.93	0.159	–	S
970	23 48 37.04	0.15	-50 21 43.07	0.16	150.696	8.390	107.531	5.934	15.49	0.16	2.28	0.05	50.79	0.61	0.486	-0.77	M
971	23 51 13.83	0.14	-55 57 27.08	0.15	80.193	4.445	65.408	3.604	5.25	0.04	0.86	0.03	152.68	0.93	0.225	-0.73	M
972	23 49 43.00	0.20	-52 55 49.06	0.20	17.198	1.028	9.068	0.537	11.88	0.42	3.25	0.19	132.81	2.84	0.198	-0.84	M
973	23 51 22.83	0.27	-56 13 02.97	0.28	3.454	0.314	2.632	0.214	5.13	0.58	3.63	0.51	35.93	24.57	0.149	–	S
974	23 50 35.65	0.80	-54 45 10.20	0.76	3.256	0.310	1.322	0.202	10.63	1.90	8.79	1.69	119.29	61.93	0.174	–	S
975	23 50 16.22	0.20	-54 06 36.79	0.21	5.705	0.428	4.716	0.315	4.12	0.34	3.24	0.33	129.10	40.14	0.172	–	S
976	23 51 57.40	0.24	-57 14 02.77	0.24	2.951	0.297	2.684	0.209	2.77	0.48	2.17	0.44	50.12	90.46	0.145	–	S
977	23 48 53.10	0.14	-51 03 14.15	0.15	50.131	2.810	50.202	2.779	0.00	0.05	0.00	0.05	0.00	5.96	0.314	0.05	S
978	23 52 15.31	0.33	-57 45 27.45	0.41	2.684	0.294	1.915	0.194	6.06	0.88	3.72	0.71	178.48	21.63	0.154	–	S
979	23 49 40.10	0.32	-52 55 26.38	0.32	5.123	0.421	3.206	0.273	7.66	0.76	4.85	0.58	126.30	14.70	0.193	–	S
980	23 51 08.91	0.71	-55 55 04.74	0.77	1.195	0.352	1.049	0.216	4.18	1.88	0.74	1.50	29.14	65.65	0.202	–	S
981	23 50 20.55	0.40	-54 23 44.70	0.53	5.636	0.449	2.727	0.275	11.24	1.28	5.44	0.74	148.12	8.31	0.216	–	S
982	23 52 54.30	0.15	-58 52 59.42	0.16	15.540	0.944	15.328	0.874	1.16	0.12	0.61	0.12	132.82	77.16	0.232	0.02	S
983	23 53 30.07	0.29	-59 46 59.77	0.29	4.269	0.401	3.185	0.270	5.14	0.62	3.86	0.55	29.08	28.21	0.195	–	S
984	23 52 32.04	0.14	-58 21 10.50	0.15	31.179	1.746	24.877	1.383	5.10	0.08	2.51	0.07	53.26	178.13	0.195	-0.98	S
985	23 49 13.53	0.80	-52 03 02.87	1.51	2.306	0.307	1.001	0.210	13.17	3.49	5.76	1.81	165.74	21.76	0.192	–	S
986	23 51 23.81	1.04	-56 31 56.41	1.42	15.856	1.027	2.799	0.264	34.16	4.09	1.19	0.49	49.63	5.17	0.215	–	M
987	23 53 00.36	0.68	-59 04 32.67	0.83	1.601	0.461	1.353	0.285	4.70	1.99	1.12	1.50	163.17	55.01	0.266	–	S
988	23 50 34.58	0.23	-54 57 32.12	0.27	3.841	0.347	3.103	0.241	4.98	0.54	2.54	0.44	10.97	15.59	0.163	–	S
989	23 49 08.68	0.69	-51 54 08.71	1.06	3.777	0.352	1.430	0.228	12.90	2.41	8.21	1.64	179.09	24.24	0.201	–	S
990	23 51 27.44	0.20	-56 35 45.22	0.20	6.655	0.531	5.844	0.396	3.13	0.35	2.76	0.32	67.83	99.58	0.225	–	S
991	23 52 12.49	0.20	-57 52 23.59	0.21	4.237	0.362	3.943	0.272	2.45	0.35	1.82	0.33	137.08	87.49	0.161	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
992	23 51 08.68	0.42	-56 03 19.96	0.46	2.238	0.284	1.605	0.185	6.56	1.13	3.01	0.81	33.10	18.35	0.154	–	S
993	23 53 29.52	0.54	-59 51 47.23	0.51	3.223	0.438	2.131	0.288	6.24	1.28	4.92	1.09	128.10	71.09	0.245	–	S
994	23 50 43.42	0.60	-55 20 31.89	0.56	2.771	0.455	1.976	0.296	5.60	1.40	4.48	1.24	60.60	80.50	0.259	–	S
995	23 48 59.41	0.19	-51 39 53.59	0.20	6.964	0.483	5.643	0.359	4.66	0.31	3.21	0.28	128.00	17.78	0.174	–	S
996	23 53 09.96	0.15	-59 26 31.02	0.16	49.145	2.796	37.369	2.104	6.11	0.13	2.06	0.09	149.97	177.87	0.429	-0.79	S
997	23 49 39.94	0.62	-53 12 18.52	0.79	1.528	0.296	1.087	0.191	6.42	1.80	3.73	1.43	13.12	45.37	0.171	–	S
998	23 50 12.47	0.47	-54 27 15.23	1.05	58.944	3.322	7.368	0.525	32.62	2.52	11.41	0.84	101.02	5.95	0.333	–	M
999	23 50 25.73	1.73	-54 50 30.20	1.11	4.009	0.290	0.876	0.164	20.10	4.23	10.91	2.23	64.68	17.17	0.164	–	S
1000	23 48 28.76	0.15	-50 30 00.10	0.15	74.083	4.276	53.303	2.980	6.57	0.12	0.00	0.07	17.84	1.89	0.536	-0.78	M
1001	23 51 46.70	1.29	-57 21 51.06	0.45	4.216	0.381	1.018	0.163	0.00	3.06	0.00	0.85	0.00	12.66	0.153	–	M
1002	23 51 10.47	0.70	-56 18 05.39	0.81	0.886	0.258	0.758	0.159	4.13	1.92	2.13	1.58	168.78	94.89	0.149	–	S
1003	23 48 59.32	0.25	-51 50 23.29	0.25	5.222	0.431	3.980	0.298	5.05	0.50	4.00	0.45	78.23	28.65	0.192	–	S
1004	23 52 27.98	0.92	-58 30 52.27	0.77	4.822	0.471	1.448	0.195	12.08	2.68	0.00	0.72	136.65	10.85	0.178	–	M
1005	23 49 57.33	0.50	-53 59 06.08	0.56	3.148	0.361	1.878	0.237	7.48	1.29	5.70	1.09	25.86	37.46	0.197	–	S
1006	23 49 40.95	1.26	-53 26 04.62	1.08	8.832	0.551	1.619	0.239	20.94	3.31	13.60	2.02	52.20	15.49	0.239	–	S
1007	23 50 41.85	0.64	-55 29 01.96	0.75	1.977	0.300	1.203	0.199	7.30	1.75	5.43	1.45	15.11	50.12	0.174	–	S
1008	23 51 44.36	0.72	-57 21 46.36	0.91	3.236	0.270	1.127	0.167	12.93	2.18	8.79	1.56	154.82	22.14	0.147	–	S
1009	23 51 01.59	0.18	-56 07 03.49	0.19	6.315	0.434	5.161	0.326	4.38	0.29	3.02	0.26	35.29	13.92	0.154	–	S
1010	23 50 36.71	0.39	-55 20 04.62	0.48	4.243	0.426	2.564	0.278	7.59	1.06	5.30	0.86	163.83	25.89	0.222	–	S
1011	23 48 37.30	0.22	-51 06 48.32	0.40	76.972	4.450	18.693	1.170	15.80	0.87	7.42	0.41	84.89	4.84	0.558	–	M
1012	23 49 38.98	0.15	-53 27 58.42	0.16	18.039	1.055	16.818	0.949	2.28	0.11	2.07	0.11	1.24	172.11	0.209	-0.68	S
1013	23 49 35.01	0.30	-53 18 54.58	0.28	5.696	0.529	4.302	0.358	5.37	0.63	3.70	0.54	62.30	23.56	0.255	–	S
1014	23 52 44.84	0.69	-59 02 57.45	0.65	2.969	0.451	1.912	0.295	8.49	1.87	2.39	1.05	41.65	15.38	0.261	–	S
1015	23 51 42.12	0.78	-57 24 59.62	1.18	1.343	0.218	0.702	0.148	9.64	2.77	5.29	1.77	5.19	29.50	0.133	–	S
1016	23 50 53.96	0.26	-56 02 20.98	0.33	4.220	0.354	2.800	0.233	6.97	0.70	4.21	0.53	173.50	12.50	0.163	–	S
1017	23 51 08.53	0.45	-56 30 30.88	0.50	3.473	0.348	1.971	0.227	7.68	1.13	6.16	1.00	156.44	42.43	0.183	–	S
1018	23 48 59.57	0.20	-52 09 16.36	0.20	11.251	0.762	8.305	0.537	4.89	0.32	4.81	0.32	64.36	164.56	0.266	–	S
1019	23 50 42.67	0.53	-55 46 43.64	0.48	4.441	0.353	2.031	0.215	11.11	1.36	6.21	0.83	47.15	9.77	0.171	–	S
1020	23 51 42.19	0.76	-57 35 03.51	1.25	2.283	0.244	0.881	0.164	12.75	2.90	7.23	1.75	172.16	21.21	0.148	–	S
1021	23 49 30.49	0.27	-53 24 47.81	0.28	5.268	0.515	4.278	0.353	4.10	0.57	3.67	0.53	168.08	153.66	0.252	–	S
1022	23 53 09.34	0.39	-59 52 10.09	0.37	8.216	0.584	3.860	0.339	10.76	0.96	5.89	0.63	130.28	6.67	0.247	–	S
1023	23 52 33.23	0.76	-59 01 26.86	0.53	1.679	0.416	1.437	0.258	0.00	1.70	0.00	1.23	0.00	35.94	0.239	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1024	23 52 03.35	0.37	-58 16 02.08	0.33	3.867	0.349	2.432	0.227	7.03	0.80	5.04	0.70	111.71	26.82	0.171	–	S
1025	23 50 55.02	1.02	-56 22 08.09	1.10	4.787	0.307	1.064	0.144	21.49	3.19	9.41	1.35	36.71	7.89	0.139	–	S
1026	23 50 21.31	0.17	-55 18 00.75	0.18	7.949	0.532	6.783	0.416	3.77	0.24	2.83	0.23	139.70	26.31	0.178	–	S
1027	23 52 47.44	0.14	-59 26 21.73	0.15	48.050	2.773	47.536	2.659	1.29	0.08	0.00	0.08	48.04	110.84	0.486	-0.56	S
1028	23 48 31.82	0.34	-51 20 10.04	0.21	9.561	0.972	6.720	0.502	0.00	0.77	0.00	0.26	0.00	4.87	0.339	–	M
1029	23 52 36.09	0.28	-59 10 08.97	0.28	3.506	0.431	3.284	0.290	2.68	0.59	1.10	0.53	146.89	57.94	0.224	–	S
1030	23 49 53.66	0.26	-54 29 51.05	0.28	5.251	0.465	3.985	0.317	5.02	0.55	4.00	0.51	173.24	41.92	0.217	–	S
1031	23 51 52.91	0.92	-58 07 04.77	0.71	1.495	0.286	0.953	0.189	7.16	2.11	4.69	1.67	88.05	57.37	0.169	–	S
1032	23 51 32.69	0.38	-57 34 33.44	0.54	3.248	0.286	1.696	0.181	9.81	1.25	5.20	0.80	160.41	10.75	0.145	–	S
1033	23 48 15.33	0.14	-50 47 39.17	0.16	21.923	1.269	21.263	1.192	2.11	0.09	0.29	0.09	159.92	11.45	0.228	-0.30	S
1034	23 49 41.00	0.32	-54 10 36.99	1.13	16.974	1.050	5.814	0.390	22.86	2.65	4.91	0.66	88.88	6.71	0.224	–	M
1035	23 52 41.47	0.15	-59 27 49.10	0.17	184.035	10.618	124.293	7.146	7.20	0.19	3.12	0.13	16.67	178.44	1.963	-0.94	S
1036	23 52 01.50	0.14	-58 29 05.76	0.15	46.567	2.585	41.930	2.316	3.07	0.04	2.12	0.04	94.59	2.23	0.206	-0.25	S
1037	23 52 25.64	0.14	-59 07 39.77	0.15	28.213	1.604	27.367	1.524	1.63	0.07	1.06	0.07	147.20	113.88	0.234	-0.62	S
1038	23 50 56.77	0.15	-56 43 55.08	0.16	8.594	0.553	8.406	0.491	0.00	0.16	0.00	0.16	0.00	15.47	0.166	-0.37	S
1039	23 49 14.31	0.22	-53 22 57.31	0.22	6.175	0.581	5.918	0.427	2.34	0.39	0.30	0.38	59.06	42.91	0.273	–	S
1040	23 49 33.89	0.31	-54 05 44.96	0.34	4.199	0.376	2.814	0.248	6.19	0.70	5.11	0.66	159.81	48.93	0.181	–	S
1041	23 48 39.78	0.15	-52 09 38.59	0.16	96.616	5.375	38.108	2.124	13.06	0.14	11.52	0.13	177.11	6.02	0.345	-1.03	M
1042	23 48 55.18	1.20	-52 44 11.05	1.58	4.239	0.287	0.868	0.148	22.43	4.15	10.87	2.04	142.86	14.45	0.150	–	S
1043	23 49 52.21	0.18	-54 49 24.18	0.19	8.552	0.553	6.176	0.387	5.55	0.30	4.32	0.27	37.82	12.23	0.175	–	S
1044	23 47 50.93	0.22	-50 08 44.77	0.23	5.472	0.456	4.695	0.331	3.83	0.41	2.77	0.38	53.88	30.99	0.201	–	S
1045	23 48 19.04	0.67	-51 22 23.18	0.54	5.454	0.482	2.443	0.305	10.27	1.57	7.89	1.20	83.34	26.12	0.253	–	S
1046	23 51 52.28	0.14	-58 28 25.03	0.15	38.488	2.151	36.677	2.030	2.03	0.05	1.38	0.05	39.28	98.98	0.221	-0.41	S
1047	23 49 25.77	0.16	-53 58 24.44	0.18	7.866	0.528	7.158	0.433	3.28	0.22	1.60	0.20	148.48	15.35	0.177	-0.28	S
1048	23 52 51.59	0.48	-59 59 45.23	0.54	3.417	0.552	2.578	0.356	6.02	1.32	2.43	0.98	145.94	25.30	0.311	–	S
1049	23 50 18.39	0.83	-55 45 25.27	0.93	1.371	0.290	0.902	0.190	7.30	2.31	4.09	1.73	142.53	46.77	0.172	–	S
1050	23 50 06.87	0.77	-55 26 01.30	0.72	1.682	0.286	1.058	0.189	6.59	1.84	5.64	1.59	58.17	104.40	0.167	–	S
1051	23 50 59.96	0.55	-57 04 44.36	0.98	1.574	0.225	0.892	0.149	10.18	2.32	3.19	1.17	163.29	15.00	0.133	–	S
1052	23 52 21.85	0.60	-59 19 35.86	0.83	2.542	0.365	1.459	0.243	8.26	1.92	5.02	1.36	177.86	27.75	0.213	–	S
1053	23 51 32.73	0.14	-58 04 05.62	0.15	88.592	4.900	70.523	3.885	5.40	0.03	0.84	0.02	119.47	0.79	0.214	-0.72	M
1054	23 52 05.14	0.44	-58 55 51.96	0.45	2.977	0.446	2.343	0.289	5.06	1.06	2.95	0.89	138.53	40.36	0.246	–	S
1055	23 52 01.18	0.17	-58 51 10.63	0.18	10.926	0.727	9.468	0.576	3.87	0.23	2.08	0.21	146.04	10.17	0.240	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1056	23 52 30.26	0.19	-59 37 00.00	0.20	6.920	0.574	6.612	0.442	1.95	0.32	1.33	0.29	165.37	82.56	0.249	–	S
1057	23 48 12.07	0.15	-51 21 46.19	0.16	15.534	0.971	14.883	0.862	1.89	0.15	1.54	0.15	129.08	11.20	0.268	0.42	S
1058	23 50 59.64	0.47	-57 14 25.91	0.65	1.894	0.235	1.146	0.155	7.89	1.47	4.72	1.07	177.52	23.14	0.132	–	S
1059	23 49 02.81	0.87	-53 29 03.05	1.12	2.331	0.413	1.280	0.279	8.54	2.55	6.11	2.08	174.42	62.51	0.250	–	S
1060	23 50 36.82	0.52	-56 39 37.58	0.51	2.273	0.298	1.512	0.195	7.42	1.34	3.67	0.96	130.09	21.52	0.166	–	S
1061	23 50 21.55	0.27	-56 10 59.83	0.30	3.274	0.333	2.635	0.226	4.59	0.61	3.12	0.55	4.35	31.59	0.166	–	S
1062	23 50 51.21	0.73	-57 04 57.96	1.05	1.170	0.234	0.758	0.152	8.87	2.60	1.91	1.38	150.93	21.18	0.139	–	S
1063	23 51 16.66	0.14	-57 51 34.72	0.15	45.868	2.556	31.788	1.762	3.60	0.06	3.29	0.06	8.89	13.53	0.221	-1.00	M
1064	23 49 51.74	0.86	-55 14 30.83	1.33	1.854	0.240	0.787	0.165	11.76	3.08	6.93	1.99	168.88	29.60	0.149	–	S
1065	23 50 03.59	0.18	-55 42 19.32	0.19	7.724	0.551	6.662	0.423	3.76	0.28	2.47	0.26	14.09	18.72	0.205	–	S
1066	23 49 10.31	0.22	-53 52 55.04	0.21	13.447	0.932	7.413	0.476	7.08	0.43	3.55	0.30	32.81	8.10	0.245	–	M
1067	23 52 34.83	1.13	-59 58 03.24	0.74	17.265	1.141	4.538	0.400	17.90	3.01	4.73	0.90	25.83	9.90	0.313	–	M
1068	23 49 44.20	0.28	-55 03 47.81	0.29	2.741	0.305	2.375	0.207	3.57	0.60	2.63	0.56	28.15	59.62	0.156	–	S
1069	23 48 07.52	1.95	-51 27 20.68	0.94	4.735	0.380	1.188	0.234	20.31	4.77	8.98	2.00	95.63	15.45	0.232	–	S
1070	23 48 38.36	0.96	-52 42 04.40	0.74	1.469	0.264	0.898	0.176	7.90	2.24	4.95	1.70	95.76	43.21	0.157	–	S
1071	23 51 09.24	0.62	-57 42 41.08	0.75	0.991	0.277	0.877	0.170	4.15	1.76	0.00	1.37	9.15	56.23	0.159	–	S
1072	23 47 36.55	0.19	-50 14 01.48	0.19	10.713	0.676	7.646	0.471	6.12	0.31	4.15	0.24	69.14	5.94	0.200	–	S
1073	23 50 45.45	2.00	-57 06 44.89	0.36	3.217	0.313	0.829	0.134	0.00	4.72	0.00	0.65	0.00	10.20	0.126	–	M
1074	23 49 59.37	0.32	-55 43 05.12	0.32	4.056	0.408	3.004	0.273	5.48	0.72	3.84	0.62	46.01	27.69	0.205	–	S
1075	23 50 53.88	0.24	-57 25 42.85	0.30	2.677	0.281	2.329	0.193	0.00	0.61	0.00	0.45	0.00	11.33	0.140	–	S
1076	23 51 30.15	0.37	-58 27 06.46	0.35	2.248	0.320	1.938	0.208	4.16	0.84	1.86	0.73	124.16	38.64	0.173	–	S
1077	23 48 47.30	0.43	-53 14 18.33	0.44	2.813	0.413	2.248	0.267	4.75	0.99	3.32	0.92	128.91	65.84	0.226	–	S
1078	23 50 51.89	0.46	-57 22 52.24	0.57	2.289	0.256	1.343	0.168	7.64	1.29	5.52	1.04	179.64	29.85	0.140	–	S
1079	23 48 47.98	0.15	-53 21 25.14	0.16	194.509	11.901	170.011	9.597	0.00	0.10	0.00	0.10	0.00	16.48	2.161	-0.76	M
1080	23 49 50.40	0.30	-55 33 01.91	0.29	3.137	0.295	2.328	0.198	5.35	0.64	3.98	0.57	55.10	29.97	0.143	–	S
1081	23 50 37.01	0.40	-57 01 29.30	0.45	3.267	0.288	1.769	0.184	8.00	1.02	6.51	0.88	15.80	30.01	0.144	–	S
1082	23 51 19.50	0.54	-58 15 11.46	0.51	4.496	0.380	2.080	0.237	10.22	1.36	6.69	0.97	44.01	15.54	0.192	–	S
1083	23 50 52.97	0.56	-57 30 18.63	1.00	2.133	0.242	1.010	0.160	11.54	2.34	5.04	1.24	168.03	14.49	0.142	–	S
1084	23 51 34.97	0.71	-58 42 39.19	0.64	4.652	0.378	1.810	0.230	12.61	1.84	7.14	1.12	45.02	12.28	0.196	–	S
1085	23 48 45.68	0.16	-53 21 14.50	0.16	224.530	13.726	197.911	11.464	4.32	0.18	0.67	0.14	119.77	2.73	3.505	-0.73	S
1086	23 48 38.47	0.36	-53 05 18.78	0.57	3.605	0.398	2.317	0.260	8.82	1.31	2.86	0.74	163.20	10.92	0.214	–	S
1087	23 48 55.88	0.46	-53 44 36.67	0.43	4.210	0.468	2.738	0.307	7.46	1.13	4.29	0.84	121.24	21.15	0.250	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1088	23 51 22.30	1.30	-58 24 19.06	1.04	2.132	0.273	0.890	0.187	12.77	3.38	5.90	1.79	50.06	20.60	0.171	–	S
1089	23 50 06.05	1.39	-56 10 04.98	1.72	5.121	0.331	0.900	0.157	24.30	4.68	11.52	2.11	31.29	12.86	0.167	–	S
1090	23 50 51.92	1.02	-57 34 01.69	1.05	3.621	0.281	1.003	0.168	14.68	2.67	10.93	2.09	137.21	33.58	0.154	–	S
1091	23 52 21.54	1.08	-59 59 20.73	1.40	6.474	0.523	1.673	0.324	15.56	3.38	10.98	2.39	157.94	28.49	0.308	–	S
1092	23 49 51.66	0.43	-55 44 55.38	0.51	2.471	0.344	1.806	0.224	5.78	1.14	3.74	0.95	10.93	36.49	0.190	–	S
1093	23 50 04.09	0.16	-56 10 52.82	0.17	10.547	0.720	8.804	0.515	3.56	0.19	0.00	0.14	34.38	6.21	0.175	-0.01	M
1094	23 47 37.93	1.78	-50 41 27.21	1.85	7.310	0.432	0.860	0.149	28.64	5.29	17.46	2.94	42.52	17.11	0.175	–	S
1095	23 52 08.73	0.50	-59 42 40.80	0.49	5.211	0.454	2.513	0.287	8.15	1.19	8.00	1.06	26.05	110.08	0.231	–	S
1096	23 47 41.98	0.14	-50 55 01.73	0.16	26.071	1.496	23.518	1.318	3.38	0.10	1.92	0.09	2.26	5.81	0.248	-0.47	S
1097	23 50 00.09	1.31	-56 04 12.67	1.36	2.725	0.241	0.751	0.157	14.59	3.51	11.25	2.67	36.26	41.13	0.148	–	S
1098	23 49 15.63	0.15	-54 35 49.91	0.15	20.336	1.166	16.400	0.916	4.58	0.10	0.00	0.07	29.05	2.86	0.161	-0.23	M
1099	23 51 20.60	1.15	-58 28 03.79	1.36	3.049	0.287	0.913	0.190	13.54	3.32	10.48	2.50	19.29	40.17	0.177	–	S
1100	23 47 42.50	0.16	-50 57 09.75	0.17	10.816	0.747	10.749	0.646	0.00	0.20	0.00	0.20	0.00	40.74	0.261	-0.55	S
1101	23 51 52.80	1.25	-59 21 31.32	0.35	3.370	0.543	1.085	0.236	0.00	2.93	0.00	0.75	0.00	15.68	0.229	–	M
1102	23 50 30.80	0.14	-57 06 47.93	0.15	21.361	1.202	20.736	1.150	1.73	0.06	0.87	0.06	173.65	102.01	0.147	-0.30	S
1103	23 48 15.01	0.29	-52 23 37.32	0.37	3.559	0.364	2.683	0.243	6.10	0.78	2.93	0.58	10.13	16.16	0.184	–	S
1104	23 51 18.85	0.77	-58 31 16.34	1.39	2.238	0.293	0.964	0.201	12.11	3.25	5.89	1.77	179.20	21.27	0.183	–	S
1105	23 48 19.20	0.47	-52 37 06.97	0.64	2.788	0.254	1.368	0.162	10.57	1.49	6.07	0.99	154.29	15.99	0.133	–	S
1106	23 51 37.46	0.64	-59 02 56.06	0.63	3.220	0.402	1.800	0.267	7.54	1.57	6.32	1.33	36.03	58.95	0.228	–	S
1107	23 48 47.52	1.20	-53 43 52.38	1.04	3.474	0.434	1.407	0.299	10.60	2.80	8.96	2.42	89.70	81.39	0.268	–	S
1108	23 47 36.78	0.48	-50 55 08.46	0.58	4.578	0.511	2.702	0.336	7.66	1.24	6.06	1.15	4.38	56.00	0.278	–	S
1109	23 50 08.52	0.25	-56 33 42.35	0.20	19.964	1.212	7.904	0.490	11.66	0.53	4.54	0.26	155.37	3.91	0.227	–	M
1110	23 49 46.18	0.21	-55 51 04.92	0.24	7.025	0.472	4.525	0.307	6.72	0.43	5.06	0.36	3.56	11.99	0.167	–	S
1111	23 47 53.65	0.42	-51 39 43.53	0.65	3.252	0.357	1.900	0.234	9.11	1.46	4.66	0.95	173.75	17.31	0.195	–	S
1112	23 49 17.43	0.68	-54 55 21.09	0.63	6.140	0.412	1.877	0.212	14.75	1.79	9.53	1.14	47.18	11.68	0.179	–	S
1113	23 49 14.82	0.65	-54 50 49.52	0.52	3.453	0.305	1.591	0.193	10.83	1.59	6.47	1.02	59.05	14.60	0.160	–	S
1114	23 51 33.38	0.72	-59 05 14.61	0.38	17.708	1.097	4.057	0.336	19.69	1.78	5.59	0.54	154.38	5.62	0.251	–	M
1115	23 50 40.82	0.35	-57 36 53.17	0.40	3.494	0.318	2.152	0.206	7.59	0.90	4.80	0.70	149.84	16.59	0.157	–	S
1116	23 48 11.32	0.57	-52 32 13.40	0.42	4.698	0.360	2.102	0.215	11.76	1.40	6.25	0.78	62.57	8.52	0.170	–	S
1117	23 48 38.85	0.27	-53 35 46.87	0.30	3.982	0.421	3.343	0.286	4.19	0.60	2.78	0.56	1.48	40.58	0.212	–	S
1118	23 48 37.00	0.41	-53 31 35.01	0.45	2.577	0.405	2.154	0.260	4.26	0.99	2.84	0.91	153.25	73.37	0.223	–	S
1119	23 48 14.68	1.15	-52 42 52.81	0.71	1.411	0.279	0.879	0.184	8.86	2.72	3.33	1.58	94.37	26.85	0.167	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1120	23 47 46.90	0.32	-51 37 00.49	0.23	17.578	1.056	8.401	0.503	14.43	0.73	3.54	0.27	21.93	3.47	0.200	–	M
1121	23 48 15.16	0.17	-52 48 44.45	0.20	17.462	1.049	8.850	0.521	10.27	0.35	4.04	0.18	58.25	3.04	0.187	-0.92	M
1122	23 51 30.55	1.04	-59 08 17.70	0.92	1.902	0.353	1.069	0.238	7.97	2.53	5.86	2.00	117.27	78.81	0.213	–	S
1123	23 49 48.94	1.05	-56 12 10.47	1.47	6.934	0.512	1.408	0.191	18.06	4.11	0.00	0.91	51.57	11.11	0.175	–	M
1124	23 51 32.89	0.48	-59 13 29.13	0.41	2.747	0.337	1.881	0.222	6.04	1.05	4.56	0.92	87.44	57.24	0.183	–	S
1125	23 49 07.90	0.49	-54 50 02.41	0.52	2.398	0.305	1.572	0.200	6.23	1.19	5.35	1.08	26.03	73.67	0.168	–	S
1126	23 50 32.39	0.16	-57 33 49.27	0.17	7.506	0.488	6.784	0.404	3.23	0.20	1.66	0.18	5.71	11.83	0.152	-0.74	S
1127	23 47 21.34	0.94	-50 37 18.36	1.17	3.561	0.309	1.134	0.197	14.51	2.80	9.85	2.06	147.44	31.90	0.178	–	S
1128	23 47 39.34	0.19	-51 27 41.58	0.19	12.305	0.812	6.999	0.429	6.29	0.30	5.39	0.27	32.74	20.63	0.189	–	M
1129	23 50 10.24	0.19	-56 57 20.14	0.21	6.276	0.513	4.610	0.301	4.59	0.38	0.00	0.24	50.29	7.05	0.163	–	M
1130	23 49 13.51	0.79	-55 06 10.76	0.70	1.653	0.279	1.031	0.185	6.88	1.85	5.53	1.60	92.16	89.52	0.163	–	S
1131	23 49 12.56	0.15	-55 10 00.99	0.15	51.196	2.864	38.290	2.117	17.23	0.16	2.13	0.04	149.45	0.51	0.217	-0.71	M
1132	23 48 39.74	1.00	-54 00 08.35	0.76	4.180	0.393	1.571	0.256	12.00	2.31	8.81	1.75	87.93	32.48	0.225	–	S
1133	23 47 21.96	0.28	-50 53 35.23	0.23	45.570	2.594	15.491	0.901	18.13	0.67	3.46	0.20	142.21	2.34	0.292	-1.13	M
1134	23 47 46.02	1.29	-51 58 24.97	1.27	3.794	0.363	1.157	0.243	12.42	3.14	12.21	2.85	79.94	176.36	0.223	–	S
1135	23 49 56.50	0.77	-56 43 50.27	0.67	6.238	0.425	1.869	0.222	15.66	2.02	8.87	1.15	47.94	9.90	0.193	–	S
1136	23 48 47.19	0.44	-54 23 35.95	0.52	2.143	0.361	1.751	0.231	4.86	1.16	2.54	0.98	158.95	45.42	0.202	–	S
1137	23 51 00.69	0.70	-58 37 26.06	0.73	1.173	0.309	0.991	0.191	5.70	1.95	0.00	1.27	135.78	29.71	0.178	–	S
1138	23 47 14.80	0.24	-50 41 56.57	0.53	15.321	0.950	8.490	0.503	16.24	1.24	2.58	0.35	72.42	4.36	0.187	-0.45	M
1139	23 47 24.02	0.28	-51 08 43.12	0.69	26.963	1.666	6.147	0.529	0.00	1.59	0.00	0.52	0.00	7.87	0.407	–	M
1140	23 48 57.12	0.74	-54 47 27.52	0.37	3.502	0.454	1.339	0.195	0.00	1.73	0.00	0.76	0.00	16.25	0.181	–	M
1141	23 47 42.40	0.21	-51 57 41.33	0.21	18.156	1.119	8.232	0.515	7.78	0.36	6.92	0.34	140.07	42.77	0.245	–	M
1142	23 48 18.37	0.54	-53 23 39.67	0.53	3.075	0.468	2.217	0.304	6.18	1.32	3.79	1.09	122.95	40.80	0.263	–	S
1143	23 49 26.70	0.25	-55 52 15.17	0.29	3.027	0.306	2.544	0.210	4.51	0.58	2.04	0.49	15.88	19.59	0.151	–	S
1144	23 48 33.96	0.26	-54 01 08.67	0.28	4.652	0.460	3.898	0.317	4.57	0.57	2.33	0.49	143.20	23.41	0.225	–	S
1145	23 48 18.85	0.14	-53 27 47.29	0.15	51.624	2.882	48.541	2.685	2.15	0.05	1.90	0.05	73.55	113.01	0.285	-0.48	S
1146	23 50 18.92	0.22	-57 35 15.43	0.22	3.358	0.324	3.220	0.236	1.94	0.40	1.26	0.37	149.61	114.12	0.154	–	S
1147	23 50 38.50	0.71	-58 10 54.75	0.87	1.443	0.314	1.048	0.200	7.62	2.25	0.00	1.26	143.81	21.90	0.184	–	S
1148	23 49 49.59	0.40	-56 44 23.92	0.40	5.741	0.429	2.813	0.258	10.16	1.03	5.93	0.67	39.53	8.55	0.192	–	S
1149	23 50 48.76	0.30	-58 29 38.66	0.28	5.252	0.425	3.407	0.278	6.36	0.61	5.20	0.57	99.09	43.72	0.191	–	S
1150	23 48 51.66	0.39	-54 48 11.74	0.43	4.902	0.407	2.624	0.256	8.85	1.03	6.01	0.76	31.48	15.49	0.196	–	S
1151	23 50 30.45	0.14	-57 59 56.09	0.15	52.609	2.933	41.309	2.292	5.66	0.07	2.24	0.06	95.47	177.80	0.287	-1.15	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1152	23 47 19.87	0.14	-51 10 36.08	0.15	402.183	22.244	395.659	21.804	0.00	0.03	0.00	0.03	0.00	180.00	1.355	0.12	S
1153	23 49 11.67	0.35	-55 30 19.21	0.40	2.704	0.314	1.996	0.207	5.34	0.86	4.12	0.78	174.06	50.26	0.165	-	S
1154	23 47 09.91	0.19	-50 43 34.58	0.20	6.827	0.517	6.118	0.398	3.91	0.33	1.14	0.27	119.92	12.79	0.208	-	S
1155	23 49 36.61	0.63	-56 20 39.34	1.15	1.539	0.241	0.842	0.161	10.14	2.66	4.06	1.45	174.97	20.61	0.145	-	S
1156	23 48 44.11	1.08	-54 35 16.92	1.39	3.063	0.278	0.933	0.181	15.38	3.52	9.11	2.08	26.95	22.24	0.169	-	S
1157	23 48 22.72	0.94	-53 51 46.40	0.92	2.807	0.514	1.634	0.344	7.64	2.35	5.95	1.97	46.47	71.30	0.307	-	S
1158	23 48 53.88	0.31	-55 01 20.51	0.33	2.841	0.324	2.325	0.217	4.14	0.69	3.37	0.64	167.80	82.98	0.168	-	S
1159	23 47 08.25	0.17	-50 48 57.07	0.22	17.291	1.050	10.633	0.655	8.86	0.37	4.10	0.23	169.04	1.66	0.277	-	S
1160	23 47 27.77	0.16	-51 47 50.67	0.17	8.826	0.572	7.990	0.475	2.85	0.20	2.44	0.19	0.03	166.92	0.176	-0.21	S
1161	23 49 10.59	0.16	-55 44 12.00	0.17	10.568	0.666	9.226	0.544	3.07	0.19	3.01	0.18	35.07	122.84	0.190	-0.58	S
1162	23 49 48.28	0.29	-56 58 10.87	0.30	4.217	0.363	2.887	0.241	5.68	0.62	5.03	0.58	36.62	49.48	0.170	-	S
1163	23 47 36.78	1.10	-52 12 45.39	1.00	2.894	0.313	1.108	0.211	12.20	2.77	8.59	2.09	118.14	38.31	0.189	-	S
1164	23 50 15.60	1.01	-57 51 15.75	1.37	2.058	0.234	0.747	0.161	12.49	3.30	8.38	2.23	13.62	32.34	0.147	-	S
1165	23 49 23.65	0.23	-56 16 48.19	0.26	3.824	0.320	2.954	0.222	5.28	0.51	3.14	0.42	6.37	14.95	0.144	-	S
1166	23 48 43.92	0.86	-54 57 22.56	1.13	1.688	0.298	0.926	0.201	8.86	2.68	5.59	1.93	15.00	42.04	0.180	-	S
1167	23 48 41.77	0.87	-54 54 41.24	0.91	2.867	0.300	1.158	0.200	10.20	2.19	9.25	1.94	30.69	87.39	0.175	-	S
1168	23 48 50.83	0.50	-55 14 45.32	0.49	5.368	0.451	2.547	0.282	8.78	1.16	8.04	1.07	108.75	121.22	0.225	-	S
1169	23 51 19.43	0.64	-59 43 45.68	0.77	2.160	0.305	1.229	0.204	7.71	1.82	5.76	1.44	179.69	42.35	0.178	-	S
1170	23 50 07.78	0.95	-57 45 41.24	0.88	2.404	0.289	1.052	0.196	9.47	2.16	8.40	2.09	106.68	174.39	0.173	-	S
1171	23 48 05.60	0.58	-53 38 45.63	0.48	7.696	0.511	2.659	0.263	13.97	1.48	8.37	0.87	55.13	8.37	0.209	-	S
1172	23 46 52.40	0.35	-50 31 12.57	0.38	2.608	0.319	2.087	0.211	5.34	0.87	2.73	0.70	136.46	28.55	0.169	-	S
1173	23 51 03.22	0.59	-59 21 46.88	0.65	3.291	0.356	1.676	0.235	8.28	1.53	7.02	1.30	165.08	51.86	0.199	-	S
1174	23 46 55.17	0.58	-50 41 29.24	0.65	4.047	0.394	1.967	0.255	9.90	1.54	7.11	1.25	139.05	33.21	0.213	-	S
1175	23 49 32.13	0.14	-56 44 28.86	0.15	30.650	1.730	29.062	1.615	2.56	0.07	0.79	0.06	124.33	3.55	0.225	-0.81	S
1176	23 49 31.78	0.33	-56 45 03.11	0.36	4.310	0.448	3.084	0.297	5.46	0.77	4.50	0.71	170.92	51.41	0.229	-	S
1177	23 48 31.05	0.82	-54 40 50.39	0.69	3.561	0.337	1.458	0.218	10.75	1.90	8.54	1.60	97.47	44.26	0.188	-	S
1178	23 49 37.23	2.24	-56 56 48.25	1.17	8.497	0.489	0.885	0.138	33.58	5.29	15.52	2.43	69.72	10.89	0.170	-	S
1179	23 48 45.78	0.58	-55 14 20.87	0.61	2.888	0.396	1.797	0.262	6.50	1.40	5.95	1.33	164.03	176.15	0.224	-	S
1180	23 50 59.94	0.50	-59 22 10.45	0.62	2.437	0.370	1.669	0.242	6.32	1.42	4.10	1.13	176.30	35.99	0.210	-	S
1181	23 50 11.68	0.79	-58 03 25.07	0.46	39.924	2.307	6.022	0.528	22.55	1.98	7.84	0.68	151.32	6.19	0.411	-	M
1182	23 48 19.83	0.39	-54 18 42.74	0.53	2.375	0.265	1.535	0.173	8.01	1.23	3.54	0.78	16.71	13.87	0.142	-	S
1183	23 49 08.45	0.53	-56 02 44.83	0.99	3.608	0.287	1.278	0.173	14.54	2.28	7.24	1.19	174.80	11.25	0.152	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1184	23 50 01.88	0.15	-57 45 21.91	0.16	12.945	0.779	12.541	0.714	2.05	0.12	0.00	0.12	15.57	12.40	0.183	-0.38	S
1185	23 50 10.31	0.49	-58 02 25.08	0.29	42.394	2.460	9.541	0.670	17.35	1.13	8.04	0.51	160.25	5.55	0.416	-	M
1186	23 46 46.49	1.20	-50 29 00.36	1.13	2.070	0.265	0.845	0.184	10.31	2.86	9.51	2.58	75.84	100.25	0.165	-	S
1187	23 49 32.05	1.09	-56 54 03.11	1.54	2.165	0.237	0.726	0.163	13.76	3.68	8.70	2.42	159.39	32.12	0.151	-	S
1188	23 50 36.77	0.67	-58 50 23.77	0.68	2.100	0.420	1.535	0.270	5.93	1.72	3.44	1.36	138.15	50.05	0.243	-	S
1189	23 47 14.08	0.43	-51 48 22.76	0.40	3.469	0.373	2.301	0.245	6.24	0.95	5.36	0.88	80.15	54.34	0.196	-	S
1190	23 49 00.85	0.68	-55 54 34.86	1.37	4.523	0.302	1.052	0.152	20.21	3.20	9.68	1.53	169.07	10.67	0.147	-	S
1191	23 46 34.91	0.54	-50 00 51.64	0.55	2.378	0.437	1.928	0.278	5.22	1.38	2.30	1.09	47.35	38.37	0.247	-	S
1192	23 47 09.42	0.93	-51 37 55.52	0.83	4.453	0.366	1.507	0.225	14.25	2.45	8.86	1.56	119.57	19.72	0.200	-	S
1193	23 47 26.99	0.18	-52 24 47.49	0.21	11.586	0.760	6.352	0.406	5.11	0.35	1.23	0.26	71.68	9.27	0.208	-	M
1194	23 49 36.14	0.27	-57 05 23.52	0.29	4.410	0.356	2.958	0.235	5.98	0.58	5.07	0.53	170.64	35.78	0.158	-	S
1195	23 51 12.74	0.18	-59 54 26.21	0.24	16.859	1.044	8.305	0.508	9.69	0.44	4.69	0.26	70.07	5.06	0.222	-	M
1196	23 46 48.24	0.15	-50 48 01.43	0.17	48.140	2.725	30.699	1.705	15.05	0.22	4.06	0.08	111.65	1.03	0.240	-0.63	M
1197	23 50 45.26	1.41	-59 13 25.53	1.79	5.601	0.356	0.861	0.162	22.57	4.43	14.68	2.91	150.68	22.26	0.176	-	S
1198	23 48 30.49	0.88	-54 58 47.53	1.15	1.627	0.288	0.880	0.195	8.78	2.67	5.95	2.05	166.56	52.83	0.175	-	S
1199	23 49 52.55	0.14	-57 44 21.90	0.15	45.587	2.531	41.710	2.303	3.38	0.04	0.90	0.04	129.26	178.67	0.201	-0.91	S
1200	23 50 56.43	0.65	-59 34 05.94	0.56	2.920	0.368	1.688	0.244	7.52	1.49	5.82	1.26	63.34	53.71	0.208	-	S
1201	23 47 03.37	0.20	-51 41 16.26	0.46	46.727	2.669	11.594	0.699	19.29	1.01	6.35	0.34	87.02	3.61	0.287	-	M
1202	23 47 56.98	0.16	-53 56 19.30	0.17	210.493	11.648	86.408	4.779	15.28	0.24	7.05	0.11	50.03	1.36	0.503	-1.04	M
1203	23 47 55.00	0.63	-53 51 15.84	0.73	15.423	1.082	4.412	0.384	17.29	2.16	0.00	0.54	126.72	6.70	0.298	-	M
1204	23 50 35.29	0.73	-59 04 41.31	0.62	1.499	0.338	1.192	0.213	6.00	1.79	0.83	1.24	119.89	31.27	0.195	-	S
1205	23 48 17.84	0.18	-54 42 58.46	0.17	12.517	0.824	8.075	0.483	6.78	0.29	0.32	0.18	14.91	4.24	0.191	-0.47	M
1206	23 46 35.93	0.63	-50 26 20.30	1.05	2.227	0.290	1.144	0.194	11.10	2.44	5.08	1.40	163.11	21.01	0.172	-	S
1207	23 48 01.37	1.09	-54 05 50.34	1.30	2.188	0.267	0.839	0.185	11.23	3.03	9.19	2.54	14.07	68.85	0.167	-	S
1208	23 49 45.56	0.38	-57 41 35.19	0.34	2.566	0.335	2.116	0.220	4.74	0.83	2.33	0.70	114.11	31.79	0.179	-	S
1209	23 48 14.42	0.40	-54 38 56.26	0.47	2.749	0.308	1.813	0.202	6.61	1.03	4.88	0.89	170.14	38.44	0.164	-	S
1210	23 49 48.56	0.38	-57 48 24.11	0.39	5.563	0.452	3.052	0.283	9.42	0.98	4.83	0.64	135.10	8.95	0.213	-	S
1211	23 50 28.76	0.40	-58 59 24.48	0.40	1.980	0.338	1.780	0.215	3.28	0.95	1.81	0.83	140.37	79.18	0.187	-	S
1212	23 48 19.22	0.38	-54 51 44.35	0.66	5.663	0.408	2.226	0.232	13.23	1.51	6.88	0.84	173.46	8.32	0.186	-	S
1213	23 50 16.53	1.06	-58 41 44.17	1.08	2.285	0.274	0.913	0.189	10.84	2.76	8.41	2.20	139.21	58.02	0.169	-	S
1214	23 49 16.29	0.14	-56 54 06.14	0.15	20.871	1.190	20.704	1.153	0.00	0.07	0.00	0.07	0.00	123.49	0.180	-0.32	S
1215	23 48 32.07	0.28	-55 25 02.65	0.31	4.462	0.452	3.505	0.305	4.82	0.64	3.42	0.57	16.81	33.37	0.225	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1216	23 49 39.60	0.78	-57 38 20.24	0.86	1.071	0.270	0.803	0.172	5.11	2.07	3.92	1.72	10.60	111.48	0.158	–	S
1217	23 48 36.53	0.30	-55 35 24.11	0.30	4.851	0.409	3.244	0.270	6.61	0.67	4.50	0.55	47.62	16.79	0.189	–	S
1218	23 48 41.54	0.58	-55 47 41.94	0.49	1.593	0.287	1.270	0.183	5.32	1.34	2.30	1.05	61.47	35.60	0.162	–	S
1219	23 48 21.44	0.88	-55 06 08.55	0.85	1.428	0.280	0.899	0.185	6.72	2.17	5.49	1.84	47.47	95.08	0.166	–	S
1220	23 47 12.10	0.15	-52 29 35.19	0.16	32.651	1.893	22.092	1.240	7.74	0.16	0.00	0.08	15.89	1.74	0.246	-1.15	M
1221	23 49 14.27	0.87	-57 00 16.91	0.99	5.846	0.374	1.348	0.174	19.45	2.70	10.15	1.37	33.98	9.38	0.163	–	S
1222	23 49 41.19	0.15	-57 51 49.53	0.16	12.045	0.745	11.092	0.643	2.56	0.15	2.04	0.15	137.08	42.24	0.198	-0.60	S
1223	23 47 07.17	0.14	-52 19 22.76	0.15	253.090	14.066	211.913	11.685	5.45	0.04	0.00	0.03	130.29	0.99	0.831	-0.71	M
1224	23 49 20.42	0.51	-57 13 24.84	0.52	2.154	0.243	1.280	0.159	7.73	1.27	5.31	1.03	137.28	31.00	0.132	–	S
1225	23 47 33.97	0.14	-53 28 39.02	0.15	63.774	3.532	61.138	3.371	1.74	0.03	1.61	0.03	150.15	177.12	0.239	-0.23	S
1226	23 47 57.59	0.45	-54 23 58.74	0.47	5.235	0.401	2.377	0.241	9.91	1.14	7.68	0.90	37.01	20.87	0.187	–	S
1227	23 49 25.68	0.32	-57 26 56.67	0.42	2.664	0.276	1.831	0.181	7.07	0.93	3.27	0.66	158.18	13.31	0.142	–	S
1228	23 47 19.11	0.41	-52 53 10.55	0.66	4.386	0.387	2.134	0.245	10.93	1.50	5.81	0.91	172.22	12.98	0.200	–	S
1229	23 49 21.24	0.25	-57 20 56.02	0.23	36.687	2.094	8.900	0.539	14.67	0.54	9.41	0.35	143.93	5.09	0.227	–	M
1230	23 47 37.04	0.14	-53 38 36.71	0.15	34.181	1.928	31.840	1.769	2.53	0.07	1.82	0.07	138.08	13.11	0.249	-0.61	S
1231	23 46 29.36	0.15	-50 44 03.80	0.16	14.430	0.869	13.283	0.760	2.94	0.14	1.84	0.13	138.81	17.11	0.206	-0.48	S
1232	23 47 56.53	0.73	-54 27 22.20	0.65	1.112	0.270	0.905	0.169	4.58	1.72	3.00	1.48	97.62	98.44	0.155	–	S
1233	23 47 12.42	0.83	-52 41 59.02	0.67	1.196	0.275	0.916	0.174	6.32	2.02	2.07	1.42	108.17	36.78	0.159	–	S
1234	23 48 24.09	0.73	-55 31 51.43	1.10	9.418	0.559	1.686	0.203	21.91	2.62	13.00	1.55	158.79	10.63	0.196	–	S
1235	23 47 58.41	0.86	-54 35 48.73	1.40	4.791	0.437	1.003	0.184	11.69	3.68	0.00	1.06	57.61	16.06	0.176	–	M
1236	23 47 04.38	0.44	-52 24 37.94	0.39	4.003	0.417	2.597	0.274	6.81	0.98	5.11	0.84	97.38	33.55	0.217	–	S
1237	23 48 16.08	0.84	-55 19 24.78	0.98	1.464	0.289	0.908	0.192	7.75	2.38	4.70	1.80	147.13	48.79	0.172	–	S
1238	23 47 02.27	0.15	-52 26 36.38	0.16	15.730	0.942	14.009	0.802	3.05	0.14	2.66	0.14	154.83	151.47	0.217	-0.39	S
1239	23 47 10.30	0.45	-52 46 39.85	0.52	3.009	0.329	1.833	0.216	7.28	1.15	5.70	1.02	11.63	44.56	0.177	–	S
1240	23 48 18.89	0.72	-55 26 58.53	0.61	2.487	0.326	1.411	0.217	7.83	1.65	6.08	1.40	69.47	51.51	0.187	–	S
1241	23 48 35.49	0.32	-56 04 45.73	0.41	1.926	0.267	1.650	0.174	4.74	0.88	0.00	0.68	2.74	21.67	0.144	–	S
1242	23 46 45.68	0.52	-51 56 22.61	0.44	10.309	0.652	3.347	0.310	13.06	1.21	10.52	0.95	94.10	17.44	0.237	–	S
1243	23 49 31.95	0.33	-58 02 07.39	0.29	3.693	0.400	2.929	0.268	4.82	0.68	3.16	0.61	87.88	36.28	0.204	–	S
1244	23 48 19.24	0.71	-55 38 28.34	0.88	1.298	0.251	0.853	0.165	6.79	2.03	4.64	1.64	1.14	57.71	0.147	–	S
1245	23 48 29.56	0.19	-56 06 23.06	0.20	5.704	0.402	4.566	0.296	4.40	0.31	3.47	0.29	24.18	22.98	0.149	–	S
1246	23 49 10.88	0.49	-57 28 16.52	0.69	1.311	0.236	0.979	0.152	6.35	1.59	2.18	1.10	178.04	26.00	0.135	–	S
1247	23 46 55.16	0.28	-52 28 53.80	0.38	6.303	0.470	3.489	0.291	9.09	0.82	5.53	0.57	169.96	10.87	0.202	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1248	23 48 54.74	0.62	-56 58 07.00	0.71	1.192	0.273	0.953	0.172	4.80	1.68	2.96	1.39	168.56	74.02	0.157	–	S
1249	23 49 42.67	0.22	-58 32 24.31	0.22	57.341	3.218	12.094	0.720	14.92	0.47	8.67	0.27	37.77	3.40	0.276	–	M
1250	23 47 49.29	0.26	-55 00 14.01	0.22	5.725	0.496	4.724	0.350	5.17	0.50	1.60	0.38	95.49	10.65	0.227	–	S
1251	23 47 14.30	0.28	-53 29 53.62	0.63	42.615	2.435	13.173	0.772	21.91	1.47	7.88	0.52	96.49	4.94	0.266	-0.81	M
1252	23 46 47.76	0.37	-52 21 32.00	0.37	4.729	0.432	2.961	0.282	6.36	0.82	6.21	0.77	64.42	117.37	0.213	–	S
1253	23 45 56.32	0.47	-50 00 41.47	0.90	16.292	0.918	2.547	0.223	27.53	2.14	12.88	0.94	12.14	3.96	0.199	–	S
1254	23 49 55.66	0.29	-59 03 11.10	0.26	5.205	0.456	3.827	0.309	5.44	0.57	3.92	0.51	70.36	27.85	0.213	–	S
1255	23 48 42.21	0.30	-56 48 26.03	0.30	4.022	0.369	2.870	0.247	5.06	0.62	4.97	0.62	4.78	176.17	0.178	–	S
1256	23 50 18.29	0.17	-59 48 29.39	0.17	9.817	0.652	8.763	0.529	2.82	0.21	2.57	0.20	38.51	72.59	0.213	-0.39	S
1257	23 47 52.41	0.48	-55 10 48.26	0.61	2.074	0.347	1.558	0.224	5.85	1.38	3.09	1.08	6.12	35.64	0.196	–	S
1258	23 49 02.00	0.19	-57 35 49.56	0.21	4.926	0.370	4.079	0.272	4.36	0.35	2.63	0.31	177.37	14.64	0.149	–	S
1259	23 48 21.92	0.19	-56 16 50.61	0.20	4.522	0.341	4.017	0.261	3.52	0.31	1.85	0.28	24.60	17.99	0.136	–	S
1260	23 49 46.99	1.29	-58 59 17.74	0.79	2.022	0.254	0.927	0.170	13.74	3.18	3.49	1.28	113.09	12.86	0.157	–	S
1261	23 46 16.28	0.94	-51 16 40.00	1.91	10.343	0.618	1.533	0.228	29.11	4.59	12.61	1.88	12.89	10.35	0.249	–	S
1262	23 49 57.40	0.30	-59 25 55.62	0.51	12.032	0.842	6.690	0.434	19.71	1.26	3.12	0.32	111.36	3.54	0.230	–	M
1263	23 46 31.27	0.98	-52 04 13.85	1.15	2.260	0.347	1.101	0.238	9.97	2.74	6.83	2.17	145.55	52.77	0.212	–	S
1264	23 47 33.46	0.61	-54 40 51.95	0.93	2.360	0.275	1.153	0.183	10.73	2.16	5.71	1.34	163.11	20.52	0.160	–	S
1265	23 47 06.58	1.76	-53 41 23.98	1.03	57.399	3.234	5.776	0.525	34.80	4.42	15.03	1.79	19.63	11.08	0.418	–	M
1266	23 46 08.24	0.52	-51 06 35.06	0.48	3.341	0.522	2.562	0.338	5.17	1.18	3.78	1.07	91.24	59.40	0.291	–	S
1267	23 45 51.07	1.15	-50 17 49.87	0.73	2.150	0.226	0.874	0.150	12.67	2.82	7.25	1.58	78.55	19.99	0.134	–	S
1268	23 45 48.47	1.14	-50 10 48.95	0.91	1.928	0.229	0.807	0.156	11.01	2.69	8.43	2.07	88.03	41.87	0.138	–	S
1269	23 48 09.61	0.22	-56 07 53.51	0.22	4.837	0.408	3.096	0.216	4.48	0.43	2.22	0.35	40.42	18.10	0.134	–	M
1270	23 46 30.63	0.74	-52 15 45.22	0.31	23.506	1.390	4.869	0.374	22.46	1.76	5.10	0.48	161.60	4.89	0.261	–	M
1271	23 46 05.49	0.77	-51 08 35.06	1.83	19.670	1.225	2.455	0.363	20.73	4.37	7.90	1.58	75.42	15.44	0.337	–	M
1272	23 48 05.48	0.36	-56 01 25.52	0.50	2.882	0.287	1.749	0.187	8.10	1.12	4.54	0.78	178.38	15.42	0.150	–	S
1273	23 46 09.94	0.48	-51 18 05.40	0.44	2.813	0.426	2.232	0.275	5.69	1.18	2.23	0.88	116.57	27.18	0.236	–	S
1274	23 45 47.67	0.77	-50 13 22.94	1.21	1.583	0.220	0.763	0.150	11.00	2.73	6.29	1.84	172.96	32.65	0.133	–	S
1275	23 46 22.22	0.23	-51 54 16.13	0.25	6.240	0.502	4.695	0.346	5.03	0.46	4.34	0.46	3.40	65.51	0.218	–	S
1276	23 47 02.66	1.48	-53 42 05.07	2.17	50.191	2.772	2.274	0.273	48.66	5.30	27.99	3.09	154.35	9.97	0.435	–	S
1277	23 49 55.83	0.23	-59 42 31.94	0.18	53.030	3.019	37.765	2.097	33.25	0.49	4.27	0.07	148.17	0.71	0.291	-0.15	M
1278	23 46 54.36	0.15	-53 23 54.14	0.16	18.256	1.062	15.179	0.861	4.53	0.14	2.49	0.11	65.86	2.70	0.204	-0.96	S
1279	23 46 18.05	0.15	-51 50 15.79	0.17	61.946	3.458	29.102	1.632	11.10	0.19	8.99	0.15	74.98	3.79	0.319	-0.81	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1280	23 48 57.11	0.15	-57 52 23.76	0.16	13.244	0.810	12.048	0.695	2.73	0.14	2.22	0.14	135.16	39.46	0.206	-0.69	S
1281	23 46 39.48	0.18	-52 51 22.08	0.40	26.521	1.571	10.195	0.620	16.58	0.86	3.80	0.27	87.91	3.22	0.264	-	M
1282	23 46 41.88	0.17	-52 55 21.71	0.17	18.582	1.252	12.623	0.741	7.37	0.26	0.00	0.13	41.89	2.79	0.259	0.05	M
1283	23 47 03.31	0.31	-53 50 52.96	0.31	8.352	0.616	4.692	0.382	7.42	0.66	6.80	0.63	62.72	45.13	0.259	-	S
1284	23 47 05.71	0.17	-53 56 54.09	0.19	9.846	0.688	8.731	0.543	3.52	0.26	2.07	0.24	22.14	17.72	0.248	-	S
1285	23 47 01.85	0.20	-53 48 40.76	0.22	6.234	0.568	6.124	0.427	0.00	0.36	0.00	0.34	0.00	34.12	0.262	-	S
1286	23 46 33.50	0.19	-52 37 12.43	0.20	6.463	0.462	5.448	0.350	3.83	0.30	3.15	0.29	40.78	35.09	0.174	-	S
1287	23 46 03.10	0.16	-51 19 37.22	0.17	11.072	0.711	9.821	0.583	3.80	0.21	1.74	0.18	27.53	9.11	0.214	-0.98	S
1288	23 46 17.00	1.43	-51 54 32.09	1.04	2.824	0.351	1.098	0.243	12.62	3.46	7.94	2.27	103.40	33.54	0.221	-	S
1289	23 45 54.70	0.49	-50 52 14.08	0.42	2.164	0.347	1.788	0.222	4.97	1.14	1.97	0.89	74.22	31.91	0.192	-	S
1290	23 45 58.85	0.40	-51 08 43.83	0.75	24.839	1.509	4.975	0.449	14.93	1.74	7.65	0.88	87.70	11.15	0.356	-	M
1291	23 48 15.13	0.59	-56 39 38.79	0.68	1.812	0.275	1.171	0.181	7.20	1.64	4.35	1.23	25.30	32.03	0.158	-	S
1292	23 49 03.77	0.18	-58 18 36.48	0.20	53.783	3.041	23.928	1.352	16.77	0.39	5.49	0.15	125.55	1.67	0.311	-1.09	M
1293	23 46 45.04	0.98	-53 13 50.07	0.98	1.343	0.271	0.807	0.181	7.08	2.45	6.07	2.11	47.97	119.56	0.163	-	S
1294	23 46 36.91	0.14	-52 54 31.53	0.15	97.331	5.373	95.483	5.258	1.51	0.02	0.56	0.02	5.97	4.53	0.266	-0.52	S
1295	23 45 51.08	0.22	-50 49 56.90	0.22	5.412	0.453	4.618	0.328	3.87	0.42	2.86	0.39	89.05	34.16	0.200	-	S
1296	23 45 55.90	0.91	-51 05 44.71	0.80	2.802	0.406	1.488	0.274	8.46	2.13	6.89	1.83	73.49	59.25	0.241	-	S
1297	23 45 50.47	0.14	-50 50 50.96	0.15	24.998	1.421	23.503	1.310	2.40	0.08	1.73	0.07	145.01	19.84	0.208	-0.48	S
1298	23 48 52.40	0.65	-57 58 22.99	0.60	1.231	0.342	1.138	0.208	3.01	1.54	1.13	1.33	60.20	122.22	0.195	-	S
1299	23 45 56.12	0.73	-51 12 06.76	0.51	34.239	2.205	17.521	1.044	21.32	1.94	6.74	0.63	28.50	6.29	0.402	-0.43	M
1300	23 46 09.47	0.26	-51 50 34.69	0.26	9.428	0.740	6.605	0.498	5.82	0.53	4.79	0.47	59.18	26.77	0.319	-	S
1301	23 47 59.85	0.80	-56 17 08.36	0.88	1.494	0.261	0.893	0.174	7.40	2.14	5.55	1.73	26.11	60.80	0.155	-	S
1302	23 48 30.78	0.20	-57 21 23.82	0.22	3.783	0.301	3.228	0.221	4.59	0.39	1.25	0.31	157.31	9.46	0.128	-	S
1303	23 48 05.24	0.96	-56 29 25.56	1.52	3.391	0.274	0.978	0.168	18.90	3.89	6.96	1.47	23.17	11.31	0.162	-	S
1304	23 48 11.92	1.14	-56 43 54.82	0.81	1.918	0.295	0.967	0.201	9.56	2.60	6.17	1.91	85.09	41.89	0.179	-	S
1305	23 49 00.27	0.44	-58 18 51.27	0.47	3.712	0.568	2.896	0.368	4.79	1.09	3.46	0.95	158.19	61.97	0.315	-	S
1306	23 47 27.69	0.17	-55 11 17.48	0.17	39.482	2.251	18.624	1.065	10.62	0.23	7.11	0.16	177.96	3.49	0.292	-1.26	M
1307	23 46 02.16	0.26	-51 33 11.51	0.23	8.058	0.614	4.428	0.305	7.50	0.57	0.00	0.32	147.06	7.29	0.183	-	M
1308	23 45 54.04	0.19	-51 10 02.77	0.20	11.322	0.862	10.149	0.662	3.47	0.32	2.00	0.29	133.99	26.32	0.347	-	S
1309	23 49 02.50	0.16	-58 26 51.88	0.18	14.871	0.914	10.926	0.654	6.34	0.25	2.72	0.18	149.82	1.55	0.245	-0.63	S
1310	23 46 43.48	0.49	-53 26 56.85	0.41	4.755	0.401	2.426	0.252	9.03	1.13	6.76	0.88	70.62	22.03	0.197	-	S
1311	23 47 57.62	0.24	-56 25 10.10	0.30	3.459	0.293	2.486	0.197	6.17	0.61	3.56	0.47	176.30	13.13	0.134	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1312	23 48 08.37	0.71	-56 47 05.39	0.78	1.849	0.343	1.232	0.224	6.93	1.91	4.19	1.48	143.91	45.61	0.200	–	S
1313	23 48 34.02	0.20	-57 39 59.28	0.21	5.359	0.418	4.610	0.311	3.90	0.34	2.33	0.32	142.60	21.00	0.174	–	S
1314	23 47 45.81	0.90	-56 01 28.62	0.81	0.972	0.215	0.670	0.139	6.91	2.27	3.48	1.63	49.86	41.72	0.127	–	S
1315	23 48 29.59	0.41	-57 34 05.79	0.60	1.971	0.261	1.355	0.170	7.88	1.41	1.85	0.82	156.45	13.08	0.145	–	S
1316	23 48 14.59	0.76	-57 04 57.70	0.94	1.550	0.249	0.870	0.167	8.38	2.26	5.48	1.66	18.27	38.93	0.148	–	S
1317	23 48 02.53	1.05	-56 46 31.57	2.11	5.229	0.364	0.995	0.197	22.58	4.94	11.24	2.41	171.14	16.96	0.206	–	S
1318	23 47 31.07	0.48	-55 39 18.07	0.51	3.352	0.357	1.964	0.234	7.93	1.22	5.46	0.99	140.86	29.27	0.192	–	S
1319	23 48 50.26	2.09	-58 21 55.35	1.30	5.381	0.374	1.023	0.202	23.81	5.17	10.29	2.25	59.26	14.94	0.213	–	S
1320	23 46 59.19	0.44	-54 26 00.24	0.52	1.862	0.291	1.445	0.188	5.06	1.14	3.49	1.01	177.62	58.75	0.162	–	S
1321	23 48 28.57	0.18	-57 41 43.91	0.19	8.579	0.558	6.526	0.405	5.23	0.28	3.52	0.24	153.54	9.48	0.178	–	S
1322	23 46 30.71	1.57	-53 17 21.27	0.78	2.438	0.259	0.882	0.175	14.97	3.72	6.82	1.76	82.09	18.27	0.162	–	S
1323	23 48 19.22	0.92	-57 25 17.76	0.68	1.098	0.270	0.829	0.172	6.12	2.13	2.49	1.55	70.07	44.51	0.158	–	S
1324	23 45 33.61	0.64	-50 40 35.86	0.73	2.370	0.401	1.600	0.262	7.20	1.75	4.18	1.37	140.62	41.24	0.231	–	S
1325	23 47 04.96	0.46	-54 45 51.11	0.47	2.673	0.307	1.716	0.202	6.48	1.08	5.50	1.00	131.14	87.22	0.166	–	S
1326	23 45 44.27	0.18	-51 16 08.82	0.20	7.883	0.585	7.239	0.461	3.42	0.30	1.08	0.26	148.06	16.91	0.229	–	S
1327	23 47 03.12	0.64	-54 43 35.67	0.66	2.339	0.286	1.286	0.190	7.84	1.56	6.67	1.40	138.50	93.99	0.162	–	S
1328	23 47 55.55	0.14	-56 43 35.58	0.15	67.385	3.724	61.148	3.370	3.31	0.03	1.52	0.03	132.62	178.82	0.215	-0.79	S
1329	23 45 32.17	0.71	-50 44 30.21	1.43	2.544	0.445	1.386	0.299	11.13	3.29	3.83	1.65	2.19	23.32	0.273	–	S
1330	23 46 21.21	0.82	-53 05 16.32	0.65	1.575	0.285	1.058	0.186	7.30	1.97	3.72	1.38	64.44	32.35	0.166	–	S
1331	23 47 22.80	0.47	-55 39 43.20	0.55	3.071	0.357	1.904	0.234	7.90	1.31	4.50	0.95	146.97	21.86	0.195	–	S
1332	23 45 32.66	0.98	-50 57 44.24	0.99	2.459	0.320	1.126	0.218	10.39	2.51	7.55	2.03	127.32	49.70	0.193	–	S
1333	23 49 31.48	0.18	-59 55 02.95	0.19	11.021	0.743	8.923	0.558	4.76	0.28	2.48	0.24	31.72	6.84	0.254	–	S
1334	23 47 40.23	0.27	-56 22 57.35	0.31	3.773	0.332	2.671	0.222	5.88	0.63	4.24	0.55	175.56	23.59	0.157	–	S
1335	23 46 23.15	0.54	-53 21 37.18	0.84	2.867	0.306	1.395	0.201	10.60	1.93	6.05	1.24	0.38	20.35	0.173	–	S
1336	23 45 52.80	0.18	-52 03 58.33	0.20	94.234	5.250	29.182	1.639	16.14	0.38	6.92	0.16	47.56	1.92	0.334	-1.31	M
1337	23 49 19.10	0.96	-59 36 28.47	0.79	3.239	0.366	1.386	0.247	10.05	2.23	8.03	1.84	78.37	68.12	0.217	–	S
1338	23 46 46.85	0.96	-54 24 23.32	1.22	2.246	0.268	0.895	0.184	11.18	2.81	8.60	2.26	4.18	52.93	0.165	–	S
1339	23 47 19.27	0.50	-55 41 07.76	0.47	2.366	0.326	1.694	0.212	6.59	1.25	3.09	0.90	47.15	22.22	0.181	–	S
1340	23 46 08.83	1.05	-52 48 48.91	0.91	1.826	0.288	0.955	0.195	9.71	2.65	5.80	1.85	117.13	36.67	0.175	–	S
1341	23 45 13.36	0.52	-50 08 43.11	0.72	4.030	0.309	1.545	0.183	12.37	1.63	8.74	1.21	7.09	23.09	0.151	–	S
1342	23 49 23.33	0.94	-59 49 05.69	1.00	5.478	0.415	1.670	0.241	17.68	2.88	6.80	1.23	135.60	9.24	0.224	–	S
1343	23 47 37.70	0.59	-56 26 46.90	0.65	2.508	0.283	1.351	0.187	9.30	1.64	5.38	1.14	139.85	21.70	0.159	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1344	23 46 26.30	0.69	-53 38 28.13	0.73	1.387	0.309	1.066	0.197	5.35	1.75	3.44	1.51	140.07	78.86	0.178	–	S
1345	23 47 19.18	1.91	-55 49 04.60	0.99	7.576	0.623	3.739	0.282	25.50	4.97	2.54	0.90	150.63	9.60	0.193	–	M
1346	23 49 08.67	0.34	-59 26 21.01	0.34	3.479	0.513	3.170	0.333	2.64	0.74	2.20	0.72	158.34	86.08	0.277	–	S
1347	23 48 03.99	0.47	-57 26 10.12	0.74	1.821	0.268	1.192	0.175	8.13	1.73	2.65	1.01	9.53	16.77	0.153	–	S
1348	23 48 44.78	0.14	-58 47 11.99	0.15	80.119	4.423	78.519	4.324	0.00	0.02	0.00	0.02	0.00	0.41	0.217	0.23	S
1349	23 46 15.56	0.91	-53 18 16.33	1.02	1.966	0.249	0.883	0.170	9.99	2.39	7.96	2.08	148.77	73.59	0.150	–	S
1350	23 46 27.98	0.90	-53 53 01.81	0.46	5.943	0.493	2.441	0.224	13.82	2.29	0.00	0.45	152.12	6.89	0.179	–	M
1351	23 48 04.00	0.19	-57 32 47.70	0.21	4.373	0.340	3.830	0.256	4.27	0.35	0.00	0.28	9.79	8.49	0.141	–	S
1352	23 48 01.60	0.38	-57 28 16.79	0.46	3.076	0.285	1.754	0.184	7.78	1.02	5.86	0.85	176.76	25.71	0.145	–	S
1353	23 46 39.58	0.57	-54 25 26.42	0.86	2.904	0.310	1.382	0.204	10.83	1.99	6.09	1.28	164.49	20.06	0.176	–	S
1354	23 48 39.31	0.47	-58 43 34.66	0.42	2.795	0.371	2.027	0.242	6.25	1.10	3.25	0.86	121.40	26.12	0.203	–	S
1355	23 46 20.09	0.69	-53 38 44.02	0.85	1.862	0.309	1.142	0.205	7.40	1.92	5.40	1.62	177.01	61.50	0.181	–	S
1356	23 45 36.32	0.26	-51 43 29.55	0.29	5.310	0.405	3.470	0.266	6.71	0.57	5.20	0.51	155.11	29.05	0.172	–	S
1357	23 46 23.20	0.48	-53 52 44.21	0.47	2.025	0.308	1.559	0.200	4.72	1.11	4.06	1.01	53.36	110.30	0.171	–	S
1358	23 47 09.67	0.86	-55 44 30.24	1.14	1.767	0.298	0.933	0.203	8.85	2.64	6.17	2.01	2.41	50.79	0.181	–	S
1359	23 45 53.75	0.58	-52 35 29.03	0.69	1.975	0.302	1.294	0.198	6.93	1.58	4.80	1.31	18.95	46.96	0.173	–	S
1360	23 49 08.32	0.22	-59 42 21.66	0.23	4.713	0.414	4.009	0.295	3.72	0.43	2.71	0.40	14.31	33.91	0.190	–	S
1361	23 47 12.94	0.52	-55 53 38.07	0.59	1.519	0.234	1.063	0.152	5.78	1.35	4.60	1.18	4.46	72.85	0.132	–	S
1362	23 48 06.54	0.14	-57 50 25.85	0.15	69.893	3.874	52.594	2.908	6.20	0.06	2.42	0.04	141.74	177.62	0.287	-1.33	S
1363	23 46 41.33	0.83	-54 43 46.52	0.70	2.486	0.297	1.222	0.199	9.40	1.98	6.87	1.54	62.49	37.57	0.173	–	S
1364	23 48 41.55	0.27	-58 59 27.59	0.27	4.357	0.397	3.300	0.270	4.56	0.57	4.29	0.52	157.08	118.29	0.189	–	S
1365	23 47 21.27	0.15	-56 19 43.39	0.16	10.882	0.662	9.729	0.561	2.93	0.15	2.51	0.15	42.32	33.05	0.164	-0.55	S
1366	23 46 05.89	0.16	-53 23 30.29	0.17	20.856	1.231	13.156	0.749	8.02	0.20	3.46	0.13	123.47	3.00	0.195	-0.72	M
1367	23 45 12.39	0.18	-50 54 44.57	0.30	18.847	1.198	11.248	0.667	12.57	0.64	0.00	0.20	69.77	2.90	0.250	-0.53	M
1368	23 47 20.12	0.55	-56 28 10.54	0.67	10.630	0.683	2.280	0.224	15.41	1.83	6.36	0.79	49.64	9.45	0.186	–	M
1369	23 46 54.89	0.70	-55 30 20.61	0.49	1.866	0.296	1.288	0.192	7.12	1.59	3.29	1.12	89.33	26.49	0.169	–	S
1370	23 48 14.35	0.20	-58 20 08.45	0.20	8.379	0.614	6.791	0.449	4.52	0.34	2.99	0.31	140.64	17.33	0.239	–	S
1371	23 48 02.81	0.45	-57 57 20.29	0.53	1.939	0.402	1.742	0.251	3.83	1.22	0.00	1.00	166.47	47.94	0.226	–	S
1372	23 48 00.98	0.29	-57 55 25.41	0.19	19.544	1.232	8.297	0.526	10.78	0.61	3.40	0.28	175.42	4.34	0.261	–	M
1373	23 45 06.51	0.86	-50 44 23.76	0.96	4.316	0.543	2.116	0.363	11.96	2.68	4.93	1.37	135.13	18.05	0.324	–	S
1374	23 45 39.07	0.62	-52 20 51.03	0.80	1.171	0.307	1.004	0.189	5.38	1.89	0.00	1.33	150.20	38.11	0.176	–	S
1375	23 45 47.56	0.89	-52 45 43.07	0.79	2.750	0.287	1.163	0.191	10.73	2.13	8.26	1.74	110.23	43.75	0.166	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1376	23 45 35.33	0.34	-52 11 39.16	0.44	2.945	0.373	2.280	0.244	5.73	0.96	2.86	0.75	1.07	26.16	0.200	–	S
1377	23 46 42.01	0.19	-55 07 36.31	0.21	7.178	0.501	5.402	0.355	5.26	0.35	3.84	0.31	7.51	15.73	0.184	–	S
1378	23 48 02.85	1.10	-58 05 09.07	0.91	6.613	0.426	1.388	0.202	17.34	2.60	13.32	2.05	59.46	27.35	0.193	–	S
1379	23 47 28.56	0.60	-56 53 06.43	0.61	1.987	0.344	1.427	0.223	6.10	1.54	3.60	1.21	38.48	40.05	0.197	–	S
1380	23 45 06.80	0.14	-50 53 58.62	0.15	82.238	4.540	77.785	4.284	2.90	0.03	0.13	0.02	164.54	179.13	0.227	-0.85	S
1381	23 45 50.83	0.57	-53 03 01.50	0.51	4.022	0.346	1.877	0.217	9.78	1.37	7.51	1.07	61.97	25.49	0.177	–	S
1382	23 45 45.03	0.50	-52 50 35.89	2.03	4.339	0.410	0.912	0.178	0.00	4.85	0.00	0.63	0.00	10.08	0.171	–	M
1383	23 47 38.29	0.14	-57 20 42.17	0.15	42.489	2.352	40.864	2.253	1.76	0.03	1.38	0.03	128.90	105.09	0.152	-0.01	S
1384	23 45 42.81	0.80	-52 43 19.34	0.53	2.798	0.309	1.495	0.201	11.21	2.04	3.45	0.91	62.12	10.69	0.175	–	S
1385	23 46 42.53	0.71	-55 17 28.72	0.76	1.222	0.252	0.882	0.163	6.42	1.89	3.33	1.44	138.61	44.70	0.147	–	S
1386	23 48 07.29	0.44	-58 21 16.14	0.41	3.115	0.420	2.352	0.274	5.41	1.00	3.48	0.86	121.32	42.41	0.229	–	S
1387	23 45 06.96	0.22	-51 07 19.52	0.24	28.037	1.672	11.313	0.688	13.20	0.54	4.94	0.25	128.48	3.57	0.294	–	M
1388	23 47 21.91	0.14	-56 55 59.93	0.15	41.545	2.313	41.043	2.267	0.00	0.04	0.00	0.04	0.00	2.10	0.206	-0.66	S
1389	23 47 00.59	0.44	-56 05 58.05	0.61	1.837	0.225	1.152	0.148	8.03	1.43	3.96	0.94	13.31	18.11	0.125	–	S
1390	23 44 48.22	0.58	-50 10 27.66	1.10	1.787	0.249	0.974	0.165	11.12	2.56	3.89	1.26	10.45	17.48	0.148	–	S
1391	23 48 11.57	0.54	-58 35 12.62	0.46	1.931	0.312	1.479	0.201	5.16	1.21	3.45	1.03	71.26	58.13	0.175	–	S
1392	23 46 16.73	0.22	-54 23 50.44	0.24	4.400	0.354	3.441	0.249	4.96	0.45	3.47	0.40	159.06	24.42	0.154	–	S
1393	23 45 22.72	0.98	-51 59 16.35	1.09	2.046	0.329	1.043	0.225	8.85	2.56	7.14	2.22	31.18	77.42	0.200	–	S
1394	23 44 46.20	0.68	-50 06 49.43	0.81	1.521	0.286	1.043	0.186	7.04	1.89	4.11	1.53	145.21	48.80	0.166	–	S
1395	23 44 47.81	0.23	-50 16 47.30	0.40	9.866	0.689	3.919	0.283	10.56	0.87	3.87	0.43	86.31	7.12	0.183	–	M
1396	23 46 18.63	0.60	-54 34 29.69	0.77	2.703	0.285	1.312	0.187	10.46	1.85	6.12	1.24	150.91	21.19	0.160	–	S
1397	23 48 42.37	1.21	-59 39 47.69	0.81	2.388	0.312	1.069	0.213	11.38	2.83	6.07	1.76	64.83	25.77	0.192	–	S
1398	23 45 41.13	0.53	-53 00 55.18	0.42	4.016	0.366	2.134	0.234	8.86	1.21	6.32	0.92	90.75	22.78	0.187	–	S
1399	23 46 45.08	0.16	-55 43 00.53	0.17	10.463	0.646	9.153	0.534	3.54	0.17	2.39	0.16	176.75	13.17	0.172	-0.08	S
1400	23 46 58.01	0.61	-56 11 49.76	0.55	1.071	0.238	0.916	0.149	4.22	1.43	2.11	1.21	109.84	71.97	0.135	–	S
1401	23 45 41.13	1.44	-53 01 20.32	1.03	2.856	0.294	0.986	0.198	14.80	3.68	7.73	1.92	61.00	20.84	0.183	–	S
1402	23 47 14.25	0.15	-56 50 57.52	0.16	14.999	0.898	13.841	0.790	2.91	0.13	1.41	0.12	176.77	9.20	0.207	0.38	S
1403	23 45 17.08	0.23	-51 57 08.64	0.27	5.191	0.409	3.762	0.279	6.39	0.54	3.57	0.41	146.11	12.47	0.176	–	S
1404	23 46 22.83	1.13	-54 52 44.58	0.83	1.578	0.281	0.875	0.190	8.70	2.61	5.62	1.94	89.79	47.43	0.170	–	S
1405	23 46 56.44	0.14	-56 13 50.10	0.15	61.193	3.378	58.782	3.237	1.69	0.02	1.52	0.02	82.99	117.96	0.165	-0.94	S
1406	23 47 47.32	0.84	-58 01 33.63	1.01	1.779	0.333	1.042	0.223	7.61	2.41	5.56	1.88	166.61	62.17	0.200	–	S
1407	23 47 24.64	0.14	-57 19 20.27	0.15	20.803	1.183	20.161	1.123	1.77	0.07	0.88	0.07	24.70	104.69	0.174	0.18	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1408	23 46 05.64	0.67	-54 13 11.22	1.19	2.039	0.263	0.961	0.178	11.64	2.77	5.45	1.54	169.11	21.03	0.159	–	S
1409	23 45 05.46	0.29	-51 34 28.27	0.28	42.842	2.403	7.817	0.510	15.69	0.61	14.36	0.57	9.90	29.89	0.275	–	M
1410	23 48 11.51	0.31	-58 54 21.56	0.32	3.143	0.341	2.464	0.228	4.29	0.70	3.90	0.62	0.52	93.76	0.174	–	S
1411	23 46 38.47	0.74	-55 37 42.49	1.50	2.678	0.258	0.919	0.169	15.78	3.52	6.80	1.63	167.02	15.79	0.158	–	S
1412	23 47 40.86	0.34	-57 57 45.99	0.36	4.161	0.402	2.760	0.265	5.84	0.80	5.35	0.72	178.79	72.66	0.202	–	S
1413	23 45 59.85	0.15	-54 09 55.54	0.16	11.011	0.671	9.973	0.575	3.10	0.15	2.03	0.14	149.72	16.67	0.168	-0.85	S
1414	23 45 46.20	0.89	-53 34 04.43	0.70	2.703	0.286	1.213	0.189	11.55	2.23	6.44	1.38	113.50	20.36	0.165	–	S
1415	23 44 51.09	0.48	-50 55 44.00	0.54	3.720	0.396	2.199	0.258	8.78	1.35	4.88	0.92	137.86	19.43	0.212	–	S
1416	23 48 05.24	0.16	-58 52 27.77	0.16	18.963	1.126	12.891	0.738	6.66	0.20	0.00	0.12	136.27	2.79	0.206	-0.68	M
1417	23 46 36.58	0.53	-55 44 38.52	0.59	2.525	0.287	1.437	0.189	7.87	1.39	5.94	1.14	27.43	36.39	0.158	–	S
1418	23 46 43.06	0.92	-56 00 13.71	0.99	1.067	0.215	0.647	0.143	7.54	2.46	5.27	1.96	141.71	68.92	0.129	–	S
1419	23 47 17.72	0.24	-57 18 51.02	0.27	4.655	0.410	3.646	0.283	4.71	0.51	3.51	0.47	178.23	29.98	0.190	–	S
1420	23 46 02.02	1.09	-54 23 13.26	0.65	4.260	0.323	1.328	0.189	15.99	2.62	8.27	1.35	70.84	12.68	0.170	–	S
1421	23 48 06.44	0.93	-58 58 36.11	0.93	1.598	0.317	0.959	0.212	6.95	2.32	5.83	2.01	141.01	131.05	0.190	–	S
1422	23 46 51.46	0.80	-56 25 20.99	0.86	2.468	0.249	1.004	0.164	10.18	2.05	8.99	1.79	157.71	87.10	0.143	–	S
1423	23 45 13.40	0.16	-52 16 10.33	0.17	9.006	0.576	8.563	0.501	2.57	0.18	0.69	0.16	121.59	16.16	0.170	-0.08	S
1424	23 45 42.13	1.08	-53 37 08.47	0.79	1.452	0.254	0.829	0.171	8.80	2.57	5.06	1.75	71.16	35.77	0.153	–	S
1425	23 46 48.70	0.47	-56 21 57.45	0.47	2.151	0.267	1.447	0.175	6.17	1.11	4.89	0.99	136.04	63.44	0.146	–	S
1426	23 45 31.95	0.62	-53 10 17.50	0.63	1.936	0.265	1.181	0.175	6.73	1.51	6.20	1.36	50.09	122.66	0.151	–	S
1427	23 47 54.26	0.59	-58 40 55.15	0.52	3.660	0.358	1.844	0.232	8.62	1.35	6.94	1.16	60.26	44.07	0.192	–	S
1428	23 47 50.22	1.11	-58 32 33.36	0.81	1.755	0.282	0.921	0.192	9.40	2.57	5.59	1.83	105.55	39.06	0.171	–	S
1429	23 44 40.57	0.14	-50 41 14.65	0.15	213.643	11.895	207.214	11.448	2.01	0.05	0.48	0.04	27.97	4.85	1.070	-0.69	S
1430	23 48 30.35	0.64	-59 48 13.59	0.52	1.712	0.291	1.240	0.189	6.14	1.47	3.31	1.14	60.80	36.81	0.166	–	S
1431	23 47 10.21	0.30	-57 16 07.73	0.32	2.782	0.375	2.583	0.247	3.16	0.68	0.00	0.60	31.15	38.44	0.199	–	S
1432	23 46 49.76	1.15	-56 31 40.26	1.70	3.707	0.261	0.770	0.143	20.50	4.23	11.19	2.23	20.54	17.38	0.144	–	S
1433	23 46 04.39	1.21	-54 44 43.19	1.15	2.351	0.265	0.851	0.182	11.07	2.85	10.20	2.66	101.05	176.71	0.165	–	S
1434	23 47 14.83	0.39	-57 28 29.74	0.51	3.553	0.299	1.851	0.187	10.45	1.23	4.59	0.70	149.32	8.30	0.147	–	S
1435	23 45 35.82	0.96	-53 33 15.48	1.01	1.624	0.258	0.847	0.175	9.14	2.57	6.28	1.93	38.61	44.95	0.156	–	S
1436	23 44 46.71	0.28	-51 13 23.59	0.32	5.538	0.446	3.582	0.291	7.18	0.68	4.95	0.55	149.69	20.46	0.200	–	S
1437	23 47 07.69	0.14	-57 18 14.33	0.15	34.963	1.951	34.414	1.903	1.51	0.04	0.00	0.04	134.45	8.47	0.192	0.31	S
1438	23 47 11.60	0.85	-57 27 45.64	1.22	3.547	0.269	1.031	0.156	18.19	3.15	7.39	1.36	147.65	10.69	0.147	–	S
1439	23 46 56.38	0.26	-56 56 39.27	0.19	28.818	1.694	10.833	0.644	17.27	0.57	5.42	0.20	153.26	2.24	0.245	-0.22	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1440	23 45 58.59	0.61	-54 38 08.42	0.73	0.984	0.257	0.854	0.159	4.20	1.67	1.65	1.40	163.66	73.45	0.147	–	S
1441	23 44 42.86	0.30	-51 05 54.99	0.31	3.964	0.396	3.066	0.267	4.80	0.64	4.06	0.62	105.22	62.82	0.196	–	S
1442	23 48 11.37	0.34	-59 29 25.20	0.36	5.037	0.481	3.309	0.316	5.95	0.79	5.29	0.71	179.33	51.79	0.240	–	S
1443	23 44 32.30	0.25	-50 39 55.78	0.44	212.136	15.270	111.968	7.490	15.35	1.08	0.00	0.19	62.18	2.81	4.264	–	M
1444	23 45 48.02	1.15	-54 16 44.40	0.86	1.475	0.236	0.757	0.161	9.39	2.70	6.22	1.97	74.77	43.12	0.144	–	S
1445	23 47 20.62	0.26	-57 53 13.16	0.25	3.899	0.406	3.516	0.282	3.09	0.50	2.00	0.47	58.68	56.38	0.201	–	S
1446	23 47 01.28	0.49	-57 13 16.30	0.64	2.260	0.326	1.506	0.213	7.02	1.47	3.97	1.09	168.39	28.34	0.184	–	S
1447	23 46 48.80	1.19	-56 48 54.30	1.56	4.720	0.335	0.975	0.186	17.75	3.66	13.44	2.76	168.75	34.82	0.185	–	S
1448	23 46 56.38	0.17	-57 06 46.02	0.18	6.091	0.446	5.871	0.366	0.00	0.24	0.00	0.23	0.00	18.96	0.170	–	S
1449	23 46 10.70	0.85	-55 22 59.75	1.31	2.299	0.266	0.981	0.178	14.51	3.36	4.29	1.32	148.85	13.49	0.165	–	S
1450	23 47 05.07	0.77	-57 29 27.63	0.37	3.891	0.377	1.733	0.168	0.00	1.86	0.00	0.57	0.00	9.14	0.138	–	M
1451	23 46 38.64	0.15	-56 35 46.04	0.16	11.889	0.738	11.826	0.680	0.00	0.14	0.00	0.13	0.00	9.33	0.198	0.74	S
1452	23 47 28.65	0.15	-58 23 01.51	0.16	15.675	0.951	15.000	0.858	2.06	0.13	1.09	0.13	22.48	21.49	0.232	-0.18	S
1453	23 47 50.82	0.18	-59 07 40.11	0.18	14.235	0.960	11.681	0.728	4.08	0.26	3.20	0.25	140.07	25.72	0.328	–	S
1454	23 47 51.94	0.15	-59 15 43.39	0.16	164.868	9.605	155.876	8.773	2.13	0.10	1.60	0.10	135.89	119.99	1.839	-0.18	S
1455	23 45 02.72	1.96	-52 39 24.26	0.98	2.680	0.233	0.714	0.150	18.74	4.73	8.90	2.15	77.86	18.70	0.147	–	S
1456	23 46 10.60	0.27	-55 41 55.91	0.28	3.215	0.324	2.649	0.222	4.24	0.57	3.07	0.53	151.23	46.16	0.160	–	S
1457	23 45 05.01	0.52	-52 49 25.41	0.72	1.708	0.326	1.303	0.209	6.10	1.61	2.64	1.21	175.33	36.80	0.187	–	S
1458	23 45 57.82	0.18	-55 14 13.91	0.20	5.784	0.523	4.641	0.307	0.00	0.34	0.00	0.24	0.00	8.69	0.170	–	M
1459	23 44 23.07	0.89	-50 44 37.06	0.70	2.836	0.522	1.849	0.342	7.76	2.17	4.02	1.49	105.27	34.07	0.306	–	S
1460	23 45 15.17	0.71	-53 21 33.57	1.88	2.766	0.264	0.891	0.174	18.30	4.37	6.21	1.63	172.97	14.40	0.168	–	S
1461	23 46 11.36	0.14	-55 51 53.93	0.15	23.399	1.308	22.830	1.263	1.68	0.05	0.61	0.05	154.97	9.74	0.136	0.13	S
1462	23 46 47.57	0.23	-57 12 36.56	0.25	3.915	0.376	3.441	0.265	3.42	0.47	2.36	0.44	168.04	46.03	0.181	–	S
1463	23 45 01.79	1.20	-52 48 14.84	1.15	2.171	0.255	0.879	0.173	14.26	3.52	5.78	1.64	128.40	18.28	0.159	–	S
1464	23 44 31.53	0.14	-51 19 05.80	0.15	42.363	2.354	39.984	2.208	2.40	0.04	1.56	0.04	144.38	6.79	0.195	-0.69	S
1465	23 45 19.46	0.89	-53 40 43.32	1.13	1.342	0.249	0.759	0.168	8.83	2.69	5.30	1.96	152.44	45.60	0.151	–	S
1466	23 44 46.79	0.72	-52 10 04.02	0.72	1.467	0.279	1.020	0.182	5.51	1.72	5.27	1.60	90.93	176.97	0.162	–	S
1467	23 44 19.26	0.18	-50 46 12.65	0.19	8.883	0.688	8.419	0.543	2.32	0.29	1.38	0.28	67.39	47.41	0.281	–	S
1468	23 46 49.81	1.09	-57 27 05.99	2.28	4.451	0.283	0.683	0.130	25.86	5.36	12.70	2.52	1.13	15.65	0.144	–	S
1469	23 44 20.70	0.41	-50 53 40.02	0.34	2.779	0.348	2.209	0.228	5.61	0.95	2.12	0.68	88.49	20.08	0.185	–	S
1470	23 46 12.72	1.27	-56 06 13.98	1.01	5.589	0.392	0.899	0.143	15.10	3.58	3.64	1.24	140.45	15.57	0.134	–	M
1471	23 44 31.29	0.62	-51 29 32.06	0.68	3.635	0.324	1.574	0.206	10.31	1.54	8.47	1.41	143.47	56.78	0.172	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1472	23 45 00.56	0.17	-52 58 09.28	0.18	6.594	0.452	5.956	0.365	3.03	0.23	2.21	0.23	28.99	32.53	0.157	–	S
1473	23 44 39.38	0.77	-51 56 56.24	1.11	4.366	0.416	0.811	0.168	8.66	2.77	2.08	1.48	111.54	29.15	0.162	–	M
1474	23 44 45.99	0.98	-52 17 50.39	1.00	2.037	0.276	0.953	0.188	10.00	2.57	7.33	1.98	42.81	45.03	0.167	–	S
1475	23 47 47.54	0.56	-59 30 33.49	0.51	2.702	0.368	1.771	0.242	6.54	1.32	4.72	1.10	48.65	43.94	0.206	–	S
1476	23 45 28.45	0.18	-54 22 10.03	0.21	17.734	1.066	8.100	0.492	8.72	0.33	6.99	0.28	95.02	11.18	0.209	–	M
1477	23 47 23.94	0.19	-58 45 40.00	0.20	7.384	0.573	6.578	0.436	3.14	0.31	2.33	0.30	107.30	52.97	0.236	–	S
1478	23 45 35.85	0.17	-54 42 27.59	0.18	15.026	0.907	10.206	0.612	6.30	0.25	4.70	0.22	134.45	8.93	0.228	-0.80	S
1479	23 47 31.87	0.49	-59 02 55.01	0.60	3.763	0.394	2.025	0.257	8.42	1.39	5.98	1.07	12.01	25.47	0.215	–	S
1480	23 44 17.93	1.05	-50 56 58.02	0.91	2.010	0.310	1.030	0.211	8.83	2.44	7.17	2.11	91.89	67.75	0.188	–	S
1481	23 45 25.04	0.30	-54 17 48.80	0.39	3.203	0.334	2.341	0.221	6.36	0.84	3.17	0.62	165.92	17.32	0.171	–	S
1482	23 47 00.79	0.19	-58 05 04.36	0.19	5.671	0.449	5.249	0.346	2.77	0.30	1.60	0.29	104.40	39.25	0.187	–	S
1483	23 46 34.43	0.81	-57 07 29.68	0.90	1.868	0.319	1.080	0.214	7.24	2.15	6.23	1.82	1.16	102.73	0.190	–	S
1484	23 46 02.49	0.32	-55 55 19.31	0.38	3.861	0.301	2.128	0.188	8.39	0.84	5.91	0.65	22.04	15.31	0.136	–	S
1485	23 45 25.34	1.04	-54 20 10.19	1.15	2.912	0.298	1.042	0.200	13.06	2.93	8.63	2.07	139.48	32.85	0.180	–	S
1486	23 45 53.86	0.61	-55 32 46.42	0.63	0.925	0.278	0.905	0.167	2.33	1.53	0.00	1.31	34.89	114.44	0.158	–	S
1487	23 47 03.64	0.21	-58 13 49.82	0.24	9.942	0.734	5.684	0.377	6.56	0.46	2.81	0.32	56.64	8.98	0.211	–	M
1488	23 45 38.30	0.55	-54 56 18.06	0.62	1.844	0.364	1.475	0.231	5.29	1.49	2.28	1.16	28.04	40.61	0.207	–	S
1489	23 44 58.86	0.44	-53 13 11.12	0.44	3.895	0.336	2.060	0.213	7.71	1.01	7.56	0.94	61.14	136.35	0.166	–	S
1490	23 44 46.10	0.41	-52 36 42.27	0.43	2.456	0.293	1.734	0.192	5.55	0.97	4.94	0.89	135.84	157.07	0.157	–	S
1491	23 44 05.97	0.53	-50 30 39.22	0.55	2.962	0.502	2.283	0.324	4.55	1.27	4.45	1.18	0.47	177.11	0.283	–	S
1492	23 47 40.16	0.95	-59 30 40.53	0.64	1.768	0.345	1.162	0.226	7.51	2.14	3.66	1.51	85.97	36.82	0.204	–	S
1493	23 46 51.90	0.68	-57 54 18.56	0.57	1.125	0.341	1.097	0.204	0.00	1.58	0.00	1.27	0.00	70.61	0.194	–	S
1494	23 44 28.49	0.29	-51 49 24.75	0.32	3.373	0.349	2.686	0.236	4.87	0.66	3.35	0.60	142.68	40.79	0.175	–	S
1495	23 46 44.76	0.17	-57 44 17.62	0.19	8.956	0.600	7.267	0.452	4.35	0.26	3.14	0.24	4.94	14.89	0.202	–	S
1496	23 45 45.43	0.98	-55 25 58.38	1.24	1.952	0.248	0.803	0.171	10.92	2.89	8.21	2.27	166.87	53.19	0.154	–	S
1497	23 46 48.92	0.80	-57 54 27.52	0.43	6.541	0.546	1.917	0.222	9.69	1.85	3.33	0.94	178.60	16.09	0.196	–	M
1498	23 46 45.04	0.29	-57 47 34.25	0.31	3.641	0.357	2.750	0.240	4.78	0.64	4.15	0.59	6.61	60.00	0.177	–	S
1499	23 43 51.31	0.14	-50 02 19.17	0.15	48.802	2.705	47.245	2.606	1.85	0.04	0.97	0.03	68.10	5.75	0.194	-0.61	S
1500	23 45 14.73	0.56	-54 14 47.26	0.55	1.440	0.248	1.087	0.160	5.22	1.34	3.86	1.19	49.54	69.57	0.140	–	S
1501	23 46 29.71	0.68	-57 19 03.91	1.03	1.874	0.239	0.918	0.160	10.80	2.48	5.19	1.40	14.96	19.51	0.143	–	S
1502	23 46 12.99	0.14	-56 41 56.15	0.15	23.795	1.348	22.888	1.273	2.10	0.07	0.73	0.07	5.03	7.69	0.186	-0.30	S
1503	23 44 52.79	0.64	-53 16 42.27	0.88	2.659	0.251	1.103	0.162	11.61	2.02	7.72	1.45	163.95	26.25	0.140	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1504	23 46 20.56	0.79	-57 00 32.44	1.22	3.038	0.317	1.155	0.212	12.89	2.87	7.45	1.76	163.94	22.98	0.192	–	S
1505	23 43 54.80	0.19	-50 20 42.77	0.23	5.049	0.443	4.717	0.330	0.00	0.42	0.00	0.32	0.00	13.07	0.201	–	S
1506	23 46 20.13	1.96	-57 06 45.15	1.15	8.559	0.656	1.060	0.200	16.18	4.90	6.52	2.08	154.17	24.04	0.191	–	M
1507	23 45 05.60	0.20	-54 03 50.60	0.21	49.689	2.793	23.129	1.292	20.22	0.46	4.65	0.13	130.32	1.42	0.223	-1.02	M
1508	23 44 27.05	1.06	-52 07 22.51	0.80	1.595	0.300	0.955	0.200	8.07	2.47	5.15	1.84	85.01	45.83	0.180	–	S
1509	23 46 35.93	0.72	-57 41 38.43	0.57	2.671	0.323	1.455	0.214	8.63	1.64	5.81	1.30	104.88	35.19	0.184	–	S
1510	23 46 17.39	0.41	-57 00 54.43	0.53	2.956	0.350	1.918	0.230	7.20	1.20	4.28	0.91	168.34	23.37	0.191	–	S
1511	23 45 50.32	0.19	-56 00 19.06	0.22	4.244	0.318	3.442	0.231	4.84	0.37	2.56	0.31	17.80	11.42	0.127	–	S
1512	23 46 51.38	0.20	-58 23 07.63	0.25	56.555	3.227	25.973	1.494	18.03	0.55	3.64	0.16	119.87	1.81	0.438	-1.42	M
1513	23 46 34.67	0.51	-57 53 20.43	0.36	6.184	0.445	2.667	0.256	11.30	1.14	6.89	0.78	74.91	10.99	0.195	–	S
1514	23 46 43.72	1.12	-58 12 41.97	0.85	1.952	0.342	1.054	0.232	8.62	2.59	5.92	2.00	93.33	59.53	0.207	–	S
1515	23 45 03.16	0.88	-54 11 04.92	1.32	1.601	0.254	0.787	0.174	10.87	3.14	5.53	1.91	158.41	30.29	0.157	–	S
1516	23 47 25.11	0.21	-59 40 01.39	0.22	5.424	0.397	4.077	0.279	4.85	0.38	4.05	0.35	15.14	25.56	0.157	–	S
1517	23 44 12.28	0.60	-51 46 06.47	0.75	4.916	0.386	1.822	0.231	11.94	1.68	9.42	1.40	6.17	36.05	0.195	–	S
1518	23 46 44.11	0.16	-58 22 31.05	0.18	48.578	2.820	28.217	1.616	11.55	0.29	2.88	0.12	124.20	1.84	0.451	-1.23	M
1519	23 45 25.56	0.14	-55 20 36.74	0.15	24.059	1.356	21.683	1.206	2.98	0.07	2.27	0.07	163.75	9.78	0.174	-0.67	S
1520	23 44 02.69	0.28	-51 27 19.58	0.18	17.183	1.056	9.320	0.552	15.07	0.58	2.29	0.19	163.71	2.49	0.206	-0.59	M
1521	23 45 03.61	0.85	-54 24 08.64	1.05	2.492	0.295	1.082	0.200	11.28	2.57	7.15	1.79	148.50	31.94	0.177	–	S
1522	23 46 28.56	0.98	-57 51 45.71	0.90	2.321	0.327	1.123	0.223	9.16	2.42	7.09	1.93	48.66	57.72	0.197	–	S
1523	23 45 32.00	0.29	-55 40 54.86	0.36	3.619	0.343	2.515	0.227	6.42	0.77	3.99	0.61	8.65	18.64	0.169	–	S
1524	23 47 25.04	0.53	-59 49 42.24	0.46	2.338	0.315	1.587	0.206	5.96	1.20	4.78	1.03	85.47	89.60	0.175	–	S
1525	23 45 40.11	0.77	-56 03 01.75	0.70	1.796	0.239	0.972	0.160	8.31	1.86	6.29	1.51	52.96	47.67	0.139	–	S
1526	23 44 55.30	0.93	-54 06 17.79	0.85	2.188	0.276	1.041	0.186	10.64	2.42	6.32	1.63	123.92	28.96	0.165	–	S
1527	23 45 17.56	0.18	-55 07 54.96	0.17	15.907	0.967	11.051	0.663	6.69	0.27	3.79	0.20	105.81	3.60	0.250	-0.89	S
1528	23 44 38.30	0.90	-53 19 33.17	0.82	1.524	0.255	0.877	0.171	7.52	2.13	6.33	1.86	70.80	90.18	0.151	–	S
1529	23 44 00.84	0.38	-51 26 43.32	0.54	5.335	0.435	2.701	0.269	11.15	1.29	5.13	0.71	152.64	9.48	0.210	–	S
1530	23 46 05.51	0.84	-57 10 58.31	0.87	1.839	0.245	0.955	0.163	11.04	2.47	4.08	1.27	134.18	16.88	0.146	–	S
1531	23 45 41.90	0.61	-56 16 43.60	0.89	2.002	0.239	0.993	0.159	9.92	2.07	6.04	1.40	5.10	25.01	0.139	–	S
1532	23 44 10.06	0.14	-52 05 23.65	0.15	34.680	1.933	33.050	1.827	2.37	0.05	1.01	0.04	109.82	4.00	0.180	-0.99	S
1533	23 45 56.79	0.32	-56 54 02.37	0.36	4.713	0.400	2.856	0.258	7.33	0.80	5.35	0.66	22.54	20.00	0.190	–	S
1534	23 43 33.50	0.68	-50 04 29.83	1.03	2.424	0.284	1.160	0.189	11.84	2.52	5.51	1.34	22.36	18.55	0.167	–	S
1535	23 43 51.15	0.23	-51 05 37.26	0.25	4.474	0.402	3.798	0.285	4.18	0.48	2.69	0.43	142.78	34.41	0.187	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1536	23 44 57.38	0.40	-54 26 10.84	0.43	3.410	0.344	2.147	0.225	6.65	0.95	5.63	0.86	25.82	51.88	0.178	–	S
1537	23 45 38.64	0.25	-56 16 44.52	0.30	2.583	0.276	2.246	0.189	0.00	0.61	0.00	0.48	0.00	15.87	0.139	–	S
1538	23 45 50.86	0.93	-56 43 52.21	0.90	2.002	0.294	1.040	0.198	9.78	2.51	5.35	1.60	43.00	27.54	0.177	–	S
1539	23 45 58.12	0.38	-57 05 30.86	0.34	3.672	0.318	2.219	0.205	7.87	0.86	4.91	0.66	121.66	16.46	0.153	–	S
1540	23 45 54.23	0.24	-57 00 38.08	0.27	3.748	0.372	3.246	0.258	4.15	0.53	1.58	0.45	6.31	19.95	0.181	–	S
1541	23 43 54.08	0.14	-51 30 20.56	0.15	77.523	4.276	76.127	4.191	1.39	0.02	0.77	0.02	171.10	8.35	0.186	-0.20	S
1542	23 44 37.87	0.34	-53 47 28.26	0.74	10.113	0.642	3.731	0.259	17.39	1.79	0.00	0.42	67.38	5.23	0.159	–	M
1543	23 43 48.28	0.14	-51 14 57.44	0.15	117.298	6.520	63.824	3.529	9.69	0.09	6.03	0.06	9.49	1.46	0.363	-0.95	M
1544	23 45 22.99	0.61	-55 47 29.64	0.56	2.203	0.292	1.389	0.191	8.13	1.58	3.75	1.01	48.23	19.31	0.165	–	S
1545	23 44 55.58	1.00	-54 36 26.09	0.82	1.487	0.290	0.910	0.193	7.38	2.32	5.35	1.90	82.57	68.45	0.173	–	S
1546	23 47 02.43	0.36	-59 31 49.07	0.33	4.118	0.382	2.685	0.251	6.64	0.79	4.72	0.67	56.81	25.22	0.189	–	S
1547	23 44 02.36	0.19	-52 02 37.04	0.21	7.353	0.490	5.417	0.346	5.47	0.33	4.27	0.29	4.16	20.91	0.166	–	S
1548	23 44 29.16	0.88	-53 27 05.31	0.68	4.071	0.306	1.323	0.178	14.12	2.17	9.28	1.39	63.61	17.49	0.156	–	S
1549	23 45 55.60	0.24	-57 11 04.96	0.27	3.307	0.307	2.732	0.214	4.70	0.53	2.25	0.44	156.12	17.85	0.146	–	S
1550	23 46 49.27	0.96	-59 08 18.26	1.00	3.162	0.595	1.798	0.401	8.14	2.59	5.45	1.94	139.71	54.96	0.360	–	S
1551	23 46 29.47	0.20	-58 28 24.93	0.21	6.856	0.582	6.369	0.438	2.59	0.34	1.68	0.33	141.06	55.92	0.258	–	S
1552	23 46 46.17	0.29	-59 04 29.41	0.33	17.600	1.112	7.480	0.575	10.25	0.71	7.94	0.58	158.24	11.77	0.373	–	S
1553	23 44 07.18	0.29	-52 23 46.88	0.33	2.785	0.294	2.217	0.198	5.09	0.69	3.04	0.59	148.74	29.84	0.149	–	S
1554	23 44 59.26	1.38	-54 59 19.02	0.64	82.848	4.644	8.201	0.631	38.75	3.41	12.08	1.01	157.95	6.53	0.442	–	M
1555	23 46 59.72	0.14	-59 38 03.90	0.15	17.985	1.020	16.702	0.930	2.49	0.07	1.82	0.07	102.30	106.77	0.144	-0.51	S
1556	23 46 54.75	0.18	-59 29 26.91	0.18	9.638	0.634	7.631	0.472	4.33	0.25	3.67	0.24	108.56	46.45	0.206	–	S
1557	23 44 46.05	0.73	-54 26 36.34	1.53	2.519	0.285	0.976	0.193	14.34	3.54	6.18	1.69	178.55	18.67	0.178	–	S
1558	23 44 02.51	0.27	-52 20 15.68	0.31	5.057	0.403	3.274	0.264	6.92	0.64	5.10	0.55	162.28	24.64	0.179	–	S
1559	23 46 54.62	0.18	-59 32 55.71	0.18	6.394	0.462	5.763	0.364	2.97	0.26	2.18	0.25	108.53	47.95	0.174	–	S
1560	23 46 48.41	1.07	-59 20 40.79	0.55	7.818	0.724	3.059	0.465	13.62	2.39	6.27	1.31	90.20	14.50	0.413	–	S
1561	23 43 33.27	0.38	-50 51 21.13	1.60	6.564	0.602	1.802	0.246	0.00	3.76	0.00	0.79	0.00	11.00	0.225	–	M
1562	23 44 51.76	0.79	-54 53 38.00	2.31	11.318	0.774	1.256	0.278	17.17	5.51	3.29	1.59	77.05	18.80	0.269	–	M
1563	23 44 00.55	0.15	-52 20 57.38	0.16	13.349	0.843	10.682	0.614	4.65	0.17	1.10	0.13	55.17	5.47	0.178	-0.41	M
1564	23 43 35.68	0.22	-50 59 07.73	0.21	4.637	0.393	4.147	0.290	3.87	0.41	1.12	0.34	100.35	16.68	0.174	–	S
1565	23 45 33.32	0.14	-56 39 26.49	0.15	44.567	2.472	43.170	2.382	1.88	0.04	0.70	0.03	179.91	4.11	0.185	-0.34	S
1566	23 43 43.97	0.47	-51 29 46.40	0.49	3.264	0.346	1.981	0.226	8.07	1.22	5.09	0.91	133.21	24.50	0.184	–	S
1567	23 45 54.54	0.71	-57 29 37.97	0.97	1.814	0.225	0.874	0.151	10.38	2.34	5.90	1.48	18.52	23.50	0.134	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
1568	23 43 22.74	0.20	-50 19 03.64	0.22	6.999	0.489	5.052	0.338	5.52	0.37	4.74	0.37	177.26	149.46	0.182	-	S
1569	23 44 57.44	0.18	-55 10 10.07	0.18	6.821	0.498	6.340	0.399	2.92	0.26	1.22	0.24	118.23	22.52	0.190	-	S
1570	23 44 40.25	1.06	-54 27 42.49	0.55	5.194	0.377	1.695	0.211	17.83	2.61	6.04	0.94	67.37	7.25	0.190	-	S
1571	23 44 19.39	0.41	-53 27 17.30	0.43	3.861	0.329	2.085	0.208	8.66	1.02	6.27	0.82	132.89	24.42	0.160	-	S
1572	23 43 35.47	0.59	-51 09 41.07	0.51	3.130	0.390	1.953	0.256	7.55	1.41	5.11	1.09	107.32	32.47	0.216	-	S
1573	23 43 20.84	0.42	-50 23 58.55	0.43	4.015	0.355	2.233	0.227	8.22	1.02	6.53	0.88	123.67	35.51	0.176	-	S
1574	23 46 03.64	0.31	-58 04 36.80	0.50	25.250	1.472	5.750	0.412	14.67	1.13	8.19	0.65	80.74	8.82	0.264	-	M
1575	23 45 29.33	0.47	-56 42 38.92	0.54	2.275	0.326	1.615	0.212	5.99	1.23	4.05	1.03	158.26	43.22	0.181	-	S
1576	23 44 52.18	0.30	-55 08 10.83	0.31	2.900	0.375	2.677	0.249	2.63	0.65	1.95	0.60	167.03	137.26	0.197	-	S
1577	23 44 00.20	0.40	-52 38 54.99	0.37	2.998	0.310	2.011	0.204	6.45	0.92	4.84	0.77	63.51	31.79	0.160	-	S
1578	23 43 21.87	1.89	-50 35 30.47	2.12	15.993	0.919	1.547	0.258	35.53	6.07	17.45	2.88	135.02	14.49	0.326	-	S
1579	23 43 30.25	0.43	-51 06 56.51	0.44	1.414	0.303	1.433	0.186	0.00	1.02	0.00	0.90	0.00	152.30	0.169	-	S
1580	23 45 41.02	0.33	-57 17 13.37	0.57	2.679	0.280	1.653	0.182	8.96	1.30	2.89	0.71	174.93	9.91	0.149	-	S
1581	23 44 13.83	0.26	-53 32 24.23	0.32	3.801	0.336	2.735	0.226	6.49	0.68	3.45	0.51	156.16	14.40	0.159	-	S
1582	23 43 22.56	0.63	-50 48 48.38	0.84	8.489	0.583	2.800	0.309	18.56	2.31	6.06	0.82	141.78	6.23	0.269	-	S
1583	23 46 21.04	0.33	-58 54 43.13	0.28	3.720	0.423	3.084	0.283	4.56	0.68	2.40	0.59	91.50	30.29	0.218	-	S
1584	23 44 27.88	0.88	-54 17 17.85	0.69	1.296	0.246	0.853	0.161	7.00	2.03	4.47	1.59	78.93	49.69	0.144	-	S
1585	23 44 48.67	0.45	-55 17 39.87	0.39	7.283	0.485	2.869	0.259	11.36	1.04	8.47	0.79	62.24	14.66	0.191	-	S
1586	23 46 41.99	0.45	-59 41 20.84	0.64	4.680	0.330	1.693	0.182	13.05	1.51	7.78	0.95	159.96	10.33	0.149	-	S
1587	23 45 13.85	0.39	-56 26 49.04	0.61	4.249	0.364	2.068	0.228	10.63	1.40	5.59	0.84	7.90	11.41	0.185	-	S
1588	23 44 00.94	0.58	-53 07 52.25	0.61	5.207	0.375	1.960	0.211	14.50	1.73	6.74	0.87	133.41	8.54	0.174	-	S
1589	23 45 25.29	0.14	-56 58 43.66	0.15	34.266	1.912	34.100	1.885	0.00	0.04	0.00	0.04	0.00	101.08	0.188	-0.36	S
1590	23 46 22.37	0.18	-59 06 39.05	0.20	11.863	0.798	8.992	0.573	5.21	0.31	3.45	0.27	3.98	9.55	0.274	-	S
1591	23 45 37.90	0.35	-57 30 50.33	0.45	3.424	0.292	1.880	0.185	8.55	1.01	5.65	0.75	179.57	15.81	0.142	-	S
1592	23 44 07.16	0.17	-53 32 29.18	0.17	8.508	0.549	7.321	0.439	3.41	0.21	3.09	0.21	113.00	166.64	0.168	-1.03	S
1593	23 44 14.48	0.72	-53 54 53.93	0.74	1.178	0.257	0.877	0.165	4.86	1.72	4.57	1.64	28.00	177.08	0.149	-	S
1594	23 44 35.07	0.18	-54 55 50.87	0.18	9.526	0.698	8.804	0.556	2.96	0.27	1.37	0.25	74.44	22.66	0.269	-	S
1595	23 43 06.61	1.72	-50 16 23.39	2.02	4.682	0.314	0.814	0.160	26.55	5.79	11.54	2.43	136.35	16.50	0.173	-	S
1596	23 43 15.97	0.18	-50 51 59.89	0.19	8.790	0.589	7.086	0.442	4.71	0.29	3.33	0.25	143.62	18.86	0.199	-	S
1597	23 45 03.75	1.37	-56 15 06.44	1.90	3.640	0.258	0.695	0.143	21.11	4.72	12.31	2.76	152.43	23.13	0.148	-	S
1598	23 43 04.88	0.24	-50 19 59.87	0.32	17.643	1.101	10.670	0.633	14.87	0.76	4.92	0.30	118.51	3.88	0.238	-0.52	M
1599	23 44 12.13	0.27	-54 00 38.51	0.32	2.650	0.302	2.280	0.203	4.53	0.68	1.42	0.55	161.02	22.46	0.155	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1600	23 44 22.01	0.28	-54 31 52.47	0.50	8.542	0.642	3.315	0.275	11.86	1.15	3.49	0.50	103.13	7.50	0.205	–	M
1601	23 46 31.17	1.02	-59 42 18.15	1.50	2.726	0.255	0.863	0.167	16.63	3.85	6.92	1.72	150.18	15.71	0.159	–	S
1602	23 43 57.17	1.84	-53 22 05.00	1.71	5.499	0.338	0.746	0.140	25.60	4.99	16.04	3.13	125.80	23.14	0.158	–	S
1603	23 45 33.08	1.28	-57 40 19.35	0.80	10.151	0.650	1.660	0.209	18.49	3.35	5.82	1.11	24.88	11.75	0.188	–	M
1604	23 44 51.28	0.57	-55 54 30.66	1.09	2.748	0.247	1.084	0.156	15.04	2.64	5.09	1.07	159.16	10.12	0.141	–	S
1605	23 44 32.81	0.17	-55 06 21.06	0.17	14.259	0.892	11.387	0.679	4.15	0.21	3.87	0.21	45.42	47.07	0.251	-0.01	S
1606	23 45 03.05	0.16	-56 34 04.35	0.23	101.981	5.707	30.849	1.733	22.14	0.40	10.63	0.19	77.67	1.68	0.352	-0.67	M
1607	23 45 50.15	0.59	-58 20 33.21	0.67	4.674	0.625	2.833	0.411	8.76	1.73	3.65	1.06	142.36	18.04	0.358	–	S
1608	23 45 19.27	0.33	-57 10 40.44	0.41	3.386	0.334	2.224	0.219	6.99	0.91	4.29	0.70	167.48	18.82	0.170	–	S
1609	23 43 27.71	0.14	-51 59 12.02	0.15	40.652	2.261	37.867	2.092	2.54	0.05	1.85	0.04	16.35	7.68	0.194	-0.69	S
1610	23 43 03.80	0.15	-50 36 27.28	0.16	15.451	0.921	13.966	0.797	3.33	0.14	1.98	0.12	153.58	12.40	0.208	-0.78	S
1611	23 45 40.30	1.05	-58 04 13.76	0.98	2.554	0.356	1.169	0.245	9.42	2.58	7.72	2.14	123.38	93.59	0.218	–	S
1612	23 43 17.08	0.21	-51 27 27.35	0.21	6.803	0.495	5.293	0.354	5.88	0.42	2.45	0.30	114.76	7.46	0.193	–	S
1613	23 43 44.66	0.87	-52 59 05.17	0.84	2.352	0.242	0.984	0.160	11.25	2.27	7.86	1.62	47.95	29.42	0.140	–	S
1614	23 44 54.52	0.47	-56 24 57.34	0.54	3.441	0.345	1.878	0.224	7.93	1.22	6.53	1.06	2.18	43.57	0.183	–	S
1615	23 43 49.21	0.68	-53 22 32.71	0.60	1.439	0.281	1.085	0.180	5.50	1.57	3.63	1.35	101.32	64.96	0.161	–	S
1616	23 45 14.42	0.44	-57 16 54.36	0.64	1.642	0.279	1.244	0.179	6.27	1.46	1.89	1.00	176.98	24.03	0.158	–	S
1617	23 44 58.03	0.74	-56 41 05.47	0.82	1.425	0.306	1.004	0.198	6.12	1.99	4.06	1.61	150.41	67.96	0.179	–	S
1618	23 45 21.09	0.15	-57 38 54.93	0.16	12.990	0.776	11.919	0.680	2.88	0.13	1.67	0.12	12.15	11.09	0.176	-0.16	S
1619	23 44 41.57	0.87	-56 03 05.95	1.17	1.968	0.214	0.798	0.143	13.37	3.02	6.00	1.50	27.38	17.01	0.130	–	S
1620	23 43 26.27	0.42	-52 23 52.68	0.39	1.417	0.243	1.301	0.154	3.37	0.94	0.85	0.84	100.61	56.15	0.134	–	S
1621	23 42 45.79	0.21	-50 21 45.37	0.23	8.344	0.618	6.421	0.438	5.75	0.44	3.00	0.33	39.98	9.89	0.247	–	S
1622	23 46 04.63	0.95	-59 25 12.14	0.93	1.834	0.309	0.988	0.210	7.32	2.20	7.13	2.17	154.23	86.71	0.187	–	S
1623	23 46 16.25	0.15	-59 50 40.18	0.17	12.762	0.752	9.649	0.557	5.53	0.17	2.99	0.14	2.80	1.83	0.161	-0.59	S
1624	23 43 51.51	0.25	-53 52 11.05	0.36	5.730	0.413	3.223	0.254	9.20	0.76	4.94	0.49	177.74	7.68	0.169	–	S
1625	23 42 43.95	0.18	-50 08 57.19	0.19	5.157	0.381	4.787	0.303	2.91	0.28	1.61	0.26	164.86	34.47	0.147	–	S
1626	23 43 53.63	0.16	-54 03 07.88	0.17	19.390	1.143	11.508	0.667	5.69	0.20	2.96	0.16	47.37	5.84	0.211	-1.04	M
1627	23 43 11.39	0.60	-51 52 15.01	1.01	18.167	1.163	2.568	0.273	23.96	2.62	7.04	0.78	114.25	7.33	0.234	–	M
1628	23 44 45.56	0.15	-56 27 29.86	0.16	12.642	0.751	10.734	0.615	3.58	0.14	3.08	0.14	12.24	21.52	0.166	-0.39	S
1629	23 45 04.99	1.73	-57 16 09.58	0.47	4.389	0.411	1.127	0.175	0.00	4.09	0.00	0.95	0.00	14.52	0.164	–	M
1630	23 44 27.47	0.18	-55 40 30.69	0.19	6.863	0.478	5.810	0.366	3.89	0.28	2.81	0.26	19.31	21.60	0.172	–	S
1631	23 43 03.38	0.35	-51 22 01.39	0.37	3.097	0.321	2.205	0.213	5.36	0.79	5.05	0.75	49.55	111.12	0.164	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
1632	23 46 17.08	0.39	-59 58 30.95	0.41	3.757	0.348	2.210	0.225	7.67	0.96	5.32	0.78	142.19	22.33	0.175	–	S
1633	23 45 58.37	0.16	-59 20 32.69	0.17	12.558	0.797	11.481	0.674	2.48	0.17	2.30	0.16	144.38	118.98	0.232	-0.30	S
1634	23 43 51.33	0.15	-54 05 13.92	0.16	18.454	1.072	16.319	0.921	3.99	0.12	1.27	0.10	16.43	2.65	0.202	-0.56	S
1635	23 42 57.33	0.17	-51 10 52.10	0.18	7.907	0.546	7.175	0.441	3.06	0.24	2.15	0.23	137.67	37.05	0.192	–	S
1636	23 43 30.21	0.96	-53 09 57.13	0.83	2.319	0.348	1.218	0.236	8.46	2.23	6.91	1.92	83.92	72.22	0.208	–	S
1637	23 45 32.08	0.39	-58 37 19.49	0.25	22.711	1.451	8.193	0.557	12.45	0.88	5.33	0.42	163.90	5.95	0.327	–	M
1638	23 42 45.65	0.39	-50 46 50.70	0.56	6.502	0.499	2.986	0.299	11.93	1.34	6.13	0.77	153.56	10.50	0.234	–	S
1639	23 44 47.89	0.37	-56 51 32.20	0.54	2.637	0.317	1.788	0.207	7.61	1.23	2.79	0.78	165.76	14.57	0.173	–	S
1640	23 43 27.80	0.76	-53 09 19.55	1.14	7.230	0.468	1.624	0.224	18.17	2.62	12.26	1.78	176.24	19.57	0.209	–	S
1641	23 44 49.96	0.23	-57 01 12.73	0.26	4.240	0.367	3.371	0.256	5.13	0.51	2.66	0.42	154.14	15.45	0.168	–	S
1642	23 44 54.13	0.59	-57 11 40.17	0.79	1.382	0.271	0.988	0.175	6.44	1.84	3.22	1.34	3.12	37.44	0.157	–	S
1643	23 42 43.33	0.20	-50 39 57.15	0.24	9.086	0.601	5.825	0.389	7.69	0.46	4.58	0.33	15.23	7.44	0.206	–	S
1644	23 43 48.08	0.85	-54 16 03.13	0.90	1.625	0.278	0.940	0.187	7.77	2.18	5.95	1.86	139.54	79.06	0.166	–	S
1645	23 42 34.10	1.05	-50 08 16.16	1.12	2.473	0.243	0.858	0.162	11.61	2.62	11.07	2.44	146.12	177.43	0.145	–	S
1646	23 43 56.54	0.18	-54 43 59.69	0.18	9.623	0.641	8.030	0.494	3.96	0.25	3.13	0.23	67.12	24.93	0.213	–	S
1647	23 43 13.04	0.57	-52 31 28.92	0.62	2.559	0.296	1.439	0.195	8.27	1.47	6.10	1.23	138.18	43.39	0.165	–	S
1648	23 43 55.62	1.04	-54 51 00.16	0.47	24.278	1.458	3.966	0.326	24.50	2.51	8.25	0.84	162.15	7.38	0.243	–	M
1649	23 43 25.62	1.52	-53 23 12.62	1.60	3.349	0.256	0.739	0.154	18.65	4.37	12.08	2.73	39.92	27.34	0.153	–	S
1650	23 42 53.07	0.33	-51 34 35.77	0.39	3.838	0.361	2.512	0.237	6.67	0.81	5.22	0.74	3.80	42.49	0.179	–	S
1651	23 42 40.01	0.69	-50 47 09.00	0.75	2.042	0.406	1.475	0.262	6.56	1.85	3.49	1.44	134.69	45.67	0.235	–	S
1652	23 44 22.84	0.73	-56 14 50.04	0.78	1.243	0.237	0.826	0.155	6.00	1.82	5.26	1.68	167.80	157.68	0.138	–	S
1653	23 43 43.94	0.20	-54 27 04.79	0.22	6.558	0.498	5.276	0.360	4.84	0.39	2.95	0.33	166.75	16.37	0.203	–	S
1654	23 43 45.68	0.16	-54 34 04.93	0.17	7.903	0.554	7.993	0.482	0.00	0.20	0.00	0.20	0.00	86.44	0.198	-0.06	S
1655	23 42 36.48	0.36	-50 44 00.29	0.35	2.612	0.408	2.479	0.262	0.00	0.80	0.00	0.73	0.00	50.85	0.222	–	S
1656	23 43 06.55	0.41	-52 31 17.27	0.52	2.002	0.294	1.539	0.191	5.63	1.14	3.15	0.93	176.97	37.64	0.163	–	S
1657	23 43 55.73	0.61	-55 10 40.91	0.80	1.655	0.296	1.117	0.193	7.07	1.85	3.86	1.37	161.64	37.79	0.172	–	S
1658	23 42 44.08	0.53	-51 24 28.44	0.62	1.437	0.292	1.184	0.184	4.55	1.37	2.98	1.26	167.66	94.06	0.166	–	S
1659	23 44 29.45	0.15	-56 52 46.13	0.16	16.465	0.963	15.633	0.881	2.66	0.10	0.00	0.10	163.22	6.13	0.190	-0.17	S
1660	23 43 21.17	0.15	-53 38 26.19	0.16	13.654	0.801	12.816	0.724	2.11	0.11	2.01	0.11	105.64	177.26	0.163	-0.46	S
1661	23 44 47.15	0.88	-57 39 48.38	1.09	4.495	0.356	1.307	0.215	13.76	2.55	10.90	2.02	166.81	36.83	0.196	–	S
1662	23 44 40.10	0.18	-57 23 18.34	0.19	6.221	0.442	5.379	0.341	3.63	0.28	2.50	0.26	179.54	22.11	0.164	–	S
1663	23 45 48.23	0.92	-59 59 21.54	0.88	1.644	0.310	1.020	0.203	9.10	2.57	2.55	1.40	132.18	22.37	0.186	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1664	23 42 34.30	0.77	-51 05 59.84	1.29	1.987	0.269	0.926	0.184	11.75	2.97	6.01	1.77	167.49	27.34	0.165	–	S
1665	23 44 44.41	0.19	-57 40 22.03	0.18	22.120	1.282	10.340	0.604	9.61	0.31	7.48	0.24	157.03	7.33	0.205	-0.81	M
1666	23 43 22.35	0.66	-53 51 27.40	0.85	2.001	0.293	1.140	0.195	8.23	1.94	5.76	1.55	1.21	46.30	0.171	–	S
1667	23 45 40.05	0.44	-59 46 20.78	0.41	1.229	0.271	1.242	0.166	0.00	1.01	0.00	0.88	0.00	115.54	0.151	–	S
1668	23 42 43.77	0.49	-51 44 23.34	0.54	4.012	0.463	2.458	0.304	7.12	1.19	5.89	1.13	152.94	82.14	0.252	–	S
1669	23 43 04.71	0.18	-52 57 15.35	0.19	6.608	0.452	5.458	0.343	4.15	0.28	3.28	0.26	157.24	33.15	0.158	–	S
1670	23 44 06.59	0.52	-56 02 33.66	0.63	3.178	0.311	1.578	0.202	8.97	1.43	7.03	1.18	178.87	36.35	0.168	–	S
1671	23 43 59.45	0.54	-55 42 29.51	0.58	1.562	0.327	1.321	0.205	4.49	1.39	1.89	1.14	30.39	51.76	0.185	–	S
1672	23 44 09.62	0.30	-56 14 57.67	0.33	2.203	0.285	2.000	0.189	4.46	0.75	0.00	0.54	30.49	15.57	0.151	–	S
1673	23 45 16.96	1.42	-59 00 42.27	1.70	25.117	1.456	2.325	0.290	19.21	5.06	1.58	1.15	125.96	13.51	0.260	–	M
1674	23 42 47.96	0.19	-52 06 06.94	0.19	10.497	0.675	7.686	0.478	5.62	0.30	4.18	0.25	106.54	12.55	0.210	–	S
1675	23 43 00.45	0.23	-52 46 15.50	0.25	3.920	0.391	3.622	0.277	2.92	0.46	1.61	0.44	173.99	53.34	0.190	–	S
1676	23 44 36.07	0.30	-57 29 04.72	0.46	3.616	0.325	2.187	0.209	8.72	1.02	3.70	0.62	168.08	9.31	0.161	–	S
1677	23 45 38.15	0.38	-59 53 04.17	0.41	3.055	0.361	2.181	0.238	5.30	0.93	4.51	0.81	171.55	62.14	0.193	–	S
1678	23 43 14.27	0.64	-53 39 25.76	0.76	1.234	0.281	0.970	0.178	5.12	1.72	3.21	1.48	165.46	79.71	0.162	–	S
1679	23 45 05.00	0.21	-58 50 56.36	0.32	378.046	20.861	214.419	11.804	51.79	0.77	1.56	0.06	57.58	0.62	0.506	-0.74	M
1680	23 43 10.36	2.03	-53 32 07.08	1.63	4.619	0.308	0.778	0.156	24.63	5.53	12.52	2.62	53.23	18.30	0.169	–	S
1681	23 45 25.71	0.51	-59 31 25.54	0.56	2.418	0.275	1.398	0.181	7.29	1.30	5.99	1.11	160.64	49.35	0.151	–	S
1682	23 42 24.08	0.36	-50 53 58.21	0.42	3.578	0.410	2.632	0.270	6.34	0.95	3.40	0.73	146.27	24.27	0.216	–	S
1683	23 43 08.23	1.03	-53 32 05.98	0.83	1.898	0.281	0.989	0.189	10.27	2.63	5.19	1.60	117.03	26.86	0.169	–	S
1684	23 45 33.94	1.19	-59 55 29.29	0.54	2.767	0.488	0.966	0.208	0.00	2.97	0.00	0.68	0.00	14.17	0.201	–	M
1685	23 44 03.03	1.27	-56 17 28.51	0.96	2.366	0.251	0.853	0.170	12.74	3.04	8.52	2.11	64.41	33.21	0.154	–	S
1686	23 44 30.30	0.51	-57 30 38.17	0.58	6.136	0.516	1.910	0.207	8.94	1.33	7.28	1.13	69.17	46.51	0.178	–	M
1687	23 43 16.30	0.29	-54 02 59.55	0.33	3.023	0.307	2.308	0.206	5.28	0.69	3.62	0.61	164.05	33.75	0.154	–	S
1688	23 44 28.66	0.82	-57 27 19.91	1.26	4.573	0.317	1.091	0.170	17.48	2.97	11.04	1.86	167.49	18.39	0.161	–	S
1689	23 44 39.70	0.68	-57 55 16.66	0.71	5.493	0.544	2.442	0.355	9.69	1.75	7.87	1.44	31.03	41.85	0.304	–	S
1690	23 45 27.29	0.14	-59 53 36.30	0.15	30.723	1.730	30.990	1.718	0.00	0.05	0.00	0.05	0.00	97.91	0.213	0.23	S
1691	23 44 28.16	0.36	-57 31 33.05	0.40	1.693	0.329	1.725	0.204	0.00	0.89	0.00	0.75	0.00	47.12	0.182	–	S
1692	23 43 07.27	0.18	-53 48 50.15	0.17	38.059	2.154	16.930	0.968	12.26	0.27	8.54	0.19	22.77	3.59	0.263	-0.79	M
1693	23 42 24.72	0.81	-51 24 13.57	0.86	12.451	0.712	1.869	0.199	20.01	1.99	18.99	1.87	3.95	177.46	0.192	–	S
1694	23 43 20.51	0.44	-54 34 31.73	0.47	1.980	0.365	1.761	0.230	3.25	1.06	2.34	0.96	19.74	130.47	0.204	–	S
1695	23 43 14.86	0.73	-54 26 02.82	0.38	64.552	3.589	15.623	0.907	27.56	1.77	10.26	0.62	16.14	4.89	0.292	-0.77	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1696	23 42 48.82	0.86	-53 14 57.22	3.52	40.887	2.322	3.002	0.312	58.12	8.43	8.75	1.16	76.19	8.39	0.265	–	M
1697	23 43 15.71	0.18	-54 28 49.71	0.18	10.870	0.775	9.744	0.612	2.99	0.26	2.44	0.25	86.51	54.96	0.288	–	S
1698	23 45 04.99	0.30	-59 23 19.04	0.88	36.046	2.055	10.039	0.593	25.59	2.06	6.82	0.58	94.51	5.23	0.216	-0.24	M
1699	23 42 36.95	0.46	-52 23 25.76	0.50	1.993	0.290	1.513	0.188	6.15	1.21	2.74	0.90	137.32	27.31	0.161	–	S
1700	23 44 43.21	0.49	-58 29 16.60	0.29	16.858	1.231	6.283	0.498	10.45	1.10	4.42	0.57	170.10	9.40	0.359	–	M
1701	23 43 08.95	0.14	-54 12 37.90	0.15	18.695	1.076	17.738	0.993	2.66	0.09	0.00	0.08	56.86	5.36	0.183	-0.60	S
1702	23 42 24.97	0.15	-51 44 58.39	0.16	102.556	5.721	41.769	2.329	10.69	0.14	6.38	0.10	14.90	1.93	0.382	-1.08	M
1703	23 42 25.27	0.20	-51 43 53.24	0.21	10.344	0.838	9.304	0.630	3.67	0.37	1.47	0.32	131.64	20.10	0.359	–	S
1704	23 43 36.56	1.11	-55 36 23.60	0.90	4.819	0.357	1.285	0.206	14.84	2.57	11.70	2.09	97.20	39.76	0.189	–	S
1705	23 42 31.76	0.46	-52 10 15.69	0.56	4.590	0.397	2.244	0.250	9.53	1.27	7.16	1.01	16.97	28.39	0.201	–	S
1706	23 44 59.36	0.40	-59 10 48.64	0.47	3.150	0.351	2.038	0.231	6.94	1.08	4.48	0.85	157.88	24.81	0.188	–	S
1707	23 44 33.22	0.63	-58 11 17.44	0.98	16.163	1.315	4.209	0.518	11.66	2.49	3.15	1.06	61.11	15.70	0.464	–	M
1708	23 44 53.80	0.14	-59 03 31.85	0.15	51.813	2.900	43.712	2.416	5.03	0.06	2.03	0.05	126.27	1.88	0.244	-0.23	M
1709	23 42 56.39	0.80	-53 41 20.21	0.76	0.965	0.268	0.795	0.167	4.29	1.93	3.12	1.69	106.45	153.71	0.155	–	S
1710	23 44 14.40	0.20	-57 28 11.83	0.22	3.795	0.330	3.532	0.246	0.00	0.38	0.00	0.32	0.00	15.76	0.148	–	S
1711	23 44 59.13	0.20	-59 18 46.03	0.24	8.110	0.538	5.150	0.347	7.21	0.43	4.48	0.33	160.96	6.74	0.186	–	S
1712	23 42 49.60	0.23	-53 22 55.06	0.24	4.115	0.380	3.625	0.271	3.03	0.44	2.91	0.43	82.33	177.37	0.179	–	S
1713	23 42 57.30	1.03	-53 49 13.13	1.01	6.273	0.480	1.791	0.283	15.91	2.88	9.84	1.73	44.25	19.14	0.260	–	S
1714	23 43 14.99	0.16	-54 44 37.73	0.17	8.705	0.571	8.041	0.479	2.47	0.19	2.11	0.19	41.21	66.38	0.181	-0.36	S
1715	23 43 45.74	0.14	-56 15 49.08	0.15	18.760	1.073	17.055	0.954	2.82	0.09	2.16	0.08	9.20	13.54	0.172	-0.19	S
1716	23 43 49.31	0.21	-56 25 23.47	0.21	6.885	0.501	5.239	0.354	5.60	0.40	3.05	0.32	41.75	9.56	0.195	–	S
1717	23 43 58.18	0.58	-56 48 43.31	0.72	2.350	0.293	1.306	0.194	8.49	1.69	5.61	1.27	159.37	31.46	0.167	–	S
1718	23 44 17.16	0.19	-57 40 55.46	0.19	13.920	0.834	8.123	0.500	8.43	0.33	4.85	0.24	124.10	3.11	0.208	–	S
1719	23 41 54.26	1.01	-50 04 28.80	0.77	1.116	0.256	0.778	0.166	7.01	2.42	3.50	1.72	98.33	43.62	0.151	–	S
1720	23 44 50.84	0.19	-59 05 02.39	0.19	37.060	2.126	25.773	1.440	16.19	0.40	1.24	0.10	42.30	1.29	0.254	-0.17	M
1721	23 44 18.23	0.22	-57 45 19.50	0.24	4.836	0.421	4.044	0.299	4.29	0.45	2.45	0.40	176.44	20.60	0.192	–	S
1722	23 42 24.17	0.15	-52 08 47.05	0.16	15.901	0.957	15.205	0.867	2.30	0.13	1.01	0.12	148.79	18.71	0.225	-0.75	S
1723	23 43 30.23	0.89	-55 43 37.91	0.75	1.514	0.365	1.119	0.233	6.10	2.12	3.19	1.63	113.40	56.16	0.213	–	S
1724	23 43 53.88	1.06	-56 51 17.09	0.77	3.369	0.324	1.258	0.213	12.63	2.49	8.05	1.72	104.87	27.01	0.189	–	S
1725	23 43 01.46	0.29	-54 20 53.10	0.27	4.401	0.422	3.471	0.288	4.88	0.59	3.37	0.53	109.77	32.91	0.205	–	S
1726	23 44 31.89	0.14	-58 34 07.60	0.16	79.466	4.478	52.268	2.902	7.89	0.11	0.00	0.06	64.84	1.16	0.400	-0.78	M
1727	23 41 55.15	0.68	-50 30 31.29	0.48	3.477	0.330	1.726	0.212	10.62	1.68	5.88	0.98	100.17	15.24	0.177	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
1728	23 43 35.58	0.14	-56 06 59.63	0.15	22.000	1.248	21.237	1.182	1.94	0.07	0.86	0.07	5.11	11.60	0.176	0.09	S
1729	23 43 11.05	0.27	-54 57 47.17	0.30	5.005	0.391	3.219	0.255	7.04	0.64	4.79	0.50	27.71	15.10	0.171	-	S
1730	23 41 56.27	0.47	-50 42 36.23	0.49	2.687	0.320	1.784	0.210	7.15	1.20	4.50	0.93	130.04	29.55	0.174	-	S
1731	23 41 57.04	0.14	-50 51 04.19	0.15	81.174	4.509	60.244	3.337	5.93	0.07	3.49	0.05	74.46	179.59	0.377	-1.42	S
1732	23 42 18.52	0.21	-52 10 35.80	0.24	5.709	0.525	5.285	0.383	0.00	0.44	0.00	0.36	0.00	17.33	0.245	-	S
1733	23 43 20.74	0.47	-55 35 26.41	0.51	5.920	0.441	2.494	0.259	11.08	1.25	7.68	0.93	139.93	17.77	0.204	-	S
1734	23 43 05.65	0.17	-54 50 35.66	0.18	7.405	0.515	6.619	0.410	3.13	0.25	2.33	0.24	42.96	33.23	0.184	-	S
1735	23 41 54.00	0.15	-50 41 54.76	0.16	11.719	0.713	10.691	0.615	2.72	0.15	2.38	0.14	127.15	154.65	0.178	-0.51	S
1736	23 44 58.65	1.04	-59 45 57.80	0.73	1.686	0.294	0.981	0.196	8.90	2.45	4.22	1.57	63.69	29.75	0.176	-	S
1737	23 43 24.38	0.19	-55 51 36.43	0.21	11.268	0.925	10.518	0.706	2.76	0.33	1.21	0.31	0.05	31.67	0.399	-	S
1738	23 42 01.00	1.34	-51 15 32.49	1.11	2.255	0.284	0.900	0.196	12.64	3.46	7.61	2.18	116.16	32.42	0.179	-	S
1739	23 43 35.23	0.62	-56 29 08.74	1.73	0.791	0.457	0.872	0.236	0.00	4.16	0.00	0.96	0.00	16.28	0.261	-	S
1740	23 41 45.06	1.25	-50 22 02.09	0.50	21.087	1.174	2.354	0.207	38.04	3.16	13.17	0.91	77.16	3.41	0.214	-	S
1741	23 41 55.24	0.30	-50 56 06.14	0.33	4.005	0.428	3.231	0.288	5.03	0.70	2.91	0.59	140.17	29.92	0.217	-	S
1742	23 43 53.07	0.14	-57 16 27.07	0.15	51.104	2.823	49.961	2.752	1.22	0.02	1.16	0.02	155.50	98.04	0.151	-0.10	S
1743	23 42 49.41	0.74	-54 10 45.67	0.90	1.762	0.322	1.110	0.213	7.75	2.16	4.50	1.60	150.61	42.42	0.190	-	S
1744	23 41 59.73	0.25	-51 17 33.79	0.31	4.089	0.368	3.080	0.250	5.85	0.63	3.46	0.50	170.45	20.61	0.174	-	S
1745	23 43 23.83	0.82	-56 03 41.68	0.99	47.192	2.766	15.629	0.909	45.30	2.97	1.97	0.28	47.82	2.82	0.296	-1.11	M
1746	23 43 37.58	0.37	-56 38 58.05	0.34	4.157	0.368	2.575	0.239	7.16	0.81	5.26	0.70	113.40	28.00	0.179	-	S
1747	23 42 09.89	1.46	-52 11 06.20	1.53	48.907	2.747	13.514	0.798	40.29	4.66	15.84	1.69	44.26	9.62	0.291	0.12	M
1748	23 42 03.28	0.66	-51 38 17.48	0.59	1.608	0.338	1.296	0.214	5.26	1.58	2.42	1.27	111.06	48.39	0.193	-	S
1749	23 42 14.52	0.14	-52 25 19.86	0.15	59.867	3.325	46.587	2.572	8.19	0.06	2.59	0.04	161.67	0.84	0.227	-0.73	M
1750	23 44 38.16	0.31	-59 20 45.12	0.31	4.943	0.416	3.176	0.272	6.70	0.69	4.92	0.59	138.67	23.52	0.194	-	S
1751	23 44 22.13	0.63	-58 42 31.45	0.60	2.732	0.512	2.013	0.330	5.29	1.53	4.05	1.30	128.00	100.75	0.293	-	S
1752	23 44 49.59	0.14	-59 52 08.12	0.15	23.085	1.324	22.446	1.254	1.96	0.08	0.00	0.08	152.71	8.62	0.216	-0.20	S
1753	23 43 27.08	0.14	-56 26 24.23	0.15	144.460	8.123	140.136	7.770	1.74	0.06	0.93	0.06	160.32	14.27	0.978	0.32	S
1754	23 43 13.96	1.03	-55 52 50.49	1.14	60.212	3.334	4.271	0.430	31.50	2.72	26.31	2.33	151.26	22.31	0.531	-	S
1755	23 43 59.93	0.61	-58 00 23.25	0.57	6.835	0.841	2.891	0.365	8.48	1.76	0.00	0.74	135.63	13.48	0.329	-	M
1756	23 41 39.16	0.87	-50 26 00.36	1.06	1.627	0.285	0.916	0.192	8.27	2.35	6.32	2.12	165.35	95.60	0.171	-	S
1757	23 41 40.84	1.58	-50 37 22.18	1.50	4.901	0.417	0.871	0.172	16.38	5.00	0.00	1.05	41.02	14.13	0.165	-	M
1758	23 42 31.14	0.69	-53 40 07.63	0.59	2.093	0.292	1.297	0.192	8.41	1.75	4.06	1.13	119.91	23.18	0.167	-	S
1759	23 43 15.14	0.48	-55 58 31.78	0.56	2.578	0.382	1.834	0.249	6.14	1.31	3.83	1.04	20.05	36.96	0.214	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1760	23 44 45.77	0.38	-59 51 53.00	0.39	3.263	0.417	2.513	0.273	5.02	0.90	3.34	0.77	25.55	37.46	0.224	–	S
1761	23 41 44.90	0.78	-50 57 18.98	0.87	1.729	0.304	1.079	0.201	8.29	2.22	4.38	1.54	136.64	35.70	0.179	–	S
1762	23 43 34.17	0.49	-56 57 57.43	0.66	1.720	0.310	1.313	0.198	6.30	1.55	1.71	1.05	160.55	25.72	0.177	–	S
1763	23 41 47.52	0.51	-51 12 03.07	0.58	2.111	0.349	1.601	0.225	5.56	1.29	3.66	1.15	148.19	61.08	0.197	–	S
1764	23 43 07.68	1.30	-55 52 52.10	1.32	67.664	3.735	3.542	0.356	40.90	3.58	27.91	2.40	40.50	9.82	0.500	–	S
1765	23 42 39.06	0.64	-54 16 10.99	1.22	2.918	0.270	1.111	0.173	15.44	2.95	5.59	1.23	159.28	12.35	0.158	–	S
1766	23 42 15.33	0.34	-52 57 40.88	0.39	3.705	0.416	2.763	0.275	5.73	0.86	3.60	0.70	25.89	28.85	0.217	–	S
1767	23 42 12.59	0.16	-52 52 06.22	0.17	10.185	0.659	9.076	0.541	3.27	0.20	2.35	0.19	126.85	26.20	0.203	-0.63	S
1768	23 42 13.76	0.43	-52 57 54.56	0.45	3.451	0.408	2.360	0.268	5.68	1.01	5.33	0.93	40.29	148.92	0.219	–	S
1769	23 43 32.36	0.15	-57 04 59.50	0.17	12.004	0.735	10.531	0.611	3.59	0.16	2.16	0.15	173.77	9.95	0.189	-0.73	S
1770	23 41 30.22	1.03	-50 13 24.38	0.87	1.574	0.263	0.867	0.178	8.35	2.42	6.46	2.00	78.12	58.56	0.158	–	S
1771	23 41 27.72	0.30	-50 09 28.13	0.36	6.924	0.466	3.338	0.266	9.87	0.77	7.34	0.61	155.51	18.64	0.177	–	S
1772	23 44 35.66	0.32	-59 46 30.36	0.36	3.222	0.338	2.347	0.224	5.54	0.77	3.86	0.66	162.36	29.10	0.173	–	S
1773	23 44 04.68	0.84	-58 35 27.73	0.80	3.845	0.743	2.445	0.492	6.27	1.91	5.61	1.89	122.17	177.12	0.439	–	S
1774	23 42 47.87	0.35	-55 03 37.51	0.39	2.086	0.281	1.742	0.184	4.59	0.86	2.19	0.72	25.47	32.57	0.151	–	S
1775	23 43 27.24	0.84	-56 59 56.03	1.48	3.556	0.338	1.183	0.222	15.88	3.59	7.03	1.69	159.66	16.91	0.208	–	S
1776	23 42 50.49	0.90	-55 12 42.53	0.69	1.647	0.307	1.064	0.202	7.47	2.11	4.24	1.55	103.68	41.68	0.181	–	S
1777	23 42 49.68	1.92	-55 12 06.88	1.39	6.120	0.395	0.985	0.188	23.79	4.80	13.66	2.76	113.77	21.01	0.202	–	S
1778	23 43 20.48	0.21	-56 42 18.93	0.21	4.466	0.411	4.367	0.307	2.00	0.36	0.00	0.34	39.25	41.58	0.191	–	S
1779	23 44 17.65	0.59	-59 11 41.88	0.54	1.463	0.358	1.335	0.220	3.77	1.42	0.00	1.13	125.94	56.24	0.203	–	S
1780	23 44 15.81	1.05	-59 09 02.81	1.15	4.437	0.383	1.315	0.245	12.97	2.82	11.13	2.32	157.48	60.23	0.225	–	S
1781	23 44 29.54	1.15	-59 43 49.46	1.09	3.705	0.292	0.983	0.178	13.17	2.66	12.78	2.56	59.74	87.03	0.166	–	S
1782	23 42 15.90	0.84	-53 28 55.10	0.95	2.173	0.294	1.080	0.199	9.98	2.38	6.32	1.70	141.68	35.96	0.175	–	S
1783	23 42 05.81	0.28	-52 56 35.18	0.23	8.094	0.575	5.094	0.370	7.92	0.60	4.29	0.39	73.24	7.29	0.226	–	S
1784	23 41 38.08	0.39	-51 11 20.00	0.45	3.093	0.354	2.138	0.233	6.44	1.00	4.52	0.86	150.38	40.93	0.188	–	S
1785	23 44 18.75	0.66	-59 22 01.62	0.55	1.354	0.281	1.072	0.179	4.86	1.52	3.09	1.25	80.63	78.63	0.161	–	S
1786	23 43 03.01	0.94	-56 02 55.38	0.96	1.336	0.321	0.959	0.203	8.38	2.81	0.00	1.31	40.60	21.45	0.191	–	S
1787	23 41 46.86	0.17	-51 49 10.59	0.18	10.805	0.708	9.042	0.550	3.67	0.23	3.54	0.23	102.31	14.12	0.226	–	S
1788	23 44 01.34	0.77	-58 42 28.14	0.93	3.611	0.421	1.609	0.284	9.67	2.20	7.78	1.76	174.79	49.38	0.249	–	S
1789	23 42 27.55	0.30	-54 20 21.47	0.35	2.333	0.310	2.096	0.204	4.20	0.77	0.00	0.60	155.10	24.23	0.165	–	S
1790	23 42 08.34	1.43	-53 20 01.79	1.05	2.657	0.313	0.984	0.216	12.94	3.47	8.27	2.30	106.16	34.92	0.197	–	S
1791	23 44 18.47	0.55	-59 34 12.20	0.61	2.073	0.291	1.321	0.192	6.75	1.45	4.95	1.18	157.48	45.46	0.165	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1792	23 41 51.79	1.05	-52 23 23.18	2.03	3.883	0.298	0.868	0.178	20.46	4.71	10.77	2.47	1.24	21.79	0.178	–	S
1793	23 42 30.66	0.29	-54 49 08.38	0.65	50.202	2.838	23.292	1.306	31.67	1.58	3.65	0.24	67.51	2.43	0.255	-0.86	M
1794	23 41 22.43	0.37	-50 32 14.50	0.42	2.669	0.311	1.958	0.205	5.60	0.87	4.35	0.84	173.96	70.93	0.165	–	S
1795	23 43 56.02	0.53	-58 49 11.43	0.49	1.434	0.400	1.506	0.237	0.00	1.26	0.00	1.01	0.00	57.57	0.226	–	S
1796	23 41 23.60	0.19	-50 40 44.36	0.20	4.807	0.386	4.625	0.303	0.00	0.32	0.00	0.28	0.00	23.69	0.163	–	S
1797	23 44 00.78	0.38	-59 00 20.26	0.45	3.407	0.510	2.776	0.329	4.72	1.00	2.41	0.83	174.62	35.64	0.280	–	S
1798	23 41 17.84	0.63	-50 19 54.09	0.68	1.940	0.292	1.237	0.193	6.47	1.57	6.00	1.44	140.53	177.69	0.167	–	S
1799	23 43 17.27	0.14	-57 09 41.31	0.15	61.824	3.424	59.605	3.287	2.40	0.03	0.00	0.03	124.21	0.61	0.234	0.38	S
1800	23 42 18.92	0.35	-54 10 53.87	0.39	4.762	0.409	2.824	0.263	8.45	0.94	4.82	0.65	140.52	13.95	0.197	–	S
1801	23 42 16.13	0.28	-54 05 33.93	0.17	77.653	4.362	28.440	1.600	19.25	0.58	4.03	0.16	4.78	1.80	0.337	-1.01	M
1802	23 41 56.67	0.33	-53 08 49.61	0.19	136.731	7.626	29.710	1.698	22.34	0.72	8.28	0.27	178.56	2.49	0.462	-1.16	M
1803	23 41 20.53	0.62	-50 45 37.91	0.63	1.408	0.335	1.223	0.208	4.04	1.48	2.17	1.36	121.97	89.46	0.191	–	S
1804	23 42 39.01	0.25	-55 34 05.52	0.25	7.033	0.611	5.540	0.424	4.78	0.51	3.41	0.45	40.71	27.57	0.281	–	S
1805	23 42 51.25	0.41	-56 14 10.63	0.36	21.550	1.242	4.191	0.325	14.06	0.98	9.52	0.67	145.15	10.85	0.229	–	M
1806	23 42 18.04	0.19	-54 29 22.10	0.20	6.350	0.449	5.048	0.328	4.60	0.33	3.50	0.30	19.55	22.93	0.167	–	S
1807	23 43 18.47	0.46	-57 31 34.55	1.05	4.440	0.355	1.611	0.214	15.47	2.45	5.81	1.02	178.79	9.29	0.191	–	S
1808	23 44 00.58	1.15	-59 21 46.45	0.68	1.491	0.273	0.873	0.182	9.00	2.58	4.10	1.64	88.43	31.27	0.164	–	S
1809	23 43 33.14	0.66	-58 23 21.61	1.04	283.939	15.851	32.575	2.105	36.39	2.60	16.85	1.16	62.74	6.65	1.105	–	M
1810	23 42 58.31	0.26	-56 44 53.79	0.27	3.600	0.341	2.928	0.235	4.58	0.55	2.84	0.48	36.64	25.53	0.164	–	S
1811	23 42 17.78	1.54	-54 41 02.24	0.91	3.510	0.291	0.968	0.182	16.76	3.61	9.65	2.09	95.33	22.21	0.172	–	S
1812	23 43 16.97	0.49	-57 38 05.14	0.69	2.387	0.358	1.586	0.234	7.36	1.60	3.53	1.09	169.43	24.71	0.204	–	S
1813	23 43 07.35	0.18	-57 18 25.08	0.20	5.421	0.413	4.790	0.314	3.79	0.32	1.55	0.28	162.50	14.90	0.167	–	S
1814	23 41 25.81	0.27	-51 44 43.40	0.29	3.324	0.333	2.752	0.228	4.46	0.59	2.87	0.52	32.59	33.08	0.164	–	S
1815	23 42 57.81	0.15	-56 55 38.30	0.16	11.367	0.710	10.699	0.621	2.57	0.16	1.08	0.15	179.90	15.40	0.196	-0.58	S
1816	23 43 15.98	0.87	-57 53 45.11	1.14	4.680	0.525	1.865	0.355	11.70	2.77	7.65	1.86	17.75	29.74	0.319	–	S
1817	23 42 40.32	0.33	-56 12 16.36	0.36	2.389	0.347	2.190	0.225	4.29	0.84	0.00	0.61	32.14	19.25	0.187	–	S
1818	23 42 25.20	0.18	-55 28 19.95	0.19	7.503	0.573	7.056	0.453	2.47	0.28	1.40	0.27	55.48	40.89	0.231	–	S
1819	23 43 24.26	0.21	-58 24 27.37	0.16	265.710	14.970	83.513	4.733	16.23	0.38	4.07	0.12	163.13	1.44	1.143	-1.02	M
1820	23 41 12.49	0.63	-51 19 44.80	0.64	5.714	0.442	2.150	0.263	11.11	1.49	10.01	1.43	121.83	73.21	0.218	–	S
1821	23 42 43.05	0.17	-56 34 04.83	0.18	8.134	0.541	6.758	0.416	3.81	0.24	3.34	0.24	85.08	55.83	0.179	–	S
1822	23 43 39.37	0.44	-59 10 38.79	0.54	3.094	0.388	2.026	0.254	6.89	1.25	4.25	0.95	11.39	26.14	0.214	–	S
1823	23 41 06.96	0.44	-51 02 29.06	0.55	3.303	0.303	1.734	0.194	9.02	1.22	6.65	1.01	171.46	33.99	0.156	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1824	23 41 21.28	0.14	-52 02 51.26	0.15	34.170	1.906	29.186	1.617	4.17	0.06	2.34	0.05	96.12	1.15	0.188	-0.73	S
1825	23 41 59.01	0.15	-54 22 17.95	0.16	22.727	1.315	15.719	0.888	4.42	0.12	4.31	0.12	36.32	54.79	0.202	-0.79	M
1826	23 41 44.28	1.06	-53 28 14.01	2.04	3.747	0.286	0.824	0.171	20.39	4.73	10.88	2.50	0.12	21.98	0.171	-	S
1827	23 42 53.56	0.98	-57 13 13.72	1.30	3.079	0.327	1.088	0.222	12.70	3.11	8.75	2.19	160.93	35.75	0.202	-	S
1828	23 42 58.60	0.71	-57 32 01.13	0.52	4.039	0.376	1.846	0.242	10.35	1.61	6.90	1.19	77.65	24.16	0.203	-	S
1829	23 41 56.24	0.51	-54 18 14.18	0.59	2.172	0.309	1.462	0.202	6.52	1.35	4.65	1.15	159.60	51.05	0.173	-	S
1830	23 42 05.95	0.14	-55 10 11.90	0.17	51.587	2.929	37.501	2.085	13.07	0.20	0.00	0.07	96.45	0.94	0.303	-0.84	M
1831	23 41 36.14	0.70	-53 08 41.40	0.71	1.706	0.466	1.482	0.288	3.64	1.72	2.56	1.52	44.33	161.21	0.267	-	S
1832	23 43 31.25	0.67	-59 02 09.18	0.62	1.336	0.418	1.324	0.247	4.19	1.75	0.00	1.12	129.05	31.13	0.238	-	S
1833	23 41 28.36	0.33	-52 49 47.54	0.20	96.266	5.385	27.657	1.570	20.96	0.73	7.26	0.26	12.47	2.58	0.389	-1.08	M
1834	23 41 31.03	1.07	-53 04 47.55	0.79	4.413	0.437	1.687	0.289	12.36	2.56	8.31	1.76	100.94	29.01	0.256	-	S
1835	23 42 14.06	0.37	-55 36 52.85	0.18	190.325	10.584	60.918	3.394	28.34	0.82	6.06	0.18	9.70	1.65	0.541	-1.25	M
1836	23 42 06.67	0.49	-55 13 58.50	0.40	2.518	0.324	1.807	0.212	6.21	1.10	3.67	0.87	82.71	29.91	0.177	-	S
1837	23 43 25.47	0.17	-59 08 12.06	0.17	9.615	0.655	8.899	0.540	2.65	0.21	1.73	0.21	117.83	35.60	0.224	-	S
1838	23 43 29.51	0.20	-59 18 57.66	0.22	5.487	0.457	4.824	0.336	3.60	0.37	1.98	0.34	157.55	23.56	0.201	-	S
1839	23 41 15.91	0.20	-52 19 59.23	0.24	6.476	0.516	5.301	0.371	5.34	0.45	1.88	0.34	171.83	10.62	0.221	-	S
1840	23 43 44.49	0.72	-59 58 34.89	0.57	1.669	0.340	1.258	0.218	5.46	1.64	3.38	1.32	84.93	67.13	0.196	-	S
1841	23 41 29.97	1.25	-53 22 00.78	1.10	3.574	0.411	1.367	0.281	12.91	3.32	7.72	2.02	52.41	28.25	0.256	-	S
1842	23 40 54.17	0.39	-51 01 58.13	0.50	2.406	0.286	1.680	0.187	7.55	1.19	2.95	0.76	148.70	16.98	0.154	-	S
1843	23 41 03.07	0.92	-51 41 54.18	1.20	1.736	0.255	0.828	0.175	10.45	2.81	6.75	2.08	155.67	44.67	0.156	-	S
1844	23 41 23.01	0.89	-53 04 08.69	0.79	3.347	0.461	1.731	0.311	9.07	2.16	6.58	1.72	113.72	47.98	0.273	-	S
1845	23 42 56.60	0.20	-58 07 28.02	0.21	13.656	1.128	12.239	0.840	3.63	0.36	1.25	0.32	150.67	17.87	0.491	-	S
1846	23 43 36.04	0.19	-59 49 32.38	0.20	6.018	0.454	5.137	0.340	3.66	0.32	2.68	0.30	1.75	26.64	0.182	-	S
1847	23 40 45.13	0.25	-50 33 30.34	0.27	3.611	0.339	2.986	0.235	4.10	0.51	3.44	0.51	11.63	5.96	0.162	-	S
1848	23 41 35.31	0.46	-54 02 15.02	0.64	1.111	0.242	0.978	0.150	0.00	1.45	0.00	1.05	0.00	33.34	0.137	-	S
1849	23 42 24.46	0.66	-56 47 15.63	0.70	8.861	0.550	2.196	0.241	16.93	1.84	11.00	1.23	137.91	13.05	0.208	-	S
1850	23 43 21.85	0.71	-59 28 24.60	0.80	1.046	0.287	0.856	0.179	4.52	1.96	2.60	1.55	162.87	84.72	0.166	-	S
1851	23 41 38.98	1.08	-54 25 02.19	0.70	2.340	0.278	1.078	0.186	11.98	2.65	5.49	1.41	107.98	19.25	0.166	-	S
1852	23 43 21.03	1.17	-59 31 45.99	1.02	2.562	0.290	0.995	0.197	12.73	3.08	7.01	1.84	47.25	24.48	0.179	-	S
1853	23 41 25.37	0.81	-53 39 30.36	0.61	3.543	0.349	1.576	0.227	10.65	1.90	7.38	1.37	80.53	27.04	0.195	-	S
1854	23 41 36.68	0.36	-54 24 55.63	0.32	3.474	0.326	2.351	0.215	6.56	0.79	4.48	0.65	108.28	24.73	0.161	-	S
1855	23 42 08.48	0.19	-56 12 50.00	0.21	6.043	0.467	5.207	0.348	4.12	0.35	1.98	0.30	156.41	15.82	0.192	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1856	23 41 34.80	0.51	-54 20 21.53	0.52	2.554	0.299	1.563	0.197	7.01	1.22	5.79	1.11	131.77	70.40	0.164	-	S
1857	23 40 53.74	0.61	-51 42 32.11	0.79	1.783	0.274	1.113	0.181	7.84	1.83	4.78	1.37	17.05	37.55	0.159	-	S
1858	23 41 35.18	0.23	-54 23 45.95	0.26	3.923	0.350	3.257	0.246	4.55	0.50	2.52	0.42	9.04	21.41	0.162	-	S
1859	23 42 22.33	1.14	-56 58 22.96	1.79	4.419	0.305	0.897	0.163	22.36	4.50	10.30	2.06	152.99	15.49	0.167	-	S
1860	23 40 39.02	0.91	-50 42 46.65	1.05	1.400	0.261	0.816	0.175	8.47	2.52	5.46	1.98	141.26	54.77	0.157	-	S
1861	23 41 27.33	0.96	-53 57 50.56	1.25	2.203	0.239	0.814	0.163	12.39	2.94	8.76	2.20	160.45	41.84	0.147	-	S
1862	23 40 48.95	0.41	-51 31 31.04	0.45	4.372	0.353	2.219	0.219	8.84	1.02	7.28	0.87	35.94	32.89	0.167	-	S
1863	23 40 32.76	0.28	-50 21 40.28	0.29	4.598	0.383	3.212	0.256	6.44	0.64	4.35	0.51	130.77	20.65	0.174	-	S
1864	23 42 13.94	1.00	-56 38 12.39	1.27	4.435	0.334	1.114	0.195	15.31	2.98	12.11	2.32	4.81	37.96	0.184	-	S
1865	23 41 03.46	0.38	-52 34 23.11	0.34	6.657	0.696	4.709	0.460	5.96	0.85	4.41	0.72	86.17	34.08	0.358	-	S
1866	23 41 22.47	0.28	-53 52 15.43	0.31	3.536	0.339	2.690	0.229	5.41	0.65	3.56	0.55	153.50	28.05	0.166	-	S
1867	23 40 48.38	0.44	-51 41 17.00	0.52	2.032	0.289	1.503	0.188	5.67	1.13	4.01	1.01	8.02	57.01	0.160	-	S
1868	23 43 20.35	0.38	-59 55 22.92	0.42	1.825	0.309	1.648	0.197	3.43	0.94	1.04	0.80	8.14	49.91	0.171	-	S
1869	23 43 11.84	0.52	-59 35 17.10	0.62	2.966	0.319	1.581	0.210	8.24	1.44	6.28	1.15	6.08	33.02	0.176	-	S
1870	23 42 01.65	0.40	-56 16 38.10	0.45	3.036	0.329	1.970	0.216	6.58	1.01	5.05	0.86	17.90	38.28	0.174	-	S
1871	23 40 24.71	0.50	-50 07 33.50	0.60	2.893	0.286	1.517	0.186	8.75	1.31	7.04	1.20	10.44	56.13	0.153	-	S
1872	23 41 39.90	0.53	-55 06 04.48	0.47	3.963	0.393	2.207	0.255	8.53	1.27	5.66	0.94	55.85	22.65	0.208	-	S
1873	23 41 25.71	0.16	-54 19 43.76	0.17	8.253	0.528	7.286	0.432	3.34	0.20	2.47	0.19	154.69	26.16	0.158	-0.48	S
1874	23 42 21.77	0.46	-57 22 54.71	0.25	8.156	0.714	3.790	0.312	0.00	1.06	0.00	0.39	0.00	6.76	0.232	-	M
1875	23 41 17.88	0.14	-54 05 57.64	0.15	39.082	2.169	38.791	2.140	0.00	0.04	0.00	0.03	0.00	10.67	0.166	0.01	S
1876	23 42 20.52	0.43	-57 28 02.55	1.40	26.499	1.699	9.162	0.635	26.11	3.33	5.25	0.75	77.10	7.23	0.387	-	M
1877	23 40 36.01	0.32	-51 10 00.58	0.45	6.660	0.482	3.201	0.284	10.68	1.01	6.49	0.67	168.60	12.25	0.206	-	S
1878	23 40 56.52	0.52	-52 36 25.72	1.26	7.934	0.669	2.843	0.414	16.85	2.96	5.70	1.13	169.95	10.83	0.378	-	S
1879	23 42 15.77	0.37	-57 14 55.23	0.26	21.423	1.349	7.886	0.521	15.66	0.91	2.06	0.26	147.13	3.29	0.288	-	M
1880	23 41 53.18	0.15	-56 02 44.54	0.16	15.003	0.872	13.811	0.778	3.02	0.11	1.36	0.10	5.15	6.85	0.164	-0.32	S
1881	23 41 54.62	0.91	-56 10 38.14	1.77	2.522	0.244	0.768	0.163	16.36	4.16	8.14	2.10	2.73	21.53	0.155	-	S
1882	23 41 46.83	1.14	-55 45 14.37	1.04	3.036	0.437	1.371	0.302	9.49	2.75	8.06	2.32	58.84	93.99	0.269	-	S
1883	23 42 21.91	0.16	-57 39 50.64	0.17	13.977	0.861	11.696	0.685	3.83	0.18	3.07	0.17	175.38	18.24	0.228	-0.33	S
1884	23 42 30.91	0.57	-58 04 54.32	0.51	4.319	0.957	3.826	0.595	3.83	1.33	1.49	1.11	114.63	70.23	0.542	-	S
1885	23 40 35.99	0.21	-51 33 16.93	0.21	6.959	0.464	4.727	0.311	6.81	0.41	4.34	0.31	121.13	9.32	0.160	-	S
1886	23 40 20.28	0.53	-50 22 05.89	0.43	3.827	0.354	2.092	0.227	9.37	1.31	5.55	0.84	109.00	16.14	0.182	-	S
1887	23 40 41.71	0.15	-51 57 11.06	0.16	12.826	0.778	11.934	0.685	2.51	0.14	1.92	0.14	117.18	34.53	0.191	-0.80	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1888	23 42 01.45	0.29	-56 46 38.42	0.32	8.001	0.547	4.095	0.320	9.46	0.72	6.01	0.52	146.65	9.61	0.211	–	S
1889	23 42 58.62	0.99	-59 28 38.10	1.50	3.875	0.357	1.148	0.235	14.69	3.56	9.49	2.26	4.98	27.33	0.221	–	S
1890	23 41 01.68	0.68	-53 18 32.81	0.67	3.176	0.551	2.156	0.360	6.08	1.63	5.04	1.47	120.29	114.45	0.318	–	S
1891	23 43 01.98	0.63	-59 37 59.10	0.65	1.198	0.270	0.961	0.171	4.17	1.51	3.50	1.43	10.49	153.87	0.155	–	S
1892	23 41 07.42	0.34	-53 44 27.90	0.37	2.851	0.311	2.115	0.207	5.52	0.80	3.96	0.71	146.69	41.76	0.161	–	S
1893	23 40 19.83	0.56	-50 28 08.96	0.64	2.140	0.379	1.596	0.245	5.42	1.42	4.22	1.32	10.94	111.64	0.216	–	S
1894	23 42 55.33	0.26	-59 28 15.12	0.41	12.970	0.875	4.635	0.350	10.70	0.91	4.69	0.51	98.16	8.67	0.240	–	M
1895	23 40 52.15	1.12	-52 52 32.43	0.92	9.717	0.660	2.580	0.341	21.41	3.23	7.21	1.10	124.20	8.50	0.324	–	S
1896	23 40 57.88	0.94	-53 11 58.30	0.66	1.551	0.396	1.222	0.248	6.42	2.25	0.00	1.42	104.13	33.60	0.230	–	S
1897	23 40 16.16	0.52	-50 25 14.75	1.27	26.280	1.529	3.303	0.318	24.68	3.03	9.27	1.03	76.48	8.94	0.261	–	M
1898	23 42 11.64	1.14	-57 28 17.73	1.97	7.882	0.633	1.900	0.391	20.52	4.89	8.67	2.08	156.29	17.17	0.394	–	S
1899	23 42 47.20	0.43	-59 10 36.81	0.33	5.672	0.463	3.076	0.291	8.68	0.92	5.71	0.72	80.22	17.92	0.219	–	S
1900	23 41 58.69	0.31	-56 51 49.25	0.33	4.061	0.373	2.787	0.247	6.02	0.71	4.62	0.62	23.59	30.43	0.182	–	S
1901	23 41 53.35	0.71	-56 36 15.67	0.53	1.968	0.358	1.436	0.231	6.32	1.62	3.09	1.21	79.29	36.72	0.205	–	S
1902	23 41 07.34	0.45	-53 58 26.66	0.68	1.893	0.271	1.276	0.177	7.60	1.54	3.30	1.01	4.01	22.40	0.153	–	S
1903	23 40 22.35	0.15	-50 56 51.36	0.16	18.578	1.075	17.073	0.959	3.20	0.11	1.49	0.09	146.35	7.32	0.193	-1.06	S
1904	23 40 24.56	0.24	-51 14 31.39	0.22	12.030	0.950	9.288	0.665	5.64	0.50	2.96	0.37	98.96	12.15	0.406	–	S
1905	23 42 27.04	0.77	-58 23 01.49	0.79	10.640	1.263	5.085	0.847	9.16	1.97	7.26	1.62	140.70	55.95	0.737	–	S
1906	23 40 57.40	0.22	-53 30 36.65	0.27	8.345	0.572	5.178	0.365	7.67	0.52	4.92	0.39	177.36	10.23	0.212	–	S
1907	23 42 43.13	0.56	-59 12 57.55	0.70	3.652	0.363	1.718	0.237	9.39	1.63	7.13	1.27	0.61	30.94	0.200	–	S
1908	23 40 22.88	0.35	-51 12 37.33	0.44	15.005	1.195	6.629	0.517	11.47	1.18	0.00	0.39	124.04	6.08	0.367	–	M
1909	23 41 16.47	1.19	-54 44 29.45	1.45	2.806	0.281	0.871	0.190	13.85	3.49	10.16	2.64	152.96	46.92	0.176	–	S
1910	23 40 34.25	1.67	-52 04 24.59	0.99	3.160	0.320	1.012	0.216	15.51	4.05	8.53	2.18	97.17	24.67	0.203	–	S
1911	23 40 19.92	0.51	-51 13 24.38	1.41	45.379	2.779	15.901	0.970	39.97	3.48	2.63	0.40	106.12	3.99	0.419	–	M
1912	23 41 30.91	0.16	-55 46 13.96	0.18	15.195	0.978	12.938	0.775	0.00	0.24	0.00	0.17	0.00	3.44	0.299	-1.10	S
1913	23 41 22.88	1.56	-55 15 44.95	1.76	6.858	0.407	0.825	0.145	24.51	4.32	18.98	3.41	146.83	35.91	0.167	–	S
1914	23 40 08.95	0.20	-50 25 35.67	0.32	30.264	1.743	10.757	0.648	16.34	0.66	8.28	0.32	78.30	3.71	0.265	–	M
1915	23 41 45.43	0.89	-56 32 51.96	0.89	3.674	0.330	1.421	0.209	14.76	2.67	5.51	1.13	41.60	11.56	0.189	–	S
1916	23 41 55.79	0.49	-57 07 34.87	0.69	3.528	0.372	1.831	0.244	9.37	1.60	5.75	1.10	6.83	21.21	0.206	–	S
1917	23 40 15.10	1.03	-50 49 41.91	1.59	2.852	0.241	0.804	0.152	17.80	3.95	9.11	1.99	23.59	19.99	0.145	–	S
1918	23 41 44.94	0.34	-56 39 20.75	0.27	45.419	2.599	11.382	0.683	14.45	0.74	10.60	0.53	4.86	8.55	0.274	–	M
1919	23 41 38.05	1.30	-56 16 14.76	1.52	3.992	0.317	0.942	0.195	16.04	3.67	12.65	2.90	154.56	49.49	0.189	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
1920	23 40 16.66	0.62	-51 05 02.80	0.75	1.867	0.292	1.192	0.192	7.45	1.72	4.90	1.41	153.95	48.90	0.168	-	S
1921	23 40 42.71	0.75	-52 56 54.69	0.71	2.976	0.370	1.556	0.247	8.88	1.85	6.61	1.51	121.21	46.42	0.214	-	S
1922	23 41 06.59	1.02	-54 28 57.21	1.62	1.931	0.232	0.727	0.159	14.52	4.02	6.44	1.92	21.57	21.99	0.149	-	S
1923	23 41 44.66	0.60	-56 41 03.95	0.77	2.659	0.508	1.889	0.329	6.49	1.81	3.34	1.33	12.63	38.11	0.294	-	S
1924	23 41 36.76	0.82	-56 15 45.84	1.07	1.611	0.313	0.977	0.208	8.70	2.66	3.88	1.65	151.70	31.94	0.188	-	S
1925	23 40 51.82	0.24	-53 42 12.65	0.24	10.173	0.690	6.250	0.438	6.73	0.46	6.03	0.43	78.64	33.92	0.251	-	S
1926	23 40 44.26	0.31	-53 14 34.61	0.20	19.448	1.215	8.957	0.562	12.34	0.66	4.64	0.31	1.82	4.65	0.270	-	M
1927	23 40 42.97	0.58	-53 17 46.96	1.84	43.505	2.484	5.316	0.485	35.09	4.36	9.97	1.16	96.99	8.45	0.387	-	M
1928	23 42 34.37	0.15	-59 15 46.48	0.16	15.434	0.923	14.527	0.827	2.40	0.12	1.42	0.12	128.17	19.37	0.211	-0.43	S
1929	23 40 05.35	0.21	-50 29 47.08	0.33	18.653	1.077	6.719	0.445	14.91	0.70	7.52	0.37	5.92	2.89	0.237	-	S
1930	23 40 11.84	0.15	-51 02 46.13	0.16	11.286	0.686	10.376	0.596	0.00	0.16	0.00	0.13	0.00	5.67	0.170	0.32	S
1931	23 40 01.49	0.33	-50 15 06.12	0.35	2.737	0.289	2.061	0.193	5.00	0.72	4.42	0.72	55.73	72.76	0.148	-	S
1932	23 41 00.72	0.70	-54 25 32.15	0.85	2.005	0.275	1.075	0.184	8.45	1.95	6.48	1.62	1.45	56.86	0.161	-	S
1933	23 40 46.55	0.47	-53 35 56.90	0.58	3.165	0.376	1.936	0.247	7.45	1.30	5.39	1.08	172.12	41.00	0.207	-	S
1934	23 41 16.41	0.59	-55 27 26.84	0.49	2.588	0.298	1.516	0.196	7.70	1.34	5.69	1.10	77.07	38.94	0.164	-	S
1935	23 41 28.08	0.44	-56 24 29.73	0.55	25.612	1.453	3.778	0.296	18.72	1.38	10.85	0.77	55.52	8.12	0.211	-	M
1936	23 41 43.36	1.20	-57 09 07.72	2.35	6.053	0.389	0.913	0.183	25.42	5.52	13.34	2.78	2.36	18.96	0.203	-	S
1937	23 41 59.79	0.55	-57 59 52.17	0.51	6.172	1.025	4.657	0.662	5.50	1.31	3.37	1.08	126.97	49.33	0.578	-	S
1938	23 41 04.30	0.24	-55 03 21.76	0.25	4.507	0.373	3.448	0.258	4.77	0.48	4.07	0.45	10.61	51.46	0.166	-	S
1939	23 40 13.07	0.24	-51 47 33.92	0.28	3.026	0.343	2.903	0.237	0.00	0.55	0.00	0.46	0.00	27.19	0.174	-	S
1940	23 42 15.90	0.69	-59 00 31.21	0.70	2.976	0.398	1.654	0.265	8.00	1.77	5.94	1.41	36.76	44.61	0.230	-	S
1941	23 40 14.40	0.47	-52 04 06.70	0.47	3.811	0.424	2.399	0.279	6.78	1.10	5.70	1.00	51.97	55.45	0.228	-	S
1942	23 42 20.95	0.30	-59 21 17.68	0.30	4.378	0.484	3.581	0.325	3.91	0.65	3.45	0.60	149.43	115.31	0.248	-	S
1943	23 39 55.34	0.16	-50 40 53.76	0.18	17.329	1.050	10.615	0.612	8.31	0.25	0.66	0.13	115.38	2.65	0.183	-0.60	M
1944	23 42 19.77	1.12	-59 21 36.66	1.38	4.023	0.398	1.252	0.269	12.90	3.33	10.34	2.54	6.26	49.00	0.248	-	S
1945	23 40 26.15	0.21	-53 03 09.12	0.24	7.589	0.554	5.490	0.381	5.63	0.43	4.38	0.38	161.02	27.30	0.219	-	S
1946	23 39 45.27	0.49	-50 00 03.04	0.52	1.936	0.291	1.445	0.189	5.78	1.22	3.80	1.06	132.78	49.96	0.162	-	S
1947	23 40 01.31	0.30	-51 18 08.37	0.33	4.617	0.392	3.064	0.258	7.04	0.73	4.60	0.57	140.50	19.62	0.183	-	S
1948	23 39 45.45	0.94	-50 03 13.24	1.36	4.315	0.312	1.061	0.176	17.95	3.21	11.47	2.11	159.66	25.45	0.166	-	S
1949	23 40 31.35	0.25	-53 53 44.17	0.40	23.005	1.422	8.453	0.527	19.84	0.95	6.77	0.33	62.69	3.33	0.249	-	M
1950	23 40 20.16	0.94	-52 51 46.21	1.56	3.597	0.352	1.182	0.234	15.80	3.78	7.85	1.92	17.60	21.12	0.218	-	S
1951	23 42 17.07	0.22	-59 28 54.24	0.24	5.713	0.455	4.366	0.317	4.75	0.44	3.86	0.41	168.11	31.48	0.196	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1952	23 42 17.44	0.20	-59 32 06.11	0.29	18.091	1.061	6.099	0.387	12.25	0.60	5.53	0.32	101.25	4.87	0.193	–	M
1953	23 41 26.22	0.14	-57 00 35.86	0.15	23.967	1.356	23.769	1.320	1.11	0.06	0.00	0.06	129.04	117.37	0.185	-0.25	S
1954	23 39 52.52	0.32	-51 00 04.12	0.34	3.367	0.316	2.339	0.210	6.46	0.77	4.39	0.63	133.28	26.07	0.155	–	S
1955	23 40 02.21	0.50	-51 45 07.64	0.63	2.795	0.319	1.612	0.210	8.13	1.39	5.89	1.16	169.28	42.25	0.176	–	S
1956	23 39 59.14	0.50	-51 35 22.52	0.77	4.433	0.332	1.716	0.193	14.87	1.94	6.11	0.86	25.15	8.81	0.162	–	S
1957	23 41 17.10	0.39	-56 39 40.39	0.37	5.054	0.432	2.883	0.276	7.53	0.87	6.22	0.78	122.05	44.05	0.208	–	S
1958	23 40 56.79	0.89	-55 28 20.77	0.85	1.344	0.324	0.961	0.209	6.21	2.23	3.77	1.76	127.13	67.76	0.190	–	S
1959	23 40 26.46	1.67	-53 35 13.39	2.72	13.729	0.777	1.055	0.180	39.53	6.74	19.44	3.27	155.63	15.28	0.247	–	S
1960	23 40 53.17	1.20	-55 18 39.63	1.33	2.548	0.268	0.899	0.180	15.45	3.77	6.70	1.78	137.39	19.37	0.168	–	S
1961	23 42 22.44	0.32	-59 57 05.24	0.34	2.662	0.329	2.198	0.218	4.26	0.75	2.75	0.66	158.08	42.04	0.174	–	S
1962	23 41 05.99	0.49	-56 04 14.33	0.49	1.832	0.280	1.385	0.181	5.09	1.16	3.89	1.02	41.35	70.07	0.156	–	S
1963	23 39 43.63	0.20	-50 30 54.53	0.20	14.253	0.888	7.229	0.447	8.99	0.40	3.42	0.23	134.98	4.83	0.204	–	M
1964	23 40 47.11	0.69	-55 03 27.03	0.63	2.327	0.292	1.285	0.194	7.89	1.61	6.51	1.42	108.89	73.02	0.167	–	S
1965	23 42 04.83	0.35	-59 16 41.59	0.43	3.455	0.427	2.580	0.280	5.67	0.95	3.16	0.75	170.69	25.49	0.229	–	S
1966	23 40 03.60	0.52	-52 13 38.11	0.58	8.108	0.840	4.400	0.549	8.44	1.33	6.54	1.15	145.00	45.80	0.454	–	S
1967	23 42 10.30	0.77	-59 34 37.79	0.71	1.666	0.308	1.098	0.202	6.56	1.90	4.61	1.50	46.74	60.98	0.180	–	S
1968	23 41 25.92	0.66	-57 23 52.77	0.78	3.271	0.390	1.643	0.261	8.74	1.84	6.93	1.49	7.18	47.95	0.225	–	S
1969	23 39 56.29	0.31	-51 44 57.79	0.38	3.265	0.333	2.354	0.221	6.28	0.83	3.79	0.65	12.35	23.91	0.169	–	S
1970	23 40 41.94	1.52	-54 57 21.29	1.26	2.208	0.230	0.708	0.157	15.28	4.00	8.39	2.29	121.76	27.19	0.147	–	S
1971	23 39 58.42	1.23	-52 12 19.34	0.71	36.120	2.278	6.196	0.540	60.82	3.30	6.02	0.35	148.68	2.89	0.419	–	M
1972	23 42 04.18	1.14	-59 27 19.95	0.90	2.755	0.363	1.215	0.249	10.41	2.69	7.24	2.01	63.59	45.69	0.223	–	S
1973	23 40 32.90	0.28	-54 34 08.29	0.27	5.313	0.423	3.561	0.280	5.98	0.57	5.26	0.53	73.94	48.14	0.187	–	S
1974	23 39 31.17	0.38	-50 04 30.65	0.51	1.809	0.290	1.530	0.186	5.15	1.12	1.23	0.85	5.39	30.75	0.160	–	S
1975	23 40 18.29	0.33	-53 39 10.02	0.40	4.483	0.446	3.074	0.293	7.66	0.96	2.88	0.60	146.86	12.19	0.227	–	S
1976	23 40 28.07	0.87	-54 18 31.85	0.88	1.540	0.257	0.876	0.173	7.88	2.19	6.12	1.86	133.01	79.31	0.153	–	S
1977	23 39 55.76	0.23	-52 04 08.51	0.27	4.848	0.474	4.248	0.332	4.53	0.55	0.54	0.42	156.51	16.77	0.229	–	S
1978	23 40 16.06	0.14	-53 38 30.71	0.15	32.242	1.814	28.356	1.576	3.26	0.07	2.70	0.07	126.25	14.18	0.223	-0.87	S
1979	23 41 26.82	0.53	-57 51 40.25	0.50	3.675	0.517	2.525	0.339	6.04	1.25	4.56	1.08	126.13	63.02	0.289	–	S
1980	23 39 30.11	0.74	-50 09 30.03	0.92	1.141	0.246	0.796	0.160	6.45	2.01	4.45	1.81	179.55	87.84	0.144	–	S
1981	23 39 37.29	0.98	-50 54 44.37	0.91	1.290	0.229	0.739	0.154	7.67	2.31	6.49	2.07	69.68	89.63	0.137	–	S
1982	23 42 01.55	0.35	-59 48 25.68	0.36	3.568	0.356	2.400	0.234	5.85	0.81	4.98	0.72	19.14	47.36	0.181	–	S
1983	23 39 48.38	0.19	-52 06 03.51	0.20	8.111	0.629	7.473	0.488	2.84	0.30	1.87	0.29	176.33	48.11	0.258	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
1984	23 41 57.09	1.34	-59 48 20.31	2.17	6.489	0.547	1.160	0.189	17.78	5.88	0.00	1.14	57.11	14.62	0.178	–	M
1985	23 41 54.68	0.59	-59 41 56.70	0.40	1.804	0.280	1.373	0.180	6.54	1.30	1.30	0.87	71.80	19.99	0.157	–	S
1986	23 41 05.48	0.17	-57 16 04.03	0.18	6.804	0.519	6.868	0.431	0.00	0.25	0.00	0.23	0.00	22.62	0.208	–	S
1987	23 41 10.10	0.21	-57 29 32.97	0.21	4.471	0.378	4.017	0.280	3.24	0.37	1.97	0.34	85.27	36.97	0.167	–	S
1988	23 41 58.77	0.77	-59 55 33.19	1.01	2.225	0.289	1.057	0.196	10.36	2.49	5.96	1.60	155.20	26.92	0.174	–	S
1989	23 40 55.39	0.40	-56 41 22.36	0.30	11.955	0.727	4.332	0.335	13.12	0.89	8.07	0.57	66.41	6.72	0.223	–	S
1990	23 40 57.44	0.63	-56 47 20.29	0.67	2.305	0.289	1.273	0.192	7.43	1.58	6.81	1.41	4.25	115.35	0.164	–	S
1991	23 41 38.99	1.05	-59 02 51.61	1.27	3.517	0.320	1.095	0.208	14.83	3.27	8.72	1.99	146.89	23.72	0.193	–	S
1992	23 40 19.21	0.44	-54 33 44.62	0.43	3.813	0.365	2.209	0.237	7.06	1.00	6.61	0.94	95.60	136.12	0.188	–	S
1993	23 39 35.64	0.76	-51 22 54.56	1.34	2.030	0.341	1.071	0.231	10.65	3.08	4.90	1.79	172.19	30.00	0.209	–	S
1994	23 40 16.97	0.44	-54 24 04.77	0.51	1.894	0.297	1.476	0.192	5.10	1.15	3.36	1.00	165.60	56.31	0.165	–	S
1995	23 41 10.63	0.90	-57 39 02.29	1.14	10.019	0.653	1.368	0.200	11.61	3.04	4.46	1.50	121.75	22.93	0.185	–	M
1996	23 39 26.82	0.29	-50 43 47.21	0.37	4.106	0.338	2.543	0.218	7.90	0.80	5.00	0.59	10.55	17.08	0.156	–	S
1997	23 40 52.42	0.17	-56 40 18.34	0.18	10.031	0.668	8.581	0.525	3.33	0.23	3.18	0.22	3.05	110.67	0.221	–	S
1998	23 41 03.24	0.15	-57 20 39.06	0.15	22.059	1.286	21.582	1.213	1.28	0.09	1.06	0.09	88.96	133.65	0.247	0.57	S
1999	23 41 43.98	0.31	-59 27 30.80	0.32	4.882	0.540	3.888	0.361	4.18	0.69	3.68	0.62	16.93	85.24	0.278	–	S
2000	23 39 57.82	0.71	-53 13 59.60	0.76	2.625	0.555	1.920	0.357	5.85	1.82	3.90	1.55	140.88	74.64	0.322	–	S
2001	23 41 18.34	0.14	-58 16 09.95	0.15	2432.129	133.934	1606.823	88.397	10.37	0.02	5.25	0.01	137.13	0.22	1.954	-0.63	M
2002	23 41 32.04	0.23	-58 58 44.65	0.24	7.683	0.569	5.423	0.386	6.38	0.47	3.56	0.37	140.98	10.10	0.230	–	S
2003	23 39 23.27	0.21	-50 54 07.29	0.24	4.993	0.382	3.849	0.269	5.62	0.46	3.25	0.36	148.48	15.12	0.158	–	S
2004	23 39 40.16	0.54	-52 15 07.82	0.56	4.050	0.590	2.817	0.385	6.57	1.37	4.12	1.09	132.50	39.71	0.331	–	S
2005	23 41 30.79	0.53	-59 06 18.28	0.47	2.426	0.352	1.721	0.230	5.61	1.22	4.38	1.05	67.79	78.20	0.197	–	S
2006	23 39 16.22	0.87	-50 28 36.33	0.73	2.522	0.337	1.324	0.226	8.86	2.08	6.74	1.63	77.09	44.06	0.198	–	S
2007	23 41 38.71	0.36	-59 34 59.26	0.35	3.685	0.398	2.642	0.263	5.39	0.81	4.39	0.72	46.85	55.74	0.206	–	S
2008	23 40 33.28	0.19	-56 03 28.75	0.21	6.314	0.487	5.479	0.365	3.57	0.33	2.57	0.31	174.99	33.81	0.200	–	S
2009	23 40 48.16	0.18	-57 01 12.69	0.20	6.849	0.481	5.531	0.356	4.77	0.32	2.76	0.27	162.33	12.03	0.177	–	S
2010	23 39 28.83	0.24	-51 39 57.61	0.29	4.367	0.363	3.183	0.246	6.07	0.58	3.86	0.47	166.39	20.16	0.163	–	S
2011	23 41 02.97	0.43	-57 52 06.90	0.50	6.936	0.809	4.475	0.531	6.64	1.13	4.95	0.94	177.19	37.80	0.438	–	S
2012	23 39 55.79	0.37	-53 47 34.60	0.35	2.016	0.310	1.858	0.200	3.45	0.83	0.00	0.72	112.31	43.21	0.168	–	S
2013	23 41 23.21	0.95	-59 09 50.73	0.67	6.478	0.439	1.719	0.227	15.77	2.16	10.53	1.54	71.42	19.67	0.204	–	S
2014	23 39 14.84	0.17	-50 53 23.37	0.18	7.972	0.543	7.110	0.435	3.55	0.25	1.89	0.22	81.27	15.23	0.187	–	S
2015	23 39 19.19	0.15	-51 23 11.22	0.17	87.660	4.881	35.270	1.960	19.20	0.19	5.21	0.06	121.84	0.66	0.284	-0.51	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2016	23 39 05.73	0.83	-50 04 50.53	0.93	1.961	0.232	0.901	0.156	10.58	2.28	7.44	1.76	139.43	41.89	0.137	–	S
2017	23 39 22.06	0.54	-51 26 09.92	0.69	1.234	0.350	1.193	0.210	0.00	1.53	0.00	1.28	0.00	61.60	0.199	–	S
2018	23 40 48.38	0.61	-57 21 36.09	0.36	5.957	0.667	3.765	0.434	9.25	1.41	1.97	0.72	71.56	10.61	0.364	–	S
2019	23 40 01.69	0.43	-54 27 31.75	0.40	2.579	0.314	1.858	0.206	5.64	0.97	4.31	0.86	72.20	50.49	0.169	–	S
2020	23 39 29.49	0.17	-52 08 58.22	0.19	11.652	0.780	9.667	0.598	4.29	0.27	3.07	0.24	151.43	21.75	0.262	–	S
2021	23 40 04.18	1.08	-54 44 22.77	1.11	10.415	0.615	1.591	0.215	20.46	2.77	17.36	2.32	38.43	35.00	0.221	–	S
2022	23 41 28.39	0.39	-59 37 29.27	0.32	2.602	0.308	1.995	0.203	5.36	0.83	3.17	0.70	96.62	32.76	0.162	–	S
2023	23 40 14.35	0.27	-55 29 51.74	0.29	3.970	0.378	3.075	0.257	4.83	0.60	3.73	0.54	15.91	41.20	0.184	–	S
2024	23 39 49.76	0.89	-53 49 39.90	1.18	1.577	0.277	0.846	0.188	8.99	2.72	6.00	2.07	166.07	53.74	0.169	–	S
2025	23 40 43.44	0.33	-57 21 32.84	0.21	11.792	0.874	7.645	0.567	9.16	0.69	1.38	0.35	91.03	4.04	0.364	–	S
2026	23 41 30.07	0.22	-59 45 48.96	0.24	3.618	0.339	3.233	0.242	3.56	0.44	1.37	0.40	160.29	23.52	0.160	–	S
2027	23 39 50.75	0.77	-54 02 26.41	0.85	1.463	0.269	0.924	0.178	6.64	1.99	5.64	1.76	6.99	132.26	0.159	–	S
2028	23 39 39.77	0.27	-53 17 42.90	0.27	6.370	0.573	4.865	0.391	5.33	0.59	3.54	0.50	51.22	23.59	0.271	–	S
2029	23 40 05.06	0.23	-55 08 29.74	0.23	10.451	0.700	5.484	0.349	9.89	0.56	0.00	0.23	40.35	3.81	0.176	–	M
2030	23 41 23.20	0.26	-59 33 24.35	0.25	5.300	0.445	3.987	0.305	5.85	0.54	2.90	0.43	126.10	13.07	0.201	–	S
2031	23 41 17.96	0.15	-59 28 08.35	0.18	84.521	4.727	40.832	2.273	20.86	0.23	6.66	0.08	66.45	0.76	0.351	-0.44	M
2032	23 40 22.92	0.38	-56 20 43.80	0.43	4.326	0.347	2.239	0.216	9.08	1.00	6.24	0.76	146.78	18.34	0.163	–	S
2033	23 41 02.79	0.72	-58 51 49.65	1.44	39.870	2.307	6.388	0.456	38.41	3.72	4.87	0.54	113.00	4.95	0.290	–	M
2034	23 39 13.87	0.26	-51 36 14.38	0.29	3.665	0.340	2.877	0.233	4.99	0.58	3.54	0.52	155.38	37.61	0.162	–	S
2035	23 40 11.54	0.84	-55 55 00.19	0.43	79.757	4.469	12.928	0.796	31.13	2.06	10.47	0.66	157.94	4.84	0.358	–	M
2036	23 41 23.58	0.82	-59 50 39.34	1.16	1.857	0.289	0.928	0.197	9.50	2.76	5.98	1.86	4.67	36.30	0.177	–	S
2037	23 39 34.66	0.14	-53 25 00.74	0.15	256.809	14.199	247.997	13.666	2.18	0.03	0.00	0.03	50.29	1.90	0.844	-0.55	S
2038	23 40 39.60	0.61	-57 34 47.69	0.57	1.108	0.350	1.134	0.207	0.00	1.39	0.00	1.32	0.00	177.82	0.198	–	S
2039	23 39 51.70	1.13	-54 42 07.38	0.57	15.121	0.858	2.228	0.221	29.00	2.75	12.05	1.07	71.28	5.78	0.218	–	S
2040	23 40 04.67	0.58	-55 35 35.90	0.53	1.536	0.310	1.284	0.195	4.90	1.41	1.51	1.09	53.20	40.74	0.176	–	S
2041	23 39 17.91	0.72	-52 18 33.21	0.92	8.449	0.882	3.675	0.583	11.37	2.20	7.30	1.53	152.33	29.03	0.508	–	S
2042	23 39 48.37	0.72	-54 35 33.17	0.98	1.941	0.339	1.162	0.225	8.35	2.31	4.69	1.61	162.76	37.75	0.201	–	S
2043	23 39 05.87	0.56	-51 21 45.85	0.76	2.202	0.412	1.606	0.266	6.36	1.68	3.50	1.33	3.13	46.70	0.237	–	S
2044	23 39 06.37	0.64	-51 25 47.69	0.73	2.165	0.349	1.400	0.230	6.78	1.64	5.34	1.51	159.96	96.09	0.201	–	S
2045	23 39 49.27	1.22	-54 49 16.26	1.20	11.442	0.658	1.395	0.188	22.08	2.93	20.92	2.73	48.42	82.13	0.207	–	S
2046	23 40 16.18	1.38	-56 31 07.50	1.05	2.581	0.256	0.832	0.172	13.37	3.23	9.74	2.41	71.04	43.00	0.158	–	S
2047	23 39 45.04	0.61	-54 31 04.83	0.79	2.255	0.320	1.321	0.212	8.13	1.83	5.31	1.37	12.14	37.30	0.185	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2048	23 39 15.00	0.57	-52 18 28.32	0.78	5.096	0.867	3.451	0.566	7.09	1.75	4.07	1.33	177.18	41.07	0.500	–	S
2049	23 40 12.16	0.25	-56 23 32.80	0.26	7.265	0.492	4.147	0.301	7.14	0.51	6.61	0.48	24.68	43.95	0.181	–	S
2050	23 38 59.39	0.51	-51 05 10.23	0.50	3.650	0.336	1.899	0.216	8.61	1.21	7.15	1.06	117.67	44.04	0.174	–	S
2051	23 39 34.59	0.81	-53 54 16.43	0.67	1.723	0.293	1.098	0.193	7.38	1.92	4.69	1.48	108.88	44.97	0.171	–	S
2052	23 40 13.10	0.87	-56 29 53.55	0.77	0.996	0.253	0.759	0.160	5.98	2.16	2.56	1.59	121.96	51.11	0.148	–	S
2053	23 39 36.96	1.36	-54 10 22.71	1.19	2.488	0.265	0.827	0.182	12.22	3.20	10.57	2.75	75.28	84.78	0.166	–	S
2054	23 39 45.57	1.27	-54 49 37.57	1.29	5.706	0.400	1.211	0.218	15.67	3.07	15.20	2.91	35.33	178.00	0.213	–	S
2055	23 38 49.54	0.76	-50 32 49.34	0.84	2.644	0.298	1.237	0.199	10.20	2.04	7.44	1.63	139.57	43.40	0.173	–	S
2056	23 39 38.45	0.21	-54 33 28.84	0.22	6.781	0.515	5.405	0.370	4.33	0.37	3.76	0.36	127.04	64.78	0.210	–	S
2057	23 40 00.46	0.71	-56 03 29.25	0.96	2.055	0.254	0.981	0.171	9.85	2.22	6.77	1.63	176.08	36.28	0.150	–	S
2058	23 39 38.70	0.85	-54 39 08.95	0.72	3.004	0.369	1.482	0.248	8.97	1.96	7.28	1.66	80.29	60.85	0.216	–	S
2059	23 40 57.95	0.41	-59 27 16.19	0.39	4.047	0.624	3.418	0.402	3.65	0.89	3.05	0.88	109.13	87.75	0.342	–	S
2060	23 39 03.04	0.14	-52 03 09.07	0.15	87.642	4.846	80.903	4.460	3.02	0.03	1.51	0.03	11.69	1.49	0.291	-0.83	S
2061	23 40 07.31	0.42	-56 37 15.28	0.43	2.522	0.313	1.791	0.206	5.35	0.99	4.76	0.91	156.24	119.18	0.169	–	S
2062	23 39 28.89	1.58	-54 09 00.73	1.34	9.395	0.683	2.151	0.213	26.90	4.81	0.00	0.69	137.99	7.90	0.178	–	M
2063	23 39 38.70	0.19	-54 48 51.43	0.19	7.118	0.531	6.413	0.413	3.26	0.29	1.89	0.27	49.78	25.24	0.209	–	S
2064	23 40 40.22	0.16	-58 37 26.31	0.17	26.539	1.677	22.141	1.319	3.55	0.20	3.43	0.19	26.46	79.70	0.486	-1.04	S
2065	23 38 38.91	0.30	-50 13 32.47	0.38	2.613	0.297	2.082	0.198	5.35	0.80	2.89	0.65	171.95	30.16	0.154	–	S
2066	23 40 09.43	0.26	-57 02 50.83	0.26	5.656	0.439	3.845	0.292	5.86	0.52	4.98	0.48	139.42	42.81	0.188	–	S
2067	23 38 58.78	0.66	-51 59 15.65	0.76	2.514	0.493	1.796	0.319	5.82	1.71	4.48	1.55	14.94	103.42	0.285	–	S
2068	23 39 38.97	0.14	-55 05 32.90	0.15	15.056	0.874	15.230	0.853	0.00	0.08	0.00	0.08	0.00	56.47	0.162	0.18	S
2069	23 39 25.24	0.72	-54 08 28.98	0.63	3.152	0.323	1.536	0.211	11.08	1.91	5.44	1.10	124.35	16.66	0.181	–	S
2070	23 38 42.84	0.88	-50 44 28.64	0.97	2.250	0.276	1.015	0.187	9.62	2.25	8.55	2.06	31.00	117.48	0.164	–	S
2071	23 39 06.06	0.41	-52 43 31.94	0.38	7.311	0.620	4.222	0.395	9.38	1.07	4.23	0.61	51.09	9.85	0.299	–	S
2072	23 38 54.10	0.16	-51 46 03.89	0.17	8.478	0.550	7.744	0.460	2.92	0.20	2.08	0.19	179.69	34.75	0.170	-0.70	S
2073	23 40 47.11	0.39	-59 19 28.73	0.18	199.085	11.068	56.167	3.123	34.07	0.88	4.80	0.13	11.03	1.25	0.460	-0.97	M
2074	23 39 53.73	0.16	-56 13 01.90	0.17	8.304	0.525	7.151	0.424	3.49	0.19	2.85	0.18	25.22	27.25	0.152	-0.79	S
2075	23 40 10.32	0.14	-57 21 19.02	0.15	107.276	5.969	95.979	5.292	9.73	0.06	1.16	0.03	65.26	0.49	0.371	-0.89	M
2076	23 40 55.42	0.84	-59 48 00.75	0.82	1.215	0.275	0.845	0.179	5.74	2.10	4.52	1.73	37.44	107.64	0.162	–	S
2077	23 39 37.85	0.22	-55 16 29.20	0.23	5.378	0.416	4.150	0.293	5.10	0.43	3.53	0.38	143.70	21.83	0.174	–	S
2078	23 38 40.19	0.23	-50 57 11.68	0.25	3.501	0.298	2.845	0.210	5.06	0.50	2.67	0.40	140.51	18.47	0.135	–	S
2079	23 38 49.65	1.96	-51 51 36.07	1.39	5.676	0.376	0.943	0.189	21.56	4.74	15.33	3.14	79.41	29.72	0.200	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2080	23 39 55.44	0.31	-56 38 50.07	0.31	3.235	0.327	2.475	0.219	5.63	0.71	2.88	0.56	44.11	18.85	0.163	–	S
2081	23 39 17.65	1.03	-54 03 26.71	1.36	4.293	0.304	1.014	0.167	19.04	3.51	10.53	1.88	28.98	17.44	0.161	–	S
2082	23 39 15.97	0.38	-53 57 51.16	0.42	6.498	0.455	2.902	0.259	10.98	1.02	7.03	0.70	142.07	12.48	0.190	–	S
2083	23 40 10.96	0.21	-57 40 33.35	0.24	6.890	0.637	6.254	0.459	0.00	0.45	0.00	0.36	0.00	13.65	0.298	–	S
2084	23 39 39.34	0.15	-55 45 00.55	0.16	17.054	1.040	16.211	0.930	2.01	0.13	1.60	0.13	161.61	57.22	0.261	-0.27	S
2085	23 39 56.21	1.12	-56 54 59.27	0.47	33.515	1.997	7.043	0.493	25.86	2.75	5.72	0.64	16.32	6.00	0.306	–	M
2086	23 39 13.76	0.72	-53 57 33.54	0.94	3.071	0.320	1.314	0.212	11.44	2.26	7.28	1.54	154.79	27.86	0.185	–	S
2087	23 39 17.83	0.64	-54 22 26.61	0.87	21.200	1.280	4.700	0.368	20.90	2.37	7.13	0.81	54.69	7.94	0.262	–	M
2088	23 38 36.26	0.54	-51 05 20.99	0.67	2.981	0.290	1.456	0.188	9.58	1.49	7.28	1.26	165.19	43.53	0.156	–	S
2089	23 38 29.39	1.18	-50 29 42.62	0.54	6.334	0.651	3.132	0.288	15.84	2.94	0.00	0.73	18.62	9.73	0.230	–	M
2090	23 39 31.35	1.44	-55 24 55.40	1.32	2.503	0.293	0.885	0.203	14.28	3.96	7.62	2.25	128.33	28.47	0.188	–	S
2091	23 40 41.45	2.28	-59 41 38.44	1.07	6.425	0.599	1.870	0.208	18.99	5.83	0.00	0.91	21.46	11.92	0.181	–	M
2092	23 39 24.92	0.25	-55 04 49.48	0.46	7.884	0.510	3.463	0.271	13.63	1.03	4.60	0.44	164.56	3.89	0.186	–	S
2093	23 39 16.84	0.60	-54 31 27.70	0.55	1.943	0.359	1.507	0.229	5.62	1.46	2.75	1.14	122.73	41.96	0.204	–	S
2094	23 40 39.92	1.45	-59 44 40.61	1.00	2.408	0.261	0.824	0.179	13.07	3.32	8.74	2.37	78.22	41.07	0.164	–	S
2095	23 38 31.55	0.87	-50 57 24.50	0.85	2.918	0.261	1.071	0.167	12.23	2.23	9.42	1.75	124.24	38.70	0.146	–	S
2096	23 40 42.67	0.14	-59 58 03.48	0.15	25.905	1.501	24.232	1.347	0.00	0.07	0.00	0.06	0.00	2.98	0.197	0.40	M
2097	23 39 14.65	0.65	-54 35 28.37	0.88	2.214	0.298	1.212	0.199	9.72	2.17	4.73	1.29	24.05	22.56	0.175	–	S
2098	23 39 53.61	0.28	-57 18 47.91	0.34	5.654	0.525	4.006	0.350	6.41	0.73	3.44	0.55	11.30	15.26	0.256	–	S
2099	23 39 01.83	0.18	-53 50 13.50	0.20	9.261	0.578	6.268	0.388	6.18	0.29	4.95	0.26	167.07	16.57	0.166	–	S
2100	23 38 23.30	0.31	-50 31 46.91	0.35	3.578	0.438	3.072	0.291	4.04	0.71	2.61	0.67	156.12	59.93	0.230	–	S
2101	23 38 24.01	0.64	-50 38 09.29	0.77	1.482	0.298	1.090	0.191	6.45	1.83	3.29	1.41	147.13	46.11	0.172	–	S
2102	23 39 13.58	0.70	-54 45 43.20	0.52	0.954	0.300	0.982	0.176	0.00	1.65	0.00	1.10	0.00	35.10	0.170	–	S
2103	23 38 21.16	0.16	-50 48 03.22	0.17	12.632	0.783	11.154	0.651	4.22	0.19	1.00	0.15	122.22	5.87	0.211	-0.66	S
2104	23 40 31.76	0.23	-59 49 35.99	0.23	4.533	0.376	3.592	0.264	4.39	0.44	3.52	0.41	28.62	36.24	0.167	–	S
2105	23 38 37.71	0.26	-52 12 28.06	0.27	6.796	0.639	5.497	0.441	4.24	0.53	3.67	0.52	38.45	78.81	0.306	–	S
2106	23 40 10.16	0.35	-58 40 25.05	0.31	5.135	0.647	4.369	0.428	4.00	0.73	2.48	0.65	91.93	52.96	0.342	–	S
2107	23 38 25.46	1.00	-51 14 25.79	1.05	4.141	0.325	1.200	0.196	14.92	2.73	10.91	2.02	133.15	33.18	0.179	–	S
2108	23 39 23.30	1.38	-55 51 14.84	1.01	2.446	0.322	1.015	0.223	12.36	3.44	6.65	2.00	60.98	28.69	0.203	–	S
2109	23 38 24.92	1.14	-51 22 43.14	0.80	8.459	0.518	1.650	0.213	20.68	2.85	13.09	1.65	105.66	14.77	0.205	–	S
2110	23 38 15.84	0.56	-50 27 11.53	0.55	3.214	0.356	1.851	0.233	8.51	1.47	5.53	1.03	52.39	25.22	0.195	–	S
2111	23 38 56.65	0.61	-53 56 22.53	0.89	1.930	0.259	1.052	0.173	9.27	2.04	5.42	1.39	171.98	29.68	0.151	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2112	23 39 37.25	0.53	-56 55 06.91	0.46	27.310	1.614	5.715	0.437	18.81	1.47	7.28	0.57	37.50	5.84	0.303	–	M
2113	23 38 26.91	0.63	-51 29 39.87	1.05	2.394	0.237	0.989	0.155	12.66	2.42	7.06	1.45	4.33	21.80	0.136	–	S
2114	23 38 27.50	0.31	-51 39 17.18	0.31	2.386	0.302	2.160	0.201	3.15	0.66	2.03	0.63	109.43	74.33	0.158	–	S
2115	23 39 33.63	0.97	-56 45 02.77	0.86	2.711	0.284	1.076	0.190	10.94	2.32	8.62	1.91	117.93	55.55	0.167	–	S
2116	23 39 13.20	0.14	-55 23 50.88	0.15	161.553	8.918	157.953	8.699	1.52	0.02	0.80	0.02	137.58	7.36	0.443	-0.31	S
2117	23 38 27.92	1.09	-51 46 32.28	1.53	3.221	0.307	0.996	0.204	15.42	3.73	9.32	2.27	23.35	28.67	0.190	–	S
2118	23 39 25.58	0.62	-56 14 37.38	0.97	1.309	0.283	0.924	0.182	7.28	2.26	2.31	1.41	1.49	31.02	0.166	–	S
2119	23 39 22.59	0.14	-56 07 00.68	0.15	65.464	3.617	58.610	3.230	0.00	0.03	0.00	0.03	0.00	179.41	0.202	-0.80	S
2120	23 39 17.51	0.60	-55 48 59.40	0.58	1.697	0.353	1.387	0.223	4.89	1.48	2.31	1.19	47.02	51.51	0.201	–	S
2121	23 40 07.24	0.45	-59 00 32.72	0.39	2.534	0.443	2.258	0.281	3.80	1.01	1.27	0.85	105.71	51.65	0.246	–	S
2122	23 39 16.77	0.54	-55 53 25.11	0.59	3.248	0.339	1.721	0.221	8.50	1.41	6.46	1.14	29.87	35.90	0.185	–	S
2123	23 39 15.28	1.19	-55 48 32.50	0.92	2.452	0.319	1.058	0.219	10.66	2.79	7.67	2.10	74.50	47.82	0.196	–	S
2124	23 40 06.18	0.52	-59 01 34.57	0.44	3.036	0.443	2.240	0.288	5.86	1.18	3.37	0.95	115.17	37.44	0.246	–	S
2125	23 39 06.73	0.25	-55 13 02.71	0.25	4.002	0.363	3.264	0.253	3.84	0.49	3.76	0.48	50.68	178.13	0.171	–	S
2126	23 39 09.46	0.42	-55 39 12.79	0.40	3.173	0.438	2.504	0.286	4.64	0.95	3.54	0.85	56.73	70.16	0.239	–	S
2127	23 39 30.58	0.49	-57 05 19.39	0.55	2.007	0.341	1.550	0.219	5.08	1.28	3.38	1.08	164.47	58.14	0.192	–	S
2128	23 38 58.24	0.69	-54 50 08.16	0.65	1.562	0.321	1.176	0.206	5.19	1.64	3.96	1.44	118.69	109.38	0.185	–	S
2129	23 38 42.72	1.87	-53 41 32.93	0.75	3.345	0.402	0.911	0.179	0.00	4.70	0.00	0.50	0.00	9.73	0.172	–	M
2130	23 39 28.21	0.19	-57 02 48.88	0.20	6.685	0.516	5.905	0.391	3.04	0.32	2.69	0.30	158.41	96.40	0.212	–	S
2131	23 38 31.78	0.36	-52 51 11.54	0.36	6.435	0.631	4.330	0.416	6.28	0.82	5.02	0.74	125.38	45.92	0.318	–	S
2132	23 38 02.63	0.61	-50 14 17.29	0.65	2.416	0.295	1.376	0.196	7.19	1.49	7.18	1.38	44.99	178.35	0.166	–	S
2133	23 38 17.43	0.33	-51 39 28.41	0.35	2.749	0.289	2.042	0.192	5.61	0.78	3.97	0.67	135.09	37.91	0.147	–	S
2134	23 38 17.14	0.77	-51 37 33.82	0.72	1.408	0.255	0.931	0.167	6.29	1.80	5.38	1.64	79.02	103.88	0.148	–	S
2135	23 38 13.85	0.67	-51 22 19.10	0.70	5.152	0.385	1.812	0.223	13.54	1.88	8.88	1.23	132.05	18.86	0.189	–	S
2136	23 39 03.59	0.19	-55 34 00.99	0.19	18.548	1.123	11.959	0.726	8.68	0.34	2.63	0.19	125.66	1.89	0.291	-1.13	S
2137	23 39 26.72	0.61	-57 03 14.39	0.83	2.169	0.362	1.371	0.239	7.49	1.93	4.43	1.40	173.06	37.18	0.211	–	S
2138	23 38 46.71	0.16	-54 20 34.55	0.18	9.223	0.605	8.255	0.495	3.50	0.22	1.80	0.19	3.51	14.33	0.193	-0.19	S
2139	23 38 54.70	0.15	-55 01 18.18	0.16	22.876	1.322	17.994	1.021	4.77	0.13	3.52	0.12	105.73	7.70	0.240	-1.14	S
2140	23 39 48.38	0.86	-58 37 59.80	0.91	5.110	0.591	2.214	0.400	9.26	2.19	8.65	1.92	176.81	116.33	0.351	–	S
2141	23 38 54.59	1.10	-55 06 27.43	0.70	1.184	0.272	0.821	0.175	7.93	2.64	1.73	1.49	70.96	29.10	0.162	–	S
2142	23 39 15.12	1.02	-56 36 44.12	0.83	1.895	0.255	0.907	0.173	10.21	2.50	6.39	1.75	116.82	35.74	0.154	–	S
2143	23 39 18.89	0.14	-57 01 00.68	0.15	26.609	1.514	23.671	1.323	2.99	0.08	2.58	0.08	92.32	28.27	0.226	0.25	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2144	23 38 01.44	0.21	-50 50 01.26	0.22	7.020	0.509	5.341	0.360	6.01	0.43	2.95	0.31	127.29	9.66	0.198	–	S
2145	23 37 58.69	0.75	-50 37 11.66	0.89	1.675	0.309	1.075	0.204	7.57	2.10	4.70	1.66	145.39	51.33	0.182	–	S
2146	23 38 47.32	0.82	-54 50 10.19	0.77	1.179	0.328	0.960	0.205	4.72	2.00	2.80	1.68	121.13	97.12	0.190	–	S
2147	23 38 32.76	0.81	-53 42 29.09	0.66	1.355	0.287	0.991	0.185	5.94	1.87	3.68	1.51	85.36	59.56	0.167	–	S
2148	23 39 57.93	0.14	-59 37 18.31	0.15	42.179	2.343	41.048	2.266	1.66	0.04	0.75	0.04	150.42	98.38	0.189	0.14	S
2149	23 39 28.01	0.48	-57 51 39.24	0.47	4.357	0.551	2.959	0.361	6.59	1.18	4.09	0.92	42.48	30.03	0.302	–	S
2150	23 37 54.06	0.76	-50 25 21.31	0.73	1.489	0.350	1.161	0.222	5.25	1.81	3.38	1.61	114.19	78.43	0.202	–	S
2151	23 39 54.20	0.43	-59 29 26.80	0.33	2.173	0.375	2.069	0.237	0.00	0.91	0.00	0.70	0.00	26.88	0.206	–	S
2152	23 38 40.44	0.20	-54 36 53.22	0.20	9.185	0.614	6.461	0.420	5.70	0.35	4.68	0.32	75.88	22.10	0.211	–	S
2153	23 39 33.78	0.70	-58 32 40.33	0.78	2.757	0.685	2.162	0.433	4.84	1.89	3.25	1.53	168.78	89.34	0.397	–	S
2154	23 39 32.60	0.20	-58 34 22.23	0.20	11.838	0.943	10.597	0.712	3.09	0.33	2.23	0.31	134.30	47.41	0.398	–	S
2155	23 38 38.06	0.80	-54 47 14.39	0.82	1.385	0.375	1.096	0.236	4.22	1.90	4.01	1.85	14.94	178.23	0.218	–	S
2156	23 38 56.77	0.15	-56 15 10.77	0.16	9.275	0.578	8.767	0.508	2.51	0.15	1.02	0.14	52.27	17.07	0.158	-0.23	S
2157	23 37 57.25	0.97	-51 22 44.04	0.87	1.161	0.245	0.767	0.160	8.20	2.60	3.12	1.58	123.37	32.45	0.146	–	S
2158	23 38 37.96	0.14	-54 58 41.76	0.15	84.838	4.703	74.144	4.093	3.75	0.04	2.18	0.04	170.20	1.42	0.345	-1.00	S
2159	23 39 01.09	0.14	-56 44 21.22	0.15	32.246	1.802	31.444	1.740	1.81	0.05	0.00	0.05	25.08	7.17	0.186	-0.68	S
2160	23 39 43.50	0.21	-59 25 18.90	0.22	4.325	0.416	4.250	0.306	0.00	0.39	0.00	0.35	0.00	23.81	0.197	–	S
2161	23 38 27.75	0.55	-54 16 32.37	0.26	18.333	1.144	5.284	0.378	15.66	1.26	4.26	0.45	168.62	5.47	0.242	–	M
2162	23 39 45.92	0.42	-59 35 51.79	0.47	1.993	0.345	1.691	0.220	4.15	1.09	2.12	0.91	10.84	49.86	0.192	–	S
2163	23 39 37.26	0.27	-59 11 56.76	0.25	5.288	0.494	4.288	0.341	4.78	0.54	2.63	0.46	117.10	22.90	0.236	–	S
2164	23 38 49.69	0.73	-56 05 04.43	0.76	2.146	0.316	1.235	0.211	7.84	1.90	5.77	1.52	36.49	50.77	0.185	–	S
2165	23 37 40.55	0.15	-50 12 07.97	0.15	19.770	1.171	18.210	1.018	0.00	0.10	0.00	0.07	0.00	2.39	0.184	0.04	M
2166	23 37 37.92	0.14	-50 05 50.50	0.16	15.383	0.942	13.382	0.759	0.00	0.16	0.00	0.08	0.00	2.09	0.184	0.73	M
2167	23 38 45.38	0.38	-55 55 20.40	0.44	2.443	0.302	1.799	0.198	5.82	0.99	3.54	0.79	19.71	30.47	0.162	–	S
2168	23 37 56.83	0.81	-51 52 08.85	0.82	3.487	0.482	1.847	0.325	8.42	1.97	6.97	1.78	126.60	82.56	0.284	–	S
2169	23 38 12.04	0.16	-53 17 56.33	0.16	20.758	1.282	18.242	1.063	3.73	0.18	2.05	0.15	76.22	10.15	0.341	-0.61	S
2170	23 37 41.14	2.20	-50 32 27.22	1.20	6.953	0.469	1.215	0.243	23.62	5.43	13.06	2.64	82.90	20.33	0.258	–	S
2171	23 38 39.69	0.26	-55 46 37.01	0.30	2.970	0.389	2.913	0.260	0.00	0.61	0.00	0.53	0.00	33.79	0.204	–	S
2172	23 39 24.18	0.34	-58 42 08.23	0.36	5.071	0.552	3.726	0.366	5.53	0.80	3.79	0.69	151.40	32.73	0.286	–	S
2173	23 38 05.33	0.44	-53 04 51.14	0.76	25.490	1.492	4.196	0.367	17.93	1.80	9.16	0.89	73.85	9.54	0.285	–	M
2174	23 37 39.94	0.68	-50 30 49.17	1.08	2.558	0.461	1.632	0.300	10.03	2.70	1.14	1.22	152.22	19.29	0.275	–	S
2175	23 38 19.27	0.67	-54 10 28.44	0.96	3.910	0.315	1.326	0.192	13.57	2.24	9.04	1.53	167.84	23.69	0.169	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2176	23 38 20.81	0.44	-54 21 14.03	0.38	2.109	0.328	1.814	0.211	4.83	1.03	0.00	0.77	114.00	27.03	0.180	–	S
2177	23 38 25.90	0.18	-54 48 34.20	0.23	14.249	0.863	7.987	0.504	9.58	0.43	4.44	0.25	11.73	3.08	0.230	–	S
2178	23 38 47.64	1.19	-56 28 49.74	1.28	3.373	0.258	0.820	0.154	15.03	3.12	12.99	2.66	151.28	70.22	0.146	–	S
2179	23 37 51.47	0.19	-51 53 08.10	0.20	25.661	1.607	15.497	0.913	11.14	0.40	2.17	0.17	128.80	2.68	0.327	-0.93	M
2180	23 38 28.54	0.65	-55 05 59.93	0.73	2.722	0.313	1.385	0.207	9.02	1.76	6.67	1.38	28.35	38.97	0.178	–	S
2181	23 38 20.37	0.49	-54 30 19.32	0.33	8.851	0.660	3.155	0.269	9.41	1.12	4.82	0.69	177.20	14.21	0.205	–	M
2182	23 38 04.84	0.32	-53 23 34.52	0.27	5.164	0.562	4.339	0.380	4.80	0.68	1.65	0.53	80.92	20.36	0.285	–	S
2183	23 39 00.71	0.63	-57 30 35.18	0.68	1.043	0.295	0.950	0.180	3.37	1.64	0.95	1.36	18.78	94.20	0.168	–	S
2184	23 39 02.06	0.48	-57 38 32.72	0.45	5.887	0.471	2.833	0.288	10.76	1.24	5.66	0.77	130.69	11.71	0.226	–	S
2185	23 38 36.74	0.68	-55 49 55.56	1.03	2.436	0.308	1.203	0.206	11.16	2.53	4.86	1.33	20.36	19.38	0.184	–	S
2186	23 37 31.39	0.64	-50 00 22.67	0.58	2.581	0.318	1.501	0.210	7.86	1.56	6.09	1.26	68.78	41.61	0.179	–	S
2187	23 38 39.21	0.92	-56 06 34.75	1.85	5.179	0.452	0.885	0.189	13.36	4.69	0.00	1.19	111.47	17.23	0.183	–	M
2188	23 38 48.54	0.41	-56 45 54.41	0.41	2.950	0.336	2.028	0.221	5.62	0.93	5.06	0.87	134.17	133.32	0.179	–	S
2189	23 39 33.91	2.84	-59 41 47.34	1.01	6.345	0.462	0.865	0.181	19.34	7.02	0.00	0.97	15.87	13.15	0.174	–	M
2190	23 38 16.34	0.15	-54 19 26.26	0.15	19.762	1.136	17.948	1.006	2.77	0.09	2.32	0.09	104.19	26.43	0.192	0.22	S
2191	23 38 30.55	0.82	-55 30 29.27	0.90	2.644	0.310	1.196	0.209	10.28	2.25	7.30	1.71	143.46	40.49	0.183	–	S
2192	23 37 38.97	0.16	-51 00 27.75	0.17	14.637	0.868	10.660	0.622	5.48	0.20	4.49	0.17	68.05	10.57	0.195	-0.93	S
2193	23 37 51.31	1.05	-52 14 52.75	1.37	6.097	0.817	2.508	0.568	11.37	3.18	8.19	2.45	15.56	54.20	0.512	–	S
2194	23 39 28.62	0.45	-59 32 55.49	0.72	3.053	0.390	1.253	0.168	0.00	1.86	0.00	0.56	0.00	10.08	0.154	–	M
2195	23 39 32.68	1.00	-59 44 59.84	1.24	2.068	0.296	0.937	0.203	11.37	3.23	5.71	1.83	28.17	26.72	0.185	–	S
2196	23 39 03.38	1.24	-57 58 50.48	0.89	9.888	0.737	2.673	0.425	17.58	3.08	8.96	1.65	117.57	16.38	0.399	–	S
2197	23 39 01.42	0.59	-57 48 59.54	0.71	2.048	0.410	1.533	0.263	5.71	1.68	3.19	1.30	160.05	48.77	0.236	–	S
2198	23 39 30.68	0.49	-59 45 40.58	0.32	7.171	0.476	2.863	0.253	12.36	1.05	7.01	0.69	88.36	9.44	0.186	–	S
2199	23 37 58.97	0.33	-53 02 20.29	0.39	3.430	0.452	2.902	0.296	5.28	0.90	0.00	0.63	146.61	19.61	0.242	–	S
2200	23 37 33.97	0.54	-50 36 13.66	0.58	1.643	0.397	1.532	0.243	2.59	1.34	1.79	1.21	131.41	178.45	0.225	–	S
2201	23 37 30.07	1.35	-50 26 29.79	2.50	18.558	1.034	1.222	0.172	43.72	6.00	21.76	2.88	14.20	12.78	0.244	–	S
2202	23 39 18.39	0.18	-59 06 20.02	0.19	7.344	0.561	6.814	0.440	2.62	0.28	1.65	0.27	141.42	42.41	0.227	–	S
2203	23 38 19.95	0.53	-54 59 50.33	0.63	2.135	0.422	1.708	0.268	4.95	1.44	2.90	1.21	169.02	61.42	0.240	–	S
2204	23 39 10.55	0.66	-58 39 23.98	0.82	8.584	0.720	3.420	0.443	14.33	2.20	5.24	0.96	143.63	10.25	0.389	–	S
2205	23 37 54.81	0.73	-52 57 43.93	0.55	2.689	0.495	1.969	0.319	6.37	1.70	3.09	1.23	89.15	36.44	0.284	–	S
2206	23 37 32.74	1.28	-50 56 36.48	2.04	4.661	0.317	0.826	0.167	22.00	4.70	14.05	3.06	175.09	29.94	0.174	–	S
2207	23 38 00.81	1.23	-53 39 41.19	0.92	2.423	0.302	1.011	0.207	11.18	2.90	7.91	2.10	77.42	42.19	0.186	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2208	23 38 19.36	1.65	-55 13 19.98	0.39	3.389	0.371	0.843	0.161	0.00	3.88	0.00	0.83	0.00	13.52	0.154	–	M
2209	23 38 05.75	0.33	-54 06 44.27	0.34	2.717	0.301	2.103	0.200	5.23	0.77	3.37	0.65	131.76	34.32	0.155	–	S
2210	23 38 03.36	0.73	-53 53 14.56	1.08	1.265	0.227	0.743	0.152	8.64	2.50	4.78	1.71	172.79	38.71	0.136	–	S
2211	23 39 23.53	0.22	-59 42 00.84	0.22	6.613	0.468	4.624	0.317	5.28	0.40	4.93	0.37	34.46	57.09	0.178	–	S
2212	23 37 56.45	0.25	-53 22 00.74	0.26	7.303	0.592	5.318	0.403	5.14	0.50	4.74	0.49	16.63	105.33	0.262	–	S
2213	23 39 01.44	0.25	-58 23 23.84	0.26	7.515	0.841	7.062	0.580	2.32	0.51	1.60	0.48	144.89	113.44	0.425	–	S
2214	23 38 32.37	0.68	-56 23 26.54	0.98	1.201	0.238	0.789	0.156	7.80	2.34	3.28	1.48	14.28	31.73	0.141	–	S
2215	23 38 02.98	0.26	-54 08 18.84	0.31	4.086	0.345	2.844	0.230	6.60	0.65	3.92	0.50	160.58	16.26	0.159	–	S
2216	23 38 26.34	0.95	-56 00 35.96	1.37	3.747	0.313	1.059	0.197	15.16	3.21	10.36	2.19	171.57	30.06	0.183	–	S
2217	23 37 38.95	0.21	-51 57 23.22	0.24	11.915	0.955	9.705	0.684	4.90	0.44	2.76	0.36	152.56	18.60	0.411	–	S
2218	23 37 55.37	0.26	-53 31 56.14	0.26	6.990	0.551	4.922	0.371	5.58	0.51	4.86	0.48	56.86	44.29	0.238	–	S
2219	23 39 19.31	0.29	-59 38 34.52	0.29	2.928	0.326	2.483	0.220	3.85	0.62	2.69	0.56	136.23	53.74	0.167	–	S
2220	23 38 56.75	0.21	-58 20 05.99	0.52	44.281	2.717	19.924	1.186	22.07	1.20	3.43	0.27	100.45	2.94	0.453	-0.95	M
2221	23 38 41.70	0.43	-57 20 06.08	0.74	2.298	0.258	1.271	0.169	9.73	1.70	4.20	0.96	176.89	15.42	0.144	–	S
2222	23 37 52.69	0.47	-53 30 01.53	0.38	4.771	0.498	3.045	0.327	7.24	1.06	4.81	0.81	79.55	25.35	0.261	–	S
2223	23 37 21.24	0.14	-50 33 27.17	0.15	283.744	15.690	278.190	15.329	1.63	0.03	0.46	0.03	176.53	6.87	0.937	-0.40	S
2224	23 37 21.32	1.48	-50 32 56.73	1.59	10.822	0.712	1.860	0.352	18.76	3.73	17.44	3.47	172.34	178.49	0.364	–	S
2225	23 39 00.35	0.26	-58 49 46.78	0.35	38.996	2.248	9.710	0.653	16.16	0.83	6.42	0.36	116.45	4.19	0.376	–	M
2226	23 37 43.48	0.76	-52 48 03.04	0.72	6.724	0.837	3.535	0.558	9.31	1.97	6.04	1.39	51.31	30.98	0.484	–	S
2227	23 38 00.23	0.43	-54 19 02.48	0.53	1.945	0.328	1.583	0.210	4.89	1.18	2.59	0.98	0.07	46.75	0.183	–	S
2228	23 38 54.02	0.52	-58 22 26.13	0.55	4.232	0.708	3.179	0.457	5.17	1.31	3.80	1.11	150.36	70.56	0.400	–	S
2229	23 39 16.21	0.17	-59 48 45.87	0.17	8.006	0.525	6.928	0.419	3.61	0.21	2.50	0.21	113.89	22.50	0.168	-0.35	S
2230	23 37 54.79	0.64	-53 54 34.13	0.79	1.269	0.236	0.880	0.153	7.22	1.93	3.22	1.32	148.66	33.36	0.137	–	S
2231	23 37 44.96	0.56	-53 02 34.92	0.49	3.316	0.466	2.297	0.305	6.30	1.30	4.38	1.06	69.82	43.14	0.260	–	S
2232	23 37 45.24	0.28	-53 09 26.58	0.26	4.763	0.627	4.897	0.422	0.00	0.57	0.00	0.50	0.00	37.85	0.328	–	S
2233	23 39 05.14	0.33	-59 18 28.00	0.23	10.746	0.683	5.103	0.372	10.92	0.68	5.64	0.43	86.63	5.79	0.228	–	S
2234	23 38 07.75	0.50	-55 12 16.21	0.54	2.335	0.280	1.449	0.184	7.03	1.26	5.42	1.07	31.56	46.40	0.154	–	S
2235	23 37 47.09	0.50	-53 28 08.50	1.41	7.099	0.707	1.548	0.294	0.00	3.31	0.00	1.14	0.00	17.60	0.281	–	M
2236	23 38 36.09	0.88	-57 21 52.63	1.02	2.533	0.310	1.119	0.210	10.86	2.57	6.92	1.77	146.54	32.91	0.187	–	S
2237	23 37 50.38	0.43	-53 44 47.06	0.49	3.212	0.310	1.849	0.201	8.46	1.16	5.37	0.85	145.00	21.96	0.160	–	S
2238	23 38 32.58	0.70	-57 16 46.55	0.68	2.247	0.308	1.282	0.205	7.84	1.74	5.86	1.42	132.73	53.86	0.178	–	S
2239	23 37 26.67	0.91	-51 45 40.64	1.69	10.247	0.663	1.937	0.316	22.49	3.92	12.36	2.13	175.77	18.11	0.320	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2240	23 37 13.58	0.19	-50 27 36.95	0.21	9.608	0.714	7.921	0.526	4.41	0.35	3.19	0.32	153.98	31.61	0.283	–	S
2241	23 37 24.72	0.15	-51 45 56.00	0.16	24.530	1.481	23.252	1.328	2.09	0.13	1.74	0.13	9.58	170.44	0.355	-0.53	S
2242	23 38 57.70	0.28	-59 18 31.20	0.35	3.900	0.429	3.097	0.286	5.22	0.74	2.25	0.58	175.63	19.36	0.220	–	S
2243	23 37 41.89	0.36	-53 34 27.57	0.33	4.593	0.464	3.261	0.307	6.39	0.84	3.79	0.64	118.87	22.00	0.235	–	S
2244	23 37 39.56	2.04	-53 21 43.49	0.97	5.592	0.415	1.225	0.241	21.51	4.89	10.12	2.18	94.79	18.34	0.244	–	S
2245	23 37 07.01	2.20	-50 10 19.41	1.08	5.594	0.404	0.715	0.160	17.51	5.65	0.00	1.06	22.94	14.48	0.156	–	M
2246	23 37 52.22	0.86	-54 35 14.73	0.95	2.231	0.314	1.110	0.213	8.68	2.23	7.45	1.97	160.33	109.34	0.188	–	S
2247	23 38 07.47	0.91	-56 03 06.96	1.36	2.241	0.270	0.892	0.185	12.60	3.29	7.06	1.94	16.51	27.68	0.169	–	S
2248	23 38 49.68	0.66	-59 08 00.24	0.70	3.664	0.405	1.802	0.268	9.23	1.75	6.66	1.36	145.79	35.28	0.230	–	S
2249	23 38 24.93	0.80	-57 30 34.41	0.47	6.913	0.452	2.023	0.223	16.04	1.81	8.96	1.07	94.89	11.53	0.189	–	S
2250	23 37 23.17	0.14	-52 16 20.01	0.15	493.273	27.292	477.589	26.324	1.98	0.03	0.60	0.03	83.52	3.97	1.718	0.00	S
2251	23 38 03.39	1.75	-55 53 02.82	0.57	35.035	1.985	4.229	0.385	30.78	4.11	10.31	1.29	177.92	9.58	0.307	–	M
2252	23 38 16.31	1.42	-57 01 22.89	1.12	8.439	0.509	1.367	0.196	25.23	3.78	12.26	1.80	52.77	12.44	0.206	–	S
2253	23 37 54.32	0.71	-55 13 58.08	0.70	1.979	0.257	1.080	0.172	7.68	1.70	6.88	1.53	50.37	111.57	0.148	–	S
2254	23 38 12.32	0.88	-56 41 08.50	0.69	1.934	0.269	1.034	0.181	8.55	2.01	6.24	1.61	90.85	52.59	0.158	–	S
2255	23 37 14.34	0.66	-51 47 09.45	0.73	54.814	3.153	6.778	0.632	16.25	1.69	15.02	1.51	103.71	48.22	0.511	–	M
2256	23 36 59.92	0.16	-50 16 06.36	0.21	13.204	0.842	9.170	0.535	9.69	0.36	0.00	0.15	75.31	2.56	0.179	-0.04	M
2257	23 37 57.70	1.05	-55 53 06.26	1.18	25.646	1.434	2.424	0.271	28.99	3.01	20.80	2.11	33.08	14.81	0.313	–	S
2258	23 38 29.43	0.50	-58 07 39.34	0.61	2.908	0.505	2.183	0.325	5.67	1.42	3.14	1.11	165.38	40.97	0.287	–	S
2259	23 38 13.23	0.94	-57 01 31.03	0.96	7.209	0.460	1.540	0.213	16.98	2.46	13.46	1.93	37.67	29.05	0.201	–	S
2260	23 37 42.28	1.09	-54 26 44.90	0.59	3.454	0.457	1.213	0.198	0.00	2.82	0.00	0.60	0.00	10.46	0.187	–	M
2261	23 38 14.67	1.61	-57 11 41.95	0.88	4.123	0.453	1.234	0.195	15.48	4.27	0.00	0.51	26.21	8.31	0.183	–	M
2262	23 37 03.35	0.28	-50 49 06.98	0.20	18.160	1.140	9.958	0.595	13.01	0.61	2.49	0.23	20.70	3.28	0.232	-0.27	M
2263	23 38 26.27	0.22	-58 03 16.60	0.24	6.840	0.667	6.255	0.475	3.19	0.45	1.17	0.41	11.09	30.44	0.321	–	S
2264	23 38 00.54	1.47	-56 11 11.33	0.69	3.165	0.324	0.746	0.143	11.50	3.66	0.00	0.97	157.51	15.04	0.137	–	M
2265	23 37 24.55	0.18	-53 01 44.04	0.18	12.390	0.851	10.747	0.667	3.62	0.26	2.63	0.24	79.11	25.12	0.299	–	S
2266	23 37 51.54	0.32	-55 34 44.80	0.30	3.410	0.355	2.671	0.239	5.00	0.68	3.28	0.59	64.54	32.17	0.179	–	S
2267	23 37 04.18	0.16	-51 09 10.63	0.16	30.622	1.746	18.824	1.062	8.36	0.17	3.74	0.11	165.47	2.61	0.238	-0.93	M
2268	23 37 04.29	0.28	-51 08 24.69	0.23	12.108	0.806	5.222	0.368	7.76	0.60	2.07	0.36	154.08	8.37	0.230	–	M
2269	23 37 01.53	0.20	-50 51 38.13	0.20	7.001	0.489	5.502	0.356	4.72	0.34	3.80	0.30	91.28	23.83	0.179	–	S
2270	23 37 48.14	0.16	-55 27 11.89	0.17	10.137	0.651	9.042	0.536	3.08	0.19	2.43	0.18	33.93	32.42	0.196	-1.00	S
2271	23 37 55.68	1.46	-56 00 51.73	0.50	6.501	0.502	1.178	0.188	15.52	3.45	2.74	1.05	171.63	13.12	0.176	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2272	23 37 18.27	0.53	-52 38 23.05	0.51	5.471	0.948	4.333	0.608	4.66	1.23	3.60	1.13	68.18	89.38	0.533	–	S
2273	23 37 54.95	0.59	-56 02 01.51	0.54	2.229	0.295	1.398	0.195	6.85	1.39	5.38	1.19	58.96	58.61	0.166	–	S
2274	23 37 38.51	0.59	-54 37 33.79	0.68	1.965	0.311	1.297	0.204	6.44	1.56	5.05	1.36	178.96	76.50	0.178	–	S
2275	23 36 54.94	1.32	-50 32 04.31	0.77	1.345	0.420	1.065	0.258	0.00	3.38	0.00	1.41	0.00	24.76	0.248	–	S
2276	23 37 15.12	1.04	-52 30 29.21	0.73	5.003	0.610	2.347	0.410	11.24	2.57	6.05	1.51	108.19	24.08	0.364	–	S
2277	23 37 21.27	0.31	-53 09 42.69	0.33	5.788	0.656	4.765	0.439	4.51	0.70	2.90	0.62	140.01	42.03	0.339	–	S
2278	23 37 33.23	0.48	-54 19 22.04	0.58	2.846	0.316	1.701	0.206	8.98	1.44	4.03	0.87	145.55	16.46	0.172	–	S
2279	23 37 25.51	0.53	-53 42 03.97	0.51	3.643	0.380	2.039	0.249	7.47	1.22	6.84	1.13	112.26	114.69	0.204	–	S
2280	23 36 52.72	0.68	-50 28 14.31	0.69	5.279	0.478	2.348	0.303	12.43	1.99	6.13	1.05	130.93	14.86	0.258	–	S
2281	23 38 31.95	0.35	-59 06 14.87	0.38	3.701	0.424	2.738	0.280	5.50	0.85	3.64	0.72	157.94	32.07	0.223	–	S
2282	23 37 34.73	0.44	-54 46 20.03	0.40	2.378	0.315	1.809	0.206	5.46	1.01	3.37	0.83	60.31	36.77	0.171	–	S
2283	23 36 54.91	1.31	-50 47 12.40	1.03	2.519	0.345	1.092	0.238	11.60	3.30	7.22	2.11	111.30	35.54	0.215	–	S
2284	23 38 05.85	0.18	-57 25 51.06	0.16	42.619	2.401	19.086	1.084	13.45	0.26	5.93	0.12	179.76	1.65	0.269	-0.74	M
2285	23 38 02.07	0.77	-57 04 56.44	0.74	1.164	0.290	0.918	0.183	5.50	1.96	2.32	1.48	131.37	53.19	0.168	–	S
2286	23 37 43.74	0.85	-55 40 24.08	1.40	3.598	0.316	1.121	0.203	15.88	3.37	8.26	1.79	161.43	19.97	0.188	–	S
2287	23 36 58.93	1.89	-51 27 13.89	0.99	7.387	0.589	1.931	0.231	20.54	4.91	0.00	0.92	24.50	11.32	0.205	–	M
2288	23 38 22.24	0.21	-58 48 49.87	0.25	67.705	3.875	19.904	1.252	11.29	0.48	7.80	0.35	92.43	7.87	0.608	–	M
2289	23 38 27.94	0.83	-59 08 02.43	0.87	2.364	0.356	1.258	0.241	7.64	2.10	7.00	1.84	16.66	123.20	0.212	–	S
2290	23 36 56.85	1.82	-51 25 29.78	0.91	7.441	0.465	1.267	0.203	24.68	4.44	12.67	2.02	89.31	14.87	0.214	–	S
2291	23 36 56.90	1.51	-51 25 10.36	0.90	3.433	0.343	1.194	0.228	15.87	3.84	6.96	1.69	107.91	18.51	0.213	–	S
2292	23 37 48.11	1.29	-56 33 23.92	2.32	48.527	2.706	2.818	0.298	42.20	5.98	13.11	1.74	62.83	10.47	0.254	–	M
2293	23 37 07.10	0.14	-52 36 44.60	0.15	86.392	4.824	80.433	4.451	3.05	0.06	0.76	0.05	49.11	2.60	0.483	-0.68	S
2294	23 37 48.62	1.54	-56 23 20.38	1.42	2.257	0.218	0.696	0.145	17.94	4.52	6.79	1.84	130.71	18.16	0.141	–	S
2295	23 38 19.72	0.18	-58 48 18.85	0.18	57.183	3.410	30.265	1.797	7.20	0.29	4.63	0.22	138.39	7.14	0.678	0.08	M
2296	23 37 18.00	1.02	-53 49 38.18	0.88	1.167	0.248	0.751	0.163	8.22	2.67	3.48	1.66	122.64	35.24	0.148	–	S
2297	23 38 15.61	0.16	-58 47 34.59	0.18	114.125	6.473	51.513	2.902	12.91	0.25	7.95	0.16	118.58	2.67	0.627	-1.02	M
2298	23 38 18.22	0.63	-58 51 17.68	0.58	3.704	0.647	2.654	0.420	5.51	1.49	4.32	1.26	55.94	93.46	0.370	–	S
2299	23 38 01.44	0.27	-57 56 57.81	0.29	4.305	0.625	4.494	0.411	0.00	0.59	0.00	0.53	0.00	73.92	0.333	–	S
2300	23 37 45.88	0.23	-56 36 45.88	0.46	28.339	1.669	6.961	0.473	16.40	1.02	6.51	0.43	92.63	5.01	0.277	–	M
2301	23 37 10.65	0.98	-53 24 23.53	1.17	4.640	0.464	1.629	0.310	12.10	2.70	9.92	2.29	13.79	64.57	0.279	–	S
2302	23 37 22.12	0.49	-54 41 20.30	0.62	2.177	0.358	1.605	0.231	6.14	1.43	3.18	1.08	17.16	35.51	0.203	–	S
2303	23 38 12.90	2.04	-58 54 26.47	1.81	16.458	0.925	1.188	0.190	33.16	5.14	23.66	3.74	49.95	23.98	0.262	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2304	23 38 15.91	0.21	-59 10 34.03	0.24	19.028	1.148	7.459	0.478	10.06	0.52	4.11	0.28	53.39	4.81	0.245	–	M
2305	23 37 43.54	0.56	-56 47 14.49	0.58	1.833	0.279	1.263	0.182	6.72	1.48	3.72	1.09	38.99	32.19	0.158	–	S
2306	23 37 48.89	1.58	-57 18 44.59	1.20	14.484	0.841	1.813	0.261	28.00	4.04	15.18	2.17	55.91	13.90	0.293	–	S
2307	23 37 40.18	0.30	-56 44 06.83	0.30	2.206	0.305	2.132	0.201	2.09	0.65	0.23	0.59	151.42	93.38	0.162	–	S
2308	23 37 24.71	0.82	-55 26 00.83	0.85	2.509	0.294	1.151	0.198	9.48	2.09	7.85	1.76	37.39	63.67	0.172	–	S
2309	23 38 23.14	1.28	-59 59 45.44	0.59	5.740	0.419	1.683	0.235	19.08	2.95	6.49	1.15	105.26	10.26	0.220	–	S
2310	23 36 57.46	0.35	-53 13 25.94	0.21	14.836	1.017	8.720	0.627	10.84	0.77	1.13	0.31	78.90	3.41	0.390	–	S
2311	23 37 41.54	0.82	-57 12 32.83	1.10	2.293	0.280	0.991	0.191	10.61	2.60	7.49	1.88	6.32	39.17	0.170	–	S
2312	23 36 50.50	0.40	-52 30 37.48	0.50	5.739	0.835	4.509	0.540	6.05	1.17	1.85	0.81	150.83	23.77	0.460	–	S
2313	23 36 38.32	0.52	-51 11 56.27	0.55	2.004	0.329	1.520	0.213	5.01	1.28	4.25	1.15	139.14	156.12	0.185	–	S
2314	23 37 37.58	0.92	-56 59 13.61	0.96	1.632	0.308	0.955	0.207	7.73	2.44	5.57	1.92	141.86	68.04	0.185	–	S
2315	23 37 01.87	1.02	-53 46 59.96	1.10	2.322	0.272	0.931	0.186	10.83	2.67	8.90	2.25	34.51	68.10	0.166	–	S
2316	23 37 06.14	0.34	-54 16 38.07	0.50	2.326	0.290	1.713	0.190	6.76	1.11	2.34	0.73	175.12	18.15	0.157	–	S
2317	23 37 38.04	0.28	-57 18 52.38	0.24	12.532	0.817	6.874	0.483	9.95	0.62	4.21	0.35	56.41	4.66	0.283	–	S
2318	23 36 55.71	0.15	-53 18 28.31	0.16	30.188	1.775	26.275	1.494	3.59	0.13	2.58	0.12	113.13	12.80	0.367	-0.55	S
2319	23 37 45.40	0.14	-58 08 14.31	0.15	116.529	6.458	110.211	6.072	3.70	0.03	0.00	0.02	111.80	1.35	0.348	-0.35	M
2320	23 37 57.29	0.55	-59 10 50.81	0.35	3.768	0.579	1.923	0.258	0.00	1.36	0.00	0.54	0.00	12.55	0.235	–	M
2321	23 37 15.91	0.15	-55 54 56.64	0.16	15.718	0.930	13.241	0.758	3.84	0.14	3.00	0.13	11.07	14.60	0.201	-0.49	S
2322	23 36 58.01	1.22	-54 13 10.55	0.92	1.358	0.208	0.654	0.143	9.96	2.89	6.70	2.07	73.96	45.44	0.128	–	S
2323	23 36 55.73	0.74	-53 59 55.41	0.69	1.465	0.229	0.910	0.151	7.88	1.89	4.60	1.36	125.10	35.71	0.133	–	S
2324	23 36 43.30	1.95	-52 44 51.62	0.83	11.083	0.898	2.891	0.554	20.29	4.72	8.14	1.80	81.83	16.20	0.549	–	S
2325	23 36 45.87	1.69	-53 02 03.73	1.03	5.912	0.680	2.107	0.468	14.89	4.19	7.16	2.04	69.75	24.04	0.438	–	S
2326	23 37 35.15	1.56	-57 41 37.91	1.15	11.499	0.810	2.496	0.240	26.43	4.49	0.00	0.68	34.23	7.51	0.197	–	M
2327	23 36 35.98	0.69	-52 03 54.87	0.74	5.691	0.885	3.531	0.585	7.63	1.85	5.03	1.42	41.40	42.81	0.513	–	S
2328	23 37 51.62	0.26	-59 17 13.19	0.27	4.408	0.363	3.090	0.243	5.35	0.55	4.82	0.50	175.51	50.19	0.163	–	S
2329	23 37 00.93	0.27	-55 07 42.99	0.25	4.632	0.354	3.073	0.233	6.60	0.56	4.75	0.47	110.17	19.97	0.150	–	S
2330	23 37 58.54	0.19	-59 50 27.39	0.20	6.863	0.466	5.108	0.330	5.28	0.33	3.73	0.29	161.74	13.48	0.164	–	S
2331	23 36 16.66	0.57	-50 19 00.74	1.04	2.692	0.284	1.219	0.187	12.55	2.40	5.87	1.29	170.80	18.85	0.164	–	S
2332	23 37 51.73	1.62	-59 24 22.15	1.16	3.622	0.265	0.773	0.152	17.57	3.68	12.68	2.78	84.72	40.14	0.150	–	S
2333	23 36 42.60	0.39	-53 23 24.55	0.33	7.999	0.747	5.170	0.489	6.92	0.86	4.96	0.69	82.54	25.93	0.371	–	S
2334	23 37 43.56	0.16	-58 49 41.77	0.17	13.106	0.865	12.491	0.742	1.84	0.18	1.62	0.18	175.95	114.43	0.277	-0.72	S
2335	23 36 59.00	2.53	-55 12 06.44	1.58	3.265	0.391	0.764	0.168	15.35	6.99	0.00	0.71	146.93	12.48	0.163	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2336	23 36 49.81	0.69	-54 21 33.36	0.77	0.987	0.298	0.889	0.182	3.73	1.81	1.05	1.53	152.83	93.46	0.171	–	S
2337	23 36 54.16	0.39	-54 49 32.94	0.41	2.479	0.308	1.858	0.202	5.87	0.99	3.15	0.76	39.82	26.76	0.165	–	S
2338	23 36 49.33	0.48	-54 24 23.24	0.60	5.649	0.405	2.117	0.228	11.86	1.38	8.95	1.07	165.23	23.88	0.184	–	S
2339	23 37 07.39	0.59	-56 07 32.78	0.85	0.961	0.229	0.755	0.144	5.94	1.97	1.49	1.36	175.46	38.39	0.132	–	S
2340	23 37 09.58	1.29	-56 27 43.97	0.83	5.084	0.442	1.267	0.178	16.90	3.53	0.00	0.62	30.01	8.51	0.164	–	M
2341	23 37 48.73	1.26	-59 36 15.09	0.64	5.861	0.386	1.422	0.190	20.58	2.90	8.43	1.29	105.99	10.73	0.180	–	S
2342	23 37 48.32	0.18	-59 39 06.69	0.19	6.339	0.452	5.391	0.344	3.52	0.28	2.98	0.27	11.53	40.43	0.169	–	S
2343	23 36 46.72	0.41	-54 27 01.02	0.39	3.640	0.405	2.517	0.267	5.93	0.93	4.75	0.82	67.58	51.91	0.213	–	S
2344	23 36 45.44	0.74	-54 28 15.50	0.60	4.506	0.392	1.844	0.247	10.90	1.72	8.41	1.36	94.89	34.38	0.209	–	S
2345	23 36 12.16	0.47	-50 55 58.27	0.38	24.631	1.471	5.632	0.438	17.90	1.26	6.01	0.47	143.32	5.33	0.310	–	M
2346	23 36 32.94	0.15	-53 26 48.37	0.16	45.412	2.597	30.473	1.701	7.97	0.14	0.00	0.07	138.72	1.47	0.291	-0.84	M
2347	23 36 24.32	0.36	-52 24 10.19	0.19	38.406	2.459	17.026	1.094	12.92	0.77	1.51	0.28	176.49	3.95	0.566	–	M
2348	23 37 03.48	0.23	-56 25 00.18	0.25	4.935	0.375	3.523	0.255	5.52	0.47	4.49	0.42	14.27	29.29	0.156	–	S
2349	23 36 24.33	1.08	-52 44 04.38	0.52	26.918	2.082	9.729	0.839	17.16	2.70	0.00	0.63	156.79	8.07	0.646	–	M
2350	23 36 25.75	0.34	-52 56 31.64	0.29	9.372	0.900	6.789	0.601	6.01	0.74	3.84	0.59	92.96	22.86	0.444	–	S
2351	23 36 36.05	0.21	-54 11 41.80	0.21	5.025	0.368	3.910	0.264	4.40	0.36	4.18	0.35	67.11	106.85	0.145	–	S
2352	23 37 11.43	0.16	-57 38 44.42	0.17	10.860	0.706	10.321	0.609	2.77	0.18	0.00	0.16	147.13	12.07	0.218	-0.19	S
2353	23 37 26.80	0.14	-59 01 13.65	0.15	65.186	3.612	65.893	3.633	0.00	0.03	0.00	0.03	0.00	3.47	0.254	0.59	S
2354	23 37 37.88	0.25	-59 43 11.96	0.26	3.990	0.394	3.407	0.273	3.75	0.52	2.62	0.47	146.69	44.82	0.192	–	S
2355	23 37 08.18	0.87	-57 28 08.84	1.29	2.462	0.270	0.960	0.181	13.71	3.25	6.20	1.60	23.22	19.55	0.166	–	S
2356	23 37 34.98	0.15	-59 38 34.71	0.16	17.584	1.024	16.638	0.936	2.07	0.10	1.59	0.09	172.02	118.16	0.195	0.04	S
2357	23 35 58.84	0.15	-50 11 47.97	0.16	11.829	0.698	10.289	0.586	3.30	0.13	3.09	0.13	55.39	43.79	0.147	-0.24	S
2358	23 37 27.83	0.29	-59 11 43.21	0.46	11.794	0.938	4.487	0.353	11.60	1.03	5.62	0.58	80.03	9.37	0.252	–	M
2359	23 36 50.78	0.74	-56 02 28.30	1.13	6.850	0.423	1.370	0.179	19.77	2.66	12.51	1.66	165.75	15.87	0.171	–	S
2360	23 37 00.00	0.56	-56 53 12.06	0.45	1.644	0.288	1.329	0.184	5.31	1.28	1.95	0.98	108.88	35.24	0.162	–	S
2361	23 36 53.86	0.91	-56 22 28.95	0.93	3.185	0.274	1.057	0.174	12.08	2.31	10.45	1.97	35.85	62.03	0.155	–	S
2362	23 35 59.44	0.79	-50 30 07.24	0.65	10.821	0.652	2.570	0.261	20.66	2.21	9.80	0.94	55.31	7.77	0.228	–	S
2363	23 36 58.64	0.53	-56 47 47.41	0.62	1.430	0.272	1.110	0.174	5.11	1.45	3.24	1.20	171.99	60.76	0.155	–	S
2364	23 37 31.52	2.65	-59 34 21.79	0.40	16.289	1.070	3.353	0.291	37.68	6.24	3.70	0.78	174.61	7.49	0.225	–	M
2365	23 37 08.82	0.15	-58 01 48.71	0.16	122.894	7.755	123.244	7.124	0.00	0.14	0.00	0.14	0.00	36.69	2.195	-0.08	S
2366	23 36 36.57	0.69	-55 23 20.93	0.96	1.734	0.270	0.976	0.181	8.64	2.24	5.37	1.59	4.84	38.49	0.160	–	S
2367	23 36 12.15	0.14	-52 36 21.97	0.15	1854.292	102.180	1843.426	101.454	0.81	0.02	0.36	0.02	21.53	19.57	3.637	-0.06	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2368	23 37 27.50	0.26	-59 42 34.58	0.26	3.806	0.400	3.380	0.277	3.43	0.53	1.93	0.48	144.36	40.78	0.199	-	S
2369	23 36 15.57	0.17	-53 01 34.18	0.19	18.835	1.308	16.884	1.044	3.44	0.26	1.94	0.23	170.68	21.26	0.466	-	S
2370	23 36 57.58	0.27	-57 17 55.07	0.46	8.247	0.507	3.121	0.242	14.69	1.05	5.87	0.47	161.76	4.35	0.165	-	S
2371	23 36 24.55	0.73	-54 05 13.19	0.61	2.942	0.291	1.353	0.190	9.88	1.72	7.55	1.36	72.28	36.61	0.161	-	S
2372	23 35 52.23	0.28	-50 19 13.74	0.28	3.369	0.352	2.864	0.241	4.34	0.63	2.31	0.52	55.95	28.93	0.176	-	S
2373	23 37 28.82	0.98	-59 58 05.99	0.83	2.051	0.357	1.155	0.241	7.67	2.29	6.08	1.90	103.73	108.44	0.214	-	S
2374	23 35 57.93	0.21	-51 16 50.54	0.25	58.704	3.271	15.939	0.928	20.28	0.58	6.52	0.20	124.66	2.02	0.306	-1.00	M
2375	23 37 21.15	0.38	-59 42 37.74	0.36	4.850	0.430	2.889	0.278	6.83	0.84	6.02	0.75	127.54	75.57	0.210	-	S
2376	23 36 04.74	0.15	-52 24 39.91	0.16	29.500	1.859	28.355	1.647	1.89	0.16	1.36	0.15	175.80	157.40	0.525	-0.50	S
2377	23 36 56.96	1.04	-57 47 04.81	0.96	2.063	0.340	1.069	0.232	8.69	2.59	6.50	2.04	126.50	69.69	0.207	-	S
2378	23 36 02.20	0.22	-52 22 16.92	0.27	11.699	1.075	10.027	0.759	4.61	0.52	1.58	0.41	169.15	18.11	0.505	-	S
2379	23 36 37.42	0.79	-56 17 44.44	0.70	3.949	0.290	1.266	0.166	13.79	2.00	9.46	1.39	52.13	21.10	0.144	-	S
2380	23 36 36.15	0.44	-56 10 17.17	0.45	5.176	0.367	2.149	0.208	9.62	1.02	9.24	0.95	30.19	98.61	0.159	-	S
2381	23 36 33.24	0.29	-55 55 19.33	0.39	3.120	0.316	2.239	0.209	6.54	0.84	3.13	0.60	178.81	16.61	0.160	-	S
2382	23 36 53.20	0.61	-57 47 22.06	0.73	1.623	0.355	1.250	0.226	5.24	1.73	3.16	1.38	175.39	62.64	0.205	-	S
2383	23 36 45.34	0.62	-57 06 25.04	0.80	2.236	0.308	1.267	0.205	8.50	1.90	5.22	1.34	18.18	31.31	0.179	-	S
2384	23 35 45.15	0.61	-50 22 21.06	0.55	2.217	0.287	1.380	0.189	7.13	1.43	5.65	1.21	95.91	49.45	0.161	-	S
2385	23 35 54.99	0.15	-51 52 14.83	0.17	37.591	2.395	29.255	1.698	0.00	0.21	0.00	0.13	0.00	3.78	0.543	-0.23	M
2386	23 36 48.79	0.78	-57 36 33.22	1.23	1.656	0.261	0.837	0.178	10.04	2.89	5.46	1.79	172.87	31.92	0.160	-	S
2387	23 36 19.38	0.26	-55 03 42.59	0.21	29.896	1.731	9.814	0.580	13.80	0.58	3.78	0.22	27.24	2.89	0.212	-0.74	M
2388	23 36 18.77	0.50	-54 56 31.68	0.47	2.642	0.304	1.660	0.199	7.39	1.23	4.83	0.94	51.87	28.91	0.165	-	S
2389	23 37 02.18	0.74	-59 14 57.36	1.06	2.469	0.281	1.054	0.189	11.11	2.51	6.98	1.66	166.80	28.03	0.168	-	S
2390	23 36 35.41	0.14	-57 02 08.43	0.15	47.346	2.630	44.369	2.450	2.90	0.04	0.46	0.04	149.45	2.00	0.215	-0.94	S
2391	23 35 58.27	0.15	-53 10 52.84	0.15	127.997	7.403	125.582	7.034	0.00	0.09	0.00	0.08	0.00	6.59	1.325	-0.06	S
2392	23 36 54.08	1.06	-58 49 36.94	0.68	3.767	0.436	1.669	0.294	11.13	2.39	6.57	1.61	93.76	29.19	0.260	-	S
2393	23 36 48.78	0.23	-58 25 56.08	0.22	7.814	0.608	5.962	0.425	5.05	0.43	3.68	0.39	107.42	28.00	0.256	-	S
2394	23 35 37.12	0.32	-50 48 34.22	0.29	297.249	16.452	103.162	5.707	39.19	0.88	6.48	0.15	137.63	1.29	0.611	-1.07	M
2395	23 35 50.41	0.28	-52 33 07.68	0.28	11.036	1.123	9.239	0.769	4.17	0.59	2.89	0.53	64.30	41.11	0.556	-	S
2396	23 37 02.75	0.76	-59 47 33.26	0.68	2.319	0.293	1.223	0.196	9.01	1.88	5.76	1.38	128.43	33.30	0.170	-	S
2397	23 35 43.88	0.58	-51 51 33.70	0.58	13.375	1.295	4.706	0.536	9.97	1.73	0.00	0.71	42.95	11.88	0.470	-	M
2398	23 35 31.63	1.30	-50 24 26.76	1.46	5.290	0.466	0.991	0.192	14.07	4.42	0.00	1.20	47.73	16.66	0.184	-	M
2399	23 36 01.24	0.55	-54 09 48.55	0.67	1.722	0.258	1.137	0.170	6.97	1.55	4.49	1.22	159.23	42.40	0.147	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2400	23 35 28.71	0.93	-50 03 54.93	0.84	3.003	0.255	1.059	0.159	13.97	2.53	8.62	1.51	122.24	21.21	0.141	–	S
2401	23 36 45.39	0.35	-58 40 29.41	0.36	3.218	0.337	2.294	0.223	6.20	0.84	3.60	0.66	139.95	22.55	0.173	–	S
2402	23 35 30.57	0.15	-50 29 30.61	0.16	16.561	0.964	12.750	0.729	5.42	0.17	3.39	0.13	103.52	4.86	0.189	-1.15	S
2403	23 35 28.41	0.66	-50 08 36.51	1.15	1.201	0.229	0.752	0.151	9.17	2.65	3.45	1.53	170.40	29.85	0.136	–	S
2404	23 36 18.66	0.58	-56 20 02.13	0.97	1.688	0.212	0.865	0.141	10.60	2.29	4.76	1.26	10.17	19.80	0.125	–	S
2405	23 35 51.12	0.14	-53 22 26.85	0.15	64.756	3.666	52.753	2.927	4.19	0.07	2.20	0.06	22.40	3.89	0.384	-0.96	M
2406	23 35 51.90	1.02	-53 29 38.56	1.39	4.576	0.402	1.343	0.260	14.87	3.30	10.37	2.32	15.63	35.33	0.241	–	S
2407	23 35 30.51	2.20	-50 45 47.75	2.08	34.438	1.924	2.176	0.341	38.63	6.12	25.86	3.78	51.63	19.97	0.496	–	S
2408	23 35 51.72	0.89	-53 29 17.81	1.48	4.092	0.396	1.334	0.263	14.76	3.43	8.76	2.09	175.13	27.93	0.242	–	S
2409	23 36 43.19	0.84	-58 46 30.88	0.67	3.932	0.424	1.783	0.282	9.89	1.92	7.36	1.55	101.68	46.69	0.244	–	S
2410	23 36 22.83	0.87	-56 56 38.37	1.06	2.795	0.348	1.232	0.237	10.46	2.58	7.36	1.87	23.09	40.14	0.211	–	S
2411	23 36 39.45	1.54	-58 33 36.40	1.09	3.236	0.312	0.968	0.210	14.49	3.57	9.75	2.53	103.27	39.77	0.196	–	S
2412	23 35 23.50	0.17	-50 01 57.35	0.19	7.436	0.481	5.803	0.356	4.73	0.26	4.06	0.25	172.08	149.65	0.151	–	S
2413	23 35 24.48	0.24	-50 18 48.14	0.26	3.792	0.339	3.103	0.237	4.11	0.49	3.66	0.48	122.38	2.93	0.158	–	S
2414	23 36 36.40	1.03	-58 33 37.36	0.47	7.406	0.592	2.329	0.231	13.93	2.50	0.49	0.75	161.05	9.95	0.193	–	M
2415	23 35 49.77	0.86	-53 46 07.32	1.13	2.734	0.281	1.036	0.187	12.52	2.72	8.26	1.87	156.99	32.65	0.167	–	S
2416	23 36 07.60	0.58	-55 49 20.43	0.70	2.249	0.281	1.266	0.187	7.94	1.61	6.05	1.31	5.24	47.57	0.160	–	S
2417	23 36 04.71	0.72	-55 30 41.64	1.01	1.640	0.276	0.950	0.184	8.66	2.37	4.83	1.60	164.89	35.83	0.165	–	S
2418	23 35 27.95	0.49	-51 11 03.90	0.33	50.002	2.837	11.927	0.759	23.04	1.22	8.61	0.47	152.58	4.30	0.382	–	M
2419	23 35 55.76	0.68	-54 34 43.06	0.70	1.761	0.320	1.212	0.209	6.00	1.68	4.78	1.48	140.60	101.74	0.185	–	S
2420	23 36 16.00	0.27	-56 46 11.80	0.29	3.657	0.365	2.957	0.249	4.49	0.59	3.12	0.53	27.17	36.44	0.180	–	S
2421	23 35 53.24	0.55	-54 21 39.29	0.64	4.608	0.398	2.009	0.250	9.92	1.46	8.36	1.27	10.58	49.68	0.207	–	S
2422	23 35 31.49	0.86	-51 36 01.18	1.14	3.147	0.323	1.237	0.214	13.58	2.93	6.99	1.57	30.56	21.22	0.193	–	S
2423	23 36 33.12	0.32	-58 32 00.47	0.30	4.086	0.394	2.985	0.263	5.97	0.70	3.43	0.57	127.24	20.72	0.195	–	S
2424	23 36 28.30	0.23	-58 06 00.53	0.27	4.547	0.453	4.037	0.317	0.00	0.52	0.00	0.42	0.00	18.51	0.221	–	S
2425	23 35 59.27	0.42	-55 13 13.47	0.36	3.413	0.324	2.130	0.212	7.45	0.95	4.90	0.74	110.69	23.21	0.164	–	S
2426	23 36 44.60	0.15	-59 37 35.50	0.16	9.680	0.596	8.995	0.520	2.53	0.14	1.66	0.14	164.67	22.32	0.156	-0.37	S
2427	23 36 03.23	0.44	-55 50 40.48	0.49	2.706	0.284	1.625	0.185	7.95	1.19	4.97	0.88	145.50	23.84	0.151	–	S
2428	23 35 31.75	1.44	-52 05 21.39	2.06	12.896	0.800	1.829	0.342	25.81	5.12	15.30	2.92	24.13	22.53	0.380	–	S
2429	23 36 40.97	0.55	-59 26 48.64	0.39	1.691	0.247	1.266	0.160	6.25	1.20	2.50	0.88	88.76	26.00	0.137	–	S
2430	23 36 21.51	1.26	-57 45 06.18	0.79	2.408	0.295	1.035	0.201	12.44	3.00	5.92	1.66	109.10	23.63	0.181	–	S
2431	23 35 22.90	0.97	-51 09 21.63	0.69	61.050	3.439	12.124	0.781	30.40	2.64	9.56	0.82	145.93	6.42	0.407	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2432	23 35 49.78	0.22	-54 26 48.73	0.20	7.721	0.621	5.235	0.348	5.59	0.42	0.00	0.26	146.15	7.27	0.196	-	M
2433	23 35 44.58	0.30	-53 51 16.26	0.25	7.451	0.503	4.030	0.300	8.91	0.65	5.88	0.46	79.11	10.64	0.186	-	S
2434	23 35 42.50	0.84	-53 37 41.69	0.63	4.173	0.374	1.716	0.237	12.77	2.14	6.70	1.19	115.60	16.61	0.205	-	S
2435	23 36 01.75	0.55	-55 52 11.66	0.68	1.677	0.243	1.073	0.160	7.44	1.61	4.34	1.17	21.60	31.82	0.138	-	S
2436	23 35 50.29	0.57	-54 39 30.79	0.51	4.027	0.341	1.864	0.212	10.73	1.46	6.55	0.95	53.04	16.97	0.173	-	S
2437	23 35 46.70	0.25	-54 11 50.97	0.28	3.859	0.362	3.107	0.249	5.10	0.58	2.57	0.47	146.65	20.13	0.174	-	S
2438	23 35 58.75	0.86	-55 35 26.74	1.56	1.911	0.267	0.863	0.182	13.77	3.86	3.83	1.50	157.35	18.57	0.170	-	S
2439	23 36 09.98	0.27	-56 53 15.65	0.47	7.667	0.523	3.445	0.292	12.15	1.06	5.39	0.55	172.41	6.74	0.211	-	S
2440	23 35 20.58	0.34	-51 04 31.13	0.26	7.135	0.579	4.767	0.381	8.44	0.81	2.21	0.42	107.08	7.29	0.262	-	S
2441	23 35 53.09	0.32	-55 11 45.77	0.36	2.141	0.325	2.017	0.210	0.00	0.79	0.00	0.67	0.00	42.55	0.176	-	S
2442	23 35 14.31	0.71	-50 11 39.60	0.85	2.059	0.276	1.117	0.184	9.56	2.12	5.64	1.44	144.19	31.88	0.161	-	S
2443	23 36 07.36	0.38	-56 53 01.56	0.37	4.341	0.415	2.769	0.272	6.91	0.88	4.99	0.74	129.61	30.37	0.209	-	S
2444	23 36 29.51	0.18	-58 58 42.45	0.18	8.729	0.599	7.509	0.466	4.04	0.26	2.09	0.23	121.94	13.91	0.210	-	S
2445	23 35 19.99	0.37	-51 12 44.88	0.36	4.202	0.580	3.644	0.378	4.73	0.90	0.00	0.67	125.25	25.32	0.312	-	S
2446	23 35 48.36	0.72	-54 56 39.86	1.15	1.327	0.282	0.853	0.185	8.35	2.70	3.21	1.62	167.24	33.08	0.169	-	S
2447	23 35 17.28	0.35	-50 57 36.63	0.33	3.060	0.368	2.544	0.244	4.57	0.78	2.58	0.65	107.06	34.67	0.193	-	S
2448	23 35 12.33	0.66	-50 21 41.78	0.52	2.535	0.302	1.474	0.199	8.35	1.60	5.49	1.11	82.52	27.75	0.168	-	S
2449	23 36 24.27	0.41	-58 50 16.31	0.39	3.123	0.494	2.693	0.317	3.93	0.95	2.17	0.81	127.26	58.88	0.272	-	S
2450	23 35 17.29	1.60	-51 21 05.24	2.20	29.175	1.611	1.235	0.152	46.64	5.22	32.48	3.65	162.42	18.26	0.248	-	S
2451	23 35 18.76	0.74	-51 25 07.92	0.77	1.375	0.376	1.153	0.234	3.98	1.85	3.17	1.65	128.41	178.91	0.217	-	S
2452	23 36 27.09	0.80	-59 10 28.61	0.88	1.529	0.293	0.956	0.194	6.78	2.16	5.26	1.72	158.91	78.42	0.173	-	S
2453	23 35 18.76	0.58	-51 39 37.65	0.62	1.308	0.282	1.097	0.177	4.70	1.48	2.13	1.24	41.19	57.68	0.160	-	S
2454	23 36 30.09	0.97	-59 36 12.22	0.60	2.782	0.269	1.132	0.175	12.09	2.17	6.96	1.43	91.69	23.15	0.153	-	S
2455	23 36 08.02	0.22	-57 57 01.56	0.81	62.319	3.703	17.579	1.094	31.76	1.89	5.57	0.36	94.75	3.30	0.512	-	M
2456	23 35 15.33	0.26	-51 20 39.27	0.27	4.623	0.501	4.258	0.347	2.76	0.51	1.96	0.51	56.31	86.57	0.251	-	S
2457	23 35 59.77	1.44	-56 48 20.95	1.21	3.060	0.289	0.888	0.193	13.49	3.39	11.31	2.83	81.96	82.07	0.180	-	S
2458	23 35 07.32	0.36	-50 13 13.96	0.36	2.409	0.281	1.878	0.186	5.31	0.86	3.32	0.70	117.68	33.22	0.148	-	S
2459	23 36 01.15	0.66	-57 08 44.43	0.90	2.078	0.258	1.033	0.173	9.59	2.11	6.28	1.49	167.78	32.54	0.151	-	S
2460	23 35 50.11	0.27	-56 06 11.85	0.33	4.413	0.336	2.664	0.214	7.60	0.68	5.21	0.53	176.69	16.12	0.145	-	S
2461	23 35 14.52	0.86	-51 37 27.19	1.04	2.137	0.311	1.073	0.212	9.38	2.39	6.95	2.00	157.44	63.83	0.187	-	S
2462	23 35 14.24	0.24	-51 58 05.30	0.21	63.726	3.704	19.920	1.191	14.43	0.52	6.86	0.27	31.00	3.53	0.466	-	M
2463	23 35 38.59	0.20	-55 13 37.60	0.20	6.943	0.477	5.168	0.337	4.86	0.33	4.49	0.32	34.29	61.84	0.171	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2464	23 36 10.48	0.96	-58 35 09.07	1.04	3.262	0.308	1.152	0.201	13.54	2.79	7.89	1.71	141.13	23.47	0.182	–	S
2465	23 35 01.54	0.71	-50 15 24.05	0.29	3.999	0.412	1.859	0.190	0.00	1.67	0.00	0.53	0.00	8.87	0.160	–	M
2466	23 36 00.57	0.54	-57 48 22.47	0.36	8.689	0.567	3.312	0.291	14.72	1.29	5.83	0.59	114.57	6.23	0.220	–	S
2467	23 35 53.05	0.16	-57 17 14.97	0.16	9.466	0.589	7.493	0.432	0.00	0.17	0.00	0.13	0.00	4.99	0.129	-0.03	M
2468	23 34 56.15	0.49	-50 00 59.35	0.53	2.942	0.299	1.653	0.195	7.74	1.16	6.89	1.14	34.77	92.51	0.159	–	S
2469	23 35 55.83	0.16	-57 43 55.35	0.17	11.208	0.680	8.998	0.526	4.56	0.18	3.13	0.16	27.46	9.81	0.171	-0.71	S
2470	23 36 03.00	0.44	-58 29 14.43	0.44	2.818	0.389	2.107	0.253	5.31	1.05	3.73	0.89	141.12	50.73	0.213	–	S
2471	23 35 19.26	1.03	-53 41 09.98	0.92	2.257	0.318	1.077	0.218	9.00	2.42	7.87	2.14	85.64	103.90	0.193	–	S
2472	23 35 00.85	0.79	-51 05 23.83	0.88	3.254	0.485	1.786	0.326	7.93	2.05	6.97	1.81	19.92	161.26	0.286	–	S
2473	23 34 52.63	0.34	-50 01 53.42	0.38	2.680	0.301	2.040	0.199	5.46	0.82	3.77	0.72	142.47	42.22	0.156	–	S
2474	23 35 28.79	1.40	-55 12 22.35	1.21	2.825	0.275	0.857	0.185	13.48	3.37	10.80	2.73	112.70	62.85	0.172	–	S
2475	23 35 14.33	0.31	-53 48 30.52	1.17	27.644	1.610	6.390	0.415	31.09	2.76	6.52	0.58	94.91	5.13	0.221	–	M
2476	23 36 09.82	0.90	-59 41 35.57	0.38	6.563	0.431	2.189	0.215	19.74	2.08	3.85	0.58	71.26	5.10	0.187	–	S
2477	23 35 48.20	0.56	-57 34 42.35	0.96	2.777	0.255	1.134	0.163	13.14	2.30	5.97	1.16	163.55	14.68	0.144	–	S
2478	23 34 52.68	0.52	-50 26 18.44	0.71	4.892	0.416	2.114	0.259	11.27	1.61	7.76	1.18	8.89	26.82	0.215	–	S
2479	23 35 52.95	0.17	-58 10 15.63	0.17	15.838	1.003	13.099	0.782	4.06	0.21	3.11	0.20	100.06	23.19	0.293	-0.23	S
2480	23 35 38.61	0.14	-56 51 13.63	0.15	78.854	4.352	78.360	4.315	0.00	0.02	0.00	0.02	0.00	4.85	0.206	-0.29	S
2481	23 35 13.78	0.40	-53 45 07.91	0.35	2.483	0.360	2.148	0.233	4.30	0.90	1.57	0.73	102.73	36.16	0.195	–	S
2482	23 36 02.50	0.14	-59 18 14.34	0.15	38.218	2.133	32.924	1.824	4.48	0.06	0.82	0.05	41.41	0.87	0.214	-1.09	S
2483	23 34 46.95	0.36	-50 17 24.37	0.41	3.054	0.351	2.327	0.231	7.27	1.05	0.00	0.58	138.40	12.30	0.185	–	S
2484	23 34 49.59	1.21	-50 26 32.54	0.82	6.500	0.434	1.506	0.220	18.05	2.99	12.21	1.80	95.87	19.81	0.207	–	S
2485	23 35 52.52	0.62	-58 32 10.93	0.66	1.245	0.357	1.157	0.216	3.56	1.65	0.00	1.28	146.67	65.21	0.204	–	S
2486	23 35 11.54	0.21	-53 59 22.56	0.22	6.080	0.438	4.555	0.308	4.78	0.37	4.54	0.36	36.56	109.20	0.169	–	S
2487	23 34 52.31	1.31	-51 13 34.92	0.90	3.947	0.493	1.677	0.337	12.56	3.31	6.57	1.79	109.03	25.66	0.305	–	S
2488	23 35 07.10	0.82	-53 27 48.40	0.79	1.896	0.500	1.493	0.316	4.56	1.95	3.81	1.77	103.33	178.95	0.290	–	S
2489	23 35 24.81	1.02	-55 59 42.33	1.48	4.256	0.357	0.760	0.145	14.11	4.06	0.00	1.13	121.41	15.46	0.138	–	M
2490	23 35 55.71	0.89	-59 09 46.96	0.68	1.276	0.307	0.960	0.196	6.08	2.08	2.62	1.50	109.63	48.99	0.179	–	S
2491	23 34 52.51	0.24	-51 31 01.73	0.24	5.503	0.420	4.032	0.289	5.51	0.47	4.33	0.41	115.16	27.16	0.175	–	S
2492	23 35 39.71	0.30	-57 35 24.49	0.31	3.224	0.312	2.359	0.209	5.03	0.67	4.49	0.61	25.36	76.24	0.154	–	S
2493	23 35 27.17	0.98	-56 12 55.10	1.89	2.890	0.234	0.733	0.145	19.85	4.58	8.48	1.95	162.51	17.96	0.143	–	S
2494	23 35 26.28	0.33	-56 18 06.66	0.39	2.637	0.269	1.822	0.177	6.43	0.86	4.06	0.68	22.56	23.84	0.137	–	S
2495	23 35 47.38	0.19	-58 44 36.93	0.19	11.628	0.882	10.635	0.687	3.90	0.31	0.00	0.25	131.43	10.08	0.354	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2496	23 35 32.06	0.69	-57 05 40.51	1.13	1.689	0.273	0.925	0.184	9.61	2.65	4.57	1.57	172.53	28.12	0.165	–	S
2497	23 34 54.96	0.39	-52 19 19.05	0.46	7.348	0.718	4.431	0.468	7.42	1.01	5.79	0.88	3.71	44.39	0.370	–	S
2498	23 34 46.83	0.15	-51 18 41.32	0.18	165.652	9.188	67.569	3.744	14.53	0.26	5.75	0.11	65.34	1.43	0.458	-1.15	M
2499	23 35 27.01	0.44	-56 35 22.73	0.59	2.573	0.299	1.564	0.197	7.74	1.33	4.89	0.99	178.32	27.08	0.164	–	S
2500	23 34 56.89	0.91	-52 38 37.23	1.80	9.896	0.996	3.170	0.671	16.69	4.25	7.64	2.02	168.69	22.51	0.634	–	S
2501	23 35 18.22	0.52	-55 36 32.19	0.54	3.240	0.336	1.761	0.220	7.62	1.26	6.99	1.16	155.86	118.02	0.181	–	S
2502	23 34 49.93	0.60	-51 44 23.17	0.61	6.815	0.516	2.593	0.303	11.73	1.54	9.17	1.21	128.53	29.76	0.249	–	S
2503	23 35 45.74	0.36	-58 47 01.44	0.35	2.920	0.421	2.566	0.274	3.27	0.78	2.54	0.75	110.57	143.70	0.228	–	S
2504	23 34 55.14	0.72	-52 37 46.24	1.30	13.997	1.165	4.419	0.724	15.93	3.03	8.46	1.64	6.16	19.43	0.662	–	S
2505	23 35 38.35	0.14	-58 43 48.30	0.15	99.456	5.549	78.214	4.315	11.24	0.08	2.21	0.03	125.75	0.52	0.340	-0.73	M
2506	23 35 17.81	0.61	-55 53 27.79	0.54	1.268	0.247	1.007	0.157	4.80	1.41	3.22	1.21	106.76	79.97	0.141	–	S
2507	23 35 17.32	0.60	-55 52 06.22	0.60	1.861	0.265	1.181	0.175	6.37	1.42	5.71	1.33	137.86	151.81	0.151	–	S
2508	23 35 01.56	0.45	-53 56 35.57	0.46	1.186	0.246	1.132	0.153	1.98	1.03	1.50	1.00	33.39	178.97	0.138	–	S
2509	23 34 47.83	0.34	-52 08 04.98	0.45	29.389	1.730	9.153	0.696	17.19	1.15	7.72	0.51	32.09	4.79	0.474	–	S
2510	23 35 07.87	0.43	-55 12 53.12	0.69	6.568	0.452	2.326	0.243	14.23	1.61	7.61	0.89	13.89	10.84	0.198	–	S
2511	23 35 23.10	0.42	-57 08 36.31	0.54	2.042	0.295	1.541	0.190	6.93	1.30	0.00	0.78	151.76	16.75	0.164	–	S
2512	23 34 53.44	0.62	-53 32 27.01	0.40	3.320	0.353	1.944	0.230	9.19	1.45	4.13	0.84	81.59	15.49	0.191	–	S
2513	23 35 20.98	0.66	-57 07 58.64	0.49	1.244	0.290	1.097	0.179	0.00	1.50	0.00	1.12	0.00	41.75	0.165	–	S
2514	23 35 25.90	0.57	-57 48 47.43	0.56	2.125	0.379	1.606	0.244	4.82	1.34	4.11	1.23	34.84	136.29	0.215	–	S
2515	23 35 02.82	0.17	-55 03 44.24	0.18	7.563	0.512	6.835	0.416	2.78	0.22	2.43	0.22	95.97	82.45	0.174	–	S
2516	23 34 40.50	0.22	-51 55 17.29	0.20	19.871	1.215	7.851	0.515	6.18	0.40	2.61	0.29	166.24	9.75	0.281	–	M
2517	23 35 00.00	0.15	-54 55 36.41	0.16	41.006	2.298	19.396	1.094	9.42	0.18	4.97	0.11	40.95	2.31	0.242	-0.84	M
2518	23 35 18.81	0.37	-57 14 00.24	0.47	3.114	0.270	1.705	0.171	9.00	1.09	5.28	0.74	157.59	15.48	0.133	–	S
2519	23 34 32.14	0.51	-50 40 22.38	0.75	8.195	0.516	2.254	0.236	16.51	1.75	10.59	1.12	164.22	14.98	0.197	–	S
2520	23 34 56.73	0.46	-54 32 01.42	0.39	5.443	0.425	2.652	0.259	9.43	1.06	7.02	0.82	68.87	22.33	0.198	–	S
2521	23 34 44.91	0.25	-52 51 19.29	0.30	644.344	78.311	619.650	53.161	0.00	0.59	0.00	0.50	0.00	32.50	40.466	–	S
2522	23 35 12.80	0.23	-56 36 58.90	0.28	6.193	0.453	3.962	0.294	7.35	0.57	4.41	0.42	161.42	11.40	0.184	–	S
2523	23 35 01.06	0.38	-55 09 33.22	0.43	1.945	0.292	1.634	0.189	4.34	0.96	2.46	0.82	156.53	50.58	0.160	–	S
2524	23 35 26.05	0.76	-58 12 13.90	0.61	2.144	0.421	1.543	0.272	6.26	1.78	3.42	1.35	112.04	47.96	0.244	–	S
2525	23 34 32.17	0.14	-50 59 43.85	0.15	25.977	1.464	24.674	1.370	2.13	0.07	1.63	0.06	7.92	27.79	0.186	-0.81	S
2526	23 35 30.72	0.30	-58 55 42.13	0.30	5.521	0.489	3.816	0.325	5.39	0.64	5.06	0.59	150.25	105.40	0.233	–	S
2527	23 34 50.26	0.64	-53 58 39.27	0.79	1.684	0.287	1.101	0.188	7.38	1.88	4.22	1.38	154.85	39.69	0.167	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2528	23 35 13.67	1.07	-57 09 36.91	0.91	2.437	0.275	0.977	0.187	10.90	2.57	8.45	2.03	62.77	54.90	0.166	–	S
2529	23 34 39.24	0.70	-52 29 15.15	0.78	5.466	0.763	3.062	0.510	7.67	1.79	6.75	1.63	16.41	138.36	0.443	–	S
2530	23 34 33.52	0.19	-51 40 26.09	0.24	11.980	0.738	6.798	0.437	9.04	0.45	5.22	0.29	19.70	6.16	0.211	–	S
2531	23 35 15.39	1.01	-57 23 32.41	0.68	1.037	0.244	0.740	0.157	6.86	2.31	2.82	1.58	92.64	42.55	0.143	–	S
2532	23 35 31.61	0.24	-59 18 59.29	0.26	12.369	0.768	4.639	0.314	8.10	0.54	5.47	0.41	125.91	12.57	0.184	–	M
2533	23 34 56.98	0.20	-55 14 44.22	0.21	8.658	0.578	5.918	0.389	5.44	0.35	5.43	0.35	105.64	178.99	0.198	–	S
2534	23 34 58.34	0.67	-55 21 57.89	0.75	3.601	0.337	1.534	0.217	10.82	1.86	7.74	1.37	32.04	29.77	0.186	–	S
2535	23 35 27.43	1.64	-58 53 28.57	1.13	4.365	0.346	1.055	0.212	17.64	3.90	10.59	2.43	66.18	27.17	0.206	–	S
2536	23 34 45.24	0.21	-53 49 20.05	0.21	6.490	0.476	5.058	0.341	4.61	0.37	3.95	0.35	126.67	47.90	0.187	–	S
2537	23 34 29.02	0.17	-51 20 28.95	0.18	13.787	0.957	13.117	0.799	2.88	0.24	0.00	0.20	135.54	15.88	0.339	–	S
2538	23 35 01.07	0.80	-56 08 15.96	1.28	8.509	0.493	1.280	0.152	26.67	3.20	12.80	1.46	21.95	9.97	0.157	–	S
2539	23 34 42.80	1.16	-53 36 00.18	1.65	2.800	0.261	0.855	0.171	18.01	4.36	7.23	1.81	147.76	18.59	0.165	–	S
2540	23 34 50.06	0.48	-54 41 07.92	0.65	2.330	0.306	1.478	0.201	7.91	1.53	4.06	1.03	15.11	24.36	0.172	–	S
2541	23 35 12.57	0.14	-57 38 49.79	0.15	15.522	0.891	14.214	0.796	2.58	0.09	2.17	0.09	175.87	25.05	0.149	-0.47	S
2542	23 34 23.44	0.96	-50 39 11.54	0.75	1.803	0.295	1.043	0.197	8.36	2.30	5.54	1.66	79.64	42.07	0.175	–	S
2543	23 35 02.33	0.92	-56 42 42.71	1.11	18.421	1.153	5.625	0.369	31.80	3.33	3.11	0.49	49.49	4.94	0.201	–	M
2544	23 34 58.20	0.46	-55 55 30.12	0.56	1.159	0.250	1.049	0.155	0.00	1.29	0.00	1.02	0.00	46.35	0.141	–	S
2545	23 34 23.32	1.09	-50 42 48.39	1.54	12.320	0.710	1.493	0.208	26.10	3.56	18.74	2.58	4.61	25.32	0.232	–	S
2546	23 34 44.98	0.20	-54 19 08.55	0.21	51.357	2.979	18.565	1.086	15.36	0.45	5.04	0.17	135.15	2.14	0.370	-0.72	M
2547	23 34 28.69	0.46	-51 47 53.69	0.80	6.990	0.518	2.623	0.298	14.85	1.92	6.68	0.91	17.01	10.93	0.250	–	S
2548	23 34 56.21	0.82	-55 57 20.55	1.10	2.122	0.243	0.884	0.165	11.21	2.61	7.64	1.84	12.77	35.73	0.146	–	S
2549	23 34 51.61	0.43	-55 27 36.63	0.53	2.459	0.341	1.775	0.222	6.40	1.23	3.27	0.91	158.25	28.40	0.189	–	S
2550	23 35 22.88	0.50	-59 41 34.49	0.47	2.967	0.322	1.757	0.211	7.08	1.17	5.86	1.00	52.02	60.63	0.174	–	S
2551	23 34 39.00	0.67	-54 24 03.58	0.88	2.290	0.380	1.414	0.251	8.23	2.11	4.28	1.41	156.31	33.06	0.223	–	S
2552	23 35 09.68	0.73	-58 32 03.25	0.64	1.231	0.335	1.089	0.205	5.08	1.84	0.00	1.22	126.72	35.29	0.192	–	S
2553	23 34 37.04	0.15	-54 41 44.42	0.16	10.480	0.653	10.006	0.579	2.35	0.15	0.77	0.14	65.01	19.05	0.178	0.67	S
2554	23 34 32.76	0.89	-54 12 53.38	0.94	5.243	0.663	2.693	0.436	12.84	2.83	2.18	1.03	135.60	13.54	0.400	–	S
2555	23 34 45.52	0.26	-56 02 15.13	0.28	3.882	0.349	2.949	0.238	5.13	0.57	3.75	0.50	18.99	31.36	0.165	–	S
2556	23 34 20.31	0.74	-52 27 01.56	0.79	2.770	0.643	2.103	0.410	5.55	1.90	3.47	1.60	40.26	73.00	0.373	–	S
2557	23 34 53.86	0.45	-57 28 41.84	0.51	2.540	0.288	1.574	0.189	7.11	1.19	5.17	0.96	20.30	35.32	0.156	–	S
2558	23 34 56.27	0.55	-57 47 30.42	0.68	1.443	0.305	1.155	0.193	5.08	1.58	2.40	1.22	2.83	49.46	0.175	–	S
2559	23 34 39.59	0.17	-55 54 41.10	0.16	12.715	0.830	8.094	0.477	0.00	0.24	0.00	0.15	0.00	4.07	0.172	-0.23	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2560	23 34 45.84	0.74	-56 41 54.77	1.00	1.662	0.288	0.968	0.193	8.15	2.34	5.17	1.69	1.17	44.38	0.172	–	S
2561	23 34 20.49	0.47	-52 59 54.88	0.46	5.889	0.827	4.383	0.539	4.95	1.07	4.54	0.99	75.05	156.47	0.456	–	S
2562	23 34 29.10	0.75	-54 31 05.74	0.70	5.572	0.479	2.170	0.300	11.62	1.90	8.51	1.41	51.75	29.38	0.257	–	S
2563	23 34 37.70	0.21	-55 52 15.62	0.23	6.456	0.447	4.398	0.299	6.78	0.45	3.95	0.33	36.68	9.81	0.165	–	S
2564	23 34 50.43	0.18	-57 58 53.58	0.19	7.115	0.506	6.203	0.392	3.16	0.27	2.85	0.26	10.61	70.61	0.188	–	S
2565	23 34 25.22	0.46	-54 33 15.03	0.48	3.353	0.408	2.228	0.268	6.31	1.12	5.06	0.99	34.96	59.62	0.223	–	S
2566	23 35 04.30	0.58	-59 41 28.49	0.62	1.402	0.329	1.206	0.204	4.70	1.57	0.00	1.15	33.17	41.42	0.188	–	S
2567	23 34 00.79	1.06	-50 26 46.37	0.88	2.182	0.254	0.930	0.172	11.06	2.63	8.05	1.90	108.02	39.40	0.152	–	S
2568	23 34 15.87	0.66	-53 24 15.82	0.66	1.815	0.379	1.392	0.242	4.63	1.57	4.27	1.48	113.45	179.13	0.218	–	S
2569	23 34 04.98	1.24	-51 32 30.33	1.25	2.745	0.280	0.940	0.189	14.76	3.61	8.23	2.02	132.22	26.31	0.174	–	S
2570	23 34 04.83	2.35	-51 42 34.46	1.18	5.090	0.335	0.829	0.166	25.18	5.71	13.09	2.65	89.03	20.14	0.180	–	S
2571	23 34 03.10	0.32	-51 18 32.07	0.38	5.466	0.568	3.955	0.377	5.91	0.81	4.21	0.70	166.13	40.73	0.290	–	S
2572	23 34 53.94	0.15	-58 59 20.01	0.16	25.696	1.459	20.191	1.133	5.32	0.11	2.46	0.09	164.53	2.26	0.215	-0.71	S
2573	23 33 56.66	0.14	-50 11 48.99	0.15	16.413	0.940	15.593	0.871	2.36	0.09	1.35	0.08	154.61	16.42	0.152	-0.81	S
2574	23 34 42.59	0.31	-57 37 19.28	0.28	4.000	0.317	2.535	0.206	6.72	0.63	5.26	0.56	88.61	31.54	0.141	–	S
2575	23 34 37.48	0.74	-57 00 48.32	0.61	11.841	0.690	2.550	0.237	22.78	2.02	9.07	0.80	51.42	6.14	0.205	–	S
2576	23 34 22.62	1.09	-54 52 14.93	1.04	3.806	0.369	1.337	0.243	13.75	3.01	8.19	1.82	47.41	25.57	0.221	–	S
2577	23 34 58.27	0.70	-59 38 59.89	1.01	8.454	0.669	2.000	0.252	12.60	2.60	4.68	1.19	60.42	16.80	0.227	–	M
2578	23 34 51.46	0.84	-58 46 14.53	0.56	2.107	0.310	1.247	0.206	8.42	1.90	4.56	1.32	91.23	31.51	0.181	–	S
2579	23 34 39.60	0.63	-57 17 56.19	0.72	2.036	0.247	1.082	0.164	8.73	1.76	6.06	1.33	151.36	36.16	0.142	–	S
2580	23 34 33.33	0.68	-56 25 56.46	0.76	1.858	0.300	1.152	0.199	7.18	1.84	5.19	1.48	152.38	57.12	0.175	–	S
2581	23 34 51.90	0.57	-58 51 47.74	0.58	1.776	0.350	1.408	0.223	4.33	1.34	3.64	1.27	152.87	154.13	0.199	–	S
2582	23 34 39.09	0.88	-57 21 08.29	1.12	1.202	0.202	0.634	0.137	9.18	2.75	5.71	1.89	157.89	42.57	0.123	–	S
2583	23 34 08.01	0.40	-52 41 05.38	0.78	10.732	0.958	5.088	0.604	12.40	1.80	4.80	0.85	8.35	11.79	0.508	–	S
2584	23 34 25.68	0.22	-55 40 41.85	0.18	21.539	1.303	10.665	0.650	9.29	0.42	2.59	0.21	166.78	3.86	0.280	–	M
2585	23 34 37.91	0.32	-57 31 03.96	0.23	13.753	0.861	5.210	0.341	12.53	0.74	4.64	0.33	22.11	4.59	0.185	–	M
2586	23 34 55.89	0.17	-59 39 20.17	0.18	9.385	0.651	8.688	0.532	2.40	0.23	1.98	0.21	161.99	63.74	0.230	–	S
2587	23 34 19.38	1.14	-54 46 42.23	1.10	2.938	0.332	1.099	0.228	10.68	2.71	10.04	2.53	65.53	179.11	0.204	–	S
2588	23 34 25.02	1.71	-55 41 15.27	1.78	14.337	0.824	1.479	0.232	32.46	5.17	16.60	2.58	136.49	15.35	0.284	–	S
2589	23 34 46.38	0.14	-58 53 59.26	0.15	95.888	5.304	50.452	2.785	10.55	0.10	1.06	0.04	54.28	0.64	0.232	-0.72	M
2590	23 34 21.37	1.25	-55 40 27.26	1.18	6.351	0.513	1.666	0.318	13.76	2.91	12.96	2.77	76.89	179.11	0.298	–	S
2591	23 34 52.35	0.52	-59 41 10.10	0.47	1.223	0.371	1.358	0.216	0.00	1.12	0.00	1.09	0.00	166.38	0.209	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2592	23 34 00.57	0.53	-52 14 56.52	0.55	4.255	0.598	2.938	0.391	6.89	1.39	3.83	1.01	43.88	30.53	0.334	-	S
2593	23 34 50.85	0.67	-59 35 16.30	0.59	1.380	0.322	1.138	0.202	4.20	1.53	2.96	1.37	72.64	130.81	0.184	-	S
2594	23 34 51.68	0.76	-59 43 04.88	0.74	2.738	0.359	1.437	0.240	8.78	1.95	6.04	1.48	136.09	40.15	0.210	-	S
2595	23 34 43.16	0.26	-58 42 42.66	0.26	3.979	0.408	3.495	0.283	3.04	0.50	2.78	0.49	150.53	89.03	0.202	-	S
2596	23 33 46.18	0.52	-50 11 15.66	0.54	3.055	0.298	1.625	0.193	8.07	1.21	7.42	1.18	53.09	83.94	0.157	-	S
2597	23 34 02.22	0.68	-53 22 51.85	0.62	2.871	0.397	1.732	0.263	7.53	1.63	5.55	1.33	117.40	50.06	0.227	-	S
2598	23 33 56.34	1.31	-52 24 35.45	1.39	14.795	0.915	2.553	0.386	25.05	4.09	12.10	1.86	135.36	14.35	0.401	-	S
2599	23 34 43.49	0.29	-59 31 28.52	0.28	4.581	0.442	3.552	0.300	4.55	0.60	3.84	0.54	55.62	75.07	0.216	-	S
2600	23 34 41.55	0.51	-59 18 05.15	1.28	5.486	0.380	1.513	0.202	19.59	3.03	6.83	1.08	6.69	9.85	0.192	-	S
2601	23 34 19.13	0.14	-56 29 00.30	0.15	40.010	2.239	31.610	1.751	5.62	0.07	1.95	0.05	127.08	1.75	0.207	-0.63	M
2602	23 33 49.18	0.29	-51 17 54.05	0.36	4.947	0.521	3.795	0.348	5.59	0.76	3.37	0.62	0.16	30.21	0.265	-	S
2603	23 33 58.11	0.59	-53 08 50.42	0.74	10.381	0.769	3.624	0.442	13.10	1.78	9.12	1.25	24.03	21.95	0.373	-	S
2604	23 34 04.15	1.93	-54 26 26.58	1.16	8.787	0.566	1.448	0.268	22.95	4.57	13.93	2.67	94.76	22.93	0.284	-	S
2605	23 34 00.52	0.76	-54 03 04.16	1.19	6.418	0.436	1.674	0.226	20.05	3.06	8.21	1.24	26.40	11.40	0.213	-	S
2606	23 34 37.62	1.02	-59 25 34.05	0.32	19.218	1.157	3.550	0.307	20.58	2.37	5.62	0.67	179.49	6.81	0.237	-	M
2607	23 33 52.76	0.76	-52 37 55.89	1.26	4.370	0.676	2.236	0.458	10.76	2.95	5.15	1.70	167.23	29.29	0.413	-	S
2608	23 34 20.74	0.50	-57 20 04.10	0.53	1.530	0.268	1.210	0.172	4.62	1.25	3.43	1.08	16.67	82.14	0.151	-	S
2609	23 34 32.26	0.14	-58 56 46.86	0.15	19.709	1.135	18.687	1.047	2.20	0.09	1.39	0.08	127.22	19.17	0.195	-0.78	S
2610	23 34 37.07	1.53	-59 34 23.68	1.86	8.087	0.485	0.984	0.181	23.46	4.51	18.63	3.43	15.80	35.12	0.209	-	S
2611	23 33 48.72	0.41	-52 16 32.56	0.31	15.546	1.160	8.320	0.709	10.20	0.98	4.78	0.54	67.87	8.77	0.507	-	S
2612	23 34 19.73	0.80	-57 30 32.03	0.93	1.284	0.288	0.876	0.188	6.67	2.30	3.94	1.70	153.63	55.65	0.170	-	S
2613	23 34 06.13	0.36	-55 47 06.96	0.34	6.287	0.469	3.265	0.285	8.68	0.83	6.63	0.68	54.56	22.14	0.204	-	S
2614	23 34 00.47	0.49	-54 53 31.97	0.42	4.737	0.484	2.829	0.316	7.50	1.11	5.61	0.91	71.04	35.22	0.255	-	S
2615	23 34 06.24	0.21	-56 06 29.06	0.16	41.070	2.335	15.107	0.863	18.94	0.38	5.76	0.13	170.64	1.33	0.235	-0.71	M
2616	23 34 13.91	0.16	-57 41 52.56	0.17	7.902	0.508	7.287	0.430	2.95	0.18	1.33	0.17	5.33	15.75	0.154	-0.74	S
2617	23 33 41.97	0.79	-52 33 18.17	0.37	16.018	1.299	5.532	0.542	12.99	1.85	3.77	0.78	173.41	10.97	0.448	-	M
2618	23 33 54.33	0.16	-54 55 39.80	0.18	31.503	1.891	18.915	1.086	8.04	0.24	2.63	0.14	111.46	3.03	0.312	-1.01	M
2619	23 33 55.49	0.16	-55 08 45.21	0.17	18.005	1.062	12.521	0.732	6.20	0.21	4.30	0.17	42.35	6.93	0.233	-1.10	S
2620	23 34 26.64	0.21	-59 38 26.95	0.22	6.175	0.503	5.272	0.367	3.77	0.38	2.57	0.35	157.95	29.69	0.217	-	S
2621	23 34 01.81	0.51	-56 08 11.76	0.61	2.805	0.417	1.905	0.273	6.35	1.41	4.51	1.16	173.16	50.52	0.236	-	S
2622	23 33 29.85	0.33	-50 27 03.66	0.36	3.494	0.312	2.268	0.205	6.82	0.79	5.31	0.68	145.42	39.22	0.151	-	S
2623	23 34 08.47	0.16	-57 34 31.65	0.16	17.843	1.054	14.696	0.824	9.24	0.18	0.00	0.08	15.33	1.43	0.158	-0.88	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2624	23 34 12.77	1.37	-58 06 24.85	1.19	2.976	0.300	0.934	0.203	13.01	3.33	10.31	2.62	59.06	62.45	0.188	–	S
2625	23 34 13.87	1.08	-58 21 14.53	0.84	1.761	0.342	1.044	0.229	8.32	2.60	4.64	1.80	115.16	44.44	0.206	–	S
2626	23 33 52.05	0.30	-55 11 04.08	0.32	3.142	0.404	2.863	0.268	3.06	0.66	1.77	0.61	20.96	68.91	0.213	–	S
2627	23 34 02.56	0.34	-56 57 07.20	0.44	3.911	0.375	2.441	0.244	7.71	0.99	4.39	0.70	15.09	17.52	0.190	–	S
2628	23 34 19.17	0.15	-59 33 12.65	0.18	23.009	1.313	13.118	0.760	9.36	0.25	3.81	0.14	166.93	1.65	0.224	-1.17	S
2629	23 33 54.35	0.48	-55 58 26.95	0.39	4.646	0.419	2.571	0.269	8.34	1.07	5.95	0.85	91.01	26.67	0.211	–	S
2630	23 34 19.09	1.03	-59 40 52.87	0.66	11.796	0.783	2.368	0.274	16.10	2.67	5.08	0.95	150.72	11.02	0.241	–	M
2631	23 33 24.10	0.81	-50 07 15.76	1.07	4.630	0.328	1.272	0.180	17.32	2.72	10.06	1.55	148.02	18.22	0.163	–	S
2632	23 33 51.01	0.15	-56 01 22.38	0.16	14.938	0.885	13.525	0.769	3.67	0.13	0.51	0.11	31.89	5.68	0.192	-0.96	S
2633	23 34 15.37	0.27	-59 40 14.56	0.36	4.886	0.472	3.494	0.314	6.58	0.78	2.75	0.55	171.14	13.65	0.235	–	S
2634	23 34 15.58	0.67	-59 36 45.61	0.60	2.122	0.379	1.502	0.246	6.27	1.63	3.64	1.25	125.98	45.86	0.218	–	S
2635	23 33 25.43	0.65	-51 12 16.72	0.79	2.158	0.322	1.293	0.214	7.59	1.74	5.84	1.57	10.08	76.27	0.187	–	S
2636	23 33 46.13	0.22	-55 38 17.24	0.24	6.470	0.641	6.179	0.461	3.16	0.45	0.00	0.37	31.75	20.51	0.309	–	S
2637	23 33 43.93	0.74	-55 17 38.84	0.80	3.324	0.341	1.446	0.225	9.90	1.90	8.32	1.64	151.43	64.90	0.194	–	S
2638	23 33 38.90	0.14	-54 44 58.95	0.15	44.422	2.471	42.862	2.367	1.72	0.04	1.31	0.04	39.58	20.61	0.214	0.34	S
2639	23 33 51.84	0.15	-57 01 32.10	0.16	14.778	0.874	14.105	0.799	2.33	0.11	0.73	0.11	19.20	13.68	0.187	0.05	S
2640	23 33 50.36	0.16	-56 47 48.67	0.17	9.013	0.567	8.235	0.481	2.86	0.17	1.91	0.16	28.61	22.85	0.160	1.80	S
2641	23 34 07.29	0.33	-59 42 41.19	0.29	4.927	0.429	3.259	0.282	6.36	0.68	4.79	0.60	67.50	33.35	0.203	–	S
2642	23 33 30.56	1.37	-53 47 08.44	0.96	1.926	0.247	0.787	0.170	12.06	3.31	7.41	2.10	105.20	35.02	0.154	–	S
2643	23 33 32.07	0.19	-54 07 33.53	0.19	15.017	1.001	11.541	0.727	5.13	0.31	3.61	0.26	58.41	15.33	0.337	–	S
2644	23 33 28.77	0.89	-53 38 46.57	0.98	3.375	0.308	1.185	0.199	11.70	2.27	10.26	2.06	157.52	90.67	0.176	–	S
2645	23 33 40.76	1.52	-56 00 32.54	0.68	3.618	0.432	0.877	0.192	0.00	3.73	0.00	1.11	0.00	19.10	0.186	–	M
2646	23 33 32.95	0.41	-54 45 02.74	0.45	3.717	0.422	2.497	0.277	6.73	1.07	4.38	0.84	34.95	30.00	0.226	–	S
2647	23 33 29.74	1.02	-54 09 50.09	1.39	18.495	1.198	3.603	0.572	20.03	3.38	13.13	2.18	156.88	23.01	0.567	–	S
2648	23 33 31.19	0.78	-54 27 49.79	0.76	1.967	0.402	1.358	0.262	5.58	1.83	5.18	1.74	108.90	179.28	0.235	–	S
2649	23 33 25.96	0.82	-53 40 14.99	0.76	2.243	0.311	1.203	0.209	8.23	1.94	6.77	1.69	115.94	76.17	0.182	–	S
2650	23 33 23.81	0.26	-53 20 04.32	0.26	4.567	0.419	3.658	0.289	4.37	0.53	3.66	0.50	82.69	59.10	0.199	–	S
2651	23 33 34.81	0.31	-55 38 44.16	0.59	18.376	1.083	5.269	0.422	18.95	1.39	7.24	0.54	163.54	4.86	0.312	–	S
2652	23 33 58.55	0.16	-59 36 43.24	0.24	26.491	1.517	11.276	0.661	11.87	0.43	4.15	0.20	85.01	3.04	0.228	-0.09	M
2653	23 33 17.97	0.88	-52 15 21.93	0.99	8.372	1.629	3.662	0.700	0.00	3.03	0.00	0.62	0.00	13.27	0.670	–	M
2654	23 33 59.87	0.29	-59 43 26.84	0.30	2.753	0.374	2.640	0.247	2.41	0.64	0.00	0.57	30.59	60.51	0.198	–	S
2655	23 34 00.00	0.22	-59 53 33.42	0.22	4.270	0.410	4.125	0.300	2.21	0.39	0.00	0.36	44.69	44.29	0.194	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2656	23 33 49.49	1.73	-58 23 21.24	1.14	4.637	0.351	1.024	0.208	18.06	3.98	11.83	2.69	79.30	32.49	0.206	-	S
2657	23 33 14.22	0.27	-51 43 17.18	0.32	3.608	0.395	3.075	0.268	4.27	0.64	2.42	0.56	175.48	38.73	0.201	-	S
2658	23 33 50.93	0.79	-58 34 09.97	0.70	1.199	0.314	0.973	0.196	5.19	1.96	1.86	1.45	52.63	54.95	0.182	-	S
2659	23 33 48.42	0.39	-58 24 45.42	0.46	2.564	0.359	1.969	0.233	5.28	1.05	3.13	0.85	1.84	36.50	0.197	-	S
2660	23 33 43.06	0.47	-57 36 33.58	1.01	4.903	0.333	1.440	0.173	17.66	2.37	7.50	1.02	5.24	10.09	0.155	-	S
2661	23 33 38.71	0.84	-57 12 31.17	0.87	9.899	0.580	1.666	0.195	17.96	2.09	17.14	1.89	15.67	73.18	0.187	-	S
2662	23 33 19.41	0.56	-53 30 15.02	0.54	4.291	0.353	1.869	0.218	9.46	1.29	8.92	1.22	97.96	100.24	0.177	-	S
2663	23 33 03.87	0.19	-50 18 36.01	0.22	4.155	0.361	4.031	0.275	0.00	0.37	0.00	0.31	0.00	23.30	0.162	-	S
2664	23 33 10.85	1.36	-52 23 37.18	2.13	42.770	2.367	2.309	0.283	45.43	5.23	25.31	2.82	20.15	12.54	0.421	-	S
2665	23 33 11.81	0.35	-52 27 24.50	0.38	6.897	0.707	4.794	0.468	5.74	0.80	5.03	0.77	5.42	106.36	0.361	-	S
2666	23 33 48.19	0.36	-59 13 40.38	0.32	3.207	0.340	2.343	0.226	5.44	0.77	4.05	0.68	93.90	49.74	0.175	-	S
2667	23 33 43.25	0.15	-58 31 14.99	0.16	13.749	0.830	12.941	0.740	2.49	0.13	1.22	0.12	150.67	16.56	0.199	-0.26	S
2668	23 33 26.96	0.20	-55 57 43.91	0.22	4.764	0.373	3.954	0.271	4.47	0.39	2.53	0.33	17.92	18.44	0.156	-	S
2669	23 33 45.02	0.60	-59 08 49.11	0.66	4.183	0.413	1.361	0.174	8.99	1.79	3.25	0.99	129.10	18.86	0.157	-	M
2670	23 33 50.15	0.84	-59 50 00.31	0.81	1.139	0.295	0.862	0.187	5.56	2.18	3.07	1.63	42.23	66.78	0.172	-	S
2671	23 33 44.37	0.70	-59 18 03.48	0.77	13.748	0.875	3.750	0.292	19.44	2.33	3.85	0.62	131.17	6.77	0.207	-	M
2672	23 33 38.61	0.68	-58 23 04.68	0.39	5.370	0.444	2.421	0.274	11.78	1.52	5.72	0.88	87.53	13.32	0.225	-	S
2673	23 33 33.29	0.60	-57 35 45.25	0.86	1.872	0.271	1.073	0.180	8.50	2.00	4.95	1.36	177.11	31.12	0.159	-	S
2674	23 33 05.62	0.15	-52 10 27.65	0.16	292.041	17.773	271.656	15.600	3.94	0.16	0.00	0.12	42.79	4.53	4.425	-0.30	S
2675	23 33 17.81	0.14	-54 56 05.20	0.15	23.298	1.329	21.848	1.219	2.21	0.08	1.90	0.08	30.66	39.37	0.204	-0.35	S
2676	23 33 25.85	0.66	-56 30 12.53	0.87	3.332	0.290	1.257	0.183	12.07	2.07	8.36	1.46	16.81	26.41	0.159	-	S
2677	23 33 26.90	0.35	-56 39 37.10	0.36	2.595	0.320	2.074	0.211	4.77	0.82	3.06	0.70	140.82	41.91	0.169	-	S
2678	23 33 02.59	0.86	-51 41 55.51	0.99	15.746	0.888	1.926	0.205	24.30	2.38	19.70	1.91	148.58	25.75	0.212	-	S
2679	23 33 08.41	0.31	-54 16 16.34	1.03	463.700	25.564	20.068	1.560	65.39	2.41	17.36	0.60	95.87	2.79	1.103	-	M
2680	23 33 08.53	0.47	-53 15 06.32	0.65	3.297	0.350	1.812	0.229	9.20	1.50	5.43	1.02	164.90	23.32	0.191	-	S
2681	23 32 56.43	0.69	-50 15 03.97	0.69	1.790	0.259	1.082	0.172	7.25	1.64	6.09	1.52	121.39	80.97	0.149	-	S
2682	23 33 20.75	0.70	-55 56 35.53	0.60	1.394	0.273	1.057	0.174	6.44	1.75	1.78	1.15	55.74	30.53	0.157	-	S
2683	23 32 55.40	0.17	-50 18 32.33	0.18	8.017	0.523	6.790	0.411	3.85	0.23	3.18	0.22	160.25	48.30	0.165	-0.69	S
2684	23 33 22.06	0.19	-56 38 02.38	0.20	6.100	0.466	5.476	0.358	2.91	0.30	2.41	0.29	39.15	72.72	0.189	-	S
2685	23 33 05.13	1.20	-53 20 12.12	1.02	2.566	0.275	0.948	0.186	12.62	3.03	8.59	2.08	118.74	36.60	0.168	-	S
2686	23 33 26.03	0.17	-57 35 44.68	0.19	6.380	0.446	5.476	0.344	3.81	0.27	2.45	0.25	175.68	19.42	0.161	-	S
2687	23 33 28.75	0.17	-58 18 08.10	0.18	9.254	0.625	8.206	0.501	3.83	0.24	1.13	0.20	7.57	10.57	0.212	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2688	23 33 06.56	3.56	-55 02 27.36	4.59	15.557	1.006	3.262	0.319	58.22	13.58	6.40	1.49	51.73	12.18	0.264	–	M
2689	23 33 12.50	1.43	-55 40 13.31	1.18	11.747	0.676	1.427	0.194	27.66	3.76	16.32	2.16	54.94	15.23	0.217	–	S
2690	23 33 35.14	0.61	-59 29 04.26	0.59	1.255	0.320	1.127	0.197	3.52	1.51	1.31	1.23	40.49	87.17	0.182	–	S
2691	23 32 49.84	0.32	-50 08 53.63	0.33	2.733	0.321	2.294	0.214	4.41	0.74	2.66	0.63	124.13	40.02	0.167	–	S
2692	23 33 34.64	0.73	-59 55 49.97	0.96	2.202	0.332	1.195	0.222	9.29	2.38	4.82	1.48	22.67	28.14	0.198	–	S
2693	23 33 19.30	0.35	-57 32 22.40	0.30	5.019	0.431	3.225	0.281	7.32	0.77	4.35	0.58	61.49	16.75	0.204	–	S
2694	23 32 59.30	0.14	-53 25 59.04	0.15	46.269	2.562	45.682	2.518	1.48	0.03	0.00	0.03	129.00	7.03	0.170	-0.19	S
2695	23 33 31.04	0.14	-59 43 42.94	0.15	44.520	2.490	37.098	2.052	6.22	0.07	1.98	0.05	99.05	1.37	0.216	0.10	M
2696	23 32 53.01	0.88	-52 01 36.81	0.72	3.572	0.784	2.581	0.503	6.97	2.23	2.55	1.44	62.94	36.11	0.459	–	S
2697	23 32 49.62	0.20	-51 52 24.28	0.23	8.454	0.632	6.703	0.454	5.35	0.41	2.83	0.32	16.47	14.21	0.254	–	S
2698	23 32 47.92	0.73	-51 32 02.74	1.15	2.663	0.289	1.191	0.190	14.35	2.98	4.07	1.12	150.99	14.18	0.173	–	S
2699	23 33 03.22	0.68	-55 24 29.69	0.77	1.536	0.330	1.131	0.212	5.62	1.83	3.84	1.52	20.10	76.75	0.191	–	S
2700	23 32 58.50	0.23	-54 25 03.57	0.24	10.999	0.989	9.343	0.700	3.65	0.45	3.09	0.44	10.06	85.49	0.459	–	S
2701	23 33 06.83	0.17	-56 35 34.83	0.19	10.056	0.643	7.675	0.470	4.97	0.26	3.80	0.23	178.44	16.28	0.196	–	S
2702	23 32 44.57	0.51	-51 24 29.75	0.65	2.287	0.299	1.422	0.197	7.54	1.46	5.25	1.20	175.29	46.65	0.168	–	S
2703	23 33 20.94	0.33	-59 44 09.82	0.34	6.344	0.481	3.433	0.297	7.97	0.76	6.37	0.66	146.42	25.69	0.211	–	S
2704	23 32 51.27	0.39	-53 48 04.84	0.38	6.010	0.426	2.787	0.247	10.52	1.00	6.82	0.68	48.79	13.53	0.179	–	S
2705	23 32 56.16	0.37	-55 05 25.66	0.39	4.433	0.479	3.098	0.316	5.56	0.85	4.93	0.79	2.32	97.58	0.249	–	S
2706	23 32 43.12	0.16	-52 08 27.56	0.17	44.398	2.688	36.629	2.129	4.82	0.19	2.41	0.15	42.33	6.88	0.663	-0.95	S
2707	23 32 36.59	0.20	-50 56 41.83	0.31	84.905	4.848	37.070	2.091	23.63	0.71	3.85	0.15	114.50	1.62	0.462	-1.21	M
2708	23 32 53.11	0.33	-55 10 56.23	0.21	65.274	3.753	25.677	1.466	27.98	0.77	3.72	0.14	23.47	1.39	0.393	-1.40	M
2709	23 33 14.34	0.62	-59 01 04.29	0.49	1.561	0.307	1.278	0.194	5.37	1.43	1.17	1.04	64.48	34.75	0.174	–	S
2710	23 33 18.49	0.18	-59 57 46.62	0.19	6.981	0.557	6.759	0.440	0.00	0.29	0.00	0.27	0.00	26.29	0.234	–	S
2711	23 32 57.98	0.77	-55 57 25.59	1.36	1.574	0.237	0.760	0.161	11.35	3.22	5.07	1.71	9.82	26.33	0.147	–	S
2712	23 33 16.18	0.56	-59 30 30.75	0.56	1.807	0.319	1.366	0.205	5.37	1.40	3.36	1.13	39.05	53.24	0.181	–	S
2713	23 33 00.41	0.22	-57 02 11.41	0.22	7.053	0.645	6.395	0.467	2.94	0.41	2.08	0.38	47.36	62.20	0.300	–	S
2714	23 33 06.83	1.00	-58 17 28.39	0.78	2.147	0.364	1.210	0.245	8.30	2.34	5.53	1.77	106.88	53.88	0.218	–	S
2715	23 32 44.31	0.27	-53 33 28.03	0.27	3.649	0.361	3.054	0.249	4.57	0.59	2.28	0.48	120.78	24.72	0.177	–	S
2716	23 33 04.65	0.80	-58 35 45.73	1.09	2.388	0.278	1.016	0.188	11.29	2.65	6.93	1.70	18.88	29.01	0.168	–	S
2717	23 32 55.41	0.38	-56 46 35.58	0.48	2.792	0.333	1.931	0.219	6.72	1.10	3.63	0.81	161.28	23.97	0.180	–	S
2718	23 32 30.25	0.47	-50 20 59.97	0.52	2.472	0.294	1.590	0.193	6.57	1.16	5.74	1.07	155.43	140.38	0.160	–	S
2719	23 32 30.18	0.57	-50 53 43.99	0.62	11.033	0.809	4.082	0.464	11.31	1.37	10.17	1.32	34.24	72.16	0.379	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2720	23 32 36.70	0.21	-52 49 50.15	0.24	11.622	1.000	9.921	0.718	4.18	0.45	2.40	0.38	173.93	27.06	0.451	-	S
2721	23 32 46.09	1.05	-55 26 30.32	0.86	5.100	0.548	1.160	0.240	8.66	2.95	0.00	1.11	142.03	19.90	0.231	-	M
2722	23 32 56.48	1.83	-57 47 42.28	0.55	10.189	0.699	1.989	0.236	22.52	4.40	1.52	0.82	11.81	9.17	0.209	-	M
2723	23 32 51.37	0.61	-56 42 37.74	0.62	1.623	0.285	1.160	0.185	5.90	1.55	4.03	1.27	138.20	60.50	0.163	-	S
2724	23 32 57.96	0.17	-58 23 32.31	0.17	15.881	1.074	12.229	0.723	5.47	0.25	0.00	0.15	141.10	4.08	0.266	-0.71	M
2725	23 32 26.72	1.54	-50 38 04.65	1.33	6.336	0.480	1.040	0.184	16.54	4.52	3.99	1.50	139.77	18.20	0.175	-	M
2726	23 33 05.59	0.14	-59 55 59.89	0.15	43.775	2.456	34.431	1.907	6.70	0.08	2.20	0.05	177.88	1.28	0.226	-0.97	M
2727	23 33 04.25	0.15	-59 46 08.07	0.16	20.729	1.197	18.315	1.031	3.67	0.10	1.66	0.09	145.97	5.70	0.214	-0.79	S
2728	23 32 26.69	0.72	-50 38 33.85	0.75	2.535	0.308	1.317	0.205	8.95	1.85	6.89	1.51	47.39	49.00	0.177	-	S
2729	23 32 27.62	1.10	-51 03 12.79	0.78	4.432	0.347	1.430	0.207	16.88	2.96	7.45	1.26	116.80	13.78	0.188	-	S
2730	23 32 57.65	0.56	-58 33 34.78	0.50	3.344	0.330	1.765	0.214	9.09	1.37	5.73	0.99	52.06	23.29	0.177	-	S
2731	23 32 28.59	0.49	-51 33 17.44	0.52	3.225	0.334	1.848	0.218	7.91	1.23	6.21	1.04	134.69	44.45	0.178	-	S
2732	23 32 27.19	0.50	-51 17 19.54	0.75	7.679	0.521	2.539	0.274	15.69	1.84	8.11	0.95	23.76	11.61	0.228	-	S
2733	23 32 59.08	1.05	-58 58 57.64	1.47	2.606	0.265	0.830	0.180	13.41	3.50	9.54	2.41	1.21	38.60	0.166	-	S
2734	23 32 55.67	0.38	-58 26 45.11	0.39	6.357	0.545	3.579	0.348	7.17	0.88	6.64	0.79	20.35	69.67	0.264	-	S
2735	23 32 51.86	1.04	-57 48 02.99	0.71	6.240	0.557	1.615	0.227	12.02	2.77	0.00	0.90	148.20	13.08	0.209	-	M
2736	23 33 01.41	0.75	-59 53 08.05	0.81	1.313	0.358	1.051	0.225	4.66	2.02	2.93	1.60	159.99	92.61	0.208	-	S
2737	23 32 58.92	0.61	-59 31 27.77	0.75	3.436	0.296	1.395	0.186	11.97	1.89	6.95	1.17	27.41	17.78	0.159	-	S
2738	23 32 38.29	0.14	-57 02 29.22	0.15	143.084	7.909	82.424	4.545	9.21	0.06	1.59	0.03	157.00	0.54	0.326	-1.10	M
2739	23 32 25.52	0.79	-51 34 13.94	0.82	1.360	0.317	1.004	0.203	5.04	1.94	4.70	1.78	48.15	179.50	0.185	-	S
2740	23 32 51.00	0.14	-58 25 27.38	0.15	77.178	4.285	54.026	2.984	8.43	0.07	4.20	0.04	36.29	0.97	0.276	-0.32	M
2741	23 32 48.32	0.41	-58 13 40.53	1.16	12.339	0.814	4.743	0.334	19.15	2.73	5.38	0.88	93.31	9.38	0.209	-	M
2742	23 32 19.57	0.21	-50 14 22.51	0.23	5.002	0.370	3.880	0.264	4.84	0.38	4.05	0.37	159.02	58.34	0.147	-	S
2743	23 32 22.02	0.65	-50 59 22.59	0.63	4.648	0.562	2.618	0.372	8.77	1.70	5.65	1.21	127.02	30.84	0.318	-	S
2744	23 32 43.79	0.35	-57 09 29.36	0.51	9.899	0.699	4.182	0.395	11.45	1.16	7.05	0.75	3.55	12.51	0.300	-	S
2745	23 32 36.58	0.98	-55 21 21.54	1.03	1.842	0.341	1.029	0.231	7.81	2.52	6.38	2.14	33.03	101.60	0.206	-	S
2746	23 32 47.73	0.14	-58 33 29.63	0.15	28.939	1.624	28.222	1.564	1.34	0.05	1.16	0.05	121.02	89.62	0.188	-0.19	S
2747	23 32 38.24	0.39	-56 28 00.91	0.46	2.567	0.333	1.892	0.218	5.58	1.03	3.79	0.85	0.02	41.62	0.181	-	S
2748	23 32 47.83	0.22	-58 54 34.09	0.22	7.953	0.527	5.019	0.338	7.18	0.43	4.74	0.34	132.07	11.15	0.181	-	S
2749	23 32 49.34	0.47	-59 17 02.10	0.45	5.204	0.376	2.140	0.216	9.90	1.09	8.81	0.97	46.93	51.78	0.167	-	S
2750	23 32 18.40	1.37	-51 13 34.83	1.77	5.816	0.428	1.188	0.248	18.28	4.01	14.28	3.34	173.73	58.49	0.248	-	S
2751	23 32 27.45	0.74	-53 58 27.79	0.65	0.987	0.323	0.951	0.193	0.00	1.72	0.00	1.49	0.00	107.24	0.184	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2752	23 32 47.96	1.49	-59 44 01.48	0.99	14.282	0.864	2.314	0.245	24.95	4.08	4.68	0.88	147.14	8.67	0.209	–	M
2753	23 32 40.73	1.52	-58 21 45.48	1.51	3.896	0.332	0.967	0.214	16.72	4.18	10.92	2.73	136.70	34.19	0.208	–	S
2754	23 32 14.98	0.56	-51 29 21.71	0.54	1.106	0.289	1.089	0.174	0.00	1.31	0.00	1.17	0.00	80.95	0.163	–	S
2755	23 32 15.78	1.58	-52 48 07.07	0.57	43.933	2.748	15.960	1.108	22.96	3.87	0.00	0.70	162.72	8.08	0.677	–	M
2756	23 32 11.39	0.24	-51 15 47.30	0.17	26.516	1.612	11.317	0.673	12.70	0.46	4.23	0.21	0.96	3.11	0.257	–	M
2757	23 32 23.61	0.30	-55 04 40.07	0.29	4.922	0.466	3.685	0.314	5.42	0.65	3.76	0.55	50.52	30.18	0.227	–	S
2758	23 32 12.02	0.15	-51 38 56.17	0.16	12.736	0.758	10.599	0.609	3.94	0.15	3.41	0.15	19.03	35.42	0.171	-0.47	S
2759	23 32 07.28	0.17	-50 36 27.75	0.19	10.958	0.678	8.004	0.482	6.30	0.28	3.57	0.20	141.92	7.34	0.187	-0.79	S
2760	23 32 41.32	0.57	-59 52 00.32	0.64	2.157	0.360	1.504	0.234	6.53	1.59	3.49	1.16	149.78	35.31	0.206	–	S
2761	23 32 23.75	1.12	-55 46 51.75	1.31	2.652	0.289	0.922	0.198	12.37	3.20	9.48	2.44	24.85	52.92	0.180	–	S
2762	23 32 28.79	0.78	-57 07 58.35	0.72	3.290	0.443	1.759	0.297	7.86	1.82	6.89	1.65	112.63	128.19	0.259	–	S
2763	23 32 16.13	0.58	-53 47 12.47	0.68	3.575	0.300	1.468	0.186	10.79	1.59	8.55	1.30	160.81	39.03	0.155	–	S
2764	23 32 24.85	1.63	-56 47 28.06	1.04	14.660	0.907	2.705	0.271	24.95	4.36	7.02	1.22	149.59	11.09	0.226	–	M
2765	23 32 15.19	0.73	-54 42 09.68	1.18	42.519	2.571	4.663	0.505	28.70	3.09	9.17	0.95	117.75	7.56	0.436	–	M
2766	23 32 15.50	0.73	-54 05 58.37	0.57	2.663	0.455	1.831	0.296	6.74	1.71	3.93	1.27	83.13	41.06	0.262	–	S
2767	23 32 08.13	0.21	-51 48 23.16	0.24	4.457	0.449	4.450	0.327	0.00	0.43	0.00	0.37	0.00	29.18	0.217	–	S
2768	23 32 29.51	0.55	-58 29 25.87	0.49	2.028	0.427	1.773	0.267	4.15	1.31	1.26	1.05	122.00	54.73	0.241	–	S
2769	23 32 05.71	0.31	-51 51 34.06	0.36	7.197	0.614	4.531	0.399	7.33	0.79	5.18	0.63	154.09	25.36	0.290	–	S
2770	23 32 30.32	0.67	-58 45 24.63	0.63	1.315	0.256	0.986	0.164	6.65	1.77	1.46	1.13	133.78	28.13	0.148	–	S
2771	23 32 26.82	0.35	-58 49 36.46	0.35	2.413	0.316	2.016	0.208	4.10	0.80	2.76	0.70	135.01	58.03	0.169	–	S
2772	23 32 29.99	0.67	-59 41 10.73	0.64	2.153	0.330	1.348	0.218	6.86	1.66	5.16	1.35	133.24	63.01	0.190	–	S
2773	23 32 13.97	0.31	-56 11 59.83	0.31	2.862	0.349	2.506	0.233	3.33	0.66	2.63	0.61	40.83	104.60	0.182	–	S
2774	23 31 58.78	0.91	-50 51 48.04	0.74	4.781	0.514	2.107	0.342	10.44	2.18	8.05	1.64	95.43	39.63	0.297	–	S
2775	23 32 11.17	0.17	-55 13 49.50	0.17	9.680	0.656	9.089	0.549	2.57	0.21	1.33	0.20	48.03	28.40	0.223	-0.72	S
2776	23 32 07.53	0.47	-54 43 54.93	0.81	15.481	0.971	4.298	0.442	18.25	1.95	8.39	0.89	18.60	9.00	0.375	–	S
2777	23 31 55.62	0.17	-50 21 59.77	0.17	19.674	1.121	11.527	0.664	9.86	0.26	3.59	0.13	53.68	1.93	0.185	-0.84	S
2778	23 31 57.62	0.76	-50 54 02.60	0.84	2.284	0.427	1.493	0.281	7.02	1.99	4.92	1.69	141.40	67.42	0.250	–	S
2779	23 32 11.34	0.78	-55 55 19.03	1.03	1.287	0.269	0.839	0.176	8.11	2.57	3.09	1.55	152.77	33.06	0.160	–	S
2780	23 32 05.07	0.52	-54 00 32.06	0.57	1.424	0.300	1.247	0.187	4.92	1.43	0.00	1.00	142.93	33.44	0.170	–	S
2781	23 31 54.93	0.14	-51 19 41.96	0.15	36.912	2.078	32.584	1.812	3.41	0.07	2.54	0.07	150.53	10.52	0.258	-0.81	S
2782	23 31 52.22	0.77	-50 02 09.38	0.99	1.649	0.345	1.094	0.226	7.06	2.16	4.74	1.89	179.49	78.42	0.204	–	S
2783	23 31 58.03	1.13	-52 40 24.77	1.81	10.508	0.738	2.103	0.405	20.16	4.21	12.83	2.66	175.64	28.52	0.408	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2784	23 32 15.73	1.20	-58 16 02.11	1.05	2.016	0.273	0.859	0.189	10.90	3.03	7.40	2.17	125.33	46.66	0.170	–	S
2785	23 31 59.07	0.29	-53 25 38.57	0.34	4.183	0.378	2.896	0.251	6.62	0.74	4.06	0.57	150.93	20.58	0.182	–	S
2786	23 31 52.97	0.28	-51 28 52.32	0.30	4.130	0.385	3.152	0.261	5.15	0.61	3.95	0.55	144.12	44.55	0.185	–	S
2787	23 31 57.95	0.28	-53 30 37.37	0.40	10.418	0.675	4.574	0.361	11.86	0.90	6.51	0.53	14.12	8.49	0.243	–	S
2788	23 31 51.15	0.26	-50 51 54.06	0.30	5.074	0.571	4.614	0.391	3.50	0.59	1.43	0.52	176.81	42.11	0.291	–	S
2789	23 31 54.90	0.59	-52 22 14.29	1.06	3.367	0.503	1.905	0.334	10.21	2.48	3.91	1.31	170.74	22.91	0.299	–	S
2790	23 32 09.39	0.15	-57 22 20.49	0.16	13.398	0.810	11.847	0.682	3.45	0.15	2.11	0.14	161.06	12.43	0.197	-0.90	S
2791	23 31 50.71	1.05	-50 59 26.69	1.05	2.737	0.439	1.412	0.299	10.04	2.90	5.85	1.88	130.79	37.87	0.268	–	S
2792	23 31 51.95	0.18	-52 04 04.42	0.18	56.075	3.178	21.879	1.272	10.90	0.29	5.89	0.18	31.38	3.24	0.411	-0.86	M
2793	23 31 47.86	2.02	-50 33 46.60	1.59	5.318	0.333	0.802	0.147	27.74	5.70	13.17	2.41	121.74	17.60	0.163	–	S
2794	23 31 47.34	0.66	-50 04 53.23	0.75	1.151	0.339	1.053	0.206	3.46	1.70	1.16	1.55	30.06	114.71	0.194	–	S
2795	23 31 47.22	2.53	-50 59 04.38	1.81	28.903	1.596	1.206	0.154	54.29	6.79	28.28	3.18	63.24	12.08	0.260	–	S
2796	23 32 06.25	0.14	-58 08 46.87	0.15	23.182	1.315	21.779	1.213	2.53	0.07	1.20	0.07	1.80	8.57	0.187	-0.39	S
2797	23 32 05.78	0.20	-57 58 37.08	0.21	5.654	0.454	4.875	0.335	3.50	0.36	2.73	0.34	167.09	44.35	0.194	–	S
2798	23 32 01.66	0.34	-56 44 52.77	0.41	5.184	0.580	3.791	0.382	6.72	0.96	2.29	0.64	151.17	16.20	0.304	–	S
2799	23 32 07.24	0.69	-58 32 12.88	0.62	2.061	0.370	1.427	0.241	5.73	1.57	4.72	1.45	100.30	139.47	0.214	–	S
2800	23 31 50.00	0.22	-52 54 29.85	0.25	4.176	0.590	5.055	0.404	0.00	0.46	0.00	0.40	0.00	36.22	0.310	–	S
2801	23 32 07.00	0.71	-58 29 49.05	0.90	2.958	0.377	1.501	0.252	10.36	2.29	4.99	1.33	150.59	22.56	0.223	–	S
2802	23 32 02.92	0.46	-57 17 02.41	0.62	1.554	0.296	1.266	0.188	5.43	1.43	0.96	1.01	11.34	31.80	0.168	–	S
2803	23 31 50.74	0.38	-53 26 09.48	0.55	3.227	0.359	2.086	0.234	8.42	1.29	3.16	0.75	19.23	15.63	0.193	–	S
2804	23 31 57.63	0.20	-55 58 19.47	0.23	5.780	0.442	4.614	0.317	5.04	0.41	2.72	0.33	13.94	14.92	0.182	–	S
2805	23 31 41.74	0.43	-50 01 01.65	0.64	3.883	0.420	2.247	0.275	9.09	1.46	5.07	0.97	3.56	23.61	0.228	–	S
2806	23 31 47.54	0.15	-53 04 07.06	0.16	19.798	1.163	17.470	0.992	3.12	0.12	2.80	0.12	176.74	57.64	0.239	-0.41	S
2807	23 31 38.15	0.31	-50 04 16.53	0.37	6.263	0.501	3.777	0.320	9.06	0.90	4.22	0.53	34.14	10.94	0.228	–	S
2808	23 31 52.13	0.30	-55 25 35.43	0.30	24.889	1.485	7.524	0.510	12.29	0.73	7.92	0.48	43.60	8.39	0.299	–	M
2809	23 31 42.30	0.85	-51 20 56.19	0.48	10.158	0.736	2.455	0.273	15.05	2.11	3.68	0.76	157.47	9.81	0.238	–	M
2810	23 31 50.99	0.47	-55 00 09.84	0.60	3.149	0.301	1.608	0.194	9.18	1.38	6.47	1.04	13.77	28.24	0.159	–	S
2811	23 31 57.68	0.28	-57 19 13.36	0.27	2.988	0.359	2.806	0.243	2.58	0.57	1.25	0.52	126.07	72.92	0.185	–	S
2812	23 31 39.25	0.29	-51 05 59.79	0.19	23.788	1.372	7.685	0.487	15.06	0.60	6.21	0.28	173.71	3.68	0.241	–	M
2813	23 31 38.64	0.53	-51 26 02.23	1.17	5.824	0.557	1.825	0.236	13.72	2.93	0.00	0.64	110.64	9.48	0.213	–	M
2814	23 31 57.76	0.45	-58 25 25.52	0.66	4.662	0.364	1.958	0.217	12.52	1.60	6.00	0.85	156.91	11.82	0.179	–	S
2815	23 31 44.08	0.20	-53 52 00.41	0.21	4.152	0.374	4.074	0.282	1.84	0.35	0.00	0.33	138.42	54.88	0.171	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2816	23 31 59.68	0.90	-59 18 38.33	0.70	1.345	0.272	0.894	0.178	6.82	2.10	4.25	1.60	105.80	59.87	0.160	–	S
2817	23 31 53.50	0.58	-57 27 32.98	0.69	1.651	0.362	1.320	0.228	5.15	1.65	2.38	1.27	161.35	51.44	0.207	–	S
2818	23 31 52.26	0.59	-57 22 09.78	0.67	1.112	0.297	1.006	0.182	3.88	1.62	0.00	1.26	155.80	61.67	0.170	–	S
2819	23 31 56.96	0.34	-59 13 03.38	0.29	3.367	0.356	2.593	0.238	5.10	0.70	3.41	0.61	101.47	38.57	0.181	–	S
2820	23 31 40.03	1.25	-53 11 47.79	1.17	3.059	0.317	1.026	0.215	11.83	2.97	10.95	2.69	75.99	130.41	0.196	–	S
2821	23 31 58.60	1.03	-59 35 52.72	1.00	1.463	0.258	0.780	0.176	8.41	2.68	6.18	2.03	137.20	67.53	0.157	–	S
2822	23 31 51.41	0.40	-57 36 15.32	0.54	11.540	0.859	4.959	0.504	10.99	1.24	7.17	0.85	11.00	15.67	0.395	–	S
2823	23 31 46.02	0.73	-55 37 27.87	0.88	3.132	0.360	1.482	0.240	10.91	2.27	5.92	1.37	32.59	23.72	0.210	–	S
2824	23 31 46.60	1.49	-56 14 56.60	1.29	4.852	0.364	1.121	0.213	18.86	4.00	10.73	2.26	127.31	23.47	0.209	–	S
2825	23 31 44.92	0.89	-55 36 58.99	0.76	1.498	0.364	1.100	0.233	5.56	2.07	3.97	1.75	100.18	101.57	0.213	–	S
2826	23 31 52.77	1.04	-58 31 29.58	0.65	3.145	0.323	1.314	0.213	12.42	2.43	6.32	1.41	71.78	21.28	0.189	–	S
2827	23 31 45.23	0.16	-56 21 46.47	0.17	11.491	0.767	10.768	0.645	2.17	0.20	1.93	0.19	30.15	121.83	0.252	-0.36	S
2828	23 31 37.49	1.42	-53 37 28.73	1.88	4.838	0.481	0.989	0.210	14.36	5.46	0.00	0.81	126.47	13.05	0.203	–	M
2829	23 31 30.36	0.42	-50 11 52.03	0.40	2.965	0.356	2.181	0.234	6.03	1.01	3.69	0.78	118.30	30.45	0.190	–	S
2830	23 31 37.32	0.91	-53 38 06.44	0.82	1.771	0.334	1.105	0.221	7.81	2.33	4.59	1.66	55.77	44.79	0.198	–	S
2831	23 31 36.09	0.42	-53 29 26.92	0.45	11.732	0.720	3.911	0.327	15.46	1.23	7.80	0.63	137.46	7.49	0.238	–	S
2832	23 31 53.70	0.24	-59 39 17.50	0.24	2.880	0.315	2.764	0.220	1.98	0.48	1.09	0.44	145.86	105.02	0.158	–	S
2833	23 31 49.66	0.19	-59 06 52.29	0.22	31.742	1.821	11.459	0.681	12.47	0.38	9.27	0.29	93.59	6.81	0.258	–	M
2834	23 31 44.84	0.15	-57 37 26.72	0.16	53.422	3.092	36.588	2.055	9.84	0.19	3.30	0.10	46.59	1.69	0.418	-1.26	M
2835	23 31 33.60	1.43	-52 55 57.49	0.78	3.746	0.524	1.694	0.359	12.12	3.43	5.72	1.77	90.67	26.32	0.327	–	S
2836	23 31 50.41	0.16	-59 32 51.29	0.16	9.504	0.587	8.331	0.486	3.27	0.16	2.56	0.16	130.38	27.29	0.157	-0.50	S
2837	23 31 39.28	1.75	-56 14 13.21	1.37	5.804	0.405	1.100	0.220	20.05	4.34	13.24	2.85	117.08	30.62	0.226	–	S
2838	23 31 31.48	0.23	-53 07 42.12	0.24	5.826	0.483	4.679	0.341	4.29	0.44	3.72	0.43	26.44	77.08	0.214	–	S
2839	23 31 31.02	0.41	-53 48 31.76	0.39	3.693	0.352	2.262	0.229	7.05	0.94	5.75	0.82	116.65	44.19	0.178	–	S
2840	23 31 39.61	0.34	-57 31 00.97	0.29	11.296	0.748	3.907	0.301	8.17	0.74	5.57	0.55	159.68	15.74	0.211	–	M
2841	23 31 36.54	0.74	-56 17 23.80	0.77	1.430	0.367	1.141	0.231	4.81	1.90	3.06	1.58	144.00	94.26	0.212	–	S
2842	23 31 26.68	0.54	-52 08 43.18	0.95	11.526	0.749	3.226	0.364	19.06	2.34	8.11	0.99	20.65	10.01	0.321	–	S
2843	23 31 26.61	0.87	-52 23 16.44	0.77	14.738	0.879	2.848	0.328	18.68	2.17	14.70	1.62	117.18	23.15	0.303	–	S
2844	23 31 31.49	1.17	-54 54 49.76	1.45	3.389	0.334	1.061	0.225	14.73	3.69	9.23	2.32	149.81	32.62	0.209	–	S
2845	23 31 43.55	0.44	-59 43 24.34	0.50	2.614	0.292	1.606	0.192	6.82	1.15	5.46	0.96	169.57	43.94	0.158	–	S
2846	23 31 33.43	0.15	-56 27 52.74	0.16	40.970	2.348	32.315	1.824	5.42	0.13	2.49	0.10	115.62	3.60	0.393	-1.20	S
2847	23 31 19.70	0.78	-50 15 55.93	0.92	4.059	0.350	1.458	0.221	12.60	2.21	9.56	1.71	33.20	39.20	0.193	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2848	23 31 25.02	0.61	-53 10 35.88	0.56	2.230	0.380	1.641	0.246	5.95	1.48	3.58	1.17	118.34	46.48	0.216	–	S
2849	23 31 19.48	0.28	-50 27 29.46	0.35	2.798	0.310	2.311	0.208	4.97	0.73	2.43	0.58	167.29	29.22	0.159	–	S
2850	23 31 19.90	0.72	-51 22 11.68	0.77	2.299	0.306	1.248	0.205	7.83	1.79	7.21	1.66	8.43	179.73	0.178	–	S
2851	23 31 26.31	0.58	-54 40 47.71	0.71	2.723	0.598	2.176	0.378	5.03	1.63	2.84	1.34	178.58	66.41	0.343	–	S
2852	23 31 18.90	1.29	-51 14 08.50	0.71	10.702	0.644	1.949	0.247	23.21	3.20	12.47	1.51	80.92	12.64	0.244	–	S
2853	23 31 33.73	0.30	-58 11 32.98	0.29	3.253	0.334	2.565	0.225	4.62	0.64	3.47	0.57	128.75	49.68	0.168	–	S
2854	23 31 28.47	1.89	-56 40 58.82	1.29	5.137	0.344	0.884	0.176	20.72	4.38	14.43	3.07	87.39	34.28	0.185	–	S
2855	23 31 15.55	0.51	-50 14 57.58	0.64	10.954	0.652	2.658	0.251	17.15	1.54	12.30	1.08	152.21	16.39	0.204	–	S
2856	23 31 15.25	0.27	-51 05 24.41	0.33	20.782	1.256	10.861	0.637	16.09	0.85	1.73	0.24	127.38	3.04	0.221	-0.96	M
2857	23 31 22.76	0.93	-55 15 26.66	1.22	2.743	0.303	1.043	0.206	11.99	2.90	8.47	2.08	16.77	41.17	0.185	–	S
2858	23 31 29.82	0.25	-58 36 58.14	0.27	4.112	0.395	3.345	0.271	4.25	0.55	3.17	0.49	177.16	41.02	0.191	–	S
2859	23 31 16.04	0.17	-52 11 48.48	0.18	15.785	1.049	13.537	0.826	4.35	0.26	1.98	0.21	39.39	11.46	0.346	–	S
2860	23 31 16.44	0.16	-52 35 43.46	0.16	41.565	2.391	26.408	1.494	8.65	0.19	3.52	0.12	169.06	2.48	0.348	-1.29	M
2861	23 31 23.18	0.17	-56 28 11.38	0.17	39.019	2.294	21.907	1.269	7.91	0.25	4.45	0.17	36.37	4.38	0.399	-1.29	M
2862	23 31 28.89	1.03	-58 40 01.26	1.15	2.964	0.300	1.054	0.200	13.39	3.07	7.88	1.86	35.38	26.84	0.183	–	S
2863	23 31 19.32	0.21	-55 27 02.02	0.30	18.445	1.118	6.986	0.452	12.20	0.62	7.13	0.38	95.65	6.25	0.238	–	M
2864	23 31 11.01	0.14	-50 41 13.93	0.15	60.930	3.367	56.129	3.093	2.85	0.03	1.88	0.03	48.07	4.16	0.187	-0.83	S
2865	23 31 26.88	0.52	-58 39 42.90	0.45	2.697	0.341	1.790	0.224	6.47	1.18	4.67	0.99	114.95	48.82	0.188	–	S
2866	23 31 14.51	1.24	-53 15 41.18	1.76	13.883	0.778	1.209	0.153	36.84	4.57	18.21	2.15	29.46	12.00	0.192	–	S
2867	23 31 14.66	0.33	-53 52 38.30	0.32	3.376	0.337	2.452	0.225	5.44	0.73	4.43	0.66	111.36	52.60	0.169	–	S
2868	23 31 12.64	0.15	-53 20 14.12	0.16	20.082	1.147	16.402	0.922	5.14	0.12	2.16	0.09	20.23	3.54	0.182	-1.03	S
2869	23 31 24.80	0.36	-59 06 59.35	0.39	3.238	0.386	2.413	0.254	5.14	0.88	3.92	0.76	9.34	48.08	0.205	–	S
2870	23 31 07.83	0.78	-50 23 50.57	1.64	2.377	0.258	0.869	0.175	15.43	3.81	6.89	1.83	178.86	23.13	0.162	–	S
2871	23 31 13.79	0.17	-54 30 24.43	0.18	14.409	0.937	12.223	0.738	3.65	0.22	3.12	0.21	173.89	45.08	0.294	-0.70	S
2872	23 31 13.29	0.42	-54 16 01.66	0.46	2.411	0.319	1.772	0.209	5.31	1.02	4.32	0.94	12.87	83.00	0.174	–	S
2873	23 31 08.57	0.16	-51 49 50.99	0.17	10.812	0.728	10.554	0.630	1.74	0.20	0.41	0.19	76.96	43.41	0.243	-0.16	S
2874	23 31 20.49	0.15	-58 56 11.15	0.16	13.731	0.821	13.062	0.743	2.52	0.12	0.00	0.11	169.45	11.15	0.186	-0.69	S
2875	23 31 19.04	0.63	-57 43 30.61	0.70	2.224	0.358	1.436	0.236	6.77	1.70	4.84	1.35	155.59	54.34	0.207	–	S
2876	23 31 23.29	0.58	-59 51 31.45	0.55	1.477	0.245	1.060	0.159	5.45	1.40	4.31	1.18	130.40	93.75	0.139	–	S
2877	23 31 13.48	0.62	-55 46 40.56	1.37	8.518	0.502	1.442	0.174	25.85	3.23	11.32	1.35	8.16	10.37	0.176	–	S
2878	23 31 04.81	1.91	-50 47 08.08	1.63	7.330	0.459	1.087	0.202	26.22	5.36	14.41	2.67	123.91	20.49	0.223	–	S
2879	23 31 19.03	0.27	-59 04 48.55	0.26	3.878	0.412	3.410	0.283	3.31	0.55	2.46	0.49	115.33	81.41	0.206	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2880	23 31 06.61	0.19	-53 04 26.10	0.20	8.027	0.554	6.148	0.398	4.65	0.32	4.30	0.32	5.24	109.06	0.200	–	S
2881	23 31 11.05	0.57	-55 52 14.62	0.70	3.212	0.309	1.480	0.200	9.65	1.61	7.56	1.29	7.71	39.82	0.168	–	S
2882	23 31 06.99	1.05	-53 43 55.44	0.44	4.789	0.468	1.724	0.199	0.00	2.53	0.00	0.77	0.00	11.88	0.175	–	M
2883	23 31 06.50	0.17	-53 31 25.64	0.18	9.609	0.660	8.729	0.535	3.25	0.24	1.63	0.22	70.57	19.67	0.231	–	S
2884	23 31 01.97	1.20	-50 30 08.01	0.99	1.672	0.230	0.748	0.158	10.66	2.98	7.63	2.13	69.67	45.42	0.142	–	S
2885	23 31 13.63	1.23	-59 04 53.05	0.59	7.499	0.482	1.781	0.227	21.17	2.83	8.40	1.20	105.22	11.02	0.214	–	S
2886	23 31 13.02	0.15	-58 32 52.34	0.15	45.606	2.578	32.173	1.786	6.99	0.10	0.94	0.06	21.16	1.32	0.244	-1.24	M
2887	23 31 04.81	0.95	-53 32 00.50	1.21	4.809	0.407	1.548	0.254	16.79	3.30	7.29	1.46	35.00	16.47	0.236	–	S
2888	23 31 04.61	0.31	-53 45 54.52	0.32	3.335	0.332	2.500	0.222	5.20	0.69	4.09	0.62	136.95	49.46	0.165	–	S
2889	23 31 07.08	0.54	-56 10 56.34	0.78	34.782	2.034	6.824	0.471	22.69	1.95	11.48	0.96	116.14	8.38	0.284	–	M
2890	23 31 11.21	0.77	-57 57 26.50	0.83	2.678	0.301	1.262	0.200	11.31	2.28	5.36	1.27	140.83	20.03	0.176	–	S
2891	23 31 08.48	0.66	-56 29 40.04	0.66	5.825	0.544	2.574	0.350	10.38	1.71	7.47	1.29	136.23	31.06	0.296	–	S
2892	23 31 05.98	0.58	-55 45 29.52	0.53	2.547	0.327	1.591	0.216	6.70	1.33	5.64	1.18	74.18	83.83	0.183	–	S
2893	23 30 59.11	0.19	-51 28 36.47	0.17	21.822	1.252	11.898	0.677	11.80	0.29	5.50	0.16	176.54	2.70	0.175	-0.66	M
2894	23 30 59.19	0.30	-52 23 45.12	0.24	26.230	1.563	7.801	0.529	13.09	0.67	7.00	0.39	25.05	5.89	0.309	–	M
2895	23 31 04.47	0.86	-56 09 31.74	1.06	4.015	0.442	1.611	0.299	10.82	2.49	8.61	1.98	7.22	54.63	0.265	–	S
2896	23 31 00.18	0.61	-53 32 37.02	0.68	4.667	0.445	2.135	0.287	9.61	1.58	7.98	1.36	27.78	55.18	0.241	–	S
2897	23 31 06.15	0.75	-57 19 25.97	1.01	1.494	0.253	0.848	0.170	8.46	2.41	5.21	1.68	12.31	41.57	0.151	–	S
2898	23 31 06.73	0.67	-57 59 38.25	0.67	1.573	0.291	1.099	0.190	5.48	1.58	4.83	1.50	152.18	157.37	0.168	–	S
2899	23 31 02.44	0.19	-56 08 53.02	0.16	29.538	1.697	18.099	1.023	12.74	0.30	3.23	0.12	3.56	1.64	0.236	0.25	M
2900	23 30 54.73	0.15	-51 54 38.39	0.16	33.279	1.887	24.686	1.388	7.22	0.15	0.63	0.08	70.40	1.70	0.276	-0.89	S
2901	23 30 57.42	0.14	-55 20 23.98	0.15	22.127	1.265	20.251	1.133	2.85	0.09	1.94	0.08	144.77	13.24	0.201	-0.47	S
2902	23 30 51.92	2.08	-52 19 08.06	1.15	17.761	1.163	2.741	0.369	19.40	5.23	6.77	1.94	22.37	20.37	0.337	–	M
2903	23 30 51.62	0.38	-53 31 23.67	0.36	3.790	0.469	2.994	0.309	4.73	0.84	3.53	0.75	73.03	57.99	0.249	–	S
2904	23 30 48.22	0.68	-50 11 08.43	0.93	1.547	0.298	1.028	0.195	7.44	2.11	4.28	1.61	167.12	50.62	0.175	–	S
2905	23 30 49.14	1.16	-52 09 08.28	2.09	77.914	4.369	6.229	0.859	36.51	4.90	20.69	2.71	175.82	15.70	1.119	–	S
2906	23 30 55.27	0.21	-57 10 30.97	0.24	6.326	0.449	4.416	0.304	6.42	0.44	3.80	0.34	159.15	11.59	0.172	–	S
2907	23 30 52.30	0.29	-55 32 55.93	0.29	3.652	0.408	3.176	0.277	3.66	0.61	2.42	0.55	129.21	54.69	0.208	–	S
2908	23 30 56.19	0.14	-59 08 40.32	0.15	37.252	2.070	35.984	1.987	1.59	0.04	1.34	0.04	64.82	42.35	0.173	-0.32	S
2909	23 30 43.83	0.47	-50 47 38.64	0.21	33.491	1.929	15.043	0.856	21.47	1.05	6.00	0.33	177.86	3.40	0.219	-0.30	M
2910	23 30 47.15	0.29	-53 12 29.59	0.31	4.331	0.390	3.113	0.262	6.12	0.68	3.90	0.54	140.45	22.73	0.186	–	S
2911	23 30 47.47	1.10	-55 46 13.32	1.10	4.612	0.345	1.172	0.201	13.71	2.57	13.58	2.57	141.30	179.84	0.188	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
2912	23 30 41.59	1.41	-51 17 12.83	1.27	5.218	0.335	0.932	0.158	19.42	3.53	15.85	2.73	114.98	39.46	0.160	-	S
2913	23 30 50.10	0.31	-59 04 23.91	0.43	13.761	0.849	3.831	0.284	16.35	1.10	4.40	0.37	121.97	4.37	0.191	-	M
2914	23 30 43.51	0.38	-53 44 12.53	0.39	2.600	0.307	1.938	0.202	5.37	0.88	4.01	0.78	138.06	51.63	0.162	-	S
2915	23 30 43.70	0.15	-54 37 32.42	0.16	18.262	1.132	17.470	1.009	1.82	0.14	1.59	0.14	5.29	128.43	0.303	-0.58	S
2916	23 30 49.10	0.17	-59 06 18.12	0.17	6.830	0.472	6.593	0.399	2.49	0.21	0.00	0.19	48.95	17.27	0.166	-	S
2917	23 30 44.80	0.22	-56 01 22.72	0.23	5.292	0.436	4.416	0.314	3.83	0.40	3.23	0.38	15.26	61.84	0.191	-	S
2918	23 30 44.38	0.71	-56 01 59.07	0.93	1.414	0.326	1.012	0.210	6.53	2.22	3.20	1.58	15.10	48.15	0.191	-	S
2919	23 30 38.73	0.93	-52 29 39.63	1.16	5.233	0.447	1.627	0.283	13.79	2.72	10.52	2.13	160.52	44.99	0.257	-	S
2920	23 30 37.00	0.33	-51 30 07.15	0.32	6.882	0.439	2.951	0.230	10.43	0.78	8.46	0.61	119.63	18.49	0.150	-	S
2921	23 30 36.33	1.46	-50 54 52.72	1.67	4.106	0.317	0.900	0.192	17.68	4.10	13.53	3.18	144.21	49.92	0.189	-	S
2922	23 30 38.28	0.27	-53 55 17.04	0.31	2.828	0.271	2.152	0.183	5.22	0.64	3.76	0.56	3.90	37.27	0.133	-	S
2923	23 30 35.31	0.16	-53 31 21.79	0.18	82.982	4.612	23.114	1.303	18.64	0.24	12.27	0.16	106.93	1.77	0.287	-0.47	M
2924	23 30 35.10	0.78	-50 52 33.68	0.72	2.178	0.322	1.267	0.215	7.51	1.82	6.38	1.64	80.96	76.95	0.188	-	S
2925	23 30 40.26	0.31	-56 59 19.27	0.39	4.080	0.368	2.578	0.240	7.18	0.85	4.79	0.66	177.27	21.60	0.180	-	S
2926	23 30 38.43	0.14	-56 25 03.62	0.15	219.222	12.442	201.990	11.258	3.10	0.08	1.15	0.07	27.36	6.00	1.787	-0.78	S
2927	23 30 39.91	0.47	-57 17 36.29	0.62	2.261	0.275	1.372	0.181	7.97	1.45	4.58	1.01	164.62	25.44	0.153	-	S
2928	23 30 37.93	0.22	-56 25 23.42	0.31	37.589	2.811	24.672	1.841	7.95	0.63	3.07	0.39	2.67	8.31	1.174	-	S
2929	23 30 37.98	0.14	-57 22 57.70	0.15	21.448	1.228	18.188	1.011	0.00	0.08	0.00	0.06	0.00	2.95	0.145	-0.73	M
2930	23 30 33.29	0.72	-51 47 11.39	1.03	1.869	0.404	1.262	0.263	7.32	2.34	3.91	1.71	2.78	50.46	0.238	-	S
2931	23 30 33.72	0.42	-54 31 48.64	0.47	10.447	0.751	4.516	0.432	11.23	1.17	7.22	0.78	34.70	15.07	0.329	-	S
2932	23 30 35.81	0.36	-57 07 38.96	0.53	15.237	0.949	4.299	0.324	12.51	1.20	7.54	0.76	82.08	12.60	0.221	-	M
2933	23 30 29.09	0.53	-50 33 28.31	0.68	1.536	0.279	1.158	0.180	5.94	1.52	3.39	1.25	9.31	53.27	0.159	-	S
2934	23 30 31.07	0.53	-54 13 44.50	0.63	4.070	0.379	1.944	0.243	9.60	1.47	7.22	1.16	24.53	34.54	0.202	-	S
2935	23 30 34.13	0.60	-58 30 20.13	0.53	3.351	0.291	1.521	0.183	10.23	1.44	7.02	1.08	125.80	25.15	0.151	-	S
2936	23 30 30.46	0.57	-54 31 10.23	0.90	7.061	0.629	2.873	0.398	13.01	2.17	6.55	1.18	161.06	17.00	0.346	-	S
2937	23 30 28.36	0.65	-53 51 02.35	0.79	2.436	0.263	1.166	0.174	10.25	1.95	6.59	1.34	29.32	29.11	0.150	-	S
2938	23 30 26.30	0.52	-51 24 24.97	0.56	2.737	0.313	1.635	0.206	7.93	1.37	5.49	1.05	137.40	34.84	0.172	-	S
2939	23 30 29.21	1.56	-57 41 42.89	0.63	8.878	0.585	1.307	0.187	20.09	3.81	3.88	0.95	162.78	10.36	0.172	-	M
2940	23 30 25.88	0.14	-54 03 19.41	0.15	17.089	0.971	16.576	0.923	1.80	0.07	0.90	0.07	156.96	19.51	0.141	0.06	S
2941	23 30 26.67	0.44	-55 37 10.70	0.41	4.676	0.407	2.540	0.259	8.59	1.06	6.01	0.81	128.23	23.98	0.201	-	S
2942	23 30 25.64	0.76	-55 26 27.89	0.79	9.283	0.661	2.913	0.249	16.34	2.43	3.57	0.76	46.06	9.13	0.190	-	M
2943	23 30 26.79	0.32	-56 15 15.59	0.34	4.334	0.402	2.948	0.266	6.75	0.79	3.99	0.60	36.14	19.57	0.197	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2944	23 30 26.45	0.14	-56 14 30.69	0.15	41.226	2.293	39.788	2.197	1.67	0.04	1.33	0.04	7.57	24.65	0.196	-0.50	S
2945	23 30 27.12	0.24	-57 35 46.21	0.26	3.616	0.346	3.073	0.241	4.02	0.51	2.43	0.45	6.79	31.62	0.167	-	S
2946	23 30 22.91	0.61	-51 06 02.70	0.75	1.659	0.344	1.272	0.219	5.94	1.75	2.90	1.34	154.24	49.42	0.198	-	S
2947	23 30 25.94	0.62	-56 50 12.27	0.78	2.657	0.313	1.346	0.208	9.06	1.85	6.53	1.40	168.00	38.52	0.179	-	S
2948	23 30 20.13	0.24	-54 21 53.91	0.25	5.393	0.555	4.982	0.390	2.68	0.48	1.88	0.46	14.31	88.40	0.273	-	S
2949	23 30 19.53	1.03	-53 42 00.71	0.73	2.109	0.274	1.021	0.185	10.20	2.45	6.43	1.64	98.04	33.90	0.164	-	S
2950	23 30 16.97	0.71	-52 07 43.68	0.59	19.484	1.263	6.126	0.618	18.17	2.02	6.76	0.75	126.01	8.07	0.521	-	S
2951	23 30 17.42	0.15	-53 20 52.09	0.15	17.734	1.022	16.698	0.936	2.18	0.09	1.83	0.09	124.85	41.28	0.177	-0.35	S
2952	23 30 16.43	0.40	-50 38 33.29	0.43	2.212	0.300	1.740	0.196	4.61	0.93	3.96	0.89	135.21	126.55	0.162	-	S
2953	23 30 16.90	0.37	-52 52 04.86	0.44	6.001	0.500	3.275	0.316	9.05	1.04	5.74	0.73	27.96	18.49	0.240	-	S
2954	23 30 18.30	0.17	-57 13 44.36	0.18	5.600	0.407	5.449	0.337	0.00	0.24	0.00	0.22	0.00	25.56	0.154	-	S
2955	23 30 16.99	0.18	-56 56 38.89	0.19	8.283	0.542	6.090	0.384	5.14	0.30	4.32	0.27	12.33	24.78	0.177	-	S
2956	23 30 15.72	1.04	-55 11 51.80	1.11	1.719	0.290	0.894	0.197	10.11	3.05	5.20	1.84	139.16	34.41	0.178	-	S
2957	23 30 16.35	0.59	-58 06 57.27	0.73	2.326	0.273	1.223	0.180	9.14	1.78	5.71	1.24	156.25	28.03	0.155	-	S
2958	23 30 13.26	0.50	-55 28 19.08	0.78	6.983	0.460	2.072	0.231	15.34	1.81	9.49	1.11	8.80	14.77	0.195	-	S
2959	23 30 13.39	0.40	-55 35 36.74	0.53	3.180	0.355	1.995	0.233	7.50	1.20	4.68	0.89	3.29	26.74	0.191	-	S
2960	23 30 10.48	0.14	-50 13 14.78	0.15	62.635	3.463	61.129	3.369	1.40	0.03	1.20	0.03	168.89	148.96	0.207	-0.37	S
2961	23 30 10.50	0.30	-53 18 23.80	0.21	16.092	0.935	6.672	0.428	14.67	0.67	4.74	0.26	70.56	3.19	0.214	-	S
2962	23 30 10.13	0.30	-53 58 02.34	0.36	2.142	0.250	1.750	0.166	4.98	0.78	2.35	0.61	8.07	28.14	0.130	-	S
2963	23 30 09.51	0.22	-52 45 08.08	0.24	5.755	0.463	4.633	0.330	4.68	0.44	3.25	0.38	20.44	28.97	0.200	-	S
2964	23 30 10.50	0.43	-57 39 42.65	0.41	3.862	0.367	2.264	0.238	6.97	0.97	6.27	0.88	126.75	93.31	0.188	-	S
2965	23 30 10.88	0.54	-57 39 11.13	0.80	2.005	0.325	1.300	0.213	7.73	1.88	3.52	1.21	7.48	28.09	0.188	-	S
2966	23 30 07.79	0.59	-54 49 22.96	0.54	3.925	0.414	2.098	0.271	8.33	1.40	6.61	1.17	116.45	47.33	0.226	-	S
2967	23 30 07.93	0.59	-58 04 27.13	0.49	1.537	0.260	1.152	0.168	5.49	1.35	3.53	1.11	101.03	58.27	0.147	-	S
2968	23 30 05.24	0.14	-50 27 52.40	0.15	30.279	1.688	28.362	1.568	2.30	0.05	1.99	0.05	9.00	43.95	0.160	-0.46	S
2969	23 30 06.16	0.62	-57 05 05.18	0.61	1.612	0.263	1.101	0.172	5.88	1.49	4.88	1.31	42.18	103.18	0.150	-	S
2970	23 30 03.72	0.45	-54 14 23.45	0.39	8.615	0.563	3.261	0.291	11.64	1.05	8.99	0.81	113.04	19.49	0.214	-	S
2971	23 30 02.57	0.98	-56 41 33.47	1.13	6.176	0.410	1.357	0.205	17.76	2.87	12.36	1.97	31.63	24.69	0.196	-	S
2972	23 30 01.16	1.41	-52 34 54.32	1.09	7.797	0.652	1.500	0.248	16.26	4.04	0.00	1.03	143.39	13.27	0.234	-	M
2973	23 30 01.49	0.23	-51 09 15.70	0.25	5.603	0.485	4.691	0.345	4.38	0.47	2.77	0.41	31.13	30.25	0.221	-	S
2974	23 30 00.39	0.15	-54 37 07.60	0.16	169.714	9.437	58.033	3.238	15.01	0.17	9.97	0.11	141.71	1.67	0.547	-1.08	M
2975	23 30 00.46	1.72	-58 32 25.28	1.00	2.112	0.227	0.690	0.155	15.01	3.98	7.95	2.26	76.40	29.49	0.146	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
2976	23 29 59.83	0.90	-58 34 02.72	0.69	2.150	0.250	1.005	0.167	10.14	2.11	6.65	1.53	66.77	35.29	0.146	–	S
2977	23 29 58.37	0.56	-58 29 17.26	0.20	14.035	0.850	7.366	0.433	19.24	1.27	2.25	0.29	6.95	3.32	0.152	-0.59	M
2978	23 29 57.79	0.14	-57 55 46.06	0.15	15.937	0.921	15.321	0.859	1.83	0.09	1.27	0.09	30.76	31.41	0.164	-0.10	S
2979	23 29 56.60	0.82	-51 21 06.58	0.98	1.634	0.262	0.904	0.177	8.68	2.32	6.06	1.84	29.18	56.75	0.156	–	S
2980	23 29 55.42	1.80	-55 31 14.69	0.98	2.698	0.295	0.886	0.203	15.20	4.22	8.00	2.28	95.41	28.90	0.191	–	S
2981	23 29 54.15	0.32	-51 08 10.46	0.24	35.689	2.029	6.647	0.423	15.36	0.67	9.51	0.43	2.09	6.40	0.212	–	M
2982	23 29 54.93	0.58	-51 26 17.25	0.81	1.667	0.289	1.126	0.188	7.32	1.85	3.95	1.34	177.06	40.48	0.167	–	S
2983	23 29 53.12	0.59	-58 48 48.31	0.45	2.052	0.260	1.311	0.171	7.34	1.33	4.40	1.01	74.26	31.92	0.144	–	S
2984	23 29 52.83	0.69	-59 25 57.02	0.68	1.846	0.284	1.129	0.188	6.83	1.73	5.59	1.43	37.16	80.97	0.164	–	S
2985	23 29 52.47	0.72	-56 42 53.29	0.76	9.674	0.581	2.069	0.225	18.93	2.04	11.90	1.27	40.37	13.84	0.202	–	S
2986	23 29 52.07	0.60	-56 07 26.65	0.28	13.757	0.817	3.613	0.252	18.43	1.40	6.33	0.50	11.12	5.33	0.154	–	M
2987	23 29 52.15	0.57	-53 20 44.66	0.92	6.693	0.443	1.848	0.222	17.03	2.19	9.64	1.23	164.97	14.62	0.195	–	S
2988	23 29 50.62	0.28	-59 04 36.04	0.32	4.248	0.393	3.060	0.263	6.16	0.69	3.33	0.53	23.61	17.61	0.190	–	S
2989	23 29 52.34	0.36	-53 21 24.58	0.55	3.722	0.379	2.259	0.246	8.89	1.26	3.94	0.76	169.10	15.92	0.200	–	S
2990	23 29 48.67	0.72	-57 43 10.35	0.54	2.778	0.269	1.293	0.174	9.95	1.62	6.99	1.24	86.14	32.82	0.147	–	S
2991	23 29 48.61	0.87	-57 10 35.33	1.66	7.623	0.454	1.132	0.166	25.57	3.91	13.53	1.97	173.52	15.23	0.178	–	S
2992	23 29 48.64	0.41	-57 53 07.02	0.53	2.475	0.277	1.533	0.181	7.44	1.21	4.77	0.91	3.03	26.89	0.149	–	S
2993	23 29 48.63	0.47	-51 30 25.03	0.53	2.680	0.311	1.686	0.204	7.17	1.21	5.40	1.03	149.13	48.21	0.169	–	S
2994	23 29 47.04	0.17	-55 30 02.64	0.18	7.740	0.538	7.248	0.443	2.78	0.23	1.02	0.21	176.94	22.53	0.191	–	S
2995	23 29 47.22	0.44	-54 15 07.07	0.72	2.280	0.343	1.567	0.223	7.81	1.66	2.43	0.98	176.65	21.75	0.195	–	S
2996	23 29 45.13	0.61	-55 14 58.22	0.60	4.796	0.364	1.802	0.214	10.64	1.42	9.96	1.33	125.69	107.34	0.177	–	S
2997	23 29 47.27	0.52	-50 34 14.13	0.66	2.016	0.277	1.306	0.182	7.96	1.61	4.06	1.07	150.30	27.81	0.157	–	S
2998	23 29 47.08	0.15	-50 01 03.55	0.16	35.430	2.060	34.397	1.932	1.74	0.10	1.07	0.09	141.31	35.94	0.387	0.04	S
2999	23 29 46.18	0.30	-52 24 29.10	0.36	4.265	0.472	3.372	0.315	5.08	0.75	3.21	0.63	9.68	37.32	0.243	–	S
3000	23 29 44.20	0.45	-56 34 08.78	0.41	2.382	0.335	1.853	0.217	5.62	1.07	2.53	0.81	54.80	29.77	0.183	–	S
3001	23 29 42.98	0.18	-54 25 24.35	0.22	111.031	6.199	35.849	2.022	17.23	0.42	8.17	0.20	60.45	2.21	0.449	-1.27	M
3002	23 29 41.59	0.35	-57 33 17.24	0.32	3.725	0.342	2.453	0.225	6.62	0.78	4.69	0.65	120.29	28.71	0.168	–	S
3003	23 29 41.10	0.37	-58 03 19.00	0.41	2.702	0.293	1.850	0.193	5.97	0.91	4.63	0.78	173.08	42.43	0.154	–	S
3004	23 29 44.05	0.21	-50 05 42.62	0.22	6.259	0.650	6.633	0.480	0.00	0.39	0.00	0.37	0.00	156.90	0.317	–	S
3005	23 29 39.14	1.03	-55 58 40.17	3.58	9.284	0.576	0.976	0.183	28.21	8.69	0.00	1.14	104.22	13.04	0.174	–	M
3006	23 29 42.29	0.45	-53 12 53.66	0.42	1.910	0.288	1.550	0.186	5.15	1.09	2.27	0.84	58.52	34.64	0.158	–	S
3007	23 29 43.53	0.98	-50 12 50.12	0.88	1.629	0.354	1.069	0.232	6.89	2.34	4.96	1.97	70.01	72.61	0.210	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3008	23 29 42.19	1.23	-50 14 07.15	1.03	3.407	0.325	1.138	0.214	13.83	3.19	9.58	2.08	64.48	33.00	0.195	-	S
3009	23 29 37.27	0.95	-58 59 20.87	1.53	2.825	0.377	0.841	0.164	10.58	4.16	0.00	0.68	59.10	12.32	0.157	-	M
3010	23 29 40.27	0.52	-54 28 44.39	0.57	5.609	0.680	3.422	0.447	7.81	1.42	4.95	1.05	144.13	31.01	0.377	-	S
3011	23 29 41.07	0.16	-50 58 48.30	0.15	56.847	3.168	27.169	1.509	11.58	0.16	1.73	0.07	175.09	1.04	0.211	-0.96	M
3012	23 29 40.70	0.23	-50 44 37.09	0.25	4.021	0.409	3.791	0.291	2.66	0.46	1.23	0.44	17.03	61.67	0.200	-	S
3013	23 29 39.91	0.75	-52 14 48.35	0.94	6.514	0.666	2.695	0.441	10.95	2.15	8.50	1.77	10.11	53.09	0.384	-	S
3014	23 29 35.60	0.15	-59 13 09.00	0.16	15.357	0.907	14.046	0.797	2.79	0.12	1.94	0.11	65.33	20.89	0.192	-0.33	S
3015	23 29 36.95	0.53	-57 34 21.97	0.56	2.137	0.300	1.415	0.197	5.93	1.31	5.31	1.18	179.12	112.45	0.169	-	S
3016	23 29 37.68	2.88	-53 48 32.06	0.71	5.176	0.403	0.781	0.165	0.00	6.89	0.00	1.12	0.00	16.34	0.159	-	M
3017	23 29 38.21	0.96	-52 17 09.14	0.68	3.617	0.645	2.254	0.426	8.03	2.29	4.40	1.52	84.37	37.27	0.381	-	S
3018	23 29 33.05	0.27	-57 26 52.44	0.27	48.964	2.743	17.638	0.993	18.46	0.69	7.80	0.29	135.92	3.04	0.211	-0.88	M
3019	23 29 36.81	0.43	-53 14 45.82	0.38	2.422	0.331	1.930	0.215	5.20	0.99	2.69	0.78	108.87	34.10	0.179	-	S
3020	23 29 36.27	0.93	-53 22 40.53	0.60	2.231	0.301	1.229	0.200	10.17	2.29	4.18	1.21	72.13	21.16	0.177	-	S
3021	23 29 35.97	1.05	-53 29 21.46	0.92	2.377	0.366	1.202	0.250	8.66	2.44	7.30	2.13	94.25	92.24	0.222	-	S
3022	23 29 30.61	0.74	-58 17 18.03	0.84	3.623	0.269	1.144	0.155	14.45	2.18	8.89	1.37	35.23	19.05	0.136	-	S
3023	23 29 33.64	0.71	-54 23 40.53	0.88	3.567	0.687	2.346	0.451	6.82	2.03	4.72	1.64	7.68	66.47	0.403	-	S
3024	23 29 29.34	0.20	-58 58 49.79	0.22	4.716	0.384	4.096	0.283	3.67	0.37	2.22	0.33	179.86	26.41	0.166	-	S
3025	23 29 32.38	0.52	-55 06 55.69	0.79	5.289	0.436	2.115	0.268	12.48	1.86	7.23	1.12	166.15	17.99	0.227	-	S
3026	23 29 30.43	1.07	-56 09 42.81	0.66	11.995	0.743	1.432	0.198	8.89	2.50	4.12	1.50	6.10	30.50	0.182	-	M
3027	23 29 33.76	0.32	-52 23 24.20	0.33	3.615	0.447	3.104	0.297	3.57	0.70	3.01	0.67	65.66	120.58	0.234	-	S
3028	23 29 33.66	0.90	-51 18 45.87	1.00	4.226	0.334	1.302	0.201	14.72	2.61	10.03	1.74	39.96	27.53	0.181	-	S
3029	23 29 33.28	0.34	-51 10 01.88	0.36	4.095	0.379	2.680	0.249	6.04	0.78	5.89	0.74	143.98	0.09	0.187	-	S
3030	23 29 31.59	0.22	-52 18 02.76	0.21	42.271	2.430	20.084	1.156	14.37	0.48	5.66	0.21	139.52	2.80	0.342	-0.73	M
3031	23 29 29.49	0.84	-55 06 58.03	0.67	7.013	0.486	2.145	0.260	16.49	2.22	8.13	1.10	55.98	12.91	0.228	-	S
3032	23 29 28.62	0.31	-53 27 36.71	0.21	18.207	1.096	9.143	0.542	14.62	0.68	5.16	0.29	16.28	3.67	0.202	-0.57	M
3033	23 29 20.66	0.37	-59 49 53.01	0.46	27.395	1.560	5.252	0.372	21.37	1.24	6.71	0.40	127.33	3.91	0.234	-	M
3034	23 29 27.45	0.17	-54 12 41.28	0.18	8.182	0.574	7.956	0.484	1.93	0.22	0.13	0.21	165.67	38.89	0.206	-	S
3035	23 29 29.23	0.62	-51 12 21.83	0.65	1.050	0.286	0.975	0.174	3.41	1.54	0.00	1.36	47.25	83.88	0.163	-	S
3036	23 29 25.14	0.14	-54 54 34.84	0.16	154.299	8.652	115.847	6.459	6.78	0.11	1.46	0.07	147.27	1.78	1.011	-0.85	S
3037	23 29 21.98	0.63	-56 59 33.55	0.77	1.056	0.322	0.977	0.194	0.00	1.90	0.00	1.30	0.00	43.96	0.185	-	S
3038	23 29 22.15	0.15	-57 10 23.01	0.16	15.643	0.911	13.369	0.757	3.45	0.12	3.05	0.11	31.20	29.02	0.176	-0.67	S
3039	23 29 21.84	1.36	-57 32 27.48	1.19	2.530	0.244	0.778	0.163	14.27	3.48	9.58	2.36	127.18	37.13	0.151	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3040	23 29 18.19	0.17	-59 41 00.11	0.18	10.826	0.720	9.393	0.572	3.55	0.22	2.43	0.21	20.97	20.67	0.237	–	S
3041	23 29 19.34	0.17	-56 24 28.73	0.64	86.511	4.931	41.346	2.309	35.16	1.48	2.93	0.20	84.20	1.96	0.398	-1.23	M
3042	23 29 16.72	0.30	-59 02 55.54	0.32	5.891	0.461	3.481	0.293	6.73	0.68	6.26	0.62	8.34	56.27	0.205	–	S
3043	23 29 20.53	0.59	-55 55 06.26	0.55	1.558	0.313	1.260	0.198	4.53	1.40	3.13	1.22	61.40	92.80	0.178	–	S
3044	23 29 18.31	0.19	-53 39 03.50	0.30	51.673	2.953	11.320	0.675	19.65	0.61	9.10	0.28	76.41	2.74	0.261	–	M
3045	23 29 18.72	0.45	-54 55 40.74	0.42	3.030	0.530	2.676	0.337	3.41	1.00	2.34	0.93	103.55	110.08	0.294	–	S
3046	23 29 17.78	0.14	-54 13 28.54	0.15	162.551	8.971	159.766	8.798	1.18	0.02	0.93	0.02	158.11	27.55	0.432	-0.44	S
3047	23 29 15.32	0.14	-53 51 53.64	0.15	19.168	1.086	18.150	1.010	2.28	0.07	1.46	0.07	129.48	15.51	0.151	-0.86	S
3048	23 29 14.95	1.17	-53 38 19.71	0.78	2.670	0.442	1.496	0.295	10.64	2.98	3.20	1.39	65.01	22.72	0.269	–	S
3049	23 29 10.24	0.60	-56 59 56.78	0.95	1.839	0.299	1.112	0.197	8.77	2.24	3.68	1.32	11.91	26.44	0.177	–	S
3050	23 29 10.64	0.84	-55 33 45.17	0.41	8.789	0.575	2.891	0.287	18.86	2.05	5.07	0.64	109.55	7.15	0.245	–	S
3051	23 29 06.17	0.39	-59 01 27.65	0.32	2.925	0.377	2.411	0.248	4.81	0.83	2.17	0.68	96.41	32.46	0.201	–	S
3052	23 29 10.98	0.15	-54 53 22.01	0.16	13.139	0.832	12.759	0.742	1.87	0.16	0.61	0.15	26.91	33.12	0.239	0.28	S
3053	23 29 03.86	0.17	-59 18 28.66	0.18	32.260	1.814	11.066	0.645	7.80	0.24	6.56	0.21	85.45	15.24	0.213	-0.74	M
3054	23 29 12.01	0.73	-54 17 17.39	0.70	1.736	0.451	1.448	0.281	4.38	1.76	2.63	1.52	125.02	98.58	0.260	–	S
3055	23 29 05.40	0.17	-58 20 58.83	0.18	8.511	0.534	6.336	0.384	4.82	0.24	4.35	0.23	164.93	30.61	0.153	-0.38	S
3056	23 29 09.57	0.45	-55 32 02.46	0.65	5.991	0.474	2.533	0.286	11.66	1.52	7.04	0.97	13.94	17.01	0.234	–	S
3057	23 29 08.61	0.69	-56 35 09.75	1.24	2.455	0.291	1.071	0.196	12.49	2.95	5.59	1.49	168.62	21.64	0.178	–	S
3058	23 29 06.36	0.19	-57 32 18.04	0.20	6.125	0.445	5.018	0.329	3.88	0.32	3.51	0.30	149.15	70.39	0.172	–	S
3059	23 29 14.51	0.29	-50 57 57.10	0.37	3.564	0.396	2.851	0.265	5.41	0.78	2.61	0.60	12.46	26.57	0.204	–	S
3060	23 29 14.19	0.20	-50 31 39.42	0.22	9.001	0.592	6.046	0.394	6.57	0.39	4.92	0.32	135.65	16.09	0.198	–	S
3061	23 29 06.42	0.22	-56 34 58.28	0.23	4.627	0.396	3.969	0.285	3.45	0.41	2.98	0.38	3.13	82.70	0.178	–	S
3062	23 29 12.53	0.64	-51 15 44.25	0.88	5.253	0.500	1.741	0.216	11.06	2.39	0.00	0.80	123.73	12.58	0.194	–	M
3063	23 29 04.69	0.24	-56 48 12.22	0.24	5.095	0.450	4.185	0.316	4.31	0.48	3.01	0.43	55.30	35.75	0.208	–	S
3064	23 29 06.23	0.84	-55 30 27.43	0.79	1.405	0.366	1.093	0.231	5.80	2.17	2.27	1.56	130.55	52.39	0.213	–	S
3065	23 29 06.37	0.92	-54 58 57.86	0.23	8.528	0.692	2.450	0.238	0.00	2.15	0.00	0.41	0.00	5.24	0.196	–	M
3066	23 29 00.60	0.93	-58 02 25.89	1.02	3.370	0.282	1.048	0.176	13.29	2.57	10.18	1.95	148.87	38.32	0.159	–	S
3067	23 29 02.43	0.82	-57 02 52.88	0.84	1.533	0.323	1.047	0.210	7.39	2.30	2.99	1.48	138.50	36.25	0.190	–	S
3068	23 29 02.65	0.19	-56 34 45.51	0.20	6.521	0.471	5.382	0.351	4.07	0.32	3.18	0.29	144.77	33.41	0.180	–	S
3069	23 29 06.07	0.31	-53 59 12.28	0.41	3.073	0.288	2.008	0.189	7.58	0.92	3.98	0.63	161.55	17.12	0.143	–	S
3070	23 29 02.94	0.32	-55 33 16.95	0.27	8.097	0.610	4.901	0.387	8.68	0.74	3.98	0.46	118.97	9.89	0.261	–	S
3071	23 28 59.21	0.26	-58 15 15.63	0.25	3.661	0.316	2.780	0.216	5.03	0.52	3.80	0.47	107.96	38.95	0.145	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3072	23 29 00.67	0.48	-56 30 11.59	0.39	2.968	0.489	2.525	0.313	4.63	1.08	1.47	0.85	87.35	37.98	0.271	–	S
3073	23 29 04.62	0.93	-53 13 04.33	1.64	10.228	0.598	1.379	0.196	26.66	3.84	15.45	2.16	175.93	17.09	0.213	–	S
3074	23 29 05.31	1.27	-52 10 02.68	2.17	10.366	0.658	1.581	0.301	25.46	5.19	14.15	2.79	165.59	23.00	0.329	–	S
3075	23 28 54.13	0.51	-59 24 27.27	0.40	2.706	0.346	1.871	0.227	6.41	1.13	3.98	0.91	87.62	37.16	0.190	–	S
3076	23 29 02.88	0.27	-53 38 53.39	0.32	6.232	0.553	4.440	0.370	6.26	0.68	3.90	0.53	21.16	21.74	0.262	–	S
3077	23 29 03.44	0.18	-51 42 56.55	0.38	88.136	5.047	20.125	1.228	21.38	0.83	6.44	0.25	96.57	2.52	0.531	–	M
3078	23 28 55.81	0.46	-58 02 01.00	0.49	1.796	0.295	1.429	0.189	4.60	1.15	3.27	0.98	159.41	70.04	0.165	–	S
3079	23 29 03.76	0.20	-52 26 17.85	0.22	6.928	0.578	6.121	0.426	3.52	0.39	2.31	0.35	17.13	40.60	0.254	–	S
3080	23 28 54.86	0.15	-58 06 20.51	0.17	8.989	0.555	7.931	0.462	3.31	0.16	2.33	0.15	3.58	18.23	0.147	-0.63	S
3081	23 28 55.44	0.14	-57 16 31.89	0.15	118.405	6.545	114.106	6.287	1.90	0.03	1.02	0.03	15.26	6.84	0.379	-0.82	S
3082	23 29 01.52	0.34	-53 19 31.20	0.39	7.760	0.560	3.824	0.332	9.85	0.92	6.58	0.65	31.67	15.97	0.237	–	S
3083	23 29 00.91	1.42	-53 28 08.96	1.49	6.653	0.427	1.108	0.200	18.55	3.52	17.60	3.31	25.19	0.20	0.208	–	S
3084	23 29 01.26	0.49	-53 18 57.63	1.04	15.555	0.888	2.535	0.249	26.05	2.42	12.33	1.09	178.99	8.85	0.234	–	S
3085	23 28 52.11	0.75	-58 50 20.50	0.38	5.488	0.390	2.075	0.217	15.07	1.70	5.60	0.75	104.38	9.53	0.179	–	S
3086	23 28 57.25	0.49	-55 54 46.83	0.45	1.678	0.314	1.460	0.198	3.85	1.14	2.13	0.99	113.86	75.35	0.176	–	S
3087	23 29 00.18	0.32	-53 32 53.14	0.32	6.072	0.486	3.671	0.312	6.86	0.69	6.20	0.65	51.93	65.73	0.220	–	S
3088	23 29 01.11	0.40	-52 36 35.80	0.35	4.215	0.419	2.797	0.276	6.61	0.91	4.88	0.73	84.46	32.45	0.213	–	S
3089	23 29 00.72	0.15	-52 30 16.82	0.16	17.982	1.066	15.176	0.869	3.72	0.15	3.25	0.14	69.70	27.18	0.234	-0.30	S
3090	23 29 02.92	0.31	-50 53 10.02	0.37	13.191	0.842	5.555	0.439	11.14	0.83	8.22	0.62	25.07	16.82	0.292	–	S
3091	23 28 56.90	0.62	-55 24 28.75	0.51	1.592	0.363	1.408	0.225	4.21	1.43	0.22	1.13	103.68	53.27	0.206	–	S
3092	23 28 52.84	1.18	-57 06 32.84	1.73	8.991	0.531	1.147	0.184	24.73	4.09	17.10	2.73	173.97	23.95	0.207	–	S
3093	23 29 00.33	0.22	-52 14 10.39	0.18	54.591	3.168	20.477	1.187	14.56	0.43	5.23	0.18	159.64	2.39	0.375	-1.09	M
3094	23 28 57.91	0.21	-54 02 41.47	0.20	9.349	0.589	5.857	0.375	7.12	0.37	5.25	0.30	101.70	12.42	0.178	–	S
3095	23 29 00.44	0.58	-52 04 50.22	0.72	3.849	0.532	2.356	0.351	8.23	1.74	4.68	1.20	28.84	31.72	0.304	–	S
3096	23 28 58.16	0.96	-53 33 37.15	0.77	1.644	0.381	1.155	0.247	6.42	2.26	3.93	1.75	80.35	63.38	0.224	–	S
3097	23 29 00.46	0.26	-50 53 48.49	0.29	15.631	0.975	7.369	0.522	9.97	0.61	7.48	0.47	33.61	14.51	0.303	–	S
3098	23 28 49.47	0.26	-57 51 57.84	0.28	3.230	0.313	2.613	0.214	4.40	0.57	3.14	0.50	177.96	37.71	0.152	–	S
3099	23 28 43.64	0.29	-59 37 18.61	0.27	4.001	0.443	3.457	0.300	3.73	0.60	2.37	0.53	121.89	50.24	0.225	–	S
3100	23 28 47.95	1.00	-57 13 22.76	0.87	3.152	0.366	1.367	0.247	11.47	2.60	6.67	1.64	127.58	28.87	0.220	–	S
3101	23 28 49.72	0.77	-55 59 46.00	0.75	2.007	0.286	1.116	0.192	8.14	1.94	6.05	1.55	47.55	55.70	0.168	–	S
3102	23 28 47.83	0.45	-56 41 54.99	0.33	6.471	0.503	3.313	0.308	9.45	0.98	6.04	0.71	95.32	17.21	0.230	–	S
3103	23 28 56.42	0.75	-50 26 42.68	1.07	2.936	0.437	0.922	0.193	0.00	2.98	0.00	0.53	0.00	11.32	0.187	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3104	23 28 55.52	0.47	-51 00 10.07	0.44	3.036	0.384	2.137	0.252	5.84	1.08	4.75	0.96	98.93	58.96	0.209	–	S
3105	23 28 49.62	0.16	-53 36 52.96	0.17	14.210	0.874	11.786	0.691	4.39	0.19	2.81	0.17	53.25	12.01	0.230	-0.65	S
3106	23 28 40.60	1.08	-58 18 04.00	1.51	2.529	0.245	0.778	0.164	14.96	3.76	8.84	2.20	21.87	28.85	0.154	–	S
3107	23 28 38.22	0.26	-59 04 47.72	0.31	6.254	0.499	4.021	0.326	6.77	0.64	4.77	0.52	177.14	19.22	0.223	–	S
3108	23 28 36.14	0.14	-59 39 35.73	0.15	113.461	6.281	111.643	6.154	1.17	0.03	0.77	0.03	31.43	112.69	0.410	-0.35	S
3109	23 28 46.21	0.53	-55 14 12.94	0.55	2.179	0.353	1.625	0.228	6.21	1.41	2.78	1.01	42.61	32.46	0.199	–	S
3110	23 28 46.37	0.14	-54 23 28.57	0.15	30.151	1.712	28.638	1.595	2.05	0.07	1.62	0.07	153.72	31.64	0.246	-0.07	S
3111	23 28 42.96	0.18	-55 41 22.22	0.18	22.972	1.358	14.250	0.851	8.23	0.29	4.05	0.19	50.14	4.66	0.310	-1.01	S
3112	23 28 40.95	0.24	-55 35 37.97	0.18	50.365	2.836	21.731	1.233	16.25	0.45	7.98	0.22	174.01	2.58	0.302	-0.57	M
3113	23 28 34.27	0.47	-58 39 27.48	0.44	5.549	0.397	2.271	0.226	9.82	1.07	9.02	0.97	116.22	95.13	0.174	–	S
3114	23 28 42.29	0.47	-54 53 25.95	0.76	1.408	0.378	1.320	0.228	0.00	1.76	0.00	1.04	0.00	28.72	0.215	–	S
3115	23 28 42.72	0.42	-54 21 27.97	0.43	2.641	0.497	2.470	0.311	2.85	0.99	0.99	0.90	139.57	91.16	0.276	–	S
3116	23 28 47.50	0.31	-51 20 07.13	0.36	2.867	0.350	2.408	0.233	4.19	0.73	2.93	0.69	10.87	68.03	0.184	–	S
3117	23 28 30.94	1.16	-59 22 02.99	1.63	3.196	0.268	0.869	0.168	18.74	4.30	7.74	1.80	150.87	18.56	0.165	–	S
3118	23 28 44.77	0.15	-52 03 43.68	0.17	291.769	16.940	185.550	10.444	9.13	0.20	0.00	0.10	97.38	1.72	2.219	-0.77	M
3119	23 28 45.10	0.70	-51 47 22.57	1.02	4.277	0.611	1.600	0.272	0.00	2.82	0.00	0.46	0.00	9.04	0.257	–	M
3120	23 28 28.03	0.15	-59 25 53.18	0.16	10.260	0.638	9.859	0.570	1.65	0.14	1.49	0.14	0.46	125.56	0.173	-0.50	S
3121	23 28 43.61	0.59	-52 09 14.50	0.72	5.641	0.591	2.773	0.388	9.58	1.69	7.03	1.33	21.77	40.73	0.329	–	S
3122	23 28 40.08	0.15	-53 05 34.74	0.16	14.284	0.874	13.225	0.762	2.69	0.15	1.80	0.14	80.44	23.87	0.223	-0.73	S
3123	23 28 37.18	1.28	-54 21 28.16	1.72	8.647	0.535	1.293	0.227	22.21	4.06	16.41	2.95	11.22	33.53	0.244	–	S
3124	23 28 37.81	0.21	-53 58 34.19	0.23	3.994	0.328	3.386	0.238	3.88	0.40	2.90	0.37	23.49	43.65	0.143	–	S
3125	23 28 35.26	0.15	-54 41 24.52	0.20	58.078	3.287	21.837	1.239	12.18	0.32	2.84	0.13	77.21	1.85	0.303	-0.46	M
3126	23 28 22.81	0.77	-59 24 59.17	1.30	2.052	0.275	0.942	0.187	12.10	3.18	4.74	1.51	162.09	21.94	0.171	–	S
3127	23 28 30.15	1.07	-55 55 37.57	2.57	6.800	0.641	1.337	0.276	17.69	6.51	0.00	0.66	112.23	10.69	0.267	–	M
3128	23 28 39.69	0.57	-51 48 29.28	0.55	1.954	0.406	1.659	0.255	4.01	1.32	2.76	1.23	114.32	103.22	0.230	–	S
3129	23 28 22.03	0.22	-59 01 43.55	0.24	5.884	0.472	4.496	0.328	4.84	0.45	3.77	0.41	10.12	30.13	0.204	–	S
3130	23 28 40.76	0.26	-50 27 48.41	0.29	5.208	0.421	3.607	0.282	6.59	0.63	4.34	0.48	38.88	20.30	0.187	–	S
3131	23 28 18.16	3.91	-59 59 42.83	2.22	9.476	0.646	1.120	0.244	24.93	10.56	0.00	0.79	151.01	11.84	0.236	–	M
3132	23 28 18.36	0.21	-59 40 06.43	0.29	46.008	2.665	14.122	0.904	13.89	0.64	4.97	0.28	114.49	3.59	0.462	–	M
3133	23 28 26.47	0.86	-57 11 30.36	0.84	2.343	0.437	1.443	0.290	7.16	2.18	5.28	1.74	44.93	73.63	0.259	–	S
3134	23 28 33.15	0.35	-54 15 44.90	0.38	2.581	0.364	2.233	0.237	3.78	0.83	2.46	0.75	164.88	69.99	0.197	–	S
3135	23 28 37.35	0.79	-51 04 38.37	0.85	3.409	0.419	1.692	0.280	10.46	2.30	6.10	1.45	44.09	28.95	0.246	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3136	23 28 28.62	0.90	-55 14 40.42	1.19	3.350	0.384	1.375	0.260	12.80	3.05	6.51	1.67	29.58	24.90	0.235	–	S
3137	23 28 26.59	0.73	-56 01 11.22	0.77	1.397	0.364	1.128	0.228	4.65	1.87	3.00	1.59	35.18	102.31	0.210	–	S
3138	23 28 18.61	0.83	-58 50 33.89	0.96	1.692	0.278	0.934	0.187	8.56	2.42	5.46	1.70	153.22	43.07	0.167	–	S
3139	23 28 29.42	0.42	-54 15 14.83	0.43	2.626	0.348	1.978	0.228	5.41	1.02	3.71	0.86	139.38	47.80	0.189	–	S
3140	23 28 28.64	1.87	-54 26 44.15	0.96	5.109	0.425	1.321	0.268	18.80	4.48	9.16	2.12	80.91	22.21	0.262	–	S
3141	23 28 30.68	0.18	-53 04 34.73	0.18	11.686	0.779	9.527	0.590	4.22	0.27	3.45	0.24	95.49	28.75	0.260	–	S
3142	23 28 25.09	0.14	-55 15 08.42	0.15	91.254	5.035	85.110	4.687	2.42	0.02	1.84	0.02	12.24	6.65	0.233	-0.47	S
3143	23 28 15.81	0.56	-58 37 26.37	0.48	2.631	0.345	1.730	0.226	7.11	1.33	4.10	0.99	121.21	30.97	0.192	–	S
3144	23 28 29.43	0.81	-53 03 20.52	0.75	4.237	0.431	1.865	0.283	11.28	2.15	7.04	1.39	52.70	26.49	0.246	–	S
3145	23 28 25.68	0.40	-54 46 50.38	0.47	2.407	0.397	2.049	0.254	4.28	1.05	2.17	0.88	166.61	52.71	0.220	–	S
3146	23 28 18.06	0.14	-56 50 46.17	0.15	60.413	3.357	57.654	3.183	2.07	0.04	1.30	0.04	150.49	9.99	0.277	-0.64	S
3147	23 28 20.87	0.80	-55 57 44.11	0.87	2.471	0.409	1.429	0.274	7.66	2.13	5.89	1.74	30.88	72.20	0.243	–	S
3148	23 28 27.34	1.04	-53 03 42.37	1.47	7.551	0.505	1.588	0.256	21.31	3.79	11.05	1.89	28.88	18.14	0.253	–	S
3149	23 28 10.41	0.61	-59 36 40.96	0.60	1.914	0.576	1.874	0.345	2.08	1.44	0.00	1.33	147.35	147.53	0.327	–	S
3150	23 28 23.37	0.24	-54 52 51.91	0.27	3.353	0.379	3.191	0.262	0.00	0.54	0.00	0.46	0.00	32.26	0.192	–	S
3151	23 28 13.04	0.25	-58 22 51.41	0.29	4.090	0.334	2.826	0.223	6.05	0.58	4.34	0.49	174.60	22.23	0.150	–	S
3152	23 28 19.48	0.35	-56 08 21.88	0.43	2.801	0.306	1.931	0.202	6.45	0.96	4.09	0.75	169.84	28.21	0.161	–	S
3153	23 28 28.62	0.17	-51 38 06.24	0.18	15.207	0.985	12.319	0.750	4.41	0.25	3.47	0.22	133.55	23.81	0.307	-0.83	S
3154	23 28 21.05	2.78	-54 31 25.74	0.93	30.783	1.796	2.043	0.307	39.41	6.77	7.94	1.32	15.25	10.31	0.286	–	M
3155	23 28 09.32	0.54	-58 59 57.32	0.65	3.405	0.360	1.755	0.236	8.73	1.53	6.38	1.17	165.55	33.25	0.199	–	S
3156	23 28 12.69	0.18	-57 44 04.34	0.19	7.190	0.510	6.198	0.393	3.60	0.28	2.63	0.26	152.64	29.66	0.189	–	S
3157	23 28 07.92	0.61	-59 19 45.17	0.70	2.218	0.339	1.388	0.224	7.01	1.70	4.97	1.32	159.70	48.15	0.196	–	S
3158	23 28 07.80	0.36	-59 09 21.46	0.51	3.971	0.502	2.843	0.327	6.92	1.17	2.15	0.75	13.75	18.30	0.274	–	S
3159	23 28 27.35	0.72	-51 15 05.30	0.81	1.495	0.329	1.101	0.211	5.54	1.84	4.25	1.67	26.16	127.91	0.191	–	S
3160	23 28 03.27	0.53	-59 42 25.57	0.67	6.961	0.663	3.269	0.427	9.61	1.56	6.90	1.16	12.56	28.10	0.359	–	S
3161	23 28 15.89	0.14	-55 22 02.98	0.15	56.146	3.104	54.644	3.011	1.64	0.03	0.90	0.03	32.02	9.99	0.184	-0.49	S
3162	23 28 25.63	0.14	-51 06 41.58	0.15	256.697	14.319	208.015	11.482	0.00	0.05	0.00	0.04	0.00	1.21	0.975	-0.69	M
3163	23 28 18.87	0.27	-54 10 25.72	0.22	7.178	0.593	4.189	0.300	6.68	0.57	0.00	0.34	23.53	8.10	0.193	–	M
3164	23 28 19.39	0.64	-53 40 33.11	0.66	1.843	0.359	1.379	0.231	5.53	1.60	3.74	1.36	43.13	72.28	0.206	–	S
3165	23 28 22.00	0.15	-51 40 57.68	0.16	27.430	1.652	26.843	1.528	1.72	0.12	0.32	0.12	10.06	30.14	0.390	-0.42	S
3166	23 28 12.11	0.16	-55 58 08.25	0.18	21.879	1.321	13.677	0.795	7.93	0.26	2.59	0.15	117.13	3.28	0.257	-0.24	M
3167	23 28 18.55	0.42	-53 39 09.45	0.39	3.819	0.410	2.554	0.269	6.23	0.94	5.10	0.83	73.59	54.94	0.214	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3168	23 28 07.67	0.40	-56 52 02.31	0.72	2.259	0.517	2.042	0.315	0.00	1.69	0.00	0.85	0.00	19.65	0.294	–	S
3169	23 28 23.83	0.26	-50 02 55.65	0.26	9.653	1.025	8.802	0.712	3.21	0.55	1.62	0.48	96.91	43.62	0.511	–	S
3170	23 28 16.18	0.14	-53 13 32.10	0.15	37.929	2.107	37.429	2.066	1.18	0.04	0.62	0.04	2.47	26.10	0.172	-0.57	S
3171	23 28 09.85	0.29	-55 36 40.78	0.22	12.537	0.804	6.653	0.465	9.76	0.59	5.19	0.37	82.95	7.80	0.267	–	S
3172	23 28 22.54	0.58	-50 18 13.33	0.73	1.962	0.341	1.383	0.221	6.89	1.73	3.66	1.26	154.36	40.93	0.196	–	S
3173	23 27 54.26	1.48	-59 54 45.50	0.69	26.849	1.564	5.182	0.400	29.64	3.73	7.13	0.85	158.66	7.24	0.281	–	M
3174	23 28 04.98	0.53	-56 30 11.41	0.23	139.849	7.723	56.796	3.147	35.17	1.24	8.44	0.28	165.97	2.16	0.384	-0.05	M
3175	23 27 57.79	0.99	-59 18 04.28	0.96	1.977	0.364	1.113	0.246	7.97	2.56	5.78	1.94	43.53	68.43	0.220	–	S
3176	23 28 01.06	1.13	-58 13 21.19	1.20	2.049	0.234	0.747	0.162	11.11	3.00	9.63	2.46	26.82	88.34	0.146	–	S
3177	23 28 00.46	0.16	-58 11 05.13	0.17	8.448	0.530	7.066	0.419	3.62	0.20	3.33	0.18	54.70	77.83	0.150	-0.05	S
3178	23 28 07.36	0.15	-55 41 07.95	0.17	52.707	3.019	34.136	1.915	10.12	0.20	3.09	0.10	93.66	1.65	0.377	-1.05	M
3179	23 28 09.06	0.44	-55 14 13.84	0.52	2.073	0.345	1.690	0.220	5.80	1.29	0.00	0.85	31.62	24.80	0.193	–	S
3180	23 28 18.45	0.27	-51 08 16.50	0.28	6.130	0.565	4.812	0.387	5.90	0.66	2.14	0.45	131.60	15.07	0.270	–	S
3181	23 28 07.04	0.16	-55 38 54.14	0.17	11.529	0.790	11.033	0.667	2.19	0.21	0.99	0.20	43.64	36.29	0.273	-0.52	S
3182	23 28 13.10	0.65	-53 17 25.59	0.68	3.301	0.304	1.528	0.193	12.58	1.98	4.90	0.92	44.59	13.66	0.165	–	S
3183	23 28 19.88	0.65	-50 25 27.96	0.69	2.490	0.324	1.424	0.215	7.72	1.58	6.56	1.50	42.51	91.49	0.185	–	S
3184	23 27 56.16	0.74	-58 58 03.85	0.81	1.471	0.288	0.980	0.189	6.68	2.04	4.26	1.53	149.60	54.32	0.169	–	S
3185	23 28 10.34	1.36	-54 15 38.07	2.19	6.280	0.394	0.914	0.174	26.41	5.41	13.94	2.72	159.17	21.28	0.194	–	S
3186	23 28 14.02	1.03	-52 48 52.17	0.78	1.684	0.380	1.142	0.248	7.07	2.45	3.87	1.74	80.68	50.68	0.225	–	S
3187	23 28 04.94	0.24	-55 58 52.93	0.26	4.808	0.516	4.517	0.360	2.63	0.50	1.14	0.45	13.34	57.02	0.257	–	S
3188	23 28 01.31	0.37	-56 58 01.19	0.36	5.049	0.607	3.859	0.400	4.66	0.81	4.12	0.78	115.85	137.52	0.321	–	S
3189	23 28 12.90	0.80	-52 45 43.25	0.73	1.440	0.332	1.085	0.212	5.57	1.92	3.58	1.60	117.13	74.32	0.193	–	S
3190	23 27 52.40	0.87	-58 48 21.19	0.82	9.644	0.669	4.251	0.303	18.78	2.71	0.00	0.54	43.62	6.66	0.193	–	M
3191	23 28 13.21	0.16	-51 33 51.64	0.19	16.169	1.026	12.808	0.773	5.51	0.26	2.67	0.20	177.79	8.79	0.304	-1.22	S
3192	23 27 53.58	0.26	-58 35 16.30	0.31	14.579	0.867	5.478	0.391	11.28	0.65	8.92	0.52	177.39	12.57	0.233	–	S
3193	23 28 05.74	0.73	-55 06 47.01	0.95	1.322	0.332	0.985	0.212	6.00	2.22	3.13	1.67	175.46	60.45	0.194	–	S
3194	23 28 10.15	0.19	-52 38 32.53	0.31	30.965	1.782	9.466	0.597	15.25	0.63	6.55	0.28	85.06	3.45	0.292	–	M
3195	23 28 01.34	0.20	-55 41 16.49	0.20	17.745	1.167	12.551	0.803	6.17	0.35	3.98	0.28	50.35	12.04	0.387	–	S
3196	23 27 49.08	0.49	-59 09 08.59	0.20	74.886	4.195	22.990	1.301	26.98	1.12	5.43	0.24	170.98	2.21	0.308	-1.07	M
3197	23 28 06.11	0.14	-53 58 30.95	0.15	20.850	1.186	19.838	1.105	2.25	0.08	1.28	0.07	162.20	15.16	0.174	-0.58	S
3198	23 28 15.47	0.16	-50 16 47.49	0.17	11.468	0.721	10.249	0.601	3.29	0.19	2.37	0.17	39.20	26.49	0.204	-0.38	S
3199	23 27 56.14	1.25	-56 57 31.85	1.35	6.664	0.524	1.629	0.319	15.29	3.38	12.58	2.68	149.11	55.13	0.305	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3200	23 27 52.13	1.29	-57 55 12.20	1.93	12.268	0.693	1.101	0.158	33.70	4.81	18.28	2.53	22.97	15.47	0.200	–	S
3201	23 28 02.56	0.53	-54 48 40.79	0.59	2.462	0.390	1.755	0.254	5.73	1.36	4.39	1.18	158.97	75.28	0.220	–	S
3202	23 28 10.44	1.56	-51 25 38.20	1.14	2.652	0.292	0.997	0.196	16.78	4.41	4.80	1.44	122.19	17.23	0.188	–	S
3203	23 27 45.09	0.64	-59 22 45.25	0.83	2.073	0.311	1.199	0.207	7.90	1.97	5.30	1.44	3.81	40.95	0.182	–	S
3204	23 27 54.25	0.63	-56 39 48.04	0.67	2.503	0.335	1.448	0.223	7.10	1.57	6.42	1.43	166.15	120.00	0.192	–	S
3205	23 27 53.65	0.14	-56 22 19.90	0.15	78.789	4.392	75.836	4.192	0.00	0.05	0.00	0.04	0.00	2.72	0.416	-0.61	S
3206	23 28 04.00	1.87	-52 59 46.89	1.70	7.389	0.591	1.224	0.248	18.64	5.90	0.00	0.68	138.20	10.34	0.238	–	M
3207	23 28 08.21	0.18	-51 20 18.46	0.19	5.653	0.441	5.589	0.357	1.23	0.27	0.32	0.27	3.45	133.55	0.181	–	S
3208	23 27 53.87	0.77	-56 10 10.64	1.13	1.291	0.237	0.751	0.159	8.89	2.70	4.41	1.67	165.19	35.48	0.143	–	S
3209	23 27 40.92	0.38	-59 29 41.50	0.64	3.522	0.326	1.800	0.208	10.26	1.47	4.79	0.83	2.96	14.51	0.172	–	S
3210	23 28 04.22	0.24	-52 18 17.75	0.26	7.105	0.637	5.779	0.444	4.15	0.49	3.64	0.48	34.55	104.47	0.297	–	S
3211	23 27 49.92	0.25	-56 55 47.42	0.27	4.315	0.474	3.966	0.327	3.54	0.56	0.00	0.46	159.44	26.26	0.239	–	S
3212	23 27 55.32	0.54	-55 11 06.69	0.54	2.609	0.322	1.628	0.212	7.61	1.39	4.71	1.02	46.12	31.10	0.179	–	S
3213	23 28 04.69	2.19	-51 39 06.43	1.01	10.797	0.664	1.604	0.276	27.82	5.37	13.10	2.22	95.57	16.77	0.306	–	S
3214	23 27 43.24	0.27	-58 29 48.87	0.30	3.314	0.346	2.727	0.235	4.81	0.64	2.05	0.51	150.06	22.49	0.174	–	S
3215	23 28 05.43	0.33	-51 12 20.07	0.37	3.924	0.444	3.025	0.295	4.89	0.76	4.06	0.75	169.68	103.22	0.231	–	S
3216	23 27 41.35	0.87	-58 36 30.10	1.16	6.185	0.513	1.545	0.213	11.70	3.33	0.00	0.62	126.57	10.27	0.196	–	M
3217	23 27 58.14	1.27	-53 22 55.23	0.75	1.918	0.267	0.907	0.181	11.35	3.05	5.68	1.68	96.87	27.76	0.164	–	S
3218	23 27 34.09	0.29	-59 59 58.64	0.29	5.007	0.388	3.077	0.249	6.38	0.62	5.94	0.56	30.17	66.53	0.169	–	S
3219	23 27 40.32	0.81	-58 17 25.00	0.84	2.212	0.265	1.028	0.179	9.39	2.12	7.46	1.69	35.61	57.42	0.156	–	S
3220	23 27 54.17	0.20	-54 03 45.09	0.22	4.472	0.406	4.321	0.304	2.37	0.38	0.00	0.34	144.62	37.30	0.187	–	S
3221	23 28 03.09	1.06	-50 35 37.82	0.69	3.022	0.297	1.214	0.195	12.82	2.65	7.29	1.44	79.46	21.98	0.172	–	S
3222	23 27 34.21	0.85	-59 23 07.82	0.88	4.003	0.337	1.341	0.211	12.12	2.22	9.91	1.78	34.61	46.78	0.187	–	S
3223	23 27 42.51	0.15	-57 10 09.92	0.16	34.785	2.025	26.105	1.463	5.76	0.12	0.00	0.08	143.48	2.14	0.278	-1.01	M
3224	23 28 00.92	0.51	-51 20 14.71	0.64	1.828	0.334	1.432	0.213	5.90	1.51	2.33	1.09	154.20	37.65	0.190	–	S
3225	23 27 35.04	1.04	-58 59 52.28	1.85	4.333	0.356	1.077	0.223	18.54	4.50	9.31	2.19	166.01	22.65	0.220	–	S
3226	23 27 59.38	0.30	-51 33 48.99	0.31	3.725	0.526	3.676	0.346	2.49	0.68	0.00	0.58	136.41	42.99	0.280	–	S
3227	23 27 41.04	0.37	-57 09 16.37	0.35	3.445	0.532	3.140	0.342	3.06	0.82	1.73	0.74	115.45	86.98	0.289	–	S
3228	23 27 45.17	0.14	-55 32 08.99	0.15	60.275	3.344	59.103	3.261	1.56	0.04	0.32	0.03	38.55	10.18	0.252	-0.17	S
3229	23 27 52.03	1.03	-53 05 25.94	0.79	1.728	0.284	0.954	0.191	8.60	2.44	5.92	1.81	88.33	50.29	0.170	–	S
3230	23 27 58.13	0.46	-50 41 36.52	0.61	2.538	0.313	1.605	0.206	7.60	1.36	4.97	1.06	179.30	38.81	0.173	–	S
3231	23 27 26.04	0.41	-59 39 58.20	0.34	4.906	0.546	3.495	0.360	6.15	0.89	3.70	0.72	69.71	29.97	0.286	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3232	23 27 35.65	0.16	-57 09 47.08	0.17	15.431	0.981	13.855	0.817	2.98	0.18	2.29	0.17	168.19	30.95	0.287	-0.13	S
3233	23 27 38.81	0.21	-55 53 17.78	0.32	95.959	5.393	24.056	1.408	19.69	0.68	9.25	0.31	106.01	3.11	0.481	-1.04	M
3234	23 27 33.27	0.75	-57 46 20.16	1.19	1.780	0.263	0.881	0.179	10.26	2.81	5.56	1.70	175.67	31.44	0.160	-	S
3235	23 27 53.04	0.18	-51 47 27.13	0.20	9.000	0.708	8.479	0.553	2.78	0.31	0.88	0.28	150.21	30.85	0.294	-	S
3236	23 27 29.31	0.25	-58 16 11.06	0.26	3.913	0.356	3.136	0.246	4.10	0.51	3.69	0.47	3.03	82.71	0.168	-	S
3237	23 27 54.26	0.84	-50 45 01.26	0.89	2.301	0.291	1.112	0.197	9.46	2.15	7.58	1.85	46.26	65.85	0.172	-	S
3238	23 27 46.58	0.27	-52 56 49.85	0.34	53.560	3.074	10.463	0.676	14.34	0.72	10.54	0.52	106.17	8.66	0.355	-	M
3239	23 27 31.37	0.39	-57 28 30.27	0.43	2.877	0.317	1.922	0.208	6.06	0.97	5.02	0.84	176.77	55.51	0.168	-	S
3240	23 27 54.54	0.60	-50 18 09.76	0.70	2.710	0.322	1.498	0.213	9.03	1.73	5.82	1.22	145.69	32.70	0.181	-	S
3241	23 27 53.53	0.20	-50 31 53.59	0.20	7.034	0.499	5.620	0.366	4.66	0.35	3.55	0.30	60.65	25.26	0.187	-	S
3242	23 27 46.39	0.67	-52 26 09.20	0.79	36.909	2.084	5.334	0.508	22.49	1.93	17.34	1.43	150.04	18.21	0.474	-	S
3243	23 27 52.32	0.74	-50 24 11.66	0.83	1.920	0.269	1.061	0.180	8.82	2.05	6.03	1.55	40.33	45.32	0.157	-	S
3244	23 27 41.46	1.27	-53 35 41.17	1.06	3.032	0.314	1.045	0.213	12.41	3.03	9.87	2.40	75.57	56.79	0.193	-	S
3245	23 27 44.65	0.14	-52 25 32.33	0.15	67.541	3.842	52.159	2.910	4.26	0.09	3.30	0.08	136.04	8.86	0.487	0.09	M
3246	23 27 17.43	0.49	-59 18 25.09	1.28	4.916	0.506	1.163	0.216	0.00	3.08	0.00	0.86	0.00	15.51	0.206	-	M
3247	23 27 24.00	0.26	-57 57 34.03	0.26	3.660	0.387	3.240	0.267	3.25	0.54	2.37	0.49	55.84	75.59	0.193	-	S
3248	23 27 37.18	0.29	-54 16 21.99	0.19	14.897	0.972	8.716	0.527	13.48	0.63	2.24	0.22	162.12	2.98	0.218	-0.69	M
3249	23 27 42.41	0.14	-52 50 52.45	0.15	46.578	2.609	41.743	2.315	3.33	0.06	2.04	0.06	109.37	6.42	0.289	-0.55	S
3250	23 27 49.64	0.15	-50 24 43.89	0.16	13.262	0.781	12.167	0.690	2.93	0.12	1.92	0.11	131.35	16.93	0.163	-0.15	S
3251	23 27 43.74	0.42	-51 44 02.44	1.28	22.897	1.386	16.651	0.946	35.11	3.12	0.00	0.34	73.93	3.73	0.239	-0.77	M
3252	23 27 42.35	1.48	-52 24 45.12	1.66	53.699	2.970	2.920	0.340	40.20	4.31	28.55	2.97	38.30	18.11	0.493	-	S
3253	23 27 41.50	0.94	-52 53 46.29	0.78	3.006	0.466	1.658	0.313	8.28	2.20	6.29	1.77	84.86	60.41	0.277	-	S
3254	23 27 10.28	0.18	-59 52 26.91	0.19	7.038	0.503	6.168	0.391	3.68	0.28	1.91	0.25	28.26	18.17	0.188	-	S
3255	23 27 39.24	0.14	-52 27 45.76	0.15	88.870	4.977	76.561	4.228	0.00	0.05	0.00	0.04	0.00	1.78	0.385	-0.88	M
3256	23 27 25.33	0.14	-56 08 22.07	0.15	17.164	0.981	16.039	0.896	2.23	0.08	1.96	0.08	161.00	43.19	0.154	-0.02	S
3257	23 27 45.69	0.51	-50 15 58.99	0.56	2.210	0.344	1.649	0.223	6.33	1.39	3.05	1.00	42.59	33.71	0.193	-	S
3258	23 27 26.89	0.72	-55 29 56.50	1.07	3.938	0.400	1.583	0.264	12.57	2.59	7.01	1.51	161.14	23.87	0.235	-	S
3259	23 27 23.17	0.36	-56 21 14.07	0.59	4.610	0.409	2.416	0.259	10.27	1.35	4.72	0.76	173.71	13.76	0.209	-	S
3260	23 27 33.60	1.50	-53 35 28.62	0.99	2.343	0.283	0.908	0.195	13.85	3.79	6.67	1.90	67.94	26.20	0.179	-	S
3261	23 27 08.30	0.34	-59 20 08.43	0.41	3.195	0.378	2.372	0.249	5.67	0.91	3.30	0.72	13.49	28.49	0.200	-	S
3262	23 27 38.00	0.29	-51 50 00.56	0.30	4.994	0.489	3.874	0.331	4.80	0.63	3.94	0.58	117.46	54.60	0.240	-	S
3263	23 27 27.41	0.19	-54 32 50.22	0.16	110.399	6.117	52.667	2.910	18.04	0.30	3.83	0.09	173.32	1.00	0.280	-0.92	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3264	23 27 08.01	2.52	-58 55 52.77	1.40	15.440	0.857	0.841	0.120	43.32	5.71	24.34	3.39	94.46	16.93	0.183	–	S
3265	23 27 24.55	0.14	-54 51 13.27	0.15	81.762	4.524	65.729	3.621	8.60	0.05	2.58	0.03	132.88	0.52	0.209	-0.71	M
3266	23 27 08.98	0.75	-58 24 11.49	0.43	9.517	0.590	2.570	0.261	16.98	1.68	9.39	0.99	93.88	12.15	0.217	–	S
3267	23 27 23.95	0.99	-55 03 19.49	0.33	9.954	0.668	2.047	0.244	0.00	2.32	0.00	0.61	0.00	8.80	0.216	–	M
3268	23 27 16.57	0.21	-56 44 31.04	0.21	6.243	0.542	5.749	0.402	2.71	0.37	1.87	0.34	48.44	64.81	0.244	–	S
3269	23 27 02.24	0.71	-59 28 14.14	0.86	2.539	0.318	1.257	0.214	9.34	2.11	6.37	1.51	21.84	36.63	0.187	–	S
3270	23 27 33.52	0.63	-51 48 00.90	0.76	2.290	0.465	1.743	0.296	6.98	1.96	0.30	1.15	145.31	28.11	0.269	–	S
3271	23 27 14.79	0.83	-56 34 38.33	0.95	2.685	0.325	1.211	0.220	9.95	2.32	7.54	1.79	26.34	50.57	0.193	–	S
3272	23 27 19.21	0.52	-55 17 35.43	0.64	1.757	0.288	1.251	0.187	6.12	1.48	3.94	1.17	7.17	49.77	0.164	–	S
3273	23 27 01.91	0.37	-58 56 53.74	0.42	2.085	0.354	1.908	0.225	0.00	0.94	0.00	0.77	0.00	44.04	0.195	–	S
3274	23 27 17.94	0.14	-55 09 36.20	0.15	71.661	3.956	69.954	3.853	1.31	0.02	1.19	0.02	21.66	51.48	0.196	-0.51	S
3275	23 27 19.38	0.87	-55 01 17.60	1.16	2.409	0.332	1.109	0.227	10.36	2.76	6.98	1.96	14.16	44.50	0.203	–	S
3276	23 27 22.45	0.85	-54 14 20.97	0.81	1.296	0.333	0.987	0.211	5.41	2.09	3.46	1.74	125.93	86.07	0.194	–	S
3277	23 27 23.49	0.67	-53 31 36.19	0.76	11.354	0.659	2.068	0.213	18.14	1.75	16.12	1.56	169.71	45.77	0.192	–	S
3278	23 26 56.94	1.43	-59 37 12.95	1.57	10.169	0.580	1.004	0.151	26.53	3.95	20.86	3.05	29.58	29.90	0.183	–	S
3279	23 27 03.23	0.80	-58 33 44.48	1.01	1.285	0.290	0.867	0.188	7.54	2.56	2.82	1.57	153.88	36.66	0.172	–	S
3280	23 27 00.56	0.84	-58 54 46.89	0.97	3.336	0.303	1.172	0.196	11.83	2.36	9.46	1.83	19.90	44.07	0.174	–	S
3281	23 27 15.60	0.18	-55 24 45.18	0.22	14.932	0.973	8.279	0.516	7.65	0.40	3.70	0.26	101.70	6.62	0.243	–	M
3282	23 27 04.80	0.91	-57 54 13.71	0.69	1.849	0.313	1.110	0.208	7.71	2.09	5.13	1.59	93.07	54.90	0.185	–	S
3283	23 27 22.79	0.53	-53 21 02.98	0.52	2.924	0.321	1.692	0.211	7.75	1.31	6.03	1.08	53.54	46.34	0.175	–	S
3284	23 27 01.14	0.14	-57 49 22.33	0.15	48.530	2.697	47.379	2.616	0.00	0.04	0.00	0.04	0.00	6.11	0.225	-0.44	S
3285	23 27 22.63	1.10	-52 34 21.78	1.47	4.427	0.417	1.369	0.276	15.49	3.71	9.13	2.17	151.81	29.25	0.257	–	S
3286	23 27 27.71	0.48	-50 46 10.91	0.53	2.293	0.295	1.549	0.194	6.56	1.21	4.84	1.04	35.54	54.23	0.162	–	S
3287	23 26 58.57	0.75	-57 58 51.24	0.87	1.133	0.298	0.873	0.189	5.08	2.09	3.35	1.68	7.90	91.64	0.174	–	S
3288	23 27 13.37	0.44	-54 21 07.37	0.27	4.284	0.415	2.987	0.272	8.52	1.01	0.00	0.48	103.30	9.69	0.209	–	S
3289	23 27 17.34	0.74	-53 36 10.83	0.73	1.311	0.291	0.985	0.186	5.52	1.83	3.66	1.55	52.53	79.60	0.169	–	S
3290	23 27 07.59	0.48	-55 41 59.76	0.46	1.896	0.386	1.749	0.240	3.07	1.11	1.25	0.98	58.54	93.79	0.216	–	S
3291	23 27 14.85	0.80	-53 39 35.98	0.72	1.206	0.260	0.876	0.167	6.22	1.98	3.50	1.51	58.72	55.05	0.151	–	S
3292	23 27 04.91	0.30	-55 44 10.36	0.36	4.496	0.491	3.446	0.327	5.39	0.78	3.26	0.63	7.35	30.14	0.253	–	S
3293	23 27 22.66	0.35	-51 02 59.44	0.29	16.143	1.033	5.403	0.382	13.04	0.86	4.96	0.40	34.60	5.77	0.240	–	M
3294	23 27 17.56	0.66	-52 30 38.78	0.59	8.082	0.561	2.660	0.303	12.57	1.57	10.65	1.27	109.84	34.88	0.252	–	S
3295	23 26 53.47	0.36	-57 37 30.80	0.25	7.545	0.480	3.385	0.255	11.42	0.77	6.18	0.48	98.12	8.80	0.163	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3296	23 27 21.03	0.39	-51 04 29.36	0.37	4.387	0.447	2.972	0.295	6.02	0.86	5.27	0.79	94.14	58.87	0.229	–	S
3297	23 26 41.89	1.03	-59 35 35.66	1.13	2.754	0.309	1.029	0.211	10.76	2.81	9.41	2.26	16.20	79.13	0.190	–	S
3298	23 27 08.01	0.56	-54 16 36.03	0.74	1.111	0.317	1.032	0.192	0.00	1.72	0.00	1.27	0.00	51.68	0.181	–	S
3299	23 26 55.73	0.42	-56 48 10.14	0.51	5.313	0.492	2.886	0.316	8.88	1.21	5.58	0.85	24.29	21.33	0.253	–	S
3300	23 26 47.02	0.43	-58 26 09.82	0.45	1.886	0.321	1.605	0.205	3.93	1.06	2.47	0.90	158.08	70.42	0.179	–	S
3301	23 27 00.38	0.69	-55 39 49.63	1.04	1.783	0.359	1.152	0.236	7.81	2.43	3.74	1.58	0.36	38.77	0.213	–	S
3302	23 27 19.80	1.02	-50 42 22.86	1.43	3.222	0.291	0.970	0.190	14.81	3.29	10.48	2.41	169.16	43.47	0.175	–	S
3303	23 27 20.43	0.86	-50 35 03.89	1.45	1.571	0.236	0.735	0.162	11.85	3.41	5.92	1.95	12.75	33.28	0.147	–	S
3304	23 27 06.61	0.20	-54 02 04.01	0.19	12.323	0.782	6.434	0.388	10.90	0.41	1.49	0.17	144.81	2.66	0.158	–	M
3305	23 27 06.45	0.22	-53 51 03.14	0.18	16.572	0.989	8.629	0.511	10.76	0.39	4.23	0.20	12.25	3.41	0.189	-0.41	M
3306	23 27 18.56	0.76	-50 42 53.41	1.00	1.467	0.290	0.961	0.189	8.45	2.53	3.13	1.47	149.03	31.98	0.172	–	S
3307	23 26 39.48	1.15	-59 17 24.35	1.22	2.428	0.271	0.863	0.187	11.57	3.12	9.49	2.41	150.83	65.37	0.169	–	S
3308	23 27 11.64	0.95	-52 01 54.49	0.56	43.625	2.413	3.835	0.315	34.24	2.32	19.85	1.21	83.86	7.82	0.321	–	S
3309	23 26 43.71	0.44	-58 23 26.30	0.59	4.921	0.415	2.268	0.258	9.97	1.35	6.97	0.98	176.22	22.65	0.209	–	S
3310	23 26 38.71	0.47	-59 04 28.89	0.47	2.723	0.335	1.811	0.220	7.00	1.21	3.94	0.89	42.35	27.50	0.184	–	S
3311	23 26 47.93	0.18	-57 14 09.55	0.19	11.154	0.777	9.527	0.599	3.64	0.27	2.85	0.25	147.62	34.47	0.280	–	S
3312	23 26 36.21	0.28	-59 09 28.34	0.29	3.253	0.327	2.562	0.221	4.83	0.63	3.17	0.54	32.85	32.57	0.163	–	S
3313	23 27 07.62	0.54	-52 33 42.87	0.56	5.588	0.634	2.874	0.278	10.85	1.74	0.00	0.36	134.37	6.19	0.229	–	M
3314	23 26 33.00	0.40	-59 35 10.81	0.36	3.701	0.377	2.436	0.248	6.29	0.88	4.96	0.77	70.72	54.74	0.194	–	S
3315	23 27 00.26	0.15	-54 13 10.62	0.16	15.686	0.916	14.461	0.816	2.42	0.11	2.26	0.11	111.10	83.71	0.179	-0.40	S
3316	23 27 13.69	0.17	-50 39 17.05	0.18	7.618	0.510	6.693	0.407	3.09	0.24	3.04	0.22	133.52	0.57	0.170	–	S
3317	23 26 47.77	0.19	-56 27 29.67	0.20	8.735	0.594	6.563	0.423	5.59	0.34	3.37	0.28	148.52	12.62	0.209	–	S
3318	23 27 10.78	0.89	-51 06 05.72	1.98	4.885	0.357	1.112	0.203	22.57	4.72	9.32	1.90	12.57	18.14	0.204	–	S
3319	23 26 53.27	0.35	-55 13 30.19	0.66	3.053	0.322	1.810	0.208	10.11	1.53	2.44	0.72	10.38	12.65	0.175	–	S
3320	23 26 58.91	0.40	-53 43 32.01	0.42	3.087	0.360	2.170	0.237	5.50	0.93	4.98	0.88	173.76	152.27	0.191	–	S
3321	23 26 41.02	0.30	-57 21 27.44	0.31	6.595	0.514	3.921	0.327	6.68	0.67	6.34	0.62	9.63	84.24	0.227	–	S
3322	23 26 54.23	0.18	-54 38 19.23	0.19	7.173	0.516	6.220	0.397	3.71	0.29	2.47	0.26	168.41	26.76	0.195	–	S
3323	23 27 09.12	0.24	-50 48 51.08	0.24	5.398	0.407	3.866	0.278	5.32	0.45	5.02	0.44	111.93	65.60	0.168	–	S
3324	23 27 05.69	1.82	-51 40 36.11	1.02	2.909	0.282	0.866	0.189	16.51	4.45	8.95	2.25	84.41	26.71	0.180	–	S
3325	23 26 42.92	0.14	-56 33 37.19	0.15	35.919	2.023	34.026	1.889	2.45	0.06	1.04	0.06	131.97	9.03	0.253	-0.88	S
3326	23 26 56.50	0.56	-53 31 51.32	0.70	1.356	0.272	1.051	0.173	5.67	1.63	2.79	1.25	16.94	49.22	0.156	–	S
3327	23 26 30.46	0.23	-58 19 38.35	0.54	5.639	0.596	3.881	0.298	0.00	1.23	0.00	0.42	0.00	6.16	0.208	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3328	23 26 41.37	1.06	-56 16 11.52	0.77	2.488	0.236	0.925	0.154	12.85	2.55	7.95	1.63	112.50	27.23	0.137	-	S
3329	23 27 02.01	0.14	-51 29 43.04	0.15	97.461	5.386	91.807	5.059	2.33	0.03	1.71	0.03	29.17	9.49	0.307	-0.74	S
3330	23 27 06.02	0.77	-50 27 13.86	0.86	1.413	0.260	0.909	0.171	7.43	2.11	4.79	1.63	141.36	53.85	0.153	-	S
3331	23 27 02.68	0.54	-51 14 57.57	0.58	3.318	0.372	1.891	0.245	7.62	1.31	6.62	1.23	138.29	81.11	0.204	-	S
3332	23 26 54.58	0.22	-52 41 52.23	0.31	55.439	3.173	15.893	0.976	15.06	0.65	9.70	0.41	85.31	5.63	0.435	-	M
3333	23 26 57.10	0.64	-52 02 53.12	0.79	49.603	2.739	3.935	0.310	30.71	1.82	25.11	1.47	172.25	17.76	0.313	-	S
3334	23 26 41.38	0.49	-55 39 39.73	0.41	4.397	0.446	2.627	0.291	7.55	1.10	5.51	0.89	82.61	35.20	0.234	-	S
3335	23 26 49.07	0.15	-53 53 20.28	0.16	12.455	0.744	12.153	0.689	1.83	0.12	0.00	0.11	158.68	23.20	0.168	-0.09	S
3336	23 26 51.18	0.90	-53 00 19.74	1.83	10.345	0.735	1.645	0.266	19.02	4.65	2.70	1.15	113.67	13.29	0.250	-	M
3337	23 26 48.50	0.88	-53 43 49.17	0.65	3.427	0.339	1.545	0.219	12.84	2.32	5.03	1.06	61.00	15.70	0.192	-	S
3338	23 26 33.30	0.30	-56 31 09.86	0.35	4.452	0.445	3.233	0.296	5.66	0.75	3.98	0.62	170.20	32.49	0.224	-	S
3339	23 26 45.98	0.60	-53 48 43.51	0.49	1.013	0.276	1.017	0.165	0.00	1.39	0.00	1.09	0.00	55.10	0.156	-	S
3340	23 26 56.62	1.38	-50 58 55.14	1.17	2.735	0.258	0.832	0.172	13.58	3.33	11.26	2.64	103.39	55.85	0.159	-	S
3341	23 26 13.43	0.14	-58 59 22.01	0.15	38.516	2.155	38.050	2.105	1.14	0.05	0.47	0.05	126.31	119.53	0.229	-0.48	S
3342	23 26 51.88	0.61	-51 46 34.18	0.70	2.280	0.379	1.553	0.247	6.93	1.71	4.13	1.28	146.00	43.36	0.218	-	S
3343	23 26 54.00	0.90	-51 07 45.86	0.79	1.615	0.284	1.011	0.186	8.94	2.47	3.31	1.35	56.00	27.32	0.168	-	S
3344	23 26 45.79	0.27	-52 33 43.91	0.28	7.893	0.598	5.061	0.389	7.09	0.62	5.01	0.48	139.24	19.69	0.253	-	S
3345	23 26 34.03	0.25	-54 43 01.08	0.27	4.220	0.417	3.553	0.288	3.93	0.54	2.96	0.50	164.98	56.92	0.204	-	S
3346	23 26 05.76	0.31	-59 26 28.80	0.34	2.757	0.285	2.051	0.190	5.90	0.77	2.99	0.59	34.06	21.19	0.145	-	S
3347	23 26 21.20	0.14	-56 55 38.14	0.15	86.288	4.815	85.066	4.702	1.49	0.04	0.00	0.04	147.27	11.59	0.470	0.04	S
3348	23 26 17.38	1.27	-57 29 25.12	0.61	4.137	0.510	1.310	0.224	0.00	3.22	0.00	0.67	0.00	11.26	0.212	-	M
3349	23 26 46.55	0.37	-51 29 37.02	0.49	30.338	1.876	8.629	0.567	17.70	1.23	8.00	0.55	122.06	6.00	0.311	-	M
3350	23 26 30.83	0.45	-54 22 22.02	0.38	7.237	0.499	3.025	0.277	10.95	1.05	8.04	0.79	68.78	19.41	0.206	-	S
3351	23 26 48.41	0.17	-50 35 53.99	0.17	8.097	0.534	7.319	0.439	3.50	0.23	1.52	0.19	127.86	15.42	0.172	-0.31	S
3352	23 26 27.72	0.16	-55 00 20.01	0.18	9.523	0.605	7.700	0.463	5.16	0.25	2.27	0.19	0.96	8.57	0.180	-0.89	S
3353	23 26 23.59	0.98	-55 35 09.66	1.07	2.276	0.336	1.101	0.230	10.14	2.82	6.33	1.89	143.28	40.23	0.205	-	S
3354	23 25 57.87	0.53	-59 35 34.01	0.70	2.238	0.238	1.136	0.156	9.40	1.66	5.87	1.14	17.59	25.25	0.133	-	S
3355	23 26 07.84	1.15	-58 01 53.00	1.52	2.880	0.275	0.856	0.184	14.99	3.82	9.38	2.34	156.53	32.04	0.173	-	S
3356	23 26 20.52	0.14	-55 48 35.68	0.15	48.115	2.681	44.340	2.452	2.66	0.05	1.94	0.05	64.35	10.98	0.252	-0.61	S
3357	23 26 41.70	0.15	-51 35 43.95	0.16	19.227	1.125	18.802	1.058	1.76	0.10	0.00	0.09	144.94	22.03	0.221	-0.43	S
3358	23 26 00.18	0.78	-58 58 12.35	0.52	4.693	0.467	2.227	0.303	10.95	1.80	5.64	1.11	72.20	20.36	0.259	-	S
3359	23 26 08.75	1.46	-57 21 43.96	1.38	44.079	2.429	1.691	0.168	40.99	3.45	38.08	3.19	60.00	66.78	0.266	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3360	23 26 06.72	0.94	-57 54 58.78	1.04	2.732	0.434	1.394	0.296	8.96	2.63	6.42	1.94	150.62	55.03	0.264	-	S
3361	23 26 36.20	0.49	-52 31 40.97	0.46	3.174	0.510	2.542	0.328	5.19	1.20	2.62	0.94	123.10	41.03	0.284	-	S
3362	23 26 43.69	0.17	-50 36 32.81	0.16	17.994	1.082	10.498	0.602	9.20	0.23	2.83	0.13	13.17	2.51	0.171	-0.23	M
3363	23 25 58.63	0.22	-58 49 09.67	0.17	32.900	1.870	11.215	0.645	12.84	0.41	5.83	0.20	11.83	2.73	0.188	-0.61	M
3364	23 26 06.36	0.59	-57 51 02.46	0.72	1.369	0.430	1.335	0.256	0.00	1.80	0.00	1.19	0.00	40.45	0.245	-	S
3365	23 26 39.15	1.56	-51 34 21.07	1.17	3.164	0.357	1.144	0.243	15.55	4.30	6.55	1.82	121.36	22.70	0.229	-	S
3366	23 25 49.53	0.38	-59 54 25.58	0.34	1.125	0.284	1.371	0.167	0.00	0.84	0.00	0.70	0.00	60.32	0.158	-	S
3367	23 26 30.98	0.20	-53 14 19.63	0.21	4.795	0.362	3.935	0.265	4.34	0.37	3.18	0.33	34.20	31.64	0.146	-	S
3368	23 26 13.03	2.05	-56 24 13.11	0.86	3.884	0.311	0.959	0.191	20.68	4.78	8.39	1.96	85.10	19.68	0.191	-	S
3369	23 25 58.24	0.89	-58 36 25.52	0.64	3.283	0.308	1.318	0.199	11.40	2.02	7.86	1.50	90.92	34.13	0.173	-	S
3370	23 25 53.55	0.66	-58 58 18.62	0.47	18.425	1.052	3.467	0.308	19.40	1.47	13.48	1.08	100.90	14.13	0.257	-	S
3371	23 25 56.60	0.55	-58 46 10.41	0.59	5.230	0.390	1.973	0.227	11.15	1.43	8.98	1.15	151.04	31.02	0.186	-	S
3372	23 26 40.47	0.33	-50 45 00.77	0.44	4.728	0.377	2.551	0.235	9.53	1.01	5.73	0.68	20.70	17.14	0.175	-	S
3373	23 25 49.02	0.59	-59 49 11.24	0.95	1.919	0.261	1.024	0.174	9.64	2.24	4.69	1.31	174.59	24.72	0.154	-	S
3374	23 25 48.95	0.78	-59 41 19.19	0.75	2.729	0.265	1.130	0.173	10.60	1.97	7.97	1.52	137.09	39.02	0.150	-	S
3375	23 26 14.29	0.17	-55 46 42.04	0.18	9.854	0.658	8.685	0.528	3.24	0.23	2.57	0.21	160.68	38.39	0.218	-	S
3376	23 26 18.97	0.51	-54 58 36.07	0.62	2.795	0.354	1.706	0.233	7.34	1.42	5.41	1.15	10.72	47.47	0.198	-	S
3377	23 25 56.49	0.65	-58 33 17.23	0.68	3.037	0.373	1.651	0.248	8.80	1.76	5.53	1.25	39.21	31.85	0.214	-	S
3378	23 26 38.92	1.12	-50 46 41.74	0.78	3.368	0.323	1.246	0.211	12.89	2.75	8.59	1.71	95.86	28.30	0.188	-	S
3379	23 26 30.39	0.29	-52 40 45.28	0.31	6.207	0.797	5.822	0.532	2.60	0.62	1.46	0.60	32.38	95.49	0.418	-	S
3380	23 26 07.99	0.36	-56 42 09.85	0.46	2.531	0.504	2.515	0.311	0.00	1.06	0.00	0.73	0.00	27.22	0.280	-	S
3381	23 26 38.17	0.50	-50 20 16.14	0.48	1.719	0.281	1.382	0.180	5.06	1.21	2.84	0.98	119.94	46.57	0.156	-	S
3382	23 25 51.36	1.05	-58 40 01.83	1.40	2.095	0.257	0.789	0.179	11.89	3.40	8.30	2.33	13.68	44.28	0.163	-	S
3383	23 26 09.87	0.46	-55 45 48.84	0.83	4.429	0.394	1.988	0.247	12.93	1.98	4.76	0.89	164.40	13.06	0.213	-	S
3384	23 26 19.57	0.38	-53 59 05.84	0.43	2.440	0.320	1.877	0.209	5.08	0.95	3.69	0.83	172.26	58.98	0.173	-	S
3385	23 26 34.59	0.16	-50 45 20.29	0.17	11.310	0.691	9.600	0.559	3.64	0.18	3.28	0.16	102.72	33.97	0.177	-0.54	S
3386	23 26 24.78	0.93	-52 42 09.94	0.23	82.828	4.687	28.452	1.623	38.73	2.18	4.96	0.32	7.86	2.96	0.430	-1.06	M
3387	23 25 57.45	0.32	-57 31 36.40	0.83	10.148	0.752	3.572	0.319	13.30	1.96	0.00	0.55	78.08	7.79	0.251	-	M
3388	23 26 03.23	0.65	-56 38 49.79	0.74	2.199	0.542	1.787	0.340	4.58	1.75	2.88	1.46	6.54	91.48	0.312	-	S
3389	23 26 08.07	0.22	-55 44 40.77	0.22	6.181	0.505	5.122	0.363	4.06	0.41	3.16	0.38	55.27	46.25	0.220	-	S
3390	23 25 52.42	0.67	-58 14 11.41	0.71	1.469	0.308	1.084	0.198	5.16	1.71	4.14	1.48	161.99	113.24	0.178	-	S
3391	23 26 15.34	0.86	-54 12 41.04	0.75	1.104	0.248	0.792	0.160	6.07	2.05	3.92	1.65	68.45	71.31	0.145	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3392	23 26 14.85	0.73	-54 03 21.52	0.24	35.074	2.081	15.649	0.894	32.33	1.73	3.51	0.26	12.30	2.63	0.242	-1.13	M
3393	23 25 47.39	0.90	-58 32 20.68	0.77	1.431	0.338	1.018	0.219	5.78	2.11	4.19	1.76	109.24	106.79	0.198	-	S
3394	23 25 41.81	0.86	-59 08 18.59	0.59	2.079	0.297	1.182	0.198	8.68	1.96	4.95	1.37	82.08	34.92	0.173	-	S
3395	23 25 50.68	0.40	-57 50 15.32	0.41	3.413	0.517	2.859	0.334	4.18	0.96	2.60	0.82	144.41	58.70	0.284	-	S
3396	23 25 46.69	1.03	-58 18 39.57	1.37	2.007	0.261	0.831	0.180	12.79	3.57	6.00	1.83	151.83	26.67	0.165	-	S
3397	23 25 49.70	0.92	-57 46 58.11	0.80	2.144	0.502	1.500	0.326	5.87	2.13	4.44	1.83	108.04	118.04	0.295	-	S
3398	23 26 14.58	0.60	-53 37 40.14	0.59	1.972	0.318	1.389	0.206	6.80	1.58	3.42	1.11	50.13	34.42	0.181	-	S
3399	23 25 37.99	1.15	-59 07 45.96	1.19	2.789	0.296	0.965	0.201	12.41	3.13	9.14	2.28	38.50	47.33	0.183	-	S
3400	23 25 49.31	0.62	-57 32 50.94	0.60	1.803	0.417	1.517	0.261	3.93	1.46	2.86	1.34	134.74	136.02	0.238	-	S
3401	23 26 16.48	0.82	-52 46 09.08	0.64	3.203	0.557	2.087	0.365	7.29	1.96	4.42	1.42	81.73	43.52	0.324	-	S
3402	23 26 05.12	0.25	-54 32 21.30	0.20	11.931	0.780	5.869	0.385	8.74	0.51	3.44	0.29	162.88	5.97	0.209	-	M
3403	23 25 34.65	0.64	-59 05 20.05	0.66	3.849	0.359	1.679	0.231	9.15	1.60	8.61	1.40	16.59	98.06	0.195	-	S
3404	23 25 51.26	0.16	-56 39 55.04	0.17	18.277	1.151	16.144	0.950	3.02	0.18	2.73	0.17	175.79	61.80	0.327	-0.34	S
3405	23 26 25.75	0.35	-50 04 12.04	0.83	9.299	0.596	2.994	0.288	19.09	1.95	6.23	0.68	169.46	8.10	0.238	-	S
3406	23 25 44.44	1.59	-57 34 30.74	1.95	7.526	0.452	0.922	0.171	25.84	4.99	17.01	3.17	151.84	26.46	0.198	-	S
3407	23 26 07.85	0.48	-53 29 11.47	0.55	5.006	0.369	2.263	0.215	14.38	1.57	3.44	0.55	40.63	8.01	0.172	-	S
3408	23 25 28.40	0.33	-59 17 31.10	0.31	10.024	0.631	4.132	0.322	9.79	0.70	8.88	0.64	116.35	55.42	0.211	-	S
3409	23 26 10.52	0.85	-52 59 24.42	1.10	2.500	0.340	1.171	0.232	10.00	2.55	7.30	1.99	10.98	56.90	0.206	-	S
3410	23 26 18.63	0.83	-51 09 37.95	1.28	2.417	0.280	0.981	0.190	12.45	2.98	7.61	1.93	172.77	35.20	0.171	-	S
3411	23 25 23.96	1.38	-59 43 09.77	1.18	2.379	0.254	0.825	0.172	14.87	3.74	6.98	1.91	50.85	24.89	0.161	-	S
3412	23 26 08.71	0.84	-52 54 23.68	0.75	2.356	0.346	1.313	0.232	8.22	2.04	6.19	1.63	116.07	55.96	0.203	-	S
3413	23 26 03.91	0.61	-53 36 20.14	0.48	1.584	0.263	1.199	0.169	6.33	1.47	2.25	0.99	68.75	29.62	0.149	-	S
3414	23 25 32.69	0.78	-58 04 33.21	0.69	30.489	1.741	6.955	0.456	24.48	2.33	6.68	0.64	140.32	5.89	0.248	-	M
3415	23 26 01.84	0.59	-53 45 51.98	0.52	2.571	0.335	1.631	0.220	6.90	1.37	5.29	1.14	105.75	53.05	0.187	-	S
3416	23 25 23.20	0.93	-59 17 03.13	0.73	1.987	0.353	1.201	0.235	7.75	2.20	4.89	1.62	69.17	52.51	0.209	-	S
3417	23 25 19.70	0.40	-59 39 27.34	0.39	2.563	0.323	1.923	0.212	4.97	0.93	3.99	0.80	37.27	71.41	0.174	-	S
3418	23 26 16.15	0.39	-50 45 35.95	0.41	2.198	0.320	1.847	0.208	4.01	0.89	3.12	0.87	131.72	98.39	0.174	-	S
3419	23 25 27.96	0.74	-58 29 51.63	1.22	4.113	0.380	1.421	0.247	13.86	2.90	7.89	1.66	8.90	23.55	0.224	-	S
3420	23 26 12.41	0.39	-51 21 25.57	0.43	3.545	0.430	2.610	0.283	5.69	0.97	4.07	0.82	143.08	47.36	0.230	-	S
3421	23 25 43.64	0.53	-56 09 55.96	0.62	1.926	0.258	1.205	0.170	7.14	1.47	5.08	1.16	160.30	44.49	0.145	-	S
3422	23 25 35.74	0.67	-57 10 55.91	0.81	5.723	0.605	2.644	0.399	10.80	2.06	6.25	1.29	150.59	24.26	0.346	-	S
3423	23 26 04.42	0.18	-52 22 55.45	0.25	14.560	0.965	8.659	0.528	9.88	0.48	3.38	0.24	107.68	4.24	0.228	-	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3424	23 25 26.91	0.16	-57 53 23.12	0.16	113.925	6.367	60.707	3.385	11.45	0.16	7.21	0.10	167.60	1.77	0.555	-1.20	M
3425	23 25 56.50	0.25	-53 22 18.88	0.27	5.666	0.430	3.769	0.284	6.25	0.54	5.21	0.48	158.97	38.33	0.180	-	S
3426	23 25 26.35	0.50	-57 52 31.65	0.59	15.362	1.168	6.106	0.689	10.64	1.37	8.73	1.11	178.14	32.52	0.559	-	S
3427	23 25 22.39	1.12	-58 22 21.66	0.72	4.791	0.480	1.919	0.315	13.75	2.75	5.79	1.34	116.75	18.80	0.284	-	S
3428	23 25 39.21	0.18	-55 57 22.61	0.19	6.725	0.482	5.846	0.372	3.32	0.28	2.83	0.27	33.59	64.20	0.181	-	S
3429	23 25 19.10	0.21	-58 22 57.65	0.18	32.807	1.910	13.230	0.782	12.91	0.42	4.18	0.17	154.24	2.34	0.286	-1.46	M
3430	23 25 48.26	0.25	-54 23 20.78	0.30	4.709	0.368	3.132	0.243	6.81	0.61	4.52	0.48	12.66	19.18	0.160	-	S
3431	23 25 53.11	0.35	-53 24 11.17	1.59	7.957	0.611	2.045	0.230	0.00	3.74	0.00	0.71	0.00	8.77	0.201	-	M
3432	23 26 03.19	0.77	-51 42 55.92	0.84	4.412	0.337	1.415	0.199	12.52	1.90	11.29	1.83	29.55	109.19	0.174	-	S
3433	23 25 52.87	1.04	-53 28 50.21	1.18	1.781	0.270	0.832	0.187	9.73	2.83	7.54	2.33	29.48	76.99	0.167	-	S
3434	23 25 52.51	1.10	-53 27 27.94	0.70	3.704	0.308	1.284	0.190	15.59	2.79	7.03	1.28	68.30	16.32	0.172	-	S
3435	23 26 00.32	0.18	-51 56 07.22	0.19	15.434	0.974	11.218	0.688	5.51	0.28	4.44	0.24	119.25	18.11	0.287	-	S
3436	23 25 12.29	0.23	-59 03 10.94	0.27	9.677	0.618	5.131	0.356	10.00	0.60	4.53	0.34	151.04	6.96	0.203	-	S
3437	23 25 54.18	0.25	-52 45 28.22	0.24	24.745	1.532	17.915	1.027	18.41	0.64	1.69	0.16	41.69	1.88	0.289	-1.29	M
3438	23 26 08.42	0.67	-50 22 50.58	0.87	2.832	0.281	1.262	0.183	12.14	2.23	6.41	1.24	148.35	21.11	0.159	-	S
3439	23 26 08.04	0.31	-50 20 10.97	0.36	2.914	0.324	2.309	0.216	5.22	0.77	3.16	0.64	24.71	36.73	0.167	-	S
3440	23 25 07.09	0.68	-59 31 59.70	1.52	2.440	0.230	0.822	0.150	15.89	3.60	6.42	1.52	176.38	18.46	0.142	-	S
3441	23 25 48.46	0.37	-53 44 57.86	0.43	2.344	0.316	1.845	0.206	5.00	0.96	3.31	0.82	6.10	51.34	0.171	-	S
3442	23 25 57.11	0.15	-52 00 09.78	0.16	83.782	4.669	40.323	2.239	12.29	0.18	1.63	0.07	119.58	0.95	0.311	-1.25	M
3443	23 26 06.18	0.40	-50 22 25.12	0.55	4.329	0.341	2.072	0.207	11.62	1.36	5.70	0.73	151.76	13.15	0.162	-	S
3444	23 25 10.42	0.44	-58 54 07.13	0.38	1.822	0.301	1.601	0.192	3.86	0.98	1.72	0.82	82.34	57.34	0.166	-	S
3445	23 25 57.59	0.59	-51 55 11.85	0.70	3.006	0.474	1.998	0.311	6.83	1.61	4.74	1.32	157.63	56.59	0.272	-	S
3446	23 25 17.44	1.00	-57 36 42.73	1.77	10.938	0.758	2.384	0.235	19.33	4.56	5.03	1.38	116.50	14.76	0.195	-	M
3447	23 25 36.78	1.19	-54 56 53.92	1.11	3.979	0.399	1.363	0.267	13.55	3.20	8.77	2.06	130.59	33.35	0.244	-	S
3448	23 25 56.06	1.44	-51 24 58.79	1.15	3.960	0.377	1.199	0.252	13.80	3.45	11.07	2.63	91.33	51.55	0.233	-	S
3449	23 25 35.33	2.39	-54 43 39.57	0.60	20.643	1.208	2.841	0.305	32.53	5.70	5.35	1.03	10.27	9.45	0.262	-	M
3450	23 25 25.06	0.30	-56 06 54.78	0.44	2.681	0.265	1.788	0.174	7.57	0.97	3.32	0.63	5.04	16.11	0.135	-	S
3451	23 25 22.41	0.93	-56 28 17.37	0.87	1.525	0.342	1.017	0.224	6.45	2.29	4.71	1.87	128.33	89.25	0.203	-	S
3452	23 25 31.87	0.58	-54 55 21.44	0.71	8.996	0.594	2.680	0.299	14.98	1.77	9.80	1.14	151.62	17.22	0.252	-	S
3453	23 25 22.87	0.44	-56 15 53.52	0.81	2.481	0.254	1.248	0.165	11.19	1.90	4.45	0.95	173.55	15.85	0.142	-	S
3454	23 25 24.89	0.54	-55 59 51.53	0.54	1.445	0.274	1.167	0.174	3.95	1.23	3.82	1.23	153.15	0.94	0.155	-	S
3455	23 25 37.73	1.14	-54 00 05.27	0.66	2.807	0.345	0.858	0.149	9.94	2.97	0.00	0.77	153.68	13.19	0.141	-	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3456	23 25 47.78	0.21	-52 12 16.24	0.23	6.102	0.465	4.789	0.331	4.94	0.42	3.53	0.35	142.99	25.90	0.191	–	S
3457	23 25 39.18	0.47	-53 24 58.07	0.48	1.868	0.322	1.552	0.205	3.96	1.11	3.32	1.03	40.38	179.44	0.180	–	S
3458	23 25 10.88	0.79	-57 19 59.47	0.79	5.403	0.466	2.072	0.291	13.70	2.28	6.59	1.19	44.91	17.20	0.256	–	S
3459	23 25 26.49	0.56	-55 14 03.21	0.81	2.962	0.316	1.433	0.208	10.18	1.88	6.33	1.26	9.12	27.39	0.178	–	S
3460	23 25 07.69	0.47	-57 41 28.33	0.45	3.610	0.509	2.659	0.332	5.40	1.12	3.97	0.94	130.28	60.64	0.281	–	S
3461	23 24 48.33	0.17	-59 49 40.90	0.18	6.032	0.416	5.374	0.332	3.08	0.24	2.36	0.22	68.75	48.79	0.147	–	S
3462	23 24 57.98	0.15	-58 39 15.10	0.16	122.050	7.305	113.285	6.459	3.20	0.13	0.00	0.12	40.35	8.99	1.675	-0.76	S
3463	23 25 21.37	0.14	-55 36 22.11	0.15	25.644	1.455	24.875	1.384	1.78	0.07	0.88	0.07	11.07	19.68	0.208	-0.74	S
3464	23 25 25.46	0.33	-55 04 37.33	0.68	4.600	0.394	2.293	0.246	12.04	1.57	3.85	0.69	6.05	11.08	0.201	–	S
3465	23 25 24.59	0.51	-55 10 31.11	0.69	2.066	0.353	1.487	0.228	6.51	1.60	3.19	1.14	179.36	36.29	0.202	–	S
3466	23 25 10.58	0.14	-56 56 28.74	0.15	1043.560	57.563	1027.620	56.576	1.03	0.02	0.94	0.02	74.18	109.39	2.532	-0.62	S
3467	23 24 46.01	0.16	-59 44 46.25	0.17	7.846	0.513	6.961	0.417	3.04	0.20	2.52	0.19	61.73	57.57	0.162	-0.67	S
3468	23 24 55.95	0.17	-58 39 29.62	0.18	53.738	3.545	46.509	2.818	4.19	0.23	1.47	0.20	32.68	10.93	1.147	-1.10	S
3469	23 25 32.50	0.17	-53 44 50.09	0.18	11.124	0.773	10.357	0.634	2.41	0.23	1.96	0.22	9.34	85.15	0.274	–	S
3470	23 24 53.19	0.49	-58 53 22.72	0.48	2.735	0.326	1.753	0.214	6.91	1.20	4.74	0.95	137.32	36.35	0.178	–	S
3471	23 25 33.14	0.14	-53 29 32.16	0.15	19.408	1.106	19.050	1.061	1.46	0.07	0.60	0.07	42.20	28.36	0.167	-0.19	S
3472	23 24 53.45	0.25	-58 48 56.59	0.25	3.833	0.358	3.159	0.249	4.05	0.51	3.16	0.46	45.35	56.40	0.171	–	S
3473	23 25 46.97	0.28	-51 00 06.61	0.33	4.962	0.375	2.940	0.237	7.80	0.70	5.85	0.57	22.48	26.74	0.161	–	S
3474	23 25 35.30	0.83	-53 03 48.53	0.64	0.855	0.262	0.776	0.159	0.00	1.98	0.00	1.42	0.00	52.37	0.150	–	S
3475	23 25 20.70	0.14	-55 02 28.96	0.15	130.970	7.218	87.741	4.832	6.17	0.03	3.96	0.03	87.87	1.09	0.255	-0.72	M
3476	23 25 30.95	0.70	-53 26 20.87	0.48	4.289	0.360	1.877	0.223	11.69	1.67	6.67	0.99	76.07	17.69	0.185	–	S
3477	23 25 26.02	0.46	-53 55 18.31	0.55	2.603	0.308	1.624	0.203	7.13	1.25	5.37	1.04	8.91	49.11	0.169	–	S
3478	23 25 46.26	0.79	-50 29 54.19	0.77	1.481	0.256	0.941	0.169	7.52	2.04	4.88	1.54	55.44	49.55	0.150	–	S
3479	23 25 43.01	0.42	-50 49 01.24	0.50	2.926	0.340	1.935	0.224	6.63	1.08	5.15	0.98	169.20	62.77	0.183	–	S
3480	23 24 49.05	0.77	-58 32 47.18	0.88	1.438	0.338	1.024	0.218	5.70	2.13	4.16	1.71	175.66	89.46	0.198	–	S
3481	23 24 44.39	0.64	-58 50 27.13	0.60	2.252	0.305	1.343	0.202	6.72	1.43	6.17	1.41	91.08	91.08	0.174	–	S
3482	23 24 51.36	0.84	-57 49 29.85	0.77	2.689	0.479	1.653	0.318	6.91	2.02	5.54	1.70	125.86	96.31	0.283	–	S
3483	23 24 27.99	2.63	-59 59 21.84	1.54	12.004	0.675	0.862	0.141	39.28	6.17	19.63	3.26	70.89	18.35	0.198	–	S
3484	23 25 37.93	0.61	-50 37 11.43	0.86	0.901	0.260	0.800	0.159	0.00	1.96	0.00	1.42	0.00	51.18	0.149	–	S
3485	23 25 34.68	0.20	-51 03 57.20	0.22	7.744	0.520	5.388	0.354	5.88	0.37	4.98	0.34	161.80	38.32	0.181	–	S
3486	23 25 28.14	0.68	-52 04 06.75	1.33	2.561	0.285	1.049	0.191	13.61	3.12	6.28	1.57	176.94	23.11	0.173	–	S
3487	23 25 04.54	0.49	-55 27 12.81	0.69	4.241	0.460	2.288	0.301	9.53	1.64	5.12	1.03	164.32	21.85	0.255	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3488	23 24 34.40	0.68	-58 56 33.82	0.61	3.611	0.322	1.530	0.205	9.90	1.59	8.38	1.35	121.32	61.76	0.172	–	S
3489	23 24 40.48	0.89	-58 09 43.03	0.84	1.812	0.300	1.039	0.201	8.81	2.38	4.66	1.55	47.98	35.58	0.179	–	S
3490	23 24 47.42	0.74	-57 19 39.76	0.67	2.194	0.424	1.531	0.275	6.02	1.78	4.33	1.47	60.68	80.81	0.246	–	S
3491	23 24 40.75	0.57	-58 04 19.12	0.67	1.328	0.321	1.141	0.199	4.33	1.60	1.37	1.24	165.11	59.61	0.183	–	S
3492	23 25 31.75	0.52	-50 58 32.84	0.66	1.428	0.275	1.139	0.174	5.88	1.57	1.89	1.10	25.94	37.61	0.156	–	S
3493	23 25 01.52	0.25	-55 26 15.52	0.28	4.980	0.569	4.621	0.389	3.23	0.57	0.00	0.49	18.20	36.00	0.290	–	S
3494	23 25 21.16	1.21	-52 37 05.10	1.11	3.338	0.339	1.193	0.226	14.66	3.44	7.45	1.77	51.78	24.24	0.208	–	S
3495	23 24 38.48	1.26	-58 09 50.66	1.18	2.399	0.284	0.885	0.197	12.04	3.28	8.61	2.37	48.56	50.57	0.179	–	S
3496	23 25 03.78	1.59	-55 04 10.32	1.10	2.478	0.334	1.075	0.226	15.21	4.32	3.16	1.41	59.11	18.81	0.217	–	S
3497	23 25 31.21	0.33	-50 50 16.42	0.38	2.921	0.326	2.223	0.217	5.43	0.82	3.76	0.70	27.20	45.67	0.170	–	S
3498	23 25 16.38	0.42	-52 52 59.34	0.58	12.078	0.932	4.529	0.389	14.22	1.49	5.06	0.62	121.59	8.00	0.299	–	M
3499	23 25 19.71	1.01	-52 33 55.86	0.83	2.106	0.338	1.147	0.228	8.86	2.48	5.94	1.79	71.67	47.87	0.203	–	S
3500	23 25 14.36	0.25	-53 10 31.84	0.35	5.505	0.469	2.929	0.230	8.37	0.83	0.00	0.34	62.34	6.32	0.164	–	M
3501	23 25 13.45	0.96	-53 16 52.76	0.87	3.134	0.289	1.163	0.187	13.40	2.60	7.84	1.54	53.91	24.23	0.166	–	S
3502	23 25 09.41	0.59	-53 45 25.25	0.92	3.223	0.410	1.690	0.273	9.98	2.15	5.36	1.33	175.91	27.44	0.239	–	S
3503	23 24 59.32	0.26	-55 06 06.33	0.29	4.742	0.432	3.631	0.294	5.06	0.58	3.73	0.51	6.60	36.77	0.205	–	S
3504	23 24 38.15	1.13	-57 35 24.92	1.68	18.822	1.053	1.577	0.196	35.23	4.20	18.95	2.20	24.18	13.69	0.247	–	S
3505	23 25 10.60	0.64	-53 20 52.08	1.40	9.182	0.532	1.388	0.164	27.81	3.31	12.59	1.43	8.25	11.70	0.169	–	S
3506	23 24 21.64	0.21	-59 14 45.88	0.22	5.188	0.437	4.464	0.317	3.34	0.39	2.93	0.36	29.10	88.49	0.194	–	S
3507	23 24 34.04	0.26	-57 47 15.20	0.31	5.192	0.523	4.158	0.355	5.16	0.65	2.28	0.51	11.15	20.99	0.260	–	S
3508	23 25 05.76	0.18	-53 46 24.73	0.20	10.415	0.691	8.110	0.507	5.07	0.30	3.45	0.25	167.22	16.58	0.230	–	S
3509	23 24 54.41	0.27	-55 10 28.78	0.38	5.482	0.498	3.756	0.329	7.71	0.85	2.57	0.51	14.91	12.56	0.243	–	S
3510	23 25 23.78	0.90	-50 54 59.43	0.98	1.721	0.300	0.980	0.202	8.13	2.36	6.15	1.99	139.02	72.71	0.180	–	S
3511	23 25 09.80	0.82	-52 36 55.06	0.57	1.044	0.360	1.049	0.211	0.00	1.97	0.00	1.26	0.00	41.06	0.205	–	S
3512	23 24 32.73	0.28	-57 38 08.53	0.18	14.573	0.993	8.220	0.521	0.00	0.58	0.00	0.23	0.00	3.70	0.259	–	M
3513	23 25 18.32	1.09	-51 23 10.38	2.10	4.166	0.353	1.069	0.225	20.64	5.16	8.55	2.09	161.64	21.55	0.223	–	S
3514	23 24 25.05	0.73	-58 16 58.01	0.58	1.651	0.280	1.122	0.183	7.03	1.74	3.58	1.23	116.84	36.82	0.162	–	S
3515	23 24 16.32	0.60	-59 09 27.86	0.48	2.531	0.365	1.714	0.239	6.62	1.37	4.13	1.08	73.73	43.03	0.205	–	S
3516	23 24 31.25	0.25	-57 34 42.56	0.26	5.374	0.563	4.859	0.391	3.26	0.52	1.63	0.46	149.91	42.16	0.279	–	S
3517	23 24 21.78	0.51	-58 33 09.12	0.64	1.806	0.291	1.269	0.190	6.19	1.49	3.81	1.13	176.09	42.33	0.166	–	S
3518	23 25 09.58	0.21	-52 27 16.69	0.22	5.859	0.455	4.836	0.331	4.25	0.39	3.20	0.35	36.72	38.40	0.190	–	S
3519	23 25 00.05	0.17	-53 45 08.05	0.18	15.576	0.947	11.388	0.677	5.72	0.23	3.99	0.19	146.24	11.16	0.242	-1.18	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3520	23 24 38.40	0.15	-56 30 13.00	0.15	27.135	1.619	25.030	1.403	0.00	0.11	0.00	0.08	0.00	2.67	0.268	-0.89	M
3521	23 24 46.66	0.43	-55 24 31.75	0.40	34.686	2.026	6.948	0.535	13.16	0.97	11.80	0.86	163.65	31.76	0.374	-	M
3522	23 25 11.47	0.59	-52 00 44.70	0.78	1.334	0.341	1.152	0.210	5.46	1.91	0.00	1.23	155.07	37.04	0.196	-	S
3523	23 24 35.94	0.98	-56 42 32.68	0.73	4.167	0.507	1.943	0.342	10.41	2.33	6.60	1.61	72.52	35.67	0.301	-	S
3524	23 25 05.36	0.49	-52 23 12.10	0.39	1.788	0.325	1.626	0.204	0.00	1.14	0.00	0.81	0.00	32.14	0.181	-	S
3525	23 25 16.12	0.71	-51 09 55.43	0.87	1.896	0.334	1.214	0.220	7.96	2.14	4.25	1.47	31.60	39.96	0.196	-	S
3526	23 24 06.69	0.63	-59 34 26.49	0.84	1.384	0.297	0.998	0.191	6.24	2.01	3.07	1.41	176.78	44.81	0.173	-	S
3527	23 24 03.67	1.03	-59 47 47.85	0.90	2.305	0.377	0.950	0.166	8.97	3.15	0.00	0.42	42.14	8.62	0.158	-	M
3528	23 24 52.88	0.67	-54 09 44.87	0.70	2.929	0.263	1.218	0.168	9.96	1.63	9.11	1.52	148.43	98.82	0.142	-	S
3529	23 24 16.43	0.56	-58 24 16.65	0.60	3.314	0.299	1.511	0.190	9.26	1.44	7.87	1.20	159.22	47.50	0.158	-	S
3530	23 25 02.54	0.21	-52 28 45.33	0.22	4.954	0.424	4.421	0.312	3.13	0.39	2.47	0.37	103.60	64.74	0.190	-	S
3531	23 25 13.10	1.40	-50 38 30.15	1.20	3.039	0.267	0.877	0.172	16.10	3.79	10.04	2.21	59.88	29.51	0.162	-	S
3532	23 24 16.56	0.41	-57 34 43.25	0.67	27.559	1.614	4.670	0.386	18.09	1.59	9.38	0.83	75.00	9.02	0.288	-	M
3533	23 24 52.99	0.81	-53 21 07.36	0.97	1.779	0.285	0.978	0.192	8.36	2.28	6.26	1.86	161.82	67.44	0.170	-	S
3534	23 24 39.95	0.76	-54 57 03.92	0.61	1.627	0.397	1.336	0.248	4.88	1.76	2.28	1.40	93.41	65.40	0.228	-	S
3535	23 23 59.42	0.47	-59 17 07.69	0.38	3.716	0.406	2.435	0.267	7.06	1.04	4.21	0.80	111.94	27.47	0.215	-	S
3536	23 25 11.68	0.47	-50 01 34.11	0.45	21.348	1.231	5.069	0.413	15.12	1.10	14.51	0.95	92.10	32.73	0.305	-	S
3537	23 24 31.70	0.22	-55 38 29.89	0.18	35.098	2.039	20.413	1.156	13.92	0.42	2.46	0.14	27.62	1.91	0.275	-0.88	M
3538	23 24 14.92	0.93	-57 29 37.78	1.17	1.947	0.322	0.979	0.221	8.93	2.80	6.71	2.11	179.76	64.24	0.198	-	S
3539	23 25 00.50	0.39	-51 28 45.43	0.36	16.689	1.053	5.560	0.403	12.23	1.02	5.41	0.54	39.32	8.26	0.263	-	M
3540	23 25 06.27	0.24	-50 39 58.08	0.31	3.213	0.346	2.860	0.238	0.00	0.64	0.00	0.46	0.00	19.66	0.174	-	S
3541	23 24 29.05	0.15	-55 42 59.17	0.16	17.433	1.015	16.801	0.944	2.00	0.10	0.91	0.09	66.42	21.24	0.194	-0.53	S
3542	23 24 47.77	0.31	-53 17 05.63	0.31	2.244	0.268	1.933	0.179	3.58	0.66	2.87	0.64	70.50	98.99	0.140	-	S
3543	23 24 04.40	0.79	-58 19 42.34	0.92	2.122	0.278	1.037	0.188	9.41	2.28	6.62	1.65	156.02	42.40	0.166	-	S
3544	23 25 08.34	0.41	-50 01 01.53	0.41	3.541	0.588	3.209	0.375	3.72	0.98	0.64	0.82	122.19	48.15	0.323	-	S
3545	23 25 04.56	0.14	-50 23 51.18	0.15	26.334	1.469	25.896	1.431	1.47	0.05	0.52	0.04	0.15	18.94	0.142	-0.55	S
3546	23 24 11.11	0.16	-57 19 18.51	0.21	29.043	1.768	14.864	0.876	9.48	0.36	2.22	0.18	98.13	3.15	0.315	-1.13	M
3547	23 25 00.15	0.18	-51 00 34.34	0.19	7.253	0.495	6.206	0.385	3.57	0.26	3.17	0.25	132.20	60.02	0.172	-	S
3548	23 23 54.00	0.88	-58 59 06.51	0.98	1.918	0.278	0.946	0.190	8.51	2.39	7.33	1.94	170.88	86.33	0.168	-	S
3549	23 24 56.70	0.55	-51 24 44.95	0.58	1.599	0.363	1.425	0.225	3.03	1.33	2.69	1.24	149.33	1.04	0.206	-	S
3550	23 24 21.96	0.14	-55 51 27.01	0.15	59.197	3.273	53.077	2.926	3.80	0.03	0.84	0.03	177.86	2.77	0.193	-0.99	S
3551	23 25 02.64	0.15	-50 20 43.62	0.17	10.190	0.624	9.110	0.527	3.06	0.16	2.62	0.16	158.39	59.61	0.160	-0.59	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3552	23 24 38.02	0.65	-53 50 52.74	0.59	2.318	0.313	1.412	0.207	7.23	1.54	5.64	1.28	115.52	58.36	0.178	–	S
3553	23 24 13.60	0.17	-56 39 28.47	0.18	10.989	0.766	10.234	0.628	3.03	0.24	0.48	0.21	150.39	18.01	0.274	–	S
3554	23 23 45.00	1.03	-59 29 43.03	0.88	1.954	0.280	0.945	0.191	9.18	2.49	6.98	1.93	119.82	67.35	0.170	–	S
3555	23 24 55.70	0.99	-51 15 29.44	1.52	5.128	0.388	1.324	0.227	19.50	3.89	9.23	1.76	153.63	19.17	0.218	–	S
3556	23 24 13.27	0.19	-56 37 01.39	0.21	12.222	0.842	8.962	0.589	5.39	0.36	4.11	0.31	1.44	21.15	0.304	–	S
3557	23 24 50.27	0.83	-51 37 34.33	0.43	17.794	1.064	4.241	0.414	19.93	2.01	10.05	0.91	86.43	9.96	0.353	–	S
3558	23 24 45.32	1.93	-52 26 28.57	1.32	8.737	0.502	0.898	0.141	28.92	4.70	19.80	2.95	84.19	23.25	0.170	–	S
3559	23 24 19.77	0.47	-55 25 43.75	0.24	35.806	2.138	21.706	1.248	18.18	1.09	3.48	0.30	18.20	3.48	0.364	-0.23	M
3560	23 24 46.08	0.18	-52 05 13.46	0.20	6.571	0.469	5.512	0.354	4.22	0.32	2.85	0.27	149.64	24.18	0.175	–	S
3561	23 24 42.62	0.24	-52 08 53.65	0.26	3.724	0.345	3.178	0.243	3.80	0.48	2.93	0.46	162.83	65.12	0.163	–	S
3562	23 24 36.89	0.66	-52 51 13.92	0.70	3.916	0.368	1.705	0.237	9.84	1.63	8.65	1.51	37.41	87.75	0.201	–	S
3563	23 23 28.96	0.85	-59 59 05.65	1.15	5.692	0.583	1.199	0.244	9.43	3.18	0.00	1.00	125.45	16.93	0.235	–	M
3564	23 24 12.13	0.15	-55 47 09.47	0.16	11.716	0.719	10.960	0.631	2.19	0.14	1.99	0.14	130.03	106.28	0.185	-0.56	S
3565	23 23 57.85	0.47	-57 11 27.50	0.48	3.384	0.505	2.552	0.327	5.60	1.19	3.22	0.93	141.39	39.93	0.281	–	S
3566	23 24 08.31	0.63	-56 05 40.82	0.58	1.016	0.226	0.846	0.142	4.06	1.43	3.03	1.33	80.91	146.55	0.129	–	S
3567	23 24 04.40	0.75	-56 27 45.72	0.60	1.641	0.400	1.355	0.250	4.80	1.73	2.19	1.36	91.45	66.48	0.230	–	S
3568	23 24 35.46	0.19	-52 39 44.65	0.19	7.462	0.525	6.119	0.392	4.02	0.30	3.56	0.29	96.87	50.30	0.193	–	S
3569	23 24 34.93	1.50	-52 37 48.98	2.14	6.801	0.628	0.950	0.183	15.82	5.37	8.85	2.98	65.99	37.14	0.176	–	M
3570	23 23 38.11	0.84	-58 56 59.82	0.53	0.718	0.254	0.729	0.148	0.00	1.91	0.00	1.21	0.00	39.76	0.145	–	S
3571	23 23 35.25	0.76	-59 06 29.71	0.76	14.182	0.845	2.782	0.316	16.94	1.90	14.76	1.62	143.29	36.53	0.289	–	S
3572	23 24 33.54	0.14	-52 43 41.65	0.15	68.909	3.814	67.226	3.706	1.58	0.03	0.89	0.03	65.34	12.75	0.246	-0.75	S
3573	23 24 25.91	1.45	-53 27 50.46	0.76	5.469	0.356	1.196	0.171	22.21	3.58	9.68	1.46	74.88	14.38	0.168	–	S
3574	23 24 03.17	0.53	-56 10 27.17	1.12	2.201	0.215	0.922	0.139	13.95	2.67	4.92	1.12	170.32	15.72	0.126	–	S
3575	23 24 13.49	0.32	-55 00 59.97	0.73	7.240	0.552	3.196	0.325	14.44	1.72	3.64	0.62	12.17	9.14	0.268	–	S
3576	23 23 24.59	0.34	-59 49 32.03	0.39	2.426	0.291	1.863	0.192	5.73	0.90	2.36	0.67	25.15	23.08	0.155	–	S
3577	23 23 49.48	0.17	-57 27 28.93	0.18	20.278	1.195	9.373	0.564	4.50	0.24	3.51	0.21	17.38	19.20	0.229	–	M
3578	23 24 42.13	1.40	-51 10 58.82	1.21	3.079	0.270	0.875	0.174	15.39	3.66	10.79	2.38	120.73	35.41	0.163	–	S
3579	23 23 30.37	0.41	-59 07 48.19	0.34	14.223	0.888	5.128	0.427	11.67	0.88	9.22	0.75	103.56	23.49	0.301	–	S
3580	23 24 29.64	0.45	-52 44 01.44	0.39	9.736	0.636	3.749	0.329	12.40	1.12	8.17	0.72	119.94	13.57	0.241	–	S
3581	23 24 19.77	1.16	-53 52 14.44	0.63	1.856	0.359	1.165	0.236	9.09	2.76	2.65	1.42	93.76	27.62	0.215	–	S
3582	23 24 45.05	0.49	-50 22 41.23	0.59	2.270	0.259	1.347	0.170	7.82	1.33	5.86	1.12	163.17	50.67	0.142	–	S
3583	23 23 20.41	0.66	-59 45 57.23	0.70	2.204	0.257	1.126	0.171	8.49	1.73	6.74	1.38	30.08	52.00	0.147	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3584	23 23 31.15	0.20	-58 38 37.09	0.23	6.120	0.481	4.940	0.345	4.77	0.41	2.65	0.34	14.57	18.14	0.203	-	S
3585	23 24 17.81	0.83	-53 52 11.85	0.61	2.554	0.368	1.505	0.244	8.89	2.05	4.36	1.24	112.46	27.36	0.214	-	S
3586	23 24 34.95	0.14	-51 30 31.01	0.16	117.674	6.537	61.550	3.406	10.40	0.12	1.44	0.05	100.81	0.80	0.379	-1.08	M
3587	23 24 43.55	0.60	-50 20 13.36	0.81	2.154	0.257	1.183	0.169	10.86	2.12	3.91	1.02	148.68	18.06	0.147	-	S
3588	23 23 53.49	0.53	-56 28 39.15	0.65	3.049	0.352	1.692	0.232	8.16	1.52	6.00	1.18	174.23	40.09	0.197	-	S
3589	23 24 09.68	0.65	-54 29 37.68	0.68	3.138	0.410	1.786	0.272	8.04	1.71	5.88	1.34	140.59	47.06	0.234	-	S
3590	23 23 51.09	1.43	-56 29 03.18	1.38	3.061	0.293	0.868	0.197	13.11	3.39	12.12	3.18	128.21	157.70	0.185	-	S
3591	23 24 17.80	0.24	-53 25 44.87	0.27	4.745	0.407	3.640	0.280	5.32	0.54	3.52	0.45	25.99	27.09	0.186	-	S
3592	23 24 36.73	0.49	-50 41 43.34	0.60	6.408	0.442	2.285	0.239	12.61	1.42	9.60	1.06	155.15	26.56	0.191	-	S
3593	23 23 44.88	0.31	-56 53 20.96	0.26	12.921	0.994	8.143	0.643	7.16	0.63	4.94	0.51	97.33	20.75	0.429	-	S
3594	23 24 03.51	1.05	-54 52 13.40	0.84	7.184	0.699	2.658	0.460	12.07	2.53	8.88	1.85	112.10	40.06	0.409	-	S
3595	23 24 01.40	0.35	-55 02 17.50	0.36	3.500	0.460	2.926	0.302	3.82	0.78	3.24	0.75	145.94	127.96	0.246	-	S
3596	23 23 23.23	0.85	-58 46 45.35	0.82	1.745	0.265	0.965	0.178	9.09	2.29	4.94	1.50	45.60	33.83	0.158	-	S
3597	23 23 31.67	0.84	-57 52 52.87	0.85	1.452	0.333	1.025	0.215	6.83	2.32	2.93	1.54	139.99	43.38	0.196	-	S
3598	23 23 55.86	0.52	-55 26 28.51	0.65	2.026	0.399	1.606	0.254	5.39	1.53	2.44	1.15	16.36	46.46	0.227	-	S
3599	23 24 05.88	0.25	-54 07 39.96	0.25	5.652	0.439	3.951	0.295	5.90	0.53	4.61	0.45	129.97	28.98	0.187	-	S
3600	23 23 46.73	0.57	-56 11 15.89	1.22	1.860	0.226	0.875	0.150	12.64	2.88	4.14	1.24	9.05	18.62	0.137	-	S
3601	23 23 18.88	0.62	-58 36 13.84	1.57	4.195	0.468	1.023	0.202	0.00	3.89	0.00	0.57	0.00	9.97	0.194	-	M
3602	23 24 21.70	0.51	-51 55 32.73	0.56	3.150	0.383	1.964	0.252	7.63	1.39	4.97	1.03	142.86	33.86	0.211	-	S
3603	23 23 33.52	0.48	-57 13 47.94	0.85	5.964	0.514	2.516	0.320	13.24	2.04	5.38	0.95	16.26	14.21	0.277	-	S
3604	23 24 01.80	0.63	-54 15 46.89	0.60	1.597	0.319	1.239	0.204	4.96	1.50	3.63	1.33	62.05	98.19	0.182	-	S
3605	23 23 16.95	0.75	-58 35 41.22	0.89	3.963	0.352	1.441	0.225	11.30	2.13	9.43	1.70	5.30	48.05	0.197	-	S
3606	23 23 22.33	0.64	-58 06 46.77	0.65	2.588	0.363	1.552	0.240	7.13	1.62	5.68	1.33	142.66	65.57	0.208	-	S
3607	23 23 32.24	0.48	-56 59 15.76	1.80	19.448	1.224	3.597	0.364	25.10	4.24	5.74	1.06	94.34	10.05	0.305	-	M
3608	23 23 34.41	0.76	-56 54 53.25	0.84	2.943	0.597	1.965	0.391	6.11	1.98	5.02	1.73	7.79	114.47	0.350	-	S
3609	23 23 50.80	0.18	-55 10 27.34	0.20	7.996	0.578	6.786	0.437	4.18	0.31	2.41	0.27	10.39	19.62	0.220	-	S
3610	23 23 09.05	0.58	-59 05 38.26	0.79	3.487	0.358	1.642	0.234	10.70	1.92	5.84	1.17	23.46	21.75	0.202	-	S
3611	23 23 00.22	0.15	-59 45 55.15	0.16	10.393	0.627	8.774	0.507	3.64	0.15	3.03	0.15	32.51	25.17	0.151	-0.62	S
3612	23 23 34.13	0.14	-56 45 52.62	0.15	50.779	2.872	48.633	2.703	2.47	0.07	0.00	0.06	145.73	7.84	0.389	-0.69	S
3613	23 23 13.93	0.30	-58 31 46.76	0.23	17.885	1.088	6.519	0.425	11.59	0.66	6.39	0.38	165.10	5.96	0.228	-	M
3614	23 24 02.38	0.62	-53 43 22.07	0.65	2.589	0.572	2.105	0.360	4.72	1.56	2.89	1.35	40.86	82.55	0.327	-	S
3615	23 23 25.45	0.51	-57 26 00.38	0.49	2.482	0.383	1.849	0.249	4.90	1.14	4.33	1.10	125.27	162.88	0.214	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3616	23 23 12.51	0.29	-58 30 35.84	0.28	6.228	0.529	4.282	0.352	5.58	0.61	4.99	0.55	129.02	75.18	0.244	–	S
3617	23 23 38.51	0.43	-55 59 14.88	0.66	5.371	0.383	2.009	0.214	13.10	1.54	7.61	0.91	169.14	14.95	0.174	–	S
3618	23 23 57.03	1.63	-53 47 08.84	0.59	70.534	4.047	11.819	0.817	33.44	3.83	11.98	1.31	6.30	9.03	0.494	–	M
3619	23 24 25.49	0.28	-50 18 09.95	0.31	2.725	0.286	2.268	0.195	4.62	0.66	2.67	0.54	34.73	35.69	0.144	–	S
3620	23 23 34.87	0.88	-56 07 37.94	0.64	1.845	0.251	1.022	0.167	9.77	2.18	4.34	1.24	118.22	24.23	0.147	–	S
3621	23 23 54.95	0.83	-53 48 11.39	0.57	71.794	4.003	6.940	0.617	21.25	1.93	14.38	1.29	4.70	13.81	0.485	–	M
3622	23 24 11.88	0.82	-51 38 57.54	1.42	111.516	6.508	13.524	1.192	21.21	3.50	10.05	1.57	71.29	14.73	0.932	–	M
3623	23 23 16.82	0.51	-57 34 19.21	0.45	30.347	1.733	9.493	0.576	20.69	1.47	5.71	0.43	141.72	4.40	0.244	–	M
3624	23 23 36.23	0.22	-55 45 16.80	0.22	4.994	0.390	3.944	0.277	4.33	0.40	3.88	0.38	143.76	71.26	0.164	–	S
3625	23 22 48.82	0.18	-59 48 40.35	0.20	7.526	0.552	5.195	0.328	5.07	0.33	2.29	0.25	128.22	10.47	0.160	–	M
3626	23 22 18.23	1.36	-57 16 21.53	0.63	9.738	0.605	2.438	0.262	27.51	3.36	3.74	0.63	114.62	7.72	0.262	–	S
3627	23 24 13.80	0.16	-51 10 30.80	0.17	13.121	0.788	10.767	0.623	4.15	0.17	3.51	0.16	50.21	26.62	0.186	-0.72	S
3628	23 24 20.11	0.32	-50 12 56.40	0.20	16.852	0.971	4.627	0.298	16.17	0.69	6.64	0.32	1.46	3.92	0.155	–	M
3629	23 23 15.50	0.40	-57 28 03.27	0.38	2.983	0.322	2.039	0.212	5.99	0.91	4.71	0.78	127.60	51.24	0.168	–	S
3630	23 24 14.57	0.61	-50 52 50.52	0.87	14.046	0.812	2.641	0.259	23.41	2.23	11.97	1.06	151.23	10.48	0.232	–	S
3631	23 24 07.06	0.17	-51 39 33.30	0.18	171.542	9.645	68.281	3.879	13.02	0.28	8.75	0.19	58.67	3.24	0.971	-1.34	M
3632	23 24 15.00	0.35	-50 45 23.36	0.38	6.530	0.472	3.236	0.281	9.13	0.86	7.50	0.72	42.42	33.48	0.200	–	S
3633	23 24 10.81	1.56	-51 15 08.66	2.47	18.604	1.030	0.940	0.127	46.47	5.98	27.02	3.40	18.21	17.28	0.198	–	S
3634	23 23 07.02	0.31	-57 58 04.40	0.25	46.730	2.671	11.812	0.752	14.87	0.67	10.64	0.46	161.97	6.79	0.378	–	M
3635	23 23 40.30	0.15	-54 50 28.90	0.16	37.475	2.267	37.530	2.135	0.00	0.12	0.00	0.11	0.00	24.31	0.545	-0.23	S
3636	23 24 12.92	0.55	-50 52 21.10	0.81	6.500	0.486	2.298	0.282	13.79	1.89	8.70	1.21	13.64	21.75	0.238	–	S
3637	23 24 10.26	1.38	-51 11 57.49	1.24	3.519	0.316	1.019	0.206	15.01	3.62	10.80	2.44	123.10	38.43	0.193	–	S
3638	23 23 00.94	0.16	-58 21 40.42	0.17	8.374	0.533	7.597	0.448	2.75	0.18	2.24	0.17	138.62	44.72	0.157	-0.33	S
3639	23 23 46.35	0.14	-53 38 47.99	0.15	29.382	1.670	26.194	1.463	3.38	0.09	2.17	0.08	19.34	10.42	0.246	-0.56	S
3640	23 22 43.24	0.15	-59 26 37.37	0.18	122.353	6.813	44.273	2.471	12.93	0.24	5.13	0.11	72.13	1.60	0.423	-1.21	M
3641	23 22 52.18	0.91	-58 49 13.01	1.15	2.328	0.300	1.038	0.204	11.79	3.00	5.72	1.64	31.57	26.77	0.185	–	S
3642	23 23 00.78	0.65	-57 58 02.81	0.74	21.667	1.266	4.116	0.429	17.32	1.74	15.18	1.47	169.39	30.99	0.385	–	S
3643	23 22 52.45	0.81	-58 43 25.77	0.80	2.445	0.269	1.079	0.180	8.91	1.88	8.72	1.84	91.80	91.46	0.157	–	S
3644	23 23 41.19	0.15	-54 03 22.08	0.16	12.433	0.745	12.379	0.702	0.69	0.11	0.29	0.11	101.26	1.29	0.171	-0.58	S
3645	23 22 52.66	0.25	-58 32 45.22	0.28	5.085	0.415	3.547	0.278	6.23	0.59	3.94	0.47	154.93	18.75	0.186	–	S
3646	23 23 18.74	0.16	-56 13 01.38	0.17	8.385	0.516	7.104	0.416	3.62	0.18	3.11	0.17	13.58	34.79	0.137	-0.51	S
3647	23 24 13.16	0.55	-50 01 00.88	0.61	2.034	0.332	1.469	0.216	5.61	1.35	4.64	1.30	146.31	115.66	0.188	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3648	23 22 38.35	0.72	-59 40 13.39	0.80	1.466	0.286	0.978	0.187	6.26	1.98	4.65	1.55	160.58	72.35	0.168	–	S
3649	23 24 03.30	0.99	-51 15 57.11	0.68	2.049	0.326	1.185	0.217	8.92	2.40	4.87	1.48	87.52	33.19	0.193	–	S
3650	23 22 52.37	0.37	-58 29 24.10	0.40	3.745	0.378	2.420	0.248	6.22	0.91	5.36	0.79	11.91	58.21	0.195	–	S
3651	23 22 33.46	0.84	-59 52 54.57	0.89	2.969	0.268	1.115	0.171	13.64	2.49	6.72	1.34	40.72	19.62	0.153	–	S
3652	23 22 40.41	0.57	-59 21 31.75	0.51	2.600	0.544	2.216	0.341	3.79	1.27	2.67	1.17	108.74	132.66	0.308	–	S
3653	23 22 32.00	0.19	-59 57 05.00	0.20	6.463	0.451	5.154	0.332	4.22	0.30	3.59	0.28	12.59	34.49	0.165	–	S
3654	23 23 25.92	0.19	-55 13 30.52	0.17	20.081	1.263	12.549	0.739	8.53	0.31	2.04	0.17	26.12	3.30	0.265	–	M
3655	23 23 08.02	0.15	-56 52 13.45	0.16	26.428	1.540	24.635	1.388	2.30	0.10	1.95	0.10	142.66	42.33	0.296	-0.33	S
3656	23 22 34.93	0.28	-59 36 14.78	0.32	4.031	0.362	2.801	0.241	5.79	0.67	4.46	0.57	176.20	31.45	0.173	–	S
3657	23 23 39.05	0.15	-53 38 26.65	0.16	14.380	0.898	14.006	0.809	1.62	0.15	0.95	0.14	22.88	59.77	0.247	-0.39	S
3658	23 23 38.53	2.16	-53 36 32.25	1.04	16.611	0.942	1.566	0.226	34.94	5.17	17.47	2.38	91.46	15.47	0.282	–	S
3659	23 23 12.22	0.47	-56 16 19.24	1.09	2.919	0.246	1.120	0.152	15.54	2.59	4.98	0.97	171.96	13.08	0.137	–	S
3660	23 22 28.50	3.35	-59 41 51.15	2.08	8.282	0.520	0.814	0.168	24.59	9.06	4.53	1.95	31.95	19.46	0.162	–	M
3661	23 23 16.39	0.59	-55 43 04.12	0.85	1.612	0.280	1.052	0.183	7.59	2.00	3.79	1.33	179.07	35.29	0.163	–	S
3662	23 23 32.33	0.32	-53 36 24.65	0.94	34.909	2.050	10.397	0.636	24.22	2.18	7.81	0.69	90.01	6.18	0.278	–	M
3663	23 23 21.19	0.22	-54 58 46.42	0.20	17.748	1.416	12.040	0.791	6.78	0.44	1.18	0.27	29.58	6.81	0.433	–	M
3664	23 22 25.85	0.79	-59 38 20.08	0.93	1.429	0.306	0.939	0.201	6.41	2.27	4.74	1.74	1.79	77.24	0.181	–	S
3665	23 22 38.16	0.17	-58 37 42.61	0.17	7.485	0.506	6.666	0.407	3.31	0.23	2.12	0.21	87.38	27.70	0.172	–	S
3666	23 23 37.88	0.84	-52 48 43.83	1.01	2.330	0.372	1.261	0.251	8.96	2.47	5.95	1.80	152.33	49.00	0.223	–	S
3667	23 22 55.59	0.55	-56 58 42.19	0.65	2.238	0.574	2.086	0.348	0.00	1.66	0.00	1.00	0.00	28.95	0.327	–	S
3668	23 23 46.73	0.82	-51 42 00.35	0.91	2.827	0.635	1.956	0.413	5.87	2.12	5.04	1.90	168.85	1.27	0.373	–	S
3669	23 23 06.42	0.76	-55 53 44.31	1.05	1.771	0.326	1.052	0.217	8.27	2.50	4.75	1.69	167.29	43.16	0.195	–	S
3670	23 23 47.25	1.06	-51 29 45.78	0.74	1.910	0.425	1.302	0.276	7.64	2.61	2.97	1.58	104.64	37.49	0.252	–	S
3671	23 23 36.13	0.19	-52 44 04.25	0.20	11.346	0.754	8.299	0.530	5.27	0.32	4.55	0.29	130.62	31.76	0.254	–	S
3672	23 22 21.34	0.16	-59 24 08.83	0.18	78.547	4.462	37.313	2.095	13.29	0.27	7.23	0.16	61.22	2.31	0.421	-0.97	M
3673	23 23 21.54	0.15	-54 10 50.33	0.16	23.048	1.337	21.557	1.212	2.39	0.10	1.80	0.09	155.75	27.38	0.248	-0.24	S
3674	23 22 59.72	0.35	-56 13 36.12	0.58	1.971	0.235	1.324	0.153	8.15	1.32	2.17	0.74	8.40	16.50	0.128	–	S
3675	23 22 42.78	0.16	-57 35 44.31	0.17	18.265	1.077	12.157	0.694	7.84	0.21	2.85	0.13	141.97	2.73	0.187	0.69	M
3676	23 23 30.76	0.16	-52 55 11.35	0.18	208.671	11.599	67.922	3.776	15.81	0.25	5.86	0.10	125.56	1.22	0.552	-1.08	M
3677	23 23 35.25	0.94	-52 27 53.16	1.49	5.320	0.404	1.093	0.161	14.79	4.00	0.00	0.99	61.14	13.59	0.149	–	M
3678	23 22 24.43	0.68	-59 02 56.98	1.11	1.976	0.287	1.021	0.193	10.40	2.68	4.51	1.44	15.10	25.62	0.174	–	S
3679	23 23 36.64	1.05	-52 14 19.68	0.86	2.693	0.260	1.024	0.170	13.60	2.80	7.40	1.53	60.08	23.33	0.152	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3680	23 22 19.30	0.21	-59 21 51.97	0.22	5.721	0.630	6.084	0.455	0.00	0.41	0.00	0.36	0.00	70.94	0.314	-	S
3681	23 22 38.65	0.41	-57 48 52.66	0.62	7.214	0.506	2.737	0.280	13.08	1.45	7.19	0.83	16.87	13.49	0.224	-	S
3682	23 22 44.87	0.90	-57 20 13.07	1.01	1.886	0.319	1.028	0.215	8.92	2.61	5.46	1.79	34.79	44.67	0.193	-	S
3683	23 23 47.25	0.44	-50 53 04.22	0.37	8.460	0.566	3.472	0.306	11.22	1.05	8.47	0.74	79.04	17.97	0.222	-	S
3684	23 22 36.14	0.40	-58 00 37.37	0.41	3.521	0.380	2.336	0.250	5.95	0.94	5.24	0.83	25.47	81.08	0.200	-	S
3685	23 22 57.62	1.13	-56 08 49.91	0.37	8.227	0.555	2.182	0.202	18.57	2.68	2.32	0.65	171.81	7.62	0.162	-	M
3686	23 23 34.47	0.51	-52 20 48.83	0.41	4.957	0.374	2.222	0.222	10.53	1.21	7.53	0.85	75.03	21.10	0.171	-	S
3687	23 23 42.95	0.68	-51 14 25.00	0.80	2.387	0.296	1.241	0.198	8.96	1.88	6.82	1.53	153.25	54.77	0.171	-	S
3688	23 22 25.68	0.17	-58 29 53.50	0.18	12.067	0.744	8.725	0.526	5.46	0.24	4.17	0.21	167.00	14.05	0.203	-1.09	S
3689	23 23 42.91	0.16	-50 45 08.29	0.17	10.241	0.655	9.575	0.562	2.31	0.18	2.01	0.17	68.84	167.07	0.194	-0.96	S
3690	23 23 43.31	1.08	-50 39 40.98	0.70	2.763	0.319	1.250	0.213	11.85	2.71	6.20	1.44	78.35	24.06	0.190	-	S
3691	23 23 00.64	0.94	-55 11 12.07	0.86	3.994	0.609	2.103	0.412	8.64	2.32	6.52	1.85	59.76	67.00	0.365	-	S
3692	23 23 16.50	0.17	-53 30 23.38	0.18	17.197	1.112	10.765	0.642	5.93	0.26	3.58	0.20	122.63	8.24	0.249	-	M
3693	23 23 05.50	0.30	-54 36 32.62	0.29	12.290	1.125	8.940	0.756	5.34	0.64	4.45	0.57	115.19	52.11	0.540	-	S
3694	23 23 45.66	0.35	-50 08 53.06	0.40	2.713	0.278	1.868	0.184	6.50	0.91	4.59	0.73	150.41	35.90	0.142	-	S
3695	23 23 13.68	0.71	-53 42 24.62	0.71	2.129	0.342	1.332	0.226	6.87	1.73	5.60	1.55	50.23	95.99	0.198	-	S
3696	23 23 08.74	0.15	-54 03 47.46	0.16	16.688	1.000	15.563	0.888	3.01	0.13	0.81	0.12	44.80	11.97	0.231	-1.02	S
3697	23 22 17.48	0.24	-58 27 34.72	0.24	11.686	0.726	4.331	0.297	7.56	0.55	2.45	0.33	141.11	7.25	0.178	-	M
3698	23 22 07.22	0.87	-59 14 33.08	0.91	1.731	0.288	0.960	0.194	8.01	2.33	5.97	1.78	34.22	65.66	0.172	-	S
3699	23 22 48.20	0.14	-55 45 35.93	0.15	23.432	1.327	21.047	1.173	2.75	0.08	2.62	0.08	48.95	101.91	0.186	-0.54	S
3700	23 23 25.66	0.30	-51 57 04.76	0.33	5.554	0.470	3.635	0.309	6.54	0.70	5.30	0.61	146.70	39.54	0.219	-	S
3701	23 22 17.12	0.21	-58 10 41.97	0.21	7.288	0.509	5.237	0.351	5.76	0.38	4.03	0.33	49.98	19.11	0.189	-	S
3702	23 22 20.01	1.67	-57 51 34.04	2.30	11.217	0.774	1.427	0.262	19.59	6.58	0.00	1.11	56.09	14.21	0.249	-	M
3703	23 22 00.15	0.20	-59 24 34.47	0.17	21.860	1.480	14.852	0.894	0.00	0.33	0.00	0.17	0.00	3.74	0.363	-0.58	M
3704	23 22 20.31	1.22	-57 53 29.40	1.06	6.522	0.474	1.647	0.267	18.31	3.33	9.45	1.71	131.00	19.56	0.255	-	S
3705	23 22 41.29	1.69	-56 04 58.23	0.85	3.346	0.378	0.833	0.164	0.00	4.39	0.00	0.60	0.00	11.43	0.157	-	M
3706	23 22 35.03	1.33	-56 33 10.93	0.65	1.446	0.256	0.836	0.169	11.03	3.15	1.45	1.30	76.64	21.76	0.157	-	S
3707	23 22 38.49	0.65	-56 09 28.01	1.87	4.111	0.383	1.383	0.163	15.93	4.55	0.00	0.94	76.39	12.81	0.144	-	M
3708	23 23 20.28	0.16	-51 56 22.46	0.17	11.396	0.712	9.503	0.562	3.88	0.20	3.40	0.19	169.22	53.34	0.198	-0.88	S
3709	23 22 38.58	0.48	-56 00 30.01	0.46	3.055	0.302	1.766	0.195	8.97	1.28	4.45	0.79	133.81	17.98	0.159	-	S
3710	23 23 31.44	0.25	-50 33 46.58	0.28	5.600	0.463	4.054	0.314	5.62	0.56	4.55	0.50	152.79	44.52	0.208	-	S
3711	23 22 55.64	0.71	-54 19 05.59	1.18	12.082	0.813	3.156	0.416	20.24	2.99	8.05	1.18	26.26	13.17	0.389	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3712	23 22 13.81	1.69	-57 51 57.30	1.52	8.151	0.512	1.227	0.226	23.34	4.49	14.76	2.84	51.34	27.40	0.246	-	S
3713	23 23 16.52	0.56	-52 06 39.72	0.74	2.290	0.270	1.241	0.179	8.91	1.70	6.11	1.28	4.09	40.21	0.153	-	S
3714	23 23 20.66	0.38	-51 33 49.05	0.69	12.116	0.819	4.455	0.434	15.50	1.64	6.50	0.72	164.70	10.37	0.347	-	S
3715	23 22 46.53	0.56	-55 00 39.06	0.73	4.057	0.852	3.181	0.541	5.63	1.70	2.38	1.25	11.26	46.33	0.489	-	S
3716	23 22 12.03	0.24	-57 49 58.32	0.25	4.338	0.417	3.759	0.292	3.43	0.49	2.69	0.44	179.23	64.35	0.200	-	S
3717	23 23 30.37	0.50	-50 09 22.02	0.59	1.676	0.249	1.183	0.162	6.11	1.28	4.57	1.19	18.72	80.43	0.139	-	S
3718	23 22 56.22	0.44	-53 53 11.65	0.40	3.027	0.375	2.210	0.246	5.85	1.02	3.81	0.81	117.30	37.52	0.202	-	S
3719	23 22 03.52	1.11	-58 07 16.24	0.68	18.883	1.136	13.318	0.765	29.13	2.99	3.32	0.49	31.81	4.93	0.219	-0.16	M
3720	23 21 51.36	0.23	-59 07 54.30	0.23	4.144	0.366	3.514	0.260	3.84	0.44	2.73	0.40	48.81	44.70	0.168	-	S
3721	23 23 07.49	0.62	-52 31 24.61	0.66	5.382	0.447	1.744	0.188	12.13	1.92	2.46	0.77	49.21	11.34	0.162	-	M
3722	23 22 59.72	0.64	-53 21 21.93	0.61	1.763	0.411	1.520	0.255	5.25	1.70	0.00	1.12	130.50	35.52	0.235	-	S
3723	23 22 03.27	0.50	-58 11 48.68	0.45	3.259	0.326	1.850	0.212	7.53	1.13	6.19	0.97	70.48	63.14	0.172	-	S
3724	23 22 31.98	0.15	-55 51 43.02	0.16	9.391	0.602	9.367	0.545	0.00	0.16	0.00	0.15	0.00	41.93	0.179	0.15	S
3725	23 21 56.46	0.16	-58 34 40.12	0.16	21.557	1.233	11.001	0.632	6.75	0.20	4.37	0.15	26.89	5.27	0.183	-0.98	M
3726	23 22 30.99	0.19	-55 40 00.36	0.20	6.564	0.501	5.803	0.382	2.93	0.31	2.85	0.30	47.75	91.53	0.203	-	S
3727	23 23 10.35	0.91	-51 49 26.88	0.99	1.950	0.256	0.911	0.174	9.57	2.36	7.89	2.04	143.39	77.31	0.154	-	S
3728	23 21 49.58	0.49	-58 51 38.35	0.48	1.743	0.301	1.412	0.192	4.57	1.19	2.91	0.99	40.53	66.28	0.168	-	S
3729	23 23 04.06	0.14	-52 21 55.17	0.15	43.195	2.395	42.760	2.358	0.00	0.03	0.00	0.03	0.00	11.72	0.174	0.15	S
3730	23 22 03.32	0.40	-57 50 53.08	0.35	1.999	0.328	1.848	0.209	0.00	0.89	0.00	0.74	0.00	54.56	0.180	-	S
3731	23 21 39.38	0.31	-59 25 40.71	0.39	5.127	0.500	3.439	0.329	6.72	0.86	3.99	0.65	172.57	21.45	0.252	-	S
3732	23 22 52.57	0.14	-53 22 02.75	0.15	190.219	10.494	187.379	10.317	1.00	0.02	0.99	0.02	109.22	1.46	0.470	0.07	S
3733	23 22 48.98	0.14	-53 42 08.09	0.15	37.047	2.070	34.711	1.921	2.35	0.05	1.80	0.05	85.76	16.05	0.210	-0.76	S
3734	23 23 12.72	0.96	-51 16 04.85	1.07	1.588	0.291	0.891	0.197	8.22	2.54	6.27	2.16	146.08	81.01	0.176	-	S
3735	23 21 42.73	0.90	-59 07 37.99	0.45	1.953	0.286	1.205	0.187	9.49	2.02	2.30	1.03	94.66	20.15	0.166	-	S
3736	23 21 57.48	0.97	-58 02 39.37	0.99	2.324	0.268	0.947	0.183	10.19	2.49	8.78	2.08	34.34	89.50	0.162	-	S
3737	23 23 08.87	0.67	-51 20 32.28	0.63	2.624	0.327	1.475	0.217	7.77	1.59	6.65	1.40	110.66	67.83	0.185	-	S
3738	23 22 17.50	0.15	-56 10 17.80	0.16	8.718	0.536	7.845	0.454	3.04	0.16	2.21	0.15	29.76	26.16	0.139	-0.35	S
3739	23 23 00.03	0.66	-52 11 35.64	0.72	2.984	0.325	1.474	0.215	9.67	1.81	6.86	1.35	39.97	39.26	0.183	-	S
3740	23 23 14.01	0.52	-50 31 00.95	0.48	2.586	0.338	1.773	0.221	6.35	1.23	4.73	1.01	73.66	48.39	0.186	-	S
3741	23 23 05.07	0.77	-51 29 00.58	0.80	1.298	0.380	1.105	0.235	3.80	1.94	2.98	1.72	131.77	1.42	0.219	-	S
3742	23 22 25.93	0.22	-55 07 34.59	0.23	9.936	0.790	7.864	0.560	4.41	0.42	3.78	0.39	172.74	57.81	0.338	-	S
3743	23 23 10.85	0.89	-50 35 05.34	1.32	2.890	0.315	1.090	0.213	12.89	3.03	8.48	2.10	2.08	41.37	0.192	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3744	23 22 01.58	0.55	-57 02 44.97	0.73	2.563	0.339	1.517	0.224	8.53	1.76	4.38	1.12	160.01	26.24	0.194	–	S
3745	23 21 41.94	0.68	-58 28 48.11	0.71	1.235	0.277	0.946	0.176	4.83	1.70	3.80	1.51	21.41	124.56	0.160	–	S
3746	23 22 12.11	0.14	-56 05 46.09	0.15	70.525	3.890	69.314	3.816	1.31	0.02	0.72	0.02	47.56	12.64	0.168	-0.46	S
3747	23 21 30.23	0.41	-59 13 22.68	0.46	4.642	0.373	2.295	0.230	9.90	1.13	5.88	0.76	32.96	17.07	0.178	–	S
3748	23 21 35.03	0.29	-58 51 22.15	0.19	8.168	0.601	4.920	0.322	0.00	0.60	0.00	0.26	0.00	4.44	0.174	–	M
3749	23 22 18.52	1.15	-55 23 10.97	1.19	2.840	0.385	1.187	0.268	10.34	2.99	8.50	2.44	142.29	80.41	0.240	–	S
3750	23 22 30.94	0.38	-54 16 08.99	0.39	4.131	0.537	3.256	0.352	4.40	0.86	3.92	0.83	139.23	144.15	0.288	–	S
3751	23 23 08.93	0.98	-50 20 51.82	1.04	1.371	0.247	0.767	0.167	8.30	2.53	6.33	2.14	136.67	75.51	0.149	–	S
3752	23 21 28.66	1.69	-59 06 07.98	1.16	3.216	0.253	0.750	0.155	17.41	3.97	11.34	2.63	109.09	35.44	0.152	–	S
3753	23 23 02.24	0.25	-51 02 14.64	0.29	4.849	0.395	3.447	0.266	6.43	0.60	4.00	0.46	27.95	20.97	0.176	–	S
3754	23 21 47.99	0.16	-57 39 29.09	0.17	9.731	0.620	8.431	0.501	3.84	0.20	2.23	0.18	95.48	16.37	0.183	0.02	S
3755	23 21 40.29	0.43	-58 12 05.42	0.45	3.551	0.361	2.129	0.236	6.93	1.05	5.90	0.91	32.46	61.80	0.189	–	S
3756	23 23 00.34	1.18	-51 06 35.02	2.49	5.711	0.365	0.882	0.169	28.53	5.99	12.29	2.46	15.52	20.05	0.188	–	S
3757	23 21 50.32	0.51	-57 23 14.94	0.54	2.191	0.348	1.610	0.226	5.29	1.29	4.13	1.09	156.39	77.40	0.196	–	S
3758	23 21 36.63	1.41	-58 19 41.29	0.74	1.977	0.248	0.833	0.169	12.75	3.24	5.91	1.73	98.00	27.17	0.154	–	S
3759	23 22 01.79	0.78	-56 26 56.78	0.52	1.171	0.221	0.862	0.142	7.01	1.82	1.69	1.13	77.73	29.25	0.127	–	S
3760	23 23 08.24	0.59	-50 00 23.09	0.89	3.150	0.303	1.380	0.196	12.02	2.09	6.94	1.29	17.07	25.17	0.169	–	S
3761	23 21 48.69	0.61	-57 22 33.90	0.74	4.146	0.359	1.682	0.226	11.13	1.79	7.97	1.29	158.77	28.58	0.192	–	S
3762	23 22 55.97	0.62	-51 16 42.45	0.56	5.584	0.420	2.166	0.246	12.27	1.63	8.36	1.05	123.16	20.34	0.201	–	S
3763	23 22 37.70	0.71	-53 07 13.17	0.62	1.753	0.291	1.206	0.189	7.90	1.89	2.36	1.08	56.22	25.33	0.168	–	S
3764	23 21 30.59	0.41	-58 27 06.81	0.74	5.826	0.409	2.122	0.224	15.00	1.76	6.08	0.78	16.91	11.18	0.187	–	S
3765	23 22 51.32	0.64	-51 33 58.97	0.68	2.396	0.469	1.793	0.301	5.51	1.60	3.91	1.41	139.15	79.29	0.269	–	S
3766	23 21 39.45	0.28	-57 40 41.76	0.27	12.935	0.838	5.348	0.371	9.67	0.67	5.23	0.41	141.19	8.06	0.226	–	M
3767	23 22 02.56	0.28	-55 57 33.15	0.33	4.286	0.358	2.819	0.235	7.34	0.74	3.91	0.51	153.58	15.47	0.165	–	S
3768	23 21 27.72	0.35	-58 33 31.04	0.40	2.493	0.299	1.874	0.197	5.73	0.92	3.04	0.71	27.77	28.26	0.159	–	S
3769	23 22 31.07	0.53	-53 21 03.23	0.49	2.633	0.340	1.766	0.222	7.37	1.36	3.76	0.92	56.17	26.93	0.188	–	S
3770	23 21 40.87	0.86	-57 29 48.46	0.75	1.510	0.269	0.931	0.178	7.43	2.11	4.97	1.61	60.09	58.99	0.159	–	S
3771	23 22 26.35	0.89	-53 34 43.67	0.90	7.178	0.458	1.587	0.211	15.27	2.12	15.04	2.05	66.43	1.55	0.195	–	S
3772	23 22 54.53	0.78	-50 45 00.99	0.54	3.963	0.495	2.246	0.327	9.28	1.93	4.83	1.12	103.57	24.08	0.283	–	S
3773	23 22 25.25	0.81	-53 40 17.01	0.74	1.743	0.324	1.152	0.212	7.31	2.07	4.10	1.47	57.34	44.78	0.189	–	S
3774	23 21 33.16	0.45	-57 51 42.91	0.38	2.604	0.319	1.862	0.209	5.86	1.00	4.03	0.83	100.42	45.14	0.172	–	S
3775	23 21 02.21	0.56	-59 52 35.68	0.71	2.266	0.281	1.258	0.187	8.35	1.70	5.46	1.22	166.55	32.57	0.161	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3776	23 21 23.67	0.14	-58 24 31.64	0.15	39.800	2.205	38.985	2.150	1.32	0.03	0.91	0.03	30.89	113.49	0.152	-0.29	S
3777	23 22 53.47	0.56	-50 38 13.70	0.52	2.673	0.357	1.765	0.234	6.51	1.32	5.24	1.14	84.22	58.56	0.199	-	S
3778	23 22 11.02	0.38	-54 42 24.70	0.37	15.755	2.030	12.523	1.332	4.34	0.84	3.78	0.80	117.09	123.24	1.088	-	S
3779	23 21 19.81	0.23	-58 12 56.75	0.26	7.827	0.682	5.386	0.367	7.65	0.58	0.00	0.31	57.01	6.51	0.217	-	M
3780	23 21 54.94	0.46	-56 01 00.97	0.60	1.768	0.306	1.377	0.196	5.56	1.37	2.57	1.02	0.82	39.55	0.173	-	S
3781	23 22 06.80	0.14	-54 45 30.28	0.15	1309.645	72.261	743.418	40.925	10.84	0.05	1.95	0.02	31.78	0.31	1.738	-0.74	M
3782	23 22 48.12	0.23	-50 48 58.77	0.23	70.990	3.949	14.198	0.845	23.93	0.50	15.12	0.31	45.11	2.87	0.323	-	M
3783	23 22 12.06	0.44	-54 31 04.61	0.51	4.673	0.738	3.684	0.476	4.95	1.15	3.28	0.97	7.72	62.07	0.411	-	S
3784	23 22 29.17	0.99	-52 52 55.07	0.67	1.356	0.349	1.053	0.219	6.72	2.42	0.00	1.41	76.41	35.49	0.204	-	S
3785	23 21 47.33	0.51	-56 25 51.26	0.53	1.724	0.252	1.213	0.165	5.49	1.23	4.79	1.12	162.90	111.77	0.141	-	S
3786	23 21 21.99	0.59	-58 10 40.02	0.53	1.788	0.350	1.437	0.223	4.43	1.33	3.31	1.21	77.46	125.25	0.199	-	S
3787	23 21 52.47	0.60	-55 44 39.68	1.22	20.428	1.244	6.523	0.444	25.62	3.11	4.26	0.65	68.22	6.53	0.262	-	M
3788	23 21 45.32	1.31	-56 25 26.00	0.34	3.067	0.345	0.873	0.148	0.00	3.10	0.00	0.60	0.00	10.04	0.140	-	M
3789	23 21 45.19	0.14	-56 20 26.58	0.15	48.386	2.676	47.487	2.617	0.00	0.03	0.00	0.03	0.00	5.78	0.165	0.03	S
3790	23 22 41.70	0.70	-51 11 24.37	0.89	3.819	0.385	1.628	0.253	10.92	2.04	8.20	1.63	16.03	49.45	0.219	-	S
3791	23 22 43.19	0.35	-50 56 16.15	0.24	21.346	1.342	7.630	0.507	12.88	0.78	5.53	0.40	163.61	5.86	0.284	-	M
3792	23 22 26.60	1.07	-52 38 59.33	1.95	3.074	0.247	0.735	0.153	19.26	4.61	10.45	2.42	173.05	27.14	0.151	-	S
3793	23 21 52.46	0.60	-55 37 31.49	0.78	2.993	0.336	1.492	0.223	9.41	1.84	6.56	1.34	173.28	36.08	0.191	-	S
3794	23 22 10.91	0.24	-54 03 36.59	0.26	6.360	0.624	5.562	0.436	3.71	0.51	2.25	0.45	158.56	41.17	0.302	-	S
3795	23 21 16.69	0.40	-58 15 40.98	0.50	1.767	0.289	1.460	0.185	5.10	1.16	1.09	0.84	163.68	31.11	0.161	-	S
3796	23 21 15.57	0.69	-58 04 57.28	0.78	16.840	0.948	2.313	0.220	22.86	1.94	16.85	1.40	149.64	15.79	0.210	-	S
3797	23 21 21.02	1.07	-57 47 38.37	0.86	1.767	0.246	0.832	0.168	9.57	2.53	7.16	1.97	77.03	66.00	0.149	-	S
3798	23 22 06.79	0.16	-54 07 24.14	0.17	18.671	1.221	17.316	1.030	2.38	0.19	2.11	0.19	80.44	104.27	0.384	-0.74	S
3799	23 21 02.10	0.30	-58 52 35.83	0.29	4.472	0.384	3.062	0.255	6.19	0.64	4.39	0.54	48.56	28.29	0.179	-	S
3800	23 20 56.89	0.30	-59 12 21.96	0.32	2.482	0.283	2.046	0.189	4.69	0.71	2.21	0.58	35.74	29.25	0.146	-	S
3801	23 21 56.24	0.16	-54 53 54.69	0.17	28.123	1.836	25.119	1.503	3.14	0.21	2.36	0.19	39.74	35.91	0.578	-0.27	S
3802	23 22 42.86	0.75	-50 27 06.90	0.99	2.034	0.306	1.106	0.206	8.97	2.26	6.17	1.76	165.57	54.50	0.182	-	S
3803	23 21 51.18	0.18	-55 14 22.42	0.20	9.568	0.726	8.587	0.559	3.26	0.31	2.03	0.28	5.78	33.23	0.292	-	S
3804	23 21 42.47	0.76	-55 41 15.35	0.28	11.818	0.790	3.095	0.277	16.07	1.77	3.64	0.56	179.78	6.79	0.219	-	M
3805	23 22 22.93	0.60	-52 07 06.72	0.58	3.195	0.317	1.650	0.205	10.22	1.65	5.46	0.96	131.56	19.76	0.171	-	S
3806	23 20 52.65	0.15	-58 59 28.33	0.16	14.660	0.861	14.297	0.806	1.70	0.10	0.54	0.10	56.41	26.90	0.175	-0.30	S
3807	23 21 42.70	1.05	-55 34 37.06	1.49	2.699	0.283	0.910	0.192	14.37	3.72	8.22	2.11	158.54	30.45	0.178	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3808	23 21 44.72	1.27	-55 19 23.27	0.26	17.130	1.180	3.361	0.325	28.06	2.98	1.97	0.46	4.99	4.97	0.268	–	M
3809	23 22 11.73	0.15	-52 54 34.98	0.16	13.213	0.790	11.888	0.680	3.19	0.14	2.15	0.13	53.32	19.03	0.181	-0.16	S
3810	23 20 58.28	0.63	-58 32 37.54	0.59	1.804	0.270	1.183	0.177	7.15	1.59	4.06	1.15	133.51	35.59	0.154	–	S
3811	23 21 25.58	0.16	-56 37 29.07	0.17	11.051	0.676	8.958	0.526	4.18	0.19	3.45	0.17	26.11	24.90	0.175	-1.10	S
3812	23 22 21.01	0.64	-51 56 50.80	0.66	1.585	0.338	1.255	0.214	4.79	1.55	3.50	1.42	132.08	101.41	0.194	–	S
3813	23 22 21.19	0.43	-51 48 47.08	0.33	5.289	0.477	3.235	0.309	8.04	1.00	4.79	0.67	93.90	18.87	0.236	–	S
3814	23 20 57.01	1.06	-58 29 58.32	1.26	2.387	0.265	0.853	0.182	11.46	3.07	9.56	2.38	176.00	66.66	0.165	–	S
3815	23 21 31.35	0.35	-55 57 49.84	0.33	5.555	0.446	3.185	0.282	7.30	0.77	6.42	0.69	74.76	63.27	0.204	–	S
3816	23 22 25.40	0.14	-51 11 22.65	0.15	19.718	1.136	18.848	1.055	1.99	0.09	1.53	0.09	10.66	49.16	0.197	-0.36	S
3817	23 21 57.69	0.37	-53 41 05.29	0.39	3.350	0.435	2.662	0.285	4.67	0.87	3.50	0.79	36.67	72.82	0.234	–	S
3818	23 22 12.61	0.73	-52 14 52.05	0.79	5.319	0.467	1.752	0.194	14.86	2.42	0.00	0.57	134.37	7.85	0.169	–	M
3819	23 20 35.86	0.14	-59 31 52.60	0.15	77.570	4.312	52.751	2.911	8.40	0.07	3.17	0.04	176.00	0.73	0.240	-0.85	M
3820	23 21 26.85	0.75	-56 10 37.72	0.93	1.264	0.296	0.901	0.191	6.31	2.25	3.57	1.65	163.00	59.03	0.174	–	S
3821	23 21 35.00	0.56	-55 31 49.02	0.67	1.367	0.251	1.010	0.162	5.67	1.56	3.70	1.25	175.38	60.59	0.143	–	S
3822	23 22 01.63	0.61	-53 15 30.40	0.46	1.255	0.305	1.202	0.185	0.00	1.47	0.00	0.96	0.00	32.81	0.172	–	S
3823	23 21 11.21	0.16	-57 10 06.22	0.18	7.190	0.479	6.480	0.391	3.12	0.22	1.98	0.20	178.72	25.02	0.158	0.16	S
3824	23 22 31.11	0.24	-50 17 03.58	0.25	3.702	0.307	2.910	0.215	5.23	0.52	3.22	0.40	136.35	22.31	0.137	–	S
3825	23 21 56.70	0.60	-53 29 26.40	0.39	8.791	0.554	2.928	0.263	16.47	1.51	6.98	0.65	68.08	9.21	0.204	–	S
3826	23 21 15.50	0.46	-56 42 46.18	0.71	10.073	0.764	3.901	0.311	13.54	1.79	4.58	0.75	117.10	9.97	0.225	–	M
3827	23 22 09.56	0.88	-52 18 50.29	0.85	1.550	0.259	0.888	0.174	7.29	2.12	6.74	1.92	107.38	161.26	0.154	–	S
3828	23 21 30.13	2.23	-55 38 40.62	0.51	5.797	0.486	1.065	0.190	0.00	5.26	0.00	0.98	0.00	13.60	0.181	–	M
3829	23 21 20.80	0.40	-56 16 24.65	1.57	10.978	0.620	1.512	0.150	37.04	3.69	9.06	0.85	179.49	8.11	0.162	–	S
3830	23 20 39.02	1.81	-58 50 05.11	0.89	24.820	1.375	1.621	0.177	43.12	4.16	19.97	1.99	104.15	11.70	0.237	–	S
3831	23 21 29.31	0.60	-55 24 04.57	0.73	1.610	0.332	1.219	0.213	5.49	1.70	3.42	1.36	175.09	65.57	0.191	–	S
3832	23 21 54.89	0.96	-53 16 47.93	1.19	2.178	0.304	0.981	0.210	10.14	2.79	7.75	2.22	164.51	66.22	0.187	–	S
3833	23 22 08.94	0.98	-51 53 17.93	1.02	3.985	0.416	1.516	0.279	10.94	2.41	9.89	2.25	136.00	104.07	0.248	–	S
3834	23 22 04.58	0.29	-52 04 16.00	0.56	18.858	1.137	5.581	0.375	18.13	1.34	5.81	0.47	73.38	5.12	0.216	–	M
3835	23 21 41.82	0.61	-54 09 38.81	0.50	3.379	0.678	2.835	0.426	5.39	1.50	0.00	1.00	118.26	32.82	0.384	–	S
3836	23 21 26.20	0.29	-55 20 31.43	0.31	4.537	0.471	3.621	0.318	4.54	0.65	3.45	0.58	30.76	55.93	0.237	–	S
3837	23 20 49.43	1.97	-57 50 10.37	1.29	4.358	0.378	0.770	0.158	15.40	5.44	0.00	0.96	34.23	13.85	0.152	–	M
3838	23 21 37.74	0.89	-54 18 50.83	0.80	6.906	0.608	2.584	0.385	13.52	2.45	7.43	1.35	129.68	20.99	0.340	–	S
3839	23 20 49.03	0.52	-57 52 19.80	0.64	1.229	0.246	0.983	0.156	5.22	1.52	2.20	1.13	13.94	45.45	0.140	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3840	23 21 56.58	0.97	-52 41 52.01	0.91	1.035	0.240	0.705	0.156	7.19	2.56	3.64	1.74	129.21	49.33	0.142	–	S
3841	23 20 51.35	0.89	-57 42 12.92	0.73	1.518	0.260	0.940	0.171	8.78	2.32	3.18	1.31	127.05	27.61	0.154	–	S
3842	23 21 13.59	0.25	-56 05 34.64	0.27	7.905	0.564	4.831	0.358	7.06	0.55	5.59	0.46	152.96	23.78	0.223	–	S
3843	23 20 12.29	0.18	-59 59 21.62	0.17	9.051	0.672	7.225	0.440	0.00	0.25	0.00	0.19	0.00	8.16	0.189	–	M
3844	23 22 03.75	0.43	-51 53 08.55	0.46	3.815	0.467	2.671	0.307	5.68	1.00	5.00	0.97	147.47	110.12	0.252	–	S
3845	23 20 41.62	1.80	-58 11 01.30	0.83	3.668	0.301	1.003	0.187	19.61	4.22	7.36	1.69	77.16	19.09	0.183	–	S
3846	23 20 26.58	0.69	-59 07 22.81	1.21	3.989	0.321	1.244	0.195	15.73	2.90	7.87	1.46	14.55	19.05	0.180	–	S
3847	23 21 41.57	0.14	-53 38 56.52	0.15	50.270	2.807	48.540	2.685	0.00	0.05	0.00	0.05	0.00	8.00	0.280	-0.82	S
3848	23 22 02.91	0.32	-51 41 36.35	0.35	94.416	5.366	22.107	1.330	17.35	0.88	9.48	0.48	50.71	5.57	0.538	–	M
3849	23 20 11.95	0.27	-59 48 09.40	0.31	6.577	0.453	3.511	0.270	8.61	0.66	5.85	0.50	159.71	14.52	0.175	–	S
3850	23 21 09.28	0.70	-56 08 24.90	0.83	3.556	0.370	1.573	0.245	10.39	2.04	7.44	1.48	154.52	36.21	0.212	–	S
3851	23 22 13.46	0.27	-50 26 15.90	0.35	3.095	0.305	2.382	0.206	6.32	0.77	2.26	0.51	161.17	17.49	0.151	–	S
3852	23 20 35.27	0.21	-58 05 46.88	0.21	4.595	0.372	3.891	0.271	3.78	0.38	2.89	0.35	81.15	52.30	0.161	–	S
3853	23 20 25.29	0.18	-58 34 31.09	0.18	6.943	0.456	5.652	0.347	4.20	0.24	3.28	0.23	104.54	30.27	0.147	–	S
3854	23 20 52.65	1.00	-56 48 40.29	0.63	2.228	0.260	1.051	0.173	11.30	2.37	5.55	1.35	75.65	24.60	0.153	–	S
3855	23 21 54.87	0.22	-51 40 39.05	0.23	9.601	0.966	9.565	0.704	0.00	0.40	0.00	0.40	0.00	129.28	0.467	–	S
3856	23 21 56.39	0.17	-51 25 45.90	0.18	110.734	7.367	98.416	5.957	3.08	0.22	2.72	0.22	162.87	6.49	2.421	-1.11	S
3857	23 21 22.64	0.49	-54 21 58.35	0.55	4.868	0.518	2.775	0.339	7.77	1.27	6.18	1.07	23.89	53.51	0.280	–	S
3858	23 22 01.53	0.16	-50 55 52.80	0.18	13.061	0.859	9.843	0.586	0.00	0.22	0.00	0.16	0.00	7.31	0.225	-0.78	M
3859	23 21 55.79	0.16	-51 26 06.44	0.17	172.783	10.898	151.205	8.915	4.30	0.21	1.42	0.16	168.58	10.48	3.123	-0.90	S
3860	23 20 13.07	0.54	-59 02 14.47	0.51	1.703	0.301	1.335	0.193	4.83	1.30	3.34	1.08	52.69	79.11	0.170	–	S
3861	23 20 45.05	0.48	-57 01 04.02	0.83	2.124	0.246	1.128	0.162	10.25	1.95	4.41	1.06	9.81	20.07	0.140	–	S
3862	23 21 47.70	0.44	-52 07 02.76	0.54	3.813	0.352	2.027	0.226	9.18	1.29	6.12	0.91	156.30	25.86	0.182	–	S
3863	23 20 47.76	0.67	-56 48 14.26	0.81	1.606	0.251	0.955	0.167	7.51	1.93	5.49	1.50	174.80	56.05	0.147	–	S
3864	23 21 41.54	0.21	-52 32 41.59	0.21	9.048	0.598	6.066	0.398	6.02	0.38	5.36	0.34	78.75	34.66	0.203	–	S
3865	23 20 08.82	0.51	-59 04 40.96	0.48	2.897	0.351	1.833	0.231	6.26	1.12	5.66	1.11	59.75	92.02	0.193	–	S
3866	23 21 45.13	0.27	-52 00 02.89	0.25	28.156	1.612	7.739	0.484	15.93	0.60	10.17	0.39	32.75	5.57	0.230	–	M
3867	23 21 37.92	0.30	-52 43 15.84	0.34	3.395	0.380	2.767	0.254	4.61	0.71	3.05	0.61	164.36	45.26	0.195	–	S
3868	23 20 30.78	0.62	-57 38 31.79	0.61	1.097	0.253	0.925	0.158	4.49	1.57	1.90	1.23	136.85	62.63	0.145	–	S
3869	23 21 54.21	0.21	-51 07 05.25	0.22	4.667	0.445	4.706	0.333	0.00	0.39	0.00	0.34	0.00	33.75	0.210	–	S
3870	23 21 07.19	0.44	-54 52 18.35	0.47	3.677	0.847	3.727	0.515	0.00	1.06	0.00	0.96	0.00	105.99	0.474	–	S
3871	23 20 06.53	0.64	-58 59 05.62	0.55	4.676	0.353	1.751	0.207	11.62	1.50	8.69	1.19	63.04	31.95	0.171	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3872	23 20 02.52	0.60	-59 13 03.65	1.02	3.971	0.313	1.389	0.187	15.93	2.54	5.89	1.04	24.00	14.05	0.169	–	S
3873	23 21 34.05	0.17	-52 47 31.65	0.18	8.612	0.591	7.887	0.482	3.08	0.24	1.72	0.21	26.97	27.47	0.206	–	S
3874	23 21 38.52	0.67	-52 24 31.56	0.96	1.553	0.250	0.917	0.166	8.97	2.30	4.51	1.45	20.43	34.09	0.148	–	S
3875	23 21 01.11	0.15	-55 22 00.32	0.16	13.758	0.824	13.037	0.742	2.07	0.12	1.68	0.12	63.28	61.60	0.189	0.21	S
3876	23 19 53.77	0.60	-59 38 39.05	0.72	1.978	0.263	1.147	0.174	8.77	1.82	4.33	1.15	31.68	26.11	0.151	–	S
3877	23 22 02.19	0.79	-50 05 19.86	0.87	1.481	0.250	0.887	0.167	7.20	2.04	6.34	1.80	150.78	165.89	0.147	–	S
3878	23 20 43.82	0.90	-56 31 37.08	0.79	1.471	0.229	0.809	0.154	7.92	2.14	6.42	1.79	110.44	87.89	0.136	–	S
3879	23 20 22.08	0.19	-57 49 31.27	0.19	8.370	0.566	6.554	0.415	5.34	0.31	2.73	0.25	48.98	12.52	0.196	–	S
3880	23 21 31.69	0.81	-52 46 56.15	0.66	1.578	0.338	1.169	0.216	6.41	2.00	2.80	1.39	69.12	43.96	0.196	–	S
3881	23 20 45.38	0.73	-56 05 21.70	0.91	16.152	0.965	3.109	0.362	18.92	2.20	13.88	1.58	23.53	22.26	0.337	–	S
3882	23 20 44.90	0.64	-56 16 24.15	0.77	1.260	0.244	0.883	0.158	6.18	1.83	4.07	1.43	166.88	60.49	0.141	–	S
3883	23 21 32.42	0.52	-52 34 00.20	0.51	3.682	0.348	1.938	0.225	8.77	1.31	6.61	1.00	130.37	33.29	0.182	–	S
3884	23 21 46.97	0.71	-51 10 58.74	0.86	1.812	0.332	1.189	0.217	7.77	2.14	3.99	1.45	34.05	41.01	0.194	–	S
3885	23 20 04.90	1.24	-58 36 51.92	1.40	3.265	0.249	0.758	0.149	15.62	3.46	12.94	2.70	23.30	55.70	0.144	–	S
3886	23 19 46.88	0.28	-59 30 15.38	0.29	3.428	0.307	2.490	0.207	5.12	0.60	4.44	0.54	22.56	57.67	0.146	–	S
3887	23 20 22.84	1.09	-57 23 26.86	0.93	1.310	0.243	0.738	0.163	8.89	2.81	4.90	1.81	127.22	42.55	0.147	–	S
3888	23 21 31.91	0.80	-52 11 13.57	0.97	2.617	0.289	1.129	0.194	10.98	2.38	7.78	1.71	153.51	40.96	0.170	–	S
3889	23 21 35.61	0.41	-51 47 13.12	0.44	3.008	0.399	2.311	0.260	6.10	1.11	2.38	0.76	141.04	25.71	0.217	–	S
3890	23 20 44.71	0.36	-55 43 49.39	0.36	2.574	0.309	1.991	0.204	4.41	0.78	4.20	0.78	46.23	1.90	0.163	–	S
3891	23 21 14.21	0.37	-53 29 36.06	0.33	4.813	0.529	3.643	0.351	5.69	0.84	3.29	0.65	73.73	29.16	0.274	–	S
3892	23 20 30.51	0.68	-56 40 46.15	0.57	1.448	0.252	1.025	0.163	6.37	1.63	3.65	1.22	118.82	45.14	0.144	–	S
3893	23 20 08.59	0.27	-58 01 13.00	0.31	5.062	0.391	3.099	0.251	7.11	0.66	5.33	0.54	169.52	22.78	0.171	–	S
3894	23 21 51.86	1.26	-50 03 57.24	0.96	2.323	0.269	0.913	0.183	12.08	3.17	8.43	2.05	105.65	38.18	0.165	–	S
3895	23 20 05.47	0.86	-58 05 34.43	1.00	5.143	0.485	1.726	0.207	13.33	3.01	0.00	0.65	132.22	9.62	0.184	–	M
3896	23 21 15.36	0.25	-53 13 54.93	0.24	7.344	0.504	4.499	0.320	7.07	0.51	5.78	0.43	72.97	25.58	0.187	–	S
3897	23 21 08.84	1.64	-53 44 09.04	1.13	7.308	0.491	1.407	0.252	20.29	4.00	13.19	2.46	76.74	27.79	0.255	–	S
3898	23 21 29.31	0.39	-51 53 25.31	1.02	10.582	0.752	2.738	0.270	15.41	2.38	4.04	0.81	97.81	10.06	0.224	–	M
3899	23 21 08.53	0.17	-53 39 04.60	0.18	8.675	0.623	8.117	0.505	2.63	0.25	1.49	0.23	43.86	38.83	0.233	–	S
3900	23 19 41.18	0.58	-59 23 20.92	0.54	1.413	0.281	1.145	0.178	4.39	1.36	3.12	1.17	56.51	107.00	0.159	–	S
3901	23 20 18.73	1.29	-57 03 19.40	1.18	2.357	0.258	0.830	0.177	13.25	3.45	8.34	2.17	132.24	35.98	0.162	–	S
3902	23 21 00.21	0.14	-54 02 33.88	0.15	373.545	20.753	359.127	19.788	4.07	0.03	0.00	0.02	140.65	0.81	1.194	-0.40	M
3903	23 21 30.33	1.05	-51 37 41.71	0.95	2.022	0.420	1.311	0.272	9.54	3.08	0.00	1.34	130.58	25.00	0.253	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3904	23 21 04.64	0.41	-53 43 00.49	0.50	9.340	0.624	3.635	0.332	13.19	1.27	7.18	0.70	148.80	12.14	0.251	–	S
3905	23 19 45.27	0.48	-58 53 00.24	0.55	22.903	1.358	5.202	0.379	18.12	1.51	7.52	0.64	52.89	6.79	0.248	–	M
3906	23 19 41.78	1.23	-59 08 24.92	0.91	1.805	0.264	0.844	0.181	10.98	3.04	5.83	1.86	63.95	35.61	0.163	–	S
3907	23 20 15.52	0.37	-57 04 05.79	0.44	1.883	0.290	1.604	0.187	4.49	0.99	1.49	0.78	164.60	36.99	0.159	–	S
3908	23 21 24.20	0.75	-51 55 52.69	0.60	2.048	0.358	1.418	0.233	7.20	1.89	3.26	1.22	114.93	33.30	0.207	–	S
3909	23 19 55.90	0.47	-58 11 00.37	0.46	3.516	0.340	1.968	0.220	7.79	1.13	6.12	0.93	137.69	39.94	0.177	–	S
3910	23 20 32.75	0.58	-55 51 03.00	0.73	1.934	0.376	1.425	0.242	5.89	1.70	3.45	1.30	178.01	53.59	0.216	–	S
3911	23 21 38.98	0.30	-50 24 40.53	0.32	5.359	0.475	3.696	0.316	6.08	0.69	4.99	0.61	47.16	51.00	0.226	–	S
3912	23 20 43.09	0.14	-54 57 41.47	0.15	86.524	4.813	79.629	4.400	2.85	0.05	1.76	0.04	20.34	8.11	0.417	-0.84	S
3913	23 20 24.53	0.20	-56 12 20.39	0.19	12.654	0.795	8.277	0.520	6.68	0.33	4.85	0.27	79.39	14.80	0.235	–	S
3914	23 19 36.87	1.05	-59 05 54.51	0.71	1.976	0.280	1.033	0.188	10.62	2.56	4.26	1.37	118.96	24.99	0.168	–	S
3915	23 21 07.89	0.14	-52 56 09.21	0.15	233.664	12.940	228.206	12.582	1.52	0.03	0.94	0.03	29.37	17.71	0.874	-0.62	S
3916	23 21 20.10	1.53	-51 43 05.89	0.45	22.668	1.439	2.690	0.348	27.96	3.58	7.50	0.99	1.42	8.64	0.316	–	M
3917	23 20 10.66	0.73	-56 55 39.92	0.69	1.006	0.264	0.839	0.165	3.81	1.65	3.25	1.62	91.37	2.01	0.152	–	S
3918	23 20 39.44	2.17	-54 53 11.95	1.18	14.485	0.950	2.470	0.465	25.68	5.35	11.47	2.28	73.59	20.16	0.502	–	S
3919	23 19 42.29	1.40	-58 33 17.01	2.03	4.371	0.278	0.634	0.127	22.52	4.86	15.90	3.23	4.57	32.99	0.140	–	S
3920	23 19 47.18	1.58	-58 13 59.33	1.55	4.555	0.319	0.890	0.174	21.37	4.56	11.45	2.43	46.42	24.68	0.179	–	S
3921	23 20 12.29	0.42	-56 41 46.90	0.63	2.641	0.270	1.454	0.175	9.36	1.45	4.82	0.90	11.12	20.01	0.145	–	S
3922	23 21 36.21	0.36	-50 07 39.03	0.38	2.230	0.292	1.852	0.192	4.27	0.83	3.13	0.77	137.01	69.03	0.156	–	S
3923	23 21 27.56	1.09	-50 52 38.50	1.19	4.382	0.417	1.464	0.275	14.18	3.18	9.26	2.05	44.43	34.86	0.250	–	S
3924	23 20 45.66	0.74	-54 20 20.09	0.79	1.923	0.496	1.536	0.312	4.68	1.86	3.30	1.66	150.49	119.04	0.287	–	S
3925	23 20 03.14	0.29	-57 02 12.69	0.33	3.967	0.368	2.802	0.245	5.77	0.70	4.35	0.59	168.61	34.40	0.179	–	S
3926	23 20 33.42	0.58	-54 53 26.33	1.20	36.537	2.221	7.011	0.627	21.11	2.93	7.47	1.05	74.31	10.19	0.494	–	M
3927	23 20 56.84	1.30	-53 16 03.40	0.42	5.973	0.525	1.489	0.214	0.00	3.06	0.00	0.88	0.00	12.26	0.198	–	M
3928	23 21 30.80	0.63	-50 18 44.57	0.67	2.074	0.341	1.405	0.223	6.28	1.55	5.09	1.44	136.58	87.58	0.196	–	S
3929	23 20 08.91	0.16	-56 34 53.42	0.17	7.391	0.486	7.084	0.420	2.20	0.18	0.76	0.17	160.47	29.18	0.154	-0.41	S
3930	23 19 09.19	0.15	-59 56 48.19	0.16	13.147	0.786	12.197	0.695	2.73	0.12	1.35	0.12	5.43	15.43	0.179	-0.16	S
3931	23 21 18.85	0.15	-51 17 15.11	0.16	22.549	1.320	20.767	1.173	3.09	0.12	1.51	0.10	46.68	12.86	0.263	-0.69	S
3932	23 19 26.59	0.47	-59 01 49.73	0.55	2.316	0.303	1.525	0.199	6.59	1.29	4.55	1.01	168.32	39.70	0.169	–	S
3933	23 20 01.52	0.15	-56 52 22.84	0.16	11.079	0.667	10.683	0.609	1.67	0.12	1.37	0.12	64.06	97.95	0.157	-0.54	S
3934	23 19 57.46	1.74	-57 05 12.27	1.13	3.860	0.298	0.926	0.178	19.88	4.38	9.27	2.02	118.84	21.86	0.177	–	S
3935	23 21 14.30	0.90	-51 30 11.50	0.75	1.810	0.372	1.222	0.243	6.77	2.16	4.45	1.68	80.64	60.95	0.219	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
3936	23 19 12.14	0.14	-59 37 00.19	0.15	28.334	1.577	28.433	1.570	0.00	0.04	0.00	0.04	0.00	33.67	0.139	-0.56	S
3937	23 21 03.77	0.73	-52 15 12.77	0.82	1.994	0.298	1.141	0.199	7.82	1.87	6.28	1.70	28.74	91.97	0.174	-	S
3938	23 19 49.23	0.19	-57 24 23.78	0.21	5.699	0.427	4.733	0.315	4.38	0.35	2.52	0.30	172.57	19.56	0.171	-	S
3939	23 19 54.31	0.76	-57 04 57.02	0.59	3.351	0.329	1.536	0.213	10.78	1.85	6.44	1.20	118.71	24.85	0.182	-	S
3940	23 19 32.85	0.31	-58 21 10.10	0.38	3.108	0.316	2.192	0.209	6.40	0.84	3.51	0.63	20.43	22.54	0.161	-	S
3941	23 19 46.59	0.15	-57 27 34.89	0.15	13.799	0.804	13.630	0.765	1.23	0.09	0.16	0.09	124.39	40.53	0.153	-0.04	S
3942	23 20 47.95	0.14	-53 09 44.86	0.15	48.026	2.658	46.473	2.562	1.59	0.03	1.36	0.03	15.48	39.63	0.172	0.38	S
3943	23 19 12.16	0.97	-59 16 20.98	1.21	4.523	0.315	1.045	0.170	16.49	2.97	12.13	2.08	161.37	30.44	0.162	-	S
3944	23 19 18.65	1.25	-58 56 40.47	0.86	2.249	0.337	1.072	0.231	10.57	2.97	5.90	1.87	112.54	37.92	0.208	-	S
3945	23 19 10.66	1.78	-59 16 07.64	1.54	5.292	0.333	0.812	0.148	25.40	4.87	12.81	2.48	51.75	21.75	0.162	-	S
3946	23 20 30.41	0.50	-54 18 43.06	0.57	2.169	0.447	1.867	0.280	4.41	1.36	1.52	1.07	154.12	54.01	0.252	-	S
3947	23 20 56.64	0.59	-52 13 22.66	0.90	2.017	0.292	1.175	0.193	9.27	2.15	4.40	1.27	164.89	28.25	0.170	-	S
3948	23 19 18.35	0.26	-58 41 59.97	0.29	3.346	0.308	2.543	0.209	5.58	0.62	2.97	0.49	23.95	20.93	0.148	-	S
3949	23 20 21.96	0.27	-54 44 47.47	0.34	9.088	1.017	7.575	0.683	4.87	0.72	1.81	0.55	176.72	25.41	0.522	-	S
3950	23 19 09.93	0.57	-59 06 19.95	0.50	2.205	0.305	1.458	0.200	6.30	1.32	4.91	1.11	85.46	81.30	0.171	-	S
3951	23 21 09.72	0.60	-50 54 10.37	0.43	41.957	2.466	6.975	0.523	18.67	1.38	12.49	0.96	3.43	12.58	0.356	-	M
3952	23 19 36.08	0.47	-57 35 41.26	0.49	2.195	0.264	1.419	0.173	6.50	1.17	5.14	0.98	34.70	58.69	0.144	-	S
3953	23 19 21.66	1.54	-58 16 02.74	1.06	15.445	0.858	1.201	0.131	39.00	3.89	18.34	1.82	122.11	11.92	0.165	-	S
3954	23 20 20.29	0.32	-54 43 25.10	0.34	19.556	1.296	9.243	0.724	11.11	0.86	5.80	0.49	138.64	10.30	0.482	-	S
3955	23 19 24.53	1.51	-58 07 47.19	1.23	22.241	1.282	2.266	0.282	27.86	4.29	10.74	1.53	145.05	11.59	0.253	-	M
3956	23 20 59.41	1.00	-51 45 24.37	0.93	2.762	0.384	1.324	0.262	8.91	2.33	8.10	2.16	90.06	117.35	0.232	-	S
3957	23 20 55.14	0.24	-52 02 53.50	0.24	5.113	0.420	4.032	0.295	4.73	0.48	3.64	0.41	111.05	34.28	0.185	-	S
3958	23 18 53.84	0.62	-59 45 29.39	0.59	1.354	0.267	1.041	0.171	4.88	1.49	3.62	1.26	46.66	102.63	0.153	-	S
3959	23 19 35.85	0.81	-57 28 36.33	0.85	1.197	0.260	0.824	0.169	6.72	2.23	3.67	1.58	144.04	50.99	0.153	-	S
3960	23 19 12.17	0.55	-58 46 45.66	0.46	2.117	0.302	1.499	0.197	6.49	1.28	3.44	0.96	64.23	34.70	0.168	-	S
3961	23 19 55.77	0.45	-56 12 11.22	0.62	2.860	0.384	1.881	0.251	7.34	1.44	3.90	0.99	179.72	28.96	0.215	-	S
3962	23 20 32.50	0.14	-53 37 19.81	0.15	24.680	1.407	23.412	1.306	2.07	0.08	1.67	0.08	164.37	37.40	0.215	-0.04	S
3963	23 19 20.84	1.64	-58 06 59.57	1.72	23.673	1.312	1.320	0.172	34.50	4.27	30.29	3.60	151.49	38.29	0.253	-	S
3964	23 20 05.73	0.36	-55 26 00.60	0.35	2.364	0.329	2.063	0.215	4.30	0.85	0.94	0.67	130.41	33.06	0.177	-	S
3965	23 20 59.68	0.20	-51 17 47.87	0.21	12.322	0.785	8.168	0.519	7.39	0.38	4.20	0.27	46.87	10.00	0.243	-	S
3966	23 19 14.37	0.58	-58 28 28.72	0.60	1.012	0.230	0.863	0.143	3.86	1.44	2.52	1.23	154.62	103.97	0.131	-	S
3967	23 19 54.33	1.48	-55 56 43.42	0.42	155.310	8.594	8.929	0.774	53.13	3.50	12.84	0.78	10.37	4.54	0.598	-	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
3968	23 20 45.84	0.47	-52 21 28.07	0.43	3.182	0.301	1.807	0.195	7.77	1.11	6.38	0.91	110.81	41.50	0.154	–	S
3969	23 19 35.86	0.57	-57 08 45.21	0.76	1.882	0.329	1.284	0.214	6.79	1.79	3.77	1.27	178.76	40.92	0.190	–	S
3970	23 18 57.23	0.61	-59 11 46.33	0.66	6.141	0.411	1.881	0.211	14.79	1.74	9.01	1.09	38.76	17.14	0.178	–	S
3971	23 19 34.44	0.68	-57 11 34.36	0.77	0.973	0.288	0.859	0.177	3.71	1.81	1.73	1.53	0.18	107.22	0.166	–	S
3972	23 19 00.09	0.26	-59 00 54.34	0.25	3.828	0.366	3.168	0.253	3.81	0.50	3.33	0.49	90.03	73.23	0.176	–	S
3973	23 21 04.29	0.16	-50 27 15.41	0.17	48.975	2.784	39.778	2.207	16.79	0.24	0.00	0.06	49.19	0.77	0.292	0.03	M
3974	23 19 55.94	0.51	-55 41 10.28	0.46	2.068	0.326	1.597	0.211	5.11	1.19	3.46	0.99	110.64	60.87	0.182	–	S
3975	23 20 34.17	0.58	-52 56 48.69	0.52	2.696	0.421	1.936	0.274	6.14	1.41	3.91	1.10	67.91	48.04	0.238	–	S
3976	23 20 26.39	0.34	-53 26 04.16	0.29	10.171	0.746	5.708	0.462	8.28	0.74	5.97	0.56	86.04	19.76	0.313	–	S
3977	23 20 42.82	1.35	-52 12 36.59	1.86	4.577	0.330	0.979	0.186	23.22	5.05	9.71	2.03	35.05	20.04	0.190	–	S
3978	23 20 46.74	0.17	-51 52 04.73	0.18	7.899	0.561	7.898	0.480	0.00	0.23	0.00	0.20	0.00	26.60	0.204	–	S
3979	23 20 26.21	0.19	-53 21 31.32	0.28	24.386	1.441	8.421	0.536	12.61	0.55	6.29	0.30	82.42	4.43	0.269	–	M
3980	23 20 23.94	0.77	-53 32 42.63	0.73	2.966	0.532	1.956	0.348	7.52	2.04	3.92	1.39	53.83	40.06	0.311	–	S
3981	23 20 40.74	0.24	-52 11 47.55	0.21	7.036	0.500	5.036	0.343	6.50	0.46	3.48	0.32	90.66	12.32	0.191	–	S
3982	23 19 56.19	0.17	-55 22 55.78	0.19	5.992	0.455	5.701	0.364	0.00	0.28	0.00	0.25	0.00	20.92	0.182	–	S
3983	23 20 23.75	1.60	-53 26 33.21	0.78	5.218	0.515	1.759	0.342	15.86	3.86	7.24	1.75	87.64	22.89	0.321	–	S
3984	23 20 39.41	0.17	-52 12 18.86	0.18	10.330	0.647	8.100	0.486	4.40	0.23	4.13	0.21	95.22	47.35	0.184	-0.05	S
3985	23 20 27.12	0.73	-53 12 18.69	1.06	1.601	0.296	0.966	0.197	8.30	2.47	4.76	1.70	0.32	46.20	0.177	–	S
3986	23 20 07.19	0.35	-54 34 10.51	0.64	7.498	0.637	3.807	0.397	11.88	1.51	3.69	0.66	167.22	11.80	0.322	–	S
3987	23 19 35.73	0.61	-56 32 46.66	0.96	2.064	0.231	0.988	0.152	11.83	2.39	4.61	1.14	159.82	19.06	0.135	–	S
3988	23 19 49.07	0.78	-55 35 10.03	0.72	0.913	0.283	0.817	0.172	3.91	1.91	0.54	1.54	125.09	83.62	0.162	–	S
3989	23 19 29.32	0.90	-56 46 32.23	1.09	3.538	0.279	1.025	0.169	14.04	2.66	10.80	1.96	161.41	37.94	0.154	–	S
3990	23 18 31.01	0.15	-59 50 55.70	0.15	15.552	0.896	14.407	0.808	2.42	0.09	1.96	0.09	54.81	36.30	0.156	-0.31	S
3991	23 18 47.50	0.83	-58 52 15.55	0.65	2.856	0.353	1.447	0.236	8.95	1.91	6.55	1.50	82.87	54.57	0.205	–	S
3992	23 19 39.02	0.76	-55 50 13.82	2.72	6.029	0.587	1.214	0.250	0.00	6.59	0.00	0.85	0.00	13.14	0.240	–	M
3993	23 20 34.56	0.48	-52 01 05.81	0.56	1.235	0.289	1.173	0.177	0.00	1.24	0.00	1.12	0.00	89.50	0.163	–	S
3994	23 19 16.86	1.21	-57 07 17.63	1.98	22.219	1.286	2.555	0.282	24.15	4.76	13.61	2.62	107.87	21.82	0.244	–	M
3995	23 19 15.40	0.15	-57 16 25.36	0.17	14.096	0.852	12.243	0.706	4.35	0.17	0.79	0.13	1.23	7.94	0.207	-0.81	S
3996	23 20 28.13	0.14	-52 16 27.91	0.15	19.064	1.085	18.083	1.008	2.43	0.08	1.08	0.07	105.22	12.37	0.163	-0.79	S
3997	23 19 09.49	0.85	-57 27 54.13	1.07	1.426	0.244	0.780	0.165	9.04	2.68	5.22	1.76	26.41	41.88	0.148	–	S
3998	23 20 31.98	0.53	-51 48 26.86	0.52	2.673	0.353	1.783	0.232	6.24	1.24	5.26	1.12	120.81	74.28	0.196	–	S
3999	23 20 16.89	0.33	-52 55 44.21	0.33	4.033	0.374	2.767	0.247	5.83	0.72	5.11	0.66	125.52	61.54	0.182	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4000	23 20 49.86	0.50	-50 15 28.76	0.54	2.589	0.275	1.483	0.180	7.29	1.24	6.98	1.12	141.45	1.88	0.148	–	S
4001	23 19 11.60	0.40	-57 07 47.39	0.34	7.275	0.545	3.664	0.330	8.88	0.87	6.84	0.72	91.08	29.08	0.240	–	S
4002	23 19 24.54	0.56	-56 22 40.77	1.01	1.936	0.273	1.094	0.180	10.75	2.46	2.53	1.09	19.44	19.42	0.162	–	S
4003	23 18 45.54	0.81	-58 32 30.89	0.73	0.995	0.232	0.746	0.148	6.18	2.07	2.54	1.44	53.85	48.26	0.135	–	S
4004	23 19 08.97	0.22	-57 14 13.98	0.23	4.870	0.506	4.841	0.364	0.00	0.43	0.00	0.38	0.00	42.85	0.248	–	S
4005	23 20 36.56	1.36	-51 11 46.34	1.04	4.152	0.399	1.364	0.264	14.86	3.54	8.83	1.99	67.22	29.15	0.243	–	S
4006	23 19 22.27	0.51	-56 23 08.69	0.83	1.597	0.275	1.104	0.177	8.21	2.00	0.67	1.04	18.00	22.65	0.160	–	S
4007	23 19 39.60	0.66	-55 08 07.56	0.70	1.786	0.317	1.225	0.207	6.63	1.77	4.10	1.35	39.09	52.22	0.183	–	S
4008	23 20 35.22	0.18	-51 12 20.46	0.17	42.351	2.421	18.256	1.034	11.68	0.29	4.03	0.14	153.88	2.16	0.246	-0.80	M
4009	23 19 36.98	1.46	-55 18 33.80	0.93	11.054	0.641	1.451	0.196	25.36	3.44	16.43	2.16	94.30	20.37	0.213	–	S
4010	23 18 16.34	1.25	-59 46 09.10	0.91	1.324	0.212	0.648	0.146	10.12	2.99	5.90	1.98	69.37	44.67	0.131	–	S
4011	23 20 16.55	0.94	-52 32 47.27	1.03	1.608	0.268	0.855	0.182	8.05	2.43	7.20	2.17	162.74	1.99	0.162	–	S
4012	23 18 41.75	0.40	-58 26 19.01	0.39	1.266	0.224	1.181	0.142	2.79	0.93	1.06	0.80	139.99	87.72	0.124	–	S
4013	23 20 10.75	0.23	-52 52 12.87	0.24	5.344	0.483	4.661	0.345	3.20	0.44	3.00	0.42	118.30	167.27	0.224	–	S
4014	23 19 36.45	0.25	-55 10 10.86	0.31	5.525	0.431	3.604	0.282	7.21	0.64	4.35	0.47	11.64	17.01	0.188	–	S
4015	23 20 33.74	0.16	-51 01 29.75	0.17	13.705	0.887	12.806	0.757	2.36	0.19	2.00	0.18	37.11	16.29	0.272	-1.03	S
4016	23 19 44.07	0.53	-54 40 51.49	0.67	3.025	0.486	2.098	0.317	6.56	1.56	3.97	1.17	172.49	44.14	0.277	–	S
4017	23 18 58.57	0.62	-57 25 34.67	0.67	1.674	0.322	1.226	0.208	5.25	1.59	4.23	1.38	172.99	105.58	0.185	–	S
4018	23 18 59.74	0.15	-57 13 54.47	0.23	35.714	2.097	16.053	0.917	17.62	0.41	2.16	0.11	100.31	1.27	0.247	-0.52	M
4019	23 19 04.20	1.12	-57 02 02.91	0.74	1.568	0.272	0.880	0.183	9.02	2.62	4.92	1.70	99.61	40.59	0.164	–	S
4020	23 19 00.21	0.15	-57 05 55.45	0.17	12.807	0.798	11.567	0.674	3.23	0.17	1.76	0.15	19.99	17.18	0.219	-0.04	S
4021	23 19 33.92	0.28	-55 01 58.34	0.30	4.792	0.517	4.034	0.350	4.40	0.64	2.34	0.53	41.18	34.41	0.262	–	S
4022	23 20 09.15	0.37	-52 34 22.74	0.35	6.029	0.464	3.285	0.288	9.43	0.94	5.39	0.60	54.89	15.36	0.208	–	S
4023	23 20 11.05	0.16	-52 24 42.87	0.17	8.746	0.562	7.823	0.464	3.54	0.21	1.91	0.18	29.63	18.56	0.170	-0.78	S
4024	23 20 19.25	1.58	-51 47 47.23	0.90	3.488	0.332	1.109	0.220	15.61	3.87	8.57	1.97	97.37	26.26	0.206	–	S
4025	23 19 51.27	0.39	-53 50 39.94	0.44	4.485	0.779	4.076	0.494	3.19	0.95	1.75	0.88	171.39	93.70	0.431	–	S
4026	23 18 42.38	0.87	-57 53 19.83	0.56	6.910	0.525	1.756	0.196	13.17	2.23	3.81	0.87	155.19	11.55	0.170	–	M
4027	23 20 08.53	0.21	-52 30 01.79	0.21	4.981	0.372	4.005	0.270	4.46	0.38	3.49	0.33	99.55	32.18	0.149	–	S
4028	23 19 31.18	0.16	-54 56 14.34	0.18	24.797	1.479	17.310	1.020	7.23	0.25	2.94	0.16	21.93	6.36	0.347	-1.19	S
4029	23 20 11.99	0.63	-52 03 58.28	0.56	1.393	0.269	1.093	0.172	5.09	1.48	3.27	1.24	99.03	65.99	0.153	–	S
4030	23 18 01.11	1.10	-59 47 40.90	1.27	2.000	0.220	0.752	0.148	14.58	3.57	5.88	1.62	39.03	22.77	0.138	–	S
4031	23 20 01.04	0.54	-52 50 18.50	0.70	11.660	0.726	3.089	0.324	15.43	1.62	11.73	1.22	2.12	24.92	0.270	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4032	23 20 23.73	0.43	-51 07 15.66	0.48	3.060	0.382	2.149	0.251	5.79	1.02	4.91	1.00	169.15	112.61	0.207	–	S
4033	23 17 57.01	0.26	-59 54 17.34	0.23	8.224	0.604	4.694	0.314	9.29	0.62	0.00	0.25	39.52	4.26	0.179	–	M
4034	23 19 01.31	0.71	-56 34 00.56	0.46	5.372	0.472	1.674	0.193	10.49	1.72	4.36	0.90	162.65	14.86	0.170	–	M
4035	23 18 18.59	0.17	-58 47 10.80	0.19	8.558	0.610	7.694	0.482	3.40	0.26	1.46	0.23	166.44	19.57	0.226	–	S
4036	23 20 20.28	0.24	-51 00 24.19	0.35	22.454	1.381	9.641	0.599	14.36	0.82	5.57	0.35	117.35	4.46	0.278	–	M
4037	23 18 58.56	1.30	-56 33 30.28	1.60	6.126	0.380	0.980	0.162	24.09	4.29	13.27	2.23	148.72	20.54	0.173	–	S
4038	23 19 06.59	0.61	-55 58 58.59	1.48	33.443	1.979	5.349	0.431	29.68	3.56	9.94	1.14	106.50	8.68	0.315	–	M
4039	23 18 12.61	0.71	-58 55 01.45	0.77	3.294	0.460	1.818	0.308	8.18	1.94	5.90	1.47	31.37	50.26	0.269	–	S
4040	23 19 15.69	0.68	-55 26 25.86	1.05	3.418	0.287	1.173	0.178	13.93	2.50	8.32	1.48	169.26	23.50	0.159	–	S
4041	23 18 48.98	1.05	-56 55 10.66	1.16	5.652	0.460	1.583	0.285	13.72	2.87	11.66	2.30	156.54	58.57	0.264	–	S
4042	23 18 48.06	1.26	-56 54 41.99	1.10	7.238	0.497	1.547	0.263	16.25	2.97	14.14	2.55	95.87	78.23	0.255	–	S
4043	23 18 09.77	2.16	-58 52 55.57	0.55	18.120	1.188	2.754	0.305	27.12	5.09	6.70	1.22	5.60	10.83	0.265	–	M
4044	23 19 18.29	0.46	-54 51 44.42	1.65	52.691	2.989	13.634	0.850	30.06	3.91	6.41	0.85	101.06	7.54	0.399	–	M
4045	23 17 53.90	0.26	-59 31 40.23	0.20	20.230	1.177	6.699	0.419	12.28	0.53	6.83	0.30	14.72	4.44	0.199	–	M
4046	23 18 49.22	0.15	-56 42 22.61	0.16	10.965	0.676	9.854	0.572	2.89	0.16	2.40	0.15	153.56	38.32	0.179	0.18	S
4047	23 17 52.70	0.49	-59 35 34.04	0.44	1.352	0.244	1.155	0.155	3.85	1.10	2.57	0.96	74.42	103.84	0.136	–	S
4048	23 20 05.30	0.25	-51 41 26.96	0.29	5.942	0.482	4.167	0.324	6.07	0.59	4.57	0.49	157.66	31.17	0.214	–	S
4049	23 17 42.11	1.07	-59 59 47.82	0.65	2.883	0.314	1.228	0.209	11.76	2.42	6.53	1.53	94.50	29.19	0.185	–	S
4050	23 18 24.08	0.17	-57 57 37.45	0.18	6.933	0.466	6.201	0.377	2.98	0.22	2.38	0.21	139.85	44.24	0.157	–	S
4051	23 19 36.62	0.14	-53 40 31.47	0.15	39.483	2.247	38.647	2.152	1.53	0.07	0.68	0.07	150.51	26.86	0.335	0.17	S
4052	23 18 31.85	0.46	-57 29 27.43	0.52	1.705	0.301	1.397	0.192	4.78	1.24	2.27	0.97	158.49	46.81	0.169	–	S
4053	23 18 33.05	0.20	-57 19 43.70	0.26	45.901	2.615	13.840	0.834	15.59	0.50	9.30	0.30	108.34	3.90	0.342	–	M
4054	23 18 27.75	0.27	-57 40 20.97	0.30	3.805	0.313	2.572	0.208	6.22	0.62	4.60	0.52	160.79	26.17	0.142	–	S
4055	23 18 10.94	0.27	-58 29 45.18	0.21	11.630	0.745	6.287	0.388	12.51	0.60	0.66	0.21	32.07	2.90	0.175	–	M
4056	23 18 16.83	0.14	-58 12 13.23	0.15	37.189	2.062	35.635	1.966	1.91	0.03	1.32	0.03	131.48	14.11	0.152	-0.46	S
4057	23 18 05.23	0.17	-58 44 08.36	0.17	18.777	1.103	12.710	0.743	6.65	0.21	4.13	0.17	100.88	8.77	0.235	-0.87	S
4058	23 18 15.48	0.52	-58 13 40.70	0.76	4.704	0.332	1.596	0.182	14.79	1.86	7.46	0.98	25.50	14.68	0.154	–	S
4059	23 18 30.69	1.80	-57 26 20.78	1.55	6.007	0.369	0.826	0.153	23.93	4.65	16.12	3.03	128.38	29.81	0.170	–	S
4060	23 17 41.07	0.55	-59 52 23.97	0.66	1.323	0.297	1.096	0.186	4.79	1.60	1.61	1.18	166.23	50.01	0.170	–	S
4061	23 18 19.57	0.67	-57 53 07.43	0.81	1.566	0.246	0.934	0.164	7.53	1.94	5.35	1.48	15.83	53.42	0.144	–	S
4062	23 19 10.38	0.67	-54 58 16.04	1.51	9.039	0.594	2.001	0.292	21.99	3.59	9.41	1.47	174.14	15.60	0.287	–	S
4063	23 19 48.20	0.96	-52 27 01.87	0.84	1.564	0.258	0.876	0.174	8.17	2.30	6.21	1.87	75.00	68.83	0.154	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4064	23 17 58.46	0.89	-58 50 47.90	0.38	13.646	0.962	4.325	0.360	15.60	2.15	1.53	0.59	18.88	7.39	0.271	–	M
4065	23 18 48.04	0.24	-56 14 13.22	0.26	8.899	0.640	4.488	0.310	7.20	0.55	4.72	0.42	125.47	13.89	0.187	–	M
4066	23 18 25.26	0.85	-57 30 15.92	1.49	2.400	0.253	0.839	0.171	14.02	3.54	7.69	1.94	178.11	28.47	0.158	–	S
4067	23 19 00.81	1.11	-55 25 24.56	1.01	17.047	0.947	1.401	0.146	28.70	2.70	24.75	2.25	120.29	30.14	0.173	–	S
4068	23 19 41.50	0.15	-52 46 24.10	0.18	62.094	3.549	25.716	1.464	11.77	0.25	5.35	0.13	73.03	2.10	0.377	-1.25	M
4069	23 19 39.23	0.24	-52 58 41.27	0.24	5.616	0.492	4.720	0.350	3.95	0.46	3.08	0.42	71.77	53.53	0.226	–	S
4070	23 18 42.45	1.00	-56 26 52.53	2.35	8.102	0.566	1.319	0.205	18.90	5.62	6.65	2.10	81.15	22.00	0.192	–	M
4071	23 18 43.35	1.36	-56 26 31.00	1.16	2.813	0.305	1.006	0.207	14.76	3.72	6.94	1.86	54.38	26.35	0.192	–	S
4072	23 18 35.87	0.69	-56 50 11.55	1.31	12.968	0.798	2.723	0.333	24.38	3.27	8.45	1.09	160.69	11.82	0.329	–	S
4073	23 19 39.95	0.46	-52 51 23.08	0.39	2.818	0.439	2.382	0.282	4.76	1.07	1.58	0.81	81.91	36.68	0.242	–	S
4074	23 19 05.00	1.00	-55 06 45.64	1.02	3.357	0.320	1.165	0.211	11.52	2.48	10.41	2.21	141.62	96.79	0.189	–	S
4075	23 19 35.04	0.84	-53 07 31.49	0.60	2.246	0.392	1.490	0.256	7.62	2.02	3.63	1.30	81.63	34.82	0.228	–	S
4076	23 19 13.80	0.87	-54 23 47.16	1.30	51.200	2.828	3.165	0.298	38.06	3.05	25.59	2.00	177.64	13.83	0.379	–	S
4077	23 18 42.04	0.21	-56 22 52.70	0.26	6.222	0.433	4.082	0.284	7.35	0.50	3.91	0.35	174.46	11.65	0.163	–	S
4078	23 17 33.60	1.24	-59 48 08.83	0.92	2.458	0.263	0.910	0.178	12.78	3.01	7.74	1.92	119.88	33.77	0.161	–	S
4079	23 17 59.11	0.16	-58 35 04.00	0.16	11.403	0.712	10.481	0.610	2.70	0.16	1.89	0.15	35.25	30.14	0.196	-0.12	S
4080	23 20 12.07	0.26	-50 12 33.12	0.21	18.834	1.136	11.318	0.653	15.16	0.60	2.81	0.20	151.21	2.56	0.197	-0.83	M
4081	23 18 39.41	0.55	-56 25 58.33	1.02	2.312	0.323	1.266	0.214	10.26	2.41	3.85	1.23	175.37	22.99	0.192	–	S
4082	23 19 02.74	0.58	-55 01 02.30	0.73	9.890	0.744	3.802	0.314	15.10	2.08	0.00	0.52	54.92	7.01	0.234	–	M
4083	23 18 40.85	0.36	-56 19 41.59	0.42	3.099	0.334	2.140	0.220	7.00	1.01	3.28	0.68	152.39	20.64	0.175	–	S
4084	23 18 24.31	2.35	-57 09 45.42	1.11	16.220	0.899	0.939	0.119	45.84	5.43	21.81	2.61	87.80	14.49	0.175	–	S
4085	23 18 49.93	0.70	-55 41 36.57	0.66	10.540	0.709	2.198	0.233	11.36	1.85	7.14	1.24	42.87	23.55	0.199	–	M
4086	23 17 55.51	0.89	-58 35 02.52	0.60	2.564	0.338	1.375	0.226	9.61	2.07	5.01	1.33	75.80	29.95	0.198	–	S
4087	23 20 02.04	1.87	-50 49 01.64	0.47	13.875	0.880	2.438	0.282	25.14	4.39	4.74	1.03	179.58	10.37	0.248	–	M
4088	23 19 57.08	0.47	-50 59 54.16	0.55	2.683	0.425	2.075	0.274	5.93	1.31	2.74	0.96	33.57	37.85	0.238	–	S
4089	23 19 50.72	1.64	-51 38 27.10	0.41	4.384	0.487	1.122	0.214	0.00	3.86	0.00	0.78	0.00	14.28	0.204	–	M
4090	23 18 59.94	0.57	-55 01 16.04	0.51	3.597	0.418	2.153	0.274	8.30	1.44	4.73	0.98	58.38	27.49	0.230	–	S
4091	23 17 51.34	0.63	-58 35 29.88	0.58	3.020	0.368	1.696	0.244	7.35	1.40	6.52	1.38	88.54	168.04	0.207	–	S
4092	23 17 35.72	0.91	-59 18 40.75	1.04	1.456	0.258	0.857	0.170	10.43	2.93	1.53	1.28	40.09	23.02	0.157	–	S
4093	23 17 20.72	0.38	-59 55 51.55	0.34	1.739	0.258	1.541	0.167	3.83	0.85	1.40	0.70	61.24	47.66	0.140	–	S
4094	23 19 58.95	0.74	-50 37 02.20	1.55	2.546	0.275	0.967	0.185	15.28	3.68	6.32	1.63	171.74	22.84	0.171	–	S
4095	23 19 15.22	0.88	-53 31 46.92	0.37	273.271	15.374	61.193	3.580	38.35	2.06	15.04	0.77	176.19	4.58	1.220	-0.65	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4096	23 18 31.18	0.46	-56 20 36.74	0.57	1.935	0.288	1.389	0.188	6.01	1.31	3.80	1.02	173.80	43.93	0.162	–	S
4097	23 17 37.46	0.57	-58 55 05.50	0.28	30.667	1.773	9.113	0.580	16.73	1.31	6.91	0.54	7.25	5.91	0.292	–	M
4098	23 18 37.70	0.42	-55 47 47.48	0.44	2.388	0.291	1.673	0.191	5.81	1.03	4.54	0.88	147.52	56.06	0.157	–	S
4099	23 17 54.93	0.70	-58 04 10.12	0.87	1.140	0.245	0.797	0.159	6.32	2.11	3.78	1.54	168.57	56.56	0.144	–	S
4100	23 19 40.17	0.57	-51 41 48.12	0.54	3.274	0.456	2.182	0.299	6.41	1.36	5.09	1.16	119.37	62.05	0.256	–	S
4101	23 17 20.57	0.14	-59 34 06.12	0.15	17.542	0.993	16.948	0.942	1.69	0.06	1.16	0.06	167.78	26.67	0.135	-0.18	S
4102	23 19 59.37	0.38	-50 10 29.15	0.41	3.485	0.355	2.306	0.234	6.19	0.88	5.64	0.85	48.87	143.22	0.183	–	S
4103	23 19 55.41	0.15	-50 26 58.38	0.16	13.167	0.765	12.702	0.713	1.95	0.10	1.08	0.09	143.31	26.60	0.144	-0.26	S
4104	23 18 52.29	1.34	-54 46 49.34	1.04	2.927	0.354	1.128	0.245	11.96	3.27	8.33	2.24	113.02	45.75	0.222	–	S
4105	23 18 07.40	1.18	-57 12 59.37	0.83	14.230	0.990	7.532	0.486	24.11	3.30	2.23	0.60	148.47	6.50	0.255	–	M
4106	23 19 49.53	0.97	-50 48 44.09	0.89	6.295	0.449	1.704	0.249	14.76	2.47	12.26	1.86	118.24	38.34	0.225	–	S
4107	23 17 34.05	0.50	-58 50 20.82	1.20	18.172	1.049	3.029	0.323	26.31	2.82	10.76	1.09	176.82	10.97	0.318	–	S
4108	23 18 15.23	1.24	-56 43 50.01	1.88	18.291	1.026	1.485	0.204	33.66	4.56	20.85	2.69	166.70	18.69	0.264	–	S
4109	23 18 59.38	0.33	-54 12 51.21	0.33	2.494	0.303	2.097	0.201	3.73	0.70	3.24	0.68	114.18	128.19	0.159	–	S
4110	23 17 58.56	0.34	-57 36 55.47	0.42	3.531	0.326	2.169	0.212	7.58	0.95	4.76	0.69	168.00	22.12	0.163	–	S
4111	23 19 39.52	0.25	-51 24 27.58	0.27	4.783	0.474	4.137	0.330	4.25	0.57	1.83	0.45	138.00	27.35	0.231	–	S
4112	23 18 40.36	1.23	-55 16 38.67	0.78	2.325	0.302	1.037	0.206	11.28	2.91	6.59	1.80	94.59	34.68	0.185	–	S
4113	23 19 13.96	0.24	-53 05 45.55	0.23	8.468	0.599	5.690	0.398	6.63	0.49	4.57	0.37	120.43	16.89	0.230	–	S
4114	23 19 23.31	2.01	-52 25 12.99	0.92	4.203	0.515	2.490	0.236	19.16	5.00	3.41	1.33	161.89	15.16	0.192	–	M
4115	23 18 21.84	0.95	-56 15 09.04	1.60	2.967	0.287	0.927	0.192	15.40	3.86	8.47	2.08	169.63	28.29	0.180	–	S
4116	23 19 35.21	0.58	-51 35 13.53	0.62	2.310	0.511	1.955	0.320	3.88	1.44	3.09	1.31	31.19	2.13	0.291	–	S
4117	23 19 55.95	0.36	-50 00 00.98	0.45	1.852	0.329	1.852	0.212	0.00	0.97	0.00	0.79	0.00	46.93	0.182	–	S
4118	23 18 21.96	0.80	-56 03 54.32	0.63	5.024	0.424	1.918	0.264	11.63	1.86	8.67	1.42	82.29	36.54	0.226	–	S
4119	23 19 31.22	0.16	-51 44 09.38	0.17	9.669	0.634	8.679	0.520	3.32	0.22	2.03	0.19	125.00	21.88	0.201	-0.94	S
4120	23 19 16.51	0.23	-52 44 16.09	0.24	5.526	0.505	4.864	0.361	3.44	0.45	2.51	0.42	52.14	60.84	0.236	–	S
4121	23 18 12.12	0.39	-56 35 30.30	0.69	4.679	0.363	1.965	0.216	12.56	1.60	6.16	0.85	1.97	14.81	0.177	–	S
4122	23 18 11.57	0.16	-56 36 33.18	0.17	9.958	0.644	9.123	0.541	2.72	0.19	2.02	0.18	168.38	36.69	0.197	0.31	S
4123	23 17 38.47	0.64	-58 17 44.71	0.61	1.515	0.291	1.130	0.187	5.09	1.52	4.04	1.33	133.92	109.70	0.167	–	S
4124	23 17 21.71	0.78	-59 03 41.93	0.95	1.929	0.393	1.230	0.259	6.84	2.31	4.83	1.72	176.86	66.43	0.233	–	S
4125	23 19 37.16	0.34	-51 09 39.72	0.42	12.029	0.984	7.145	0.519	12.08	1.15	0.00	0.27	54.15	4.26	0.338	–	M
4126	23 19 21.94	0.18	-52 15 19.50	0.21	5.337	0.380	4.393	0.284	4.90	0.34	2.45	0.27	7.60	16.00	0.143	–	S
4127	23 17 59.13	0.14	-57 04 56.72	0.15	63.627	3.517	61.010	3.362	1.90	0.03	1.30	0.03	174.78	11.00	0.203	-0.88	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
4128	23 18 14.22	0.80	-56 16 54.61	1.29	5.121	0.341	1.150	0.172	18.76	3.09	11.23	1.76	170.20	21.10	0.165	-	S
4129	23 17 11.07	1.71	-59 22 37.44	0.31	2.215	0.323	0.702	0.140	0.00	4.01	0.00	0.60	0.00	11.25	0.135	-	M
4130	23 17 18.68	0.88	-59 01 04.43	0.75	3.458	0.372	1.488	0.248	9.83	2.05	8.20	1.71	104.88	83.55	0.216	-	S
4131	23 18 55.71	0.68	-53 52 47.87	0.86	1.944	0.411	1.396	0.264	7.01	2.14	2.70	1.39	30.29	39.54	0.240	-	S
4132	23 19 25.67	0.73	-51 47 54.66	0.61	7.856	0.514	2.370	0.255	16.86	2.02	8.44	0.94	126.54	12.84	0.216	-	S
4133	23 18 03.56	0.48	-56 47 38.10	0.52	1.821	0.341	1.526	0.216	4.02	1.21	2.83	1.06	165.60	94.73	0.192	-	S
4134	23 18 40.79	0.48	-54 42 31.19	0.65	2.235	0.364	1.622	0.235	6.57	1.53	2.92	1.04	168.24	33.15	0.206	-	S
4135	23 19 18.55	0.15	-52 11 45.73	0.16	14.071	0.813	12.897	0.725	2.82	0.10	2.03	0.09	141.99	19.20	0.145	0.10	S
4136	23 18 17.56	1.26	-55 59 03.07	0.94	2.537	0.353	1.149	0.242	11.68	3.19	5.92	1.81	64.59	32.23	0.219	-	S
4137	23 18 37.52	0.85	-54 50 40.64	0.91	2.701	0.378	1.361	0.256	8.77	2.25	7.11	1.84	148.82	72.20	0.226	-	S
4138	23 18 18.90	0.42	-55 53 58.46	0.45	2.012	0.315	1.648	0.203	4.50	1.06	2.84	0.88	150.23	58.67	0.174	-	S
4139	23 18 43.28	0.52	-54 22 07.27	0.93	2.636	0.344	1.450	0.228	10.16	2.18	4.22	1.17	4.70	23.12	0.201	-	S
4140	23 18 27.01	0.56	-55 19 31.26	0.56	1.256	0.248	1.024	0.158	4.08	1.30	3.53	1.25	47.79	2.37	0.141	-	S
4141	23 19 22.46	0.85	-51 45 52.79	0.54	2.227	0.344	1.409	0.226	8.48	2.05	3.50	1.16	94.17	26.55	0.200	-	S
4142	23 17 09.51	0.94	-59 07 46.74	1.16	6.192	0.471	1.642	0.278	14.35	2.78	11.70	2.12	5.59	43.25	0.258	-	S
4143	23 17 16.61	0.54	-58 48 36.77	0.61	2.328	0.696	2.346	0.414	0.00	1.46	0.00	1.17	0.00	82.36	0.395	-	S
4144	23 16 59.64	0.25	-59 30 06.52	0.42	4.920	0.356	2.601	0.215	10.45	0.92	3.92	0.47	7.48	10.22	0.151	-	S
4145	23 17 07.50	0.20	-59 06 20.55	0.19	41.834	2.345	12.119	0.716	11.76	0.35	10.09	0.28	166.95	7.58	0.260	-0.90	M
4146	23 19 01.89	0.27	-52 48 01.32	0.17	89.697	5.044	47.618	2.643	22.31	0.57	0.74	0.11	15.19	1.28	0.354	-0.98	M
4147	23 17 03.74	0.89	-59 16 35.65	0.74	2.408	0.282	1.113	0.190	9.91	2.16	6.99	1.59	122.28	43.54	0.166	-	S
4148	23 18 33.26	0.32	-54 36 07.42	0.33	6.422	0.512	3.829	0.327	6.83	0.71	6.36	0.66	144.99	75.90	0.232	-	S
4149	23 17 24.28	2.07	-58 12 13.43	1.27	8.592	0.491	0.836	0.131	31.99	4.90	17.63	2.77	74.55	20.54	0.162	-	S
4150	23 17 52.97	0.76	-56 51 37.08	1.14	2.519	0.252	0.947	0.167	12.43	2.69	8.04	1.73	1.81	31.63	0.149	-	S
4151	23 17 06.29	0.17	-59 03 33.04	0.17	11.545	0.767	10.552	0.634	2.91	0.20	1.83	0.19	90.55	32.16	0.251	-0.02	S
4152	23 17 27.63	0.15	-58 04 52.76	0.16	9.389	0.576	8.418	0.488	2.93	0.15	2.37	0.15	179.50	31.91	0.150	0.16	S
4153	23 17 53.09	0.50	-56 49 32.97	0.49	3.096	0.356	1.904	0.234	7.10	1.23	5.38	1.00	135.04	45.05	0.194	-	S
4154	23 17 08.49	0.36	-58 44 59.58	0.22	29.175	1.927	17.830	1.092	13.13	0.81	3.31	0.30	165.05	3.96	0.480	-	M
4155	23 17 10.76	0.19	-58 46 13.93	0.17	41.159	2.525	29.114	1.673	9.61	0.30	3.16	0.15	163.33	2.57	0.486	-0.83	M
4156	23 17 56.29	0.16	-56 32 19.03	0.17	7.423	0.490	7.268	0.430	0.00	0.18	0.00	0.17	0.00	23.16	0.157	-0.20	S
4157	23 19 36.60	0.52	-50 11 52.45	0.62	2.682	0.311	1.566	0.205	8.37	1.48	5.62	1.11	32.38	39.19	0.172	-	S
4158	23 19 16.25	0.60	-51 38 28.42	1.12	1.541	0.360	1.121	0.229	0.00	2.62	0.00	1.36	0.00	30.64	0.212	-	S
4159	23 18 34.24	0.20	-54 19 03.72	0.21	11.697	0.732	7.300	0.464	7.85	0.39	4.45	0.27	143.57	9.34	0.217	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4160	23 19 29.37	0.15	-50 34 09.77	0.16	12.102	0.752	11.786	0.679	1.69	0.15	0.88	0.14	141.15	48.50	0.202	-0.59	S
4161	23 17 08.88	1.32	-58 43 05.69	0.77	6.406	0.617	2.238	0.406	14.40	3.06	7.42	1.72	79.07	26.05	0.371	-	S
4162	23 17 11.25	0.30	-58 35 22.10	0.32	3.142	0.401	2.802	0.266	3.29	0.69	2.00	0.60	176.34	62.01	0.212	-	S
4163	23 16 39.47	0.65	-59 56 39.56	0.74	3.430	0.318	1.440	0.204	10.57	1.82	7.75	1.36	28.30	34.29	0.175	-	S
4164	23 17 15.67	0.38	-58 20 03.09	0.40	1.716	0.285	1.550	0.181	3.40	0.93	1.27	0.78	153.79	59.39	0.157	-	S
4165	23 19 18.38	0.35	-51 06 29.85	0.39	5.988	0.609	4.127	0.402	6.15	0.83	4.88	0.76	20.47	63.72	0.311	-	S
4166	23 18 26.19	0.42	-54 29 05.21	0.39	3.691	0.365	2.318	0.239	7.27	1.01	5.00	0.77	126.69	29.14	0.188	-	S
4167	23 17 34.23	0.60	-57 15 58.96	0.57	4.856	0.413	2.098	0.258	10.31	1.48	7.84	1.17	51.93	37.05	0.213	-	S
4168	23 17 11.35	0.39	-58 15 02.34	0.36	4.988	0.385	2.560	0.236	8.54	0.89	6.75	0.74	128.87	30.30	0.174	-	S
4169	23 19 19.15	0.18	-50 53 06.55	0.20	7.014	0.526	6.387	0.411	2.98	0.29	2.15	0.28	177.91	58.69	0.209	-	S
4170	23 18 48.80	1.18	-52 58 06.15	0.97	1.712	0.272	0.840	0.187	9.25	2.78	7.23	2.23	91.24	72.17	0.167	-	S
4171	23 18 38.25	0.15	-53 35 01.17	0.16	30.988	1.870	28.570	1.636	2.83	0.14	1.74	0.13	138.88	20.26	0.447	-0.33	S
4172	23 17 41.04	0.58	-56 47 33.30	0.79	3.635	0.339	1.572	0.218	11.23	1.90	6.97	1.24	20.97	25.46	0.187	-	S
4173	23 17 30.82	0.45	-57 16 02.94	2.26	4.812	0.510	1.109	0.225	0.00	5.36	0.00	0.68	0.00	11.00	0.216	-	M
4174	23 19 09.18	0.43	-51 32 30.31	0.45	3.785	0.659	3.336	0.419	3.29	1.03	2.68	0.94	135.08	174.71	0.366	-	S
4175	23 16 47.01	0.92	-59 17 00.85	0.78	1.166	0.262	0.797	0.171	6.14	2.14	4.51	1.79	76.26	111.49	0.154	-	S
4176	23 17 10.36	0.37	-58 11 51.15	0.41	3.230	0.329	2.100	0.216	6.32	0.92	5.15	0.78	168.82	46.21	0.170	-	S
4177	23 17 39.56	0.60	-56 42 42.57	0.57	2.984	0.345	1.667	0.228	7.31	1.34	6.76	1.31	113.18	158.40	0.192	-	S
4178	23 18 11.10	0.31	-55 01 37.48	0.31	2.990	0.388	2.719	0.257	3.37	0.70	1.38	0.60	52.07	51.95	0.205	-	S
4179	23 18 39.30	0.18	-53 13 30.37	0.19	11.013	0.750	7.888	0.481	6.81	0.33	0.00	0.19	47.82	4.30	0.207	-	M
4180	23 17 20.68	0.48	-57 35 10.87	1.00	2.909	0.261	1.185	0.165	13.68	2.34	5.48	1.06	5.37	16.46	0.146	-	S
4181	23 17 31.04	0.36	-57 02 54.91	0.46	4.880	0.398	2.531	0.248	9.16	1.06	6.00	0.75	164.65	20.20	0.190	-	S
4182	23 18 04.57	0.71	-55 17 05.02	0.93	1.117	0.263	0.820	0.168	6.62	2.26	2.59	1.50	23.79	45.36	0.154	-	S
4183	23 17 06.70	1.02	-58 03 49.14	0.86	4.836	0.371	1.484	0.218	16.28	2.75	7.88	1.36	130.89	18.34	0.199	-	S
4184	23 19 06.14	0.14	-51 14 47.12	0.15	237.921	13.205	229.326	12.655	2.17	0.04	0.76	0.04	25.43	8.91	1.025	-0.59	S
4185	23 18 57.23	0.41	-51 46 38.09	0.26	9.215	0.607	4.455	0.339	12.59	0.98	3.97	0.39	109.61	7.81	0.226	-	S
4186	23 17 04.43	0.92	-58 00 02.06	0.40	2.296	0.343	0.890	0.148	0.00	2.23	0.00	0.61	0.00	11.94	0.140	-	M
4187	23 18 47.39	0.97	-52 18 58.20	1.59	2.556	0.246	0.865	0.161	17.80	4.13	5.97	1.50	29.64	19.25	0.154	-	S
4188	23 18 58.89	0.18	-51 30 17.22	0.20	13.524	1.069	12.682	0.831	3.01	0.33	0.67	0.28	7.67	28.25	0.446	-	S
4189	23 18 13.38	0.93	-54 22 30.85	1.03	1.399	0.275	0.823	0.185	7.37	2.43	6.04	2.13	156.68	110.08	0.166	-	S
4190	23 19 04.76	1.15	-51 02 15.94	1.10	5.231	0.594	1.374	0.252	11.64	3.60	0.00	0.87	138.65	13.90	0.240	-	M
4191	23 16 30.10	0.64	-59 24 05.89	0.71	3.591	0.295	1.361	0.182	10.87	1.73	9.09	1.38	161.30	41.41	0.154	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4192	23 16 52.98	0.89	-58 24 09.93	1.19	6.314	0.383	1.192	0.152	23.78	3.16	10.39	1.36	33.84	14.13	0.151	–	S
4193	23 17 48.13	0.15	-55 41 02.07	0.17	15.792	0.955	13.739	0.793	4.18	0.17	1.42	0.13	165.90	9.39	0.233	-1.19	S
4194	23 17 24.27	0.17	-56 48 11.10	0.17	9.564	0.638	8.585	0.519	2.90	0.22	2.42	0.20	127.33	55.99	0.210	-0.19	S
4195	23 17 29.51	0.72	-56 33 40.45	0.86	1.019	0.269	0.802	0.169	5.09	2.05	2.97	1.62	4.91	81.86	0.156	–	S
4196	23 16 41.46	1.56	-58 45 46.49	0.87	12.627	0.863	2.638	0.305	18.08	4.04	3.30	1.06	156.34	12.08	0.268	–	M
4197	23 18 21.09	0.39	-53 41 48.03	0.44	2.401	0.387	2.079	0.248	3.97	0.99	2.18	0.85	166.29	63.44	0.213	–	S
4198	23 18 42.57	0.97	-52 19 01.04	0.80	1.681	0.257	0.923	0.173	9.67	2.54	5.00	1.52	62.43	33.03	0.154	–	S
4199	23 17 47.22	0.78	-55 31 00.19	1.39	5.321	0.372	1.287	0.201	18.87	3.32	10.03	1.69	170.23	19.92	0.192	–	S
4200	23 19 07.48	0.18	-50 29 50.49	0.19	12.002	0.739	8.471	0.512	6.57	0.29	3.88	0.21	134.37	9.43	0.201	-0.26	S
4201	23 17 10.16	0.77	-57 23 00.70	1.26	1.489	0.268	0.816	0.181	9.53	3.01	4.58	1.74	179.03	35.65	0.164	–	S
4202	23 17 04.93	0.45	-57 34 42.90	0.79	3.350	0.292	1.450	0.183	12.11	1.85	5.96	1.00	5.80	17.57	0.155	–	S
4203	23 19 08.11	0.18	-50 15 25.30	0.20	6.103	0.434	5.240	0.333	4.14	0.31	2.50	0.26	0.93	24.63	0.162	–	S
4204	23 17 14.24	0.21	-56 49 28.31	0.22	15.604	0.968	7.029	0.444	7.83	0.40	6.15	0.34	52.45	15.58	0.218	–	M
4205	23 17 15.42	0.94	-56 47 21.59	0.68	1.982	0.343	1.202	0.228	7.94	2.19	4.77	1.56	92.98	47.01	0.203	–	S
4206	23 16 05.17	0.84	-59 51 30.89	1.25	3.898	0.291	1.056	0.169	17.24	3.13	8.85	1.61	25.54	20.31	0.159	–	S
4207	23 17 16.48	0.38	-56 37 05.02	0.37	2.779	0.323	2.054	0.213	4.94	0.83	4.47	0.79	136.82	120.02	0.171	–	S
4208	23 17 29.01	0.50	-55 55 02.74	0.41	3.697	0.372	2.183	0.243	8.02	1.16	5.21	0.86	75.30	28.98	0.196	–	S
4209	23 17 04.19	0.57	-57 06 17.03	0.42	4.393	0.360	2.035	0.223	10.26	1.30	6.80	0.93	102.87	23.75	0.178	–	S
4210	23 18 40.63	0.89	-51 40 36.88	1.23	2.906	0.398	1.322	0.273	11.00	2.91	7.02	2.00	18.76	45.41	0.244	–	S
4211	23 18 22.56	0.39	-52 48 45.29	0.39	6.726	0.772	4.883	0.509	5.58	0.90	4.37	0.79	58.15	61.68	0.407	–	S
4212	23 17 25.15	0.39	-56 02 23.85	0.45	2.511	0.490	2.410	0.305	0.00	1.02	0.00	0.84	0.00	57.53	0.273	–	S
4213	23 18 19.82	0.14	-52 49 34.46	0.15	125.686	6.958	87.530	4.833	7.25	0.06	5.47	0.05	61.93	2.20	0.425	-0.90	M
4214	23 18 55.63	0.20	-50 28 26.06	0.20	35.259	2.053	12.828	0.753	12.74	0.41	4.97	0.20	42.74	2.94	0.264	-0.91	M
4215	23 17 15.80	0.14	-56 23 07.19	0.15	150.629	8.303	149.774	8.244	0.00	0.02	0.00	0.02	0.00	10.60	0.317	-0.16	S
4216	23 16 25.09	2.09	-58 41 12.97	1.75	8.414	0.681	1.449	0.267	20.92	6.35	0.00	0.79	42.51	10.81	0.255	–	M
4217	23 18 43.18	0.27	-51 16 27.83	0.30	8.932	0.798	6.648	0.541	5.49	0.62	4.10	0.52	159.09	38.59	0.377	–	S
4218	23 18 38.80	0.21	-51 26 44.24	0.16	263.146	14.570	75.927	4.233	18.89	0.36	6.39	0.14	177.44	1.47	0.694	-1.12	M
4219	23 18 04.46	0.14	-53 32 49.87	0.15	102.781	5.714	97.983	5.411	2.15	0.04	1.33	0.04	159.94	12.02	0.481	-0.61	S
4220	23 16 42.46	0.49	-57 49 36.06	1.14	3.655	0.274	1.175	0.158	16.95	2.69	6.55	1.08	4.16	14.71	0.144	–	S
4221	23 18 28.47	0.53	-52 02 55.85	0.31	13.921	0.873	4.409	0.315	15.74	1.28	4.60	0.47	161.90	5.76	0.201	–	M
4222	23 17 57.50	0.31	-53 57 36.41	0.46	2.676	0.305	1.946	0.200	7.01	1.04	2.30	0.65	5.38	19.24	0.161	–	S
4223	23 18 31.59	0.29	-51 46 23.07	0.18	22.507	1.414	13.584	0.784	16.99	0.63	0.00	0.16	167.62	2.04	0.238	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4224	23 17 01.77	0.33	-56 43 16.82	0.44	42.763	2.439	6.420	0.442	15.93	1.02	10.00	0.63	113.84	8.22	0.266	–	M
4225	23 17 17.43	0.15	-56 01 57.09	0.16	18.519	1.113	15.913	0.917	3.47	0.15	2.96	0.14	42.40	37.53	0.263	-0.31	S
4226	23 18 43.31	0.47	-50 57 47.30	0.52	16.683	0.977	4.286	0.361	18.28	1.41	10.28	0.76	45.34	10.94	0.274	–	S
4227	23 18 24.10	1.80	-52 13 13.00	1.42	5.635	0.350	0.840	0.151	23.85	4.71	15.62	2.76	119.07	26.59	0.164	–	S
4228	23 17 18.36	0.32	-55 57 49.60	0.48	7.721	0.590	3.820	0.358	10.24	1.08	5.80	0.68	1.83	15.59	0.269	–	S
4229	23 17 03.52	1.00	-56 39 46.59	1.28	9.199	0.538	1.289	0.176	22.00	3.03	17.43	2.30	3.07	30.54	0.185	–	S
4230	23 18 50.31	0.68	-50 28 09.19	1.03	2.797	0.492	1.709	0.326	8.65	2.38	4.50	1.57	8.49	40.99	0.292	–	S
4231	23 18 40.26	0.14	-51 05 45.51	0.15	54.437	3.048	49.291	2.732	3.88	0.07	0.55	0.05	173.46	5.42	0.333	-0.87	S
4232	23 17 31.47	0.56	-55 14 29.43	0.83	3.148	0.360	1.612	0.238	10.34	1.99	5.24	1.17	19.91	24.22	0.206	–	S
4233	23 18 02.56	0.14	-53 23 08.62	0.15	23.664	1.359	23.371	1.305	0.98	0.08	0.82	0.08	178.63	2.45	0.226	0.13	S
4234	23 18 40.59	0.58	-50 57 57.16	0.69	2.516	0.474	1.904	0.304	6.24	1.67	2.85	1.20	34.69	43.63	0.271	–	S
4235	23 18 09.91	0.27	-52 51 43.49	0.28	3.812	0.601	4.330	0.392	0.00	0.56	0.00	0.53	0.00	2.42	0.322	–	S
4236	23 18 52.12	0.25	-50 03 45.17	0.29	5.110	0.513	4.386	0.355	4.09	0.56	2.58	0.50	13.92	48.84	0.252	–	S
4237	23 18 18.30	0.43	-52 18 36.88	0.45	1.285	0.280	1.301	0.171	0.00	0.99	0.00	0.94	0.00	113.43	0.156	–	S
4238	23 18 37.75	0.87	-50 58 06.85	1.15	9.140	0.593	2.130	0.284	21.23	3.11	9.82	1.38	36.77	15.70	0.269	–	S
4239	23 18 27.85	0.25	-51 37 14.74	0.21	10.065	0.718	7.032	0.486	7.20	0.52	3.02	0.32	101.67	10.50	0.278	–	S
4240	23 16 07.48	0.40	-58 52 16.76	0.31	39.060	2.272	11.826	0.704	19.52	1.04	4.61	0.29	148.11	3.06	0.270	-0.72	M
4241	23 18 28.24	0.34	-51 31 38.52	0.38	8.768	0.925	6.303	0.613	5.56	0.80	4.67	0.75	158.90	75.89	0.475	–	S
4242	23 17 29.70	0.47	-54 55 59.42	0.48	2.333	0.315	1.654	0.206	5.58	1.11	4.67	1.03	37.97	104.46	0.174	–	S
4243	23 15 42.80	0.50	-59 47 55.76	0.53	1.252	0.236	1.027	0.150	4.47	1.30	2.66	1.04	29.64	66.62	0.133	–	S
4244	23 18 41.10	1.90	-50 27 25.76	0.80	44.640	2.505	3.070	0.333	30.78	4.47	12.38	1.82	6.52	13.17	0.287	–	M
4245	23 18 46.83	1.03	-50 02 48.95	0.95	26.150	1.514	3.580	0.332	26.08	3.05	10.22	1.19	43.86	9.88	0.267	–	M
4246	23 16 56.11	0.45	-56 32 08.84	0.43	3.903	0.366	2.202	0.236	7.42	1.02	6.52	0.93	61.32	89.05	0.187	–	S
4247	23 17 57.63	0.68	-53 07 28.73	0.72	2.324	0.338	1.378	0.225	7.21	1.66	6.21	1.57	38.28	134.61	0.195	–	S
4248	23 17 22.99	0.54	-54 58 35.82	0.57	3.008	0.335	1.687	0.220	7.62	1.33	6.54	1.20	30.09	86.86	0.184	–	S
4249	23 16 15.75	0.79	-58 10 31.12	0.92	3.223	0.394	1.495	0.266	9.64	2.27	7.22	1.68	159.29	46.86	0.234	–	S
4250	23 18 00.15	0.56	-52 47 13.00	0.46	2.347	0.382	1.825	0.245	5.77	1.35	2.42	0.95	111.45	34.57	0.214	–	S
4251	23 18 28.08	0.82	-50 59 02.13	0.89	2.487	0.425	1.483	0.283	8.29	2.28	5.22	1.66	45.02	50.64	0.252	–	S
4252	23 17 20.68	0.80	-54 57 20.41	0.88	1.745	0.316	1.073	0.210	7.61	2.21	5.03	1.66	36.48	58.74	0.187	–	S
4253	23 18 09.53	0.65	-52 00 50.58	0.26	4.270	0.495	2.071	0.228	0.00	1.51	0.00	0.50	0.00	9.52	0.198	–	M
4254	23 16 54.13	0.23	-55 59 33.51	0.88	78.018	4.471	26.325	1.513	38.42	2.08	3.03	0.25	102.31	2.50	0.439	-1.30	M
4255	23 15 46.78	0.15	-59 03 14.68	0.15	38.242	2.166	27.576	1.534	6.52	0.10	3.68	0.07	7.85	2.26	0.231	0.02	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
4256	23 18 36.17	0.70	-50 06 55.11	0.86	4.227	0.375	1.638	0.239	11.84	2.00	9.05	1.61	22.78	50.46	0.206	–	S
4257	23 15 29.53	0.20	-59 38 44.97	0.17	11.537	0.721	6.613	0.401	6.98	0.33	2.26	0.20	174.45	4.79	0.168	–	M
4258	23 17 41.26	0.14	-53 24 43.32	0.15	56.908	3.158	53.214	2.937	2.65	0.04	1.47	0.04	171.29	8.09	0.243	-0.79	S
4259	23 17 54.28	0.16	-52 39 16.26	0.17	20.529	1.258	13.587	0.794	4.64	0.20	2.76	0.16	116.33	9.30	0.268	-0.90	M
4260	23 17 53.29	0.36	-52 36 57.34	0.22	46.021	2.648	21.636	1.234	19.57	0.85	2.18	0.21	25.22	2.40	0.326	-1.26	M
4261	23 16 20.71	0.84	-57 27 22.80	1.06	3.551	0.277	1.113	0.165	16.36	2.86	7.48	1.32	149.44	17.75	0.151	–	S
4262	23 17 08.62	0.52	-55 05 31.22	0.80	5.652	0.432	2.052	0.254	13.33	1.89	8.04	1.15	11.85	20.43	0.216	–	S
4263	23 16 49.15	0.18	-56 03 20.94	0.17	15.753	1.010	11.156	0.658	6.32	0.26	1.32	0.16	173.78	4.39	0.237	-0.01	M
4264	23 17 57.06	0.97	-52 19 55.20	1.13	1.685	0.288	0.881	0.197	8.46	2.55	7.10	2.33	169.80	126.80	0.176	–	S
4265	23 15 16.42	0.65	-59 57 03.23	0.91	2.319	0.277	1.120	0.185	10.03	2.20	5.96	1.39	167.90	29.38	0.163	–	S
4266	23 15 32.90	0.16	-59 13 39.63	0.15	109.303	6.067	68.807	3.794	19.05	0.20	4.05	0.05	9.93	0.58	0.265	-0.81	M
4267	23 15 21.86	0.15	-59 36 18.78	0.16	14.840	0.857	13.403	0.753	2.80	0.10	2.31	0.09	60.63	35.28	0.152	-0.68	S
4268	23 18 21.53	0.40	-50 31 09.32	0.36	4.812	0.437	2.974	0.284	7.44	0.95	5.43	0.71	81.36	27.83	0.216	–	S
4269	23 17 56.40	0.28	-52 04 20.34	0.22	9.557	0.588	4.672	0.317	10.56	0.61	6.01	0.36	104.36	9.03	0.174	–	S
4270	23 17 51.61	1.03	-52 20 14.89	1.12	5.497	0.468	1.186	0.183	14.73	3.44	0.00	0.90	134.86	12.11	0.171	–	M
4271	23 17 15.23	0.64	-54 25 54.59	0.71	2.094	0.281	1.197	0.187	7.60	1.68	6.28	1.43	157.98	74.31	0.161	–	S
4272	23 16 30.60	0.69	-56 35 54.35	0.85	1.240	0.260	0.869	0.168	6.37	2.05	3.79	1.51	166.07	55.78	0.152	–	S
4273	23 17 48.61	0.53	-52 26 06.78	0.85	1.001	0.249	0.853	0.153	0.00	2.02	0.00	1.13	0.00	30.66	0.143	–	S
4274	23 17 28.68	0.47	-53 32 11.73	0.46	3.886	0.509	2.744	0.333	5.78	1.10	4.62	0.99	56.96	77.91	0.279	–	S
4275	23 15 32.05	0.31	-59 00 04.17	0.27	4.690	0.451	3.587	0.305	5.73	0.66	2.76	0.51	71.67	22.47	0.221	–	S
4276	23 17 10.76	1.03	-54 28 22.87	0.89	1.579	0.248	0.835	0.168	9.59	2.70	5.46	1.68	126.59	37.46	0.150	–	S
4277	23 17 40.81	0.17	-52 44 15.67	0.18	9.203	0.624	8.430	0.512	2.93	0.23	1.87	0.21	87.59	30.97	0.213	–	S
4278	23 15 22.50	0.78	-59 19 21.43	1.18	2.320	0.338	1.150	0.229	10.93	2.93	4.71	1.54	23.72	27.68	0.207	–	S
4279	23 15 21.66	0.18	-59 18 25.66	0.18	8.736	0.602	7.746	0.479	3.64	0.25	1.78	0.22	81.89	20.72	0.212	–	S
4280	23 15 55.12	0.43	-57 58 24.14	0.49	1.234	0.244	1.120	0.152	3.73	1.16	0.00	0.91	22.07	51.87	0.136	–	S
4281	23 16 37.05	0.85	-56 05 02.12	1.11	2.025	0.361	1.123	0.244	8.54	2.67	5.63	1.88	168.07	52.99	0.218	–	S
4282	23 18 07.69	0.49	-50 59 06.79	0.43	11.837	0.937	5.711	0.443	13.87	1.38	1.31	0.45	143.28	6.11	0.312	–	M
4283	23 16 37.25	0.21	-55 56 15.86	0.21	8.542	0.628	6.591	0.447	4.70	0.38	3.95	0.34	42.87	48.98	0.248	–	S
4284	23 17 30.48	0.35	-52 57 38.02	0.34	64.260	3.729	23.184	1.355	31.72	1.02	3.26	0.16	45.95	1.60	0.458	–	M
4285	23 16 52.52	0.14	-55 07 52.71	0.15	236.688	13.430	178.142	9.890	5.57	0.09	1.66	0.06	64.17	2.09	1.347	-0.31	M
4286	23 18 18.77	0.34	-50 06 00.64	0.45	3.265	0.372	2.361	0.245	6.60	1.01	3.52	0.72	168.74	28.05	0.196	–	S
4287	23 17 49.41	2.97	-51 55 47.26	0.54	10.583	0.691	2.091	0.226	33.10	7.03	2.54	1.00	8.22	10.33	0.195	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4288	23 15 17.04	0.29	-59 18 07.92	0.31	4.921	0.451	3.498	0.301	5.55	0.66	4.33	0.57	170.38	35.79	0.218	–	S
4289	23 16 59.37	0.51	-54 40 27.91	0.47	1.538	0.314	1.384	0.196	3.58	1.19	1.42	1.02	73.16	76.43	0.176	–	S
4290	23 16 54.49	0.24	-54 54 15.25	0.26	7.335	0.546	4.960	0.363	6.11	0.51	4.93	0.44	156.21	30.18	0.224	–	S
4291	23 17 05.85	0.28	-54 14 53.17	0.30	6.202	0.404	3.031	0.227	9.36	0.67	7.06	0.51	144.60	17.46	0.142	–	S
4292	23 15 12.70	0.57	-59 20 59.03	0.52	2.053	0.351	1.544	0.226	5.25	1.35	3.69	1.11	58.67	77.70	0.198	–	S
4293	23 16 56.05	0.14	-54 42 02.39	0.15	27.217	1.529	26.369	1.462	1.66	0.06	1.19	0.05	36.51	33.01	0.180	0.48	S
4294	23 15 51.01	0.81	-57 44 46.13	1.78	2.416	0.213	0.695	0.138	17.67	4.23	7.81	1.85	5.03	22.64	0.133	–	S
4295	23 14 55.09	0.14	-59 55 18.57	0.15	26.605	1.489	25.478	1.411	1.71	0.05	1.57	0.05	88.35	93.09	0.159	-0.41	S
4296	23 16 04.15	0.20	-57 08 24.18	0.21	5.109	0.375	3.987	0.269	4.64	0.37	3.70	0.33	179.16	32.22	0.147	–	S
4297	23 16 38.98	0.49	-55 29 44.32	0.63	3.131	0.375	1.850	0.247	7.91	1.46	5.32	1.09	12.44	37.00	0.209	–	S
4298	23 17 56.01	1.43	-51 06 10.71	0.86	3.803	0.402	1.414	0.270	14.62	3.67	6.86	1.65	110.24	23.43	0.249	–	S
4299	23 17 15.19	0.72	-53 30 00.93	0.64	5.308	0.492	2.315	0.316	10.69	1.79	7.72	1.31	63.73	35.04	0.268	–	S
4300	23 16 08.99	0.42	-56 47 23.60	0.35	2.061	0.281	1.679	0.183	5.09	0.95	2.03	0.72	114.80	32.05	0.152	–	S
4301	23 16 13.08	0.77	-56 36 04.90	1.22	1.649	0.250	0.827	0.170	10.63	2.96	5.12	1.65	17.61	31.55	0.153	–	S
4302	23 15 53.15	0.80	-57 25 40.15	1.25	3.455	0.275	0.998	0.167	15.24	2.96	9.72	1.82	179.72	27.07	0.154	–	S
4303	23 15 35.22	0.14	-58 09 07.97	0.15	61.079	3.374	57.784	3.183	2.25	0.03	1.44	0.03	57.73	9.06	0.180	-0.82	S
4304	23 18 09.40	0.46	-50 04 05.78	0.27	5.092	0.467	2.637	0.227	0.00	1.11	0.00	0.36	0.00	6.25	0.174	–	M
4305	23 15 47.73	0.51	-57 37 18.38	0.54	1.757	0.272	1.264	0.177	5.45	1.30	4.34	1.10	158.46	77.16	0.153	–	S
4306	23 16 16.02	0.30	-56 21 40.77	0.33	2.569	0.358	2.412	0.235	3.06	0.72	0.00	0.60	156.40	45.57	0.191	–	S
4307	23 16 13.69	0.17	-56 21 21.27	0.19	7.359	0.509	6.498	0.403	3.82	0.26	1.53	0.22	166.21	16.40	0.181	–	S
4308	23 17 15.69	0.81	-53 12 05.14	0.81	1.774	0.334	1.150	0.219	7.39	2.15	4.46	1.57	49.54	52.60	0.196	–	S
4309	23 17 03.95	1.72	-53 42 44.69	1.13	4.073	0.365	1.111	0.239	16.33	4.19	10.27	2.47	105.70	33.75	0.228	–	S
4310	23 15 05.80	0.51	-59 05 43.79	0.56	2.138	0.256	1.282	0.169	7.01	1.34	5.72	1.09	161.25	54.78	0.142	–	S
4311	23 16 51.45	0.20	-54 20 38.68	0.23	6.306	0.417	4.179	0.275	6.73	0.40	4.69	0.32	8.13	16.28	0.141	–	S
4312	23 15 01.92	0.31	-59 12 56.11	0.31	3.980	0.386	2.877	0.258	4.94	0.68	4.72	0.62	174.81	109.97	0.191	–	S
4313	23 17 13.23	0.15	-53 06 28.83	0.16	16.183	0.947	13.799	0.784	4.14	0.14	2.37	0.11	118.06	10.15	0.189	-0.66	S
4314	23 16 55.41	0.50	-54 06 19.32	0.72	1.746	0.261	1.148	0.171	7.55	1.68	3.86	1.12	175.10	32.64	0.149	–	S
4315	23 17 21.65	0.61	-52 35 51.25	0.50	3.994	0.356	1.893	0.225	10.03	1.50	7.04	1.03	112.50	26.59	0.185	–	S
4316	23 17 10.08	0.91	-53 15 33.91	0.71	1.193	0.265	0.857	0.170	6.91	2.26	2.83	1.48	70.78	43.07	0.155	–	S
4317	23 17 31.30	0.73	-52 02 34.05	1.47	1.328	0.253	0.768	0.168	11.21	3.58	1.76	1.43	165.95	25.02	0.156	–	S
4318	23 14 56.70	0.46	-59 19 48.15	0.48	2.522	0.370	1.869	0.240	4.89	1.11	4.31	1.00	8.52	112.68	0.205	–	S
4319	23 16 41.88	0.81	-54 44 12.85	0.79	2.233	0.336	1.246	0.225	7.46	1.91	6.79	1.79	123.06	143.33	0.198	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4320	23 17 41.08	0.72	-51 24 22.10	0.84	3.174	0.373	1.583	0.248	10.65	2.24	5.72	1.28	143.65	26.04	0.216	–	S
4321	23 15 25.02	0.19	-58 09 46.85	0.20	6.105	0.455	5.196	0.341	4.24	0.33	1.96	0.28	156.69	17.81	0.180	–	S
4322	23 15 00.91	1.29	-59 01 04.69	0.98	5.106	0.356	1.159	0.192	17.30	3.09	11.87	2.13	118.02	31.33	0.185	–	S
4323	23 14 54.19	0.18	-59 16 42.45	0.18	8.081	0.569	7.177	0.449	3.04	0.26	2.50	0.24	54.93	69.90	0.208	–	S
4324	23 14 42.46	1.06	-59 42 59.31	1.03	2.604	0.278	1.027	0.185	13.59	3.06	5.94	1.48	139.02	22.75	0.169	–	S
4325	23 16 00.68	0.52	-56 31 22.72	0.54	1.062	0.293	1.080	0.175	0.00	1.23	0.00	1.17	0.00	153.41	0.165	–	S
4326	23 14 59.96	0.37	-58 54 31.15	0.31	4.310	0.421	2.962	0.278	6.62	0.81	3.89	0.64	74.07	26.29	0.211	–	S
4327	23 16 14.32	0.57	-55 43 23.23	0.30	58.985	3.428	12.468	0.917	19.00	1.34	7.46	0.52	167.23	5.35	0.609	–	M
4328	23 17 21.34	0.33	-52 12 44.98	0.33	3.047	0.295	2.164	0.196	5.47	0.72	4.91	0.67	119.44	71.65	0.146	–	S
4329	23 16 12.60	0.44	-55 42 16.96	0.82	54.664	3.076	8.956	0.747	27.01	1.99	11.17	0.77	163.87	8.74	0.648	–	S
4330	23 16 33.48	0.49	-54 43 37.88	0.96	3.600	0.321	1.485	0.202	13.43	2.24	5.90	1.08	178.32	17.60	0.177	–	S
4331	23 17 13.42	0.60	-52 33 45.91	0.67	9.515	0.589	2.457	0.258	15.54	1.67	12.10	1.22	146.78	24.03	0.216	–	S
4332	23 16 09.54	0.29	-55 51 48.14	0.30	4.830	0.467	3.627	0.314	5.27	0.66	3.86	0.57	41.37	42.32	0.229	–	S
4333	23 15 50.38	0.64	-56 42 42.78	0.55	1.231	0.286	1.063	0.178	4.16	1.49	1.86	1.22	76.21	76.74	0.163	–	S
4334	23 15 28.51	0.26	-57 37 11.02	0.27	6.522	0.446	3.690	0.272	7.02	0.54	6.78	0.49	166.90	66.81	0.167	–	S
4335	23 15 51.12	1.05	-56 38 37.37	0.57	1.938	0.274	1.067	0.182	10.74	2.48	3.35	1.19	79.48	22.38	0.163	–	S
4336	23 17 05.96	0.80	-52 56 56.69	0.78	1.787	0.419	1.327	0.269	5.17	1.92	4.33	1.75	119.28	154.02	0.244	–	S
4337	23 16 47.42	0.51	-53 55 41.43	0.82	2.586	0.304	1.419	0.199	10.68	2.00	3.76	0.99	23.69	19.25	0.173	–	S
4338	23 17 03.68	0.53	-53 00 09.75	0.61	6.759	0.552	2.887	0.338	10.51	1.46	8.27	1.13	156.58	35.66	0.277	–	S
4339	23 16 18.02	0.48	-55 20 07.34	0.61	2.472	0.349	1.669	0.228	6.99	1.45	3.87	1.02	163.70	33.24	0.196	–	S
4340	23 16 26.55	0.51	-54 54 10.16	0.55	4.292	0.521	2.699	0.342	7.96	1.41	4.23	0.95	42.53	27.40	0.288	–	S
4341	23 17 08.70	1.09	-52 38 42.67	0.88	1.964	0.291	0.968	0.199	9.34	2.62	7.09	2.00	96.99	60.07	0.177	–	S
4342	23 16 04.46	0.82	-55 54 37.65	0.78	1.789	0.331	1.135	0.219	6.82	2.00	5.27	1.71	58.05	96.57	0.195	–	S
4343	23 15 36.94	0.93	-57 06 05.38	1.10	1.524	0.226	0.795	0.151	11.71	3.10	2.87	1.27	145.59	21.66	0.139	–	S
4344	23 16 23.73	0.31	-54 54 01.61	0.19	70.368	3.943	25.096	1.412	21.81	0.65	8.71	0.25	169.95	2.34	0.297	-0.84	M
4345	23 17 09.23	1.19	-52 32 43.07	1.32	2.744	0.304	0.956	0.209	11.87	3.07	10.37	2.77	152.46	101.35	0.190	–	S
4346	23 15 46.25	0.53	-56 40 28.19	0.42	3.080	0.313	1.770	0.204	7.95	1.19	5.68	0.94	98.80	36.12	0.165	–	S
4347	23 16 05.96	0.16	-55 42 24.05	0.17	32.202	2.052	28.668	1.695	2.93	0.19	2.65	0.18	144.71	67.84	0.606	-0.07	S
4348	23 16 03.29	0.87	-55 50 13.51	0.82	1.483	0.342	1.041	0.222	5.65	2.03	4.71	1.88	119.86	153.85	0.201	–	S
4349	23 16 37.77	0.69	-54 08 04.08	1.05	1.271	0.271	0.851	0.177	7.67	2.47	3.37	1.57	9.33	41.75	0.161	–	S
4350	23 15 25.65	0.70	-57 25 25.45	1.11	3.437	0.294	1.156	0.185	13.81	2.63	8.50	1.59	179.04	25.78	0.166	–	S
4351	23 16 59.07	1.05	-52 55 30.75	0.82	1.463	0.302	0.920	0.200	7.59	2.52	4.75	1.83	83.38	57.19	0.180	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4352	23 17 04.52	2.35	-52 36 37.47	0.40	3.769	0.431	0.987	0.184	0.00	5.56	0.00	0.69	0.00	11.44	0.176	–	M
4353	23 16 34.92	0.55	-54 11 07.93	0.66	2.389	0.266	1.307	0.175	9.27	1.66	5.26	1.06	150.96	25.52	0.148	–	S
4354	23 14 53.24	0.70	-58 30 29.44	0.26	505.501	27.969	61.532	3.534	48.48	1.65	12.18	0.38	15.12	2.27	1.017	–	M
4355	23 15 12.39	0.64	-57 48 04.75	0.61	3.102	0.299	1.433	0.193	9.05	1.55	7.93	1.31	134.84	68.62	0.163	–	S
4356	23 16 18.19	0.45	-54 49 49.77	0.84	3.584	0.382	1.829	0.249	11.07	1.97	4.52	1.00	2.38	18.98	0.215	–	S
4357	23 16 31.58	1.52	-54 08 02.70	1.51	3.376	0.284	0.842	0.182	17.04	4.31	11.14	2.63	136.69	35.21	0.176	–	S
4358	23 15 16.17	0.58	-57 33 06.30	1.46	2.860	0.233	0.889	0.142	17.80	3.45	6.47	1.31	5.28	17.10	0.135	–	S
4359	23 16 22.88	0.15	-54 29 48.92	0.16	11.638	0.701	11.099	0.633	0.00	0.13	0.00	0.12	0.00	12.30	0.166	-0.14	S
4360	23 15 28.18	0.68	-56 54 14.27	0.75	1.201	0.244	0.857	0.158	5.61	1.78	4.37	1.53	15.16	102.64	0.142	–	S
4361	23 14 25.61	0.57	-59 16 55.35	0.49	33.975	1.952	6.540	0.460	19.57	1.55	9.65	0.72	146.08	6.94	0.286	–	M
4362	23 17 34.43	0.17	-50 15 01.16	0.18	7.662	0.543	7.247	0.446	2.48	0.25	1.31	0.22	145.08	39.01	0.198	–	S
4363	23 17 01.72	0.14	-52 10 01.43	0.15	24.420	1.379	23.765	1.320	1.89	0.07	0.46	0.06	173.96	15.64	0.180	-0.03	S
4364	23 15 32.61	0.75	-56 36 54.04	1.38	4.041	0.298	1.104	0.170	18.75	3.39	7.96	1.41	164.41	17.37	0.162	–	S
4365	23 16 58.83	0.28	-52 14 30.00	0.59	3.717	0.459	2.350	0.213	0.00	1.36	0.00	0.56	0.00	9.33	0.169	–	M
4366	23 15 42.75	0.16	-56 06 50.38	0.17	6.932	0.468	6.462	0.390	2.46	0.21	1.76	0.20	170.70	46.24	0.158	-0.14	S
4367	23 16 05.64	0.91	-55 02 56.47	0.73	2.064	0.310	1.135	0.209	8.35	2.15	6.11	1.66	88.61	59.66	0.184	–	S
4368	23 16 50.05	0.59	-52 43 28.12	0.70	3.624	0.343	1.661	0.221	10.13	1.69	7.52	1.25	153.73	36.09	0.186	–	S
4369	23 14 09.22	0.22	-59 46 21.22	0.23	5.901	0.478	4.725	0.339	4.32	0.42	3.37	0.38	178.11	35.87	0.208	–	S
4370	23 14 27.01	0.46	-59 06 56.95	0.41	2.673	0.324	1.842	0.213	6.06	1.05	4.44	0.88	73.43	57.13	0.175	–	S
4371	23 15 04.71	0.90	-57 38 29.41	0.99	1.492	0.264	0.854	0.176	9.21	2.68	4.28	1.60	40.31	35.42	0.159	–	S
4372	23 14 04.05	0.91	-59 53 30.21	1.42	5.395	0.370	1.234	0.194	20.44	3.60	9.25	1.61	27.04	18.37	0.191	–	S
4373	23 14 07.78	0.18	-59 45 59.24	0.20	6.861	0.517	5.983	0.392	3.75	0.32	1.92	0.28	11.58	21.91	0.207	–	S
4374	23 15 15.37	0.39	-57 10 29.54	0.53	2.813	0.270	1.575	0.174	8.47	1.20	5.44	0.86	3.56	24.99	0.140	–	S
4375	23 15 27.43	0.39	-56 32 38.46	1.69	8.686	0.752	2.497	0.252	0.00	4.03	0.00	0.33	0.00	4.81	0.211	–	M
4376	23 15 24.46	0.22	-56 45 59.32	0.21	7.307	0.524	4.420	0.291	6.31	0.46	0.00	0.26	150.15	6.21	0.160	–	M
4377	23 16 53.41	0.73	-52 22 03.51	0.75	1.425	0.254	0.935	0.167	6.35	1.78	5.44	1.64	50.29	159.95	0.148	–	S
4378	23 16 00.92	0.19	-55 01 43.10	0.19	7.181	0.521	6.133	0.395	3.53	0.30	3.06	0.28	132.70	59.45	0.199	–	S
4379	23 15 27.92	0.45	-56 29 36.03	1.13	7.646	0.474	1.863	0.205	22.37	2.68	7.35	0.87	172.57	11.16	0.190	–	S
4380	23 15 53.90	0.46	-55 17 38.09	0.22	6.672	0.570	3.470	0.279	0.00	1.05	0.00	0.34	0.00	5.76	0.204	–	M
4381	23 14 51.78	1.52	-57 54 39.81	1.20	7.348	0.432	0.944	0.145	23.10	3.57	18.12	2.78	109.05	38.23	0.161	–	S
4382	23 16 30.54	0.38	-53 21 30.55	0.35	3.636	0.378	2.536	0.250	5.97	0.86	4.64	0.73	81.32	47.56	0.194	–	S
4383	23 15 16.51	0.60	-56 50 21.04	0.83	2.443	0.263	1.162	0.174	10.39	2.01	6.17	1.27	165.57	27.03	0.150	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4384	23 16 58.92	0.60	-51 37 33.15	0.55	3.654	0.332	1.746	0.212	10.12	1.56	6.92	1.04	125.96	25.92	0.174	–	S
4385	23 13 46.30	0.24	-59 59 36.17	0.25	18.301	1.168	7.568	0.489	9.75	0.56	4.91	0.33	136.09	6.17	0.256	–	M
4386	23 14 51.06	0.41	-57 35 49.73	0.60	5.237	0.367	1.983	0.203	12.27	1.37	7.97	0.90	0.84	18.10	0.162	–	S
4387	23 17 09.88	0.53	-50 47 46.36	0.54	2.245	0.345	1.639	0.225	5.07	1.27	4.92	1.15	113.85	2.63	0.194	–	S
4388	23 13 51.96	0.72	-59 46 56.22	0.83	1.228	0.333	0.990	0.209	5.00	2.06	2.23	1.51	23.38	67.43	0.193	–	S
4389	23 15 24.23	0.79	-56 10 07.55	1.40	1.804	0.232	0.766	0.159	12.30	3.33	6.26	1.79	177.85	30.20	0.145	–	S
4390	23 13 59.13	0.24	-59 27 59.25	0.24	4.506	0.403	3.744	0.283	4.17	0.47	2.81	0.42	47.47	38.76	0.187	–	S
4391	23 15 49.17	0.24	-54 57 14.19	0.17	25.993	1.487	11.194	0.654	13.63	0.45	4.30	0.18	7.90	2.43	0.221	-0.81	M
4392	23 16 58.84	0.16	-51 18 16.45	0.17	15.102	0.908	11.403	0.669	5.06	0.20	4.29	0.18	40.67	29.99	0.219	-1.30	S
4393	23 16 23.00	1.95	-53 14 11.40	2.52	18.851	1.047	1.024	0.150	47.79	6.79	23.54	3.25	36.62	17.50	0.231	–	S
4394	23 14 37.69	0.71	-57 59 41.06	0.71	0.975	0.269	0.838	0.166	4.09	1.81	1.96	1.45	143.45	89.99	0.155	–	S
4395	23 14 55.68	0.58	-57 11 59.59	1.12	2.975	0.261	1.084	0.165	14.25	2.63	6.86	1.31	2.59	19.98	0.148	–	S
4396	23 14 20.78	0.25	-58 28 30.35	0.49	32.184	2.042	17.374	1.046	15.26	1.15	0.00	0.31	112.32	4.05	0.426	-0.77	M
4397	23 14 58.65	0.32	-56 59 51.75	0.57	6.860	0.452	2.627	0.235	14.40	1.33	5.99	0.61	17.20	10.82	0.179	–	S
4398	23 14 16.32	0.35	-58 37 41.88	0.36	7.762	0.821	5.526	0.543	5.68	0.83	4.21	0.69	149.83	39.94	0.423	–	S
4399	23 13 48.34	1.11	-59 37 39.80	0.95	3.153	0.398	1.345	0.273	10.77	2.80	7.36	1.95	128.66	45.60	0.244	–	S
4400	23 14 23.78	0.14	-58 16 00.88	0.15	98.751	5.477	73.961	4.078	6.07	0.05	0.17	0.03	143.40	0.80	0.292	-0.95	M
4401	23 16 10.96	0.15	-53 30 03.24	0.16	20.915	1.261	18.715	1.075	3.25	0.15	2.24	0.13	18.42	22.20	0.302	-0.49	S
4402	23 16 57.58	0.62	-50 53 25.57	0.62	2.793	0.353	1.659	0.233	8.41	1.66	5.15	1.14	52.47	34.28	0.199	–	S
4403	23 14 41.76	0.84	-57 26 26.87	0.51	6.512	0.413	1.712	0.190	16.98	1.92	9.92	1.15	98.27	16.93	0.165	–	S
4404	23 15 32.68	0.34	-55 16 52.76	0.39	5.881	0.502	3.438	0.322	7.47	0.87	5.97	0.72	0.69	37.05	0.240	–	S
4405	23 15 42.15	0.67	-54 44 05.56	1.59	2.629	0.274	0.963	0.183	15.68	3.76	5.91	1.53	2.02	21.44	0.171	–	S
4406	23 14 55.69	0.51	-56 42 44.83	0.47	5.739	0.405	2.257	0.226	12.31	1.31	7.53	0.86	52.79	17.87	0.178	–	S
4407	23 15 48.07	0.45	-54 17 35.69	0.48	2.686	0.332	1.855	0.217	7.10	1.21	3.46	0.83	43.52	26.72	0.180	–	S
4408	23 15 32.92	0.83	-54 59 24.92	0.60	1.580	0.300	1.099	0.195	7.01	1.96	3.33	1.33	81.76	40.72	0.174	–	S
4409	23 17 02.36	0.28	-50 09 46.06	0.31	6.259	0.525	4.247	0.348	6.05	0.62	5.35	0.60	15.07	148.29	0.241	–	S
4410	23 16 44.54	2.00	-51 08 50.37	1.83	4.850	0.325	0.834	0.167	25.98	6.07	11.73	2.38	131.90	21.69	0.181	–	S
4411	23 16 48.18	0.67	-50 55 34.53	0.81	1.166	0.303	0.962	0.189	4.64	1.78	2.83	1.64	173.76	108.23	0.175	–	S
4412	23 14 37.49	0.48	-57 12 16.39	0.50	2.192	0.262	1.407	0.172	7.34	1.28	4.27	0.91	143.99	28.76	0.144	–	S
4413	23 16 20.11	0.45	-52 24 24.29	0.46	2.022	0.280	1.509	0.183	5.44	1.08	4.02	0.95	52.96	67.82	0.154	–	S
4414	23 15 22.95	0.14	-55 11 57.74	0.15	55.047	3.045	53.770	2.964	1.58	0.03	0.78	0.03	65.42	13.47	0.190	-0.88	S
4415	23 16 04.98	1.61	-53 07 54.00	0.42	35.115	2.134	10.731	0.714	33.74	3.81	6.68	0.78	10.76	6.71	0.402	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4416	23 13 38.63	0.52	-59 18 29.00	0.58	2.448	0.308	1.486	0.203	6.83	1.39	5.68	1.13	2.50	61.87	0.172	–	S
4417	23 16 36.52	0.69	-51 24 48.20	0.77	2.416	0.309	1.305	0.206	8.71	1.90	6.38	1.43	145.55	47.14	0.178	–	S
4418	23 13 53.73	0.44	-58 44 54.37	0.51	4.524	0.568	3.022	0.372	6.58	1.20	4.35	0.93	21.02	37.94	0.312	–	S
4419	23 15 43.11	0.24	-54 11 21.95	0.39	9.740	0.588	3.938	0.281	14.52	0.89	5.27	0.37	162.12	7.61	0.173	–	S
4420	23 15 35.35	0.89	-54 34 07.87	1.10	1.543	0.263	0.839	0.178	9.41	2.83	5.15	1.74	152.24	39.13	0.160	–	S
4421	23 16 39.03	0.79	-51 12 33.19	0.98	1.734	0.327	1.086	0.216	8.13	2.45	4.40	1.61	152.11	43.43	0.194	–	S
4422	23 15 33.15	0.21	-54 36 22.23	0.23	4.817	0.404	4.095	0.292	4.04	0.42	2.57	0.37	173.64	32.06	0.179	–	S
4423	23 16 45.61	0.14	-50 40 36.39	0.16	71.540	4.046	42.217	2.355	9.47	0.15	0.96	0.07	74.35	1.23	0.391	-1.31	M
4424	23 15 30.26	1.86	-54 36 51.90	1.04	5.699	0.366	0.999	0.172	24.10	4.53	12.04	2.16	77.98	21.09	0.181	–	S
4425	23 15 40.08	0.39	-54 07 22.31	0.49	3.124	0.383	2.212	0.251	6.72	1.14	3.32	0.79	159.28	26.43	0.207	–	S
4426	23 15 32.51	0.31	-54 22 50.88	0.37	3.419	0.338	2.396	0.224	6.09	0.80	4.35	0.65	174.96	35.56	0.170	–	S
4427	23 14 28.85	0.89	-57 08 12.96	1.22	1.430	0.237	0.722	0.162	9.36	2.92	6.24	2.01	4.76	51.53	0.146	–	S
4428	23 15 20.23	0.92	-54 55 44.03	0.82	2.405	0.279	1.064	0.188	9.59	2.14	8.39	1.91	92.48	100.07	0.165	–	S
4429	23 15 03.41	0.75	-55 36 18.08	1.56	6.569	0.630	2.132	0.257	15.80	3.95	0.00	0.86	116.11	11.50	0.228	–	M
4430	23 15 43.87	0.17	-53 45 24.96	0.19	12.710	0.883	11.008	0.688	3.78	0.27	2.49	0.24	7.74	27.00	0.316	–	S
4431	23 15 15.67	0.17	-55 00 56.20	0.25	12.166	0.733	6.938	0.432	10.72	0.46	2.57	0.21	10.37	6.31	0.193	–	S
4432	23 16 04.61	0.91	-52 41 28.73	0.72	1.226	0.294	0.915	0.188	6.01	2.17	3.15	1.60	101.21	58.53	0.172	–	S
4433	23 16 34.71	0.45	-50 58 23.39	0.39	3.718	0.363	2.282	0.236	7.90	1.11	5.03	0.77	73.37	25.18	0.186	–	S
4434	23 16 40.97	0.15	-50 33 16.76	0.15	155.984	8.701	80.603	4.474	11.34	0.16	3.81	0.08	166.96	1.22	0.604	-0.88	M
4435	23 16 30.39	0.53	-51 12 02.34	0.72	6.489	0.455	2.334	0.249	15.90	1.89	6.64	0.83	35.59	13.00	0.207	–	S
4436	23 16 26.96	0.32	-51 22 30.28	0.35	3.941	0.354	2.617	0.233	6.41	0.77	5.22	0.65	145.32	42.91	0.171	–	S
4437	23 14 29.80	0.42	-56 54 31.45	0.42	2.524	0.265	1.607	0.174	5.99	0.93	5.96	0.92	40.43	93.18	0.139	–	S
4438	23 13 32.67	1.06	-58 59 29.80	0.92	3.706	0.352	1.293	0.231	12.58	2.64	8.94	1.93	58.65	43.66	0.208	–	S
4439	23 15 21.53	0.55	-54 37 38.63	0.52	1.479	0.295	1.255	0.186	4.51	1.36	1.80	1.06	127.08	53.87	0.167	–	S
4440	23 15 35.47	2.73	-53 52 07.35	0.85	75.000	4.318	28.543	1.660	61.61	6.67	7.19	0.77	18.87	6.01	0.539	-0.99	M
4441	23 15 43.99	0.87	-53 29 34.80	0.64	7.982	0.634	2.914	0.381	14.71	2.27	6.98	1.11	64.42	17.42	0.332	–	S
4442	23 13 45.83	0.79	-58 24 29.78	0.77	4.007	0.529	2.054	0.357	8.02	1.82	7.29	1.79	48.16	3.33	0.311	–	S
4443	23 14 56.81	0.44	-55 35 10.71	0.50	2.098	0.345	1.694	0.222	4.68	1.15	3.00	0.96	16.38	64.87	0.192	–	S
4444	23 16 05.82	0.63	-51 54 13.49	2.08	110.253	6.095	3.819	0.429	67.63	4.99	15.95	1.05	104.52	5.27	0.374	–	M
4445	23 16 15.39	0.48	-51 41 58.94	0.45	8.271	0.555	3.264	0.297	13.43	1.33	6.91	0.67	131.67	12.23	0.225	–	S
4446	23 15 46.94	0.49	-53 10 44.86	1.94	11.333	0.765	2.768	0.389	26.92	4.60	5.14	0.97	176.49	12.37	0.406	–	S
4447	23 16 14.43	1.03	-51 40 25.10	0.83	9.304	0.674	2.178	0.241	18.23	3.01	0.00	0.65	144.59	8.11	0.209	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4448	23 15 21.63	0.44	-54 21 58.54	0.43	3.836	0.359	2.225	0.232	8.39	1.13	5.16	0.77	134.76	22.55	0.183	-	S
4449	23 14 59.39	0.41	-55 16 02.41	0.42	2.754	0.340	1.997	0.224	5.33	0.95	4.50	0.88	34.88	102.94	0.183	-	S
4450	23 13 21.19	0.77	-59 03 54.77	0.71	1.666	0.325	1.130	0.212	5.79	1.71	4.99	1.70	83.34	3.41	0.190	-	S
4451	23 14 40.21	0.44	-56 03 46.76	0.43	2.381	0.329	1.801	0.215	5.11	1.05	3.85	0.89	133.93	64.35	0.180	-	S
4452	23 16 14.59	0.26	-51 29 52.92	0.29	3.793	0.337	2.860	0.229	5.28	0.60	4.03	0.51	149.66	39.13	0.158	-	S
4453	23 14 40.01	1.28	-55 58 42.19	0.91	15.767	0.909	2.096	0.268	23.97	3.00	17.10	2.11	91.42	24.28	0.284	-	S
4454	23 13 19.60	0.37	-58 59 57.19	0.45	9.336	0.584	3.202	0.277	12.66	1.04	9.07	0.76	23.36	17.17	0.202	-	S
4455	23 13 16.74	0.38	-59 05 58.44	0.34	2.509	0.370	2.237	0.239	4.40	0.88	0.00	0.66	58.66	29.87	0.201	-	S
4456	23 15 08.32	0.17	-54 40 23.17	0.18	8.308	0.558	7.411	0.451	2.99	0.22	2.58	0.22	43.04	84.82	0.187	-	S
4457	23 14 30.46	0.37	-56 18 00.65	0.39	3.385	0.309	2.056	0.201	6.63	0.86	6.12	0.78	164.14	81.03	0.153	-	S
4458	23 14 37.45	0.51	-55 59 22.50	0.30	15.783	1.036	4.995	0.396	11.54	1.16	5.41	0.62	7.39	9.75	0.285	-	M
4459	23 15 57.17	0.46	-52 12 26.93	0.58	2.128	0.273	1.399	0.179	6.95	1.31	4.80	1.04	6.00	47.79	0.151	-	S
4460	23 15 23.02	0.35	-53 54 08.56	0.42	7.799	0.869	5.537	0.573	6.27	0.96	3.90	0.73	163.49	31.65	0.456	-	S
4461	23 13 03.37	0.68	-59 23 15.98	0.59	1.483	0.277	1.078	0.179	5.85	1.63	3.59	1.25	124.66	57.37	0.159	-	S
4462	23 14 13.66	1.11	-56 48 47.22	1.18	1.990	0.286	0.868	0.199	9.31	2.75	8.69	2.59	177.94	175.54	0.178	-	S
4463	23 14 55.42	0.28	-55 01 40.65	0.31	8.543	0.575	4.341	0.334	8.61	0.66	7.13	0.55	3.36	27.92	0.215	-	S
4464	23 15 11.64	0.37	-54 16 12.14	0.45	2.548	0.302	1.824	0.198	6.35	1.04	3.58	0.76	162.57	29.76	0.161	-	S
4465	23 14 14.59	0.37	-56 42 21.59	0.44	4.242	0.406	2.582	0.264	7.37	1.00	5.24	0.77	165.06	29.95	0.207	-	S
4466	23 16 00.52	0.15	-51 48 20.91	0.16	13.215	0.794	11.727	0.673	3.42	0.15	2.29	0.13	138.61	17.61	0.187	-0.04	S
4467	23 15 53.20	1.41	-52 07 36.31	1.54	3.849	0.272	0.766	0.150	17.88	3.69	14.93	3.22	37.93	77.20	0.150	-	S
4468	23 15 34.07	0.51	-53 06 20.19	0.50	2.718	0.460	2.176	0.295	5.41	1.30	2.35	0.97	53.67	41.66	0.258	-	S
4469	23 15 31.00	0.38	-53 03 46.83	1.33	41.649	2.456	12.801	0.776	41.27	3.19	3.24	0.37	79.48	3.60	0.326	-	M
4470	23 15 53.06	1.13	-52 05 31.93	1.07	1.962	0.256	0.835	0.177	9.98	2.68	8.93	2.42	116.40	100.26	0.158	-	S
4471	23 13 48.80	0.38	-57 32 43.78	0.19	19.983	1.174	8.789	0.518	16.62	0.85	2.86	0.24	173.42	2.85	0.185	-0.81	M
4472	23 14 59.72	0.78	-54 34 48.54	0.30	13.696	0.848	3.254	0.262	19.11	1.84	4.24	0.52	13.49	5.81	0.192	-	M
4473	23 15 12.95	0.18	-53 55 29.24	0.27	57.800	3.389	24.203	1.416	12.87	0.55	1.97	0.20	70.95	2.80	0.484	-0.99	M
4474	23 15 52.86	0.14	-51 57 34.81	0.15	56.966	3.160	55.921	3.085	1.35	0.04	0.82	0.03	157.57	23.51	0.236	-0.46	S
4475	23 13 44.61	0.69	-57 36 55.75	1.01	1.891	0.239	0.935	0.160	10.94	2.52	4.83	1.31	160.17	24.37	0.143	-	S
4476	23 16 11.98	0.25	-50 51 33.96	0.28	7.509	0.544	4.765	0.352	6.94	0.56	5.53	0.46	152.05	28.02	0.218	-	S
4477	23 15 42.96	0.55	-52 25 17.11	1.09	4.073	0.311	1.336	0.182	16.15	2.56	7.71	1.23	179.90	17.89	0.162	-	S
4478	23 13 33.74	0.38	-57 57 19.95	0.41	3.013	0.328	2.048	0.216	6.08	0.94	4.64	0.78	157.99	42.90	0.172	-	S
4479	23 15 32.71	0.68	-52 51 55.54	0.53	1.656	0.296	1.230	0.190	6.41	1.65	2.74	1.12	77.78	37.10	0.169	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
4480	23 15 43.78	0.23	-52 12 46.90	0.22	5.029	0.379	3.771	0.264	5.45	0.46	3.82	0.37	117.32	22.16	0.155	–	S
4481	23 13 33.97	0.85	-57 50 51.21	0.60	7.290	0.450	1.794	0.194	19.39	2.16	9.09	1.01	123.38	13.39	0.172	–	S
4482	23 16 22.03	0.68	-50 04 01.05	1.51	6.112	0.474	1.759	0.282	19.14	3.58	8.04	1.51	10.27	19.04	0.265	–	S
4483	23 13 17.84	0.33	-58 22 24.10	0.35	4.432	0.522	3.528	0.346	4.51	0.77	3.38	0.66	22.60	59.26	0.274	–	S
4484	23 12 35.38	0.48	-59 45 57.71	0.47	6.779	0.518	2.968	0.309	10.08	1.16	7.63	0.93	46.60	30.86	0.243	–	S
4485	23 13 47.49	0.48	-57 15 31.78	0.82	1.796	0.267	1.138	0.175	8.69	1.93	2.68	1.05	11.15	23.50	0.155	–	S
4486	23 15 52.69	1.55	-51 37 25.39	1.74	4.456	0.297	0.812	0.150	23.95	5.07	11.95	2.25	141.09	21.90	0.157	–	S
4487	23 14 11.80	0.14	-56 17 19.51	0.15	17.084	0.985	16.056	0.900	2.50	0.09	1.32	0.09	150.36	15.75	0.171	0.29	S
4488	23 15 58.68	0.35	-51 14 39.80	0.32	4.616	0.391	2.886	0.254	7.12	0.81	5.50	0.63	92.17	29.27	0.184	–	S
4489	23 12 43.21	0.43	-59 29 05.31	0.36	2.816	0.371	2.178	0.243	5.33	0.96	3.03	0.77	79.75	41.94	0.201	–	S
4490	23 13 06.07	0.20	-58 40 34.80	0.21	8.474	0.571	5.995	0.392	5.35	0.34	4.69	0.31	173.35	31.37	0.199	–	S
4491	23 12 32.16	0.64	-59 46 17.78	0.62	5.747	0.470	2.349	0.287	12.60	1.76	6.37	1.01	47.09	18.59	0.242	–	S
4492	23 12 36.53	0.14	-59 35 19.96	0.15	35.388	1.994	32.017	1.780	2.86	0.07	2.20	0.07	90.65	20.50	0.253	-0.34	S
4493	23 15 52.56	0.49	-51 31 40.06	0.46	2.036	0.307	1.571	0.199	5.39	1.19	3.39	0.95	69.57	50.61	0.170	–	S
4494	23 15 44.32	0.60	-51 56 47.61	0.63	1.983	0.400	1.569	0.255	4.61	1.47	3.78	1.33	48.68	1.41	0.228	–	S
4495	23 13 09.91	1.13	-58 26 07.21	1.48	8.412	0.531	1.506	0.238	23.13	3.91	11.69	1.94	33.86	19.98	0.246	–	S
4496	23 15 47.57	0.94	-51 41 54.85	0.77	1.302	0.262	0.849	0.172	7.14	2.30	4.61	1.69	106.93	56.16	0.154	–	S
4497	23 15 53.96	0.59	-51 20 37.93	0.57	2.885	0.309	1.563	0.202	8.75	1.55	6.24	1.10	128.71	33.69	0.169	–	S
4498	23 16 09.05	0.71	-50 29 25.98	0.40	9.454	0.838	4.600	0.527	11.80	1.77	4.87	0.80	97.65	14.96	0.439	–	S
4499	23 15 04.64	0.62	-53 48 28.87	0.59	3.645	0.603	2.640	0.389	7.51	1.71	1.43	0.97	53.05	25.24	0.344	–	S
4500	23 14 29.63	0.32	-55 21 27.60	0.49	2.515	0.340	1.999	0.221	0.00	1.10	0.00	0.67	0.00	20.37	0.185	–	S
4501	23 15 38.80	0.17	-52 05 59.13	0.18	5.525	0.377	4.797	0.296	3.45	0.25	2.89	0.24	63.47	54.99	0.131	–	S
4502	23 15 44.00	0.93	-51 50 54.89	1.21	2.971	0.365	1.237	0.250	11.17	2.84	8.23	2.14	166.21	55.64	0.223	–	S
4503	23 15 52.50	0.68	-51 22 59.05	0.72	2.239	0.274	1.205	0.182	9.14	1.86	6.08	1.33	46.53	40.20	0.157	–	S
4504	23 13 13.70	0.53	-58 17 08.65	0.63	2.165	0.350	1.514	0.228	6.22	1.52	3.88	1.14	166.07	45.20	0.200	–	S
4505	23 15 06.68	0.41	-53 39 22.74	0.43	3.113	0.723	3.316	0.437	0.00	0.95	0.00	0.92	0.00	3.05	0.403	–	S
4506	23 16 05.82	1.25	-50 31 43.88	1.47	18.612	1.113	2.680	0.412	23.67	3.73	16.97	2.60	37.67	32.26	0.440	–	S
4507	23 14 13.66	0.23	-55 55 08.86	0.25	5.741	0.461	4.293	0.317	5.11	0.49	4.09	0.43	159.27	36.46	0.201	–	S
4508	23 15 23.85	0.77	-52 45 32.97	0.63	1.130	0.260	0.893	0.164	5.37	1.84	2.67	1.40	89.07	59.81	0.150	–	S
4509	23 15 15.81	0.58	-53 06 50.34	0.54	2.536	0.438	1.911	0.282	5.18	1.34	4.04	1.22	85.38	93.37	0.248	–	S
4510	23 15 20.44	1.72	-52 51 33.31	1.20	2.403	0.234	0.747	0.156	17.94	4.64	7.09	1.85	63.93	23.28	0.150	–	S
4511	23 15 34.46	0.31	-52 07 41.20	0.33	2.457	0.260	1.924	0.174	5.06	0.72	3.47	0.61	47.98	44.58	0.132	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
4512	23 14 40.35	0.83	-54 41 28.58	1.28	1.538	0.289	0.865	0.194	9.85	3.14	4.17	1.73	21.80	35.31	0.177	-	S
4513	23 14 44.52	0.30	-54 28 10.39	0.31	3.362	0.359	2.713	0.242	4.33	0.66	3.48	0.60	154.76	66.86	0.182	-	S
4514	23 15 25.08	0.87	-52 32 54.46	0.57	2.389	0.240	1.113	0.156	12.09	2.18	5.34	1.08	72.95	19.49	0.135	-	S
4515	23 12 41.87	0.15	-59 05 44.10	0.16	23.688	1.359	15.755	0.888	6.70	0.15	2.33	0.10	74.10	2.70	0.196	-0.72	M
4516	23 12 57.33	0.31	-58 36 48.13	0.39	3.627	0.378	2.570	0.250	6.23	0.86	3.58	0.65	0.99	25.38	0.194	-	S
4517	23 15 37.94	0.14	-51 47 18.41	0.15	32.986	1.836	31.439	1.737	2.03	0.05	1.57	0.04	164.50	22.23	0.163	-0.47	S
4518	23 13 54.16	0.67	-56 29 45.26	0.75	4.651	0.474	2.116	0.311	10.23	1.87	7.17	1.37	35.35	37.22	0.266	-	S
4519	23 14 01.49	0.58	-56 08 44.33	0.75	3.023	0.316	1.449	0.207	9.59	1.77	6.96	1.30	178.33	37.48	0.177	-	S
4520	23 15 35.95	0.61	-51 49 36.78	0.58	3.162	0.373	1.835	0.245	8.80	1.66	4.90	1.03	131.39	26.09	0.208	-	S
4521	23 15 48.15	0.26	-51 10 29.35	0.30	3.862	0.333	2.792	0.224	5.84	0.61	4.32	0.52	21.59	39.75	0.154	-	S
4522	23 15 46.36	0.89	-51 14 33.35	0.89	5.727	0.386	1.443	0.199	14.47	2.07	13.81	2.05	73.55	113.18	0.180	-	S
4523	23 14 36.24	0.77	-54 38 51.90	1.60	3.304	0.318	1.102	0.209	16.37	3.82	6.93	1.67	12.72	22.72	0.197	-	S
4524	23 14 24.68	0.34	-55 06 01.59	0.36	3.376	0.328	2.278	0.216	6.22	0.81	4.87	0.70	33.05	48.69	0.164	-	S
4525	23 15 46.38	0.53	-51 08 30.55	0.55	2.721	0.293	1.544	0.192	7.32	1.23	7.00	1.20	134.16	133.11	0.159	-	S
4526	23 14 03.06	1.15	-55 56 09.54	1.23	3.937	0.339	1.168	0.216	15.62	3.44	9.16	1.93	142.66	27.52	0.201	-	S
4527	23 14 06.68	0.24	-55 45 41.15	0.52	16.576	0.974	5.192	0.391	17.80	1.17	6.64	0.46	6.82	8.21	0.268	-	S
4528	23 15 53.48	0.43	-50 29 59.26	0.57	8.290	1.025	5.485	0.673	7.53	1.33	4.24	0.93	21.15	32.54	0.562	-	S
4529	23 12 46.41	0.17	-58 31 14.07	0.17	22.483	1.399	15.411	0.893	6.86	0.23	2.87	0.15	26.95	3.96	0.280	-1.31	M
4530	23 12 02.26	0.44	-59 55 07.61	0.46	2.515	0.299	1.668	0.196	6.37	1.10	4.68	0.90	35.56	46.75	0.162	-	S
4531	23 15 50.26	0.18	-50 28 50.08	0.18	23.678	1.672	21.434	1.334	3.32	0.27	1.82	0.23	70.48	25.89	0.611	-	S
4532	23 15 54.06	0.70	-50 11 11.35	0.78	2.149	0.643	1.928	0.392	3.25	1.81	2.33	1.61	178.58	2.89	0.369	-	S
4533	23 15 43.96	0.15	-50 39 32.84	0.16	39.445	2.246	24.574	1.383	7.43	0.14	5.26	0.12	2.93	5.23	0.293	0.07	M
4534	23 13 53.62	0.83	-55 52 29.94	0.72	1.172	0.303	0.925	0.191	5.11	1.98	2.98	1.61	72.35	87.11	0.176	-	S
4535	23 12 06.19	0.21	-59 39 13.11	0.21	6.610	0.532	5.620	0.389	4.00	0.38	2.40	0.33	132.62	27.92	0.228	-	S
4536	23 15 14.73	0.81	-52 13 25.89	1.18	1.546	0.257	0.825	0.174	9.44	2.75	5.81	1.88	178.16	48.28	0.156	-	S
4537	23 14 32.06	0.60	-54 10 27.74	0.76	1.750	0.510	1.607	0.309	0.00	1.77	0.00	1.36	0.00	66.20	0.291	-	S
4538	23 12 32.84	0.25	-58 43 59.36	0.29	5.092	0.421	3.562	0.281	6.40	0.61	3.67	0.46	20.03	18.99	0.190	-	S
4539	23 15 43.45	1.02	-50 30 00.51	1.25	43.021	2.768	14.862	0.989	28.11	3.70	4.59	0.71	131.55	6.96	0.556	-	M
4540	23 13 06.43	0.50	-57 32 42.07	0.66	2.946	0.269	1.374	0.171	10.32	1.59	6.48	1.05	163.27	23.88	0.143	-	S
4541	23 15 53.89	0.61	-50 01 42.92	0.65	1.875	0.518	1.766	0.314	2.70	1.53	1.06	1.37	138.97	161.14	0.295	-	S
4542	23 12 22.45	0.95	-59 02 19.79	0.68	2.092	0.274	1.044	0.185	9.48	2.19	6.25	1.58	98.40	45.23	0.162	-	S
4543	23 13 56.11	0.97	-55 37 02.55	1.11	5.779	0.393	1.328	0.205	16.36	2.78	12.90	2.06	153.70	36.77	0.193	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4544	23 15 24.31	0.46	-51 31 05.93	0.55	2.612	0.411	1.998	0.266	5.44	1.23	3.59	1.05	4.45	63.91	0.229	–	S
4545	23 13 19.67	0.86	-57 00 10.22	1.18	3.116	0.269	0.979	0.171	13.69	2.84	9.75	1.93	172.54	35.28	0.156	–	S
4546	23 11 56.02	0.57	-59 48 44.05	0.56	1.369	0.299	1.171	0.187	4.36	1.44	1.67	1.11	45.94	61.59	0.170	–	S
4547	23 11 57.49	0.14	-59 43 25.09	0.16	34.319	1.956	22.058	1.231	7.68	0.13	0.91	0.07	98.37	1.59	0.211	-0.68	M
4548	23 15 29.07	0.92	-51 12 32.53	0.92	3.182	0.325	1.254	0.216	10.28	2.20	10.05	2.07	117.24	147.71	0.190	–	S
4549	23 15 32.95	0.20	-50 59 10.78	0.22	4.413	0.380	4.088	0.284	3.35	0.40	0.65	0.33	30.66	28.42	0.170	–	S
4550	23 13 37.19	0.38	-56 15 12.69	0.40	1.552	0.314	1.598	0.194	0.00	0.89	0.00	0.80	0.00	101.09	0.174	–	S
4551	23 15 44.33	0.14	-50 18 39.71	0.15	338.877	19.308	322.939	18.006	0.00	0.09	0.00	0.07	0.00	7.86	2.923	0.60	S
4552	23 15 08.19	0.61	-52 14 04.28	1.13	2.907	0.283	1.171	0.185	13.66	2.66	6.51	1.35	9.90	22.41	0.164	–	S
4553	23 13 04.10	0.29	-57 27 33.18	0.27	4.081	0.364	2.981	0.245	5.49	0.61	4.08	0.53	78.25	40.94	0.172	–	S
4554	23 13 53.70	0.27	-55 32 59.96	0.34	5.139	0.430	3.351	0.281	7.17	0.73	4.35	0.54	1.36	20.03	0.199	–	S
4555	23 14 19.35	0.19	-54 28 15.06	0.17	9.272	0.647	6.509	0.404	0.00	0.30	0.00	0.19	0.00	5.58	0.187	–	M
4556	23 14 56.10	0.94	-52 47 15.64	0.74	2.062	0.279	1.075	0.187	10.21	2.42	5.32	1.42	66.91	30.41	0.165	–	S
4557	23 12 28.23	0.27	-58 35 50.41	0.28	10.417	0.736	4.972	0.351	8.44	0.69	1.82	0.37	51.03	7.17	0.220	–	M
4558	23 11 50.99	0.25	-59 46 50.22	0.25	6.817	0.483	4.266	0.310	7.22	0.53	4.73	0.41	139.50	16.75	0.188	–	S
4559	23 14 12.65	0.62	-54 39 20.89	0.58	2.894	0.402	1.812	0.266	6.61	1.44	5.76	1.31	110.59	101.74	0.228	–	S
4560	23 15 03.39	0.15	-52 17 49.78	0.16	19.838	1.141	17.382	0.977	4.06	0.11	1.71	0.09	65.89	8.59	0.195	-1.36	S
4561	23 13 42.59	0.43	-55 50 36.20	0.44	3.483	0.343	2.065	0.223	7.26	1.04	5.93	0.89	39.76	57.64	0.178	–	S
4562	23 15 19.53	0.26	-51 26 34.42	0.29	3.081	0.357	2.880	0.244	3.40	0.61	0.00	0.49	157.48	33.15	0.183	–	S
4563	23 14 34.61	0.47	-53 37 49.96	0.50	4.086	0.904	3.907	0.556	2.79	1.15	0.00	1.02	41.16	87.76	0.508	–	S
4564	23 15 04.18	0.76	-52 12 01.11	0.69	1.879	0.285	1.131	0.190	7.42	1.81	5.82	1.53	75.76	71.26	0.166	–	S
4565	23 13 15.00	0.53	-56 52 31.83	0.62	1.896	0.309	1.346	0.201	6.13	1.49	3.86	1.14	21.33	50.05	0.176	–	S
4566	23 12 37.96	0.14	-58 07 12.80	0.15	24.132	1.352	22.729	1.259	2.09	0.05	1.79	0.05	169.22	26.96	0.149	-0.32	S
4567	23 14 13.36	1.01	-54 24 09.90	0.39	26.238	1.495	3.364	0.290	19.27	2.36	6.57	0.84	179.61	8.78	0.224	–	M
4568	23 14 48.80	0.81	-52 47 59.54	0.71	4.205	0.314	1.418	0.181	15.20	2.23	7.96	1.17	56.69	18.39	0.158	–	S
4569	23 15 01.59	0.57	-52 08 33.32	0.74	1.888	0.281	1.190	0.185	7.47	1.71	5.00	1.31	178.81	50.68	0.161	–	S
4570	23 15 20.91	0.40	-51 08 35.30	0.45	3.137	0.379	2.248	0.249	6.15	1.04	4.15	0.84	32.60	46.71	0.204	–	S
4571	23 14 02.74	0.14	-54 43 44.71	0.15	80.931	4.494	73.322	4.043	3.26	0.04	2.17	0.03	114.97	3.86	0.284	-0.80	M
4572	23 13 41.26	0.42	-55 37 16.00	0.38	2.483	0.304	1.860	0.199	6.37	1.04	2.24	0.69	129.35	22.84	0.163	–	S
4573	23 12 56.66	0.14	-57 17 36.40	0.15	149.210	8.445	126.035	7.038	3.91	0.09	2.83	0.08	47.26	12.30	1.171	-0.85	S
4574	23 13 19.04	0.39	-56 26 54.65	0.54	11.297	0.831	4.810	0.483	10.94	1.23	7.50	0.85	178.38	20.89	0.376	–	S
4575	23 14 35.90	0.82	-53 08 48.01	0.96	1.515	0.328	1.004	0.215	6.49	2.16	5.05	1.95	179.06	115.88	0.194	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4576	23 14 48.91	0.47	-52 28 01.42	0.48	2.935	0.296	1.692	0.193	7.26	1.11	6.66	1.04	134.18	85.34	0.156	–	S
4577	23 11 54.44	1.03	-59 14 03.79	0.59	2.187	0.274	1.085	0.183	10.98	2.36	4.90	1.33	82.44	26.39	0.162	–	S
4578	23 12 00.32	0.45	-59 01 53.44	0.46	2.102	0.303	1.575	0.197	4.78	1.07	4.23	0.96	166.34	111.50	0.167	–	S
4579	23 15 00.92	1.12	-51 48 35.78	1.14	3.905	0.493	1.595	0.206	14.29	3.63	0.00	0.87	137.42	12.19	0.187	–	M
4580	23 14 43.53	0.21	-52 38 55.25	0.22	5.867	0.422	4.328	0.294	5.61	0.41	4.06	0.35	41.88	25.92	0.163	–	S
4581	23 13 50.06	0.58	-54 58 51.05	0.94	2.554	0.288	1.217	0.191	10.88	2.21	5.92	1.31	4.10	26.92	0.167	–	S
4582	23 14 00.61	0.36	-54 32 15.30	0.41	3.006	0.465	2.680	0.299	3.74	0.91	1.42	0.75	167.08	52.16	0.254	–	S
4583	23 15 11.59	0.14	-51 10 07.50	0.15	47.411	2.634	45.468	2.510	1.93	0.04	1.41	0.04	86.35	16.96	0.214	-0.59	S
4584	23 13 12.33	0.72	-56 25 54.28	0.40	28.396	1.784	6.645	0.576	14.16	1.69	6.53	0.81	171.70	10.43	0.445	–	M
4585	23 12 16.19	0.55	-58 22 42.43	0.91	4.337	0.481	1.770	0.207	11.03	2.36	0.00	0.68	65.73	10.73	0.183	–	M
4586	23 13 26.23	0.51	-55 52 20.23	0.60	2.799	0.306	1.550	0.201	7.99	1.40	6.27	1.12	179.19	48.13	0.168	–	S
4587	23 13 20.69	0.24	-56 03 51.65	0.19	17.103	1.100	10.722	0.649	10.16	0.49	0.00	0.21	161.34	3.32	0.271	–	M
4588	23 14 53.07	0.70	-51 59 35.40	0.69	1.806	0.277	1.120	0.184	6.65	1.67	6.12	1.53	79.41	171.73	0.160	–	S
4589	23 15 16.97	1.86	-50 46 35.59	1.13	4.290	0.353	1.051	0.222	18.15	4.64	11.08	2.48	92.47	30.43	0.217	–	S
4590	23 15 28.72	0.88	-50 05 16.46	1.05	3.984	0.432	1.611	0.291	10.98	2.28	9.15	2.19	2.92	106.80	0.256	–	S
4591	23 14 57.67	0.67	-51 35 45.64	0.65	1.561	0.252	1.037	0.165	6.46	1.63	5.09	1.38	123.18	70.33	0.145	–	S
4592	23 14 32.26	0.31	-52 43 00.83	0.39	21.970	1.318	10.554	0.621	17.83	1.03	1.05	0.26	55.92	3.16	0.221	-0.94	M
4593	23 13 04.20	0.59	-56 25 16.49	0.23	59.350	3.544	21.436	1.281	33.16	1.40	3.19	0.20	19.12	1.99	0.501	–	M
4594	23 13 30.93	0.32	-55 26 42.91	0.38	2.449	0.306	2.006	0.202	4.77	0.83	2.51	0.66	15.98	37.83	0.162	–	S
4595	23 15 13.15	0.75	-50 43 20.50	0.87	1.897	0.404	1.330	0.262	6.43	2.00	4.32	1.73	33.11	84.22	0.236	–	S
4596	23 15 03.51	0.30	-51 07 49.86	0.41	5.190	0.461	3.303	0.300	8.12	0.92	4.24	0.60	19.91	19.35	0.224	–	S
4597	23 14 33.66	0.77	-52 38 40.30	0.72	1.332	0.277	0.966	0.178	6.62	2.02	3.13	1.40	58.16	46.94	0.161	–	S
4598	23 14 30.31	1.16	-52 45 09.27	0.95	3.274	0.301	1.110	0.196	14.47	3.08	8.47	1.77	62.94	28.53	0.178	–	S
4599	23 11 43.30	0.18	-59 05 02.90	0.18	5.804	0.433	5.356	0.342	3.00	0.28	1.29	0.25	57.71	29.53	0.170	–	S
4600	23 15 06.24	0.62	-50 53 08.36	0.55	3.417	0.345	1.753	0.224	8.72	1.49	7.24	1.18	104.17	45.51	0.187	–	S
4601	23 13 42.07	0.57	-54 46 12.37	0.54	1.675	0.327	1.359	0.208	4.29	1.30	3.42	1.24	76.17	153.21	0.185	–	S
4602	23 11 20.02	0.31	-59 38 09.85	0.33	4.016	0.348	2.620	0.228	6.85	0.73	4.45	0.58	35.11	24.15	0.165	–	S
4603	23 13 27.01	0.44	-55 10 33.97	0.61	2.903	0.315	1.676	0.206	8.89	1.44	4.70	0.92	18.70	24.03	0.171	–	S
4604	23 13 13.22	0.27	-55 42 53.82	0.29	4.299	0.383	3.160	0.258	5.70	0.63	3.72	0.50	154.38	26.01	0.181	–	S
4605	23 14 21.48	0.84	-52 49 39.65	0.64	3.456	0.301	1.368	0.189	12.81	2.14	7.40	1.25	69.43	23.09	0.163	–	S
4606	23 11 54.84	0.57	-58 27 18.28	0.49	2.168	0.387	1.700	0.248	4.77	1.29	3.43	1.11	100.01	94.47	0.219	–	S
4607	23 11 57.97	0.31	-58 20 35.41	0.35	4.177	0.371	2.727	0.243	7.06	0.80	4.18	0.58	155.48	20.71	0.179	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4608	23 14 29.70	0.98	-52 24 23.51	0.87	1.354	0.250	0.799	0.168	7.42	2.28	6.10	2.01	93.35	97.27	0.149	–	S
4609	23 14 38.14	0.21	-51 56 24.60	0.23	5.431	0.416	4.348	0.299	4.63	0.41	3.48	0.35	163.32	34.66	0.171	–	S
4610	23 11 54.14	0.15	-58 14 19.07	0.16	13.062	0.804	11.914	0.689	2.72	0.15	2.15	0.14	84.75	47.74	0.210	-0.70	S
4611	23 13 40.20	0.40	-54 17 40.40	0.39	5.035	0.424	2.846	0.269	8.91	1.03	5.03	0.66	134.11	17.95	0.204	–	S
4612	23 11 38.76	0.38	-58 33 53.08	1.19	92.144	5.135	21.135	1.219	38.60	2.81	10.21	0.73	85.30	5.02	0.367	-0.90	M
4613	23 13 05.00	0.19	-55 36 25.60	0.21	6.441	0.485	5.382	0.359	4.29	0.36	2.60	0.30	153.14	23.11	0.195	–	S
4614	23 11 00.85	0.14	-59 45 38.92	0.15	17.496	1.010	16.657	0.934	2.00	0.09	1.47	0.09	36.61	34.55	0.178	-0.47	S
4615	23 14 33.80	0.39	-51 42 28.22	0.44	2.772	0.322	1.947	0.212	6.12	1.02	4.47	0.83	152.20	45.74	0.172	–	S
4616	23 12 34.64	0.17	-56 39 25.13	0.18	10.525	0.737	9.628	0.595	3.07	0.25	1.60	0.22	42.55	27.88	0.266	–	S
4617	23 12 19.47	0.17	-57 06 15.71	0.19	8.648	0.540	6.261	0.381	6.43	0.28	3.05	0.21	25.75	9.92	0.154	-0.98	S
4618	23 11 43.38	0.99	-58 18 42.91	0.77	1.515	0.319	0.985	0.209	7.26	2.39	4.15	1.67	116.85	54.39	0.189	–	S
4619	23 11 55.08	0.61	-57 56 03.10	1.48	1.815	0.229	0.802	0.154	13.64	3.52	3.97	1.36	7.49	21.55	0.144	–	S
4620	23 10 56.67	0.22	-59 40 06.37	0.24	5.757	0.447	4.292	0.309	5.31	0.45	3.70	0.39	23.32	24.75	0.189	–	S
4621	23 10 58.71	0.79	-59 36 43.13	0.65	1.261	0.305	0.992	0.192	5.40	1.90	2.51	1.41	69.21	63.73	0.176	–	S
4622	23 10 58.23	0.45	-59 34 03.90	0.54	1.950	0.292	1.434	0.189	6.18	1.31	2.68	0.91	160.93	30.87	0.164	–	S
4623	23 10 51.81	0.40	-59 44 36.42	0.35	4.994	0.423	2.840	0.269	7.98	0.90	5.56	0.71	128.11	26.28	0.203	–	S
4624	23 11 34.91	0.15	-58 23 10.82	0.16	13.852	0.824	12.638	0.720	2.80	0.12	1.98	0.12	149.93	22.39	0.182	-1.04	S
4625	23 11 11.82	0.38	-59 04 04.12	0.51	3.815	0.332	1.995	0.210	8.98	1.16	5.86	0.82	9.27	23.03	0.166	–	S
4626	23 14 26.00	0.14	-51 36 54.09	0.15	15.924	0.911	14.889	0.832	2.69	0.09	1.48	0.08	161.72	14.88	0.145	-0.78	S
4627	23 13 06.50	0.14	-55 04 07.09	0.15	99.816	5.499	97.739	5.379	1.28	0.02	1.04	0.02	84.14	22.51	0.187	0.36	S
4628	23 14 30.25	0.34	-51 23 45.83	0.31	4.724	0.417	3.117	0.274	6.62	0.78	5.06	0.61	97.13	31.12	0.200	–	S
4629	23 12 53.75	0.51	-55 34 23.50	0.81	2.885	0.336	1.534	0.222	9.77	1.89	5.09	1.13	178.35	25.50	0.191	–	S
4630	23 13 19.38	0.83	-54 34 00.78	0.68	1.056	0.333	0.954	0.202	0.00	1.95	0.00	1.53	0.00	77.21	0.191	–	S
4631	23 13 21.24	0.14	-54 23 33.90	0.17	158.060	8.751	85.208	4.699	17.70	0.20	3.21	0.06	107.09	0.66	0.344	-0.94	M
4632	23 12 17.46	0.74	-56 53 41.51	0.79	1.475	0.307	1.039	0.199	6.49	2.06	3.50	1.45	145.97	49.91	0.179	–	S
4633	23 12 35.86	0.21	-56 09 31.25	0.17	45.890	2.688	23.252	1.355	12.00	0.39	4.19	0.18	21.86	2.64	0.446	-1.21	M
4634	23 14 16.07	1.66	-51 57 31.33	1.24	10.944	0.627	1.222	0.172	29.61	4.39	17.56	2.28	119.66	18.91	0.200	–	S
4635	23 12 34.10	0.28	-56 10 25.11	0.39	23.023	1.394	8.391	0.639	12.98	0.87	8.14	0.56	15.16	12.47	0.418	–	S
4636	23 13 07.57	0.15	-54 50 45.96	0.16	11.847	0.717	11.240	0.643	2.50	0.14	0.80	0.12	121.85	18.60	0.174	0.01	S
4637	23 14 28.99	0.14	-51 11 21.10	0.15	63.823	3.554	52.220	2.884	4.96	0.05	2.30	0.04	25.96	2.11	0.264	-0.76	M
4638	23 14 12.65	0.17	-51 56 46.50	0.18	9.325	0.616	8.155	0.493	3.28	0.22	2.90	0.22	35.05	21.61	0.199	-0.13	S
4639	23 12 39.03	0.43	-55 51 52.28	0.50	2.363	0.297	1.614	0.195	6.42	1.17	4.36	0.92	22.95	43.60	0.163	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4640	23 13 47.13	0.15	-53 01 24.97	0.16	12.249	0.734	10.557	0.607	4.82	0.17	0.00	0.12	61.87	8.18	0.171	-0.73	S
4641	23 10 38.11	0.56	-59 43 53.54	0.73	2.612	0.358	1.550	0.237	8.16	1.76	4.56	1.18	20.43	32.12	0.206	-	S
4642	23 14 03.85	0.41	-52 09 03.48	0.48	36.151	2.083	9.864	0.597	18.18	1.21	10.68	0.71	59.00	8.16	0.249	-	M
4643	23 13 56.17	0.37	-52 32 10.18	0.36	6.899	0.515	3.574	0.313	9.50	0.92	6.21	0.64	55.60	19.72	0.225	-	S
4644	23 10 45.91	0.89	-59 27 42.49	0.77	1.331	0.246	0.815	0.163	6.82	1.99	5.60	1.86	98.93	144.44	0.145	-	S
4645	23 13 55.03	0.20	-52 32 38.82	0.21	18.081	1.098	8.300	0.509	9.88	0.41	5.56	0.27	52.67	5.74	0.225	-	M
4646	23 12 23.75	0.19	-56 15 30.40	0.21	7.431	0.631	7.153	0.484	0.00	0.34	0.00	0.30	0.00	30.17	0.279	-	S
4647	23 14 39.26	0.15	-50 23 59.03	0.16	33.618	1.956	31.593	1.778	2.34	0.10	1.83	0.10	168.74	42.39	0.370	-0.69	S
4648	23 13 26.96	0.14	-53 43 29.19	0.15	1252.797	69.135	1241.332	68.352	0.00	0.02	0.00	0.02	0.00	8.80	3.266	-0.50	S
4649	23 14 06.86	0.80	-51 53 40.53	0.83	3.154	0.303	1.292	0.197	11.69	2.25	7.92	1.45	137.96	30.85	0.171	-	S
4650	23 12 45.78	0.21	-55 17 06.16	0.20	9.340	0.651	7.049	0.462	6.06	0.38	2.78	0.28	68.80	13.17	0.239	-	S
4651	23 13 52.64	0.70	-52 32 58.74	0.82	2.600	0.386	1.494	0.258	7.78	1.86	6.22	1.66	10.49	90.78	0.226	-	S
4652	23 13 55.58	0.21	-52 24 02.76	0.21	4.451	0.365	3.921	0.270	3.54	0.39	2.32	0.34	92.52	37.17	0.158	-	S
4653	23 12 06.77	1.64	-56 43 50.43	1.58	6.808	0.462	1.257	0.241	22.20	4.76	11.99	2.40	137.73	24.92	0.251	-	S
4654	23 12 46.80	1.47	-55 15 14.42	0.86	9.284	0.572	1.729	0.239	25.03	3.70	10.37	1.49	70.81	15.92	0.243	-	S
4655	23 12 01.84	0.17	-56 52 19.74	0.17	15.208	0.940	10.241	0.598	5.14	0.21	3.38	0.17	165.52	8.88	0.200	-0.67	M
4656	23 11 45.98	1.14	-57 24 47.31	0.98	2.201	0.262	0.877	0.180	10.50	2.68	8.92	2.28	105.11	100.91	0.161	-	S
4657	23 13 23.70	0.98	-53 44 24.61	0.49	11.270	1.984	5.888	0.862	0.00	2.51	0.00	0.36	0.00	7.36	0.798	-	M
4658	23 10 31.31	0.19	-59 41 46.94	0.19	7.085	0.533	6.428	0.415	3.28	0.29	1.52	0.26	66.59	28.25	0.212	-	S
4659	23 11 02.02	0.63	-58 47 51.58	0.93	2.135	0.277	1.089	0.185	9.54	2.21	5.70	1.42	3.74	33.00	0.163	-	S
4660	23 11 46.73	0.22	-57 19 11.16	0.27	5.886	0.426	3.847	0.279	7.01	0.53	4.32	0.40	3.61	16.16	0.170	-	S
4661	23 11 24.39	0.31	-58 01 08.35	0.32	4.295	0.358	2.730	0.233	7.04	0.73	4.76	0.57	143.25	23.10	0.166	-	S
4662	23 14 01.99	0.46	-51 56 21.44	0.46	4.459	0.388	2.383	0.246	9.65	1.26	5.45	0.76	135.79	18.74	0.194	-	S
4663	23 10 28.51	0.14	-59 41 11.61	0.15	53.196	2.946	51.882	2.861	1.60	0.03	0.72	0.03	34.48	103.58	0.201	1.17	S
4664	23 11 21.89	0.55	-58 04 44.35	0.69	2.788	0.306	1.437	0.202	8.74	1.63	6.46	1.23	7.84	39.97	0.171	-	S
4665	23 11 00.91	0.73	-58 42 10.50	0.39	19.195	1.148	4.153	0.328	19.67	1.80	6.23	0.59	25.19	6.01	0.235	-	M
4666	23 12 42.62	1.41	-55 15 34.41	1.29	3.769	0.384	1.232	0.259	15.83	4.02	7.65	2.00	52.85	28.17	0.243	-	S
4667	23 13 19.42	1.13	-53 43 18.73	0.30	29.517	1.827	9.318	0.808	26.64	2.72	0.00	0.34	103.72	7.49	0.757	-	S
4668	23 10 28.15	0.15	-59 40 24.05	0.16	12.560	0.776	12.156	0.700	1.99	0.14	0.50	0.13	54.84	28.41	0.204	-0.18	S
4669	23 13 01.79	0.75	-54 29 18.97	0.84	1.583	0.296	1.024	0.195	7.26	2.10	4.56	1.57	36.51	57.48	0.174	-	S
4670	23 14 26.05	0.86	-50 39 21.55	0.77	2.131	0.374	1.324	0.248	7.74	2.18	5.05	1.60	67.70	53.16	0.220	-	S
4671	23 13 21.56	0.16	-53 35 32.44	0.16	22.564	1.419	21.505	1.250	2.77	0.17	0.00	0.14	60.27	16.30	0.399	-0.93	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
4672	23 14 05.43	0.64	-51 38 39.38	1.13	1.414	0.253	0.857	0.167	9.31	2.64	3.70	1.47	4.37	32.70	0.151	-	S
4673	23 11 24.81	0.41	-57 53 53.72	0.43	1.784	0.288	1.522	0.184	3.88	1.00	2.54	0.85	24.46	78.15	0.159	-	S
4674	23 12 46.54	0.15	-54 58 19.74	0.16	15.021	0.877	13.617	0.769	2.69	0.11	2.44	0.11	5.37	61.25	0.172	-0.40	S
4675	23 14 36.21	0.59	-50 00 03.34	0.65	1.455	0.368	1.315	0.226	2.98	1.50	2.40	1.35	152.89	3.15	0.210	-	S
4676	23 12 21.01	0.95	-55 52 23.62	1.28	3.659	0.348	1.220	0.230	14.06	3.23	8.59	1.90	158.79	30.63	0.210	-	S
4677	23 10 14.28	1.39	-59 53 43.18	0.67	4.034	0.309	1.141	0.182	17.93	3.16	7.88	1.53	85.28	20.65	0.171	-	S
4678	23 13 44.45	0.64	-52 27 31.68	0.69	1.597	0.345	1.270	0.218	5.96	1.81	1.63	1.22	45.01	41.99	0.198	-	S
4679	23 10 28.12	1.03	-59 30 15.37	1.21	1.691	0.243	0.745	0.169	9.89	3.04	7.65	2.19	164.54	61.52	0.151	-	S
4680	23 12 25.52	0.38	-55 39 39.39	0.37	3.629	0.362	2.399	0.238	6.44	0.89	4.91	0.73	132.95	39.34	0.185	-	S
4681	23 10 52.19	0.36	-58 45 45.40	0.33	3.724	0.388	2.667	0.257	6.01	0.82	3.72	0.65	127.14	30.13	0.199	-	S
4682	23 12 37.84	0.15	-55 04 23.25	0.16	22.245	1.316	18.224	1.027	0.00	0.13	0.00	0.09	0.00	3.61	0.223	-0.59	M
4683	23 10 37.55	1.98	-59 05 08.21	1.67	7.951	0.725	5.216	0.373	26.81	6.01	0.00	0.83	43.89	9.51	0.238	-	M
4684	23 10 45.74	0.61	-58 51 55.11	0.93	2.791	0.272	1.155	0.177	11.53	2.21	7.10	1.38	5.94	27.40	0.155	-	S
4685	23 13 59.13	0.65	-51 36 44.94	0.67	1.711	0.301	1.199	0.196	6.04	1.62	4.57	1.39	134.91	73.71	0.173	-	S
4686	23 11 53.67	0.20	-56 39 49.94	0.20	9.209	0.740	8.347	0.561	2.97	0.34	2.07	0.31	39.98	55.35	0.314	-	S
4687	23 12 30.12	0.53	-55 20 32.30	0.64	2.662	0.321	1.544	0.212	7.80	1.49	5.77	1.17	11.31	48.01	0.180	-	S
4688	23 13 05.01	0.16	-53 54 14.48	0.16	22.654	1.418	20.736	1.209	2.89	0.17	1.90	0.16	117.58	25.79	0.394	-1.51	S
4689	23 14 28.98	0.15	-50 01 53.44	0.16	15.038	0.907	13.467	0.774	2.93	0.15	2.72	0.14	50.83	151.72	0.218	-0.41	S
4690	23 13 39.14	0.34	-52 25 13.69	0.36	3.030	0.351	2.366	0.232	4.71	0.75	3.91	0.74	31.14	113.56	0.183	-	S
4691	23 13 20.58	1.10	-53 08 52.59	0.79	2.000	0.306	1.037	0.207	9.49	2.66	6.05	1.76	98.76	43.56	0.185	-	S
4692	23 12 32.48	0.15	-55 03 50.55	0.16	14.543	0.898	13.610	0.786	2.54	0.15	1.57	0.14	39.37	30.25	0.237	0.40	S
4693	23 13 37.86	0.64	-52 19 39.70	0.59	8.385	0.517	2.205	0.224	16.13	1.71	11.27	1.08	129.13	18.07	0.187	-	S
4694	23 12 19.18	0.78	-55 33 19.52	0.75	1.304	0.287	0.942	0.185	5.10	1.79	4.79	1.75	94.20	3.62	0.167	-	S
4695	23 10 39.63	0.77	-58 50 47.19	0.62	2.030	0.288	1.172	0.192	7.77	1.79	5.65	1.41	83.27	64.02	0.167	-	S
4696	23 13 34.19	0.21	-52 27 54.79	0.18	16.053	0.939	8.553	0.519	10.45	0.39	4.59	0.21	84.96	6.97	0.207	-1.12	S
4697	23 11 08.11	0.91	-57 57 40.96	1.24	1.886	0.240	0.791	0.165	11.18	3.04	7.31	1.96	166.88	40.16	0.148	-	S
4698	23 14 01.24	0.27	-51 12 43.68	0.30	6.424	0.614	5.046	0.418	4.78	0.59	3.80	0.56	29.29	72.64	0.298	-	S
4699	23 12 14.87	1.15	-55 37 03.04	0.87	11.092	0.739	2.043	0.237	18.08	3.09	7.38	1.31	36.62	14.09	0.208	-	M
4700	23 12 44.63	0.30	-54 30 51.97	0.33	4.585	0.385	2.961	0.252	7.04	0.74	4.74	0.56	147.63	23.15	0.179	-	S
4701	23 12 51.84	0.72	-54 13 43.00	0.80	7.292	0.521	2.258	0.289	14.69	2.14	9.48	1.31	145.06	21.98	0.252	-	S
4702	23 14 03.67	0.14	-51 01 54.00	0.15	51.721	2.880	45.578	2.521	3.85	0.06	1.87	0.05	143.30	6.52	0.263	-1.05	S
4703	23 12 29.54	0.15	-55 03 39.32	0.16	23.868	1.374	20.278	1.142	3.66	0.11	3.06	0.10	63.42	25.84	0.238	-0.93	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
4704	23 14 21.90	1.09	-50 05 47.83	0.97	7.420	0.484	1.773	0.234	21.18	3.28	9.37	1.26	130.68	15.13	0.223	-	S
4705	23 13 20.35	0.49	-52 58 53.98	0.64	1.487	0.268	1.153	0.171	5.84	1.51	2.51	1.07	166.24	40.85	0.152	-	S
4706	23 13 19.34	0.17	-52 58 25.21	0.17	6.872	0.458	6.206	0.375	3.40	0.23	1.68	0.20	74.25	20.86	0.151	-0.60	S
4707	23 13 40.42	0.31	-52 02 38.68	0.36	3.370	0.334	2.441	0.223	6.33	0.81	3.66	0.60	32.59	27.54	0.168	-	S
4708	23 10 11.55	0.98	-59 30 39.31	0.80	1.695	0.278	0.928	0.188	8.09	2.31	6.14	1.83	98.35	86.27	0.166	-	S
4709	23 11 56.97	0.16	-56 04 33.74	0.18	15.271	0.941	11.762	0.699	5.41	0.23	3.04	0.18	163.98	11.30	0.252	-0.91	S
4710	23 10 50.12	1.22	-58 14 06.62	0.64	6.802	0.627	2.559	0.402	15.31	2.92	5.46	1.21	112.95	18.70	0.368	-	S
4711	23 14 02.74	0.15	-50 48 44.01	0.16	24.295	1.441	19.840	1.115	6.24	0.14	0.00	0.09	152.19	2.26	0.230	0.12	M
4712	23 10 10.84	0.84	-59 26 05.29	0.90	1.113	0.261	0.768	0.170	6.11	2.29	4.29	1.77	31.36	88.27	0.154	-	S
4713	23 11 17.65	0.16	-57 22 54.85	0.18	13.371	0.804	9.222	0.549	6.50	0.25	3.89	0.19	3.14	10.19	0.198	-1.17	S
4714	23 10 47.61	0.59	-58 19 41.49	0.56	3.406	0.712	2.809	0.449	4.23	1.41	2.90	1.20	133.32	98.61	0.405	-	S
4715	23 14 09.51	0.20	-50 26 23.86	0.21	11.711	0.789	8.419	0.547	5.98	0.39	4.18	0.29	120.80	16.31	0.274	-	S
4716	23 09 52.34	0.59	-59 53 56.95	0.80	1.557	0.272	1.029	0.178	7.26	1.93	3.57	1.28	17.60	36.99	0.158	-	S
4717	23 14 13.85	0.32	-50 11 14.11	0.31	5.967	0.603	4.609	0.406	5.00	0.71	3.86	0.59	107.72	42.82	0.301	-	S
4718	23 12 50.28	0.75	-53 55 49.65	0.66	16.586	1.027	3.993	0.445	15.98	1.86	12.70	1.37	121.31	26.60	0.388	-	S
4719	23 13 34.31	0.14	-52 00 06.72	0.15	38.512	2.145	36.819	2.035	1.97	0.05	1.50	0.04	159.26	21.51	0.194	-0.11	S
4720	23 13 58.64	0.51	-50 53 01.12	0.67	4.110	0.436	2.205	0.286	9.08	1.55	6.23	1.12	168.10	36.21	0.239	-	S
4721	23 14 01.59	0.83	-50 42 20.06	0.72	1.454	0.360	1.139	0.227	5.33	2.00	3.02	1.60	104.01	69.74	0.209	-	S
4722	23 11 03.41	0.20	-57 41 21.29	0.20	5.435	0.428	4.811	0.322	3.35	0.34	2.28	0.30	56.25	44.65	0.179	-	S
4723	23 11 18.52	0.48	-57 10 59.91	0.72	4.448	0.376	1.915	0.234	11.81	1.71	6.44	1.00	19.53	20.07	0.196	-	S
4724	23 12 25.38	0.41	-54 49 11.04	0.92	2.942	0.308	1.480	0.200	12.19	2.16	3.48	0.90	0.11	16.67	0.175	-	S
4725	23 10 40.45	0.53	-58 22 48.34	0.53	2.557	0.557	2.253	0.347	3.50	1.30	2.07	1.11	145.71	102.19	0.315	-	S
4726	23 09 52.07	0.47	-59 43 44.95	0.48	5.032	0.501	2.836	0.326	7.66	1.17	6.00	0.94	149.17	39.86	0.264	-	S
4727	23 12 51.73	0.15	-53 35 53.40	0.16	48.261	2.873	38.865	2.186	5.07	0.12	2.95	0.10	168.87	5.16	0.458	-0.59	M
4728	23 12 20.85	0.72	-54 52 25.05	0.87	2.316	0.359	1.328	0.240	8.16	2.09	5.65	1.58	24.52	55.88	0.211	-	S
4729	23 11 27.27	0.61	-56 46 50.26	0.61	1.387	0.404	1.345	0.243	3.22	1.59	0.00	1.20	140.99	62.18	0.230	-	S
4730	23 09 59.22	0.86	-59 28 31.02	1.24	1.919	0.253	0.837	0.174	11.05	3.04	6.62	1.84	168.28	35.94	0.157	-	S
4731	23 10 54.46	1.32	-57 49 13.42	0.64	4.963	0.454	0.976	0.192	9.57	3.16	0.00	1.32	171.23	21.82	0.184	-	M
4732	23 13 16.44	0.34	-52 33 59.57	0.37	3.456	0.307	2.168	0.200	7.21	0.84	5.33	0.68	34.66	36.68	0.149	-	S
4733	23 11 09.29	0.91	-57 19 01.40	0.97	1.612	0.314	0.957	0.210	7.33	2.40	5.72	1.98	32.16	98.29	0.188	-	S
4734	23 10 29.64	1.08	-58 33 00.79	1.16	2.870	0.381	1.192	0.264	9.69	2.76	8.90	2.48	5.35	127.98	0.237	-	S
4735	23 13 37.71	1.09	-51 32 27.28	0.89	5.948	0.490	1.585	0.193	16.91	3.22	0.00	0.59	144.92	8.10	0.173	-	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4736	23 13 52.64	0.63	-50 51 40.12	0.71	3.208	0.433	1.873	0.288	7.41	1.57	6.49	1.52	159.87	120.66	0.248	–	S
4737	23 11 52.05	0.17	-55 46 09.75	0.18	8.541	0.578	7.226	0.447	3.76	0.26	2.97	0.23	156.27	32.86	0.198	–	S
4738	23 11 02.33	0.61	-57 27 36.45	0.51	1.566	0.288	1.235	0.183	6.01	1.51	0.88	0.99	126.90	31.73	0.163	–	S
4739	23 13 56.61	0.18	-50 32 43.35	0.19	9.540	0.677	8.253	0.522	3.61	0.30	2.84	0.26	134.83	38.10	0.250	–	S
4740	23 13 22.49	0.36	-52 05 51.73	0.36	2.679	0.359	2.272	0.235	4.04	0.83	2.71	0.72	120.08	60.37	0.192	–	S
4741	23 11 45.22	0.73	-55 56 54.65	0.27	4.663	0.573	2.180	0.255	0.00	1.70	0.00	0.45	0.00	8.03	0.225	–	M
4742	23 13 18.93	1.13	-52 10 43.02	0.37	6.695	0.552	2.254	0.232	0.00	2.71	0.00	0.54	0.00	7.34	0.196	–	M
4743	23 12 56.48	1.04	-53 05 25.79	0.96	2.078	0.271	0.983	0.182	12.28	3.02	4.93	1.44	53.63	25.35	0.165	–	S
4744	23 11 31.09	0.21	-56 19 22.12	0.21	13.822	1.120	12.016	0.826	3.93	0.38	1.95	0.32	123.89	24.95	0.482	–	S
4745	23 09 31.18	0.91	-59 56 18.92	0.65	4.380	0.439	1.437	0.189	11.38	2.48	0.00	0.72	37.65	11.05	0.172	–	M
4746	23 10 02.68	0.24	-59 01 40.70	0.24	5.548	0.497	4.618	0.350	4.02	0.47	2.98	0.42	59.69	55.33	0.231	–	S
4747	23 14 00.59	0.22	-50 03 13.45	0.23	6.287	0.515	5.263	0.372	3.78	0.41	3.51	0.39	144.94	31.33	0.225	–	S
4748	23 09 45.31	0.69	-59 30 39.74	0.70	0.963	0.283	0.861	0.173	3.04	1.61	2.25	1.58	15.36	4.15	0.162	–	S
4749	23 12 27.67	0.58	-54 08 40.57	0.59	3.017	0.425	1.958	0.279	7.05	1.53	4.66	1.13	139.42	42.13	0.241	–	S
4750	23 12 12.36	0.27	-54 42 37.69	0.24	7.678	0.554	4.932	0.360	7.23	0.56	4.60	0.41	117.11	16.67	0.221	–	S
4751	23 11 27.71	0.33	-56 19 42.03	0.65	11.369	0.976	5.783	0.610	11.63	1.50	3.67	0.67	177.59	13.73	0.497	–	S
4752	23 09 47.73	0.40	-59 21 40.61	0.42	2.879	0.323	1.948	0.212	5.77	0.97	4.98	0.82	162.43	64.87	0.171	–	S
4753	23 12 08.26	0.66	-54 44 02.16	0.97	13.013	0.765	2.385	0.266	21.07	2.32	13.34	1.43	19.21	18.26	0.250	–	S
4754	23 12 05.40	1.10	-54 52 17.15	1.98	5.466	0.412	1.191	0.243	20.55	4.78	10.69	2.39	15.86	26.94	0.245	–	S
4755	23 12 20.06	0.41	-54 18 26.95	0.42	1.964	0.367	1.863	0.230	2.59	0.95	0.45	0.87	141.10	96.68	0.204	–	S
4756	23 09 43.87	0.35	-59 24 49.52	0.47	4.534	0.372	2.381	0.232	9.55	1.08	5.19	0.69	22.07	17.68	0.178	–	S
4757	23 12 03.37	0.52	-54 52 46.38	0.88	2.532	0.450	1.726	0.292	7.93	2.06	2.38	1.17	6.70	29.23	0.262	–	S
4758	23 10 51.01	0.72	-57 21 22.36	0.42	18.819	1.153	4.193	0.347	17.68	1.79	6.36	0.66	160.97	7.06	0.260	–	M
4759	23 13 07.66	0.14	-52 16 31.19	0.16	15.867	0.918	15.395	0.863	2.01	0.09	0.37	0.08	168.22	19.17	0.165	-0.60	S
4760	23 12 56.22	0.20	-52 45 50.21	0.20	5.092	0.363	4.017	0.264	4.57	0.35	3.78	0.31	119.68	34.08	0.137	–	S
4761	23 12 38.18	0.22	-53 28 52.24	0.21	9.025	0.687	7.320	0.498	5.75	0.44	1.02	0.29	62.84	12.81	0.282	–	S
4762	23 12 01.55	0.15	-54 54 13.47	0.15	28.830	1.691	24.885	1.392	0.00	0.10	0.00	0.08	0.00	3.87	0.253	-0.71	M
4763	23 13 40.66	0.27	-50 42 37.79	0.28	6.994	0.566	4.790	0.377	5.60	0.56	5.56	0.56	26.63	42.68	0.252	–	S
4764	23 10 20.50	0.60	-58 15 40.25	0.68	4.914	0.593	2.666	0.394	8.05	1.66	6.32	1.29	165.19	49.92	0.337	–	S
4765	23 12 40.12	0.42	-53 18 34.22	0.31	3.147	0.494	2.972	0.316	0.00	0.98	0.00	0.58	0.00	20.55	0.269	–	S
4766	23 12 19.39	0.95	-54 02 59.74	1.03	51.701	3.036	17.843	1.064	33.90	3.18	8.11	0.76	51.46	6.03	0.412	-1.39	M
4767	23 13 06.24	0.20	-52 12 26.01	0.21	5.169	0.447	4.942	0.339	2.25	0.35	1.05	0.33	157.03	61.88	0.200	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4768	23 09 35.38	0.81	-59 28 16.43	1.09	2.225	0.277	1.048	0.185	12.48	2.88	4.02	1.26	34.69	22.00	0.169	–	S
4769	23 09 25.67	0.53	-59 43 42.61	0.59	1.218	0.291	1.108	0.178	4.35	1.48	0.00	1.03	34.55	41.90	0.165	–	S
4770	23 11 32.02	0.36	-55 48 20.69	0.33	19.578	1.163	5.094	0.370	11.59	0.79	10.22	0.70	17.14	29.31	0.242	–	M
4771	23 13 21.63	1.14	-51 26 50.85	1.63	2.626	0.246	0.771	0.163	15.94	4.05	9.79	2.35	159.47	34.64	0.153	–	S
4772	23 11 48.84	1.13	-55 10 44.63	1.20	1.976	0.268	0.836	0.186	10.84	3.17	7.82	2.22	143.81	52.83	0.168	–	S
4773	23 13 32.26	0.14	-50 50 41.99	0.16	36.857	2.137	30.191	1.691	9.36	0.17	0.00	0.07	73.72	1.26	0.320	0.13	M
4774	23 13 08.55	1.84	-51 50 35.18	0.94	5.950	0.363	0.928	0.146	25.92	4.55	13.38	2.04	98.14	19.42	0.157	–	S
4775	23 09 27.76	0.39	-59 30 36.55	0.58	9.648	0.699	3.050	0.265	12.59	1.45	3.52	0.59	121.96	8.16	0.205	–	M
4776	23 09 38.22	0.72	-59 14 11.51	1.00	1.516	0.293	0.942	0.194	7.73	2.42	4.23	1.59	11.49	44.40	0.174	–	S
4777	23 11 09.24	0.14	-56 24 46.74	0.15	870.358	48.076	865.017	47.646	0.00	0.02	0.00	0.02	0.00	12.16	2.573	-0.58	S
4778	23 12 55.00	0.30	-52 23 22.89	0.30	4.213	0.354	2.818	0.234	6.68	0.69	4.75	0.55	55.30	29.58	0.163	–	S
4779	23 12 44.05	0.64	-52 50 03.50	0.76	1.416	0.240	0.931	0.158	6.60	1.71	5.10	1.50	176.08	86.42	0.139	–	S
4780	23 13 20.99	0.30	-51 10 26.77	0.33	3.409	0.504	3.386	0.329	0.00	0.66	0.00	0.66	0.00	106.56	0.270	–	S
4781	23 09 45.39	0.14	-58 54 49.86	0.15	54.940	3.045	51.678	2.851	2.70	0.04	0.91	0.03	97.82	7.95	0.220	-0.64	S
4782	23 09 39.43	0.75	-59 00 05.46	2.70	11.032	0.704	1.992	0.224	35.59	6.57	0.00	0.48	108.92	6.22	0.195	–	M
4783	23 09 05.77	0.66	-59 59 17.13	0.64	2.494	0.283	1.269	0.187	8.39	1.65	6.92	1.35	46.00	73.82	0.160	–	S
4784	23 12 04.90	0.23	-54 15 19.37	0.24	5.818	0.484	4.619	0.340	4.42	0.45	3.77	0.43	58.18	78.68	0.215	–	S
4785	23 12 15.46	0.91	-53 47 35.31	1.09	6.018	0.584	2.150	0.386	12.04	2.63	9.62	2.02	162.20	54.26	0.345	–	S
4786	23 13 18.01	0.71	-51 01 58.10	0.68	368.739	20.435	149.709	8.287	57.69	2.25	7.32	0.27	140.15	2.13	0.936	-1.02	M
4787	23 12 21.29	0.14	-53 30 51.02	0.15	32.014	1.821	30.828	1.717	2.06	0.08	0.95	0.07	53.18	18.93	0.268	-0.19	S
4788	23 10 33.05	0.44	-57 17 11.55	0.43	2.409	0.380	1.972	0.245	3.90	0.97	3.53	0.97	125.40	3.99	0.210	–	S
4789	23 12 54.32	0.15	-51 59 10.62	0.16	25.161	1.460	23.337	1.313	3.37	0.11	0.00	0.09	171.25	9.73	0.270	-1.22	S
4790	23 12 58.76	0.39	-51 48 13.14	0.34	2.021	0.279	1.745	0.182	4.38	0.89	1.53	0.68	86.64	37.16	0.150	–	S
4791	23 12 53.33	0.59	-51 58 23.13	0.44	35.174	2.059	9.731	0.603	23.99	1.62	6.00	0.43	149.45	4.13	0.278	–	M
4792	23 09 31.03	0.45	-59 02 46.85	0.37	2.045	0.315	1.711	0.203	4.60	1.01	2.06	0.80	101.24	45.60	0.173	–	S
4793	23 12 02.06	0.81	-54 05 21.28	0.97	3.217	0.485	1.702	0.328	8.80	2.32	6.41	1.80	22.24	64.24	0.290	–	S
4794	23 10 22.27	0.26	-57 30 00.42	0.24	4.713	0.425	3.841	0.296	4.45	0.51	3.01	0.44	102.66	38.29	0.199	–	S
4795	23 13 13.74	0.38	-51 00 36.42	0.90	19.589	1.609	8.373	0.980	14.99	2.12	4.52	0.80	10.56	13.76	0.840	–	S
4796	23 09 27.03	0.82	-59 06 17.66	0.77	1.389	0.346	1.048	0.221	5.03	1.95	3.84	1.72	133.42	127.73	0.202	–	S
4797	23 12 27.32	0.76	-52 57 23.23	0.71	5.439	0.352	1.631	0.171	20.15	2.32	6.14	0.75	51.98	11.43	0.150	–	S
4798	23 11 51.83	0.52	-54 20 40.27	0.62	1.553	0.306	1.252	0.194	4.83	1.43	2.90	1.18	0.74	70.32	0.174	–	S
4799	23 09 49.16	0.14	-58 22 18.58	0.15	31.500	1.805	31.598	1.762	0.00	0.07	0.00	0.07	0.00	36.32	0.292	-0.15	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4800	23 10 17.48	0.58	-57 29 44.15	0.49	2.973	0.353	1.854	0.231	8.65	1.48	3.14	0.84	130.34	20.63	0.196	–	S
4801	23 10 36.20	0.37	-56 50 25.75	0.49	8.667	0.571	3.594	0.302	14.34	1.25	4.55	0.49	151.86	10.11	0.223	–	S
4802	23 11 26.59	0.33	-55 07 33.86	1.46	2.911	0.487	0.954	0.211	0.00	3.43	0.00	0.60	0.00	12.31	0.205	–	M
4803	23 09 23.72	0.62	-59 00 16.65	0.68	3.225	0.357	1.660	0.235	9.74	1.77	5.45	1.14	39.34	27.60	0.201	–	S
4804	23 10 29.95	0.28	-56 58 54.81	0.75	15.072	1.012	6.214	0.438	16.47	1.75	2.99	0.52	101.36	6.27	0.274	–	M
4805	23 12 17.91	0.21	-53 09 56.95	0.22	6.329	0.482	5.118	0.348	5.58	0.43	1.71	0.30	54.27	14.24	0.197	–	S
4806	23 10 00.74	4.42	-57 53 26.87	1.54	13.309	0.921	3.214	0.320	43.55	10.97	2.93	1.11	165.70	10.94	0.267	–	M
4807	23 12 43.24	0.95	-52 04 24.62	1.82	4.376	0.500	1.063	0.216	14.00	4.76	0.00	0.65	66.98	10.95	0.208	–	M
4808	23 10 27.25	0.40	-57 05 23.09	0.50	3.697	0.362	2.146	0.235	8.32	1.17	5.05	0.82	24.67	25.47	0.189	–	S
4809	23 12 29.93	0.33	-52 37 18.52	0.39	2.156	0.248	1.649	0.164	5.54	0.86	3.41	0.69	25.46	39.31	0.130	–	S
4810	23 12 55.22	0.98	-51 30 10.34	1.00	1.608	0.254	0.836	0.173	8.97	2.60	6.69	1.96	135.69	59.93	0.154	–	S
4811	23 09 13.98	0.37	-59 06 28.49	0.39	2.507	0.348	2.062	0.227	4.07	0.89	3.10	0.76	170.35	74.31	0.188	–	S
4812	23 10 31.75	0.73	-56 47 47.15	0.74	2.330	0.392	1.459	0.259	6.61	1.83	5.58	1.57	147.26	98.25	0.229	–	S
4813	23 11 40.61	0.89	-54 25 16.32	0.80	1.934	0.304	1.098	0.204	8.80	2.36	5.06	1.51	130.16	38.17	0.181	–	S
4814	23 09 05.19	1.06	-59 19 00.12	0.85	4.257	0.327	1.240	0.193	15.19	2.67	9.45	1.67	127.47	26.75	0.177	–	S
4815	23 12 28.30	0.97	-52 31 34.50	1.08	1.209	0.211	0.649	0.143	8.65	2.59	6.48	2.18	36.74	85.94	0.128	–	S
4816	23 08 51.52	0.52	-59 39 46.75	0.57	1.530	0.238	1.081	0.155	5.91	1.39	4.03	1.09	25.68	54.21	0.135	–	S
4817	23 11 36.65	0.95	-54 29 40.55	1.03	2.152	0.238	0.867	0.161	11.62	2.67	8.03	1.88	41.71	45.05	0.143	–	S
4818	23 10 59.77	0.17	-55 46 32.33	0.18	13.396	0.821	9.603	0.577	6.09	0.25	3.86	0.20	67.76	12.91	0.219	-1.00	S
4819	23 13 07.89	0.61	-50 41 42.59	0.89	8.938	0.713	3.374	0.429	15.28	2.29	6.46	1.03	32.82	16.81	0.372	–	S
4820	23 10 00.51	0.42	-57 40 12.23	0.50	3.470	0.425	2.349	0.279	6.57	1.17	4.13	0.87	163.80	33.81	0.232	–	S
4821	23 12 34.01	0.85	-52 08 07.13	0.51	20.183	1.178	2.715	0.264	13.96	2.06	5.59	0.98	22.91	13.37	0.218	–	M
4822	23 08 47.25	0.24	-59 41 46.26	0.24	4.181	0.343	3.154	0.236	5.46	0.50	3.35	0.42	47.07	24.40	0.152	–	S
4823	23 10 49.48	0.52	-56 04 56.50	0.53	3.610	0.557	2.624	0.362	5.27	1.25	4.44	1.11	147.02	98.77	0.313	–	S
4824	23 12 16.65	0.17	-52 50 09.96	0.18	9.931	0.651	7.494	0.442	7.25	0.28	0.00	0.13	49.23	2.80	0.158	-0.66	M
4825	23 08 41.79	1.60	-59 48 46.61	0.70	2.367	0.234	0.817	0.155	16.15	3.65	6.10	1.58	103.20	23.04	0.146	–	S
4826	23 12 33.05	0.16	-52 04 58.82	0.16	17.104	1.013	13.708	0.789	4.44	0.17	3.63	0.14	88.06	19.32	0.223	-1.04	S
4827	23 13 10.54	0.26	-50 23 30.80	0.18	150.965	8.417	33.562	1.926	21.23	0.53	8.53	0.23	14.12	2.24	0.550	-1.06	M
4828	23 11 18.42	1.51	-54 59 59.07	0.87	5.761	0.491	1.685	0.311	16.65	3.66	8.71	1.85	107.61	25.35	0.293	–	S
4829	23 10 18.49	0.30	-56 58 01.08	0.32	4.340	0.641	4.263	0.417	0.00	0.71	0.00	0.59	0.00	50.36	0.344	–	S
4830	23 10 26.99	0.42	-56 44 07.42	0.45	3.103	0.461	2.455	0.299	4.42	1.00	3.70	0.94	15.51	119.44	0.254	–	S
4831	23 12 25.54	0.14	-52 21 51.51	0.15	41.692	2.325	27.651	1.534	6.71	0.08	4.84	0.07	7.28	3.53	0.203	-0.70	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4832	23 10 23.97	0.98	-56 47 20.58	0.87	2.470	0.447	1.428	0.300	8.16	2.52	5.28	1.76	129.23	53.33	0.268	–	S
4833	23 12 09.21	0.25	-52 59 44.71	0.24	5.234	0.398	3.733	0.271	5.73	0.50	4.49	0.41	94.57	30.14	0.166	–	S
4834	23 09 56.28	0.15	-57 35 32.75	0.16	72.745	4.099	41.994	2.349	8.56	0.13	6.28	0.11	109.81	3.50	0.428	-1.49	M
4835	23 11 33.22	0.63	-54 22 45.05	0.53	3.702	0.369	1.866	0.240	9.11	1.52	6.79	1.13	113.62	37.14	0.200	–	S
4836	23 09 39.10	1.78	-58 06 31.94	0.47	5.425	0.674	1.675	0.284	0.00	4.25	0.00	0.72	0.00	11.76	0.268	–	M
4837	23 11 15.95	0.14	-54 57 47.66	0.15	78.701	4.366	71.524	3.949	2.95	0.04	2.06	0.04	93.44	10.12	0.333	-0.92	S
4838	23 12 46.23	0.91	-51 18 23.25	1.74	19.566	1.148	2.760	0.270	29.72	4.40	9.51	1.34	70.30	10.63	0.223	–	M
4839	23 12 50.51	1.34	-51 11 51.70	1.33	3.196	0.359	1.093	0.249	12.78	3.43	10.06	2.79	57.63	72.73	0.227	–	S
4840	23 12 10.92	2.08	-52 51 21.96	0.77	2.947	0.352	0.732	0.155	0.00	5.15	0.00	0.73	0.00	13.08	0.150	–	M
4841	23 09 51.27	0.67	-57 41 50.00	0.79	1.432	0.405	1.227	0.250	4.40	1.93	1.30	1.44	168.39	70.17	0.233	–	S
4842	23 11 58.68	0.14	-53 17 41.85	0.15	89.570	4.962	83.475	4.604	2.37	0.04	1.98	0.03	91.22	16.76	0.344	-0.73	S
4843	23 12 59.28	0.89	-50 40 08.51	1.24	82.877	4.620	5.887	0.610	24.04	2.90	18.53	2.06	98.44	20.36	0.517	–	M
4844	23 09 37.91	0.40	-58 04 29.29	0.45	4.191	0.532	3.041	0.348	5.84	1.06	3.63	0.81	161.78	36.58	0.288	–	S
4845	23 09 35.74	0.47	-58 07 43.71	0.51	3.801	0.517	2.639	0.338	5.90	1.22	4.43	0.98	156.50	54.05	0.286	–	S
4846	23 11 39.71	0.45	-53 59 59.47	0.29	29.386	1.806	14.989	0.891	17.13	1.15	0.00	0.26	155.15	3.33	0.338	-1.38	M
4847	23 12 20.61	0.33	-52 24 18.01	0.35	2.435	0.301	2.040	0.199	3.88	0.74	3.28	0.70	26.22	173.38	0.159	–	S
4848	23 09 52.72	0.24	-57 35 13.60	0.23	39.513	2.305	12.197	0.795	8.06	0.46	6.83	0.40	11.80	18.87	0.426	–	M
4849	23 09 24.45	0.73	-58 26 45.28	0.74	2.207	0.395	1.434	0.260	6.79	1.92	4.70	1.47	40.94	66.26	0.231	–	S
4850	23 09 00.74	0.33	-58 58 59.44	0.50	17.315	1.072	8.109	0.480	20.60	1.29	2.63	0.30	63.43	3.32	0.178	-0.29	M
4851	23 11 10.38	1.46	-54 59 37.25	0.83	10.122	0.654	2.023	0.310	20.88	3.48	11.88	1.88	100.12	21.95	0.307	–	S
4852	23 09 56.26	0.77	-57 27 16.91	0.29	1.847	0.421	0.858	0.180	0.00	1.80	0.00	0.50	0.00	13.15	0.174	–	M
4853	23 12 17.68	0.16	-52 23 58.80	0.17	9.781	0.602	8.397	0.490	3.59	0.18	2.96	0.16	120.16	27.63	0.158	-0.42	S
4854	23 08 58.97	0.31	-59 03 35.63	0.29	4.235	0.362	2.822	0.239	6.39	0.67	4.68	0.57	63.14	35.80	0.169	–	S
4855	23 10 51.79	1.51	-55 36 13.65	1.88	13.600	0.765	1.105	0.162	33.66	4.82	21.18	2.99	33.72	23.16	0.211	–	S
4856	23 12 01.68	1.42	-53 01 39.31	1.19	3.165	0.283	0.894	0.185	14.15	3.41	11.71	2.71	90.07	64.84	0.173	–	S
4857	23 12 52.54	1.87	-50 40 30.91	1.08	65.547	3.621	3.501	0.371	47.94	4.79	24.76	2.18	79.97	13.26	0.534	–	S
4858	23 12 49.51	0.45	-50 54 26.94	0.48	5.181	0.843	4.269	0.541	4.15	1.08	3.46	0.99	40.35	3.52	0.468	–	S
4859	23 10 35.95	0.64	-56 02 28.81	1.09	7.936	0.597	2.518	0.345	16.79	2.72	7.10	1.15	162.78	16.87	0.313	–	S
4860	23 10 52.33	0.39	-55 27 41.04	0.43	3.493	0.479	2.721	0.312	4.82	0.98	3.64	0.85	14.92	74.08	0.261	–	S
4861	23 10 22.25	0.95	-56 22 08.35	2.67	12.579	0.991	2.132	0.387	18.85	6.51	0.00	1.33	77.89	16.47	0.369	–	M
4862	23 10 58.53	0.16	-55 09 20.76	0.16	32.734	1.942	23.879	1.350	7.29	0.17	2.45	0.11	5.90	2.53	0.313	-1.30	M
4863	23 10 48.56	1.55	-55 27 32.63	1.15	20.306	1.248	4.420	0.365	29.73	4.43	5.69	0.93	39.55	8.49	0.272	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4864	23 11 20.56	0.15	-54 18 57.76	0.16	13.150	0.764	11.921	0.672	3.18	0.11	1.78	0.10	122.86	13.77	0.144	-0.63	S
4865	23 09 03.08	0.85	-58 42 23.96	0.70	1.397	0.325	1.026	0.208	5.62	1.99	3.77	1.60	100.15	93.60	0.189	-	S
4866	23 11 34.71	0.85	-53 47 22.79	1.67	6.650	0.490	1.637	0.280	20.64	4.06	8.85	1.71	18.79	20.48	0.274	-	S
4867	23 10 55.83	0.17	-55 10 00.34	0.16	31.630	1.905	18.706	1.076	8.41	0.23	4.23	0.15	11.39	3.42	0.316	-1.01	M
4868	23 12 14.40	0.41	-52 06 49.80	0.41	8.586	0.541	3.065	0.263	11.19	0.96	10.67	0.84	119.80	48.18	0.189	-	S
4869	23 09 46.50	0.85	-57 21 14.26	0.62	4.832	0.377	1.658	0.225	12.91	1.96	9.07	1.42	93.10	31.94	0.194	-	S
4870	23 08 36.01	0.22	-59 20 02.89	0.23	4.391	0.339	3.328	0.237	4.69	0.43	4.11	0.38	14.36	50.29	0.142	-	S
4871	23 10 13.09	0.28	-56 29 37.95	0.27	5.856	0.835	6.230	0.554	0.00	0.57	0.00	0.51	0.00	83.29	0.443	-	S
4872	23 11 06.29	0.50	-54 39 04.88	0.52	1.819	0.276	1.343	0.179	5.97	1.32	3.32	0.97	142.27	39.62	0.155	-	S
4873	23 10 55.31	0.27	-55 01 22.59	0.49	7.905	0.532	3.616	0.295	13.75	1.15	3.75	0.44	20.37	9.81	0.211	-	S
4874	23 12 35.91	0.18	-51 00 17.19	0.18	14.471	0.956	9.395	0.576	6.13	0.32	0.00	0.21	41.83	5.88	0.255	-	M
4875	23 11 33.06	0.16	-53 32 13.84	0.17	15.023	0.949	13.966	0.816	2.87	0.18	1.34	0.16	177.21	21.84	0.272	-1.27	S
4876	23 10 29.10	0.79	-55 47 46.07	0.91	4.863	0.474	1.259	0.205	10.01	2.60	0.00	1.07	54.81	17.76	0.193	-	M
4877	23 08 04.32	0.19	-59 58 32.57	0.19	5.297	0.426	4.936	0.328	2.25	0.31	1.96	0.29	43.88	94.50	0.181	-	S
4878	23 11 07.24	0.77	-54 29 52.32	0.71	0.906	0.262	0.788	0.161	4.11	1.87	1.65	1.54	123.01	87.98	0.151	-	S
4879	23 08 59.02	1.05	-58 30 36.19	0.59	3.597	0.352	1.466	0.230	12.78	2.40	6.42	1.36	92.49	24.88	0.203	-	S
4880	23 09 17.76	0.18	-57 57 53.91	0.19	7.063	0.552	7.002	0.447	0.00	0.27	0.00	0.24	0.00	28.85	0.227	-	S
4881	23 10 37.95	0.17	-55 25 51.78	0.18	10.290	0.683	8.555	0.526	4.03	0.25	3.14	0.23	23.83	32.98	0.225	-	S
4882	23 11 38.33	0.68	-53 12 48.98	0.71	2.978	0.428	1.768	0.285	7.39	1.67	6.01	1.52	44.00	97.85	0.247	-	S
4883	23 11 17.35	0.38	-53 59 25.18	0.29	5.664	0.692	3.750	0.335	0.00	0.97	0.00	0.29	0.00	5.85	0.264	-	M
4884	23 10 35.91	0.60	-55 27 04.82	0.63	2.791	0.420	1.816	0.277	6.25	1.44	5.44	1.37	22.80	139.26	0.240	-	S
4885	23 11 47.77	1.23	-52 49 14.65	1.28	1.652	0.188	0.587	0.129	11.90	3.24	9.96	2.61	139.69	73.40	0.118	-	S
4886	23 09 44.83	1.01	-57 02 22.06	1.19	79.850	4.405	4.376	0.402	39.20	3.04	27.37	2.03	153.17	15.17	0.529	-	S
4887	23 10 11.45	0.69	-56 10 09.76	1.14	2.384	0.466	1.466	0.308	8.66	2.72	3.56	1.55	2.46	35.95	0.280	-	S
4888	23 10 58.66	0.49	-54 31 53.23	0.59	2.136	0.278	1.376	0.183	6.96	1.38	4.89	1.06	168.23	45.04	0.155	-	S
4889	23 08 48.20	0.63	-58 36 25.59	0.61	3.073	0.412	1.826	0.273	7.13	1.58	5.79	1.27	141.36	66.49	0.235	-	S
4890	23 10 47.61	0.74	-54 54 21.45	0.97	2.251	0.330	1.193	0.223	8.81	2.28	6.26	1.68	2.60	53.96	0.196	-	S
4891	23 12 14.64	0.32	-51 31 20.43	0.32	2.910	0.314	2.333	0.211	5.06	0.75	2.78	0.57	130.45	30.19	0.160	-	S
4892	23 08 08.17	0.76	-59 38 17.78	0.90	1.369	0.238	0.805	0.159	7.32	2.21	5.65	1.68	4.29	69.84	0.141	-	S
4893	23 09 40.18	0.65	-57 03 16.11	0.68	19.103	1.300	5.791	0.682	14.01	1.75	10.12	1.28	41.86	27.66	0.580	-	S
4894	23 09 08.25	0.90	-57 57 18.75	2.12	4.524	0.521	1.161	0.223	14.14	5.32	0.00	0.86	73.12	13.64	0.213	-	M
4895	23 09 00.11	0.69	-58 10 55.66	0.24	448.733	26.707	233.227	13.504	22.58	1.63	0.00	0.28	16.99	3.26	4.220	-0.76	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4896	23 11 09.71	0.19	-54 01 10.10	0.17	17.454	1.094	12.034	0.702	9.28	0.34	0.00	0.16	30.59	2.87	0.234	-0.77	M
4897	23 09 14.77	0.75	-57 47 06.39	1.44	2.001	0.316	1.007	0.213	11.85	3.53	3.34	1.46	169.04	25.51	0.198	–	S
4898	23 12 11.57	0.14	-51 33 15.21	0.15	22.439	1.301	19.797	1.104	3.78	0.09	0.00	0.07	140.86	3.44	0.182	-1.07	M
4899	23 07 59.54	1.90	-59 43 06.69	1.52	7.051	0.528	3.108	0.239	26.95	5.66	0.00	0.83	42.82	9.21	0.167	–	M
4900	23 11 53.23	1.00	-52 18 58.85	1.28	2.751	0.316	1.106	0.214	14.19	3.47	6.08	1.62	38.73	25.86	0.195	–	S
4901	23 11 52.27	0.65	-52 20 55.51	0.85	2.257	0.299	1.235	0.199	9.53	2.14	5.17	1.29	155.42	30.61	0.174	–	S
4902	23 09 35.32	0.79	-57 03 54.69	0.93	99.844	5.500	5.163	0.408	38.06	2.22	30.08	1.75	22.27	16.68	0.493	–	S
4903	23 11 30.16	0.28	-53 11 13.60	0.28	3.805	0.414	3.348	0.283	4.30	0.63	0.91	0.49	58.30	27.82	0.209	–	S
4904	23 11 58.30	0.93	-52 03 26.40	0.99	2.343	0.268	0.981	0.182	10.11	2.32	9.10	2.14	144.99	100.93	0.160	–	S
4905	23 08 34.71	0.14	-58 46 41.21	0.15	123.819	6.842	105.494	5.808	4.74	0.03	0.25	0.02	66.81	0.78	0.270	-0.68	M
4906	23 08 39.09	0.37	-58 40 29.60	0.40	3.414	0.396	2.472	0.261	5.47	0.91	4.10	0.75	164.95	46.00	0.210	–	S
4907	23 12 12.10	0.32	-51 26 09.46	0.38	2.551	0.311	2.116	0.205	5.43	0.88	0.61	0.59	151.15	23.22	0.164	–	S
4908	23 08 38.16	0.71	-58 39 08.16	0.56	10.336	0.633	2.899	0.273	19.94	1.92	6.51	0.66	131.97	11.06	0.230	–	S
4909	23 09 58.49	0.17	-56 18 00.99	0.18	10.434	0.752	10.035	0.621	0.00	0.24	0.00	0.22	0.00	30.69	0.282	–	S
4910	23 10 49.12	0.21	-54 33 54.64	0.19	16.766	0.977	6.474	0.394	9.80	0.38	6.30	0.26	163.82	5.73	0.169	–	M
4911	23 08 38.61	0.31	-58 35 58.37	0.31	3.393	0.436	3.040	0.289	3.47	0.70	1.51	0.59	142.40	48.06	0.230	–	S
4912	23 11 07.42	0.60	-53 49 20.44	0.54	1.946	0.409	1.650	0.256	4.65	1.47	1.50	1.10	121.98	51.69	0.232	–	S
4913	23 12 31.73	0.53	-50 27 34.73	0.84	2.306	0.377	1.549	0.246	8.54	2.02	2.61	1.11	22.01	27.53	0.218	–	S
4914	23 12 24.72	0.26	-50 44 52.15	0.28	6.888	0.620	5.394	0.426	4.73	0.56	3.90	0.50	146.14	54.34	0.291	–	S
4915	23 09 14.78	0.16	-57 31 52.90	0.17	9.994	0.633	9.045	0.532	2.82	0.18	2.23	0.17	154.89	37.49	0.183	-0.34	S
4916	23 11 45.31	1.41	-52 16 09.73	0.69	1.758	0.247	0.846	0.167	12.56	3.50	4.08	1.42	104.06	23.87	0.154	–	S
4917	23 11 57.94	0.65	-51 43 54.21	0.66	2.086	0.233	1.081	0.154	8.84	1.71	6.87	1.30	134.16	44.94	0.131	–	S
4918	23 07 46.23	0.61	-59 49 07.60	0.62	1.156	0.259	0.944	0.163	3.89	1.42	3.44	1.41	1.63	4.56	0.148	–	S
4919	23 07 46.15	0.22	-59 46 43.93	0.23	4.681	0.375	3.696	0.265	4.69	0.43	3.24	0.38	20.44	28.28	0.162	–	S
4920	23 12 06.04	0.81	-51 19 05.66	0.80	1.468	0.255	0.917	0.168	7.74	2.19	4.78	1.50	132.82	45.41	0.150	–	S
4921	23 10 31.30	1.13	-54 55 12.15	0.91	2.231	0.322	1.058	0.221	9.99	2.75	6.91	1.99	73.76	55.24	0.197	–	S
4922	23 09 42.48	0.14	-56 29 37.33	0.15	47.247	2.673	46.878	2.604	0.00	0.06	0.00	0.06	0.00	34.30	0.361	-0.39	S
4923	23 10 17.44	0.92	-55 21 26.89	0.75	1.150	0.288	0.863	0.184	6.11	2.24	2.86	1.60	71.40	59.68	0.168	–	S
4924	23 11 33.64	0.41	-52 34 29.81	0.46	2.656	0.306	1.812	0.201	6.99	1.11	4.04	0.80	40.20	31.58	0.163	–	S
4925	23 12 32.77	0.19	-50 02 06.19	0.19	13.272	0.807	8.320	0.511	7.62	0.35	4.92	0.24	114.91	10.34	0.213	–	S
4926	23 09 53.64	0.46	-56 03 23.07	0.53	1.429	0.546	1.880	0.297	0.00	1.41	0.00	0.75	0.00	27.11	0.307	–	S
4927	23 08 34.64	0.17	-58 23 46.60	0.18	12.202	0.828	11.049	0.673	3.01	0.22	1.95	0.21	21.32	31.27	0.282	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
4928	23 11 24.60	0.14	-52 48 51.40	0.15	18.897	1.062	18.320	1.016	1.53	0.06	1.35	0.06	90.71	67.07	0.126	-0.32	S
4929	23 08 09.33	0.71	-58 59 11.92	0.73	2.337	0.286	1.214	0.191	9.41	1.94	5.66	1.32	43.94	34.64	0.165	-	S
4930	23 10 01.38	0.45	-55 41 32.57	0.52	2.486	0.303	1.621	0.199	6.53	1.20	5.07	0.98	3.07	55.44	0.166	-	S
4931	23 08 04.84	0.53	-59 03 35.91	0.46	4.707	0.359	2.060	0.213	11.55	1.35	6.22	0.80	133.64	17.37	0.169	-	S
4932	23 08 24.59	1.00	-58 31 15.65	1.38	3.778	0.356	1.181	0.235	14.30	3.40	9.15	2.12	22.53	35.27	0.218	-	S
4933	23 11 13.24	0.42	-53 05 10.41	0.52	2.128	0.267	1.500	0.174	7.79	1.30	2.03	0.74	36.69	20.71	0.146	-	S
4934	23 10 17.96	0.23	-55 02 52.36	0.24	6.053	0.497	4.749	0.348	4.89	0.47	3.46	0.41	54.11	34.90	0.219	-	S
4935	23 08 29.83	0.68	-58 19 08.86	0.53	10.168	0.892	3.822	0.375	10.35	1.85	0.00	0.69	149.67	10.82	0.311	-	M
4936	23 10 27.19	0.52	-54 43 29.76	0.54	2.088	0.307	1.471	0.200	5.98	1.33	4.30	1.06	145.11	55.17	0.172	-	S
4937	23 09 54.10	0.98	-55 47 53.05	0.89	1.405	0.302	0.893	0.200	6.55	2.24	5.51	2.09	83.10	173.04	0.180	-	S
4938	23 08 13.51	0.71	-58 42 50.14	0.65	1.639	0.320	1.171	0.207	5.45	1.58	4.47	1.54	74.22	174.37	0.185	-	S
4939	23 09 44.63	0.50	-56 01 23.84	0.50	9.433	0.675	3.695	0.382	11.47	1.27	8.43	0.97	48.86	28.09	0.301	-	S
4940	23 12 09.33	0.83	-50 36 15.19	0.94	5.844	0.474	1.910	0.291	12.70	2.06	10.99	2.03	18.18	118.29	0.256	-	S
4941	23 08 42.29	0.98	-57 51 14.71	1.28	2.551	0.292	0.957	0.200	12.09	3.15	8.30	2.13	21.53	44.54	0.181	-	S
4942	23 09 49.95	0.19	-55 48 45.37	0.21	8.345	0.567	6.179	0.400	5.94	0.36	3.32	0.28	22.69	14.93	0.200	-	S
4943	23 11 21.73	1.62	-52 28 37.89	0.84	10.441	0.805	6.265	0.415	27.06	4.22	0.00	0.64	29.89	7.25	0.232	-	M
4944	23 07 54.85	0.56	-59 05 32.57	0.47	1.100	0.270	1.061	0.164	0.00	1.30	0.00	1.03	0.00	71.97	0.153	-	S
4945	23 08 43.57	0.35	-57 43 14.30	0.54	16.524	0.999	4.137	0.308	15.01	1.25	8.24	0.70	109.63	9.05	0.208	-	M
4946	23 10 54.31	0.67	-53 28 07.11	0.78	2.766	0.373	1.542	0.249	8.83	1.95	5.58	1.38	35.05	41.80	0.216	-	S
4947	23 12 15.93	0.30	-50 14 09.49	0.31	2.487	0.296	2.199	0.199	3.17	0.64	2.75	0.63	106.27	34.66	0.154	-	S
4948	23 07 56.04	0.93	-59 02 11.68	0.78	1.887	0.280	0.993	0.190	8.34	2.18	6.54	1.78	88.05	92.63	0.167	-	S
4949	23 12 06.93	0.60	-50 33 40.14	0.64	3.352	0.442	2.023	0.292	7.35	1.45	6.04	1.38	48.85	94.75	0.250	-	S
4950	23 07 25.46	1.10	-59 36 58.41	1.43	2.465	0.289	0.651	0.126	11.11	4.09	0.00	0.98	131.17	15.70	0.120	-	M
4951	23 12 05.77	0.99	-50 22 48.30	0.88	1.808	0.299	0.998	0.201	8.35	2.46	6.41	1.89	113.19	61.85	0.179	-	S
4952	23 08 27.13	0.63	-57 56 03.76	0.82	1.095	0.327	0.972	0.199	0.00	1.99	0.00	1.36	0.00	53.96	0.188	-	S
4953	23 10 31.73	0.73	-53 59 33.22	0.76	1.717	0.337	1.185	0.220	5.84	1.78	4.91	1.65	148.64	122.38	0.196	-	S
4954	23 10 10.52	0.15	-54 41 00.74	0.15	16.708	0.961	15.234	0.854	2.81	0.10	2.13	0.09	99.45	22.42	0.163	-0.10	S
4955	23 11 24.57	1.29	-51 57 45.37	0.37	11.736	0.733	1.806	0.210	24.11	3.04	4.59	0.71	177.40	7.31	0.185	-	M
4956	23 11 57.42	0.54	-50 36 20.16	0.64	2.301	0.424	1.773	0.272	5.17	1.38	3.79	1.30	167.76	96.98	0.241	-	S
4957	23 12 09.45	0.89	-50 03 22.89	0.70	1.068	0.284	0.866	0.178	5.65	2.21	1.30	1.49	82.44	51.03	0.165	-	S
4958	23 10 57.81	1.02	-52 56 47.22	0.76	2.069	0.227	0.879	0.152	11.07	2.46	7.81	1.69	90.56	40.54	0.134	-	S
4959	23 11 38.92	0.19	-51 17 08.01	0.20	3.585	0.337	3.869	0.262	0.00	0.33	0.00	0.29	0.00	43.01	0.157	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4960	23 09 18.61	0.65	-56 16 04.23	0.85	1.279	0.367	1.107	0.225	5.38	2.14	0.00	1.30	159.68	40.69	0.212	–	S
4961	23 11 24.46	0.14	-51 47 58.44	0.15	20.867	1.182	19.866	1.105	2.13	0.07	1.49	0.07	156.45	23.97	0.165	-0.42	S
4962	23 10 53.30	0.87	-52 59 39.59	0.84	1.005	0.223	0.692	0.145	5.68	2.07	5.19	1.89	103.31	3.92	0.131	–	S
4963	23 07 54.91	0.19	-58 34 05.32	0.21	27.519	1.630	12.208	0.737	9.95	0.38	6.02	0.26	56.82	5.70	0.303	–	M
4964	23 09 40.86	0.33	-55 24 40.67	0.42	2.457	0.299	1.901	0.197	5.66	0.93	2.63	0.68	1.82	29.15	0.159	–	S
4965	23 08 28.96	0.46	-57 34 25.47	0.48	2.782	0.365	1.930	0.239	5.53	1.11	4.92	1.00	2.68	104.57	0.201	–	S
4966	23 11 23.17	0.14	-51 39 55.13	0.15	27.962	1.563	26.763	1.481	2.06	0.05	1.33	0.05	157.91	17.63	0.160	-0.47	S
4967	23 09 13.69	0.37	-56 14 00.84	0.32	2.585	0.381	2.365	0.247	0.00	0.83	0.00	0.66	0.00	40.46	0.206	–	S
4968	23 07 48.67	0.43	-58 34 33.44	0.57	24.908	1.486	5.552	0.424	15.54	1.40	8.24	0.78	67.08	9.94	0.294	–	M
4969	23 09 00.76	0.15	-56 35 13.19	0.16	17.078	1.027	14.990	0.862	3.83	0.15	1.73	0.13	172.35	12.55	0.243	-0.88	S
4970	23 11 24.31	0.26	-51 32 05.71	0.40	6.658	0.581	3.603	0.272	9.78	0.93	0.00	0.38	117.17	6.34	0.186	–	M
4971	23 10 32.39	0.56	-53 27 16.60	0.91	6.467	0.421	1.761	0.205	17.58	2.18	9.46	1.16	19.83	17.43	0.180	–	S
4972	23 11 38.81	0.42	-50 51 34.16	0.35	6.157	0.432	2.829	0.248	10.34	1.00	7.48	0.69	80.60	20.45	0.179	–	S
4973	23 11 05.84	0.16	-52 11 11.87	0.16	22.867	1.322	14.675	0.831	7.25	0.16	4.05	0.12	6.48	3.75	0.197	-0.75	M
4974	23 11 14.80	0.15	-51 49 16.93	0.16	14.937	0.874	13.378	0.757	2.98	0.12	2.59	0.11	162.40	41.26	0.175	-0.32	S
4975	23 11 54.16	0.17	-50 10 24.67	0.18	6.624	0.441	5.866	0.355	3.16	0.23	2.79	0.22	41.86	46.25	0.145	-0.44	S
4976	23 08 59.34	1.17	-56 30 21.22	1.29	4.789	0.382	1.324	0.232	17.70	3.70	8.55	1.71	144.25	22.58	0.222	–	S
4977	23 11 29.22	0.95	-51 13 48.99	0.83	1.746	0.246	0.890	0.167	9.06	2.32	7.02	1.83	78.72	63.25	0.147	–	S
4978	23 11 08.09	0.76	-52 03 42.75	0.59	1.770	0.273	1.126	0.180	7.45	1.83	4.72	1.29	98.84	42.69	0.158	–	S
4979	23 06 50.65	0.24	-59 54 24.19	0.22	4.944	0.434	4.174	0.308	4.37	0.45	2.17	0.39	84.44	28.11	0.199	–	S
4980	23 09 22.95	0.34	-55 44 40.25	0.38	3.576	0.372	2.514	0.246	6.18	0.86	4.12	0.68	26.98	35.27	0.191	–	S
4981	23 09 45.78	0.32	-54 59 56.11	0.33	5.912	0.483	3.657	0.312	7.90	0.78	4.62	0.56	45.75	20.14	0.222	–	S
4982	23 09 57.86	1.27	-54 32 56.49	1.43	9.972	0.572	1.244	0.162	30.70	4.16	14.08	1.72	143.83	15.77	0.182	–	S
4983	23 10 49.89	0.50	-52 40 17.78	0.43	4.765	0.345	2.009	0.198	10.96	1.20	8.11	0.87	72.81	25.89	0.152	–	S
4984	23 07 31.53	0.32	-58 49 52.01	0.36	2.645	0.270	1.869	0.179	5.67	0.80	4.33	0.67	4.35	41.41	0.138	–	S
4985	23 08 19.62	0.84	-57 32 52.05	0.71	1.703	0.323	1.125	0.212	7.03	2.08	4.13	1.47	125.35	50.35	0.190	–	S
4986	23 09 55.78	0.20	-54 33 43.42	0.22	5.858	0.442	4.799	0.323	4.43	0.37	3.03	0.32	0.92	28.57	0.179	–	S
4987	23 09 19.70	0.68	-55 44 06.87	1.23	5.706	0.387	1.409	0.201	18.35	2.90	10.07	1.53	8.08	20.67	0.188	–	S
4988	23 08 50.42	0.64	-56 38 18.13	0.91	1.292	0.327	1.014	0.205	6.04	2.19	0.90	1.39	172.40	43.16	0.190	–	S
4989	23 08 05.18	0.51	-57 53 23.45	0.44	2.985	0.355	1.918	0.234	6.64	1.17	5.11	0.97	93.47	62.55	0.194	–	S
4990	23 08 49.49	0.25	-56 36 54.25	0.29	4.348	0.434	3.629	0.298	4.49	0.59	2.25	0.48	176.95	29.11	0.213	–	S
4991	23 10 37.76	0.36	-52 59 21.85	0.30	1.921	0.263	1.761	0.172	0.00	0.81	0.00	0.58	0.00	26.88	0.140	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
4992	23 07 20.17	0.89	-59 02 19.10	0.92	1.673	0.242	0.836	0.165	8.06	2.18	7.56	2.02	163.65	136.13	0.145	–	S
4993	23 10 35.16	0.42	-53 06 06.84	0.35	2.516	0.272	1.758	0.179	6.75	0.99	3.71	0.70	76.57	26.79	0.142	–	S
4994	23 11 00.62	0.46	-52 05 22.37	0.46	2.717	0.325	1.848	0.213	6.83	1.20	4.15	0.84	136.28	31.45	0.176	–	S
4995	23 09 58.60	0.89	-54 20 55.02	1.01	1.352	0.230	0.745	0.156	8.26	2.49	6.19	1.91	152.93	67.18	0.139	–	S
4996	23 08 10.91	0.17	-57 38 11.98	0.18	9.159	0.622	8.010	0.492	3.75	0.25	2.01	0.22	23.99	20.71	0.214	–	S
4997	23 06 35.88	0.96	-59 59 08.41	0.72	6.742	0.630	3.701	0.293	16.11	2.74	0.00	0.54	40.74	7.36	0.211	–	M
4998	23 10 27.59	0.40	-53 14 55.07	0.42	2.977	0.311	1.944	0.204	7.09	1.03	4.69	0.78	45.20	34.97	0.162	–	S
4999	23 10 28.48	0.53	-53 10 35.65	0.47	2.128	0.281	1.455	0.184	6.84	1.30	4.07	0.95	66.66	37.41	0.155	–	S
5000	23 10 58.64	0.21	-52 01 34.45	0.24	5.512	0.405	4.041	0.280	5.70	0.45	4.08	0.36	161.58	24.31	0.161	–	S
5001	23 07 02.57	0.14	-59 18 00.30	0.16	22.693	1.288	18.862	1.056	4.49	0.10	2.17	0.08	155.73	8.61	0.188	-1.14	S
5002	23 08 12.63	1.07	-57 26 20.39	0.71	11.520	0.660	1.746	0.189	25.27	2.63	13.35	1.35	118.90	15.10	0.187	–	S
5003	23 06 43.24	0.14	-59 44 45.30	0.15	28.088	1.576	27.142	1.504	1.75	0.05	1.06	0.05	143.70	21.31	0.181	-0.87	S
5004	23 07 48.68	0.16	-58 03 32.94	0.17	7.736	0.536	7.719	0.464	0.00	0.20	0.00	0.18	0.00	29.03	0.188	-0.17	S
5005	23 08 29.92	0.38	-56 54 05.08	0.62	6.023	0.421	2.302	0.232	13.06	1.43	7.20	0.82	9.63	16.30	0.185	–	S
5006	23 10 01.73	0.22	-53 57 58.78	0.19	8.754	0.642	5.761	0.368	7.26	0.42	0.99	0.25	23.51	5.74	0.188	–	M
5007	23 09 42.49	1.01	-54 35 43.41	0.99	8.205	0.491	1.411	0.183	20.83	2.72	14.74	1.90	51.69	27.09	0.181	–	S
5008	23 10 37.04	0.39	-52 39 10.24	0.45	6.826	0.535	2.826	0.213	9.82	1.01	7.73	0.83	72.94	27.47	0.146	–	M
5009	23 10 02.73	0.25	-53 52 54.12	0.27	4.437	0.355	3.125	0.239	5.72	0.55	4.69	0.47	166.18	39.98	0.156	–	S
5010	23 08 27.07	0.18	-56 53 57.89	0.20	8.227	0.547	6.240	0.394	5.06	0.30	3.78	0.26	178.80	21.65	0.184	–	S
5011	23 08 00.69	0.43	-57 38 02.72	0.56	3.259	0.391	2.071	0.257	7.27	1.29	4.50	0.93	178.56	32.20	0.215	–	S
5012	23 09 29.64	0.58	-54 58 55.83	0.73	2.069	0.386	1.504	0.249	6.41	1.77	3.04	1.21	161.54	41.62	0.222	–	S
5013	23 10 38.72	1.41	-52 28 37.75	1.21	70.045	3.902	4.355	0.407	28.93	3.43	23.06	2.67	158.65	25.65	0.329	–	M
5014	23 07 13.11	0.27	-58 52 07.43	0.26	2.968	0.288	2.433	0.198	4.44	0.56	2.79	0.48	120.27	36.80	0.140	–	S
5015	23 06 36.30	0.35	-59 44 17.56	0.38	3.650	0.353	2.373	0.231	7.05	0.90	4.28	0.68	34.88	26.21	0.178	–	S
5016	23 09 28.56	0.37	-54 57 47.79	0.35	2.552	0.387	2.333	0.250	3.46	0.84	0.91	0.70	69.36	54.70	0.210	–	S
5017	23 08 01.02	0.38	-57 34 15.18	0.40	3.407	0.330	2.141	0.216	6.83	0.93	5.22	0.75	149.21	36.59	0.168	–	S
5018	23 11 39.47	1.54	-50 01 14.08	2.65	6.582	0.400	0.790	0.158	30.58	6.45	16.09	3.28	20.39	27.28	0.187	–	S
5019	23 07 56.75	0.51	-57 39 39.23	0.49	1.731	0.356	1.531	0.223	3.42	1.20	2.14	1.06	135.61	108.37	0.201	–	S
5020	23 11 02.49	0.15	-51 30 40.51	0.16	22.584	1.300	15.516	0.875	5.37	0.13	4.02	0.11	122.84	6.67	0.195	-0.75	M
5021	23 07 55.58	1.05	-57 41 21.93	0.90	1.575	0.285	0.886	0.192	8.58	2.70	5.24	1.80	128.37	49.56	0.172	–	S
5022	23 09 34.58	1.28	-54 42 23.50	1.29	2.185	0.242	0.761	0.166	13.72	3.63	8.45	2.27	49.25	40.49	0.152	–	S
5023	23 07 14.44	0.15	-58 41 45.54	0.16	14.481	0.868	12.407	0.714	3.88	0.15	2.36	0.14	14.92	14.69	0.202	-0.95	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5024	23 10 07.95	0.83	-53 26 45.58	0.42	20.296	1.211	6.726	0.431	23.77	2.08	4.30	0.48	26.71	5.01	0.221	–	M
5025	23 10 07.28	1.22	-53 29 49.02	0.74	3.243	0.336	1.289	0.222	14.10	3.08	6.10	1.42	75.41	23.13	0.202	–	S
5026	23 09 41.38	2.20	-54 20 52.94	1.32	3.834	0.260	0.683	0.136	24.56	5.61	11.42	2.36	116.35	23.61	0.146	–	S
5027	23 06 29.00	1.40	-59 43 08.44	0.81	2.506	0.262	0.916	0.176	14.27	3.30	6.68	1.70	113.45	27.22	0.161	–	S
5028	23 08 21.71	0.73	-56 46 21.66	0.82	0.945	0.252	0.756	0.158	4.60	1.92	3.19	1.67	177.74	116.30	0.146	–	S
5029	23 11 09.92	0.15	-50 58 00.43	0.16	13.794	0.826	12.612	0.720	2.75	0.14	2.28	0.13	7.46	59.58	0.191	-0.69	S
5030	23 10 17.47	1.13	-52 57 29.47	0.76	5.032	0.321	1.147	0.148	20.28	2.94	10.31	1.34	118.58	16.97	0.140	–	S
5031	23 09 39.56	1.31	-54 16 54.02	1.28	3.859	0.286	0.914	0.166	17.79	3.73	11.37	2.17	137.05	29.26	0.160	–	S
5032	23 07 49.24	0.56	-57 36 32.59	0.61	2.929	0.316	1.540	0.208	7.96	1.46	7.00	1.23	11.49	76.55	0.175	–	S
5033	23 11 12.60	0.43	-50 47 30.22	0.53	2.783	0.305	1.722	0.200	7.92	1.25	5.02	0.91	28.01	34.96	0.164	–	S
5034	23 08 38.41	0.24	-56 11 44.12	0.24	4.704	0.433	3.986	0.305	3.59	0.46	3.15	0.46	59.63	70.19	0.204	–	S
5035	23 07 16.29	0.32	-58 27 51.83	0.33	3.177	0.332	2.379	0.221	4.78	0.72	4.28	0.64	158.20	81.12	0.169	–	S
5036	23 08 16.61	0.55	-56 49 29.34	0.57	1.605	0.264	1.164	0.171	5.06	1.29	4.66	1.25	166.89	171.85	0.150	–	S
5037	23 10 31.30	0.18	-52 22 22.04	0.19	6.406	0.459	5.758	0.362	3.39	0.28	1.97	0.24	25.02	31.10	0.171	–	S
5038	23 08 29.95	0.44	-56 23 46.12	0.57	2.214	0.342	1.664	0.221	6.31	1.37	2.12	0.90	165.03	29.56	0.192	–	S
5039	23 10 47.50	0.76	-51 43 05.81	0.59	1.828	0.280	1.184	0.183	8.37	1.99	3.02	1.08	120.85	26.22	0.162	–	S
5040	23 09 30.26	0.74	-54 29 28.57	0.66	2.357	0.283	1.224	0.188	8.42	1.73	7.03	1.48	86.27	78.31	0.162	–	S
5041	23 08 40.26	0.20	-56 03 51.85	0.23	5.353	0.435	4.522	0.316	4.27	0.41	2.35	0.34	17.19	25.89	0.188	–	S
5042	23 09 10.32	1.41	-55 07 03.81	0.37	10.628	0.726	3.093	0.281	21.65	3.31	4.03	0.80	3.80	8.48	0.223	–	M
5043	23 11 03.10	0.33	-51 04 02.23	0.37	3.991	0.375	2.665	0.247	6.29	0.79	5.30	0.71	162.80	61.41	0.185	–	S
5044	23 09 30.70	0.76	-54 27 43.97	0.80	2.280	0.284	1.145	0.191	8.95	2.03	6.99	1.56	145.38	54.32	0.166	–	S
5045	23 08 00.52	0.15	-57 10 22.83	0.16	11.811	0.711	11.859	0.673	0.00	0.11	0.00	0.11	0.00	94.51	0.167	0.02	S
5046	23 07 25.84	0.76	-58 03 27.70	1.81	12.128	0.757	1.569	0.222	21.86	4.26	8.66	1.72	88.63	15.84	0.205	–	M
5047	23 08 45.78	0.64	-55 50 00.39	0.91	6.913	0.461	1.839	0.233	15.66	2.15	10.96	1.45	4.26	25.33	0.207	–	S
5048	23 09 33.57	1.67	-54 17 03.15	1.57	5.619	0.344	0.835	0.140	26.78	4.95	13.25	2.20	136.05	20.75	0.154	–	S
5049	23 09 46.58	0.79	-53 50 18.88	1.14	2.202	0.254	0.937	0.171	12.03	2.78	6.86	1.67	23.15	33.11	0.153	–	S
5050	23 06 54.55	2.04	-58 47 57.91	0.80	2.780	0.253	0.800	0.165	19.41	4.71	6.69	1.79	87.94	23.31	0.162	–	S
5051	23 08 49.22	0.30	-55 37 41.40	0.76	8.725	0.519	2.344	0.203	20.67	1.76	7.05	0.61	0.95	10.31	0.164	–	S
5052	23 11 06.37	0.16	-50 44 56.76	0.17	8.944	0.573	7.823	0.465	3.20	0.20	3.03	0.19	15.59	3.87	0.172	-0.25	S
5053	23 10 12.11	0.72	-52 45 20.08	0.74	1.412	0.210	0.834	0.140	7.55	1.78	5.98	1.58	52.64	88.18	0.122	–	S
5054	23 09 24.52	0.43	-54 23 55.82	0.51	3.385	0.311	1.812	0.200	8.36	1.17	6.60	0.94	0.78	42.11	0.160	–	S
5055	23 07 22.03	0.90	-57 59 52.04	1.28	1.823	0.277	0.853	0.191	10.13	3.09	6.58	2.01	2.90	46.70	0.172	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5056	23 07 43.40	0.90	-57 25 13.65	1.27	2.809	0.262	0.925	0.172	14.08	3.13	8.66	1.91	23.19	32.40	0.157	–	S
5057	23 06 10.46	0.21	-59 45 08.16	0.24	7.353	0.502	4.728	0.326	6.95	0.45	4.55	0.36	22.77	16.71	0.183	–	S
5058	23 09 16.94	0.59	-54 36 53.87	1.22	2.381	0.244	0.974	0.160	13.87	2.89	5.68	1.31	7.96	21.79	0.145	–	S
5059	23 06 47.42	0.63	-58 51 29.51	0.91	1.897	0.283	1.085	0.188	9.11	2.22	4.20	1.31	21.79	30.52	0.167	–	S
5060	23 08 05.09	0.34	-56 47 05.26	0.35	3.179	0.297	2.087	0.195	6.10	0.80	5.32	0.69	158.36	56.91	0.147	–	S
5061	23 08 41.62	0.38	-55 40 30.59	0.54	1.668	0.286	1.412	0.182	0.00	1.23	0.00	0.82	0.00	30.66	0.160	–	S
5062	23 06 00.79	0.71	-59 55 16.40	0.77	1.502	0.338	1.116	0.217	5.70	1.96	3.29	1.44	32.70	65.46	0.197	–	S
5063	23 10 12.97	0.54	-52 32 58.53	0.62	2.279	0.373	1.640	0.243	5.86	1.40	4.27	1.23	18.75	81.19	0.212	–	S
5064	23 09 49.42	0.14	-53 21 17.92	0.15	16.623	0.961	16.210	0.908	1.52	0.09	1.04	0.08	59.56	55.68	0.171	-0.52	S
5065	23 06 18.23	0.54	-59 25 31.95	0.50	2.911	0.318	1.655	0.209	7.02	1.18	6.59	1.17	121.35	94.86	0.173	–	S
5066	23 10 54.94	0.47	-50 52 03.85	0.52	1.706	0.275	1.361	0.177	5.85	1.34	1.46	0.87	142.69	30.87	0.154	–	S
5067	23 10 05.73	0.14	-52 43 14.01	0.15	21.205	1.192	20.791	1.152	1.15	0.06	1.14	0.06	145.17	4.08	0.142	-0.70	S
5068	23 11 13.71	0.55	-50 02 31.03	0.55	3.692	0.346	1.854	0.222	8.53	1.33	7.90	1.17	121.92	65.42	0.182	–	S
5069	23 10 19.61	0.32	-52 11 40.14	0.36	3.086	0.311	2.235	0.207	5.95	0.79	4.09	0.64	33.27	40.39	0.157	–	S
5070	23 06 18.79	0.26	-59 21 48.03	0.28	3.456	0.335	2.791	0.229	4.64	0.58	2.79	0.49	19.09	31.67	0.163	–	S
5071	23 10 12.38	0.16	-52 25 51.32	0.18	11.553	0.725	9.343	0.558	4.23	0.22	3.69	0.20	37.38	59.51	0.207	-0.16	S
5072	23 07 23.04	0.61	-57 43 46.13	0.58	2.683	0.282	1.375	0.185	7.88	1.36	7.49	1.35	128.56	158.19	0.155	–	S
5073	23 08 56.05	0.15	-55 00 05.68	0.16	28.825	1.684	22.315	1.277	6.05	0.17	2.15	0.12	42.65	8.18	0.338	-1.85	S
5074	23 10 30.28	0.20	-51 43 24.32	0.21	6.057	0.485	5.466	0.367	3.79	0.37	0.52	0.29	143.36	20.61	0.206	–	S
5075	23 10 51.79	0.51	-50 40 39.53	1.94	8.647	0.737	6.376	0.419	27.67	4.66	0.00	0.62	81.72	7.18	0.229	–	M
5076	23 06 03.52	0.17	-59 38 39.31	0.18	7.250	0.498	6.575	0.403	3.07	0.23	1.86	0.21	62.81	33.28	0.174	–	S
5077	23 09 58.40	0.85	-52 48 02.90	0.76	1.916	0.250	0.975	0.168	8.61	2.02	7.30	1.71	103.86	75.99	0.147	–	S
5078	23 07 57.06	0.29	-56 39 02.23	0.38	3.159	0.336	2.367	0.223	6.04	0.83	2.70	0.59	173.56	23.30	0.172	–	S
5079	23 10 17.12	0.63	-52 04 17.51	0.88	2.265	0.311	1.255	0.208	8.97	2.05	5.69	1.43	8.93	43.27	0.182	–	S
5080	23 10 51.83	1.21	-50 41 08.38	0.89	2.992	0.383	1.303	0.262	11.15	3.01	7.57	1.94	87.47	42.56	0.235	–	S
5081	23 08 05.11	0.57	-56 19 31.46	0.81	0.875	0.291	0.864	0.172	0.00	1.96	0.00	1.19	0.00	40.75	0.166	–	S
5082	23 09 54.31	0.37	-52 47 05.84	0.36	3.261	0.293	2.015	0.190	6.74	0.85	6.00	0.74	111.60	57.46	0.143	–	S
5083	23 07 45.36	1.49	-56 51 55.98	1.26	2.871	0.246	0.765	0.158	16.65	3.91	10.05	2.38	59.28	35.17	0.151	–	S
5084	23 07 52.87	0.48	-56 38 22.56	1.08	10.667	0.616	1.885	0.191	25.25	2.54	10.77	1.01	177.60	12.69	0.181	–	S
5085	23 06 19.57	1.19	-59 04 52.52	1.30	2.642	0.255	0.827	0.170	14.65	3.54	8.82	2.16	41.38	35.31	0.158	–	S
5086	23 10 33.59	0.96	-51 14 28.34	1.16	51.599	2.870	3.155	0.386	23.85	3.00	14.87	1.85	61.36	16.85	0.345	–	M
5087	23 10 56.05	0.14	-50 20 04.95	0.15	34.086	1.909	29.107	1.610	0.00	0.07	0.00	0.05	0.00	1.50	0.175	-0.25	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
5088	23 09 39.24	0.25	-53 14 35.59	0.21	13.614	0.875	6.158	0.394	9.64	0.50	5.49	0.33	22.21	7.36	0.201	–	M
5089	23 10 31.10	0.97	-51 15 42.73	0.62	49.816	2.809	6.659	0.504	23.85	2.29	14.02	1.38	14.83	12.74	0.346	–	M
5090	23 10 31.49	0.70	-51 13 47.74	0.90	3.969	0.540	2.111	0.362	8.97	2.06	6.47	1.63	10.10	60.52	0.316	–	S
5091	23 06 05.81	0.59	-59 16 58.44	0.76	2.601	0.309	1.350	0.205	8.80	1.82	6.14	1.30	0.22	38.09	0.177	–	S
5092	23 08 15.88	0.82	-55 47 26.60	0.82	1.831	0.282	1.073	0.186	9.67	2.43	3.16	1.20	139.63	25.59	0.167	–	S
5093	23 08 15.40	0.17	-55 45 02.06	0.18	7.354	0.496	6.397	0.392	3.46	0.24	2.64	0.22	173.99	34.33	0.168	–	S
5094	23 10 44.35	0.29	-50 33 47.17	0.32	4.008	0.317	2.515	0.205	6.93	0.69	5.76	0.57	156.36	40.23	0.141	–	S
5095	23 08 05.91	0.81	-56 01 52.62	0.89	1.370	0.298	0.924	0.195	6.06	2.05	4.98	1.89	13.33	136.08	0.175	–	S
5096	23 08 12.26	0.71	-55 50 07.61	1.05	2.400	0.299	1.168	0.200	11.53	2.67	4.66	1.28	159.52	24.03	0.179	–	S
5097	23 08 36.25	0.34	-55 05 29.20	0.44	3.636	0.440	2.718	0.289	5.95	0.98	3.09	0.72	0.95	30.55	0.235	–	S
5098	23 08 34.93	1.32	-55 04 52.77	1.59	10.067	0.599	1.360	0.216	25.43	4.15	15.89	2.54	36.80	26.20	0.239	–	S
5099	23 06 04.32	0.18	-59 10 29.24	0.18	9.779	0.627	7.217	0.447	5.17	0.27	4.15	0.25	90.82	32.57	0.194	–	S
5100	23 10 34.76	1.54	-50 49 20.54	1.12	2.371	0.232	0.732	0.156	14.77	3.88	10.00	2.40	82.38	39.68	0.145	–	S
5101	23 06 09.79	1.02	-58 59 42.68	0.86	1.703	0.284	0.913	0.193	8.12	2.38	6.46	2.00	98.39	107.78	0.171	–	S
5102	23 09 05.57	0.24	-53 58 16.78	0.22	39.197	2.240	15.023	0.864	16.01	0.59	0.00	0.16	145.17	1.96	0.253	-1.29	M
5103	23 06 58.46	0.39	-57 43 51.60	0.39	3.005	0.335	2.083	0.220	5.27	0.86	5.20	0.85	1.36	94.72	0.176	–	S
5104	23 08 21.40	0.14	-55 22 04.75	0.15	14.431	0.836	14.413	0.807	0.00	0.09	0.00	0.08	0.00	25.13	0.152	-0.44	S
5105	23 06 51.88	0.36	-57 49 45.07	0.20	13.979	0.917	5.755	0.380	11.44	0.78	1.95	0.30	179.76	4.46	0.210	–	M
5106	23 07 28.08	0.39	-56 53 35.42	0.54	2.669	0.292	1.679	0.190	8.46	1.31	3.14	0.74	161.71	19.52	0.157	–	S
5107	23 06 20.37	0.18	-58 35 15.46	0.20	27.096	1.516	8.219	0.477	11.22	0.30	8.78	0.25	107.78	6.97	0.152	-0.07	M
5108	23 08 04.41	0.74	-55 49 31.89	1.18	4.328	0.327	1.244	0.191	15.97	2.84	9.40	1.59	171.06	24.11	0.175	–	S
5109	23 08 53.11	0.40	-54 16 47.99	0.58	15.742	0.959	3.624	0.288	14.91	1.34	9.97	0.87	105.23	12.60	0.208	–	M
5110	23 09 59.57	0.15	-51 48 13.14	0.17	120.864	7.521	111.123	6.458	3.25	0.17	1.33	0.15	12.15	17.91	2.048	-0.97	S
5111	23 07 20.98	0.24	-56 53 23.70	0.27	3.623	0.336	3.006	0.234	4.61	0.53	2.19	0.43	166.61	25.14	0.159	–	S
5112	23 09 59.64	0.20	-51 47 46.15	0.18	72.801	5.098	44.761	2.797	6.25	0.34	1.11	0.23	22.77	6.60	1.327	–	M
5113	23 06 34.78	0.14	-58 02 14.79	0.15	21.648	1.228	19.999	1.114	2.38	0.07	2.12	0.07	178.45	34.70	0.175	-0.53	S
5114	23 09 25.06	0.27	-52 53 40.53	0.26	2.295	0.273	2.212	0.186	0.00	0.57	0.00	0.49	0.00	52.26	0.140	–	S
5115	23 08 21.05	0.56	-54 56 30.68	0.49	31.948	1.883	13.625	0.816	18.68	1.53	8.69	0.68	146.24	6.94	0.323	-1.07	M
5116	23 09 13.10	0.90	-53 16 16.25	1.01	1.262	0.260	0.795	0.171	8.36	2.69	3.93	1.68	42.86	44.35	0.155	–	S
5117	23 10 37.66	0.73	-50 04 17.01	0.95	8.797	0.523	1.705	0.193	20.95	2.37	13.39	1.47	32.91	20.87	0.179	–	S
5118	23 07 43.65	0.73	-56 03 30.50	0.87	0.950	0.262	0.768	0.164	5.29	2.14	2.05	1.55	27.40	65.43	0.152	–	S
5119	23 08 59.17	0.67	-53 42 56.22	0.65	1.265	0.265	0.980	0.169	5.34	1.65	3.27	1.35	58.27	75.46	0.152	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5120	23 06 16.50	0.92	-58 20 54.45	0.76	1.309	0.260	0.840	0.171	6.99	2.23	4.69	1.66	119.72	67.13	0.154	–	S
5121	23 09 38.67	0.65	-52 16 49.84	0.59	6.616	0.500	2.470	0.293	12.26	1.65	8.94	1.18	64.33	30.46	0.243	–	S
5122	23 07 22.50	0.28	-56 36 04.38	0.43	3.070	0.297	2.084	0.195	7.98	0.98	1.95	0.54	172.43	15.70	0.150	–	S
5123	23 07 55.94	0.16	-55 37 40.35	0.17	7.540	0.483	6.685	0.396	3.59	0.20	1.92	0.18	16.34	19.13	0.144	-0.13	S
5124	23 09 12.98	0.78	-53 07 51.42	0.99	14.349	0.811	1.832	0.193	23.56	2.34	18.96	1.78	172.80	27.14	0.196	–	S
5125	23 06 42.14	0.58	-57 36 10.68	0.57	1.567	0.307	1.241	0.195	4.18	1.32	3.90	1.29	82.23	94.78	0.175	–	S
5126	23 05 33.38	0.15	-59 14 19.65	0.16	11.068	0.681	10.148	0.587	2.75	0.15	1.92	0.14	103.44	33.65	0.178	-0.17	S
5127	23 09 33.76	0.58	-52 16 39.51	0.76	6.749	0.509	2.389	0.297	12.80	1.79	9.33	1.30	16.85	33.61	0.251	–	S
5128	23 10 26.21	0.70	-50 16 19.30	1.01	1.213	0.283	0.879	0.181	6.93	2.33	3.07	1.60	13.73	52.70	0.166	–	S
5129	23 07 41.76	0.33	-55 52 36.22	0.35	2.384	0.289	1.941	0.191	4.32	0.77	3.23	0.67	16.08	69.42	0.152	–	S
5130	23 05 35.85	0.16	-59 05 54.99	0.16	11.975	0.735	10.753	0.623	3.75	0.16	1.01	0.14	93.86	13.54	0.191	-0.79	S
5131	23 07 43.49	0.46	-55 48 25.30	0.64	1.360	0.279	1.153	0.175	0.00	1.51	0.00	0.99	0.00	35.48	0.159	–	S
5132	23 06 16.69	0.55	-58 05 58.34	0.46	16.909	1.073	5.437	0.357	19.79	1.56	4.29	0.43	43.48	4.65	0.195	–	M
5133	23 10 12.46	0.20	-50 45 24.92	0.21	4.282	0.371	4.127	0.282	2.16	0.36	0.57	0.32	138.01	55.67	0.166	–	S
5134	23 07 11.99	0.65	-56 37 51.75	0.36	2.557	0.342	1.764	0.222	8.32	1.50	0.89	0.78	93.92	20.15	0.191	–	S
5135	23 10 08.82	1.14	-50 52 25.07	1.15	2.164	0.267	0.866	0.184	10.39	2.84	9.75	2.52	74.60	4.07	0.165	–	S
5136	23 08 33.08	0.26	-54 13 34.80	0.24	13.081	0.823	4.872	0.342	7.92	0.60	0.00	0.31	149.67	6.12	0.213	–	M
5137	23 06 39.15	0.14	-57 29 38.32	0.15	40.485	2.244	39.177	2.161	1.57	0.03	1.30	0.03	33.95	34.10	0.160	-0.23	S
5138	23 10 17.95	1.83	-50 26 38.11	0.58	14.136	0.910	5.594	0.378	33.37	4.44	3.78	0.71	18.89	7.06	0.219	–	M
5139	23 08 09.58	0.23	-54 56 34.37	0.32	10.514	0.755	6.284	0.476	8.40	0.66	4.61	0.44	3.29	14.98	0.305	–	S
5140	23 08 35.57	0.94	-54 08 11.42	0.84	2.037	0.230	0.877	0.155	10.19	2.26	8.35	1.88	74.32	75.97	0.136	–	S
5141	23 06 20.91	0.56	-57 57 36.12	0.63	2.568	0.305	1.457	0.201	8.47	1.61	5.10	1.08	151.47	30.50	0.171	–	S
5142	23 05 23.58	0.78	-59 18 41.05	0.75	1.982	0.260	1.026	0.175	8.04	1.93	7.03	1.59	140.50	90.05	0.152	–	S
5143	23 10 19.35	0.81	-50 21 16.62	1.66	3.824	0.314	1.094	0.195	18.95	3.97	8.22	1.72	15.85	22.75	0.185	–	S
5144	23 07 47.26	0.39	-55 31 33.13	0.50	1.872	0.255	1.396	0.166	6.08	1.15	2.99	0.83	18.87	33.60	0.140	–	S
5145	23 05 00.50	0.53	-59 46 30.23	0.54	1.684	0.332	1.393	0.210	4.52	1.37	2.24	1.05	151.92	58.14	0.188	–	S
5146	23 08 29.22	0.39	-54 12 20.65	0.48	7.379	0.498	3.014	0.270	12.51	1.19	6.89	0.66	151.87	14.50	0.201	–	S
5147	23 08 35.79	0.85	-53 57 59.54	0.77	1.504	0.233	0.859	0.155	8.32	2.20	5.52	1.53	127.52	46.15	0.137	–	S
5148	23 05 53.12	0.48	-58 30 19.03	0.39	1.468	0.253	1.273	0.161	4.23	1.08	1.50	0.85	103.50	51.13	0.141	–	S
5149	23 06 51.40	0.38	-57 01 00.30	0.46	2.905	0.306	1.861	0.201	6.89	1.04	4.86	0.81	3.91	35.40	0.161	–	S
5150	23 08 05.29	0.91	-54 54 18.96	0.98	4.832	0.469	1.776	0.309	11.46	2.47	9.53	1.92	149.39	57.52	0.274	–	S
5151	23 07 57.87	1.15	-55 04 23.31	1.76	19.729	1.100	1.496	0.186	36.61	4.31	21.07	2.42	22.84	18.43	0.241	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5152	23 07 45.03	1.20	-55 26 31.28	0.77	1.802	0.252	0.863	0.171	10.84	2.89	5.80	1.67	108.09	34.39	0.154	–	S
5153	23 09 36.97	0.64	-51 41 59.90	2.50	9.236	0.727	1.798	0.281	21.86	5.99	0.00	0.88	82.82	11.23	0.264	–	M
5154	23 06 02.41	1.39	-58 10 22.73	0.99	4.335	0.301	0.964	0.162	18.38	3.38	11.47	2.07	118.99	28.25	0.157	–	S
5155	23 07 03.83	0.29	-56 33 51.45	0.36	2.245	0.257	1.825	0.171	5.44	0.80	1.03	0.56	164.55	22.48	0.134	–	S
5156	23 10 04.92	0.44	-50 38 18.42	0.45	2.165	0.341	1.788	0.220	4.37	1.02	3.15	0.97	63.45	89.78	0.189	–	S
5157	23 08 08.94	0.74	-54 40 20.80	0.74	1.088	0.245	0.817	0.157	5.45	1.89	3.64	1.53	137.55	79.20	0.142	–	S
5158	23 04 55.68	0.52	-59 42 09.58	0.48	2.985	0.455	2.200	0.296	5.28	1.23	3.98	1.01	131.99	72.90	0.255	–	S
5159	23 07 45.71	0.28	-55 20 12.59	0.30	2.577	0.284	2.222	0.192	4.59	0.66	1.08	0.50	41.27	26.90	0.144	–	S
5160	23 09 00.38	0.40	-52 53 35.06	0.40	2.145	0.223	1.450	0.147	7.88	1.07	3.06	0.65	52.95	19.89	0.116	–	S
5161	23 06 33.33	0.43	-57 16 18.37	0.90	6.025	0.386	1.708	0.182	18.28	2.12	7.60	0.87	174.74	13.83	0.159	–	S
5162	23 08 21.72	0.21	-54 08 11.85	0.18	20.521	1.166	6.520	0.394	9.76	0.37	4.34	0.21	178.03	3.99	0.162	–	M
5163	23 05 29.62	0.88	-58 49 40.66	0.77	1.200	0.280	0.856	0.181	5.74	2.09	4.15	1.71	120.42	101.84	0.164	–	S
5164	23 06 38.73	0.23	-57 05 10.12	0.24	4.505	0.369	3.566	0.259	5.06	0.47	2.78	0.38	148.79	21.67	0.162	–	S
5165	23 07 31.89	0.68	-55 36 53.85	0.74	1.647	0.254	1.007	0.168	7.36	1.86	5.25	1.39	150.65	53.26	0.147	–	S
5166	23 05 02.22	1.55	-59 25 31.93	1.02	2.425	0.245	0.771	0.166	14.75	3.68	8.53	2.25	77.28	37.58	0.154	–	S
5167	23 05 56.59	1.21	-58 01 41.23	0.89	4.025	0.316	1.164	0.190	16.30	3.07	8.80	1.65	125.08	24.36	0.177	–	S
5168	23 09 35.47	0.74	-51 24 25.01	0.86	2.802	0.287	1.213	0.190	10.61	2.13	8.15	1.56	151.48	45.13	0.164	–	S
5169	23 07 19.09	0.17	-55 49 44.61	0.18	7.559	0.495	6.076	0.373	4.38	0.26	3.43	0.23	175.61	26.56	0.159	–	S
5170	23 08 56.54	0.81	-52 45 55.94	0.91	1.441	0.227	0.808	0.152	8.64	2.27	5.77	1.69	39.75	56.72	0.135	–	S
5171	23 05 57.21	1.91	-57 55 15.94	2.00	20.036	1.108	0.939	0.119	48.73	5.68	25.62	3.06	45.95	18.06	0.190	–	S
5172	23 07 06.49	1.70	-56 06 47.44	0.88	2.299	0.247	0.796	0.167	15.86	4.10	6.62	1.83	80.72	26.88	0.158	–	S
5173	23 09 07.92	0.63	-52 17 11.45	0.53	5.019	0.470	2.457	0.302	10.41	1.60	6.27	1.02	66.56	25.66	0.250	–	S
5174	23 06 56.45	1.23	-56 20 06.45	0.72	3.178	0.264	1.008	0.164	15.19	2.88	8.47	1.62	101.12	25.87	0.150	–	S
5175	23 09 02.29	1.08	-52 27 06.83	1.17	3.425	0.321	1.107	0.211	12.74	2.70	10.84	2.53	36.90	109.13	0.192	–	S
5176	23 05 26.47	0.75	-58 37 18.36	0.67	0.805	0.215	0.674	0.134	4.11	1.72	2.70	1.55	116.48	130.61	0.124	–	S
5177	23 05 14.02	0.99	-58 54 16.18	0.97	2.702	0.253	0.930	0.166	11.46	2.52	10.15	2.03	143.67	75.54	0.148	–	S
5178	23 05 41.35	0.77	-58 15 12.78	0.75	1.784	0.254	0.978	0.171	7.22	1.79	7.04	1.73	98.84	94.98	0.149	–	S
5179	23 06 42.01	0.55	-56 39 46.33	0.71	1.970	0.226	1.047	0.149	8.71	1.68	6.11	1.21	0.31	38.53	0.127	–	S
5180	23 05 31.00	0.64	-58 24 15.20	1.72	10.586	0.690	2.917	0.231	28.10	4.24	3.27	0.72	113.03	7.39	0.167	–	M
5181	23 09 08.27	0.74	-52 07 07.44	1.24	1.596	0.306	0.944	0.204	9.31	2.95	4.06	1.66	174.97	37.86	0.185	–	S
5182	23 06 29.40	0.36	-56 55 22.05	0.46	2.474	0.276	1.679	0.181	6.76	1.05	3.93	0.76	1.68	28.77	0.146	–	S
5183	23 05 11.45	0.18	-58 49 08.72	0.19	6.806	0.478	5.699	0.362	3.61	0.28	3.29	0.26	123.70	88.36	0.175	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5184	23 06 22.59	0.26	-57 03 03.95	0.23	6.399	0.454	4.039	0.293	7.05	0.52	5.02	0.43	98.98	22.73	0.177	–	S
5185	23 08 00.80	1.16	-54 13 48.77	0.64	1.616	0.241	0.862	0.162	10.60	2.79	4.22	1.39	100.77	28.00	0.146	–	S
5186	23 09 21.02	0.69	-51 30 03.91	1.46	1.517	0.252	0.802	0.169	11.66	3.47	3.64	1.52	176.14	27.95	0.156	–	S
5187	23 08 27.69	1.99	-53 18 40.62	1.13	5.238	0.331	0.875	0.149	26.85	5.07	11.42	2.01	74.12	20.26	0.161	–	S
5188	23 07 30.89	0.34	-55 04 52.51	0.50	9.027	0.691	4.452	0.417	11.05	1.19	5.04	0.63	161.90	14.77	0.318	–	S
5189	23 04 40.50	0.68	-59 25 40.03	0.50	1.775	0.333	1.355	0.213	5.87	1.55	2.61	1.12	92.43	46.36	0.190	–	S
5190	23 05 40.78	2.32	-58 00 05.62	0.62	3.902	0.364	0.907	0.158	0.00	5.58	0.00	0.78	0.00	12.02	0.150	–	M
5191	23 09 25.30	0.23	-51 10 59.35	0.24	5.397	0.465	4.614	0.334	4.71	0.49	1.07	0.35	135.87	18.79	0.211	–	S
5192	23 08 12.10	0.27	-53 39 11.69	0.24	19.326	1.103	4.703	0.311	11.18	0.55	8.61	0.44	20.44	12.73	0.173	–	M
5193	23 09 04.24	0.16	-51 54 20.35	0.17	10.260	0.648	9.449	0.553	3.04	0.18	1.48	0.16	148.81	20.59	0.185	-0.76	S
5194	23 07 52.96	0.34	-54 12 41.82	0.41	2.653	0.305	1.962	0.201	5.61	0.90	3.86	0.73	0.24	43.48	0.161	–	S
5195	23 09 04.57	0.22	-51 48 07.59	0.24	8.695	0.592	5.615	0.385	7.06	0.48	4.93	0.36	145.46	17.54	0.215	–	S
5196	23 06 41.65	0.61	-56 14 46.13	0.93	2.675	0.279	1.205	0.184	11.57	2.28	5.94	1.24	166.64	24.56	0.161	–	S
5197	23 06 09.44	0.63	-57 06 09.40	1.07	2.121	0.290	1.087	0.195	10.53	2.56	4.77	1.38	13.55	28.57	0.174	–	S
5198	23 08 48.37	0.22	-52 20 20.15	0.22	4.282	0.367	3.728	0.266	3.78	0.43	2.38	0.37	80.31	37.37	0.165	–	S
5199	23 08 27.01	0.83	-53 01 05.16	0.71	0.923	0.252	0.768	0.157	5.40	2.10	0.71	1.45	66.85	53.92	0.146	–	S
5200	23 05 55.06	0.26	-57 22 49.94	0.32	4.345	0.367	2.943	0.243	6.73	0.68	3.99	0.51	12.51	21.44	0.170	–	S
5201	23 04 01.50	0.53	-59 59 16.31	0.58	1.172	0.327	1.159	0.196	0.00	1.43	0.00	1.10	0.00	72.98	0.185	–	S
5202	23 04 13.10	1.08	-59 43 29.79	1.06	9.847	0.626	1.946	0.286	18.91	2.96	12.81	1.92	142.22	26.42	0.279	–	S
5203	23 06 08.32	1.13	-57 00 49.38	0.96	1.556	0.268	0.810	0.183	8.77	2.73	6.43	2.12	72.59	81.56	0.164	–	S
5204	23 08 14.33	0.62	-53 19 36.93	0.81	4.147	0.339	1.549	0.208	12.09	1.93	8.92	1.36	168.70	33.75	0.178	–	S
5205	23 06 36.39	0.18	-56 13 57.21	0.20	6.936	0.482	5.640	0.360	4.71	0.31	2.69	0.26	179.15	18.47	0.175	–	S
5206	23 08 47.57	0.85	-52 12 06.03	1.05	1.584	0.269	0.924	0.178	10.55	2.90	2.90	1.34	40.99	27.18	0.162	–	S
5207	23 07 33.80	0.76	-54 35 34.57	0.85	1.283	0.321	0.978	0.204	5.14	1.97	3.73	1.74	163.68	111.39	0.187	–	S
5208	23 04 31.27	2.79	-59 16 41.68	1.83	6.229	0.561	1.167	0.188	13.95	6.93	7.21	3.66	27.54	48.37	0.177	–	M
5209	23 05 04.69	0.45	-58 27 51.46	0.57	3.443	0.302	1.681	0.191	9.80	1.35	6.25	0.93	23.66	25.30	0.155	–	S
5210	23 05 42.96	1.49	-57 31 20.23	1.04	7.318	0.522	0.995	0.187	14.50	3.92	5.67	1.64	155.10	20.23	0.178	–	M
5211	23 07 55.89	0.15	-53 47 51.52	0.16	14.170	0.817	12.773	0.717	2.95	0.10	2.34	0.09	158.41	23.49	0.142	-0.29	S
5212	23 07 30.47	0.74	-54 34 57.03	0.76	4.050	0.349	1.537	0.220	11.49	1.92	9.09	1.53	47.30	52.96	0.189	–	S
5213	23 07 19.92	0.56	-54 53 19.14	0.70	4.512	0.379	1.868	0.235	11.15	1.70	7.90	1.17	159.79	29.06	0.197	–	S
5214	23 06 05.85	0.44	-56 56 35.88	0.48	1.429	0.271	1.272	0.170	3.94	1.15	0.93	0.91	32.02	55.78	0.151	–	S
5215	23 09 35.39	0.42	-50 18 24.27	0.48	2.710	0.273	1.643	0.178	7.26	1.06	6.06	0.93	164.08	64.78	0.142	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5216	23 08 43.97	1.07	-52 10 32.46	0.88	1.407	0.277	0.845	0.184	8.21	2.67	5.02	1.85	73.75	55.45	0.166	–	S
5217	23 09 26.19	0.22	-50 34 15.05	0.26	64.520	3.681	33.197	1.858	19.02	0.63	2.99	0.16	131.35	1.82	0.342	-1.21	M
5218	23 07 24.88	0.61	-54 42 16.16	0.80	1.672	0.277	1.085	0.182	7.51	1.94	4.05	1.28	164.21	39.08	0.161	–	S
5219	23 09 11.75	0.61	-51 09 02.93	0.56	2.805	0.323	1.601	0.213	8.37	1.54	5.86	1.13	68.44	40.67	0.179	–	S
5220	23 07 46.63	0.75	-54 02 19.63	0.75	0.983	0.230	0.748	0.146	5.31	1.84	3.66	1.63	52.67	107.43	0.133	–	S
5221	23 08 11.29	0.39	-53 13 49.37	0.48	2.316	0.270	1.574	0.177	6.65	1.10	4.42	0.85	10.92	40.38	0.145	–	S
5222	23 05 42.12	0.30	-57 28 21.90	0.30	4.339	0.374	2.940	0.248	5.50	0.61	5.38	0.61	12.85	94.98	0.175	–	S
5223	23 05 28.49	0.29	-57 48 10.97	0.28	3.828	0.341	2.763	0.229	5.15	0.58	4.63	0.57	89.43	54.72	0.161	–	S
5224	23 06 02.31	0.55	-56 57 54.68	0.79	1.724	0.266	1.092	0.175	7.90	1.89	3.82	1.18	172.65	32.58	0.154	–	S
5225	23 06 46.26	0.70	-55 45 14.21	0.55	3.759	0.291	1.423	0.173	12.17	1.71	8.31	1.15	118.02	25.87	0.144	–	S
5226	23 07 32.82	0.91	-54 24 46.05	1.00	2.153	0.257	0.925	0.175	10.05	2.34	8.49	2.10	27.69	103.73	0.154	–	S
5227	23 09 06.91	2.42	-51 13 25.38	1.81	16.884	0.935	0.824	0.114	45.01	6.36	28.93	3.53	117.20	20.64	0.182	–	S
5228	23 09 29.37	0.73	-50 25 09.95	1.06	2.902	0.273	1.129	0.177	14.08	2.68	7.03	1.40	30.72	24.80	0.157	–	S
5229	23 07 38.49	0.56	-54 12 51.38	0.55	2.777	0.337	1.667	0.222	6.75	1.28	6.36	1.25	111.85	147.70	0.187	–	S
5230	23 06 17.58	0.69	-56 30 58.57	0.98	1.882	0.222	0.891	0.148	11.05	2.45	5.56	1.34	160.95	26.92	0.132	–	S
5231	23 04 06.18	0.14	-59 37 07.28	0.16	198.062	10.982	99.721	5.509	12.21	0.12	6.24	0.07	88.42	1.08	0.522	-1.10	M
5232	23 06 50.95	0.84	-55 35 28.32	1.00	3.822	0.275	1.074	0.153	17.05	2.69	9.05	1.45	40.09	21.72	0.139	–	S
5233	23 08 30.73	1.12	-52 29 53.53	1.39	5.585	0.355	1.021	0.163	20.84	3.51	14.02	2.31	33.36	31.46	0.164	–	S
5234	23 08 21.97	0.87	-52 48 45.94	0.88	0.869	0.209	0.650	0.132	7.52	2.61	0.00	1.30	138.02	31.65	0.123	–	S
5235	23 09 05.38	0.86	-51 16 47.18	1.34	2.705	0.334	0.669	0.149	0.00	3.63	0.00	0.80	0.00	15.56	0.144	–	M
5236	23 09 34.75	0.77	-50 11 21.72	1.12	1.294	0.219	0.726	0.147	9.24	2.61	5.46	1.78	11.63	49.98	0.131	–	S
5237	23 08 33.03	0.63	-52 21 20.87	0.92	1.051	0.320	0.929	0.195	0.00	2.15	0.00	1.44	0.00	52.67	0.184	–	S
5238	23 06 52.15	0.17	-55 27 44.41	0.18	7.942	0.508	6.471	0.390	4.50	0.23	3.06	0.20	48.02	21.32	0.153	-0.55	S
5239	23 08 28.79	0.52	-52 28 10.47	0.61	1.556	0.303	1.275	0.192	5.46	1.49	1.65	1.06	36.95	43.69	0.172	–	S
5240	23 08 26.18	0.64	-52 31 51.71	0.68	6.297	0.561	1.966	0.225	11.14	1.95	2.79	0.89	51.48	14.15	0.197	–	M
5241	23 04 57.44	0.80	-58 23 17.65	0.78	2.612	0.268	1.123	0.177	10.70	2.13	7.37	1.46	141.03	35.49	0.154	–	S
5242	23 05 23.26	1.40	-57 45 13.23	1.01	3.333	0.282	0.936	0.179	15.61	3.38	9.95	2.20	75.66	37.17	0.168	–	S
5243	23 04 53.89	0.27	-58 26 53.24	0.25	4.379	0.348	3.050	0.233	6.14	0.55	4.20	0.46	73.25	28.83	0.152	–	S
5244	23 08 44.79	0.42	-51 49 39.75	0.35	10.897	0.699	4.235	0.356	11.66	0.99	8.84	0.70	94.50	19.75	0.251	–	S
5245	23 04 44.15	0.14	-58 38 49.96	0.15	34.838	1.932	34.234	1.888	1.46	0.03	0.28	0.03	116.43	15.61	0.141	0.14	S
5246	23 05 00.21	0.88	-58 17 22.85	0.81	1.892	0.244	0.909	0.166	8.59	1.98	7.76	1.96	96.00	5.13	0.145	–	S
5247	23 06 25.18	1.25	-56 06 01.39	0.46	4.471	0.414	1.069	0.175	0.00	2.99	0.00	0.85	0.00	12.87	0.164	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5248	23 07 41.78	0.66	-53 52 48.68	1.37	3.041	0.233	0.880	0.137	17.72	3.24	8.25	1.47	178.42	20.72	0.128	-	S
5249	23 09 05.40	0.30	-51 00 15.34	0.28	2.666	0.335	2.554	0.225	0.00	0.65	0.00	0.51	0.00	35.65	0.175	-	S
5250	23 07 28.05	0.17	-54 13 55.03	0.18	12.220	0.783	9.344	0.572	4.92	0.27	3.94	0.23	148.86	23.41	0.239	-	S
5251	23 08 20.81	0.74	-52 32 30.58	0.70	5.436	0.404	1.796	0.233	12.02	1.74	11.13	1.59	89.67	82.38	0.200	-	S
5252	23 07 13.32	0.17	-54 40 00.63	0.19	8.603	0.565	7.012	0.430	4.59	0.26	2.90	0.22	171.66	18.44	0.182	-	S
5253	23 07 39.24	0.56	-53 53 24.73	0.79	1.648	0.232	0.996	0.153	8.90	1.92	4.01	1.14	26.34	29.29	0.133	-	S
5254	23 04 23.69	0.20	-59 00 43.88	0.20	8.738	0.589	6.292	0.409	5.00	0.33	4.73	0.30	161.80	50.24	0.205	-	S
5255	23 05 45.72	0.97	-57 04 09.05	1.18	2.177	0.334	1.034	0.230	9.68	2.91	6.97	2.10	23.62	62.15	0.206	-	S
5256	23 06 45.48	0.34	-55 26 40.01	0.42	2.727	0.309	1.958	0.203	6.11	0.95	3.76	0.73	9.58	34.15	0.163	-	S
5257	23 06 24.43	0.26	-56 01 07.40	0.29	5.052	0.428	3.601	0.288	5.55	0.59	4.49	0.50	168.71	39.68	0.196	-	S
5258	23 04 27.63	0.14	-58 52 23.19	0.15	27.395	1.532	26.713	1.478	1.59	0.05	0.85	0.05	71.34	24.59	0.162	-0.62	S
5259	23 09 00.59	1.10	-51 03 20.72	0.71	2.631	0.305	1.224	0.202	13.10	2.92	4.54	1.20	71.64	21.31	0.182	-	S
5260	23 06 05.57	1.78	-56 29 27.74	1.42	2.636	0.212	0.598	0.133	17.82	4.56	11.77	2.81	125.21	38.44	0.131	-	S
5261	23 05 42.15	0.14	-57 04 42.55	0.15	26.366	1.494	24.942	1.388	2.35	0.07	1.35	0.07	72.92	18.73	0.208	-0.82	S
5262	23 04 06.57	0.31	-59 19 06.76	0.28	2.590	0.321	2.346	0.214	3.57	0.65	1.02	0.55	87.20	43.38	0.167	-	S
5263	23 07 17.56	0.79	-54 25 09.24	0.78	3.505	0.273	1.275	0.161	15.55	2.40	6.02	0.96	139.00	16.16	0.143	-	S
5264	23 07 20.46	0.54	-54 16 45.60	0.26	70.181	3.945	16.344	0.941	28.25	1.28	7.68	0.34	166.32	2.87	0.279	-1.16	M
5265	23 07 10.50	0.60	-54 37 04.60	1.04	2.439	0.282	1.142	0.188	11.38	2.45	5.73	1.35	179.99	27.08	0.166	-	S
5266	23 09 02.50	0.14	-50 50 59.53	0.15	73.416	4.083	62.916	3.469	7.71	0.05	3.22	0.03	47.91	0.83	0.241	0.30	M
5267	23 06 13.82	0.24	-56 12 18.32	0.28	3.713	0.348	3.041	0.241	4.69	0.56	2.56	0.45	10.70	28.77	0.167	-	S
5268	23 06 50.61	0.36	-55 10 24.77	0.39	3.156	0.310	2.053	0.203	6.72	0.90	4.99	0.74	31.82	42.65	0.157	-	S
5269	23 09 14.17	0.36	-50 25 26.46	0.47	1.860	0.279	1.575	0.180	5.04	1.06	1.46	0.76	10.34	36.89	0.153	-	S
5270	23 08 56.61	0.31	-51 02 47.82	0.37	5.922	0.426	3.087	0.256	9.29	0.85	6.42	0.59	154.82	19.94	0.177	-	S
5271	23 05 38.60	0.20	-57 03 33.03	0.20	7.577	0.553	6.077	0.403	4.66	0.35	3.16	0.31	77.82	28.56	0.215	-	S
5272	23 07 30.18	0.20	-53 56 22.35	0.22	3.915	0.311	3.386	0.231	3.69	0.37	2.61	0.33	178.88	41.25	0.132	-	S
5273	23 06 58.45	1.47	-54 51 59.89	0.88	4.033	0.315	1.099	0.189	17.96	3.66	8.84	1.71	113.84	23.08	0.180	-	S
5274	23 07 27.38	1.85	-53 59 32.23	0.88	1.703	0.195	0.599	0.134	15.59	4.47	6.72	1.94	99.10	28.17	0.126	-	S
5275	23 06 13.59	1.00	-56 03 50.64	1.60	4.078	0.306	1.027	0.178	19.99	4.13	8.43	1.64	159.28	20.91	0.175	-	S
5276	23 04 15.88	0.80	-58 56 09.61	0.71	2.987	0.275	1.182	0.177	10.77	1.92	8.63	1.55	64.89	64.88	0.153	-	S
5277	23 07 48.30	0.80	-53 16 53.51	0.67	1.784	0.284	1.109	0.188	8.23	2.05	4.28	1.32	66.90	37.63	0.166	-	S
5278	23 04 13.25	0.65	-58 59 43.12	0.58	2.152	0.335	1.447	0.219	7.55	1.67	3.14	1.08	56.37	32.41	0.192	-	S
5279	23 06 17.65	0.27	-55 56 14.40	0.28	3.522	0.341	2.839	0.234	3.97	0.54	3.83	0.54	176.09	4.86	0.166	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5280	23 06 14.60	1.15	-56 00 31.01	0.85	3.773	0.341	1.255	0.221	13.10	2.73	9.53	1.94	101.71	42.89	0.199	–	S
5281	23 09 04.64	0.24	-50 37 08.96	0.26	4.203	0.397	3.677	0.281	3.36	0.47	2.86	0.46	159.55	20.39	0.189	–	S
5282	23 07 07.55	1.99	-54 29 47.02	0.81	4.266	0.325	1.026	0.192	21.54	4.78	8.45	1.80	92.96	21.73	0.193	–	S
5283	23 04 34.08	0.63	-58 29 58.56	0.57	1.228	0.257	0.990	0.162	5.08	1.57	2.21	1.16	130.44	53.32	0.147	–	S
5284	23 09 15.75	1.13	-50 07 39.06	1.77	3.440	0.287	0.880	0.182	17.67	4.26	10.99	2.50	169.35	35.64	0.175	–	S
5285	23 08 46.34	0.61	-51 09 35.10	0.91	2.745	0.283	1.254	0.186	11.96	2.22	6.16	1.25	24.84	26.10	0.161	–	S
5286	23 05 38.49	0.20	-56 50 08.38	0.20	4.786	0.365	4.101	0.273	3.83	0.34	2.48	0.30	145.43	29.33	0.149	–	S
5287	23 07 54.28	0.81	-52 54 03.23	0.55	4.256	0.313	1.455	0.179	13.89	1.96	8.78	1.19	87.18	22.63	0.152	–	S
5288	23 07 42.43	0.16	-53 16 55.46	0.17	8.888	0.569	7.900	0.468	3.58	0.21	1.96	0.18	81.15	19.91	0.170	-0.25	S
5289	23 08 37.50	0.85	-51 20 44.30	0.85	2.963	0.270	1.112	0.174	11.88	2.20	9.34	1.73	57.66	54.23	0.152	–	S
5290	23 08 23.30	0.21	-51 48 28.69	0.20	14.396	0.874	8.062	0.511	9.10	0.42	5.35	0.28	66.75	11.09	0.235	–	S
5291	23 04 50.60	0.95	-57 55 12.18	0.93	1.957	0.241	0.861	0.165	9.50	2.24	8.27	2.10	47.91	135.75	0.145	–	S
5292	23 06 04.83	0.37	-56 00 36.54	0.45	2.185	0.374	1.964	0.237	0.00	1.04	0.00	0.78	0.00	40.44	0.207	–	S
5293	23 06 12.62	0.78	-55 46 56.56	1.06	3.482	0.332	1.300	0.216	12.75	2.63	7.94	1.59	162.20	29.99	0.193	–	S
5294	23 04 44.54	1.05	-58 00 14.61	0.76	1.616	0.295	0.957	0.197	8.48	2.54	4.46	1.61	116.79	43.04	0.177	–	S
5295	23 06 12.45	0.37	-55 46 07.65	0.66	9.112	0.560	2.701	0.247	17.06	1.57	8.03	0.72	170.28	12.87	0.196	–	S
5296	23 03 44.81	0.73	-59 18 46.93	0.95	2.025	0.318	1.118	0.214	8.50	2.33	5.46	1.59	16.47	45.94	0.190	–	S
5297	23 04 56.45	0.53	-57 38 26.28	0.56	4.451	0.404	2.131	0.258	9.46	1.40	7.02	1.08	39.09	38.55	0.212	–	S
5298	23 08 04.12	0.15	-52 19 01.07	0.16	20.471	1.204	16.962	0.969	3.89	0.14	3.52	0.14	18.94	72.18	0.251	-0.22	S
5299	23 03 26.83	0.40	-59 38 58.97	0.37	10.603	0.856	5.641	0.535	8.50	0.92	6.16	0.74	57.14	32.03	0.402	–	S
5300	23 03 26.12	0.16	-59 39 45.77	0.18	17.129	1.153	15.857	0.956	0.00	0.22	0.00	0.18	0.00	14.12	0.386	-0.90	S
5301	23 08 17.70	0.68	-51 51 12.48	1.07	3.039	0.351	1.438	0.233	12.49	2.73	4.71	1.20	159.13	21.98	0.208	–	S
5302	23 06 21.61	0.30	-55 21 50.71	0.29	2.012	0.282	2.006	0.186	0.00	0.65	0.00	0.55	0.00	50.01	0.150	–	S
5303	23 07 33.12	0.14	-53 12 59.10	0.15	165.392	9.117	160.467	8.833	1.76	0.02	1.01	0.02	61.72	10.93	0.354	-0.66	S
5304	23 03 20.34	0.27	-59 41 43.93	0.21	83.496	4.708	50.725	2.817	19.86	0.62	2.79	0.14	156.07	1.56	0.388	-0.85	M
5305	23 05 16.86	0.15	-57 02 44.20	0.16	16.895	0.988	15.412	0.871	2.97	0.11	1.79	0.10	3.07	17.44	0.196	-0.49	S
5306	23 04 49.60	0.96	-57 41 52.12	0.39	21.954	1.266	3.172	0.293	19.85	2.24	7.86	0.85	2.87	8.32	0.235	–	M
5307	23 07 02.35	0.22	-54 07 42.84	0.25	3.957	0.360	3.417	0.256	4.02	0.48	2.21	0.40	14.12	34.11	0.168	–	S
5308	23 05 54.00	0.28	-56 01 46.45	0.48	4.074	0.380	2.587	0.247	8.92	1.08	2.44	0.56	12.00	15.53	0.192	–	S
5309	23 04 26.12	0.18	-58 10 36.39	0.22	13.399	0.845	6.928	0.422	8.76	0.40	2.93	0.22	122.43	4.16	0.180	–	M
5310	23 07 41.83	0.14	-52 50 37.70	0.15	32.746	1.826	31.117	1.717	2.74	0.04	0.00	0.03	147.76	2.06	0.134	0.39	M
5311	23 05 13.69	0.41	-57 01 19.60	0.42	2.521	0.351	1.966	0.228	5.03	1.03	3.20	0.82	145.71	47.74	0.192	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
5312	23 08 56.73	1.42	-50 09 51.57	0.93	2.649	0.238	0.843	0.154	15.97	3.76	8.41	1.72	114.30	24.83	0.143	–	S
5313	23 07 17.70	1.52	-53 29 35.06	1.21	29.191	1.647	1.548	0.216	23.18	4.07	11.50	2.03	38.77	17.98	0.198	–	M
5314	23 07 23.45	0.24	-53 20 34.66	0.24	4.168	0.374	3.529	0.265	4.37	0.50	2.34	0.40	70.58	30.23	0.174	–	S
5315	23 05 59.81	0.32	-55 46 03.97	0.31	5.038	0.417	3.169	0.271	6.68	0.72	5.51	0.60	127.96	38.95	0.193	–	S
5316	23 05 54.65	0.27	-55 54 14.62	0.32	3.911	0.336	2.680	0.223	6.44	0.69	4.21	0.53	169.14	24.68	0.157	–	S
5317	23 06 53.26	0.61	-54 15 52.59	1.13	1.109	0.265	0.806	0.168	0.00	2.67	0.00	1.35	0.00	32.78	0.156	–	S
5318	23 08 58.01	0.59	-50 04 42.60	0.67	1.734	0.285	1.209	0.186	6.45	1.53	4.46	1.32	37.41	73.12	0.163	–	S
5319	23 04 10.71	0.67	-58 27 35.29	0.72	1.691	0.284	1.088	0.187	6.54	1.81	5.05	1.41	157.97	69.76	0.165	–	S
5320	23 07 39.88	0.14	-52 47 19.31	0.15	18.137	1.027	17.135	0.953	2.37	0.07	1.47	0.07	72.20	18.88	0.143	-0.42	S
5321	23 08 58.55	0.58	-50 03 11.90	0.61	1.734	0.292	1.261	0.189	5.65	1.36	4.49	1.34	52.27	118.60	0.166	–	S
5322	23 07 39.10	0.28	-52 49 29.17	0.29	2.615	0.267	2.158	0.182	4.34	0.61	3.11	0.54	46.87	58.67	0.133	–	S
5323	23 05 05.25	0.63	-57 07 29.81	0.68	1.152	0.319	1.041	0.195	4.02	1.74	0.00	1.27	150.99	61.07	0.183	–	S
5324	23 08 42.67	0.17	-50 33 58.79	0.19	8.339	0.543	6.696	0.410	4.46	0.26	3.71	0.23	178.21	44.92	0.172	–	S
5325	23 06 31.58	1.06	-54 48 38.17	0.52	1.683	0.256	1.006	0.168	10.56	2.56	0.89	1.04	107.01	21.45	0.153	–	S
5326	23 05 27.43	0.79	-56 32 53.29	1.15	1.319	0.191	0.654	0.129	10.42	2.84	5.45	1.61	165.53	33.72	0.116	–	S
5327	23 04 33.20	0.76	-57 51 35.97	0.94	3.043	0.327	1.283	0.218	10.45	2.30	7.95	1.66	169.03	45.09	0.192	–	S
5328	23 05 07.28	0.16	-57 02 03.91	0.17	8.639	0.567	8.313	0.492	2.02	0.18	0.87	0.17	179.23	38.29	0.179	-0.24	S
5329	23 04 19.59	0.18	-58 09 30.85	0.19	7.037	0.516	6.256	0.400	3.37	0.29	1.97	0.26	173.04	28.13	0.199	–	S
5330	23 07 00.51	0.14	-53 53 42.56	0.15	52.678	2.911	51.396	2.832	1.43	0.03	1.10	0.03	7.50	27.03	0.163	-0.05	S
5331	23 03 02.93	0.29	-59 48 37.33	0.29	3.711	0.457	3.407	0.307	3.01	0.63	1.43	0.54	40.19	62.72	0.238	–	S
5332	23 08 04.73	0.98	-51 49 07.99	0.74	2.526	0.366	1.338	0.246	9.25	2.44	6.02	1.59	106.40	41.56	0.218	–	S
5333	23 03 19.13	0.31	-59 26 54.46	0.30	3.610	0.407	3.008	0.273	4.23	0.68	2.58	0.57	138.44	42.83	0.209	–	S
5334	23 06 17.81	0.32	-55 05 23.30	0.26	15.308	0.927	4.527	0.321	11.35	0.72	6.10	0.44	28.76	7.64	0.202	–	M
5335	23 05 45.60	0.29	-55 58 52.48	0.30	3.972	0.363	2.872	0.243	5.36	0.65	4.43	0.56	139.00	47.84	0.174	–	S
5336	23 06 09.67	1.16	-55 16 36.32	0.35	11.400	0.745	1.927	0.227	20.23	2.71	4.45	0.73	0.82	7.80	0.201	–	M
5337	23 05 15.41	0.52	-56 42 48.32	0.62	1.895	0.227	1.136	0.148	8.87	1.61	3.65	0.91	151.07	22.77	0.127	–	S
5338	23 04 07.93	0.42	-58 19 16.07	0.46	2.403	0.306	1.699	0.200	5.64	1.08	4.38	0.88	167.90	55.36	0.166	–	S
5339	23 04 31.56	0.82	-57 45 50.37	1.22	7.662	0.509	1.821	0.255	19.83	3.14	9.23	1.38	158.65	18.46	0.244	–	S
5340	23 08 18.54	0.40	-51 14 28.09	0.43	2.836	0.312	1.934	0.205	6.67	1.05	4.39	0.77	144.55	32.90	0.164	–	S
5341	23 07 07.86	0.27	-53 32 56.21	0.29	3.318	0.310	2.558	0.211	4.87	0.61	3.89	0.53	165.65	52.09	0.149	–	S
5342	23 03 21.84	0.15	-59 17 45.30	0.16	15.437	0.961	14.359	0.833	2.50	0.15	1.72	0.15	124.20	35.56	0.261	-0.64	S
5343	23 05 48.58	0.22	-55 48 31.17	0.22	4.764	0.407	4.181	0.297	3.24	0.39	2.69	0.37	83.82	101.08	0.183	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
5344	23 04 55.92	0.83	-57 09 37.76	0.89	1.384	0.328	0.975	0.212	5.87	2.15	4.33	1.83	29.84	109.79	0.193	-	S
5345	23 04 35.48	0.77	-57 37 44.57	0.82	2.495	0.412	1.474	0.275	6.88	1.92	6.21	1.75	169.02	126.17	0.243	-	S
5346	23 04 39.28	0.54	-57 30 56.97	0.74	2.449	0.349	1.510	0.230	7.92	1.77	4.27	1.15	171.53	32.97	0.200	-	S
5347	23 07 54.22	3.34	-51 57 28.76	0.59	26.561	1.637	6.498	0.498	48.90	7.88	6.91	1.14	9.73	9.23	0.347	-	M
5348	23 05 47.78	0.53	-55 45 11.29	0.55	2.348	0.331	1.597	0.217	6.59	1.40	4.16	1.03	144.00	40.86	0.186	-	S
5349	23 08 45.20	0.91	-50 09 14.85	1.10	1.357	0.224	0.718	0.152	8.75	2.39	6.89	2.26	11.47	114.25	0.135	-	S
5350	23 03 31.49	0.38	-59 01 24.99	0.53	3.423	0.362	2.097	0.236	7.97	1.21	4.22	0.80	11.17	24.28	0.193	-	S
5351	23 04 27.50	0.14	-57 43 49.06	0.15	36.848	2.068	34.802	1.930	2.16	0.06	1.64	0.06	95.25	27.04	0.240	-0.61	S
5352	23 03 31.79	1.02	-59 00 04.41	0.91	2.216	0.360	1.156	0.245	8.81	2.57	6.23	1.91	60.28	70.00	0.218	-	S
5353	23 06 59.22	0.50	-53 40 08.73	0.45	4.682	0.360	2.209	0.216	12.53	1.39	4.70	0.65	56.28	14.30	0.170	-	S
5354	23 04 22.52	0.40	-57 50 33.05	0.40	2.977	0.352	2.133	0.231	6.05	0.98	3.80	0.77	50.51	39.74	0.188	-	S
5355	23 07 20.12	0.54	-53 00 46.78	0.73	3.444	0.264	1.309	0.156	13.21	1.78	7.75	1.08	29.31	22.32	0.130	-	S
5356	23 07 46.07	0.67	-52 10 28.05	0.63	2.128	0.476	1.729	0.300	4.57	1.55	3.18	1.43	80.53	107.67	0.272	-	S
5357	23 05 33.40	0.67	-56 03 11.07	0.63	1.568	0.297	1.141	0.192	5.39	1.52	4.33	1.45	71.41	142.75	0.171	-	S
5358	23 06 55.72	0.82	-53 44 24.01	1.11	1.575	0.225	0.771	0.154	10.15	2.69	6.39	1.80	21.44	46.11	0.137	-	S
5359	23 04 42.77	0.45	-57 18 38.11	0.48	4.686	0.466	2.677	0.303	7.62	1.16	5.99	0.92	156.14	40.47	0.244	-	S
5360	23 05 49.96	0.19	-55 35 20.19	0.20	6.573	0.455	5.106	0.330	4.69	0.32	3.85	0.29	23.27	39.65	0.165	-	S
5361	23 03 38.48	0.52	-58 44 59.36	0.46	2.198	0.287	1.479	0.188	6.12	1.21	4.79	0.99	116.25	69.75	0.159	-	S
5362	23 05 31.14	0.14	-56 00 44.71	0.15	21.327	1.213	20.013	1.116	2.23	0.08	1.84	0.07	51.76	44.94	0.180	-0.47	S
5363	23 07 15.76	0.76	-52 59 55.16	0.54	1.582	0.225	0.984	0.148	8.27	1.86	4.04	1.12	110.00	30.02	0.129	-	S
5364	23 06 20.98	1.96	-54 35 39.83	2.30	25.251	1.434	2.106	0.281	34.12	6.89	9.57	1.75	134.72	13.11	0.256	-	M
5365	23 02 38.16	0.22	-59 57 49.84	0.22	6.511	0.548	5.447	0.393	3.63	0.41	3.26	0.39	91.46	95.61	0.244	-	S
5366	23 04 49.62	0.33	-57 02 56.78	0.35	2.160	0.298	1.918	0.195	3.32	0.77	2.16	0.67	172.78	76.79	0.160	-	S
5367	23 08 30.19	0.72	-50 27 36.16	0.75	1.879	0.281	1.127	0.186	7.80	1.95	5.56	1.42	137.32	49.63	0.163	-	S
5368	23 06 30.07	0.57	-54 20 09.51	0.85	2.881	0.290	1.330	0.189	11.31	2.06	6.03	1.16	165.40	24.31	0.163	-	S
5369	23 04 11.34	0.53	-57 55 47.26	0.57	1.694	0.304	1.305	0.195	5.00	1.38	3.51	1.12	23.65	78.01	0.172	-	S
5370	23 04 56.81	0.44	-56 49 40.97	0.36	2.510	0.275	1.708	0.181	6.46	0.98	4.37	0.78	89.54	40.22	0.145	-	S
5371	23 06 58.61	0.63	-53 25 07.89	0.56	1.775	0.332	1.360	0.213	5.22	1.49	3.58	1.23	111.56	72.03	0.189	-	S
5372	23 06 17.12	0.89	-54 34 49.56	0.72	15.222	0.883	2.618	0.282	20.99	2.24	14.55	1.43	123.26	19.58	0.265	-	S
5373	23 03 46.42	0.26	-58 24 14.39	0.28	2.688	0.295	2.412	0.202	3.86	0.58	0.38	0.47	36.11	30.82	0.149	-	S
5374	23 05 57.10	0.76	-55 09 28.64	1.37	2.469	0.270	0.964	0.182	13.93	3.31	6.35	1.61	17.14	26.76	0.166	-	S
5375	23 03 49.61	0.67	-58 18 24.22	0.58	1.166	0.298	1.038	0.183	4.40	1.67	0.00	1.17	128.62	51.27	0.170	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5376	23 06 25.56	0.34	-54 18 59.16	0.51	4.915	0.365	2.272	0.216	11.23	1.18	6.20	0.71	16.12	17.60	0.164	–	S
5377	23 08 31.59	0.35	-50 09 40.55	0.42	3.559	0.323	2.192	0.210	8.02	0.97	5.08	0.70	32.95	28.48	0.159	–	S
5378	23 06 09.39	1.40	-54 40 37.21	1.05	2.372	0.267	0.878	0.182	13.85	3.69	7.22	1.88	123.88	30.48	0.168	–	S
5379	23 03 38.63	0.59	-58 25 22.21	0.55	1.197	0.269	1.035	0.168	3.91	1.42	2.06	1.16	129.92	85.56	0.153	–	S
5380	23 05 00.47	0.33	-56 28 51.62	0.51	3.438	0.281	1.794	0.175	10.05	1.17	4.98	0.67	175.44	17.28	0.135	–	S
5381	23 07 53.53	0.54	-51 22 08.04	0.42	4.364	0.340	1.997	0.205	10.94	1.36	6.80	0.81	115.42	19.39	0.161	–	S
5382	23 08 08.88	0.95	-50 48 09.87	0.84	1.456	0.264	0.879	0.175	8.19	2.53	4.88	1.63	124.27	44.68	0.157	–	S
5383	23 06 00.26	0.15	-54 47 17.64	0.16	9.654	0.624	9.617	0.562	0.00	0.16	0.00	0.15	0.00	48.96	0.189	0.15	S
5384	23 07 58.03	0.67	-51 09 15.39	0.98	2.269	0.268	1.075	0.179	10.63	2.29	6.78	1.54	7.65	39.89	0.157	–	S
5385	23 08 06.61	0.89	-50 51 14.96	0.79	1.175	0.273	0.847	0.176	5.84	2.09	4.24	1.79	103.51	87.70	0.160	–	S
5386	23 04 37.65	0.18	-56 57 44.59	0.21	10.053	0.623	6.170	0.390	7.44	0.36	5.00	0.28	1.05	13.82	0.179	–	S
5387	23 05 18.64	0.63	-55 54 45.47	0.61	1.491	0.347	1.260	0.217	3.89	1.45	2.90	1.37	63.96	2.41	0.198	–	S
5388	23 04 26.19	0.40	-57 12 26.10	0.47	3.619	0.434	2.482	0.285	6.20	1.08	4.42	0.86	15.00	45.42	0.235	–	S
5389	23 07 51.04	1.13	-51 19 00.80	0.95	1.806	0.242	0.820	0.165	10.57	2.93	7.32	1.90	119.34	44.09	0.148	–	S
5390	23 06 14.25	0.57	-54 21 19.09	0.92	1.446	0.249	0.940	0.163	8.53	2.20	2.81	1.22	17.83	30.17	0.146	–	S
5391	23 06 38.70	0.50	-53 36 44.53	0.67	2.257	0.282	1.359	0.185	8.61	1.62	4.45	1.04	26.93	29.81	0.158	–	S
5392	23 03 47.86	0.22	-58 00 52.68	0.24	4.405	0.373	3.615	0.264	4.34	0.45	2.84	0.39	163.04	30.49	0.167	–	S
5393	23 07 01.43	0.47	-52 51 03.33	0.41	2.288	0.246	1.463	0.161	7.07	1.11	5.06	0.85	86.92	39.05	0.130	–	S
5394	23 06 13.62	0.14	-54 16 41.06	0.15	16.888	0.967	16.399	0.915	1.76	0.08	0.83	0.07	157.87	25.29	0.155	-0.13	S
5395	23 05 19.12	0.85	-55 47 22.12	1.32	1.732	0.271	0.841	0.185	10.51	3.19	5.82	1.86	174.20	39.37	0.167	–	S
5396	23 02 33.59	0.15	-59 35 09.98	0.16	20.903	1.245	19.096	1.088	2.60	0.12	2.19	0.12	37.76	48.15	0.278	-0.40	S
5397	23 03 53.46	0.95	-57 49 26.82	1.24	2.336	0.308	1.001	0.212	11.14	3.14	6.99	1.93	161.70	40.04	0.191	–	S
5398	23 07 36.84	0.15	-51 36 09.16	0.17	14.946	0.899	12.749	0.735	4.86	0.18	1.29	0.13	2.65	10.23	0.214	-0.97	S
5399	23 02 47.30	0.19	-59 12 38.68	0.29	30.624	1.926	18.246	1.077	12.90	0.62	2.95	0.24	77.99	3.37	0.390	-0.80	M
5400	23 05 57.10	0.20	-54 39 49.09	0.18	13.295	0.792	8.066	0.488	8.62	0.33	4.01	0.20	111.87	9.21	0.191	-0.78	S
5401	23 06 16.31	0.90	-54 05 38.34	1.23	1.903	0.234	0.790	0.160	11.26	2.95	7.89	2.02	172.00	47.74	0.144	–	S
5402	23 02 14.04	0.16	-59 51 39.27	0.20	26.895	1.657	15.135	0.891	8.75	0.31	2.70	0.17	85.51	3.44	0.319	-0.90	M
5403	23 05 11.86	0.34	-55 50 28.22	0.44	3.600	0.337	2.241	0.219	8.01	1.02	4.13	0.66	163.93	20.54	0.170	–	S
5404	23 06 49.99	0.88	-53 03 58.03	0.77	1.314	0.249	0.844	0.164	6.98	2.15	4.99	1.65	117.49	66.06	0.147	–	S
5405	23 02 41.54	1.12	-59 19 18.11	1.03	3.911	0.495	1.627	0.341	10.70	2.92	7.82	2.06	136.04	53.34	0.306	–	S
5406	23 07 09.15	0.49	-52 14 54.13	2.51	277.084	15.389	17.439	1.182	82.43	5.93	15.97	1.03	98.75	5.05	0.691	–	M
5407	23 04 36.50	0.19	-56 40 47.68	0.20	4.855	0.347	3.921	0.256	4.43	0.33	3.23	0.29	6.11	28.29	0.131	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5408	23 04 06.42	4.74	-57 21 16.98	1.25	41.457	2.491	4.559	0.698	47.67	11.35	9.76	2.08	174.73	14.31	0.652	–	M
5409	23 05 34.35	1.00	-55 10 59.78	1.29	2.353	0.260	0.890	0.177	13.85	3.40	6.99	1.81	36.13	30.65	0.161	–	S
5410	23 08 11.13	0.79	-50 15 58.17	1.34	4.029	0.300	1.153	0.172	18.99	3.41	8.04	1.35	159.31	18.74	0.162	–	S
5411	23 03 48.72	0.75	-57 48 09.07	0.90	1.678	0.325	1.072	0.214	7.00	2.20	4.76	1.63	19.24	65.48	0.192	–	S
5412	23 03 39.86	0.91	-57 59 57.70	0.85	1.531	0.296	0.941	0.197	6.89	2.24	5.52	1.83	132.53	97.23	0.176	–	S
5413	23 02 54.99	0.23	-58 57 04.72	0.23	4.309	0.387	3.720	0.276	4.17	0.46	1.78	0.38	49.03	27.86	0.179	–	S
5414	23 04 55.71	0.15	-56 08 22.50	0.15	21.761	1.247	19.564	1.096	2.79	0.09	2.54	0.09	19.92	53.64	0.204	-0.35	S
5415	23 06 28.47	0.29	-53 35 44.14	0.29	2.555	0.316	2.383	0.213	2.63	0.60	1.58	0.57	100.22	92.32	0.165	–	S
5416	23 06 54.59	0.84	-52 46 41.56	0.60	3.212	0.250	1.211	0.148	15.41	2.23	6.00	0.94	65.99	16.44	0.129	–	S
5417	23 02 07.13	0.24	-59 54 49.25	0.25	6.599	0.539	4.860	0.368	5.07	0.50	4.22	0.44	25.69	45.90	0.239	–	S
5418	23 02 10.52	0.56	-59 50 26.49	0.54	2.899	0.555	2.321	0.353	4.45	1.36	3.22	1.12	143.64	90.83	0.315	–	S
5419	23 05 49.59	0.71	-54 41 02.73	0.70	2.353	0.324	1.338	0.216	7.23	1.65	6.73	1.58	130.77	137.03	0.187	–	S
5420	23 05 01.24	1.35	-55 56 22.51	0.81	16.171	0.967	2.116	0.258	23.35	3.52	6.70	1.06	32.77	9.98	0.230	–	M
5421	23 04 59.97	0.56	-55 58 14.68	0.36	7.034	0.503	2.962	0.286	12.22	1.29	6.56	0.74	106.75	16.72	0.221	–	S
5422	23 06 02.56	0.51	-54 17 54.70	0.64	0.863	0.241	0.863	0.143	0.00	1.59	0.00	0.99	0.00	37.29	0.136	–	S
5423	23 05 10.36	1.77	-55 40 46.18	0.61	23.928	1.423	2.673	0.284	31.39	4.25	7.67	1.02	18.39	8.43	0.243	–	M
5424	23 07 53.59	1.50	-50 41 17.24	0.89	2.227	0.225	0.774	0.150	15.08	3.86	7.63	1.76	108.47	26.54	0.140	–	S
5425	23 02 55.74	0.24	-58 47 29.80	0.23	5.571	0.470	4.507	0.332	4.60	0.46	2.86	0.39	128.86	29.07	0.211	–	S
5426	23 07 26.21	0.14	-51 35 27.67	0.15	36.417	2.034	32.045	1.776	4.06	0.07	1.38	0.05	142.28	7.45	0.209	-0.96	S
5427	23 06 54.52	0.87	-52 37 01.35	0.59	3.012	0.290	1.310	0.188	11.78	2.14	6.81	1.25	84.01	26.24	0.162	–	S
5428	23 05 21.99	1.23	-55 15 00.42	1.99	21.007	1.378	9.346	0.601	37.20	5.45	3.38	0.69	126.25	6.76	0.311	–	M
5429	23 06 23.57	0.24	-53 33 04.59	0.21	6.708	0.491	4.924	0.340	6.48	0.47	2.94	0.33	78.44	15.04	0.195	–	S
5430	23 05 17.43	0.48	-55 22 57.94	0.52	4.683	0.388	2.213	0.241	10.53	1.33	6.43	0.89	43.22	23.94	0.193	–	S
5431	23 03 16.05	0.15	-58 18 05.64	0.16	14.687	0.869	14.409	0.814	1.47	0.11	0.55	0.10	102.73	42.98	0.186	-0.27	S
5432	23 06 09.40	0.95	-53 55 37.82	1.15	3.850	0.331	1.194	0.210	13.79	2.80	10.36	2.08	27.45	49.94	0.191	–	S
5433	23 02 55.85	0.27	-58 43 18.10	0.64	4.981	0.411	2.578	0.253	12.38	1.48	1.48	0.53	7.69	12.99	0.206	–	S
5434	23 07 06.65	0.57	-52 00 03.96	0.37	32.073	2.009	8.209	0.651	17.67	1.30	10.43	0.79	11.44	9.59	0.469	–	M
5435	23 06 12.32	1.07	-53 48 56.74	1.54	2.559	0.249	0.802	0.166	15.67	3.88	8.64	2.14	28.76	33.00	0.155	–	S
5436	23 05 36.74	0.45	-54 48 49.58	0.40	2.409	0.263	1.577	0.172	6.58	1.04	5.03	0.85	91.87	50.30	0.139	–	S
5437	23 06 19.52	0.49	-53 36 02.65	0.52	2.097	0.327	1.593	0.211	5.83	1.29	3.13	0.97	45.51	45.45	0.182	–	S
5438	23 03 18.26	0.14	-58 12 35.51	0.15	47.183	2.632	32.527	1.803	6.02	0.08	5.01	0.07	12.83	4.33	0.221	-0.98	M
5439	23 06 34.75	1.15	-53 05 12.41	1.12	1.831	0.251	0.816	0.172	12.10	3.32	6.16	1.84	53.14	35.20	0.156	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5440	23 07 06.47	0.21	-52 01 49.73	0.20	12.821	1.014	11.410	0.764	0.00	0.39	0.00	0.28	0.00	17.22	0.426	-	S
5441	23 06 27.58	0.45	-53 14 31.40	0.55	6.926	0.469	2.541	0.250	13.18	1.36	8.30	0.88	35.08	20.14	0.196	-	S
5442	23 04 45.40	0.53	-56 04 17.47	0.68	2.302	0.416	1.700	0.268	6.06	1.62	3.09	1.15	173.95	44.60	0.238	-	S
5443	23 05 40.12	0.15	-54 34 46.80	0.16	12.199	0.729	10.965	0.627	4.02	0.15	0.00	0.12	170.27	10.51	0.167	-0.84	S
5444	23 06 08.98	0.17	-53 44 31.10	0.17	28.885	1.640	13.996	0.796	10.84	0.23	9.46	0.20	169.18	7.94	0.201	-0.52	M
5445	23 06 38.55	0.91	-52 51 50.34	0.88	1.271	0.204	0.696	0.138	7.95	2.15	6.81	2.03	69.89	137.40	0.122	-	S
5446	23 06 03.07	1.05	-53 54 56.27	1.94	3.946	0.307	0.921	0.185	20.38	4.72	9.86	2.21	19.23	26.80	0.184	-	S
5447	23 04 09.55	0.37	-56 51 58.35	0.37	2.820	0.330	2.114	0.218	5.33	0.89	3.68	0.71	144.19	42.52	0.174	-	S
5448	23 05 59.12	0.14	-53 57 05.35	0.15	39.460	2.232	33.131	1.838	3.52	0.07	3.03	0.06	88.89	14.66	0.243	-0.75	M
5449	23 03 42.30	0.14	-57 27 55.51	0.15	63.888	3.550	61.198	3.379	2.12	0.04	1.09	0.04	78.78	13.89	0.293	-0.92	S
5450	23 07 59.54	0.29	-50 03 41.50	0.33	3.359	0.365	2.726	0.245	4.72	0.70	3.25	0.61	28.02	59.17	0.186	-	S
5451	23 04 26.12	0.16	-56 24 40.10	0.18	11.987	0.706	8.076	0.474	6.97	0.23	3.79	0.17	155.87	9.90	0.154	-1.16	S
5452	23 06 10.54	0.37	-53 33 55.45	0.22	8.673	0.682	5.116	0.346	11.27	0.83	1.17	0.33	172.29	5.03	0.201	-	M
5453	23 02 38.87	0.16	-58 49 27.35	0.16	25.984	1.533	16.109	0.916	7.71	0.20	2.59	0.12	9.30	2.50	0.234	-0.90	M
5454	23 03 33.83	0.22	-57 36 35.02	0.23	135.129	15.024	140.641	10.730	0.00	0.43	0.00	0.39	0.00	80.95	7.515	-	S
5455	23 05 28.66	0.81	-54 44 04.68	0.73	0.964	0.283	0.828	0.174	4.47	2.01	1.28	1.53	124.67	73.73	0.163	-	S
5456	23 05 38.16	0.98	-54 27 10.53	1.38	3.364	0.394	0.769	0.167	10.65	3.85	0.00	0.92	129.07	15.21	0.162	-	M
5457	23 02 57.69	0.15	-58 22 32.68	0.16	13.631	0.823	12.683	0.726	2.68	0.13	1.50	0.13	106.28	23.97	0.197	0.36	S
5458	23 05 53.89	0.14	-53 57 16.43	0.15	87.225	4.822	73.845	4.069	4.25	0.03	3.33	0.03	120.32	2.86	0.248	-0.88	M
5459	23 03 16.17	1.37	-57 57 37.04	1.11	3.702	0.291	0.928	0.177	15.16	3.27	12.16	2.52	109.64	59.91	0.168	-	S
5460	23 07 49.71	0.42	-50 15 34.09	0.48	2.069	0.269	1.507	0.176	5.59	1.04	4.48	0.96	164.40	81.19	0.146	-	S
5461	23 02 02.11	0.74	-59 29 36.45	0.50	19.112	1.282	7.979	0.543	18.05	2.00	0.00	0.43	37.90	5.28	0.319	-	M
5462	23 02 17.31	1.29	-59 11 32.18	0.79	2.619	0.457	1.387	0.310	9.93	3.00	4.87	1.80	87.85	41.81	0.280	-	S
5463	23 06 48.05	0.64	-52 17 06.23	0.79	19.232	1.169	4.924	0.484	22.18	2.24	7.51	0.77	43.29	12.17	0.421	-	S
5464	23 07 46.28	0.14	-50 19 19.40	0.16	14.150	0.816	13.576	0.761	2.49	0.10	0.36	0.08	22.43	15.73	0.143	-0.43	S
5465	23 04 43.39	0.75	-55 50 50.05	1.38	2.700	0.281	1.001	0.188	14.01	3.28	7.00	1.67	9.46	27.82	0.172	-	S
5466	23 01 44.34	1.33	-59 44 33.40	1.51	3.784	0.317	1.045	0.199	18.93	4.38	7.24	1.67	147.81	22.74	0.196	-	S
5467	23 03 49.03	0.17	-57 03 53.45	0.18	8.015	0.534	6.768	0.415	3.73	0.25	3.00	0.22	145.75	33.69	0.177	-	S
5468	23 05 19.64	1.72	-54 45 28.62	1.34	3.771	0.267	0.737	0.148	19.40	4.26	13.48	2.87	74.46	41.19	0.150	-	S
5469	23 07 18.74	0.33	-51 09 01.86	0.38	2.822	0.334	2.242	0.221	5.03	0.83	3.29	0.69	22.52	53.14	0.176	-	S
5470	23 07 15.01	0.98	-51 12 12.34	0.75	10.235	0.594	1.712	0.190	22.03	2.54	14.93	1.47	116.85	18.60	0.182	-	S
5471	23 02 58.34	0.25	-58 09 30.44	0.28	3.588	0.364	3.056	0.250	4.30	0.57	1.83	0.47	13.39	29.44	0.179	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5472	23 05 19.11	0.55	-54 42 39.20	0.93	2.776	0.268	1.208	0.173	12.34	2.24	5.98	1.15	171.26	22.36	0.151	–	S
5473	23 06 13.69	1.43	-53 05 39.18	1.51	15.007	0.854	1.507	0.215	28.76	4.04	20.34	2.80	47.69	29.93	0.256	–	S
5474	23 06 48.17	1.21	-51 56 33.11	1.09	14.731	1.112	2.903	0.400	15.31	3.33	8.93	1.87	145.77	24.01	0.367	–	M
5475	23 03 44.86	0.19	-57 00 03.76	0.21	6.010	0.440	4.847	0.322	4.71	0.36	2.88	0.30	16.91	22.67	0.172	–	S
5476	23 06 09.60	0.16	-53 09 27.70	0.17	10.414	0.659	8.667	0.517	4.10	0.22	3.15	0.19	58.16	30.58	0.192	0.03	S
5477	23 06 11.94	0.64	-53 05 01.01	0.67	3.933	0.430	2.040	0.282	9.91	1.86	5.55	1.10	141.52	26.27	0.241	–	S
5478	23 06 10.47	2.26	-53 04 19.18	1.39	22.035	1.221	1.215	0.156	44.68	5.67	24.88	2.84	111.02	18.05	0.234	–	S
5479	23 04 54.76	0.67	-55 13 46.99	0.68	5.016	0.423	1.971	0.264	10.41	1.56	9.47	1.54	38.46	148.76	0.223	–	S
5480	23 07 24.90	0.27	-50 42 26.19	0.27	3.000	0.295	2.523	0.204	4.15	0.58	2.84	0.48	115.58	40.92	0.144	–	S
5481	23 05 49.39	0.72	-53 41 40.64	0.88	1.457	0.239	0.865	0.159	7.57	2.04	5.77	1.67	5.26	77.72	0.141	–	S
5482	23 03 31.01	0.49	-57 14 46.77	0.76	5.908	0.581	2.853	0.376	11.07	1.83	5.26	1.01	21.06	22.11	0.320	–	S
5483	23 07 10.75	0.92	-51 06 54.27	1.19	7.292	0.447	1.334	0.184	20.00	2.83	14.97	2.08	18.38	37.02	0.180	–	S
5484	23 07 39.20	0.14	-50 04 49.85	0.15	54.930	3.082	40.253	2.228	6.68	0.08	1.59	0.05	103.59	1.23	0.250	-1.01	M
5485	23 01 50.10	0.20	-59 21 17.93	0.22	20.373	1.536	16.189	1.104	4.78	0.39	2.92	0.32	164.28	22.01	0.623	–	S
5486	23 01 44.40	0.37	-59 27 34.94	0.37	5.011	0.685	4.114	0.447	3.72	0.81	3.55	0.80	160.81	95.80	0.370	–	S
5487	23 02 20.39	0.49	-58 42 37.62	0.37	6.819	0.493	2.970	0.285	11.03	1.11	6.96	0.79	81.08	22.23	0.217	–	S
5488	23 07 13.84	0.20	-50 52 46.42	0.18	6.459	0.505	4.873	0.311	0.00	0.36	0.00	0.20	0.00	5.38	0.157	–	M
5489	23 02 37.33	0.59	-58 19 21.07	0.75	2.032	0.301	1.276	0.197	8.81	1.94	2.81	1.06	34.75	26.23	0.175	–	S
5490	23 01 32.52	0.36	-59 38 16.13	0.37	6.777	0.555	3.779	0.351	8.37	0.89	5.53	0.68	44.01	25.63	0.261	–	S
5491	23 03 27.54	0.74	-57 12 00.71	0.85	3.115	0.469	1.733	0.315	7.75	2.06	6.31	1.63	176.07	74.64	0.277	–	S
5492	23 07 12.93	0.95	-50 53 34.40	1.75	3.785	0.273	0.865	0.153	21.31	4.26	10.15	1.97	20.76	24.08	0.151	–	S
5493	23 01 44.78	0.39	-59 20 31.54	0.57	86.366	5.049	25.074	1.534	20.48	1.41	9.69	0.65	122.92	6.07	0.671	–	M
5494	23 04 50.23	0.81	-55 08 09.39	0.25	4.906	0.471	2.447	0.224	0.00	1.89	0.00	0.47	0.00	6.78	0.179	–	M
5495	23 03 48.09	0.88	-56 40 35.12	1.52	1.977	0.229	0.735	0.158	13.33	3.63	7.42	2.00	4.52	34.27	0.145	–	S
5496	23 01 12.83	0.18	-59 57 04.12	0.25	51.860	3.055	19.969	1.195	13.42	0.51	4.21	0.22	72.97	2.94	0.472	–	M
5497	23 04 34.89	0.57	-55 29 22.32	0.69	1.739	0.269	1.137	0.177	7.02	1.66	4.53	1.24	22.66	50.33	0.154	–	S
5498	23 04 22.58	0.64	-55 48 12.38	0.86	1.533	0.329	1.111	0.211	6.45	2.06	3.07	1.41	12.69	49.66	0.191	–	S
5499	23 06 57.89	0.42	-51 18 11.84	0.54	9.775	0.618	3.340	0.297	15.82	1.40	7.55	0.69	38.66	13.50	0.225	–	S
5500	23 07 17.36	0.87	-50 38 39.80	0.87	2.135	0.278	1.045	0.188	8.55	2.05	8.24	1.98	116.78	133.09	0.164	–	S
5501	23 03 20.68	0.49	-57 15 46.21	0.52	2.194	0.514	2.085	0.315	2.88	1.25	0.00	1.04	35.20	87.89	0.290	–	S
5502	23 04 48.63	0.44	-55 04 24.11	0.52	1.290	0.301	1.274	0.183	0.00	1.20	0.00	0.95	0.00	62.45	0.169	–	S
5503	23 03 28.34	0.28	-57 02 54.74	0.33	4.015	0.366	2.796	0.243	6.17	0.72	4.13	0.57	174.74	28.18	0.177	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5504	23 04 45.77	0.97	-55 06 02.58	0.81	3.744	0.327	1.294	0.208	12.44	2.35	9.64	1.80	79.07	51.30	0.184	–	S
5505	23 05 04.25	0.58	-54 36 37.54	0.72	2.149	0.293	1.277	0.194	7.93	1.72	5.32	1.26	20.07	46.96	0.167	–	S
5506	23 06 49.04	0.83	-51 29 39.90	1.01	2.074	0.330	1.130	0.223	8.78	2.47	6.15	1.79	156.86	55.58	0.198	–	S
5507	23 07 24.97	0.38	-50 14 25.49	0.57	2.693	0.313	1.807	0.205	8.59	1.35	2.64	0.74	24.56	20.67	0.169	–	S
5508	23 04 47.34	1.00	-55 01 15.65	1.03	3.954	0.310	1.131	0.187	14.60	2.71	10.84	2.00	48.24	44.98	0.170	–	S
5509	23 02 22.90	0.66	-58 26 14.30	0.64	0.997	0.285	0.917	0.173	3.58	1.68	0.00	1.31	51.23	83.64	0.163	–	S
5510	23 02 31.95	0.55	-58 13 22.09	0.52	3.545	0.318	1.699	0.202	9.27	1.37	7.08	1.05	137.47	35.97	0.166	–	S
5511	23 02 01.39	0.49	-58 50 38.41	0.51	2.304	0.365	1.736	0.236	4.76	1.16	4.17	1.08	10.17	126.29	0.204	–	S
5512	23 03 34.44	0.83	-56 46 45.76	1.19	3.306	0.427	1.453	0.292	10.76	2.85	7.12	1.87	6.26	43.60	0.261	–	S
5513	23 06 26.37	0.54	-52 04 11.23	0.53	2.462	0.398	1.842	0.258	5.11	1.25	4.30	1.17	115.55	98.98	0.224	–	S
5514	23 07 13.31	0.47	-50 31 25.89	0.47	2.075	0.306	1.614	0.198	5.94	1.27	2.17	0.83	133.00	30.72	0.169	–	S
5515	23 06 08.18	0.98	-52 38 03.52	0.88	1.400	0.250	0.825	0.166	9.27	2.70	4.21	1.56	58.98	37.58	0.150	–	S
5516	23 03 32.66	1.36	-56 45 40.02	1.14	19.425	1.090	1.814	0.221	29.29	3.45	20.66	2.31	127.98	22.79	0.263	–	S
5517	23 02 31.28	0.20	-58 08 09.49	0.26	11.258	0.675	5.620	0.362	11.11	0.53	4.34	0.26	159.73	9.63	0.178	–	S
5518	23 06 31.96	0.18	-51 50 32.08	0.17	10.049	0.775	8.131	0.503	0.00	0.27	0.00	0.19	0.00	7.24	0.230	–	M
5519	23 05 28.86	0.95	-53 44 42.39	0.97	1.846	0.232	0.821	0.158	9.62	2.30	8.42	2.17	47.38	166.88	0.140	–	S
5520	23 01 22.66	0.24	-59 31 12.26	0.24	7.507	0.688	6.357	0.484	3.64	0.47	2.99	0.42	48.88	92.83	0.323	–	S
5521	23 02 32.78	0.43	-58 04 38.97	0.51	1.981	0.298	1.511	0.193	5.46	1.19	3.10	0.91	17.87	44.46	0.166	–	S
5522	23 01 36.23	0.14	-59 13 21.23	0.15	73.781	4.138	72.933	4.039	0.00	0.05	0.00	0.05	0.00	17.19	0.468	0.77	S
5523	23 01 17.86	1.32	-59 34 48.17	1.23	4.147	0.396	1.277	0.263	15.14	3.63	8.67	2.15	52.59	35.20	0.246	–	S
5524	23 03 23.52	0.36	-56 54 28.44	0.42	2.951	0.298	1.910	0.196	6.67	0.96	4.93	0.76	175.78	37.27	0.154	–	S
5525	23 05 10.62	1.35	-54 08 51.02	1.77	2.321	0.230	0.690	0.156	17.68	4.79	7.90	2.17	38.17	29.52	0.150	–	S
5526	23 04 24.62	0.70	-55 21 59.28	0.78	1.429	0.283	0.993	0.184	5.82	1.79	4.74	1.62	1.05	116.65	0.165	–	S
5527	23 06 35.57	0.55	-51 35 06.96	0.76	3.191	0.400	1.836	0.263	9.41	1.91	4.43	1.07	158.00	26.16	0.228	–	S
5528	23 03 25.90	0.60	-56 45 26.58	0.78	12.041	0.723	2.615	0.281	17.05	1.83	13.14	1.34	4.86	25.38	0.247	–	S
5529	23 07 10.12	1.89	-50 20 57.12	1.14	3.719	0.400	0.819	0.167	16.47	5.12	0.00	0.66	35.05	10.71	0.161	–	M
5530	23 02 56.58	0.54	-57 24 29.73	0.63	2.307	0.412	1.716	0.266	5.64	1.53	3.39	1.14	166.72	52.59	0.235	–	S
5531	23 02 32.78	0.22	-57 55 32.20	0.23	5.118	0.395	3.892	0.276	4.47	0.41	4.35	0.40	0.79	112.81	0.165	–	S
5532	23 01 08.05	1.11	-59 39 31.63	0.82	2.662	0.401	1.322	0.274	9.38	2.61	6.38	1.87	104.22	59.08	0.244	–	S
5533	23 06 51.06	0.69	-50 59 51.31	1.36	1.922	0.261	0.919	0.176	12.49	3.26	4.77	1.47	173.50	26.76	0.160	–	S
5534	23 06 18.68	0.14	-51 59 54.21	0.15	47.209	2.645	45.546	2.522	1.99	0.06	0.94	0.05	160.47	16.45	0.292	-0.92	S
5535	23 05 02.28	0.18	-54 13 57.45	0.21	9.929	0.631	6.806	0.427	6.86	0.34	3.85	0.25	177.61	12.92	0.193	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5536	23 07 00.78	0.45	-50 34 29.28	0.32	2.381	0.350	1.221	0.154	0.00	1.04	0.00	0.63	0.00	20.44	0.139	–	M
5537	23 01 56.78	0.90	-58 36 35.95	0.66	2.538	0.402	1.505	0.266	8.70	2.20	4.10	1.34	122.20	34.25	0.237	–	S
5538	23 04 59.87	0.33	-54 14 52.83	0.26	6.092	0.579	4.154	0.299	9.48	0.79	0.00	0.33	35.29	5.75	0.193	–	M
5539	23 04 07.61	0.89	-55 37 32.65	0.98	1.833	0.256	0.897	0.174	9.32	2.51	6.90	1.80	151.30	53.95	0.154	–	S
5540	23 01 58.31	0.71	-58 33 08.34	0.67	1.292	0.314	1.045	0.197	4.80	1.81	2.54	1.37	136.12	73.30	0.181	–	S
5541	23 04 57.64	0.83	-54 14 52.99	1.44	3.646	0.329	1.149	0.213	15.40	3.42	8.67	1.88	6.80	29.69	0.197	–	S
5542	23 05 22.36	0.64	-53 33 49.03	0.79	1.421	0.230	0.902	0.152	7.79	1.94	4.41	1.34	30.55	44.22	0.134	–	S
5543	23 00 53.73	0.49	-59 47 36.44	0.52	3.189	0.391	1.997	0.257	6.30	1.25	5.71	1.05	5.42	88.96	0.215	–	S
5544	23 06 43.00	0.55	-51 03 06.40	0.60	1.937	0.328	1.438	0.212	6.02	1.47	3.60	1.15	45.78	56.99	0.186	–	S
5545	23 03 01.48	1.42	-57 04 40.63	0.74	15.241	1.013	4.211	0.321	17.22	3.34	9.03	1.67	178.91	18.15	0.222	–	M
5546	23 03 52.36	0.36	-55 53 52.71	0.63	5.500	0.434	2.514	0.263	11.93	1.47	5.39	0.74	174.50	16.54	0.211	–	S
5547	23 04 06.98	0.19	-55 31 07.52	0.19	6.342	0.509	4.773	0.306	4.45	0.34	0.00	0.22	44.77	6.72	0.156	–	M
5548	23 02 07.29	0.59	-58 17 10.78	0.75	1.557	0.307	1.138	0.197	6.12	1.82	3.02	1.26	170.73	46.00	0.177	–	S
5549	23 03 42.70	1.31	-56 06 46.65	2.55	19.465	1.111	1.753	0.290	35.80	6.20	17.35	2.76	172.69	21.36	0.377	–	S
5550	23 07 08.44	0.16	-50 08 07.47	0.17	8.023	0.530	8.003	0.472	0.00	0.19	0.00	0.16	0.00	19.58	0.169	-0.57	S
5551	23 05 09.89	0.67	-53 47 57.70	0.76	1.180	0.286	0.948	0.180	4.74	1.72	3.16	1.55	20.41	112.97	0.165	–	S
5552	23 06 16.58	0.14	-51 47 46.64	0.15	22.598	1.297	20.996	1.176	2.46	0.09	2.01	0.08	135.41	29.01	0.216	-0.58	S
5553	23 04 38.30	0.19	-54 37 31.13	0.19	9.379	0.585	4.640	0.292	5.16	0.32	2.32	0.25	26.13	10.87	0.143	–	M
5554	23 06 26.27	0.55	-51 24 07.70	0.43	38.089	2.339	9.141	0.630	28.41	1.54	5.69	0.35	41.29	3.31	0.380	–	M
5555	23 02 08.31	0.66	-58 08 40.98	0.77	2.386	0.306	1.274	0.204	8.54	1.88	6.14	1.40	25.75	49.33	0.177	–	S
5556	23 03 37.57	0.53	-56 05 56.70	0.60	23.400	1.383	5.405	0.513	15.71	1.41	13.36	1.16	17.95	33.39	0.421	–	S
5557	23 03 19.99	0.31	-56 31 11.95	0.39	3.499	0.316	2.238	0.207	7.30	0.86	4.49	0.63	12.60	24.81	0.155	–	S
5558	23 04 21.79	0.47	-54 58 33.37	0.88	7.448	0.468	1.982	0.212	18.69	2.09	8.76	0.97	16.44	15.39	0.184	–	S
5559	23 04 42.45	0.92	-54 21 37.49	2.18	3.779	0.261	0.746	0.140	24.10	5.21	10.05	2.01	178.76	22.46	0.146	–	S
5560	23 04 11.97	0.65	-55 09 33.89	0.66	1.213	0.317	1.066	0.196	3.41	1.54	2.51	1.46	47.02	5.29	0.181	–	S
5561	23 06 16.49	1.02	-51 35 21.94	0.85	1.931	0.347	1.130	0.232	8.53	2.67	5.01	1.68	121.22	44.23	0.208	–	S
5562	23 06 54.46	0.15	-50 16 58.90	0.16	8.547	0.530	8.031	0.465	2.54	0.16	1.60	0.14	2.63	36.02	0.142	-0.47	S
5563	23 05 02.87	0.32	-53 43 46.92	0.30	1.774	0.250	1.716	0.164	0.00	0.73	0.00	0.56	0.00	36.95	0.133	–	S
5564	23 02 07.11	0.92	-58 00 46.91	0.70	1.890	0.289	1.051	0.194	8.39	2.16	5.70	1.59	93.06	57.73	0.171	–	S
5565	23 00 37.37	0.70	-59 48 30.39	0.59	1.868	0.391	1.456	0.248	6.01	1.76	1.25	1.15	131.53	38.79	0.225	–	S
5566	23 04 30.77	0.45	-54 33 37.79	0.49	3.083	0.290	1.679	0.187	7.69	1.12	6.98	0.99	168.89	78.99	0.150	–	S
5567	23 00 59.21	1.47	-59 18 28.91	1.67	33.254	2.083	5.320	0.525	17.03	4.39	11.39	2.82	132.14	34.47	0.436	–	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
5568	23 06 21.00	0.66	-51 19 17.48	0.68	2.003	0.428	1.559	0.272	4.39	1.60	4.35	1.49	122.29	4.85	0.246	–	S
5569	23 04 45.49	0.72	-54 07 03.90	0.67	1.399	0.277	1.010	0.179	5.65	1.74	4.25	1.46	122.95	85.83	0.160	–	S
5570	23 01 45.95	1.40	-58 21 40.13	1.33	4.497	0.429	1.128	0.181	15.55	4.47	0.00	0.73	49.32	10.83	0.170	–	M
5571	23 01 22.89	0.14	-58 49 31.58	0.15	148.261	8.300	147.351	8.154	0.00	0.05	0.00	0.05	0.00	15.03	0.895	-0.43	S
5572	23 06 52.31	0.80	-50 13 08.88	0.67	2.125	0.265	1.116	0.177	8.85	1.98	6.78	1.44	97.24	47.77	0.153	–	S
5573	23 03 53.42	0.42	-55 27 21.94	0.48	2.122	0.288	1.559	0.188	6.06	1.15	3.41	0.87	31.91	39.84	0.158	–	S
5574	23 03 49.21	0.58	-55 30 51.61	0.58	6.874	0.505	1.757	0.189	11.08	1.63	5.81	0.92	141.12	15.22	0.162	–	M
5575	23 03 05.77	1.83	-56 33 59.34	0.87	4.960	0.489	1.837	0.202	20.52	4.68	0.00	0.76	29.23	9.63	0.175	–	M
5576	23 01 23.72	0.31	-58 45 59.97	0.25	10.558	0.944	5.207	0.394	7.78	0.68	3.88	0.43	166.34	9.84	0.271	–	M
5577	23 01 05.92	1.61	-59 07 24.24	1.24	5.303	0.457	1.474	0.291	18.97	4.33	7.49	1.84	60.27	25.11	0.284	–	S
5578	23 06 03.34	0.71	-51 40 51.11	0.89	1.336	0.282	0.935	0.183	6.37	2.04	4.26	1.65	171.70	76.22	0.165	–	S
5579	23 02 10.08	0.61	-57 42 32.24	0.54	1.883	0.332	1.398	0.214	5.58	1.49	3.57	1.15	125.00	59.75	0.189	–	S
5580	23 01 22.52	0.16	-58 40 12.18	0.17	9.519	0.660	10.277	0.609	0.00	0.17	0.00	0.16	0.00	21.75	0.230	0.46	S
5581	23 04 33.18	1.99	-54 14 27.32	0.98	4.227	0.449	1.222	0.192	16.73	5.11	0.00	0.92	29.71	12.94	0.180	–	M
5582	23 02 11.68	0.61	-57 32 56.01	0.59	10.811	0.709	3.277	0.354	13.85	1.59	10.13	1.11	140.78	24.06	0.293	–	S
5583	23 03 45.75	1.25	-55 23 11.50	0.62	13.806	0.794	2.075	0.233	26.55	2.94	13.07	1.39	96.22	16.02	0.236	–	S
5584	23 06 05.11	0.26	-51 28 19.59	0.48	16.171	1.118	6.820	0.477	13.00	1.12	2.07	0.39	113.41	5.44	0.295	–	M
5585	23 01 54.46	1.27	-57 56 46.38	1.36	6.625	0.473	1.147	0.171	17.55	4.19	2.89	1.17	53.24	13.80	0.159	–	M
5586	23 04 48.27	1.01	-53 45 02.49	0.82	2.106	0.334	0.771	0.147	7.67	2.96	0.00	0.61	146.63	12.14	0.140	–	M
5587	23 04 51.90	0.15	-53 36 05.50	0.16	11.867	0.701	10.445	0.595	3.14	0.13	2.81	0.12	12.94	64.21	0.150	-0.54	S
5588	23 03 01.12	0.57	-56 25 08.64	0.55	1.333	0.253	1.061	0.161	4.95	1.43	2.83	1.11	137.22	59.74	0.144	–	S
5589	23 05 34.39	0.15	-52 20 52.92	0.17	9.550	0.595	8.618	0.502	3.32	0.18	1.92	0.15	7.04	22.06	0.162	-1.27	S
5590	23 05 21.64	0.18	-52 43 16.85	0.18	4.972	0.351	4.398	0.275	3.66	0.28	2.06	0.24	72.04	26.20	0.128	–	S
5591	23 04 54.88	0.70	-53 29 41.78	1.02	1.212	0.251	0.849	0.160	9.19	2.68	0.00	1.14	34.44	25.73	0.149	–	S
5592	23 01 51.09	1.37	-57 56 55.02	1.13	2.807	0.260	0.838	0.172	14.53	3.43	9.82	2.35	65.59	46.22	0.160	–	S
5593	23 02 25.93	0.16	-57 10 41.64	0.17	11.067	0.708	9.717	0.577	3.33	0.20	2.49	0.18	130.07	30.06	0.211	-0.04	S
5594	23 03 15.94	0.33	-56 00 24.16	0.44	66.849	3.830	15.468	1.020	16.57	1.03	10.84	0.65	117.95	8.15	0.562	–	M
5595	23 03 41.58	0.87	-55 24 36.18	1.01	1.714	0.374	1.108	0.246	7.48	2.56	4.25	1.78	34.93	59.36	0.223	–	S
5596	23 04 34.48	0.90	-54 01 41.47	1.05	1.071	0.212	0.644	0.142	8.33	2.68	4.76	1.82	38.19	54.45	0.128	–	S
5597	23 03 11.19	1.11	-56 06 54.33	0.79	33.318	1.951	2.978	0.332	16.85	2.60	12.04	1.81	11.30	24.74	0.289	–	M
5598	23 04 01.71	0.19	-54 51 56.66	0.21	4.187	0.378	4.231	0.290	0.00	0.35	0.00	0.30	0.00	37.63	0.173	–	S
5599	23 03 22.74	0.68	-55 51 02.56	0.71	2.303	0.379	1.477	0.249	6.94	1.78	4.97	1.42	42.47	71.19	0.219	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5600	23 05 05.47	0.16	-53 06 32.70	0.17	8.291	0.520	7.400	0.434	3.50	0.19	2.03	0.16	44.48	22.06	0.146	-0.81	S
5601	23 04 41.23	0.52	-53 47 36.01	0.64	1.316	0.323	1.205	0.198	0.00	1.51	0.00	1.13	0.00	58.25	0.184	-	S
5602	23 04 54.68	0.59	-53 24 19.17	0.47	2.300	0.282	1.458	0.185	8.09	1.45	4.06	0.93	73.29	28.42	0.156	-	S
5603	23 00 47.38	0.22	-59 10 05.37	0.24	16.010	1.121	10.459	0.734	7.33	0.49	3.92	0.36	39.10	15.94	0.426	-	S
5604	23 06 40.88	0.97	-50 06 50.17	1.13	1.142	0.237	0.710	0.156	9.67	3.16	2.90	1.57	45.57	34.63	0.143	-	S
5605	23 04 40.48	0.53	-53 47 15.29	0.82	5.272	0.382	1.843	0.215	15.07	2.04	7.23	0.97	162.20	17.24	0.184	-	S
5606	23 06 07.32	1.23	-51 11 30.39	0.90	5.238	0.361	1.238	0.192	17.13	3.05	12.51	1.95	96.49	31.25	0.181	-	S
5607	23 06 03.14	0.14	-51 17 02.76	0.15	135.689	7.503	101.667	5.601	6.29	0.04	0.91	0.02	155.94	0.67	0.318	-1.00	M
5608	23 06 11.00	0.24	-51 00 23.88	0.49	12.018	0.846	5.693	0.386	14.21	1.10	4.05	0.42	85.63	5.46	0.225	-	M
5609	23 06 16.84	0.36	-50 50 34.86	0.52	3.052	0.320	1.962	0.210	8.06	1.18	4.08	0.75	174.50	24.25	0.168	-	S
5610	23 02 47.79	0.15	-56 32 42.21	0.17	11.316	0.688	9.348	0.544	5.40	0.20	0.00	0.14	12.67	9.99	0.173	-0.96	S
5611	23 06 13.20	0.40	-50 55 46.19	0.60	6.395	0.445	2.462	0.245	12.83	1.38	8.15	0.87	1.32	20.81	0.191	-	S
5612	23 03 09.45	0.85	-55 59 54.54	1.12	65.640	3.628	4.495	0.416	33.69	2.65	25.49	1.94	10.26	19.79	0.502	-	S
5613	23 04 41.07	0.64	-53 40 00.60	0.76	2.642	0.297	1.343	0.196	10.47	1.98	5.49	1.18	39.89	28.44	0.169	-	S
5614	23 03 22.56	0.64	-55 40 53.58	0.61	2.110	0.292	1.283	0.193	6.79	1.52	5.98	1.36	124.92	101.48	0.167	-	S
5615	23 00 40.87	0.16	-59 10 30.52	0.17	32.911	1.958	24.324	1.419	5.65	0.20	3.39	0.16	176.78	12.10	0.447	-1.15	S
5616	23 00 27.18	0.45	-59 26 47.70	0.48	2.166	0.496	2.138	0.303	0.00	1.17	0.00	0.90	0.00	59.40	0.279	-	S
5617	23 06 24.66	1.15	-50 26 10.95	1.04	1.842	0.236	0.816	0.160	12.85	3.33	5.88	1.64	58.38	29.77	0.145	-	S
5618	23 05 20.06	0.44	-52 27 20.32	0.50	2.466	0.287	1.602	0.189	6.65	1.11	5.31	0.99	21.34	76.44	0.155	-	S
5619	23 05 59.07	0.57	-51 14 50.53	0.59	2.179	0.457	1.848	0.287	4.82	1.53	1.14	1.09	137.78	48.21	0.260	-	S
5620	23 06 21.92	0.86	-50 29 17.58	1.28	1.708	0.242	0.802	0.165	11.21	3.13	6.38	1.82	164.16	38.57	0.148	-	S
5621	23 01 06.93	0.29	-58 34 07.07	0.24	17.738	1.111	7.684	0.490	10.77	0.65	5.45	0.36	155.95	5.81	0.247	-	M
5622	23 06 31.96	1.01	-50 08 21.85	0.80	1.094	0.261	0.770	0.169	6.60	2.47	3.83	1.77	97.50	61.08	0.154	-	S
5623	23 04 11.41	0.19	-54 17 51.61	0.18	42.114	2.387	12.149	0.707	11.31	0.31	7.71	0.23	26.07	4.95	0.232	-	M
5624	23 02 54.27	0.89	-56 14 22.09	0.68	2.048	0.430	1.425	0.279	6.69	2.12	3.70	1.51	89.00	57.21	0.252	-	S
5625	23 04 32.82	1.37	-53 44 18.02	1.38	2.560	0.240	0.742	0.160	14.52	3.81	10.79	2.55	139.12	46.68	0.150	-	S
5626	23 02 33.14	1.24	-56 43 11.44	1.16	2.577	0.273	0.874	0.186	11.89	2.87	10.26	2.72	68.47	140.67	0.169	-	S
5627	23 01 57.85	0.32	-57 27 02.65	0.32	10.706	0.711	5.212	0.402	11.18	0.81	5.14	0.46	50.89	13.43	0.264	-	S
5628	23 00 56.01	0.45	-58 45 21.62	0.42	1.606	0.390	1.715	0.234	0.00	1.07	0.00	0.84	0.00	60.67	0.218	-	S
5629	23 04 40.09	0.26	-53 27 20.47	0.26	5.571	0.405	3.594	0.264	7.22	0.56	4.75	0.43	58.18	21.48	0.163	-	S
5630	23 02 01.97	0.72	-57 19 43.21	0.95	5.453	0.521	2.157	0.339	12.18	2.40	7.35	1.42	160.54	28.30	0.299	-	S
5631	23 06 19.48	0.17	-50 22 12.36	0.18	6.981	0.466	6.333	0.382	2.75	0.22	2.50	0.21	127.77	71.32	0.154	-0.66	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5632	23 05 53.56	0.87	-51 13 16.86	0.89	1.458	0.346	1.033	0.224	5.56	2.15	4.91	1.94	130.77	167.00	0.203	–	S
5633	23 01 38.62	0.47	-57 46 54.92	0.83	1.563	0.269	1.085	0.174	7.90	1.95	1.06	1.03	8.20	26.85	0.156	–	S
5634	23 02 51.30	0.57	-56 07 34.78	0.64	4.123	0.480	2.287	0.316	8.33	1.60	5.81	1.15	153.20	37.92	0.269	–	S
5635	23 05 11.83	1.12	-52 24 25.19	1.22	3.226	0.301	1.030	0.198	14.42	3.26	9.59	2.16	45.95	42.17	0.181	–	S
5636	23 03 52.66	0.91	-54 34 15.90	0.81	3.641	0.289	1.235	0.174	15.11	2.57	7.53	1.23	133.64	20.61	0.155	–	S
5637	23 01 22.39	0.70	-58 02 09.54	0.68	2.127	0.302	1.261	0.200	8.19	1.88	4.66	1.23	141.29	35.58	0.175	–	S
5638	23 01 43.45	0.98	-57 33 34.11	0.72	20.135	1.154	3.036	0.330	23.36	2.35	14.79	1.55	73.94	20.53	0.324	–	S
5639	23 06 01.76	0.75	-50 47 56.20	0.93	1.522	0.266	0.932	0.177	7.84	2.25	5.17	1.62	157.29	54.70	0.157	–	S
5640	23 04 05.16	0.59	-54 12 02.71	0.64	1.862	0.309	1.298	0.201	6.25	1.61	4.20	1.21	149.14	54.59	0.177	–	S
5641	23 00 00.03	0.68	-59 35 48.79	0.77	1.189	0.413	1.189	0.251	0.00	1.88	0.00	1.48	0.00	97.12	0.238	–	S
5642	23 01 03.43	0.78	-58 22 03.42	0.72	2.211	0.275	1.141	0.184	9.50	2.07	5.60	1.32	137.02	33.47	0.160	–	S
5643	23 01 20.71	0.15	-57 59 42.41	0.16	12.612	0.759	11.819	0.675	2.63	0.13	1.32	0.12	61.39	23.69	0.179	0.52	S
5644	23 03 09.63	0.16	-55 33 05.28	0.17	8.398	0.542	7.603	0.451	2.72	0.19	2.44	0.19	19.72	103.88	0.166	-0.32	S
5645	23 02 42.36	1.47	-56 11 39.74	1.30	5.593	0.380	1.072	0.198	18.01	3.70	14.71	2.77	125.50	50.31	0.199	–	S
5646	23 04 59.16	0.53	-52 38 06.14	0.67	1.543	0.314	1.243	0.199	5.16	1.55	2.56	1.19	175.16	58.94	0.179	–	S
5647	23 03 37.10	1.52	-54 50 33.41	1.27	4.546	0.331	0.969	0.189	16.84	3.65	14.03	2.90	93.78	66.59	0.186	–	S
5648	23 02 41.45	1.58	-56 11 59.72	1.35	3.653	0.324	0.960	0.212	16.07	4.06	10.85	2.72	63.69	47.12	0.203	–	S
5649	23 02 43.14	0.48	-56 09 06.88	0.53	2.708	0.384	1.917	0.251	5.94	1.27	4.13	0.99	158.55	50.08	0.214	–	S
5650	23 02 09.99	0.92	-56 53 26.31	0.67	3.831	0.345	1.456	0.221	11.91	2.15	8.41	1.53	100.64	38.41	0.192	–	S
5651	23 02 05.21	0.20	-56 59 38.07	0.20	6.891	0.495	5.518	0.362	4.24	0.33	3.65	0.30	99.85	63.50	0.189	–	S
5652	23 06 03.14	0.14	-50 35 02.09	0.15	20.879	1.175	19.224	1.068	2.78	0.07	2.03	0.06	61.37	19.31	0.145	-0.70	S
5653	23 05 51.83	1.24	-50 55 21.62	1.34	2.451	0.281	0.874	0.195	12.13	3.38	9.94	2.61	143.14	66.80	0.177	–	S
5654	23 03 11.45	1.57	-55 23 46.78	0.42	6.294	0.496	1.309	0.196	0.00	3.74	0.00	0.67	0.00	8.95	0.182	–	M
5655	23 00 49.00	0.93	-58 32 35.90	0.77	2.397	0.390	1.357	0.262	8.22	2.29	5.47	1.62	123.33	53.63	0.233	–	S
5656	23 04 41.90	0.62	-53 01 06.14	0.52	1.440	0.227	1.030	0.147	6.93	1.56	3.02	1.02	69.95	34.70	0.128	–	S
5657	23 02 06.80	0.67	-56 53 07.91	0.75	7.170	0.463	1.993	0.222	17.14	2.08	8.82	1.02	146.98	16.87	0.193	–	S
5658	23 04 49.68	0.20	-52 46 53.12	0.21	5.825	0.453	4.982	0.336	3.38	0.35	3.29	0.34	130.52	49.85	0.188	–	S
5659	23 05 58.34	0.56	-50 41 57.75	0.79	1.475	0.319	1.169	0.201	5.99	1.85	1.81	1.23	170.71	44.42	0.183	–	S
5660	23 00 00.07	0.57	-59 27 13.56	0.64	2.199	0.634	2.199	0.390	0.00	1.56	0.00	1.21	0.00	81.31	0.363	–	S
5661	23 01 49.25	0.31	-57 11 20.33	0.25	59.531	3.321	12.573	0.757	23.12	0.73	10.69	0.33	37.21	2.88	0.309	–	M
5662	23 04 47.43	0.64	-52 44 39.31	0.62	2.711	0.304	1.429	0.201	8.53	1.57	6.87	1.33	63.90	69.16	0.170	–	S
5663	23 03 47.24	0.34	-54 21 26.78	0.38	1.579	0.294	1.636	0.184	0.00	0.89	0.00	0.67	0.00	39.29	0.162	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
5664	23 01 00.44	0.51	-58 11 41.42	0.86	2.199	0.270	1.180	0.178	9.97	2.04	4.39	1.12	10.29	25.61	0.156	–	S
5665	23 03 07.12	1.36	-55 21 58.09	0.98	2.220	0.303	0.952	0.209	11.75	3.43	6.71	1.97	118.37	38.38	0.190	–	S
5666	23 04 16.45	0.50	-53 32 11.27	0.58	5.520	0.372	2.039	0.197	15.73	1.61	6.05	0.69	44.69	13.74	0.157	–	S
5667	23 01 05.49	0.28	-58 03 33.53	0.27	2.982	0.331	2.663	0.226	3.37	0.58	1.88	0.50	130.01	51.78	0.168	–	S
5668	23 05 25.33	0.16	-51 30 50.58	0.17	9.581	0.613	8.501	0.504	3.66	0.21	2.00	0.18	168.24	20.10	0.183	-0.67	S
5669	23 02 02.67	0.18	-56 46 41.86	0.19	6.150	0.461	5.831	0.370	3.02	0.28	0.00	0.23	145.38	20.79	0.182	–	S
5670	23 02 03.94	0.52	-56 45 02.75	0.74	3.182	0.352	1.665	0.232	9.67	1.76	5.41	1.11	20.42	28.67	0.198	–	S
5671	23 03 51.89	0.14	-54 06 45.99	0.15	204.751	11.435	204.573	11.310	0.00	0.05	0.00	0.04	0.00	14.68	1.146	0.08	S
5672	23 01 33.52	0.98	-57 24 12.71	1.66	4.992	0.553	1.708	0.380	14.69	4.06	7.51	2.08	19.01	32.80	0.355	–	S
5673	23 04 16.12	0.23	-53 26 07.99	0.23	7.101	0.492	4.725	0.325	6.71	0.46	4.73	0.37	65.68	22.49	0.182	–	S
5674	23 05 35.71	0.34	-51 06 19.52	0.36	3.832	0.369	2.646	0.244	6.97	0.87	3.97	0.62	51.03	26.68	0.184	–	S
5675	23 00 59.44	0.16	-58 02 11.18	0.17	19.830	1.171	11.843	0.675	7.99	0.22	1.91	0.12	42.65	2.58	0.176	-0.55	M
5676	23 05 51.83	0.30	-50 31 44.30	0.36	4.444	0.332	2.456	0.205	8.57	0.79	6.33	0.62	19.78	31.65	0.143	–	S
5677	23 05 10.32	0.24	-51 49 45.72	0.26	3.349	0.341	3.041	0.239	3.34	0.53	1.53	0.44	149.50	42.14	0.167	–	S
5678	23 05 02.02	0.70	-52 01 41.55	0.87	2.875	0.296	1.334	0.193	12.35	2.38	5.08	1.08	148.83	20.89	0.170	–	S
5679	23 05 10.90	0.31	-51 45 36.39	0.30	3.858	0.366	2.890	0.246	6.25	0.76	2.65	0.50	128.30	20.13	0.179	–	S
5680	23 05 52.09	0.49	-50 25 15.60	1.15	11.367	0.749	3.161	0.261	20.15	2.82	4.20	0.72	113.12	7.89	0.194	–	M
5681	23 04 43.98	0.75	-52 31 47.85	1.17	4.870	0.372	1.427	0.219	15.71	2.80	9.84	1.65	173.31	27.78	0.199	–	S
5682	23 04 39.42	1.10	-52 39 54.18	1.30	2.576	0.269	0.894	0.182	13.81	3.39	8.73	2.16	39.12	41.95	0.166	–	S
5683	23 00 50.80	0.23	-58 09 13.78	0.25	3.829	0.348	3.233	0.245	3.75	0.48	2.92	0.42	173.04	52.51	0.163	–	S
5684	23 02 23.58	0.22	-56 08 20.94	0.25	8.482	0.665	6.329	0.460	5.63	0.49	3.46	0.39	175.49	22.13	0.284	–	S
5685	23 04 41.84	0.27	-52 32 16.53	0.26	4.492	0.419	3.619	0.289	4.78	0.58	3.13	0.47	69.05	37.86	0.200	–	S
5686	23 02 14.44	0.16	-56 18 03.23	0.17	23.772	1.399	16.552	0.965	5.54	0.19	4.95	0.18	112.68	27.74	0.300	-1.52	S
5687	23 00 25.62	0.32	-58 35 58.89	0.30	4.546	0.463	3.460	0.311	4.87	0.68	3.92	0.60	74.12	85.22	0.232	–	S
5688	23 01 43.62	1.18	-56 59 27.41	1.95	6.744	0.416	0.983	0.174	24.91	4.73	14.39	2.59	17.38	26.83	0.192	–	S
5689	23 04 17.68	0.33	-53 11 16.96	0.33	2.672	0.310	2.172	0.206	4.80	0.77	2.87	0.62	64.12	44.03	0.161	–	S
5690	23 02 04.38	0.64	-56 29 40.56	0.66	1.614	0.346	1.261	0.220	4.93	1.59	3.43	1.39	43.22	106.05	0.199	–	S
5691	23 05 58.87	0.58	-50 05 45.36	0.79	2.051	0.270	1.181	0.179	8.59	1.84	5.61	1.29	171.57	43.32	0.155	–	S
5692	23 03 54.70	0.15	-53 44 56.94	0.15	79.611	4.429	30.938	1.723	12.47	0.15	6.82	0.09	1.27	1.40	0.270	-1.04	M
5693	23 03 47.71	0.54	-53 55 15.09	0.60	1.260	0.248	1.032	0.157	5.57	1.57	0.00	1.01	147.19	36.31	0.141	–	S
5694	23 03 29.94	0.28	-54 22 08.81	0.31	4.450	0.323	2.554	0.201	7.99	0.69	5.76	0.51	148.75	21.52	0.133	–	S
5695	23 03 04.60	0.32	-54 59 41.71	0.38	5.725	0.559	3.948	0.369	6.82	0.86	3.81	0.62	28.22	26.30	0.281	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
5696	23 02 37.94	0.17	-55 38 01.81	0.18	7.562	0.545	7.076	0.441	2.43	0.25	1.65	0.23	158.01	51.02	0.204	–	S
5697	23 05 28.04	0.73	-50 59 59.97	0.69	1.459	0.311	1.101	0.199	5.59	1.77	3.69	1.50	73.57	80.30	0.180	–	S
5698	23 00 35.39	0.30	-58 17 51.27	0.28	2.126	0.296	2.126	0.195	0.00	0.63	0.00	0.53	0.00	58.31	0.157	–	S
5699	23 01 28.77	0.80	-57 11 14.55	0.77	2.533	0.437	1.557	0.290	7.15	2.06	5.28	1.56	138.56	65.97	0.257	–	S
5700	23 05 38.42	1.60	-50 38 55.07	0.99	2.499	0.264	0.842	0.180	14.59	4.02	8.65	2.13	95.04	34.03	0.167	–	S
5701	23 02 00.11	0.14	-56 28 25.36	0.15	34.091	1.910	32.159	1.782	2.08	0.06	1.79	0.05	177.84	31.84	0.212	-0.37	S
5702	23 03 59.84	1.28	-53 29 32.90	1.18	2.329	0.256	0.848	0.174	14.47	3.66	7.30	1.91	56.16	31.85	0.160	–	S
5703	23 00 09.23	1.02	-58 44 12.69	0.56	4.105	0.414	1.751	0.271	12.45	2.33	5.99	1.29	97.24	25.99	0.239	–	S
5704	23 02 34.09	0.25	-55 37 42.10	0.26	4.242	0.423	3.739	0.295	3.80	0.53	1.62	0.44	147.19	33.13	0.206	–	S
5705	23 03 05.62	0.29	-54 48 27.39	0.34	54.079	3.019	7.957	0.529	19.09	0.76	14.50	0.55	126.32	6.79	0.296	–	M
5706	23 01 17.35	0.15	-57 19 39.96	0.16	25.825	1.508	22.884	1.295	2.97	0.11	2.67	0.11	175.90	37.74	0.295	-0.64	S
5707	23 04 01.57	1.22	-53 23 23.87	1.58	2.495	0.258	0.844	0.173	17.33	4.41	6.25	1.71	40.61	25.05	0.165	–	S
5708	23 05 43.25	0.36	-50 21 02.65	0.40	7.686	0.481	3.041	0.239	13.95	1.09	6.55	0.50	143.00	11.62	0.163	–	S
5709	23 02 48.40	0.39	-55 15 43.65	0.41	2.217	0.389	2.074	0.246	3.02	0.94	0.48	0.80	36.41	75.72	0.215	–	S
5710	23 04 06.84	0.59	-53 13 57.22	0.58	2.442	0.275	1.353	0.181	8.10	1.45	6.44	1.22	59.14	68.68	0.152	–	S
5711	23 03 34.42	0.61	-54 05 57.71	0.66	1.568	0.306	1.200	0.196	5.95	1.72	2.39	1.16	145.38	42.22	0.176	–	S
5712	23 01 49.93	0.14	-56 34 41.10	0.15	36.443	2.025	32.684	1.806	3.91	0.05	0.68	0.04	82.57	7.99	0.168	-1.07	S
5713	23 01 29.94	0.95	-57 01 11.30	0.91	5.750	0.403	1.476	0.218	14.54	2.42	12.39	1.89	136.35	48.22	0.199	–	S
5714	23 04 28.55	0.33	-52 35 33.43	0.43	3.203	0.370	2.377	0.244	6.22	0.98	3.08	0.68	168.52	28.43	0.195	–	S
5715	23 00 27.42	0.83	-58 17 48.73	0.77	1.877	0.289	1.071	0.193	8.73	2.19	4.91	1.46	55.77	42.51	0.171	–	S
5716	23 02 57.62	0.84	-54 58 28.69	0.72	1.359	0.451	1.259	0.270	4.89	2.21	0.00	1.35	62.57	46.60	0.259	–	S
5717	23 05 18.02	0.46	-51 03 41.25	0.45	6.761	0.584	3.143	0.270	11.71	1.40	0.00	0.38	141.18	5.84	0.208	–	M
5718	23 02 50.73	3.20	-55 04 16.17	0.59	30.348	1.845	9.937	0.666	45.00	7.54	7.69	1.23	1.48	9.54	0.381	–	M
5719	23 02 47.42	0.39	-55 09 41.72	0.24	6.453	0.587	4.588	0.389	0.00	0.87	0.00	0.43	0.00	13.91	0.286	–	S
5720	23 03 10.68	0.48	-54 34 25.30	1.09	7.704	0.460	1.727	0.175	25.23	2.65	7.39	0.78	21.77	12.57	0.162	–	S
5721	23 05 33.29	1.26	-50 30 24.07	1.74	3.161	0.237	0.695	0.139	19.32	4.29	12.29	2.69	27.50	38.64	0.138	–	S
5722	23 04 40.43	1.05	-52 06 09.85	0.97	1.452	0.277	0.832	0.187	7.49	2.43	6.54	2.26	101.99	127.43	0.167	–	S
5723	23 05 25.57	0.65	-50 42 46.63	0.59	1.277	0.289	1.083	0.180	4.31	1.52	2.39	1.31	95.12	81.07	0.165	–	S
5724	23 05 18.32	0.50	-50 52 42.28	0.53	1.583	0.298	1.340	0.188	4.03	1.19	2.85	1.12	139.78	95.96	0.167	–	S
5725	23 01 13.43	0.28	-57 10 34.73	0.45	6.872	0.533	3.721	0.329	10.24	1.02	4.07	0.54	14.65	15.10	0.243	–	S
5726	23 04 33.99	0.37	-52 09 14.40	0.37	2.424	0.313	1.967	0.205	4.22	0.82	3.58	0.78	114.67	93.93	0.167	–	S
5727	23 05 40.65	0.32	-50 06 14.16	0.37	2.265	0.293	1.952	0.193	4.26	0.80	2.25	0.67	34.57	53.35	0.155	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5728	23 03 32.00	1.73	-53 50 43.97	0.78	5.832	0.493	1.018	0.197	16.06	4.38	0.00	0.78	27.75	11.28	0.189	–	M
5729	23 04 33.25	0.28	-52 05 42.87	0.31	4.250	0.372	3.017	0.249	6.10	0.68	4.20	0.52	148.87	28.26	0.175	–	S
5730	23 04 36.55	0.54	-51 59 53.27	0.76	2.260	0.276	1.260	0.183	8.95	1.77	5.61	1.22	8.82	38.33	0.157	–	S
5731	23 05 34.83	0.54	-50 10 53.10	0.74	2.347	0.247	1.214	0.161	10.89	1.86	5.25	1.04	32.92	24.73	0.137	–	S
5732	23 02 10.37	0.32	-55 46 54.56	0.35	3.433	0.462	3.052	0.303	3.45	0.76	1.98	0.64	172.59	63.92	0.246	–	S
5733	23 01 08.31	0.89	-57 08 35.29	1.24	15.088	0.882	2.301	0.289	25.10	3.15	13.44	1.66	32.43	19.30	0.298	–	S
5734	23 02 30.70	0.15	-55 16 58.49	0.15	19.178	1.113	18.818	1.055	1.25	0.09	0.93	0.09	116.80	82.30	0.206	-0.17	S
5735	23 04 26.88	0.32	-52 12 30.46	0.87	6.411	0.515	1.745	0.217	0.00	2.03	0.00	0.67	0.00	11.21	0.194	–	M
5736	23 00 48.82	0.28	-57 31 31.45	0.29	95.399	5.410	26.482	1.544	19.58	0.73	9.29	0.35	51.44	3.53	0.512	-1.55	M
5737	23 03 41.14	0.44	-53 29 51.28	0.48	2.613	0.294	1.675	0.193	7.04	1.14	5.06	0.91	39.54	49.32	0.158	–	S
5738	22 59 59.92	1.53	-58 29 22.67	1.34	8.569	0.540	1.375	0.242	20.61	3.90	15.51	2.75	132.18	38.44	0.255	–	S
5739	23 00 45.38	0.89	-57 34 36.64	0.72	4.393	0.725	2.575	0.484	7.73	2.11	5.54	1.63	89.34	72.65	0.428	–	S
5740	23 02 16.69	0.16	-55 33 12.44	0.19	14.922	0.902	10.144	0.609	7.08	0.28	3.58	0.19	176.62	10.95	0.229	-0.91	S
5741	23 02 07.97	0.50	-55 43 40.79	0.61	11.268	0.693	3.237	0.304	17.66	1.62	8.25	0.79	40.72	14.43	0.245	–	S
5742	23 01 13.95	1.15	-56 56 45.97	1.09	2.020	0.305	0.921	0.211	9.49	2.74	7.83	2.49	59.78	130.09	0.189	–	S
5743	23 02 34.68	0.16	-55 04 24.29	0.17	16.838	1.059	14.515	0.857	3.79	0.20	2.55	0.17	25.70	23.61	0.301	-0.67	S
5744	23 03 26.74	0.40	-53 45 53.95	0.41	3.039	0.292	1.859	0.190	7.08	0.96	5.79	0.83	45.01	67.32	0.149	–	S
5745	23 04 00.21	1.03	-52 50 07.19	0.85	2.336	0.499	1.488	0.329	7.16	2.48	5.00	1.92	95.39	75.16	0.297	–	S
5746	23 00 20.62	0.28	-57 59 18.51	0.28	3.091	0.381	2.883	0.256	2.50	0.59	1.63	0.55	130.22	106.71	0.198	–	S
5747	23 01 14.18	0.26	-56 51 56.10	0.32	3.423	0.370	2.874	0.250	4.73	0.67	1.48	0.51	173.89	26.60	0.187	–	S
5748	23 00 42.84	0.29	-57 31 12.60	0.30	10.429	1.060	8.178	0.715	4.48	0.63	3.80	0.59	46.00	107.76	0.529	–	S
5749	23 04 42.38	0.27	-51 34 29.14	0.30	4.473	0.383	3.180	0.257	5.73	0.63	4.65	0.52	148.11	40.33	0.177	–	S
5750	23 04 19.05	0.81	-52 16 01.37	0.89	1.177	0.268	0.844	0.173	7.13	2.37	2.83	1.52	45.67	47.50	0.157	–	S
5751	23 05 02.79	0.67	-50 57 36.95	0.71	1.246	0.373	1.161	0.226	2.67	1.66	1.73	1.51	46.28	5.12	0.213	–	S
5752	23 01 23.13	0.68	-56 36 02.98	0.73	0.935	0.245	0.782	0.153	3.91	1.66	3.03	1.59	175.08	171.45	0.141	–	S
5753	23 04 39.85	0.81	-51 33 45.08	0.87	2.572	0.307	1.203	0.206	9.13	2.02	8.31	1.87	144.36	97.42	0.180	–	S
5754	23 05 28.91	0.65	-50 02 20.50	0.89	1.254	0.263	0.902	0.169	6.60	2.03	3.66	1.51	0.47	60.24	0.153	–	S
5755	23 04 00.22	0.44	-52 39 42.07	0.44	8.727	0.633	3.985	0.369	11.58	1.23	6.04	0.65	137.69	15.79	0.279	–	S
5756	23 03 35.62	0.81	-53 17 12.68	1.03	4.495	0.348	1.398	0.207	16.11	2.72	8.53	1.46	37.93	24.01	0.186	–	S
5757	23 01 28.96	1.39	-56 16 10.90	0.61	21.866	1.532	4.144	0.513	26.36	3.42	7.96	0.97	167.86	8.31	0.459	–	M
5758	23 03 24.31	0.15	-53 32 48.99	0.15	36.101	2.042	25.306	1.408	7.20	0.11	3.39	0.07	159.38	1.85	0.211	-0.87	M
5759	23 03 11.67	0.28	-53 52 27.20	0.38	4.214	0.351	2.628	0.227	7.91	0.82	4.54	0.57	12.95	21.28	0.164	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5760	23 01 52.83	0.21	-55 46 46.60	0.18	22.388	1.311	11.907	0.725	9.87	0.36	5.08	0.23	85.42	10.24	0.290	-1.50	S
5761	23 02 20.12	1.23	-55 08 45.21	0.37	3.937	0.561	1.512	0.244	0.00	2.89	0.00	0.74	0.00	13.62	0.229	-	M
5762	23 04 51.01	0.69	-51 02 12.00	0.89	2.530	0.322	1.326	0.214	10.64	2.30	5.13	1.30	37.48	30.07	0.188	-	S
5763	23 04 36.10	0.21	-51 28 03.10	0.23	8.117	0.574	5.818	0.395	5.37	0.41	4.92	0.36	155.49	55.48	0.217	-	S
5764	23 01 38.94	0.14	-56 02 34.62	0.15	64.600	3.601	59.340	3.282	2.78	0.05	1.83	0.05	146.83	12.64	0.342	-1.02	S
5765	23 02 09.06	0.37	-55 21 32.10	0.31	4.197	0.429	3.060	0.285	6.40	0.83	3.15	0.60	78.21	25.78	0.218	-	S
5766	23 03 52.37	1.34	-52 42 40.13	2.34	6.644	0.446	1.087	0.230	24.14	5.61	13.64	3.01	13.87	31.88	0.248	-	S
5767	23 02 06.27	0.46	-55 23 59.68	0.56	2.885	0.382	1.925	0.250	6.59	1.31	4.62	1.01	10.39	49.60	0.212	-	S
5768	23 04 33.63	0.73	-51 28 02.91	0.56	3.469	0.386	1.826	0.254	9.55	1.85	5.81	1.12	114.21	28.91	0.216	-	S
5769	23 01 48.59	0.46	-55 45 56.84	0.53	6.979	0.585	3.306	0.364	9.24	1.25	7.51	0.98	164.24	38.11	0.291	-	S
5770	23 01 47.08	2.22	-55 46 19.53	1.70	20.261	1.133	1.388	0.205	39.69	5.90	21.42	2.94	127.57	20.96	0.288	-	S
5771	23 03 33.04	0.17	-53 07 53.30	0.17	9.620	0.638	8.888	0.533	3.26	0.22	0.86	0.18	72.90	20.15	0.208	-0.71	S
5772	23 04 14.35	0.16	-51 55 36.83	0.17	7.704	0.502	7.301	0.432	2.63	0.20	0.41	0.17	133.56	22.89	0.157	-0.05	S
5773	23 00 31.21	0.35	-57 21 35.07	0.38	2.931	0.424	2.537	0.275	3.74	0.87	2.30	0.72	4.58	66.08	0.230	-	S
5774	23 02 09.07	1.57	-55 09 47.59	0.64	2.051	0.288	0.958	0.194	13.57	3.74	3.47	1.39	94.26	24.65	0.182	-	S
5775	23 03 48.72	0.24	-52 36 31.56	0.27	5.727	0.685	5.790	0.473	0.00	0.54	0.00	0.44	0.00	38.41	0.351	-	S
5776	23 00 00.46	0.65	-57 57 27.24	0.76	1.082	0.362	1.082	0.221	0.00	1.82	0.00	1.44	0.00	93.73	0.208	-	S
5777	23 04 29.94	0.81	-51 23 59.09	0.89	1.610	0.327	1.076	0.214	7.16	2.32	4.13	1.58	144.62	51.48	0.193	-	S
5778	23 00 30.69	0.32	-57 18 36.87	0.36	3.715	0.414	2.841	0.275	5.14	0.80	3.49	0.65	3.83	41.61	0.215	-	S
5779	23 02 22.56	1.28	-54 48 00.89	1.29	2.775	0.290	0.903	0.198	12.38	3.34	10.67	2.65	141.65	77.04	0.181	-	S
5780	23 00 10.51	0.47	-57 42 29.29	0.48	2.887	0.481	2.321	0.309	4.17	1.09	3.56	1.03	153.26	127.83	0.269	-	S
5781	23 03 59.64	0.67	-52 12 38.27	0.64	2.120	0.317	1.338	0.209	6.71	1.62	5.69	1.40	122.95	81.20	0.182	-	S
5782	23 03 02.58	1.52	-53 44 46.72	1.03	2.017	0.211	0.669	0.144	13.88	3.69	9.16	2.29	97.10	41.90	0.133	-	S
5783	23 02 04.65	0.18	-55 09 37.92	0.19	7.281	0.508	6.083	0.385	4.15	0.29	2.91	0.26	56.02	32.25	0.184	-	S
5784	23 04 27.58	0.18	-51 22 04.48	0.19	7.224	0.505	6.090	0.385	4.18	0.31	2.73	0.25	146.05	23.85	0.183	-	S
5785	23 03 47.61	0.43	-52 30 44.02	0.44	2.343	0.353	1.890	0.229	4.22	1.00	3.74	0.95	68.97	5.37	0.195	-	S
5786	23 01 03.71	0.63	-56 31 26.70	0.53	1.079	0.253	0.963	0.156	4.48	1.54	0.00	1.07	123.42	45.99	0.144	-	S
5787	23 01 14.54	0.76	-56 16 39.11	0.74	2.092	0.631	1.839	0.387	3.15	1.74	2.71	1.70	126.68	5.90	0.363	-	S
5788	23 04 22.75	0.19	-51 28 02.24	0.22	7.221	0.540	6.077	0.402	4.95	0.38	1.52	0.28	167.35	16.77	0.215	-	S
5789	23 01 28.52	0.37	-55 57 07.20	0.40	2.794	0.420	2.410	0.271	3.66	0.90	2.58	0.79	166.04	84.45	0.229	-	S
5790	23 04 38.49	0.32	-50 58 47.75	0.37	4.002	0.564	3.633	0.368	3.59	0.80	1.39	0.68	22.79	58.78	0.303	-	S
5791	23 03 47.79	1.07	-52 26 37.90	0.95	2.792	0.360	1.288	0.244	11.62	3.04	5.83	1.55	131.91	29.90	0.219	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5792	22 59 59.98	0.32	-57 46 10.01	0.40	2.312	0.379	2.184	0.241	0.00	0.90	0.00	0.67	0.00	35.50	0.207	–	S
5793	23 00 47.53	0.77	-56 46 56.95	0.91	1.845	0.328	1.104	0.219	7.26	2.19	5.68	1.73	4.53	81.53	0.194	–	S
5794	23 02 48.50	0.44	-53 57 37.70	0.49	1.644	0.271	1.353	0.174	4.33	1.11	3.04	0.96	163.31	79.95	0.151	–	S
5795	23 01 40.94	0.14	-55 34 06.29	0.15	124.085	6.860	98.331	5.416	0.00	0.04	0.00	0.02	0.00	0.54	0.283	-0.80	M
5796	23 04 03.15	1.26	-51 53 01.28	2.42	8.775	0.626	1.692	0.187	26.51	6.30	3.57	1.15	121.37	11.82	0.162	–	M
5797	23 04 34.36	0.17	-50 56 40.37	0.18	58.027	3.278	18.554	1.064	11.04	0.26	8.63	0.20	149.29	5.02	0.303	-1.20	M
5798	23 04 36.81	0.41	-50 52 41.42	0.33	9.819	0.672	4.564	0.381	11.58	1.02	6.16	0.57	70.78	14.99	0.268	–	S
5799	23 04 45.38	0.70	-50 34 02.66	0.97	2.008	0.298	1.110	0.200	8.98	2.27	5.86	1.59	175.45	49.80	0.176	–	S
5800	23 04 48.33	0.14	-50 27 32.47	0.15	24.385	1.370	23.098	1.281	2.15	0.06	1.72	0.06	161.64	29.71	0.163	-0.58	S
5801	23 01 47.07	1.05	-55 20 50.71	1.31	1.925	0.312	0.931	0.214	10.83	3.49	5.55	1.89	153.39	38.01	0.195	–	S
5802	23 01 51.87	0.80	-55 13 50.78	0.61	1.519	0.294	1.084	0.190	7.19	1.99	2.55	1.24	73.18	38.07	0.171	–	S
5803	23 04 08.86	0.52	-51 38 12.28	0.56	2.763	0.308	1.636	0.201	8.78	1.53	4.51	0.89	142.05	24.57	0.168	–	S
5804	23 03 06.31	0.37	-53 20 20.13	0.36	4.023	0.356	2.493	0.231	7.84	0.90	4.82	0.65	57.43	26.06	0.173	–	S
5805	23 04 07.98	0.99	-51 38 35.30	1.44	2.199	0.268	0.847	0.185	12.44	3.40	8.39	2.29	4.29	51.00	0.168	–	S
5806	23 03 25.32	1.35	-52 47 04.79	1.53	6.827	0.579	1.037	0.194	20.29	4.74	0.00	0.62	54.03	8.75	0.185	–	M
5807	23 01 52.02	0.48	-55 08 30.50	0.53	3.218	0.386	2.032	0.254	7.32	1.29	4.89	0.98	38.81	43.48	0.212	–	S
5808	23 04 51.91	0.25	-50 14 45.78	0.32	4.455	0.366	3.090	0.245	6.88	0.67	4.06	0.48	4.76	23.17	0.165	–	S
5809	23 00 45.61	0.59	-56 35 54.06	0.86	3.082	0.270	1.222	0.170	12.16	2.08	7.41	1.25	170.23	26.17	0.147	–	S
5810	23 04 52.22	0.22	-50 11 49.03	0.27	3.406	0.305	2.866	0.215	4.82	0.53	2.12	0.40	5.07	25.96	0.141	–	S
5811	23 02 19.77	0.35	-54 23 27.84	0.30	7.726	0.492	3.288	0.257	10.51	0.78	8.16	0.59	106.72	21.66	0.169	–	S
5812	23 04 34.68	0.16	-50 39 28.84	0.16	75.663	4.188	32.204	1.789	17.80	0.17	13.04	0.12	173.59	1.84	0.248	-0.04	M
5813	23 00 34.94	0.88	-56 46 31.26	0.38	5.393	0.492	1.926	0.208	0.00	2.13	0.00	0.60	0.00	8.97	0.179	–	M
5814	23 02 14.13	1.12	-54 24 23.05	1.01	2.011	0.279	0.910	0.192	10.52	2.88	7.24	2.05	63.52	57.85	0.171	–	S
5815	23 02 44.40	1.00	-53 37 07.04	1.00	1.878	0.311	0.983	0.212	7.76	2.37	7.65	2.28	32.61	5.59	0.188	–	S
5816	23 01 36.63	1.01	-55 15 37.26	1.04	2.091	0.308	0.995	0.212	9.24	2.52	7.56	2.25	44.49	113.66	0.188	–	S
5817	23 00 05.86	0.92	-57 12 12.87	2.07	7.265	0.587	1.233	0.237	17.56	5.27	0.00	0.77	118.79	11.00	0.227	–	M
5818	23 00 49.46	0.49	-56 17 09.22	0.62	16.256	1.156	5.286	0.399	16.16	1.65	6.93	0.71	130.63	8.13	0.273	–	M
5819	23 02 02.73	0.57	-54 36 16.79	0.84	0.983	0.258	0.841	0.159	0.00	1.99	0.00	1.24	0.00	42.99	0.149	–	S
5820	23 02 12.07	0.27	-54 18 32.38	0.30	5.270	0.373	3.075	0.231	9.29	0.73	3.88	0.40	146.73	13.16	0.148	–	S
5821	23 02 04.61	0.64	-54 30 21.09	0.56	2.228	0.253	1.219	0.167	8.03	1.52	6.56	1.22	109.73	58.98	0.141	–	S
5822	23 00 30.69	0.69	-56 37 08.16	0.83	3.415	0.275	1.335	0.166	15.18	2.33	4.78	0.86	148.83	16.43	0.147	–	S
5823	23 03 00.82	0.40	-52 58 50.79	0.48	116.407	6.721	31.998	1.878	31.82	1.35	6.63	0.30	56.94	2.59	0.655	-1.19	M

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5824	23 03 11.50	0.15	-52 38 02.73	0.24	241.856	13.375	128.235	7.079	24.11	0.45	4.03	0.10	82.84	1.02	0.603	-1.12	M
5825	23 04 40.37	0.66	-50 04 50.02	0.74	1.653	0.229	0.972	0.152	8.61	1.89	5.29	1.32	44.55	44.28	0.132	-	S
5826	23 01 56.62	0.63	-54 31 59.31	0.64	1.654	0.259	1.088	0.170	6.26	1.47	5.33	1.42	52.17	165.82	0.148	-	S
5827	23 04 19.14	0.48	-50 39 24.48	0.52	2.864	0.364	1.927	0.239	6.89	1.27	4.62	0.99	44.66	50.25	0.200	-	S
5828	23 00 01.72	0.57	-57 04 00.98	0.74	2.104	0.334	1.384	0.218	7.81	1.83	3.32	1.14	29.58	33.21	0.193	-	S
5829	23 01 44.54	0.18	-54 46 42.70	0.18	5.808	0.433	5.590	0.352	1.95	0.26	1.04	0.24	140.16	61.75	0.169	-	S
5830	23 02 58.00	0.19	-52 52 06.41	0.20	8.490	0.599	6.844	0.442	4.20	0.33	3.72	0.29	115.36	48.24	0.222	-	S
5831	23 03 30.87	1.28	-51 57 38.87	1.08	1.709	0.244	0.767	0.168	11.54	3.52	6.44	1.90	127.67	36.75	0.153	-	S
5832	23 03 39.31	1.16	-51 42 02.97	0.40	16.406	0.996	3.019	0.284	22.55	2.70	6.79	0.87	8.73	8.51	0.231	-	M
5833	23 03 27.53	0.20	-52 00 24.53	0.20	4.695	0.359	4.061	0.270	3.71	0.35	2.60	0.30	117.64	34.21	0.146	-	S
5834	23 02 05.00	0.77	-54 03 20.23	0.73	0.920	0.244	0.755	0.153	4.38	1.81	3.01	1.64	126.79	118.44	0.141	-	S
5835	23 03 36.11	0.15	-51 37 20.85	0.16	14.086	0.850	12.874	0.738	2.89	0.15	2.01	0.13	142.34	24.92	0.203	-0.47	S
5836	23 01 14.23	0.67	-55 13 48.58	0.88	2.571	0.292	1.275	0.193	11.86	2.32	4.31	1.10	37.37	22.82	0.170	-	S
5837	23 04 20.78	1.51	-50 14 46.85	1.84	9.987	0.564	0.858	0.127	31.35	4.52	23.09	3.30	33.06	37.67	0.161	-	S
5838	23 02 06.72	0.79	-53 55 39.45	1.02	2.402	0.261	1.001	0.175	11.02	2.42	8.11	1.77	15.03	51.61	0.154	-	S
5839	23 00 47.61	0.61	-55 46 22.53	0.61	2.275	0.361	1.535	0.236	6.19	1.56	4.79	1.25	141.01	69.34	0.206	-	S
5840	23 00 39.03	1.16	-55 55 23.69	1.24	2.964	0.333	1.059	0.229	11.53	3.16	9.79	2.45	151.45	73.81	0.208	-	S
5841	23 04 06.87	0.75	-50 31 42.75	0.96	3.140	0.323	1.338	0.213	12.65	2.50	6.77	1.42	37.94	29.40	0.187	-	S
5842	23 01 58.07	0.21	-54 00 57.42	0.21	5.686	0.412	4.375	0.294	5.07	0.38	3.73	0.33	61.38	33.05	0.160	-	S
5843	23 03 02.40	0.14	-52 18 54.81	0.15	27.491	1.568	24.616	1.377	3.00	0.09	2.56	0.08	80.63	30.95	0.242	-0.99	S
5844	23 03 20.51	0.35	-51 48 50.53	0.40	4.901	0.447	3.062	0.291	7.48	0.95	5.06	0.68	150.40	27.43	0.221	-	S
5845	23 03 32.47	1.03	-51 27 57.05	1.06	1.828	0.328	0.990	0.223	7.63	2.52	7.44	2.35	25.31	5.43	0.199	-	S
5846	23 01 20.36	0.65	-54 50 04.97	1.03	1.872	0.311	1.101	0.207	9.05	2.46	4.19	1.43	11.88	35.79	0.185	-	S
5847	23 03 30.62	0.14	-51 26 42.76	0.15	87.064	4.800	86.713	4.773	0.00	0.02	0.00	0.02	0.00	17.95	0.188	-0.04	S
5848	23 01 39.69	0.48	-54 21 46.96	0.47	1.580	0.225	1.168	0.146	5.97	1.24	3.28	0.89	136.39	37.83	0.124	-	S
5849	23 04 07.63	0.28	-50 21 04.34	0.38	3.643	0.317	2.400	0.208	7.75	0.84	4.08	0.55	6.14	21.38	0.151	-	S
5850	23 00 54.20	1.88	-55 21 39.06	0.92	3.191	0.291	0.906	0.191	17.92	4.51	8.25	2.05	91.88	28.50	0.184	-	S
5851	23 03 28.06	0.64	-51 27 26.99	0.64	2.147	0.339	1.459	0.221	7.34	1.79	3.46	1.10	136.92	33.57	0.194	-	S
5852	23 04 09.11	0.88	-50 10 44.91	0.83	12.542	0.715	1.920	0.195	25.12	2.59	14.61	1.25	133.90	15.34	0.187	-	S
5853	23 01 26.89	0.14	-54 32 56.88	0.16	14.710	0.879	13.236	0.741	0.00	0.09	0.00	0.08	0.00	7.84	0.140	-0.21	M
5854	23 01 59.81	0.14	-53 43 41.77	0.15	66.068	3.647	63.400	3.492	2.11	0.02	0.94	0.02	143.73	9.88	0.179	-0.26	S
5855	23 01 09.99	1.27	-54 53 37.12	1.09	2.052	0.273	0.840	0.190	10.49	3.04	8.75	2.47	111.80	86.30	0.170	-	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5856	23 01 38.89	0.24	-54 10 11.20	0.41	16.812	1.058	6.938	0.417	15.28	0.90	7.66	0.46	90.28	5.84	0.168	–	M
5857	23 03 08.91	0.19	-51 51 06.25	0.21	7.079	0.527	6.011	0.395	4.06	0.35	2.68	0.29	152.39	28.74	0.209	–	S
5858	23 03 55.92	0.49	-50 29 02.27	0.64	3.012	0.322	1.694	0.211	9.81	1.60	4.82	0.94	34.62	25.55	0.176	–	S
5859	23 02 09.55	0.57	-53 24 07.00	0.46	2.345	0.317	1.605	0.208	6.78	1.35	4.07	0.97	88.98	39.39	0.176	–	S
5860	23 03 05.04	0.91	-51 52 38.32	0.69	3.172	0.317	1.384	0.206	12.18	2.41	6.29	1.22	122.65	24.02	0.181	–	S
5861	23 00 01.38	0.24	-56 17 05.05	0.20	28.651	1.802	11.890	0.727	11.97	0.49	5.74	0.25	162.89	3.72	0.318	–	M
5862	23 00 07.18	0.20	-56 07 42.08	0.20	18.356	1.173	9.824	0.611	7.40	0.38	3.46	0.25	145.16	5.98	0.285	–	M
5863	23 01 42.19	0.16	-53 57 16.23	0.24	11.989	0.753	7.640	0.449	0.00	0.45	0.00	0.17	0.00	2.62	0.158	-0.27	M
5864	23 02 18.91	2.35	-52 58 32.59	2.53	46.316	2.580	2.024	0.354	31.62	7.67	12.32	2.67	137.92	18.60	0.336	–	M
5865	23 03 22.03	0.71	-51 16 15.34	0.76	5.400	0.387	1.712	0.216	14.49	2.02	9.83	1.35	50.09	29.62	0.186	–	S
5866	23 03 17.45	0.74	-51 22 46.67	0.65	1.920	0.339	1.310	0.221	6.72	1.89	4.21	1.33	119.71	49.25	0.196	–	S
5867	23 02 00.42	0.94	-53 25 31.22	0.82	3.256	0.316	1.275	0.207	11.91	2.47	8.22	1.57	128.05	34.64	0.182	–	S
5868	23 03 12.21	0.42	-51 28 15.86	0.52	1.839	0.359	1.695	0.224	0.00	1.25	0.00	0.84	0.00	37.13	0.200	–	S
5869	23 02 44.41	0.44	-52 11 41.51	0.36	9.232	0.596	3.602	0.306	12.32	1.09	8.03	0.66	119.27	16.50	0.219	–	S
5870	23 02 51.68	0.43	-51 57 05.29	0.45	2.442	0.286	1.697	0.187	7.10	1.18	3.25	0.74	140.20	25.11	0.153	–	S
5871	23 03 18.55	0.19	-51 11 25.10	0.18	19.763	1.183	9.938	0.597	7.73	0.31	3.81	0.21	18.70	5.95	0.241	–	M
5872	23 03 33.57	0.44	-50 44 16.79	0.46	1.970	0.290	1.552	0.188	4.55	1.01	3.95	1.00	139.85	111.13	0.160	–	S
5873	23 02 53.71	0.33	-51 51 45.54	0.33	4.604	0.417	3.127	0.276	6.20	0.77	4.93	0.61	131.19	37.50	0.202	–	S
5874	23 03 47.61	0.68	-50 18 14.76	0.62	4.820	0.355	1.687	0.203	11.97	1.68	10.54	1.33	90.29	47.72	0.170	–	S
5875	23 01 44.70	1.63	-53 34 37.43	0.74	24.553	1.513	7.205	0.523	27.76	4.00	8.73	1.26	23.30	10.45	0.341	–	M
5876	23 03 23.63	0.92	-51 00 19.09	0.99	1.598	0.327	0.996	0.217	7.22	2.44	5.45	1.97	141.98	79.22	0.195	–	S
5877	23 01 40.63	1.89	-53 42 46.43	1.10	4.198	0.321	0.944	0.192	19.56	4.66	11.01	2.37	106.10	30.00	0.191	–	S
5878	23 03 00.38	0.37	-51 37 55.06	0.48	4.202	0.401	2.533	0.260	8.18	1.12	5.00	0.75	163.17	26.00	0.205	–	S
5879	23 00 59.78	1.10	-54 40 33.12	1.06	2.671	0.289	1.001	0.196	11.88	2.97	8.82	2.03	136.97	46.91	0.176	–	S
5880	23 02 44.17	0.74	-52 02 43.95	0.48	2.757	0.288	1.469	0.187	10.83	1.89	4.01	0.87	114.71	19.60	0.160	–	S
5881	23 00 06.80	0.21	-55 50 43.02	0.23	6.584	0.499	5.027	0.351	4.99	0.42	3.85	0.37	26.93	38.52	0.205	–	S
5882	23 02 55.93	0.95	-51 43 09.49	1.08	1.717	0.308	0.962	0.208	8.78	2.82	5.57	1.85	147.26	50.70	0.186	–	S
5883	23 00 53.52	0.79	-54 44 29.16	0.67	2.092	0.296	1.183	0.197	7.92	1.91	6.10	1.48	109.06	63.09	0.172	–	S
5884	23 02 24.82	1.31	-52 27 21.40	1.50	5.229	0.481	1.479	0.318	15.92	3.97	10.33	2.55	42.55	44.43	0.300	–	S
5885	23 03 08.42	1.82	-51 12 33.93	1.24	24.871	1.425	2.828	0.290	36.56	4.99	9.68	1.34	37.76	9.86	0.245	–	M
5886	23 02 43.24	0.26	-51 54 33.18	0.26	3.528	0.342	3.005	0.238	4.13	0.56	2.43	0.45	117.72	35.52	0.165	–	S
5887	23 02 50.14	0.91	-51 41 52.48	0.96	2.621	0.330	1.275	0.221	11.67	2.84	4.90	1.31	140.84	25.65	0.198	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5888	23 00 46.12	0.82	-54 47 56.51	0.46	7.139	0.521	1.414	0.200	0.00	1.97	0.00	0.89	0.00	16.98	0.184	–	M
5889	23 02 49.91	0.52	-51 40 58.22	0.66	2.412	0.348	1.618	0.228	7.46	1.63	3.69	1.03	157.00	32.66	0.197	–	S
5890	23 00 59.14	1.43	-54 29 28.59	0.96	1.710	0.196	0.639	0.134	13.24	3.58	7.65	1.98	113.94	35.48	0.123	–	S
5891	23 01 00.71	1.41	-54 26 18.59	1.35	2.797	0.233	0.704	0.147	14.31	3.33	13.40	3.15	88.90	5.95	0.140	–	S
5892	23 00 06.36	1.29	-55 39 37.69	1.80	5.464	0.371	0.981	0.194	19.91	4.34	14.44	2.93	9.77	41.50	0.200	–	S
5893	23 01 12.06	0.25	-54 07 15.98	0.26	6.873	0.459	4.023	0.282	9.57	0.64	3.43	0.33	141.79	11.68	0.165	–	S
5894	23 03 40.90	0.42	-50 06 50.01	0.40	3.084	0.329	2.067	0.216	6.98	1.05	4.59	0.77	66.02	35.82	0.172	–	S
5895	23 01 18.10	0.28	-53 56 32.20	1.59	2.550	0.335	0.746	0.152	0.00	3.74	0.00	0.52	0.00	10.22	0.147	–	M
5896	23 02 01.44	0.14	-52 52 17.27	0.15	28.621	1.642	27.786	1.552	1.99	0.08	0.47	0.08	59.41	21.11	0.270	-0.24	S
5897	23 03 06.26	0.15	-51 03 55.73	0.16	28.148	1.621	21.365	1.197	5.39	0.11	3.25	0.09	135.40	4.02	0.227	-0.41	M
5898	23 00 05.78	0.61	-55 33 20.33	1.29	4.248	0.507	1.014	0.221	0.00	3.14	0.00	1.11	0.00	20.82	0.214	–	M
5899	23 01 30.58	0.43	-53 36 15.95	0.47	3.077	0.499	2.548	0.320	4.52	1.09	2.76	0.92	37.57	72.07	0.277	–	S
5900	23 01 47.65	0.30	-53 08 24.69	0.29	11.356	0.787	6.145	0.474	8.33	0.68	6.50	0.52	132.16	23.04	0.306	–	S
5901	23 00 30.17	0.72	-54 59 24.58	1.37	4.582	0.339	1.273	0.194	18.64	3.37	7.97	1.37	169.27	20.30	0.183	–	S
5902	23 03 17.29	0.59	-50 42 54.54	0.69	2.455	0.347	1.526	0.229	7.20	1.61	5.62	1.32	158.32	65.41	0.198	–	S
5903	23 02 06.33	0.36	-52 39 26.35	0.35	5.304	0.624	4.167	0.413	5.68	0.89	2.56	0.64	60.57	31.02	0.328	–	S
5904	23 01 56.39	0.16	-52 51 03.37	0.17	12.375	0.806	11.961	0.704	2.32	0.19	0.00	0.16	56.03	27.05	0.250	-0.62	S
5905	23 02 47.96	0.86	-51 28 43.01	0.79	1.559	0.344	1.100	0.223	6.11	2.03	4.43	1.78	79.41	94.63	0.201	–	S
5906	23 00 05.35	0.46	-55 25 41.56	0.41	22.124	1.262	4.939	0.389	16.38	1.05	13.50	0.87	80.46	26.80	0.282	–	S
5907	23 02 17.30	1.00	-52 15 07.86	0.65	6.517	0.452	1.825	0.241	16.29	2.45	10.13	1.40	89.96	23.65	0.216	–	S
5908	23 02 14.77	2.06	-52 13 43.37	1.86	8.567	0.508	1.007	0.180	30.40	6.08	15.89	2.70	134.05	23.85	0.215	–	S
5909	23 02 08.84	0.15	-52 22 53.92	0.16	22.675	1.322	18.653	1.061	4.22	0.14	3.33	0.12	60.15	23.38	0.259	-0.51	S
5910	23 01 57.13	2.33	-52 38 09.77	1.22	10.392	0.648	1.527	0.282	28.73	5.88	12.69	2.36	81.18	23.28	0.316	–	S
5911	23 01 57.85	0.14	-52 37 34.28	0.15	44.405	2.505	42.864	2.380	2.04	0.07	0.78	0.06	169.54	17.61	0.323	-0.41	S
5912	23 00 45.12	0.66	-54 20 49.86	0.93	2.561	0.267	1.130	0.176	11.30	2.29	6.77	1.36	164.74	30.12	0.154	–	S
5913	23 03 04.52	0.87	-50 43 16.78	0.87	2.058	0.276	1.029	0.187	8.37	2.13	8.11	1.91	92.05	5.52	0.164	–	S
5914	23 02 42.20	0.20	-51 18 29.72	0.21	6.631	0.499	5.606	0.372	4.50	0.38	2.03	0.29	131.91	19.81	0.201	–	S
5915	23 00 37.93	0.83	-54 26 42.40	0.79	1.427	0.266	0.908	0.176	6.56	1.98	5.55	1.77	125.19	108.69	0.157	–	S
5916	23 02 19.94	0.22	-51 52 04.03	0.27	10.097	0.647	5.476	0.378	8.92	0.55	6.10	0.39	178.97	17.23	0.212	–	S
5917	23 03 16.26	0.33	-50 15 25.69	0.39	3.176	0.335	2.305	0.222	6.13	0.89	3.89	0.66	158.30	33.23	0.172	–	S
5918	23 02 21.46	0.34	-51 45 27.11	0.36	2.787	0.341	2.285	0.226	4.83	0.85	2.47	0.64	141.07	36.13	0.180	–	S
5919	23 00 15.42	1.17	-54 49 24.88	0.60	1.380	0.314	0.979	0.200	0.00	2.84	0.00	1.23	0.00	28.78	0.187	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5920	23 02 19.39	1.23	-51 45 15.76	0.96	1.921	0.293	0.916	0.201	10.04	3.09	6.99	2.04	110.47	51.40	0.180	–	S
5921	23 02 31.10	0.28	-51 24 33.68	0.29	4.390	0.411	3.398	0.280	5.31	0.66	3.32	0.50	139.91	29.11	0.198	–	S
5922	23 01 18.13	0.75	-53 18 49.09	0.73	2.321	0.394	1.510	0.258	8.24	2.10	3.43	1.26	54.35	35.49	0.230	–	S
5923	23 01 02.96	0.27	-53 40 44.94	0.30	3.746	0.409	3.277	0.279	4.07	0.62	1.79	0.50	31.42	38.91	0.207	–	S
5924	23 02 00.15	0.28	-52 12 08.51	0.24	7.460	0.591	5.334	0.400	6.57	0.59	3.50	0.41	85.80	19.26	0.257	–	S
5925	23 02 59.50	0.14	-50 31 48.49	0.15	33.004	1.840	32.697	1.807	0.00	0.05	0.00	0.04	0.00	17.49	0.175	0.04	S
5926	23 03 17.89	0.31	-50 00 02.50	0.38	2.370	0.357	2.370	0.237	0.00	0.83	0.00	0.64	0.00	42.70	0.194	–	S
5927	23 01 59.03	0.80	-52 11 17.95	0.86	6.148	0.503	2.159	0.309	14.48	2.41	8.07	1.37	48.46	25.88	0.271	–	S
5928	23 01 56.49	0.83	-52 15 18.02	0.75	2.131	0.403	1.410	0.263	7.23	2.20	4.13	1.45	127.62	46.90	0.236	–	S
5929	23 02 24.62	0.50	-51 28 55.87	0.52	4.078	0.404	2.235	0.263	7.70	1.22	7.14	1.08	133.09	74.17	0.214	–	S
5930	23 02 55.34	0.31	-50 36 03.35	0.30	4.603	0.377	2.972	0.246	6.72	0.71	5.47	0.57	83.95	38.33	0.171	–	S
5931	23 02 38.36	0.56	-51 01 22.30	0.65	3.684	0.387	1.908	0.254	8.75	1.45	7.14	1.32	19.47	84.54	0.212	–	S
5932	23 03 05.45	0.68	-50 14 18.91	1.68	9.317	0.552	1.512	0.196	28.87	4.00	11.43	1.45	177.94	16.70	0.205	–	S
5933	23 01 14.31	0.44	-53 12 55.39	0.38	5.245	0.548	3.437	0.359	7.48	1.07	4.18	0.74	71.76	28.09	0.286	–	S
5934	23 01 07.90	1.30	-53 19 27.40	1.86	7.556	0.510	1.398	0.264	22.17	4.79	12.56	2.40	158.94	27.69	0.274	–	S
5935	23 00 19.45	0.41	-54 26 29.06	0.45	5.609	0.462	2.902	0.289	9.29	1.13	6.11	0.76	148.53	23.53	0.223	–	S
5936	23 02 37.75	1.64	-50 51 25.76	1.79	37.264	2.085	3.482	0.334	43.26	5.61	8.37	0.98	137.87	7.53	0.274	–	M
5937	23 00 48.35	0.34	-53 42 36.10	0.37	15.938	0.934	5.008	0.374	14.99	0.92	9.19	0.58	44.72	14.59	0.243	–	S
5938	23 00 19.99	0.99	-54 21 51.54	0.99	1.563	0.294	0.907	0.197	8.87	2.77	4.81	1.78	51.86	49.56	0.178	–	S
5939	23 00 14.22	1.56	-54 25 50.03	0.88	7.331	0.708	1.357	0.245	16.96	4.13	0.00	0.71	33.99	10.01	0.233	–	M
5940	23 00 27.38	0.14	-54 07 22.04	0.15	17.077	0.980	15.706	0.880	2.47	0.09	2.27	0.09	138.89	45.82	0.163	-0.28	S
5941	23 01 34.03	0.15	-52 28 53.85	0.16	24.910	1.436	23.327	1.308	2.59	0.10	1.60	0.09	39.49	23.46	0.250	-0.75	S
5942	23 00 33.92	0.29	-53 57 09.92	0.32	3.026	0.334	2.509	0.225	4.20	0.68	3.03	0.58	170.05	56.73	0.170	–	S
5943	23 02 08.19	0.70	-51 32 43.50	0.76	1.546	0.369	1.222	0.233	4.65	1.72	3.71	1.64	151.63	144.08	0.213	–	S
5944	23 00 29.64	0.14	-53 57 22.71	0.15	20.859	1.209	17.420	0.973	3.29	0.09	2.45	0.08	93.07	12.60	0.171	-0.92	M
5945	23 01 30.05	0.22	-52 28 17.25	0.25	8.784	0.640	6.055	0.430	6.06	0.48	4.86	0.40	4.70	36.89	0.255	–	S
5946	23 02 20.24	0.27	-51 07 44.07	0.31	4.115	0.420	3.338	0.285	4.58	0.65	3.31	0.55	177.26	54.81	0.209	–	S
5947	23 01 41.52	0.24	-52 09 01.29	0.19	22.728	1.382	9.752	0.599	12.13	0.50	3.55	0.21	163.46	3.13	0.266	–	M
5948	23 02 07.64	0.42	-51 24 28.15	0.95	8.145	0.535	2.435	0.266	18.57	2.23	7.54	0.90	1.41	15.44	0.230	–	S
5949	23 00 56.33	0.88	-53 14 39.34	1.21	5.235	0.475	1.750	0.308	13.85	3.00	9.10	1.82	163.29	34.17	0.279	–	S
5950	23 01 59.23	0.60	-51 34 44.46	0.66	21.971	1.329	3.428	0.342	14.08	1.53	12.60	1.35	82.04	48.04	0.285	–	M
5951	23 01 46.94	0.41	-51 54 52.97	0.47	3.198	0.317	1.922	0.207	7.30	1.08	5.97	0.88	161.91	50.69	0.164	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy $\text{bm}^{-1}$	$\sigma_{S_p}$ mJy $\text{bm}^{-1}$	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy $\text{bm}^{-1}$	$\alpha$	Type
5952	23 00 27.38	0.89	-53 54 08.71	1.03	1.617	0.297	0.925	0.200	7.85	2.39	6.11	2.07	20.79	102.17	0.178	–	S
5953	23 01 23.93	1.08	-52 29 45.16	0.87	3.288	0.415	1.470	0.283	10.47	2.66	7.65	1.90	86.50	53.88	0.251	–	S
5954	23 02 08.35	0.31	-51 18 21.08	0.37	4.301	0.433	3.121	0.288	6.22	0.82	3.83	0.62	19.37	34.38	0.218	–	S
5955	23 00 39.36	0.41	-53 31 10.67	1.50	8.621	0.662	2.045	0.267	0.00	3.53	0.00	0.81	0.00	10.45	0.242	–	M
5956	23 00 15.14	0.16	-54 04 31.94	0.17	7.936	0.529	7.534	0.450	2.10	0.20	1.56	0.18	155.07	63.44	0.173	-0.80	S
5957	23 00 03.72	0.53	-54 18 34.97	0.62	1.481	0.273	1.145	0.175	5.40	1.51	3.04	1.12	161.11	54.43	0.155	–	S
5958	23 02 24.04	0.18	-50 41 46.87	0.20	7.426	0.516	6.318	0.397	4.28	0.30	2.56	0.24	17.08	25.87	0.185	–	S
5959	23 00 57.83	0.54	-52 53 45.39	0.43	173.762	9.725	29.242	1.730	30.11	1.44	11.79	0.57	41.53	4.17	0.638	-0.95	M
5960	23 00 47.10	0.39	-53 10 57.32	0.34	18.129	1.152	7.162	0.583	12.12	0.94	8.06	0.64	70.23	18.69	0.402	–	S
5961	23 00 45.84	0.44	-53 10 13.43	0.64	9.671	0.840	4.713	0.528	11.23	1.58	5.26	0.81	161.01	19.20	0.432	–	S
5962	23 02 45.48	0.21	-50 00 01.49	0.25	4.676	0.456	4.676	0.341	0.00	0.48	0.00	0.36	0.00	26.98	0.220	–	S
5963	23 01 43.53	1.67	-51 35 42.40	1.51	8.027	0.504	1.323	0.222	25.67	5.01	12.52	2.05	134.55	22.00	0.239	–	S
5964	23 00 30.45	0.78	-53 25 25.61	0.89	2.411	0.360	1.342	0.241	9.59	2.38	4.87	1.44	43.40	37.17	0.213	–	S
5965	23 00 15.21	0.40	-53 44 32.80	0.47	1.959	0.350	1.767	0.221	3.92	1.08	0.35	0.84	27.61	53.52	0.194	–	S
5966	23 00 36.34	0.73	-53 11 40.81	0.73	9.171	0.984	3.269	0.402	11.50	2.30	0.00	0.62	50.74	9.88	0.360	–	M
5967	23 01 51.49	0.15	-51 13 59.64	0.15	69.489	3.848	42.883	2.371	10.94	0.10	4.22	0.05	177.89	0.85	0.246	-0.69	M
5968	23 01 01.04	0.31	-52 29 45.12	0.33	4.407	0.524	3.730	0.350	4.04	0.70	2.87	0.64	52.66	79.76	0.273	–	S
5969	23 01 48.47	0.28	-51 09 51.99	0.30	3.798	0.445	3.439	0.301	3.06	0.60	2.23	0.58	24.43	37.88	0.229	–	S
5970	23 00 20.81	0.39	-53 19 20.53	1.20	11.844	0.831	3.109	0.294	17.92	2.80	4.44	0.86	99.05	9.73	0.239	–	M
5971	23 01 22.02	0.18	-51 45 06.88	0.19	21.805	1.270	11.331	0.657	12.67	0.34	4.42	0.15	141.81	2.05	0.207	0.18	M
5972	23 00 48.93	0.85	-52 36 45.13	0.72	2.490	0.423	1.536	0.280	7.45	2.06	5.32	1.57	88.04	64.92	0.248	–	S
5973	23 01 40.14	1.25	-51 16 37.18	1.67	5.263	0.391	1.159	0.228	19.35	4.21	12.08	2.57	32.02	37.23	0.224	–	S
5974	23 01 38.08	0.62	-51 14 55.75	0.87	0.961	0.461	1.182	0.247	0.00	2.32	0.00	0.96	0.00	30.27	0.260	–	S
5975	23 00 54.09	0.57	-52 22 49.86	0.90	5.655	0.536	2.453	0.345	12.54	2.17	6.32	1.18	23.20	25.04	0.298	–	S
5976	23 00 02.80	0.42	-53 37 02.62	0.62	2.221	0.339	1.650	0.219	6.90	1.45	1.95	0.89	17.11	29.44	0.190	–	S
5977	23 00 49.23	0.44	-52 29 21.65	0.58	4.286	0.528	2.805	0.346	8.01	1.40	3.71	0.88	29.25	28.59	0.291	–	S
5978	23 00 38.33	0.52	-52 33 01.21	0.21	48.147	2.820	21.291	1.221	23.24	1.21	3.59	0.27	17.19	2.90	0.347	-0.91	M
5979	23 01 33.54	0.14	-51 06 49.64	0.16	71.391	3.964	41.094	2.271	11.32	0.14	2.20	0.06	107.02	0.85	0.222	-0.76	M
5980	23 01 58.99	0.14	-50 22 03.56	0.15	169.873	9.464	135.518	7.511	6.01	0.08	0.00	0.05	128.79	7.12	0.897	-0.75	S
5981	23 01 43.40	1.75	-50 46 56.07	1.15	7.877	0.567	1.158	0.221	15.50	4.60	4.06	1.72	34.87	21.98	0.211	–	M
5982	23 01 05.22	0.53	-51 48 07.65	0.62	2.680	0.367	1.737	0.241	7.13	1.46	4.93	1.15	30.11	58.67	0.206	–	S
5983	23 01 05.13	0.32	-51 47 21.26	0.38	9.220	0.594	3.901	0.313	10.81	0.87	8.27	0.62	158.86	21.54	0.211	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
5984	23 01 50.40	0.58	-50 33 43.83	0.59	1.702	0.351	1.408	0.221	4.03	1.41	3.49	1.27	84.51	5.78	0.199	–	S
5985	23 00 45.40	0.17	-52 14 11.48	0.19	12.525	0.849	10.558	0.655	4.55	0.28	2.33	0.23	21.54	19.86	0.292	–	S
5986	23 02 08.23	0.46	-50 01 22.04	0.75	3.090	0.542	2.314	0.347	7.13	1.74	1.81	1.02	6.96	32.54	0.309	–	S
5987	23 01 58.67	0.69	-50 17 18.61	0.76	1.666	0.352	1.241	0.226	5.76	1.87	3.71	1.47	144.70	68.31	0.204	–	S
5988	23 00 34.54	0.31	-52 29 16.45	0.34	5.373	0.571	4.166	0.382	5.07	0.73	3.68	0.63	37.38	59.95	0.290	–	S
5989	23 00 26.64	0.14	-52 36 46.75	0.15	50.995	2.859	44.521	2.471	4.21	0.07	1.42	0.06	96.27	9.07	0.324	-0.80	S
5990	23 01 11.44	0.55	-51 27 06.98	0.66	2.896	0.368	1.762	0.242	8.27	1.68	4.66	1.05	151.68	31.55	0.207	–	S
5991	23 01 27.67	0.16	-50 53 11.91	0.17	10.575	0.687	10.050	0.593	2.10	0.18	1.65	0.18	4.50	3.22	0.212	0.09	S
5992	23 01 26.80	0.16	-50 47 25.14	0.19	23.576	1.394	12.115	0.701	10.11	0.29	3.31	0.14	121.97	2.38	0.219	-1.42	M
5993	23 01 51.75	0.23	-50 00 32.54	0.20	167.959	9.291	91.835	5.065	28.51	0.51	2.85	0.08	150.02	0.88	0.375	-1.17	M
5994	23 00 40.99	0.60	-51 55 32.11	0.83	3.364	0.427	1.824	0.284	9.15	1.98	5.82	1.31	171.15	39.01	0.246	–	S
5995	23 01 17.10	0.73	-50 57 01.03	0.87	2.792	0.402	1.537	0.270	8.62	2.03	6.31	1.68	28.85	74.57	0.236	–	S
5996	23 00 18.27	1.08	-52 22 07.47	1.14	3.834	0.502	1.621	0.347	9.53	2.70	9.49	2.49	146.39	6.09	0.310	–	S
5997	23 01 32.68	0.16	-50 13 18.86	0.17	10.928	0.696	10.114	0.594	3.03	0.19	1.45	0.16	171.48	24.14	0.204	-0.61	S
5998	23 00 50.23	0.65	-51 21 21.30	0.68	3.991	0.412	1.946	0.270	9.39	1.77	7.34	1.27	139.33	42.27	0.229	–	S
5999	23 00 50.64	0.17	-51 16 02.04	0.19	39.942	2.283	17.764	1.021	11.07	0.28	8.42	0.22	67.94	6.29	0.296	-1.10	M
6000	23 01 19.85	1.73	-50 19 39.39	1.30	5.506	0.397	1.192	0.224	22.10	4.82	10.57	2.11	67.42	25.74	0.226	–	S
6001	23 01 03.99	0.20	-50 43 59.03	0.22	5.250	0.422	4.624	0.315	3.37	0.37	2.62	0.33	147.84	53.15	0.180	–	S
6002	23 00 39.93	0.18	-51 18 36.07	0.18	20.460	1.249	10.774	0.654	5.91	0.28	2.94	0.21	163.35	7.61	0.276	–	M
6003	23 00 31.09	0.35	-51 27 33.41	0.41	3.841	0.427	2.812	0.282	6.42	0.98	3.09	0.65	150.45	26.33	0.223	–	S
6004	23 00 49.03	1.04	-50 52 26.65	1.01	15.618	0.956	2.275	0.259	21.33	3.23	6.28	0.96	142.16	9.64	0.227	–	M
6005	23 01 03.19	1.03	-50 28 04.84	0.79	3.116	0.439	0.925	0.196	0.00	2.94	0.00	0.75	0.00	14.71	0.189	–	M
6006	23 00 00.04	0.58	-52 04 46.72	0.72	3.181	0.949	3.181	0.582	0.00	1.64	0.00	1.36	0.00	83.96	0.543	–	S
6007	23 00 00.02	0.14	-52 04 32.27	0.15	79.542	4.468	79.542	4.408	0.00	0.06	0.00	0.05	0.00	9.19	0.530	-0.27	S
6008	23 00 39.63	0.30	-51 04 04.26	0.39	3.597	0.433	2.958	0.286	5.50	0.88	1.19	0.59	168.39	26.24	0.227	–	S
6009	23 00 07.94	0.20	-51 49 39.90	0.21	11.350	0.743	7.643	0.496	5.96	0.35	5.43	0.33	19.49	38.69	0.245	–	S
6010	23 00 18.01	0.21	-51 29 55.83	0.22	7.012	0.541	5.816	0.395	4.35	0.40	2.88	0.32	134.95	27.82	0.223	–	S
6011	23 00 45.55	0.62	-50 43 25.43	0.78	3.744	0.344	1.590	0.220	10.75	1.81	8.48	1.43	2.40	55.01	0.187	–	S
6012	23 00 53.99	0.44	-50 28 05.82	0.44	2.926	0.329	1.948	0.217	6.05	0.98	5.62	0.97	94.65	104.25	0.175	–	S
6013	23 00 42.57	1.87	-50 44 47.10	1.01	4.161	0.311	0.986	0.181	21.35	4.91	9.18	1.78	113.27	22.77	0.182	–	S
6014	23 00 47.28	0.47	-50 36 06.26	0.52	2.517	0.328	1.722	0.215	5.87	1.17	5.35	1.07	173.01	5.99	0.181	–	S
6015	23 00 27.96	0.22	-50 52 43.43	0.23	6.406	0.475	4.705	0.329	5.07	0.41	4.82	0.41	88.12	3.24	0.191	–	S

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Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
6016	23 00 22.15	0.94	-50 58 10.68	0.72	2.226	0.454	0.874	0.195	0.00	2.72	0.00	0.45	0.00	10.76	0.189	-	M
6017	23 00 20.54	0.36	-50 58 08.39	0.32	3.177	0.367	2.562	0.244	5.10	0.83	2.62	0.61	95.57	33.54	0.191	-	S
6018	23 00 35.36	1.62	-50 12 45.55	1.04	3.097	0.327	1.066	0.221	15.50	4.34	7.44	1.83	116.74	28.25	0.208	-	S
6019	23 00 36.45	1.02	-50 07 18.56	0.34	9.539	0.700	2.647	0.259	16.95	2.37	2.77	0.72	7.80	8.86	0.214	-	M
6020	23 00 00.01	0.14	-51 03 25.75	0.15	33.294	1.885	33.294	1.850	0.00	0.08	0.00	0.06	0.00	9.73	0.261	-0.15	S
6021	23 00 30.44	1.97	-50 12 12.45	1.16	3.947	0.339	1.047	0.217	19.64	5.29	8.56	1.94	116.07	25.55	0.215	-	S
6022	23 00 05.95	0.87	-50 43 01.38	0.85	2.706	0.364	1.364	0.246	9.14	2.16	7.24	1.84	67.83	79.96	0.215	-	S
6023	23 27 13.73	1.81	-51 23 34.52	0.61	41.850	2.333	3.188	0.344	42.97	4.25	14.27	1.39	2.57	8.15	0.296	-	M
6024	23 23 33.01	2.27	-59 14 02.41	0.66	15.333	0.864	1.591	0.191	43.88	5.17	10.74	1.29	101.30	9.69	0.237	-	S
6025	23 19 12.62	7.78	-54 23 26.49	3.98	35.445	1.994	2.657	0.332	90.12	20.24	17.47	3.65	156.57	16.22	0.298	-	M
6026	23 18 14.85	12.61	-56 44 07.61	2.76	5.774	0.594	1.970	0.259	50.74	30.03	8.42	4.64	11.16	34.04	0.235	-	M
6027	23 17 56.15	0.79	-54 22 12.05	0.85	2.845	0.273	1.187	0.177	12.86	2.41	6.22	1.23	140.74	20.13	0.156	-	S
6028	23 53 17.77	0.67	-50 28 29.37	0.67	3.306	0.354	1.640	0.233	8.84	1.58	7.81	1.50	110.15	87.49	0.198	-	S
6029	23 11 24.08	0.65	-57 45 03.25	1.79	7.526	0.449	1.244	0.165	29.72	4.28	9.27	1.27	13.74	13.75	0.178	-	S
6030	23 09 54.82	2.34	-59 42 31.65	1.18	45.495	2.519	2.432	0.309	46.18	5.28	23.02	2.82	89.12	16.96	0.467	-	S
6031	23 07 49.75	1.96	-58 40 24.10	0.92	9.533	0.550	1.118	0.161	31.47	4.52	14.18	2.05	104.94	18.15	0.187	-	S
6032	23 11 41.13	0.56	-50 05 54.93	0.51	0.561	0.252	0.759	0.136	0.00	1.31	0.00	1.13	0.00	84.33	0.142	-	S
6033	23 55 27.72	0.81	-54 38 36.48	2.10	11.898	0.855	1.613	0.248	22.40	5.27	0.00	0.31	105.34	5.50	0.232	-	M
6034	23 07 32.50	1.89	-57 29 01.75	0.92	35.323	1.946	1.419	0.135	55.16	4.35	26.68	2.16	98.24	12.92	0.209	-	S
6035	23 06 44.13	1.71	-56 57 02.40	0.58	3.710	0.342	0.736	0.163	0.00	4.02	0.00	1.31	0.00	19.01	0.158	-	M
6036	23 00 38.02	2.61	-55 14 47.09	0.83	14.350	0.911	1.549	0.229	32.25	6.35	4.23	1.00	170.76	9.69	0.212	-	M
6037	23 52 09.18	0.65	-56 02 11.36	1.34	7.057	0.424	1.361	0.163	25.37	3.26	9.34	1.14	13.14	4.90	0.162	-	S
6038	23 49 40.59	0.52	-51 24 27.36	0.84	2.385	0.321	1.430	0.211	9.69	1.99	3.32	1.05	15.41	14.87	0.185	-	S
6039	23 52 27.08	0.65	-57 49 04.66	0.98	1.420	0.252	0.874	0.167	8.28	2.30	3.82	1.46	4.92	26.12	0.150	-	S
6040	23 48 40.87	0.91	-53 26 15.71	0.49	6.808	0.652	3.106	0.418	12.72	2.18	4.86	0.99	73.54	9.95	0.365	-	S
6041	23 48 44.97	0.77	-59 42 00.27	1.06	1.574	0.275	0.883	0.185	8.41	2.51	5.20	1.76	2.54	37.49	0.166	-	S
6042	23 45 32.53	0.77	-52 36 14.25	1.01	1.952	0.269	0.993	0.181	10.09	2.46	5.85	1.61	24.46	28.48	0.161	-	S
6043	23 45 59.99	1.09	-54 29 37.17	1.08	2.013	0.266	0.888	0.183	11.33	3.00	6.73	1.90	43.05	29.37	0.164	-	S
6044	23 44 42.11	0.73	-51 54 09.73	1.57	4.552	0.342	1.248	0.198	20.25	3.78	7.63	1.43	12.79	11.25	0.191	-	S
6045	23 47 01.74	1.12	-59 25 57.18	1.23	10.646	0.657	1.975	0.276	24.08	3.49	10.40	1.55	137.22	9.28	0.280	-	S
6046	23 44 39.46	0.69	-54 39 29.28	1.08	16.008	0.904	2.177	0.218	28.48	2.70	13.79	1.23	22.08	5.72	0.218	-	S
6047	23 42 56.86	0.58	-52 52 52.94	0.42	2.582	0.293	1.618	0.191	8.53	1.40	3.56	0.82	68.62	14.26	0.159	-	S

Continued on next page

Table 3.1: (continued) The ATLAS-SPT source catalogue containing 6,067 sources. Column descriptions are given in Section 3.2.

SID	RA	$\sigma_{\text{RA}}$ "	DEC	$\sigma_{\text{DEC}}$ "	$S$ mJy	$\sigma_S$ mJy	$S_p$ mJy bm <sup>-1</sup>	$\sigma_{S_p}$ mJy bm <sup>-1</sup>	$\Theta_{\text{Maj}}$ "	$\sigma_{\Theta_{\text{Maj}}}$ "	$\Theta_{\text{Min}}$ "	$\sigma_{\Theta_{\text{Min}}}$ "	$\Theta_{\text{PA}}$ °	$\sigma_{\Theta_{\text{PA}}}$ °	$\sigma_{\text{rms}}$ mJy bm <sup>-1</sup>	$\alpha$	Type
6048	23 44 20.31	0.36	-57 31 19.33	0.55	2.315	0.299	1.633	0.195	7.21	1.25	2.28	0.79	172.19	15.39	0.164	–	S
6049	23 57 51.58	0.70	-53 20 12.57	1.30	8.300	0.890	3.309	0.595	13.69	2.99	6.50	1.61	166.85	16.26	0.538	–	S
6050	23 39 40.50	0.43	-50 11 45.99	0.94	4.782	0.338	1.604	0.186	16.94	2.18	7.15	0.97	175.12	9.43	0.160	–	S
6051	23 36 32.40	1.03	-50 03 28.81	1.48	1.965	0.239	0.753	0.165	13.06	3.44	8.17	2.35	160.01	39.79	0.150	–	S
6052	23 37 13.78	0.76	-56 31 18.67	1.27	15.447	0.865	1.772	0.177	34.49	3.22	13.30	1.19	153.68	6.16	0.191	–	S
6053	23 35 16.97	0.78	-54 53 02.97	0.61	2.218	0.360	1.420	0.237	7.25	1.80	4.67	1.38	96.38	44.83	0.209	–	S
6054	23 34 45.30	1.98	-51 15 31.14	0.71	13.721	0.842	2.472	0.346	30.21	4.96	8.51	1.25	100.72	9.22	0.375	–	S
6055	23 34 29.90	0.64	-56 28 23.56	2.18	16.510	0.922	1.827	0.175	53.74	5.29	6.77	0.66	164.91	4.38	0.218	–	S
6056	23 32 37.64	1.95	-57 18 46.02	0.44	11.556	0.772	1.608	0.206	35.17	4.66	0.00	0.43	168.49	5.03	0.186	–	M
6057	23 30 02.29	0.45	-57 02 17.26	0.83	2.829	0.300	1.428	0.196	10.92	1.93	4.58	1.01	2.03	16.13	0.169	–	S
6058	23 18 36.72	1.98	-56 51 53.23	1.39	37.476	2.098	1.513	0.314	23.03	4.94	13.91	2.80	158.61	24.11	0.303	–	M
6059	23 18 34.16	2.83	-56 48 18.58	2.26	162.052	8.913	1.135	0.094	107.34	6.67	82.75	5.24	109.62	15.17	0.303	–	S
6060	23 28 29.75	2.22	-59 40 14.96	1.58	88.993	4.898	2.109	0.212	63.80	5.25	39.15	3.47	66.07	11.83	0.424	–	S
6061	23 28 59.48	4.90	-58 50 45.55	4.18	15.664	0.865	0.359	0.075	61.28	12.29	42.63	8.75	125.35	32.76	0.174	–	S
6062	23 31 06.32	1.21	-57 51 25.01	3.74	132.386	7.298	2.093	0.290	85.78	8.81	26.70	2.75	85.42	8.73	0.266	–	M
6063	23 31 17.96	0.81	-53 53 03.18	1.16	2.030	0.347	1.123	0.233	9.82	2.84	4.56	1.66	156.52	31.06	0.211	–	S
6064	23 42 39.67	2.19	-53 14 46.87	1.18	33.383	1.842	1.442	0.159	52.20	5.26	27.52	2.64	94.88	8.00	0.253	–	S
6065	23 48 31.50	7.35	-53 51 59.41	3.68	3.242	0.687	1.416	0.296	25.16	18.84	5.40	4.41	20.18	42.86	0.286	–	M
6066	23 39 59.83	2.90	-51 19 36.09	1.48	5.944	0.519	1.730	0.206	26.81	7.41	6.63	1.91	21.82	17.55	0.182	–	M

### 3.2.1 Source Catalogue Analysis

The flux density distribution of the ATLAS-SPT sources is shown in Figure 3.1. This distribution is positively skewed, typical for sources extracted from an image using an SNR flux density detection threshold.

#### 3.2.1.1 Completeness

A natural consequence of detecting and extracting sources down to a flux density threshold is incompleteness. Faint sources near the threshold are more affected by the underlying noise as it contributes a larger fraction to the total recovered flux density. This leads to the non-detection of a number of faint sources that happen to lie in noise troughs, causing their peak flux densities to fall below the detection threshold. (Similarly, faint sources that lie on a noise peak will still be detected, but their fluxes will be biased high. This is further discussed in Section 3.2.1.2.)

To estimate the survey completeness as a function of flux density, a similar strategy to the clean bias simulation (see Section 2.5.1) was conducted. Instead of injecting the simulated sources into the visibility data, sources were inserted directly into the final mosaic to circumvent the need to repeat the imaging and deconvolution process. Repeating the entire imaging process is not required, as the completeness simulation is merely a test of the ability of the source finder to detect sources.

Using the MIRIAD task `imgen`, 10 000 point-sources were inserted into the final mosaic at random positions constrained to be at least  $1'$  away from any real sources. The flux densities of the simulated sources were drawn randomly from a uniform distribution between  $0.1$  to  $3.0 \text{ mJy beam}^{-1}$ . Each source was added one at a time. `PyBDSF` was run on a  $1000 \times 1000$  pixel cutout centred on each simulated source position using the same parameters that were used on the final mosaic and instructed to attempt to detect an island at the given simulated source position. Supplying the source position is not expected to change the probability of `PyBDSF` detecting the source, but rather limit the island detection to the supplied position and thus prevent islands being placed on other pixels above the detection threshold. If an island was detected, a Gaussian component was fit and extracted from the image.

```
Task:  imgen
in     =  completeness_1_in.mir
out    =  completeness_1_out.mir
object =  gaussian
spar   =  <flux>,<d_ra>,<d_dec>,8,8,0
```

Each simulated source was then binned into 20 flux density bins. The total number of



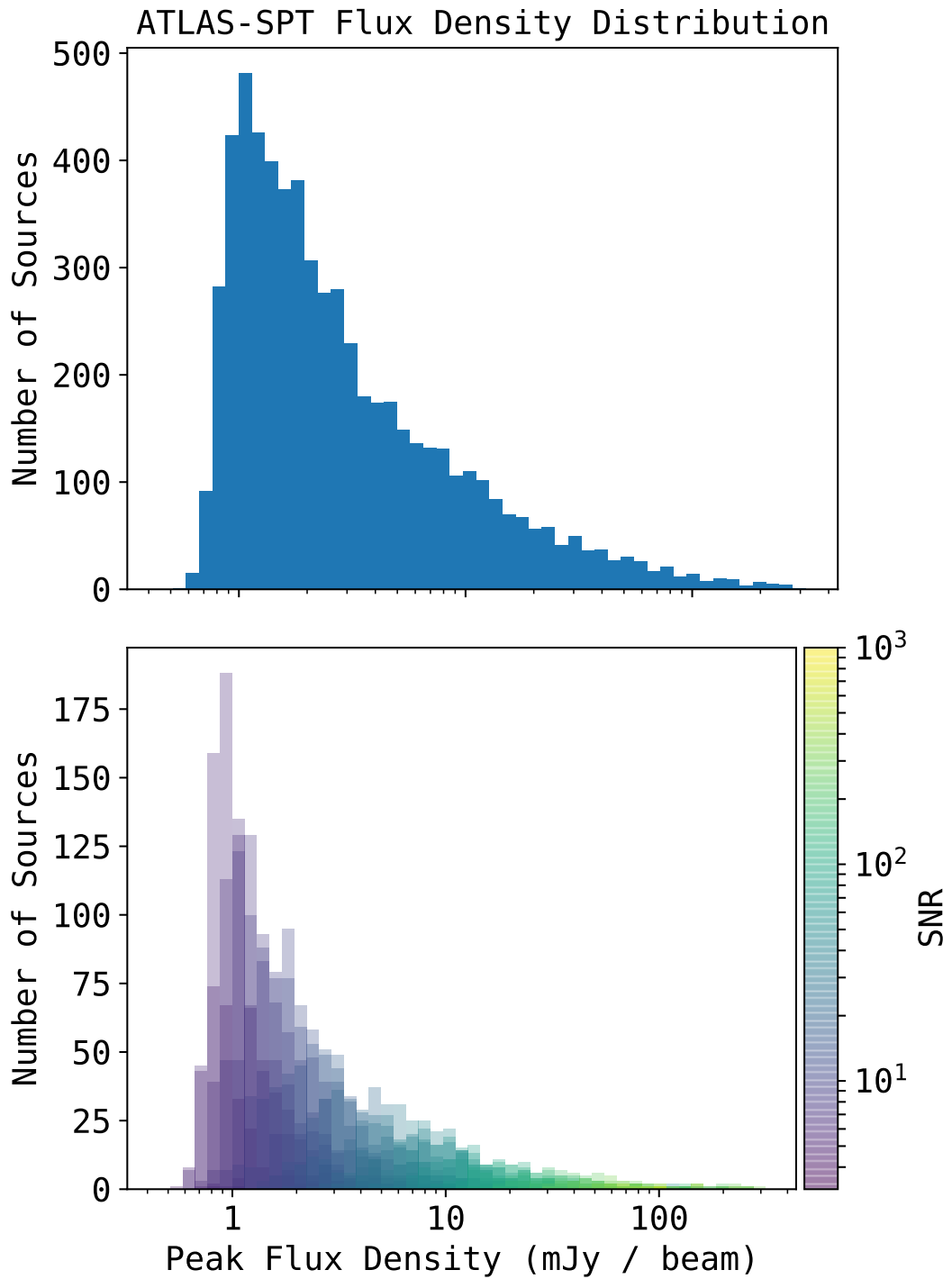


Figure 3.1: The flux density distribution of the ATLAS-SPT source catalogue. The upper panel shows the overall peak flux density distribution across 50 logarithmically spaced bins. The lower panel shows the same sources binned by their SNR computed using the peak flux density and the local rms. This is to show that although the ATLAS-SPT mosaic contains spatial variations in the rms, this variation does not appear to have a significant impact on the flux density distribution.

inserted and recovered sources in each bin were counted to determine the fraction of sources that were detected as a function of flux density. Dividing the number of recovered sources by the number of inserted sources yields the completeness for each flux density bin as shown in Figure 3.2. These results indicate that the catalogue achieves  $\sim 100\%$  completeness within the  $1.335 \text{ mJy beam}^{-1}$  bin and is  $\sim 97\%$  complete at the catalogue  $5\sigma$  detection threshold of  $0.9 \text{ mJy beam}^{-1}$ . The results of this completeness simulation are used to correct the source counts presented in Section 3.4.

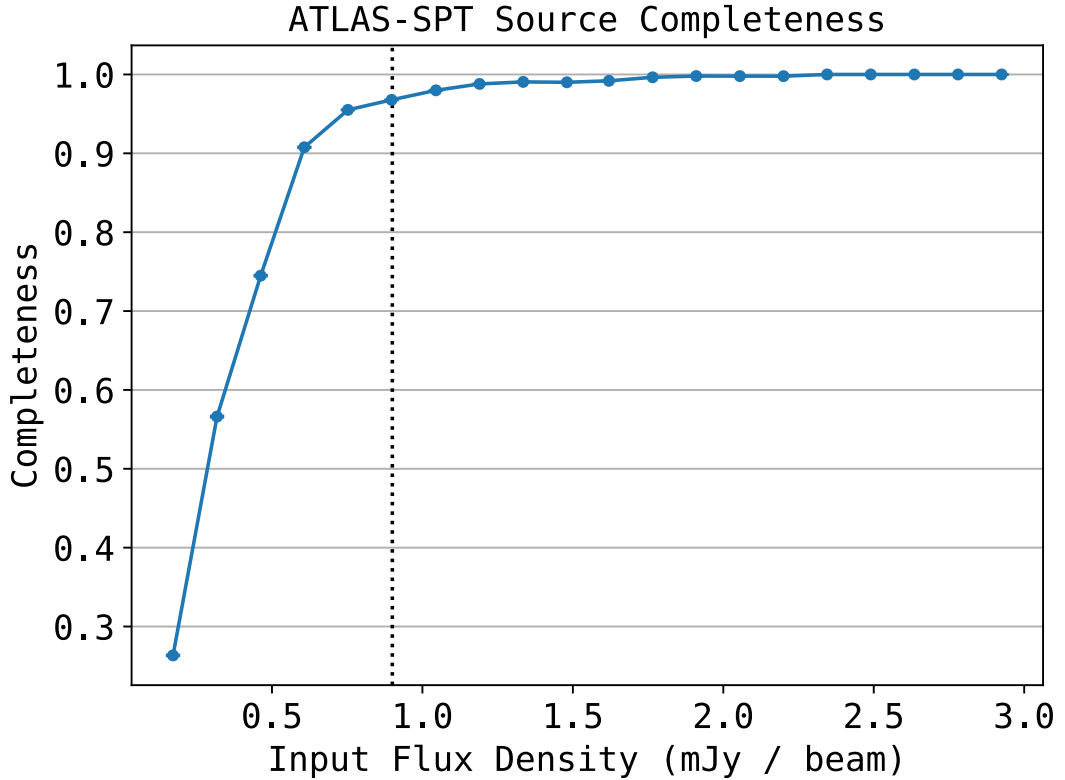


Figure 3.2: The estimated completeness of the ATLAS-SPT source catalogue for a range of flux densities. A total of 10 000 sources were inserted into the ATLAS-SPT mosaic and extracted using the same source detection parameters used to generate the source catalogue. The completeness (ordinate) values are calculated by dividing the number of recovered sources ( $N_r$ ) by the number of inserted ( $N_i$ ) sources for each flux density bin. The errors are estimated by jack-knife resampling each flux density bin and computing the standard deviation of completeness values. These errors are very small with a maximum of 0.001 and are not visible on the plot. The  $5\sigma$  detection threshold for the median rms ( $0.9 \text{ mJy beam}^{-1}$ ) is shown as a vertical dotted line.

### 3.2.1.2 Accuracy of Calibration

I use the same simulated sources from the completeness simulation (Section 3.2.1.1) to determine the accuracy of the extracted source flux densities and positions.

Flux density accuracies were estimated by calculating the ratio between the simulated sources input flux densities and the recovered output flux densities. Faint sources are ex-

pected to have an increased recovered flux density due to noise fluctuations: a noise peak at the same location as a source with an intrinsic flux density below the source detection threshold may increase the flux of that source above the detection threshold. This is referred to as flux density boosting and can clearly be seen in Figure 3.3. Sources with the faintest flux density recovered in the catalogue ( $\sim 0.36 \text{ mJy beam}^{-1}$ ) are boosted by  $\sim 30\%$  and the boosting falls below the 5% level at  $\sim 0.74 \text{ mJy beam}^{-1}$ . The few outliers with high recovered flux density ratios are caused by artefacts from nearby bright sources contributing to the extracted source peak flux density.

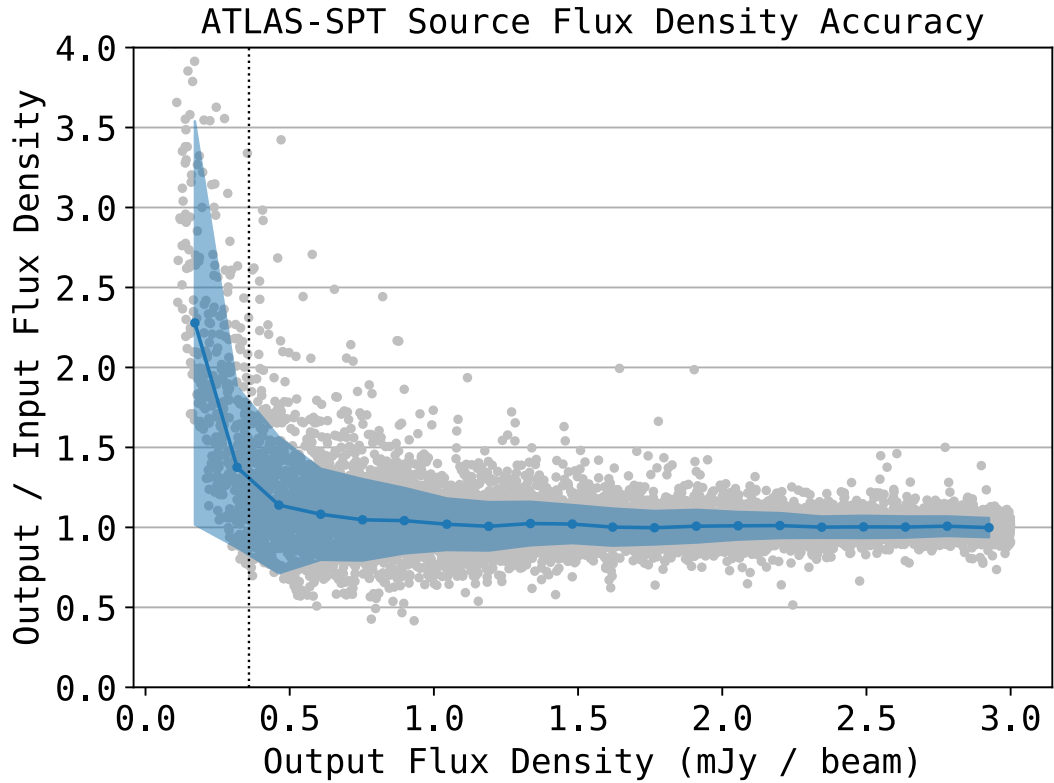


Figure 3.3: The estimated flux density accuracy of the ATLAS-SPT source catalogue by means of the ratio between the output and input flux densities from the completeness simulation. The median ratio for each flux density bin is traced as the blue solid line with the  $\pm 1\sigma$  errors shown as a filled region around the median. Each source from the simulation is plotted in the background as grey points. The faintest flux density recovered in the source catalogue is marked with the vertical dashed line at  $\sim 0.36 \text{ mJy beam}^{-1}$ . Note that the few outliers with high flux density ratios are caused by nearby source artefacts.

Positional accuracies were similarly estimated using the completeness simulation sources. The RA and Declination offset between the inserted and recovered positions were calculated for each simulated source. The distribution of positional offsets binned by input flux density is shown in Figure 3.4. As expected, sources with higher input flux densities present a smaller scatter than those of lower flux density. This can be seen in Figure 3.4 and is quantified in Figure 3.5. The median offset in both directions is  $\ll 1''$  with the uncertainty at the faint end of

the catalogue  $\sim 1.6''$ . Sources with input flux densities of  $\geq 1.3 \text{ mJy beam}^{-1}$  have an uncertainty of  $\leq 0.5''$ .

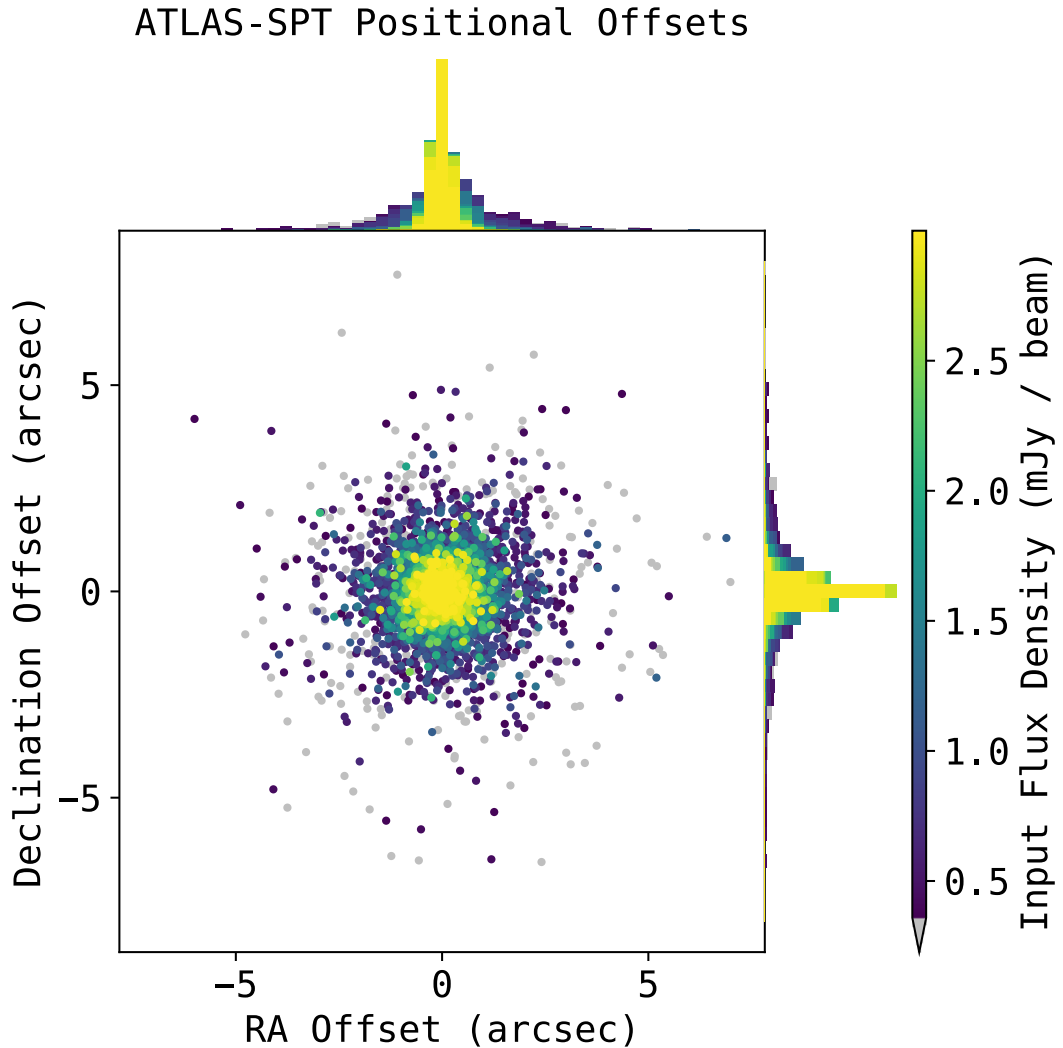


Figure 3.4: The estimated positional accuracy of the ATLAS-SPT source catalogue. The offsets between the simulated source positions and their extracted positions are shown in the centre panel coloured by their respective input flux density bin. Sources with input flux densities below the minimum peak flux detected in the catalogue are shown in grey. The distributions of the RA and Declination offsets are shown on the top and right, respectively.

### 3.2.1.3 Comparisons to other studies

One can also verify the accuracy of a source catalogue by comparing it to others from surveys of similar parameters. Prior to the ATLAS-SPT survey, no contiguous centimetre-wavelength radio observations existed for the SSDF. Another survey, the ATCA-XXL survey (Butler et al., 2017), was conducted shortly afterward and covers the  $25 \text{ deg}^2$  ultimate XMM extragalactic survey south field (XXL-S). The XXL-S is approximately centred on the SSDF and is entirely covered by the ATLAS-SPT footprint. Since the ATCA-XXL survey is smaller in area but

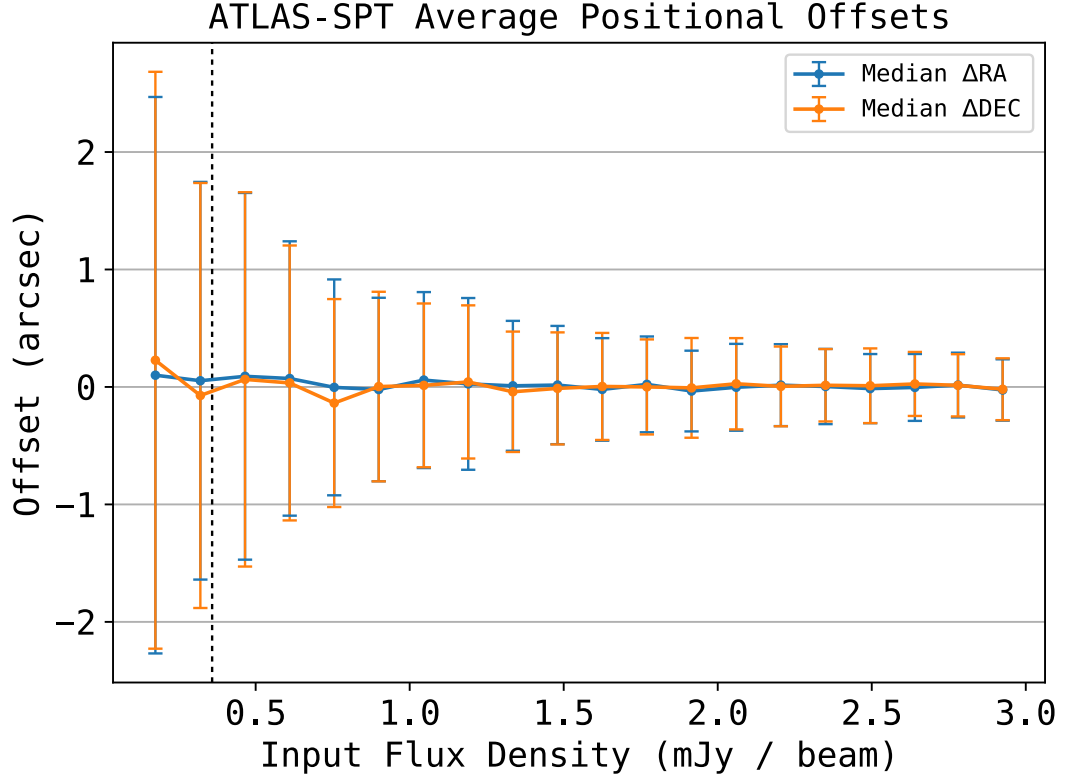


Figure 3.5: The estimated positional uncertainties of the ATLAS-SPT source catalogue. The median offsets in RA and Declination for each input flux density bin are shown in blue and orange, respectively. The error bars are the standard deviation of each flux density bin. A vertical black dotted line marks the lowest peak flux density recovered in the ATLAS-SPT catalogue.

deeper in sensitivity (median rms of  $\sim 41 \mu\text{Jy beam}^{-1}$ ), it complements the larger yet more shallow ATLAS-SPT survey. Both surveys were observed at the same frequency with similar array configurations, making the ATCA-XXL source catalogue an ideal dataset to verify the accuracy of the ATLAS-SPT catalogue.

To compare the flux densities between the ATCA-XXL and ATLAS-SPT surveys, the sources must first be crossmatched. The simplest method is to perform a simple sky position cross-match between sources with a maximum separation limit. This limit should be determined by considering the positional accuracies of both catalogues. The resolutions of the ATCA-XXL and ATLAS-SPT mosaics are  $4.8$  and  $8''$ , respectively, but positional accuracies of unresolved sources due to Gaussian noise are usually much better than this on the order of  $\sqrt{2}\theta_{\text{FWHM}}/\text{SNR}$  (Condon, 1997). Since the lower SNR cutoff for both catalogues is 5, the highest positional accuracy of the faintest sources is  $< 2''$ . To test if this was an appropriate separation limit, I crossmatched the two catalogues using a range of limits. I then repeated this crossmatching with a shifted version of the ATCA-XXL catalogue: each source was shifted by  $\pm 10''$  in both RA and Declination and the number of matches were averaged per separation limit interval.

The number of genuine matches and false matches from the shifted catalogue are shown in Figure 3.6. The number of matches between the original (i.e. non-shifted) catalogues sharply rises from 0 as expected then plateaus and continues to rise with a much smaller gradient caused by false matches. This is further demonstrated by comparing the number of matches between the original and shifted catalogues: after the plateau, the gradient of the original matches closely resembles the gradient of the shifted matches, suggesting that matches beyond approximately  $2''$  are dominated by chance matches.

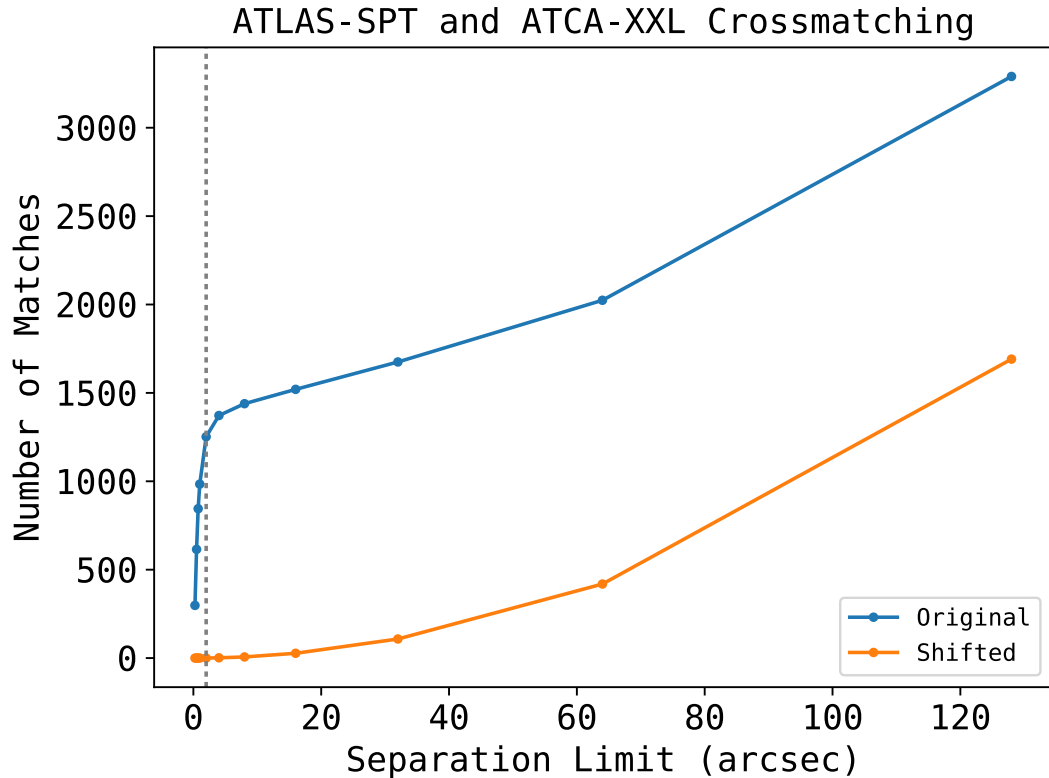


Figure 3.6: The number of sky position crossmatches between the ATLAS-SPT and ATCA-XXL source catalogues with various separation limits. The blue points trace the number of matches between the two original, unaltered catalogues; the orange points trace the average number of matches between the ATLAS-SPT catalogue and shifted ATCA-XXL catalogues. The vertical dotted line is drawn at  $2''$ , the final separation limit used to crossmatch the catalogues.

I then compared the flux densities of the crossmatched sources as shown in Figure 3.7. The flux densities are strongly correlated, with a correlation coefficient of  $r = 0.997$ . Note that no DC calibration corrections are required to compare these two catalogues as radio synthesis measurements do not measure a DC component, unlike other astronomical detectors such as CCDs. A few outliers are present which were all investigated. The three outliers at the faint end are multi-component sources that were grouped into a single source in ATLAS-SPT but were classified as separate sources in ATCA-XXL. The remaining outlier below the  $y = x$  line with an ATLAS-SPT flux of  $\sim 140 \text{ mJy beam}^{-1}$  is a point source in both catalogues and may

be intrinsically variable.

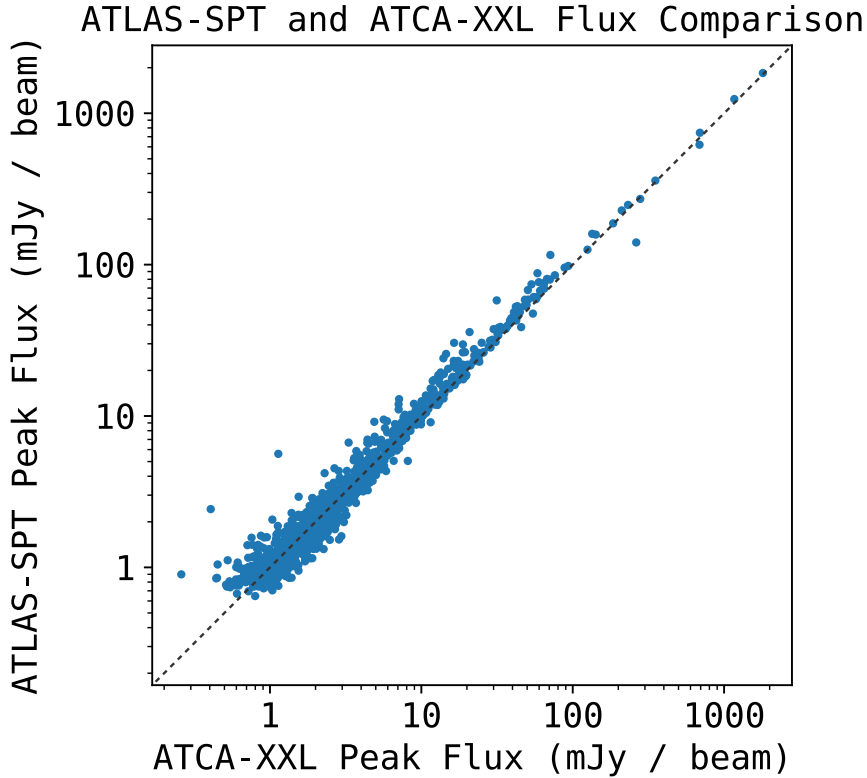


Figure 3.7: Comparison of flux densities of crossmatched sources between the ATLAS-SPT and ATCA-XXL source catalogues. The outliers were inspected visually and caused by mis-grouping in the ATCA-XXL catalogue, i.e. a source identified as a single multi-component source in the ATLAS-SPT catalogue was not grouped into a single source in the ATCA-XXL catalogue. The diagonal dotted line is drawn at  $y = x$  to guide the eye.

These crossmatched sources were also used to estimate the flux density calibration errors. To circumvent issues associated with differing beam sizes and imaging weightings, the crossmatches were restricted to unresolved ATCA-XXL sources as any source unresolved in ATCA-XXL will also be unresolved in the ATLAS-SPT catalogue. The flux density ratio between the two catalogues was calculated and the sources were grouped into 10 logarithmically spaced SNR bins. The flux density calibration error was estimated by averaging the standard deviations of the high SNR bins (the scatter in the low SNR bins is dominated by noise variations rather than calibration errors) after removing outliers that had flux density ratios beyond 1.5 times the interquartile range (i.e. flux ratios  $< Q_1 - 1.5 \times \text{IQR}$  and  $> Q_3 + 1.5 \times \text{IQR}$  were removed). The average standard deviation of the  $\geq 50$  SNR bins is  $\sigma_{\text{cal}} = 0.055$ . I therefore added a 5.5% flux density error in quadrature into the existing catalogue fitting errors. This is likely an overestimation of the ATLAS-SPT calibration error, but given that the ATCA-XXL data is deeper, the ATLAS-SPT fluxes would contribute more to the observed scatter between the two catalogue fluxes. Without a simple method to refine this estimation, I absorb the scatter into

the ATLAS-SPT calibration uncertainty.

Finally, I measured the positional accuracy between the two catalogues by comparing the coordinate offsets in the same manner as described in Section 3.2.1.2. The mean offset between source positions are  $\Delta\text{RA} = -0.01''$  and  $\Delta\text{Dec} = 0.09''$ . The standard deviation for both axes are  $\sigma_{\Delta\text{RA}} = 0.47''$  and  $\sigma_{\Delta\text{Dec}} = 0.51''$ . These results are shown in Figure 3.8.

Similarly to the flux density comparison, these positional comparisons can be used to estimate the positional errors due to calibration errors. As above, I used the high SNR bin scatter of  $\Delta\text{RA}$  and  $\Delta\text{Dec}$  to estimate the error. The average standard deviation of the  $\geq 50$  SNR bins is  $\sigma_{\text{cal,RA}} = 0.14''$  and  $\sigma_{\text{cal,Dec}} = 0.15''$ . These errors were added in quadrature to the existing fitting errors given in the catalogue.

### ATLAS-SPT and ATCA-XXL Positional Offsets

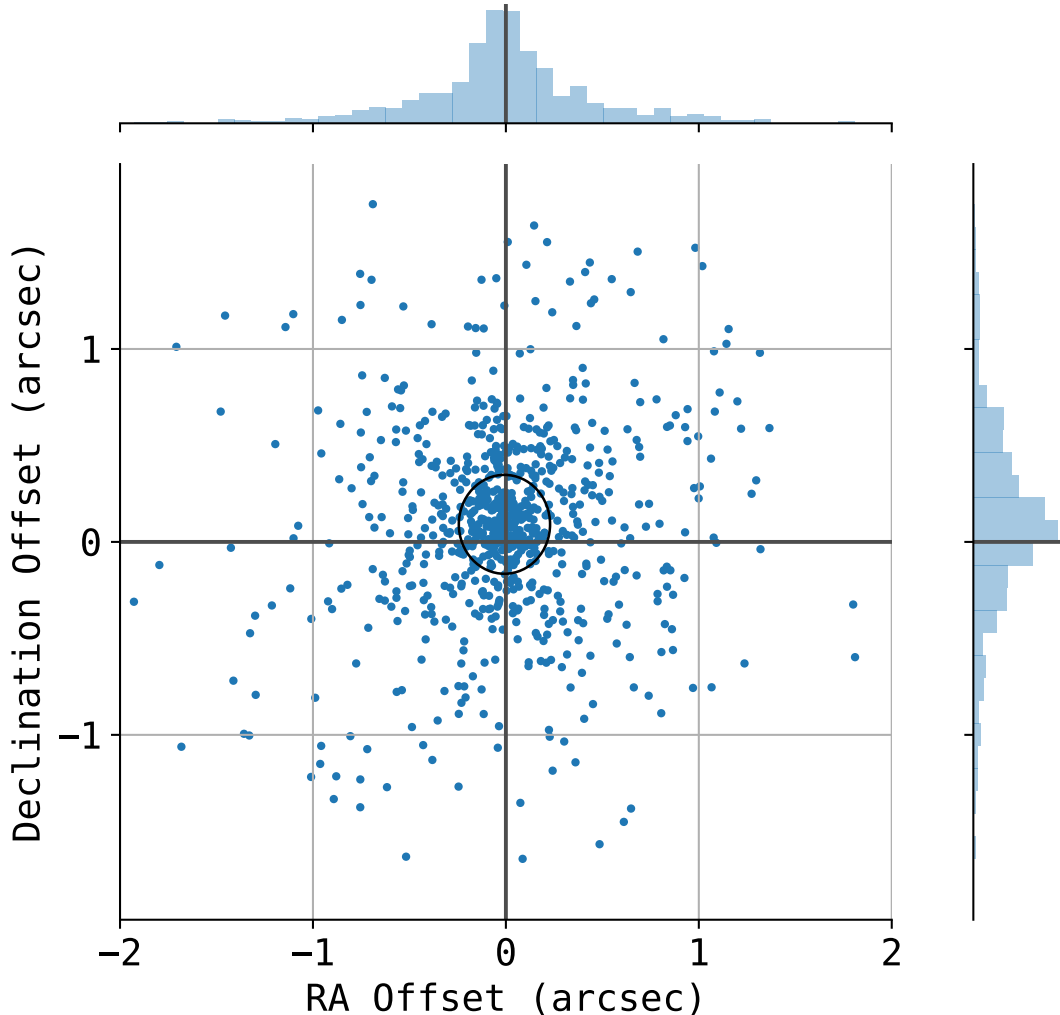


Figure 3.8: A comparison of the source positions between the ATLAS-SPT and ATCA-XXL catalogues. Each point is a cross-matched source between the two catalogues. The positions are in very good agreement: the average RA and Dec offsets ( $\Delta\text{RA}$ ,  $\Delta\text{Dec}$ ) are approximately  $-0.01$  and  $0.09''$ , respectively; and the standard deviations of both offsets ( $\sigma_{\Delta\text{RA}}$ ,  $\sigma_{\Delta\text{Dec}}$ ) are  $0.47$  and  $0.51''$ , respectively. The black ellipse is drawn centred on  $\Delta\text{RA}$ ,  $\Delta\text{Dec}$  with the width and height equal to  $\sigma_{\Delta\text{RA}}$  and  $\sigma_{\Delta\text{Dec}}$ , respectively.



### 3.3 Spectral Indices

When examining the flux distribution of a source as a function of frequency over some finite bandwidth, the gradient of the distribution is a helpful metric in determining the nature of the emission. Within the radio spectrum, continuum emission is generally assumed to follow a power law relation  $S(\nu) \propto \nu^\alpha$ , where  $\nu$  is the observed frequency and  $\alpha$  is the spectral index. The spectral index for a given source can therefore be found in log-space since  $\log S \propto \alpha \log \nu$ .

For radio continuum emission, the spectral index of thermal emission mechanisms seen in nebulae and stars is usually either positive or  $\sim 0$ . Non-thermal emission such as synchrotron radiation have negative and sometimes steep ( $< -1$ ) spectral indices. The spectral index of synchrotron radiation in particular is a measure of the electron energy distribution and from which we can infer the age of the electrons. See Chapter 13.1.3 of Kellermann and Owen (1988) for a detailed explanation of the astrophysics behind radio spectra.

The  $I\alpha$  mosaic from Section 2.4.3 was divided by the final Stokes  $I$  mosaic to produce a spectral index mosaic. The corresponding pixels for each PyBDSF Gaussian component were extracted from the spectral index mosaic and a weighted average of the pixel values was calculated. In the absence of a spectral index error map, I weighted the pixel values by their corresponding Stokes  $I$  values, reasoning that the brighter pixels of a component have more signal-to-noise and are therefore more reliable. The tool used to compute the  $I\alpha$  mosaic does not currently provide uncertainties and this is an active area of development.

Since the spectral index is calculated using data across the observed band, components near the Stokes  $I$  detection threshold are likely to have unreliable spectral indices due to significant noise contributions. Simulations by Heywood et al. (2016) found that Taylor-term derived spectral indices are artificially flattened as the source flux density approaches the detection threshold. To estimate the reliability of the spectral indices extracted from the spectral index mosaic, I cross-matched the components with sources from the 843 MHz SUMSS catalogue (Mauch et al., 2003). The resolution of SUMSS is  $43 \times 43'' \csc |\delta|$ , where  $\delta$  is the source Declination. For simplicity, I used a separation limit of  $56''$ , which corresponds to the SUMSS beam size at  $\delta = -50^\circ$ . This comparatively much lower resolution means that many unresolved sources in the SUMSS catalogue will be resolved in the ATLAS-SPT catalogue. At best, these sources must be visually inspected to ensure the matching algorithm has collected all ATLAS-SPT components that belong to an unresolved SUMSS source so that their component fluxes may be summed. At worst, the higher resolution of the ATLAS-SPT mosaic has resolved out some fraction of the source flux resulting in inaccurate spectral index calculations. To circumvent these issues, only unresolved sources from both catalogues were cross-matched. In addition, only isolated ATLAS-SPT components were considered; any component that was matched to

a SUMSS source that was either a member of multi-component source or within the separation limit of another component was discarded.

I then compared the component spectral indices with the spectral indices calculated between the ATLAS-SPT and their cross-matched SUMSS flux densities. The difference between the ATLAS-SPT Taylor-term derived spectral index and those derived from the ATLAS-SPT and cross-matched SUMSS flux densities are positively biased toward the source detection threshold indicating their unreliability (see Figure 3.9). The spectral index difference as a function of SNR is shown in Figure 3.10. This relative flattening of the ATLAS-SPT spectral index is in agreement with the result found by Heywood et al. (2016). To estimate a SNR threshold where the Taylor-term derived spectral indices are reliable, I binned the spectral index differences and calculated the median difference for each bin. I set the reliability threshold to where this median difference rises above 0 by one standard deviation. This point occurs approximately at a SNR of 40, so I therefore set a flux density SNR cutoff of 40 for components when recording their spectral index. This cutoff value is consistent with the simulations performed by Cavallaro et al. (2018). A more robust estimation of the spectral index reliability and their uncertainties could be made by injecting simulated sources with known spectra, in a similar method to the completeness simulations described in Section 3.2.1.1. This analysis will be conducted in future work.

The total integrated spectral index for each source was then calculated by first computing the total integrated flux densities at both ends of the observing band (1.1 and 3.1 GHz) for each source component using the spectral index extracted from the spectral index mosaic

$$S_{\nu,c} = S_{\nu_0,c} \left( \frac{\nu}{\nu_0} \right)^{\alpha_c}$$

where  $c$  denotes the component and  $\alpha$  is the spectral index of the component. Note that the component spectral indices were determined by the flux weighted average of the component pixels in the spectral index mosaic as described above. The component flux densities were then summed for each source and the slope between these flux densities

$$\alpha_s = \frac{\log(\sum S_{1.1,c} / \sum S_{3.1,c})}{\log(1.1/3.1)}$$

was recorded as the total integrated spectral index of the source. The total integrated spectral index of any source that did not contain at least one component above the SNR cutoff was flagged and omitted from the catalogue. The total number of sources that have a spectral index recorded is 722.

The spectral index distribution for all 722 sources is shown in Figure 3.11. The distribution

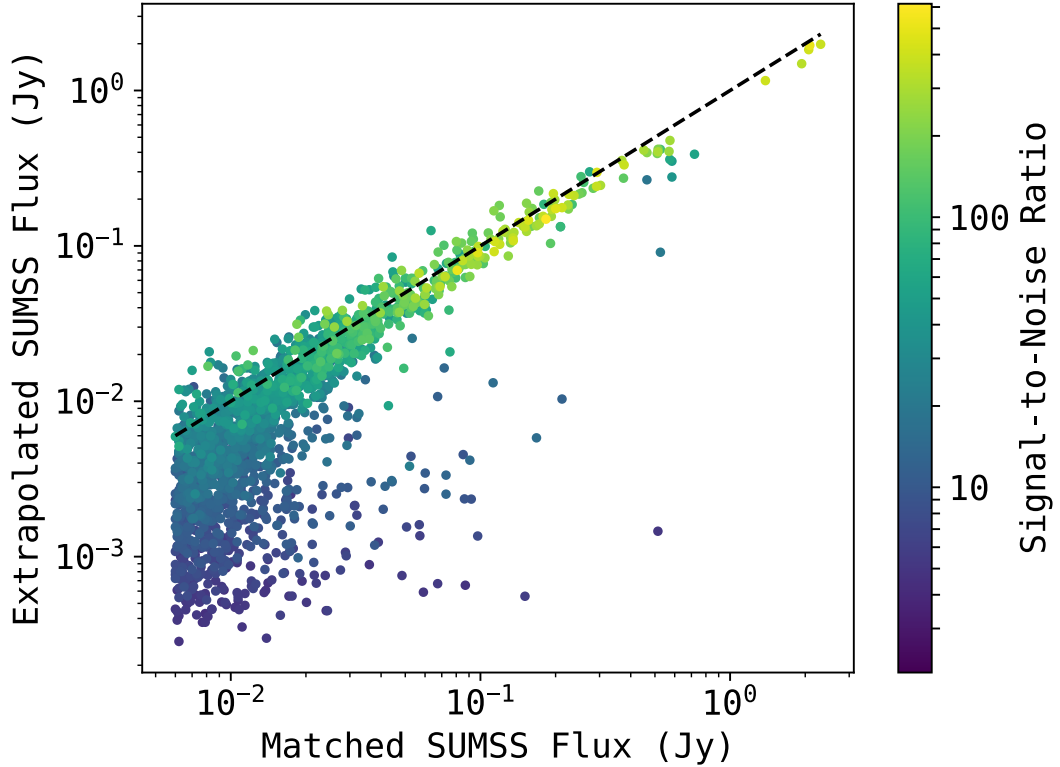


Figure 3.9: The flux densities of cross-matched point sources from the ATLAS-SPT and SUMSS source catalogues. The flux density from SUMSS is shown on the horizontal axis and the source flux densities extrapolated from the ATLAS-SPT fluxes to the SUMSS frequency (843 MHz) using the extracted spectral indices is shown on the vertical axis. Each source is coloured according to its signal-to-noise ratio. The line of equality is drawn as a black dashed line to guide the eye.

peaks within the  $\alpha = -0.8$  to  $-0.7$  bin, which is consistent with the typical spectral index of AGN (Kimball and Ivezić, 2008). The distributions of single and multiple component sources are also consistent with expectations. Sources made up of multiple components are most likely resolved AGN, where the lobe components are expected to contain ageing electrons and exhibit steeper negative spectral indices. Single component sources are also most likely AGN (the sensitivity of the ATLAS-SPT survey is not quite deep enough to significantly probe the star-forming galaxy population) and are expected to exhibit slightly flatter spectral indices due to synchrotron self-absorption.

### 3.4 Source Counts

Source counts are a measure of the number of sources at given flux densities per unit of sky area. These counts have usually been presented in one of two ways: the integral source count, or the differential source count. Integral source counts are the number of sources per unit of sky area stronger than a given flux density, i.e.  $\int_S^\infty n(s)ds$ . The more common differential source

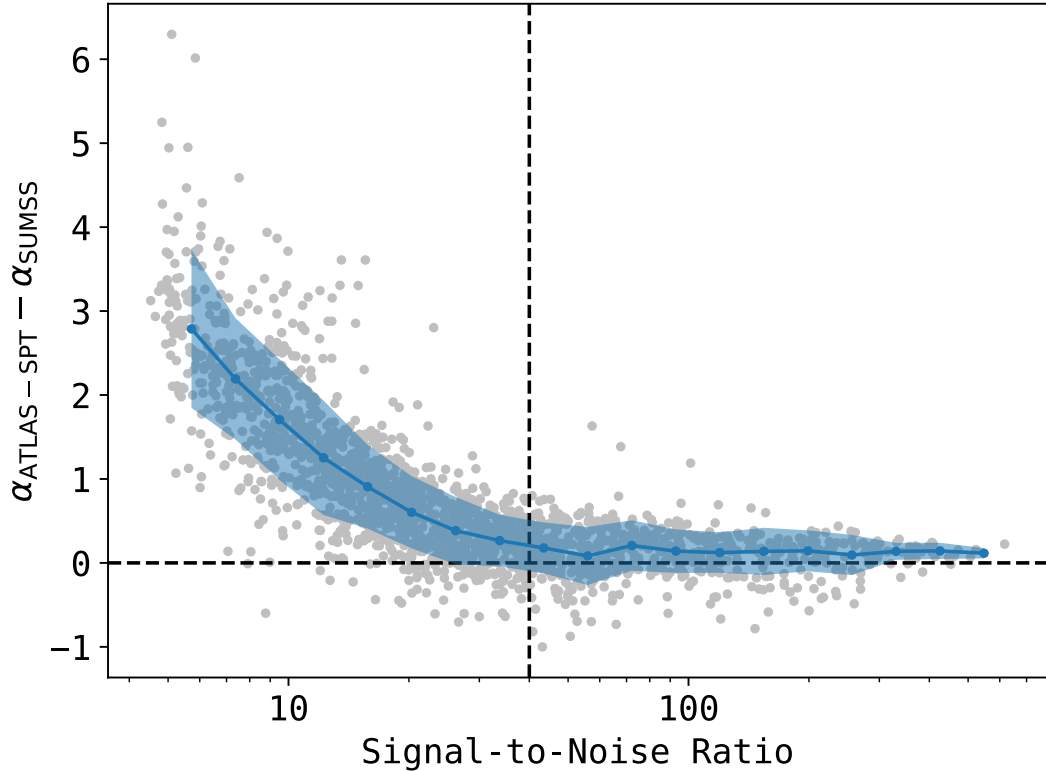


Figure 3.10: The difference between the spectral indices extracted from the ATLAS-SPT spectral index map and the spectral indices calculated using cross-matched sources from SUMSS. The spectral indices become unreliable below a SNR of 40.

counts are the number of sources per unit of sky area within a flux density range, i.e.  $n(S)dS$ .

Historically, source counts have been used to help determine the geometry of the Universe and unveil the cosmological evolution of source populations. While they are now most useful for the latter, they were initially used as evidence that the universe does not have Euclidean geometry with a constant matter density as many cosmologists believed. In such a universe filled with a population of non-evolving sources with flux density  $S$ , one would expect  $S$  to decrease with distance in accordance with the inverse-square law ( $S \propto D^{-2}$ ) and the number of sources to increase as  $D^3$ . The integrated source counts  $n(S)$  then would scale with flux density as  $n(S) \propto S^{-1.5}$ . Radio source counts were quickly found to deviate from this relationship (Ryle and Scheuer, 1955; Mills et al., 1958; Scheuer and Ryle, 1957), providing strong evidence that either the Universe is not Euclidean or it does not have a constant matter density. More recent interpretations of source counts, especially the differential form, provide evidence that the radio sources observed do not belong to a single population but are made up of a myriad of morphologies, luminosity classes and evolve differently with time (Windhorst et al., 1984; Fomalont et al., 1984; Condon and Mitchell, 1984). As such, source counts are mostly used in modern astronomy to determine the fractions of source populations (e.g. the number of AGN

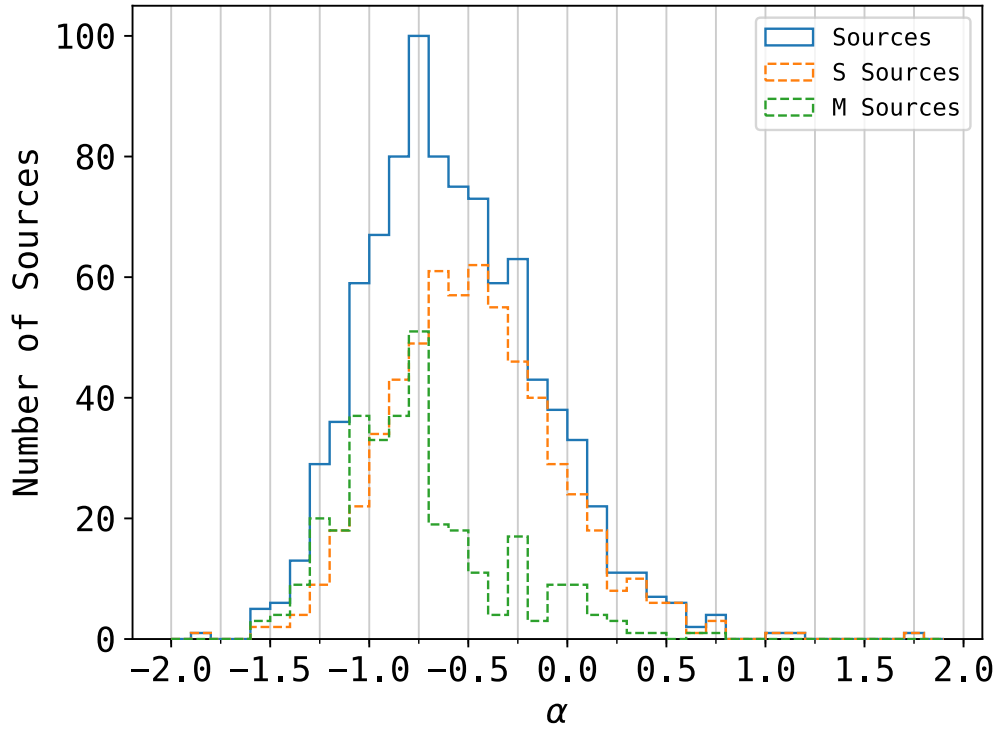


Figure 3.11: The distribution of spectral indices for all 722 sources above the reliability threshold. The total distribution is shown as a solid blue line; sources comprised of a single component are shown as a dashed orange line; and sources comprised of more than one component are shown as a dashed green line.

and star-forming galaxies) and how their luminosities evolve with time.

In this section, I present the differential source counts from the ATLAS-SPT source catalogue. While this result does not probe beyond the already well-studied differential source counts at this frequency, comparing it to previous results validates the catalogue.

The differential source counts were calculated as follows. All source flux densities were corrected for boosting using the completeness simulation results described in Section 3.2.1.2. For each flux bin in Figure 3.3, the ratio between the known simulated source flux density (input) and the measured source flux density after image processing (output) is calculated. This ratio is used to correct the catalogue fluxes for flux boosting by interpolating values from the results presented in Figure 3.3 using a cubic spline. The sources were then binned into 20 logarithmically spaced bins starting at the lowest integrated flux density in the catalogue,  $\sim 0.54$  mJy. The number of sources  $N$  falling in each bin were counted which were then corrected for completeness as described in Section 3.2.1.1 by a correction factor  $f_c$  using the results presented in Figure 3.2 in the same manner as the flux boosting correction. The number of sources per unit of sky area was determined using the results from Figure 2.7 by dividing  $Nf_c$  by the area in which sources with a flux density equal to the bin average were detectable. Finally,

the Euclidean-normalised source count  $S^{2.5}dN/dS$  was calculated by dividing the corrected counts by their bin widths and multiplying the result by  $\langle S \rangle^{2.5}$  where  $\langle S \rangle$  is the geometric mean of the flux densities for each bin. Uncertainties were calculated by adding the Poisson uncertainties of  $N$  with the completeness and flux boosting uncertainties in quadrature, i.e.  $\sqrt{\sigma_P^2 + \sigma_c^2 + \sigma_{fb}^2}$  where  $\sigma_P = (\sqrt{N}/N)(S^{2.5}dN/dS)$ .

The source counts and relevant values are given in Table 3.2 and are compared to other studies compiled by De Zotti et al. (2010) in Figure 3.12. The counts mostly agree with previous studies. Deviations toward the bright end are due to the relative low number of sources found in those flux density bins as noted by Heywood et al. (2016). Even with the large area of the ATLAS-SPT survey, accurately producing source counts for these bright sources is difficult due to their rarity and requires data covering a much larger area (e.g. NRAO VLA Sky Survey (NVSS) or EMU). The ATLAS-SPT survey best samples sources in the 1 to 10 mJy range and the slope in Figure 3.12 at these flux densities is typical for AGN evolution. The flattening toward the faint end is due to the increased number of star-forming galaxies; the ATLAS-SPT survey is limited by sensitivity and does not probe this flux density range like smaller but deeper surveys like the original Australia Telescope Large Area Survey (ATLAS). The faintest flux bin source count is poorly sampled and the uncertainty for this bin is likely underestimated. For a more detailed interpretation of the structure in the Euclidean-normalised integrated source count diagram, see Condon et al. (2012).

$S_L$ (mJy)	$S_U$ (mJy)	$\langle S \rangle$ (mJy)	$N$	Area (deg <sup>2</sup> )	$f_c$	$S^{2.5}dN/dS$ (Jy <sup>1.5</sup> sr <sup>-1</sup> )	Uncertainty (Jy <sup>1.5</sup> sr <sup>-1</sup> )
0.54	0.84	0.76	363	21.9	1.05	3.2	0.3
0.84	1.31	1.06	1292	64.3	1.02	5.6	0.2
1.31	2.04	1.63	1032	79.6	1.01	7.1	0.3
2.04	3.18	2.52	760	84.3	1.00	9.7	0.4
3.18	4.96	3.96	527	85.4	1.00	13.0	0.6
4.96	7.74	6.22	432	85.6	1.00	20.6	1.0
7.74	12.07	9.67	445	85.6	1.00	40.5	1.9
12.07	18.83	15.10	380	85.6	1.00	66.6	3.4
18.83	29.37	23.09	273	85.6	1.00	87.7	5.3
29.37	45.80	36.62	210	85.6	1.00	135.4	9.3
45.80	71.43	55.71	151	85.6	1.00	176.4	14.4
71.43	111.40	86.61	98	85.6	1.00	219.2	22.1
111.40	173.74	138.80	52	85.6	1.00	240.3	33.3
173.74	270.96	219.29	28	85.6	1.00	258.3	48.8
270.96	422.58	314.53	12	85.6	1.00	173.9	50.2
422.58	659.05	502.85	5	85.6	1.00	149.2	66.7
659.05	1027.84	865.02	1	85.6	1.00	73.8	73.8
1027.84	1602.99	1268.48	4	85.6	1.00	491.5	245.7
1602.99	2500.00	2117.42	2	85.6	1.00	565.0	399.5

Table 3.2: Differential source counts calculated from the ATLAS-SPT source catalogue. The lower and upper flux density bin boundaries are given as  $S_L$  and  $S_U$ , respectively. The geometric mean of the flux densities within each bin is given as  $\langle S \rangle$ . The raw source counts (after flux boosting corrections) are given as  $N$  and the mosaic area in which  $\langle S \rangle$  exceeded the  $5\sigma$  detection threshold is given as ‘Area’. The correction factor applied to  $N$  due to completeness is given as  $f_c$ . The Euclidean-normalised differential source count and its uncertainty is given as  $S^{2.5}dN/dS$  and ‘Uncertainty’.

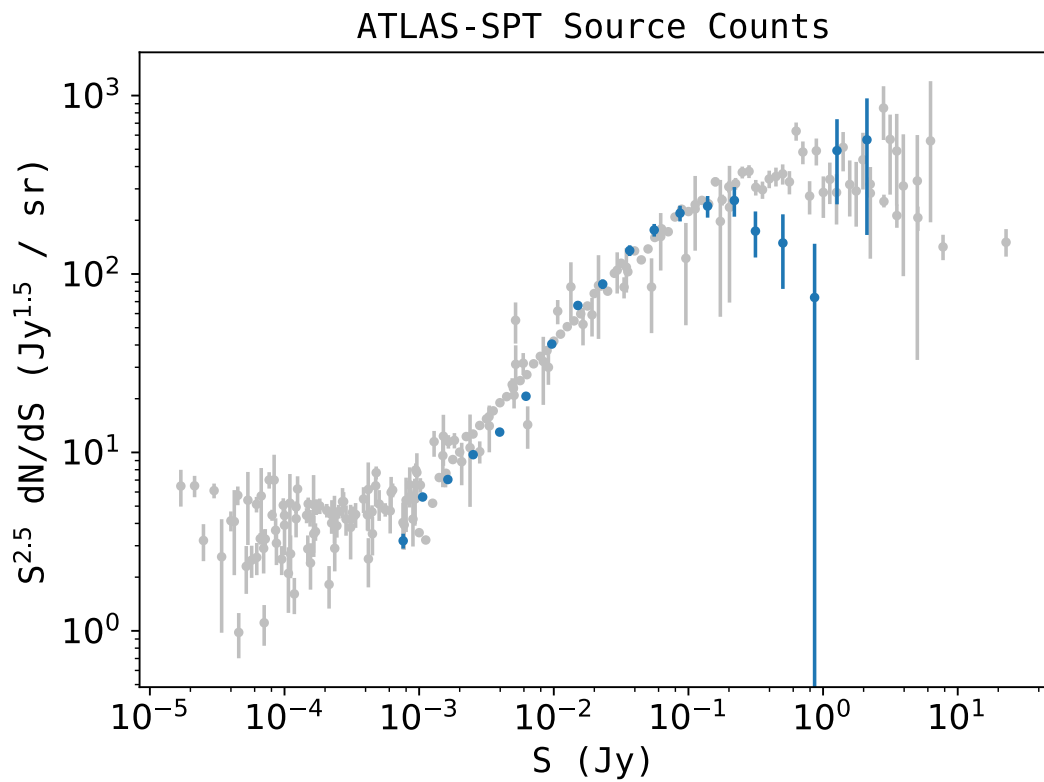


Figure 3.12: The ATLAS-SPT source counts compared with previous studies normalised for a Euclidean universe. Various previous results tabulated by De Zotti et al. (2010) are plotted in grey, source counts from this work are plotted in blue.



# Chapter 4

## Bent-Tail Radio Sources

This chapter is reproduced from my original work submitted to *Monthly Notices of the Royal Astronomical Society* in January 2018.

### 4.1 Introduction

Bent-tail (BT) radio sources (also known as head-tail galaxies, wide-angle tails and narrow-angle tails) are a class of radio galaxy in which the jets expelled from the central supermassive black hole have been bent or significantly distorted from their typical linear trajectory. The complex morphologies of BT radio sources can be explained by environmental effects, the most significant of which is the exertion of strong ram pressures on the jets caused by the relative motion of the host galaxy through a dense medium. This motion may be a galaxy moving through a dense medium, or the by medium itself moving across the galaxy. A radio galaxy with a large peculiar velocity moving through the ICM of its host cluster may produce jet distortions, provided the velocity and density of the ICM are high enough (Miley et al., 1972; Rudnick and Owen, 1976; Burns, 1990). These distortions may also be caused by violent movement of the ICM due to the merger history of the cluster (Burns, 1990; Roettiger et al., 1996; Burns et al., 1996; Filipovic et al., 2010). This makes BT radio sources a useful tool for probing galaxy interactions on large scales with several studies showing that they tend to reside in galaxy clusters (Blanton et al., 2000; Mao et al., 2009, 2010; Wing and Blanton, 2011; Dehghan et al., 2014).

Galaxy clusters are the largest gravitationally bound structures in the Universe. They are formed around dark matter concentrations where sheets and filaments of the cosmic web intersect and therefore trace the large-scale structure of the Universe. They are traditionally detected by optical searches for galaxy over-densities followed by photometric or spectroscopic measurements (Gladders and Yee, 2005; Wilson et al., 2008; Kodama et al., 2007). Another

technique is to detect the thermal emission from the diffuse ICM in the X-ray band (Rosati et al., 1998; Romer et al., 2001; Pierre et al., 2004). Both of these techniques, and others that rely on X-ray or optical observations, are typically limited to detecting clusters within the local Universe ( $z \lesssim 0.2$ ) as cosmological dimming effects make observing more distant clusters difficult. As a result of these methods, tens of thousands of clusters are known with only a few at  $z > 1$ . In order to study the evolution of clusters, larger samples of more distant (and therefore younger) clusters are required.

To study younger clusters, an alternative detection technique must be used such as the Sunyaev-Zel'dovich (SZ) effect (Sunyaev and Zeldovich, 1972) which is caused by inverse-Compton scattering of the Cosmic Microwave Background (CMB). As CMB photons pass through a dense plasma (such as an ICM), they collide with the rapidly moving particles in the plasma and receive a boost in energy. This can be observed as a localised increase in higher frequency photons and consequent decrement in lower frequency photons when compared with the surrounding CMB. As this is a direct measurement of the ICM column density, the SZ effect is an extremely useful tool for detecting galaxy clusters. A great benefit of the SZ effect technique is that it is redshift independent since the CMB energy density increases with redshift, cancelling out any cosmological dimming that affects optical or X-ray cluster measurement techniques.

The use of BT radio sources as galaxy cluster indicators shares this ability to detect more distant clusters as even modestly sensitive radio observations are able to detect radio galaxies up to high redshifts. BT radio sources have already been used to find clusters in the local Universe (up to  $z \sim 1$ ) (Blanton et al., 2003). Evidence of their effectiveness at tracing more distant clusters up to  $z \sim 2$  is growing (e.g. Dehghan et al. (2014)), suggesting that BT radio sources could be used to find galaxy clusters during their formative periods. Norris et al. (2013) has shown that the Evolutionary Map of the Universe (EMU) survey (Norris et al., 2011) may detect hundreds of thousands of BT galaxies, more than the number of currently known clusters, and this is one of the motivations driving the study reported here.

Recent simulations performed by Mguda et al. (2015) have shown that groups and clusters with host dark matter halo masses above  $10^{13}h^{-1}M_{\odot}$  typically host at least one BT radio source at some time. If true, the potential for radio surveys to detect distant clusters via correlation with BT sources is especially attractive as it comes for free in any radio dataset with sufficient resolution to resolve the jets and lobes (i.e. on the order of several arcseconds).

This paper aims to determine the efficacy of detecting distant clusters by correlating BT radio sources identified in the high-resolution ATLAS-SPT radio catalogue with confirmed galaxy clusters from the literature. A preliminary account of this work was reported by

O’Brien et al. (2016). Throughout this paper we assume a flat  $\Lambda$ CDM cosmology with  $H_0 = 69.3 \text{ km s}^{-1}\text{Mpc}^{-1}$  and  $\Omega_M = 0.286$  unless otherwise stated.

## 4.2 Results

### 4.2.1 Bent-tail Radio Source Sample

The BT sources were identified manually by searching the combined total intensity mosaic (see Section 2.4) for FR-I and FR-II radio sources (Fanaroff and Riley, 1974) that showed significant bending or distortions away from a typical linear trajectory, and radio sources that showed the typical intensity asymmetry of head-tail radio galaxies (i.e. where the source appears to have an intense core with diffuse structure on only one side). If the radio core was clearly visible, its position was recorded. If the core was not easily determined, an estimation of the core position was made based on the morphology of the source. A total of 46 BT candidates were identified and are listed in Table 4.1. Cutout images of each object are shown in Section 4.A.

### 4.2.2 Measuring Bent-tail Flux Densities

We used the source-finding software PyBDSF (Mohan and Rafferty, 2015) to measure the total integrated fluxes of the BT sources. A  $0.25 \times 0.25^\circ$  cutout image was made for each BT source and used as the input to PyBDSF. The background noise was estimated using a sliding box of  $200 \times 200$  px stepped by 50 px. The software then searched for peaks of emission above  $5\sigma$  and then flood-filled down to  $3\sigma$  around each peak to create an island. The pixels encompassed by the islands were then fit with multiple Gaussian components.

PyBDSF output a catalogue of Gaussian components and a catalogue of grouped components that the software considers sources. We found that the automated grouping, although configurable with a variety of parameters, did not always group all components from a BT source into a single source. We therefore grouped the components manually and summed the catalogued total flux densities for each component fit to the BT to determine the total integrated flux density. The total integrated flux densities for all BT sources are reported in Table 4.1 (column 11) and the distribution of these flux densities is shown in Figure 4.1.

### 4.2.3 Measuring Bent-tail Spectral Indices

The spectral index<sup>1</sup> of each bent-tail source was measured using the same method described in Section 3.3. This involves dividing the  $I\alpha$  plane of the mosaic by the total intensity plane to produce a spectral index map. For each BT source component, the pixels from this spectral

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<sup>1</sup>We use the convention  $S \propto \nu^\alpha$ .

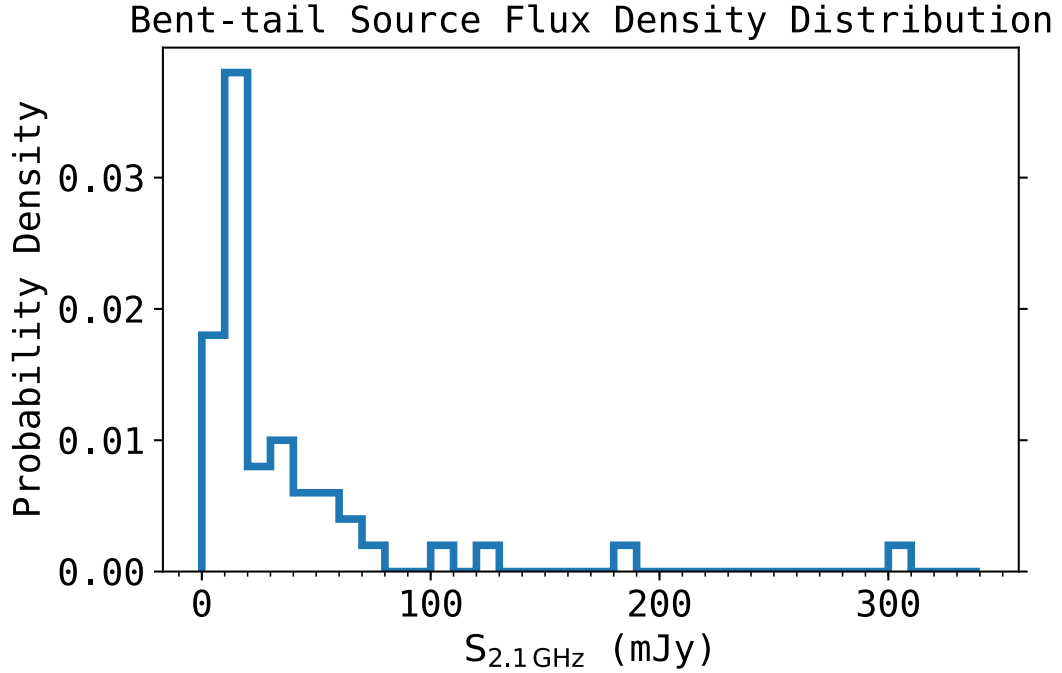


Figure 4.1: The distribution of the total integrated flux densities for the bent-tail radio sources detected in the ATLAS-SPT survey. The bin widths are 10 mJy and the values are normalised to form a probability distribution such that the integral of the histogram is equal to 1.

index map are then extracted and a flux-weighted average is calculated to produce a component spectral index. Flux densities for both sides of the 1.1 to 3.1 GHz observing band are calculated by extrapolation using the flux densities and spectral indices of each component. These extrapolated component flux densities are then summed per BT source to produce total integrated flux densities at both sides of the band from which a total integrated spectral index was derived for each BT source.

After applying a SNR reliability threshold of 40 to the spectral indices as described in Section 3.3, only 10 BT sources have a sufficient SNR to produce a reliable spectral index. The distribution of these spectral indices are shown in Figure 4.2 overplotted on the full ATLAS-SPT source spectral index distribution. We note that the spectral indices of these BT sources appear to lie in the typical range of values expected for AGN.

## 4.2.4 Cross-identification

### 4.2.4.1 Near-infrared

We visually cross-matched our BT radio source sample with catalogued sources from deep ( $5\sigma$  sensitivity of  $7.0 \mu\text{Jy}$ )  $3.6 \mu\text{m}$  images from the *Spitzer* South Pole Telescope Deep Field (Ashby et al., 2014, SSDF). If an AGN core was obvious in the radio image, a corresponding SSDF source was searched for around the radio core position. Otherwise, we selected the nearest SSDF

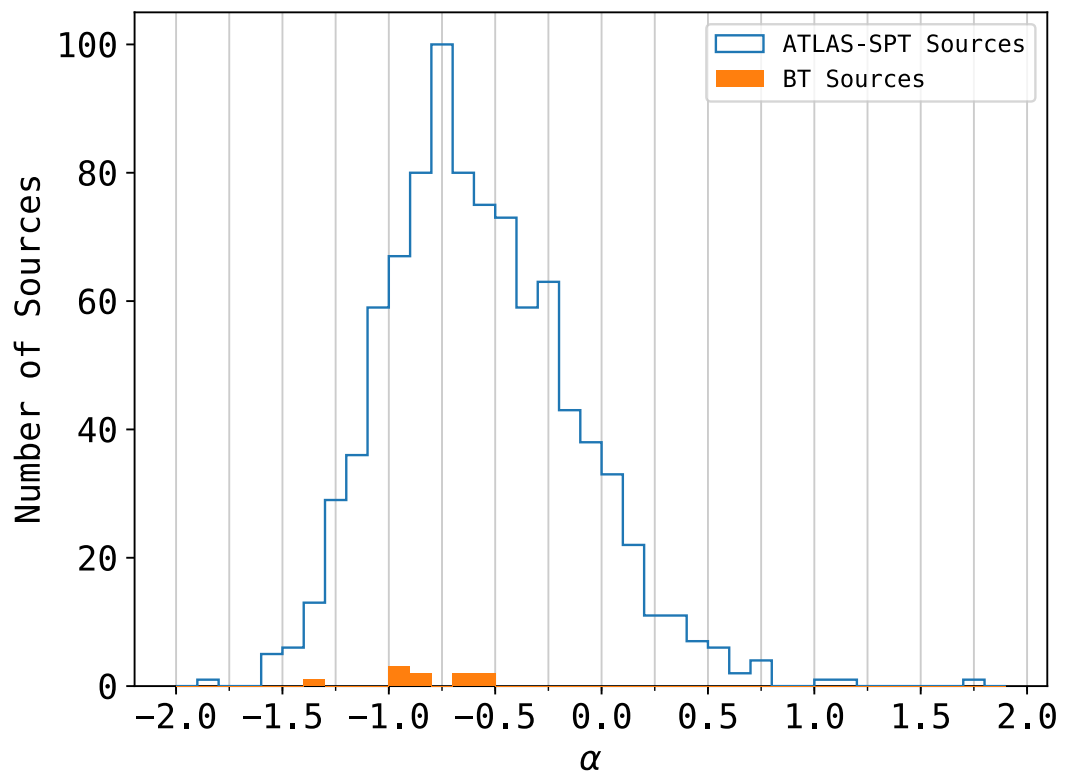


Figure 4.2: The spectral index distribution of the 10 bent-tail sources with reliable spectral indices shown on top of all spectral indices from the ATLAS-SPT catalogue. The BT source spectral indices appear consistent with values expected from AGN.

source to an estimated core position based on the source morphology. In cases where the radio core is ambiguous and there are multiple possible SSDF counterparts, we investigated each likely cross-match when determining if the candidate resides in a known cluster (see Section 4.2.6).

To estimate the number of chance cross-identifications, we repeated this cross-matching process using a copy of the SSDF catalogue shifted by  $\pm 10'$  in both RA and Declination. We counted each occurrence when a shifted SSDF source may have been misidentified as the host galaxy for a BT and find that 34% of our BT sources could be falsely matched with an SSDF source. This relatively high fraction is due to a combination of effects. The first is that the SSDF catalogue has a far greater source density and higher resolution compared to our radio BT catalogue. This, combined with the fact that all our BT sources are extended, increases the chances of finding false identifications. Secondly, for 56% of our BT sources, the position of the radio core is not always clear from the radio image alone so the core position is identified by the presence of an SSDF source. This means that when matching with the shifted SSDF catalogue there is a much larger area a shifted source may be located within which would result in recording a potential false identification. When matching a BT source which has a clearly distinguishable core in the radio image with its SSDF counterpart, the area the shifted source must be in is much smaller and therefore there is less chance of recording a potential false identification.

An infrared counterpart was recorded for all BT candidates which are the coordinates given in Table 4.1 (columns 4 and 5).

#### 4.2.4.2 Optical

20 sources of our 46 source BT sample are covered by the combined footprint of the Blanco Cosmology Survey (Desai et al., 2012, BCS) and the Dark Energy Survey (Dark Energy Survey Collaboration et al., 2016, DES) Science Verification (SV) “Gold” data release<sup>2</sup> as described in Rykoff et al. (2016). The BCS and DES SV catalogues are mostly distinct with a small region of overlap. We cross-matched our BT sample with the BCS and DES SV catalogues automatically, searching for the nearest match between the SSDF counterparts and optical sources within  $1''$ . Search radii above this value (up to  $4''$ ) did not increase the number of matches. Only 16 of our 20 BT sources in the optical survey area have optical counterparts: 10 matches from BCS and 10 matches from the DES SV catalogue (4 sources appear in both BCS and DES SV). For both optical catalogues, the cross-matching was repeated 8 times with varying coordinate offsets of  $\pm 10'$  in both RA and Declination to estimate the false cross-identification rate. An average of 0.125 offset matches were found within  $1''$  for both the BCS and DES SV catalogues.

<sup>2</sup><https://des.ncsa.illinois.edu/releases/sva1>

### 4.2.5 Estimating BT Source Redshifts

Both the BCS and DES SV optical catalogues introduced in Section 4.2.4 contain photometric redshifts which we use to estimate the redshifts for our BT sample. Photometric redshifts provided in the BCS catalogue were estimated using an artificial neural network, ANNz (Collister and Lahav, 2004), and errors were provided in the catalogue. Bonnett et al. (2016) provide photometric redshifts for the DES SV catalogue using several different techniques. We use those estimated using the ANNz2 (Sadeh et al., 2016) technique to remain as consistent as possible with the BCS estimates. No errors were provided in the catalogue, but a normalised probability distribution function (PDF) for each redshift bin was provided for each source. We estimate the photo- $z$  error by determining the cumulative sum of the PDF then calculating half the difference between the 16th and 86th quartiles.

We use the photometric redshifts for all 16 optically-matched BT sources from the optical catalogues described in Section 4.2.4.2. The redshift distribution of the BT source candidates are shown in Figure 4.3 along with the redshift distribution of the BCS and DES optical catalogues. We note that the redshift distribution of our BT sample appears to be skewed toward low redshifts compared to the optical catalogues. We confirmed that this difference was statistically significant using a K-S test (BCS-BT p-value: 0.012; DES-BT p-value: 0.008). The 4 sources that have photometric redshift estimates from both BCS and DES SV are in agreement within their errors.

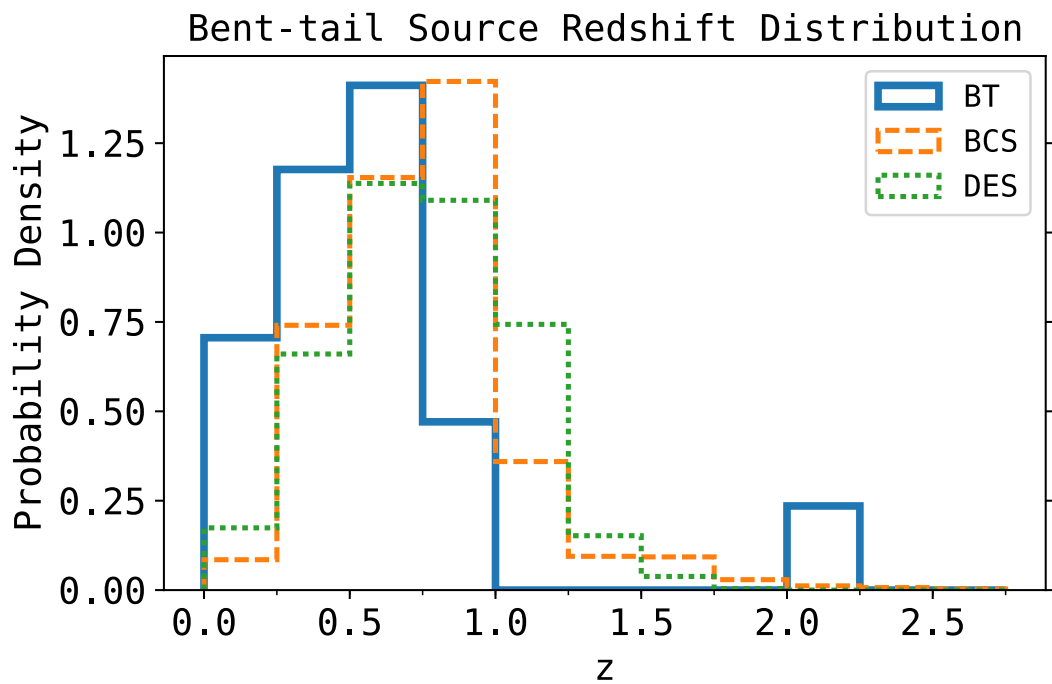


Figure 4.3: The redshift distribution of the 16 bent-tail source candidates with optical counterparts in the ATLAS-SPT survey. The bin values are normalised to form a probability distribution such that the integral of each histogram is equal to 1. The redshift distributions of the BCS and DES optical catalogues used for cross-matching as described in Section 4.2.5 are also shown for comparison.



Table 4.1: Bent-tail source candidates identified in the ATLAS-SPT survey. The ID of candidate BTs requiring follow-up observation are marked with an asterisk (\*). The RA and Dec coordinates given in columns 2 and 3 are flux-weighted radio positions, those given in columns 4 and 5 are for the 3.6  $\mu\text{m}$  counterparts from SSDF, and those given in columns 6 and 7 are for the optical counterparts from either the BCS or the DES catalogues. Columns 8, 9 and 10 are the photometric redshifts for the BT, the  $1\sigma$  error for the redshift, and the source of the redshift value, respectively. The total integrated flux densities of the BT sources and their  $1\sigma$  errors are given in columns 11 and 12, respectively.

ID	RA	Dec	SSDF RA	SSDF Dec	Optical RA	Optical Dec	$z$	$z_\sigma$	$z_{\text{ref}}$	$S$	$S_\sigma$
(1)	J2000 (hms)	J2000 (dms)	J2000 (hms)	J2000 (dms)	J2000 (hms)	J2000 (dms)	(8)	(9)	(10)	(mJy)	(12)
1*	23 <sup>h</sup> 18 <sup>m</sup> 41.296 <sup>s</sup>	-50°27'13.110''	23 <sup>h</sup> 18 <sup>m</sup> 41.596 <sup>s</sup>	-50°27'16.420''	—	—	—	—	—	48.36	0.54
2	23 <sup>h</sup> 51 <sup>m</sup> 22.159 <sup>s</sup>	-50°17'44.100''	23 <sup>h</sup> 51 <sup>m</sup> 21.874 <sup>s</sup>	-50°17'45.647''	—	—	—	—	—	58.90	0.72
3	23 <sup>h</sup> 55 <sup>m</sup> 15.044 <sup>s</sup>	-50°23'05.910''	23 <sup>h</sup> 55 <sup>m</sup> 15.138 <sup>s</sup>	-50°23'04.326''	—	—	—	—	—	48.50	0.74
4	23 <sup>h</sup> 32 <sup>m</sup> 27.232 <sup>s</sup>	-50°38'07.630''	23 <sup>h</sup> 32 <sup>m</sup> 27.128 <sup>s</sup>	-50°38'06.655''	—	—	—	—	—	17.07	0.32
5	23 <sup>h</sup> 21 <sup>m</sup> 10.191 <sup>s</sup>	-50°54'07.590''	23 <sup>h</sup> 21 <sup>m</sup> 10.182 <sup>s</sup>	-50°54'06.635''	—	—	—	—	—	29.69	0.96
6*	23 <sup>h</sup> 12 <sup>m</sup> 55.859 <sup>s</sup>	-50°40'21.710''	23 <sup>h</sup> 12 <sup>m</sup> 56.403 <sup>s</sup>	-50°40'16.756''	—	—	—	—	—	155.45	0.83
7*	23 <sup>h</sup> 13 <sup>m</sup> 15.294 <sup>s</sup>	-51°01'29.560''	23 <sup>h</sup> 13 <sup>m</sup> 14.692 <sup>s</sup>	-51°01'11.964''	—	—	—	—	—	327.41	2.50
8*	23 <sup>h</sup> 55 <sup>m</sup> 14.243 <sup>s</sup>	-50°56'25.660''	23 <sup>h</sup> 55 <sup>m</sup> 13.799 <sup>s</sup>	-50°56'28.403''	—	—	—	—	—	23.61	0.74
9	23 <sup>h</sup> 45 <sup>m</sup> 55.763 <sup>s</sup>	-51°12'14.620''	23 <sup>h</sup> 45 <sup>m</sup> 55.770 <sup>s</sup>	-51°12'14.929''	—	—	—	—	—	42.89	1.46
10*	23 <sup>h</sup> 31 <sup>m</sup> 42.469 <sup>s</sup>	-51°20'55.840''	23 <sup>h</sup> 31 <sup>m</sup> 42.520 <sup>s</sup>	-51°20'56.897''	—	—	—	—	—	8.56	0.48
11*	23 <sup>h</sup> 27 <sup>m</sup> 13.466 <sup>s</sup>	-51°23'35.730''	23 <sup>h</sup> 27 <sup>m</sup> 13.602 <sup>s</sup>	-51°23'34.260''	—	—	—	—	—	49.20	0.55
12	23 <sup>h</sup> 26 <sup>m</sup> 46.111 <sup>s</sup>	-51°29'37.690''	23 <sup>h</sup> 26 <sup>m</sup> 46.136 <sup>s</sup>	-51°29'38.684''	—	—	—	—	—	25.21	0.78
13	23 <sup>h</sup> 12 <sup>m</sup> 46.233 <sup>s</sup>	-51°18'12.610''	23 <sup>h</sup> 12 <sup>m</sup> 45.966 <sup>s</sup>	-51°18'12.938''	—	—	—	—	—	19.57	0.62
14*	23 <sup>h</sup> 09 <sup>m</sup> 25.293 <sup>s</sup>	-51°10'58.950''	23 <sup>h</sup> 09 <sup>m</sup> 25.649 <sup>s</sup>	-51°10'55.477''	—	—	—	—	—	19.24	0.49
15*	23 <sup>h</sup> 01 <sup>m</sup> 59.105 <sup>s</sup>	-51°34'42.750''	23 <sup>h</sup> 01 <sup>m</sup> 58.751 <sup>s</sup>	-51°34'41.545''	—	—	—	—	—	10.19	0.73
16	23 <sup>h</sup> 07 <sup>m</sup> 09.384 <sup>s</sup>	-52°00'06.150''	23 <sup>h</sup> 07 <sup>m</sup> 09.434 <sup>s</sup>	-52°00'06.566''	—	—	—	—	—	124.23	1.26
17*	23 <sup>h</sup> 12 <sup>m</sup> 53.843 <sup>s</sup>	-51°58'32.040''	23 <sup>h</sup> 12 <sup>m</sup> 53.981 <sup>s</sup>	-51°58'40.645''	—	—	—	—	—	52.62	0.73
18	23 <sup>h</sup> 19 <sup>m</sup> 23.468 <sup>s</sup>	-52°25'17.950''	23 <sup>h</sup> 19 <sup>m</sup> 23.479 <sup>s</sup>	-52°25'17.479''	23 <sup>h</sup> 19 <sup>m</sup> 23.554 <sup>s</sup>	-52°25'17.292''	0.42	0.10	BCS	17.88	0.83
19	23 <sup>h</sup> 10 <sup>m</sup> 39.596 <sup>s</sup>	-52°28'23.940''	23 <sup>h</sup> 10 <sup>m</sup> 39.750 <sup>s</sup>	-52°28'24.884''	—	—	—	—	—	33.71	0.61
20	23 <sup>h</sup> 40 <sup>m</sup> 51.430 <sup>s</sup>	-52°52'26.480''	23 <sup>h</sup> 40 <sup>m</sup> 51.313 <sup>s</sup>	-52°52'26.497''	23 <sup>h</sup> 40 <sup>m</sup> 51.247 <sup>s</sup>	-52°52'26.040''	0.70	0.04	BCS	12.74	0.95
21*	23 <sup>h</sup> 00 <sup>m</sup> 56.951 <sup>s</sup>	-52°53'58.960''	23 <sup>h</sup> 00 <sup>m</sup> 56.971 <sup>s</sup>	-52°53'58.621''	—	—	—	—	—	121.80	1.73
22	23 <sup>h</sup> 42 <sup>m</sup> 43.804 <sup>s</sup>	-53°15'05.700''	23 <sup>h</sup> 42 <sup>m</sup> 44.818 <sup>s</sup>	-53°15'04.651''	—	—	—	—	—	31.39	1.04
23	23 <sup>h</sup> 19 <sup>m</sup> 15.329 <sup>s</sup>	-53°31'59.950''	23 <sup>h</sup> 19 <sup>m</sup> 15.730 <sup>s</sup>	-53°31'59.164''	23 <sup>h</sup> 19 <sup>m</sup> 15.768 <sup>s</sup>	-53°31'59.052''	0.09	0.04	BCS	267.82	2.20

Continued on next page

Table 4.1: (continued) Bent-tail source candidates identified in the ATLAS-SPT survey.

ID	RA	Dec	SSDF RA	SSDF Dec	Optical RA	Optical Dec	$z$	$z_\sigma$	$z_{\text{ref}}$	$S$	$S_\sigma$
(1)	J2000 (hms)	J2000 (dms)	J2000 (hms)	J2000 (dms)	J2000 (hms)	J2000 (dms)	(8)	(9)	(10)	(mJy)	(12)
24*	23 <sup>h</sup> 54 <sup>m</sup> 50.278 <sup>s</sup>	-53°25'59.620''	23 <sup>h</sup> 54 <sup>m</sup> 50.484 <sup>s</sup>	-53°26'00.042''	23 <sup>h</sup> 54 <sup>m</sup> 50.464 <sup>s</sup>	-53°25'59.740''	0.27	0.06	DES	27.26	0.64
25	23 <sup>h</sup> 01 <sup>m</sup> 44.262 <sup>s</sup>	-53°34'49.080''	23 <sup>h</sup> 01 <sup>m</sup> 44.217 <sup>s</sup>	-53°34'48.864''	—	—	—	—	—	80.98	0.78
26*	23 <sup>h</sup> 30 <sup>m</sup> 31.811 <sup>s</sup>	-54°31'29.240''	23 <sup>h</sup> 30 <sup>m</sup> 31.488 <sup>s</sup>	-54°31'28.621''	23 <sup>h</sup> 30 <sup>m</sup> 31.460 <sup>s</sup>	-54°31'28.888''	0.68	0.09	DES	20.42	0.87
27*	23 <sup>h</sup> 43 <sup>m</sup> 55.254 <sup>s</sup>	-54°50'51.280''	23 <sup>h</sup> 43 <sup>m</sup> 55.261 <sup>s</sup>	-54°50'56.782''	23 <sup>h</sup> 43 <sup>m</sup> 55.253 <sup>s</sup>	-54°50'56.760''	0.85	0.07	BCS	16.22	0.57
28*	23 <sup>h</sup> 08 <sup>m</sup> 20.286 <sup>s</sup>	-54°56'18.890''	23 <sup>h</sup> 08 <sup>m</sup> 20.266 <sup>s</sup>	-54°56'19.572''	23 <sup>h</sup> 08 <sup>m</sup> 20.232 <sup>s</sup>	-54°56'18.481''	0.66	0.07	DES	32.36	0.56
29	23 <sup>h</sup> 21 <sup>m</sup> 44.947 <sup>s</sup>	-55°19'21.050''	23 <sup>h</sup> 21 <sup>m</sup> 44.959 <sup>s</sup>	-55°19'20.737''	23 <sup>h</sup> 21 <sup>m</sup> 44.978 <sup>s</sup>	-55°19'20.388''	2.22	0.40	BCS	9.89	0.64
30*	23 <sup>h</sup> 10 <sup>m</sup> 49.345 <sup>s</sup>	-55°27'24.840''	23 <sup>h</sup> 10 <sup>m</sup> 49.553 <sup>s</sup>	-55°27'25.290''	—	—	—	—	—	23.28	0.84
31	23 <sup>h</sup> 51 <sup>m</sup> 00.615 <sup>s</sup>	-55°22'14.580''	23 <sup>h</sup> 51 <sup>m</sup> 00.568 <sup>s</sup>	-55°22'13.372''	23 <sup>h</sup> 51 <sup>m</sup> 00.557 <sup>s</sup>	-55°22'13.116''	0.13	0.04	BCS	29.68	0.41
32*	23 <sup>h</sup> 34 <sup>m</sup> 25.694 <sup>s</sup>	-55°40'40.260''	23 <sup>h</sup> 34 <sup>m</sup> 25.640 <sup>s</sup>	-55°40'39.907''	—	—	—	—	—	14.88	0.85
33*	23 <sup>h</sup> 00 <sup>m</sup> 05.099 <sup>s</sup>	-55°25'42.620''	23 <sup>h</sup> 00 <sup>m</sup> 04.836 <sup>s</sup>	-55°25'36.512''	23 <sup>h</sup> 00 <sup>m</sup> 04.831 <sup>s</sup>	-55°25'36.415''	0.29	0.06	DES	13.58	0.71
34	23 <sup>h</sup> 19 <sup>m</sup> 06.371 <sup>s</sup>	-55°58'55.190''	23 <sup>h</sup> 19 <sup>m</sup> 07.033 <sup>s</sup>	-55°58'56.791''	23 <sup>h</sup> 19 <sup>m</sup> 07.032 <sup>s</sup>	-55°58'56.784''	0.63	0.04	BCS	18.24	0.85
35*	23 <sup>h</sup> 05 <sup>m</sup> 10.434 <sup>s</sup>	-55°40'47.360''	23 <sup>h</sup> 05 <sup>m</sup> 10.370 <sup>s</sup>	-55°40'46.862''	23 <sup>h</sup> 05 <sup>m</sup> 10.366 <sup>s</sup>	-55°40'47.039''	0.71	0.09	DES	22.23	0.48
36	23 <sup>h</sup> 55 <sup>m</sup> 43.134 <sup>s</sup>	-56°22'21.680''	23 <sup>h</sup> 55 <sup>m</sup> 43.238 <sup>s</sup>	-56°22'21.731''	—	—	—	—	—	5.34	0.47
37	23 <sup>h</sup> 37 <sup>m</sup> 47.591 <sup>s</sup>	-56°33'17.840''	23 <sup>h</sup> 37 <sup>m</sup> 47.680 <sup>s</sup>	-56°33'18.425''	23 <sup>h</sup> 37 <sup>m</sup> 47.666 <sup>s</sup>	-56°33'18.360''	0.35	0.04	BCS	18.36	0.70
38*	23 <sup>h</sup> 01 <sup>m</sup> 49.503 <sup>s</sup>	-57°11'16.870''	23 <sup>h</sup> 01 <sup>m</sup> 49.421 <sup>s</sup>	-57°11'16.048''	—	—	—	—	—	26.76	0.52
39	23 <sup>h</sup> 45 <sup>m</sup> 33.433 <sup>s</sup>	-57°40'13.130''	23 <sup>h</sup> 45 <sup>m</sup> 33.467 <sup>s</sup>	-57°40'12.097''	23 <sup>h</sup> 45 <sup>m</sup> 33.426 <sup>s</sup>	-57°40'12.410''	0.34	0.05	DES	10.61	0.33
40*	23 <sup>h</sup> 42 <sup>m</sup> 20.193 <sup>s</sup>	-57°28'02.140''	23 <sup>h</sup> 42 <sup>m</sup> 20.520 <sup>s</sup>	-57°28'01.391''	23 <sup>h</sup> 42 <sup>m</sup> 20.479 <sup>s</sup>	-57°28'01.632''	0.75	0.87	BCS	42.69	0.96
41	23 <sup>h</sup> 50 <sup>m</sup> 10.364 <sup>s</sup>	-58°02'51.320''	23 <sup>h</sup> 50 <sup>m</sup> 10.199 <sup>s</sup>	-58°02'49.621''	—	—	—	—	—	87.16	0.82
42*	23 <sup>h</sup> 43 <sup>m</sup> 32.415 <sup>s</sup>	-58°23'30.350''	23 <sup>h</sup> 43 <sup>m</sup> 33.704 <sup>s</sup>	-58°23'25.512''	—	—	—	—	—	300.97	2.62
43	23 <sup>h</sup> 51 <sup>m</sup> 33.657 <sup>s</sup>	-59°05'17.320''	23 <sup>h</sup> 51 <sup>m</sup> 33.654 <sup>s</sup>	-59°05'15.259''	—	—	—	—	—	10.43	0.52
44*	23 <sup>h</sup> 22 <sup>m</sup> 21.679 <sup>s</sup>	-59°24'07.290''	23 <sup>h</sup> 22 <sup>m</sup> 21.118 <sup>s</sup>	-59°24'07.970''	—	—	—	—	—	79.77	0.95
45*	23 <sup>h</sup> 09 <sup>m</sup> 53.839 <sup>s</sup>	-59°42'34.690''	23 <sup>h</sup> 09 <sup>m</sup> 53.865 <sup>s</sup>	-59°42'34.718''	—	—	—	—	—	42.57	0.43
46*	23 <sup>h</sup> 00 <sup>m</sup> 01.126 <sup>s</sup>	-56°17'04.776''	23 <sup>h</sup> 00 <sup>m</sup> 01.072 <sup>s</sup>	-56°17'05.845''	23 <sup>h</sup> 00 <sup>m</sup> 01.103 <sup>s</sup>	-56°17'05.640''	0.14	0.08	DES	22.07	0.78

### 4.2.6 Matching Bent-tail Sample with Known Clusters

We matched our BT source sample with cluster catalogues that cover the ATLAS-SPT field from the literature. These clusters have been detected using various methods including optical, IR, X-ray and SZ observations. The cluster catalogues used are listed in Table 4.2. First, we performed an on-sky match between our BT sample of 46 AGN and each of the 546 clusters or groups with redshifts from the cluster catalogues. We recorded 56 matches: 26 BT sources within  $20'$  of 52 known clusters. The  $20'$  search radius represents a proper separation of 2 Mpc for the lowest redshift in our BT sample ( $z = 0.09$ ).

We then refined the matches using only the 16 BT sources with redshifts, retaining only the clusters that are within 2 Mpc of the BT sources within the photometric redshift error. All BTs and clusters used for matching are shown in Figure 4.4.

We find matches for 4 BT sources to 6 known clusters using this technique which are shown in Table 4.3. Three of these clusters come from X-ray cluster catalogues, two of which provide  $M_{500}$  mass estimates while the other provides a  $M_{200}$  mass estimate. Two of the clusters are from SZ effect detections (Planck and SPTSZ) which also provide  $M_{500}$  mass estimates. The remaining cluster is from the BCS cluster catalogue which provide optical richness measurements. All cluster matches with mass measurements are of relatively low mass with the most massive being  $M_{500} = 3.75 \times 10^{14} M_{\odot}$ .

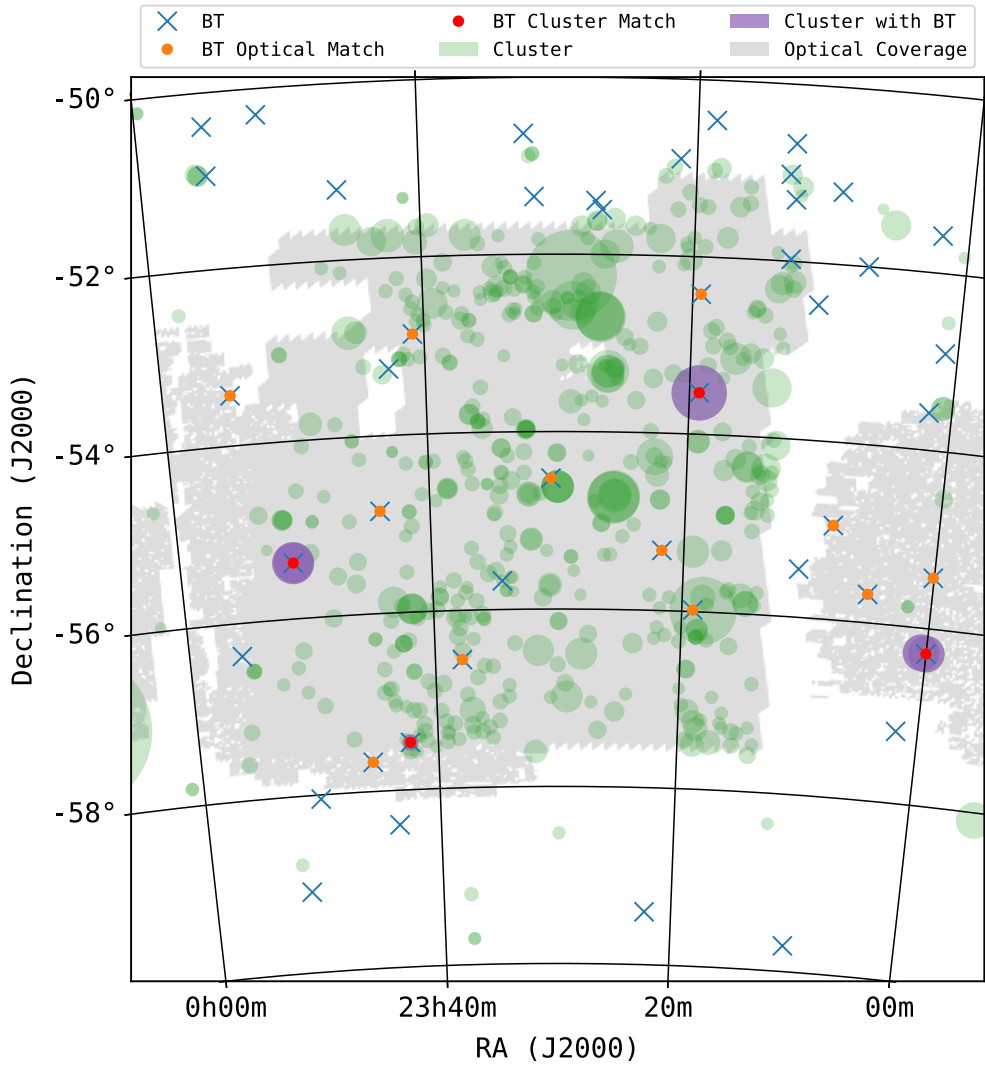


Figure 4.4: Sky plot of all bent-tail sources (blue crosses) and clusters (green circles) used in this study. Bent-tails with an optical counterpart are additionally marked with an orange dot, except for those that are also matched with a cluster which are marked in red. Clusters that were matched with a bent-tail are shown as purple circles. Both the green and purple cluster markers are drawn with a 2 Mpc radius. The union of the BCS and DES optical coverage from which photometric redshifts were used is shown as grey. There are 6 clusters matched to 4 bent-tails. Note that the cluster match for BT 40 is at  $z = 0.49$  and thus the cluster marker is too small to be visible on this plot. BTs 31 and 46 are each matched to two clusters from different catalogues whose positions and redshifts agree within their errors.

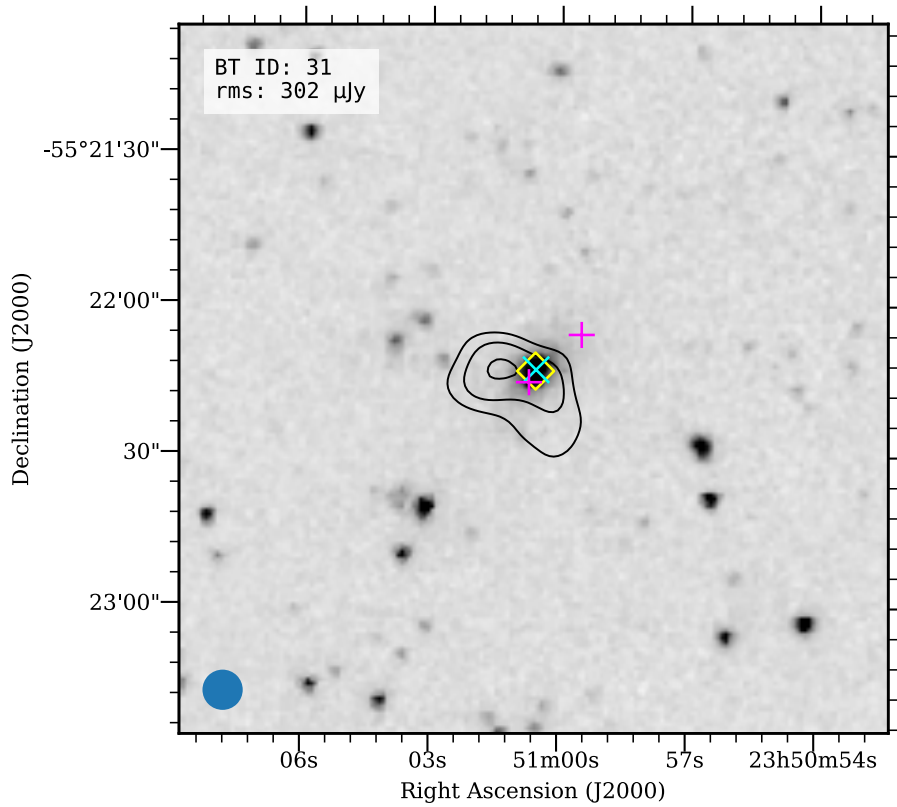
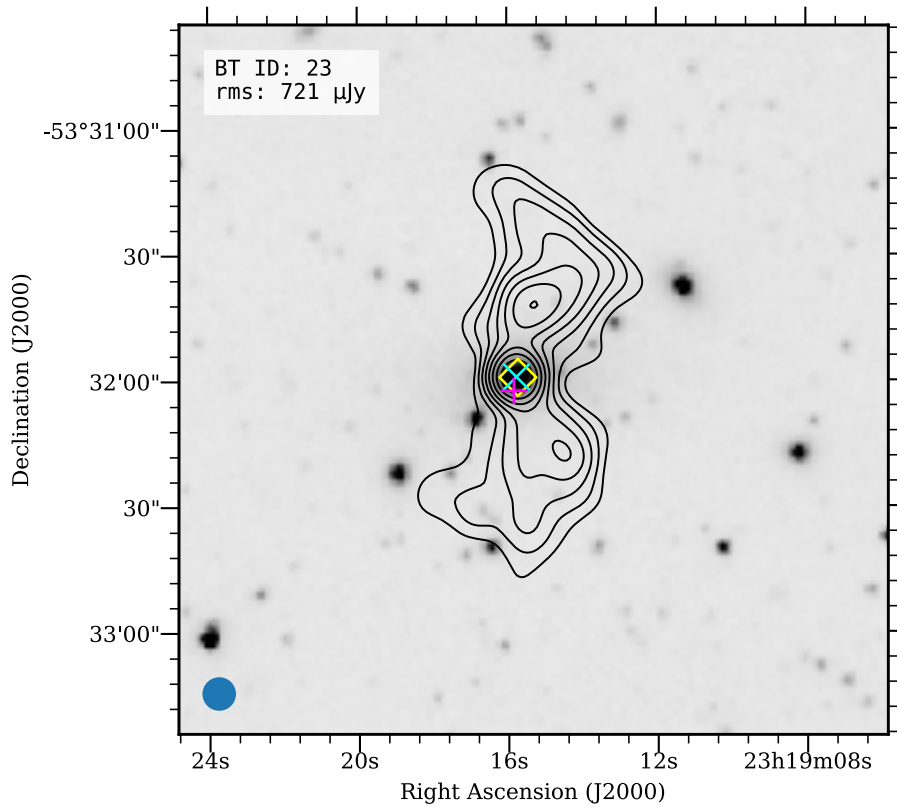


Figure 4.5: Bent-tail radio galaxies discovered in this study which reside in known clusters. Radio structure is shown in black contours overlaid on  $3.6\ \mu\text{m}$  images from the SSDF. Contours start at  $5\sigma$  and increase by factors of  $\sqrt{2}^n$  where  $n \in \mathbb{N}$ . SSDF sources identified as the likely host galaxy are marked with a yellow diamond. Optical cross-identifications are indicated with a cyan cross. Cluster centre positions are marked with a magenta plus.

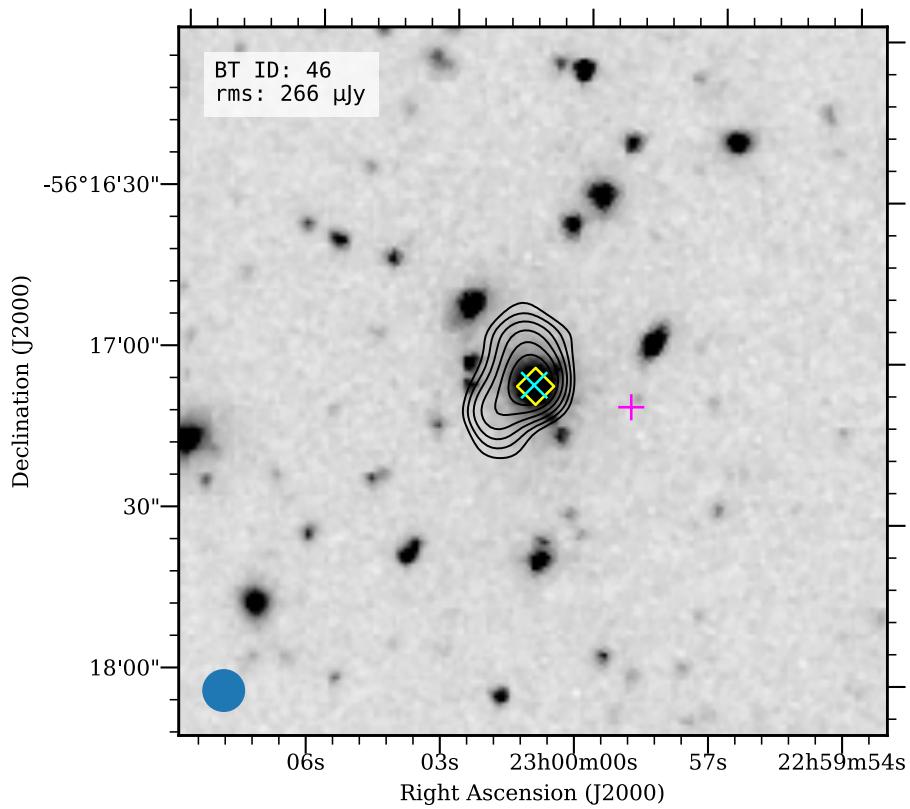
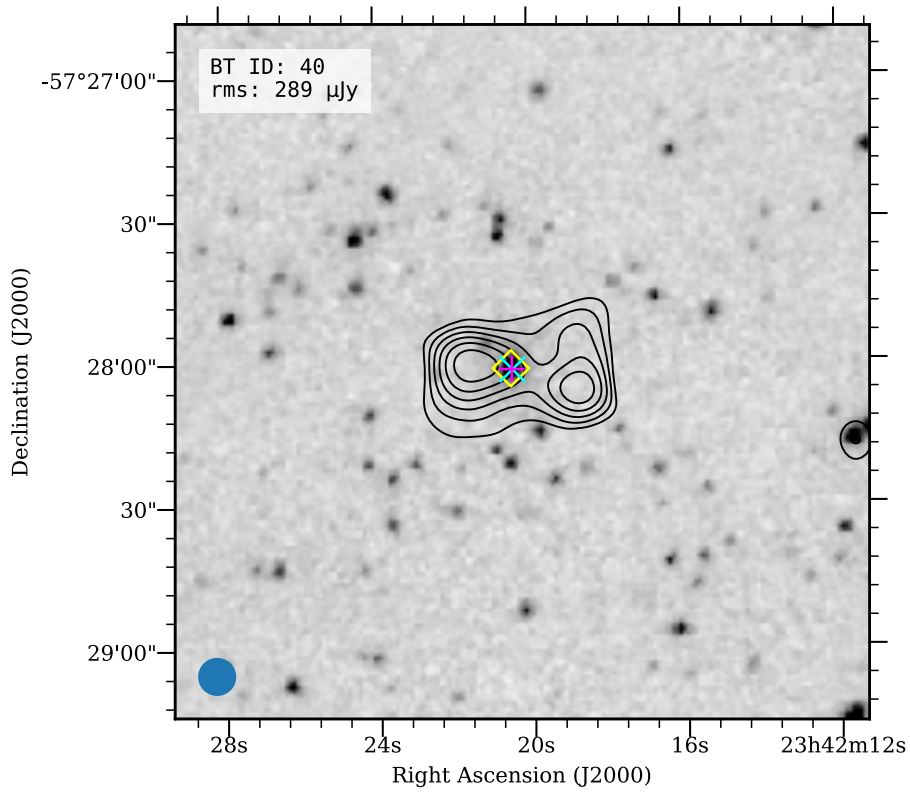


Figure 4.5: Continued. Bent-tail radio galaxies discovered in this study which reside in known clusters. Radio structure is shown in black contours overlaid on 3.6  $\mu$ m images from the SSDF. Contours start at  $5\sigma$  and increase by factors of  $\sqrt{2}^n$  where  $n \in \mathbb{N}$ . SSDF sources identified as the likely host galaxy are marked with a yellow diamond. Optical cross-identifications are indicated with a cyan cross. Cluster centre positions are marked with a magenta plus.

Table 4.2: Cluster catalogues used in this study. The short name is used throughout this paper to refer to the catalogues listed.  $N$  is the number of clusters within the ATLAS-SPT field and  $N_z$  is the number of those clusters with redshifts.

Short Name	Title	Band	$N$	$N_z$	Reference
XXL GC	The XXL Survey. II. The bright cluster sample: catalogue and luminosity function	X-ray	52	52	Fotopoulou et al. (2016)
MCXC	The MCXC: a meta-catalogue of x-ray detected clusters of galaxies	X-ray	3	3	Piffaretti et al. (2011)
Planck	Planck 2015 results. XXVII. The second Planck catalogue of Sunyaev-Zeldovich sources	SZ	5	4	Planck Collaboration et al. (2015)
SPT NIR	Redshifts, Sample Purity, and BCG Positions for the Galaxy Cluster Catalog from the First 720 Square Degrees of the South Pole Telescope Survey	IR	18	10	Song et al. (2012)
DES X	Galaxies in X-Ray Selected Clusters and Groups in Dark Energy Survey Data. I. Stellar Mass Growth of Bright Central Galaxies since $z$ 1.2	X-ray	28	28	Zhang et al. (2016)
SCS	Southern Cosmology Survey. II. Massive Optically Selected Clusters from 70 Square Degrees of the Sunyaev-Zel'dovich Effect Common Survey Area	Optical	44	44	Menanteau et al. (2010)
BCS	A New Reduction of the Blanco Cosmology Survey: An Optically Selected Galaxy Cluster Catalog and a Public Release of Optical Data Products	Optical	349	349	Bleem et al. (2015a)
SPTSZ	Galaxy Clusters Discovered via the Sunyaev-Zel'dovich Effect in the 2500-Square-Degree SPT-SZ Survey	SZ	27	26	Bleem et al. (2015b)
XMM	The cosmological analysis of X-ray cluster surveys - II. Application of the CR-HR method to the XMM archive	X-ray	12	2	Clerc et al. (2012)
Abell	A Catalog of Rich Clusters of Galaxies	Optical	15	0	Abell et al. (1989)
2MASS	Groups of Galaxies in the Two Micron All Sky Redshift Survey	Optical, IR	1	1	Crook et al. (2008)
FoF	Friends-of-friends galaxy group finder with membership refinement. Application to the local Universe	Optical	4	4	Tempel et al. (2016)
Local Groups	The matter distribution in the local Universe as derived from galaxy groups in SDSS DR12 and 2MRS	Optical, IR	23	23	Saulder et al. (2016)
Total			581	546	

Table 4.3: Bent-tail source candidates matched with galaxy clusters. The catalogue reporting the cluster and the cluster identifier are given in columns 2 and 3, respectively. The redshift of the matched cluster is given in column 4 and the mass measured within an aperture enclosing a region 500 times the critical density of the Universe (i.e.  $M_{500}$ ) is given in column 5. Masses marked with an asterisk (\*) are  $M_{200}$  measurements which by definition must be greater than  $M_{500}$ . The distance between the BT and the cluster centre is given in column 6.

ID	Cluster Cat. See Table 4.2	Cluster ID	$z_{cl}$	$M_{500,cl}$ ( $\times 10^{14} M_{\odot}$ )	$D_{BT,cl}$ (kpc)
(1)	(2)	(3)	(4)	(5)	(6)
23	XXL GC	XLSSC 544	0.095	1.52	7.280
31	XXL GC	XLSSC 511	0.130	0.52	8.517
"	DES X	XMMXCS J235059.5-552206.1	0.140	<1.58*	37.017
40	BCS	LCS-CL J234220-5728.0	0.490	—	2.087
46	Planck	PSZ2 G329.53-54.73	0.153	3.21	712.796
"	SPTSZ	SPT-CL J2259-5617	0.153	3.75	66.211

We find that the majority (12 of 16) of our BT sample have no association with known clusters or groups. Those 4 that are associated with known clusters are found in relatively low-mass clusters (on the order of  $10^{14} M_{\odot}$ ). We also find that most known high-mass clusters ( $> 10^{15} M_{\odot}$ ) do not appear to contain a bent-tailed radio galaxy.

We also find that the distances between the BTs found in known clusters and the centre of their cluster hosts are small with most being tens of kpc with the exception of BT 46 which is approximately 0.7 Mpc from its host cluster centre. However, this particular cluster match is from the Planck catalogue which has large positional errors because of the large beam size. A more accurate cluster position is provided in the SPTSZ catalogue which when used to calculate the distance between the cluster and BT gives approximately 66 kpc.

#### 4.2.7 Final BT Classification

We examined each of our 46 candidates to identify those which are unambiguous BT sources, including using data from the ATCA-XXL survey (Butler et al., 2017), using the following criteria:

1. The radio morphology is unambiguously a bent-tail or a head-tail galaxy, and cannot easily be explained as a superposition of confusing sources.
2. There is a clear infrared counterpart for the radio core and no other probable cross-identifications are obvious.

Using these criteria, 22 candidates were thus identified as unambiguous BT sources, of which 8 have redshifts. Only one of these is associated with a known cluster. We include the remaining 24 sources as BT candidates requiring follow-up observation to confirm their classification. The whole sample is listed in Table 4.1, with candidate BTs indicated with an asterisk. A brief



justification of each source is given below in Section 4.2.8.

#### 4.2.8 Notes on Individual Sources

BT 1 displays the typical brightness asymmetry of a head-tail galaxy, with the most likely morphology being both radio jets originating from the radio peak and being severely bent toward the south. The closest SSDF source to the radio peak is located  $4.4''$  to the SE. Follow up observation at higher resolution to resolve the individual jets would confirm our suggested head-tail candidate classification.

BT 2 also displays morphology typical of a head-tail with a wider jet opening angle. The nearest SSDF source to the radio peak is  $3.1''$  to the SW. We note there is an unrelated radio source to the west with a clear separate SSDF counterpart. We therefore classify this object as a head-tail.

BT 3 is a clear BT radio source with a wide jet angle. The selected SSDF counterpart is directly aligned with the radio core. We note that the jet to the SW of the core also contains an SSDF source and may contain unrelated, superimposed radio emission, but we do not believe that all of this radio emission to be unrelated. If it were, the source would be a simple radio-double with a core located between the other two radio peaks and there is no evidence of an SSDF counterpart in this region. We also note an SSDF source near the NW radio peak, offset by  $4.1''$  which may also contribute superimposed radio emission. We suggest this is also unlikely to be dominant because of the positional offset and the sub-arcsecond positional accuracy of the radio data (see Section 3.2.1.2.) We therefore classify this object as a bent-tail.

BT 4 is also a clear wide-angle BT radio source. The SSDF counterpart is aligned with the radio core with no other obvious alternative.

BT 5 is an unambiguous wide-angle BT radio source, for the same reasons as BT 4.

BT 6 is a radio double where the core is undetected. The selected SSDF counterpart is the only clear choice with a trail of radio emission directed toward the counterpart from both lobes. The lobes are mostly aligned, but we note a misalignment in the emission from the eastern lobe which extends toward the north of the core which is possibly caused by ICM movement. Follow up observations at lower frequency may detect more of the lobe emission to help confirm the classification of this BT candidate.

BT 7 is a large, complex radio source with several possible SSDF counterparts. The component to the SE is likely an unrelated source as it is mostly compact and aligned with an SSDF source. We therefore consider the remaining two components form a bent-tail candidate with a wide opening angle and a possible SSDF counterpart between the two radio peaks.

BT 8 is a very complex radio source containing three distinct emission peaks (we note two

unrelated radio sources: one to the far west and another to the SW). It is unclear which of the three peaks is the core. We selected the SSDF source nearest to the northern radio peak, but an alternative cross-identification exists within the western-most peak. In either case, an incorrect SSDF cross-identification does not affect our cluster cross-matching in Section 4.2.6 as we only consider sources with photometric redshifts, and this source is outside the boundary of available optical data. Follow up observations at higher resolution would help to more accurately determine the location of the radio core for this candidate.

BT 9 is an unambiguous wide-angle BT radio source, for the same reasons as BT 4.

BT 10 is a candidate bent-tail aligned well with an SSDF counterpart. The source is mostly straight with indications of slight bending toward the west for both jets. Low frequency follow up observations may detect more of the lobe emission to confirm the classification.

BT 11 is an atypical bent-tail candidate which shows signs of an abrupt kink in the northern jet. There are several possible SSDF counterparts; we selected the one most central to the radio source. However, it is possible that the host galaxy is one of the SSDF sources at the northern- or southern-most end of the radio emission which would make this source a head-tail. It is also possible that there is superimposed radio emission from other sources making this source appear as an apparent bent-tail. High resolution follow up is required to resolve the jets to accurately classify this source.

BT 12 is an unambiguous wide-angle BT radio source, for the same reasons as BT 4.

BT 13 is another clear bent-tail source. While the radio core is not clearly detected, resolved emission from the western lobe appears to connect the position of an SSDF source which we select as the host galaxy.

BT 14 is a candidate bent-tail with a wide opening angle. The selected SSDF counterpart is offset from the radio peak by  $4.8''$ . As the cross-identification is not well aligned with the radio core, we list this source as a candidate BT pending follow up observations at higher resolution.

BT 15 is also a candidate bent-tail with a wide opening angle, but the radio core is not easily identified. There are several possible SSDF cross-identifications. Follow up observations at high resolution is required to confirm the classification of this source.

BT 16 is another clear bent-tail with interesting complex morphology. There are several possible SSDF counterparts of which we select the most central one. Higher resolution observations are required to clearly identify the radio core and therefore the true SSDF counterpart. We note that there may be a superimposed radio sources given the large number of SSDF sources within the radio emission contours. However, given the complex morphology of the radio emission, any of the possible counterparts result in this object being identified as a bent-tail, or head-tail.

BT 17 is a bent-tail candidate with a wide opening angle and three distinct radio peaks.

The central component contains a possible SSDF counterpart offset from the peak by  $8.7''$ . The southern component is isolated from the other two, but the lack of an aligned SSDF source indicates that it may not be an unrelated source. We note that the faint radio emission around this source is most likely artefacts from incomplete deconvolution as they match the shape of the dirty beam. Due to the unclear SSDF counterpart, we cannot be certain with the classification of this source as a bent-tail and therefore include it as a candidate for follow up observation at high resolution.

BT 18 is an unambiguous wide-angle BT radio source, for the same reasons as BT 4.

BT 19: see BT 4, but note the complex, extended structure and crowded SSDF field, increasing the possibility of superimposed emission.

BT 20 is a clear bent-tail source, but there are two clear possible SSDF counterparts: the selected SSDF source, and another the north of the selected source. In either case, the radio morphology clearly depicts jet bending, therefore we classify this source as a bent-tail.

BT 21 is a candidate head-tail galaxy. There are two adjacent possible SSDF counterparts; we select the one that aligns directly with the radio peak. Higher resolution follow up observations to resolve the individual jets is required to confirm this classification.

BT 22 is a bent-tail source with a wide opening angle and a clear SSDF counterpart located at the radio peak. We note the interesting curvature of the western jet, possibly indicating strong cluster winds. There is some low-level radio emission to the south of the western jet which we believe to be an image artefact upon closer inspection of the radio image.

BT 23 is an extremely complex radio source exhibiting signs of a residing in a turbulent environment. While the average direction of the jets appears straight, the higher-resolution data from the ATCA-XXL survey reveal dramatic kinks in both jets. We therefore classify this source as a bent-tail.

BT 24 is a candidate bent-tail with a faint radio core aligned with an SSDF counterpart. The NE lobe shows signs of bending toward the NW, but the presence of another SSDF source suggests this may be another superimposed radio source. Higher resolution observations are required to disentangle these sources to confirm the classification.

BT 25 is a head-tail source with a clear SSDF counterpart aligned with the radio peak. We therefore classify this object as a head-tail.

BT 26 is a radio double source with significant bending in the SE lobe. The radio core is not detected and there are no clear SSDF counterparts visible within the radio contours. We therefore classify this source as a bent-tail candidate. Follow up high resolution observations at low frequency may resolve more of the lobes to confirm this classification.

BT 27 is a complex radio source showing signs of jet bending. Like BT 23, the average jet

direction appears straight, but the high resolution ATCA-XXL data shows a wide-angle kink in the southern jet. We note that the ATCA-XXL data, and the presence of an aligned SSDF source, appears to suggest that the emission to the SE is an unrelated point source.

BT 28 appears to be a head-tail candidate. There appears to be only one clear SSDF counterpart which is located in the northern side of the radio emission. However, a nearby saturating source in the SSDF image lowers the sensitivity in this area making it difficult to identify alternate cross-identifications. The selected counterpart fits our classification of a head-tail candidate, but higher resolution follow up is required to confirm.

BT 29 is a clear bent-tail with a very wide opening angle. The lack of alternate SSDF counterparts suggests that there are no superimposed sources.

BT 30 appears to be a clear bent-tail but the eastern lobe sits just above the radio sensitivity limit. More sensitive follow up observations to detect more of the extended structure of this source are required to confirm this classification.

BT 31 is an asymmetrical radio source with a clear SSDF counterpart, suggestive of a bent-tail with a wide opening angle. The higher resolution ATCA-XXL image resolves the jets and depicts the bending more clearly. We therefore classify this source as a bent-tail.

BT 32 appears to be three-component bent-tail with an SSDF counterpart aligned with the central component. However, the presence of an SSDF source in the western lobe casts doubt on whether this component is part of the same radio source. High resolution follow up at low frequency could resolve more of the lobes and provide stronger evidence that the three components form a single bent-tail. We therefore classify this source as a bent-tail candidate.

BT 33 is an asymmetrical radio source with two possible SSDF cross-identifications. We have selected the source nearest to the radio peak with a separation of  $6.5''$ . If this is a true cross-identification, the source is likely a head-tail with the host galaxy on the NW edge of the radio emission, with the jets severely bent toward the SE and curving toward the NE.

BT 34 is a clear bent-tail with a wide opening angle. There is a clear radio core aligned with an SSDF source with no other viable SSDF cross-identification present within the radio contours. The higher resolution ATCA-XXL data reveals some interesting structure in the SE lobe as it appears to bend back in the same direction as the opposite lobe. This suggests that relative ICM movement may be pushing these lobes to the west. We therefore classify this source as a bent-tail.

BT 35 is an extended, single component radio source with two distinct peaks. There are two possible classifications for this source: it may be a head-tail with both jets being severely bent toward the north; or it may be a bent-tail with a wide opening angle, with one jet descending to the SW and the other extending to the NE and bending toward the north. Both classifications

may be justified with a SSDF counterpart. We select the most central SSDF source and mark this source as a bent-tail candidate requiring follow up observation to confirm.

BT 36 is a faint bent-tail with a wide opening angle. There is an SSDF counterpart aligned with the radio peak with no other obvious alternative cross-identification.

BT 37 is a complex but clear bent-tail with a wide opening angle. The western lobe appears more collimated and longer than its counterpart on the eastern side which appears more extended and frustrated. This may be explained by a relative ICM movement pushing the jets to the SW. There are two possible adjacent SSDF cross-identifications; we have selected the one aligned with the radio peak.

BT 38 displays an asymmetrical radio structure, suggestive of a head-tail. There is a clear SSDF counterpart aligned with the radio peak with a majority of the radio emission extending out to the south and bending toward the west. Close inspection of the faint emission to the NE and SW suggests it is a residual of incomplete deconvolution. Higher resolution follow up observations are required to confirm this classification.

BT 39 is a head-tail candidate with a clear SSDF counterpart within the radio peak. We suggest that both jets are tightly bent toward the SW before bending to the south. We therefore classify this object as a head-tail.

BT 40 is a mostly straight radio double with a clear SSDF counterpart located between the radio peaks. We classify this source as a bent-tail candidate as the western lobe shows signs of bending toward the north. High resolution follow up observation at lower frequency may resolve more of the lobe structure to confirm this classification.

BT 41 is a clear bent-tail with interesting structure. While no radio core is detected, a single SSDF source is located between the two radio components which we select as the probable host galaxy. The northern lobe shows signs of a bending trajectory originating from the core, extending to the NE and bending around toward the NW. Similarly, the southern lobe appears to originate from the core, extend to the south, and bend toward the SE. We suggest this structure is caused by complex environmental effects.

BT 42 appears to be a bent-tail with a clear SSDF counterpart between the two radio peaks. The SW lobe appears to bend toward the NW. However, the presence of an SSDF source within this lobe indicates this may be superimposed radio emission from a separate source. We therefore classify this source as a bent-tail candidate as higher resolution follow up observations are required to disentangle the radio emission.

BT 43 is a clear bent-tail source with a wide opening angle. An SSDF counterpart is aligned with the radio peak which we select as the probably host galaxy. There are other SSDF sources within the radio contours but they are offset from the jet emission. We therefore classify this

source as a bent-tail.

BT 44 is an asymmetrical radio source with an SSDF counterpart located  $4.3''$  from the radio peak. We suggest two possible classifications for this source: a head-tail where the jets are bent tightly back from the radio peak toward the SW before bending toward the west; or a bent-tail with a wide opening angle with one lobe extending to the NE and the other to the west. The offset SSDF counterpart from the radio peak casts some doubt on our head-tail classification, and the lack of a clear radio core detection makes us unable to confirm this source is a bent-tail. In either case, the radio morphology is most likely affected by environmental effects and thus we include this source as a bent-tail candidate.

BT 45 is an extended radio source with complex, asymmetrical structure. There appears to be no obvious SSDF counterparts within the radio peaks to the east and west, and thus we select the SSDF source near the centre as the putative host galaxy. The complex structure in this source and the crowded SSDF field makes it difficult to classify this source. We therefore include this source as a candidate for follow up observation.

BT 46 is an extended, single component radio source where the peak is offset toward the west. We suggest this is most likely a bent-tail with a wide opening angle, with jets bent toward the north-NE and SE. There is a clear SSDF counterpart aligned with the radio peak. Low frequency observations at high resolution may reveal more of the lobe structure for this source to confirm this classification.

### 4.3 Discussion

The number of BTs we have detected within clusters (4 of 16) is contrary to expectations, and specifically contrary to simulations by Mguda et al. (2015) which predict that clusters with masses in excess of  $10^{15}M_{\odot}$  should contain approximately 7 BT galaxies (subject to AGN duty-cycle and projection effects). The BT cluster-centric distances are in agreement with the simulations which predict that BT galaxies may be found up to  $\sim 400$  kpc from the centre of clusters with  $13.5 \leq \log M_{\odot} \leq 14.0$ .

We note here that the masses provided by Mguda et al. (2015) are dark matter halo mass as determined by the Friend-of-Friends (FoF) algorithm, a common method used in N-body simulations. These masses are not easily matched to observationally measured cluster masses, such as those given in the cluster catalogues which are determined by spherical overdensities or other methods which are then converted to equivalent spherical overdensities using mass scaling relations. Lukić et al. (2009) measured simulated cluster masses using both the FoF and spherical overdensity methods and found that they are strongly correlated but offset by

an average of  $M_{\text{FOF}}/M_{200} \simeq 1.5$ . This mass ratio is strongly dependant on the dark matter concentration which is unknown for the observationally measured masses. However, given the relatively low ratio between the two mass definitions, we do not consider this to have a significant impact on our result.

It is clear that our results do not agree with simulations predicting the number of BT sources within clusters. Two main questions arising from these results are:

1. Why don't we see BT sources in known clusters?
2. Why don't most BT sources reside in clusters?

We discuss possible explanations for these questions in the subsections below.

### 4.3.1 Missing Bent-tail Sources

BT sources are expected to reside in galaxy clusters. Our results suggest that the completeness of BT sources as a tracer of clusters may be very low. Below we discuss putative effects that may result in BT sources being excluded from our sample.

Projection effects significantly impact measurements such as jet opening angles (see Figure 15 in Pratley et al. (2013) for an excellent example) which have previously been used to classify BT AGN as either wide- or narrow-angle tailed (WAT and NAT respectively). We avoid use of the WAT/NAT nomenclature for this reason. Projection effects can also result in a BT source being misclassified as a normal straight AGN. As our sample of BT sources include any radio source that appears bent, we expect only a small fraction of BT jets appear straight due to their orientation on the sky. Only BTs which have jets aligned within a few degrees of the line-of-sight would appear straight and therefore be excluded from our sample. Therefore, we do not think this has a significant effect on our sample.

Resolution effects may also be a significant contributor to the apparent lack of BT sources in clusters. The Mguda et al. (2015) simulations look for BT sources with jet sizes greater than 50 kpc. The resolution of our BT sample is approximately  $8''$ , which is sufficient to detect 50 kpc jets up to  $z \sim 0.5$ . This jet size is a minimum limit so our data is sensitive to jet sizes larger than this over a wider range of redshifts. We noted in Section 4.2.5 that the redshift distribution of our BT sample is biased to lower redshifts compared to the optical catalogues. This could be due to the resolution of the radio data limiting the number of BT detections at higher redshifts. To estimate the resolution limit for detecting BT sources in the ATLAS-SPT maps, we measured the maximum sky extent for each BT. This was typically the sky angle from one radio lobe to the other, but this is strongly dependent on the source morphology. The distribution of the measured BT extents is shown in Figure 4.6. The smallest BT sky extent

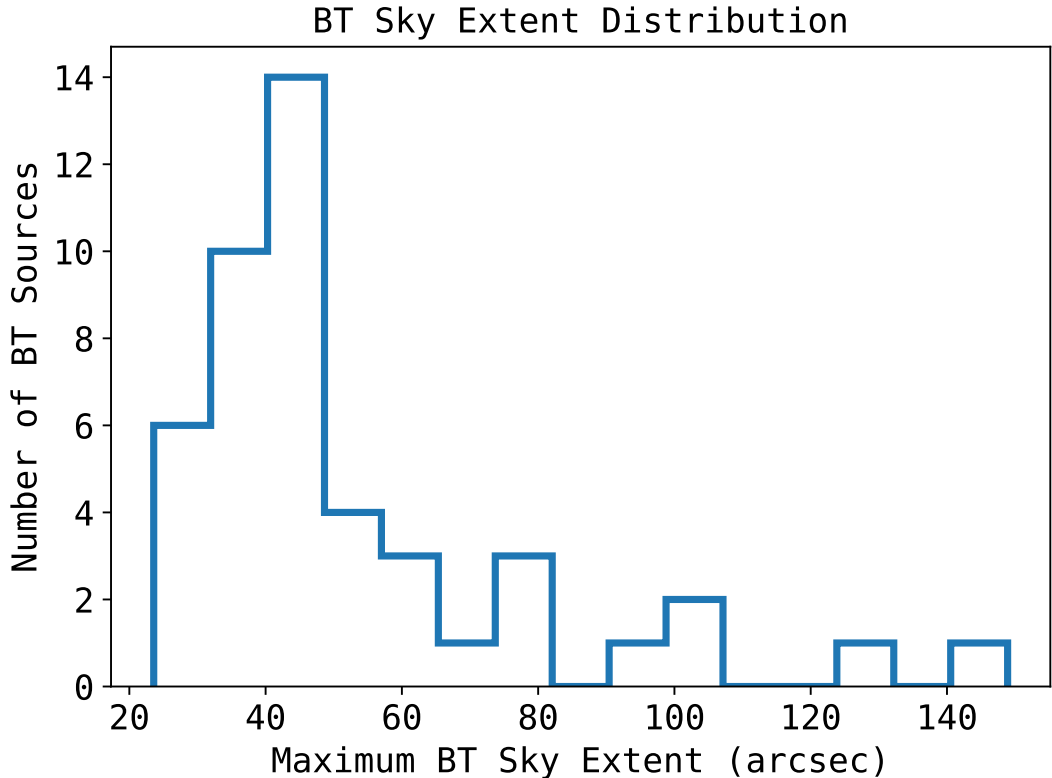


Figure 4.6: The maximum sky extent distribution for the bent-tail radio sources detected in the ATLAS-SPT survey.

measured in our catalogue is  $23.6''$ . We therefore conclude that our data is not sensitive to BTs smaller than this size.

The number of observed BT sources at a given time is heavily dependent on the duty cycle of the AGN producing the bent jets. Mguda et al. (2015) predict that clusters above  $10^{14.5} M_{\odot}$  will host at least one BT at some point in their lifetime. It is possible that many of the clusters in this study *will* host or *have* hosted a BT source at some point that is no longer visible in our dataset.

All of these effects (projection, resolution and duty cycle) are difficult to model. We cannot eliminate the possibility that clusters investigated in this study contain BT sources that are too faint or unresolved to be detected in our survey.

### 4.3.2 Missing Clusters

If BT radio galaxies are tracers of clusters, then one would expect to find most BT galaxies to be associated with clusters. Our results indicate this is not the case and we discuss putative explanations for this below.

A strong signal within the mm-wavelength bands observed by the South Pole Telescope can contaminate the SZ signal used to detect galaxy clusters leading to the possibility that the



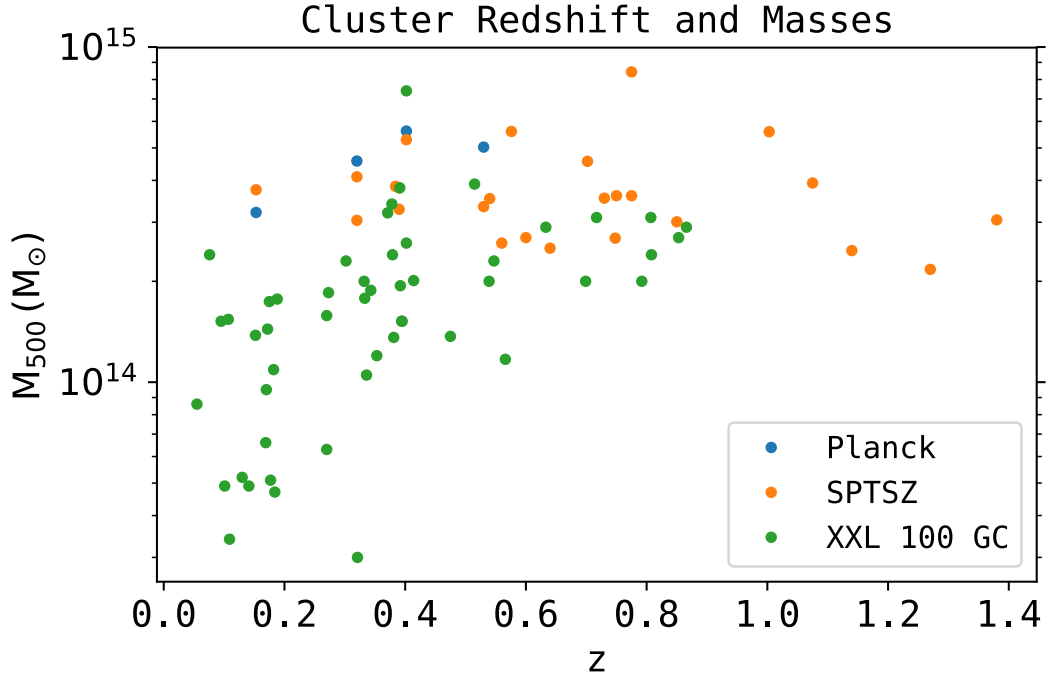


Figure 4.7: Comparison of redshifts and masses of clusters used in this study. Only the catalogues which provided  $M_{500}$  masses are shown.

SPTSZ cluster catalogue may not be able to detect clusters near strong radio sources. The SPTSZ cluster finder places a  $4'$  mask around point sources with  $S_{150\text{GHz}} > 5\sigma$ , discards any clusters found within  $8'$  around these masks and records them in a separate catalogue. We cross-matched the SPT point source catalogue (Mocanu et al., 2013) with our BT sample and find that only 3 of our 46 sources are potentially affected by masked point sources over the defined threshold. Therefore, we do not think this have a significant effect on our sample.

An alternative explanation is that with the exception of the SPTSZ cluster catalogue, all cluster catalogues used in this study are limited to low redshifts because of sensitivity. The Planck catalogue consists of clusters detected with the mostly redshift independent SZ effect, but the large beam dilutes the SZ signal which constrains cluster detections to low redshift. This means that the only available high-redshift cluster catalogue for this area is SPTSZ which itself is mass limited and expected to be nearly entirely complete for clusters with  $M_{500} > 7 \times 10^{14} h^{-1} M_{\odot}$  at  $z > 0.25$ . Therefore, the cluster catalogues used in this study lack low-mass high-redshift clusters which may host BTs. This lack of clusters is clearly seen in the redshift-mass distribution of the clusters used in this study which is shown in Figure 4.7.

Mguda et al. (2015, Figure 5) shows that  $\sim 40\%$  of BT galaxies are in clusters with  $M > 10^{14.5} h^{-1} M_{\odot}$ . Applying this fraction to our 16 BTs with redshifts, we expect that  $\sim 7$  BT galaxies will be associated with SPTSZ clusters. Instead we find only one (BT ID 46). We therefore conclude that BT galaxies are found in lower mass host clusters than predicted by

the Mguda et al. (2015) model.

It is also possible that we do not find many clusters around our BT objects because they have been misclassified. Our method for finding BTs as explained in Section 4.2.8 is subjective and some objects show only minor signs of jet bending or HT asymmetry. However, after repeated examination of the images, we are confident that the majority of our classifications are correct. In particular, a superposition of two or more unrelated sources would be betrayed by their infrared counterparts in the SSDF catalogue.

We further note that several putative BT objects identified by Dehghan et al. (2014) similarly showed only minor signs of jet bending, but when imaged using higher-resolution ( $2''$ ) data obtained with the Very Large Array (VLA), they were confirmed to be BTs. If some of our BTs were misclassified, this would reduce our BT sample size and therefore increase the fraction of BTs that we find associated with clusters. However the mismatch between the predicted number (7) and the actual number (1) of associations in SPTSZ is too large to be explained by some of our classifications being incorrect.

### 4.3.3 Comparison to Other Studies

Blanton et al. (2000) visually identified 384 BT objects from FIRST and followed up 130 of these objects with  $R$  band optical observations. Optical spectra were then obtained for 10 of these objects, selected because they contained obvious overdensities of faint galaxies in the optical images. Eight of those BT sources were associated with clusters and lie within the redshift range  $0.33 < z < 0.85$ . The authors could not rule out the possibility that the remaining 2 BT sources were not associated with clusters at higher redshift. While the BT objects were identified in a similar manner to this work (i.e. visually), the targeted followup optical observations and thus the cluster association makes it difficult to directly compare these results with this work.

Mao et al. (2009) identified 5 head-tail objects in the central region of the Horologium-Reticulum Supercluster using 1.4 GHz radio data from ATLAS. All objects were found to reside in dense regions of a large cluster merger system at  $z \sim 0.06$ . Since this study specifically targeted a region of known clusters, we cannot directly compare this result with our work.

Mao et al. (2010) identified 6 wide-angle tail objects in ATLAS that are within the redshift range  $0.14 < z < 0.38$ . They find that 4 of these WATs are associated with regions where they find evidence of galaxy overdensities using photometric redshifts from *Spitzer* Wide-area InfraRed Extragalactic Survey (SWIRE) data or targeted spectroscopic redshifts. Due to the targeted nature of the followup observations, we again cannot directly compare this result with our own.

Wing and Blanton (2011) use the same 384 bent-tail objects visually identified by Blanton

et al. (2000) from FIRST (they also identified many more BTs with automated methods but we do not discuss those results here to remain consistent with our own identifications). After cross-matching each BT with SDSS and applying colour, redshift and apparent magnitude selections, they calculate the optical richness around the BT hosts to identify those with excess galaxy counts with respect to the background. They found that 78% of the visually identified BTs lie in regions where the excess optical galaxy count is  $\geq 20$ . They also performed this analysis on samples of straight and single-component radio sources, of which they find 52% and 35% lie in regions with excess optical galaxies, respectively. The most comparable cluster catalogue used in our work are those clusters identified by Bleem et al. (2015a), which uses optical data from BCS that is slightly deeper than SDSS. However, the optical richness metric used by Bleem et al. (2015a) is more robust and may exclude many groups compared to the relatively simple metric used by Wing and Blanton (2011). We therefore attribute the discrepancy between these results to the likelihood that the Wing and Blanton (2011) cluster identification is more sensitive to smaller clusters and groups and thus is more likely to attribute a source to an optical galaxy overdensity.

Dehghan et al. (2014) identified 45 bent-tail objects in the ATLAS *Chandra* Deep Field South (CDFSS) field, also by visual inspection. A robust cross-match against cluster catalogues is not described by Dehghan et al. (2014), but they do state that one of their BT objects is matched with an Abell cluster.

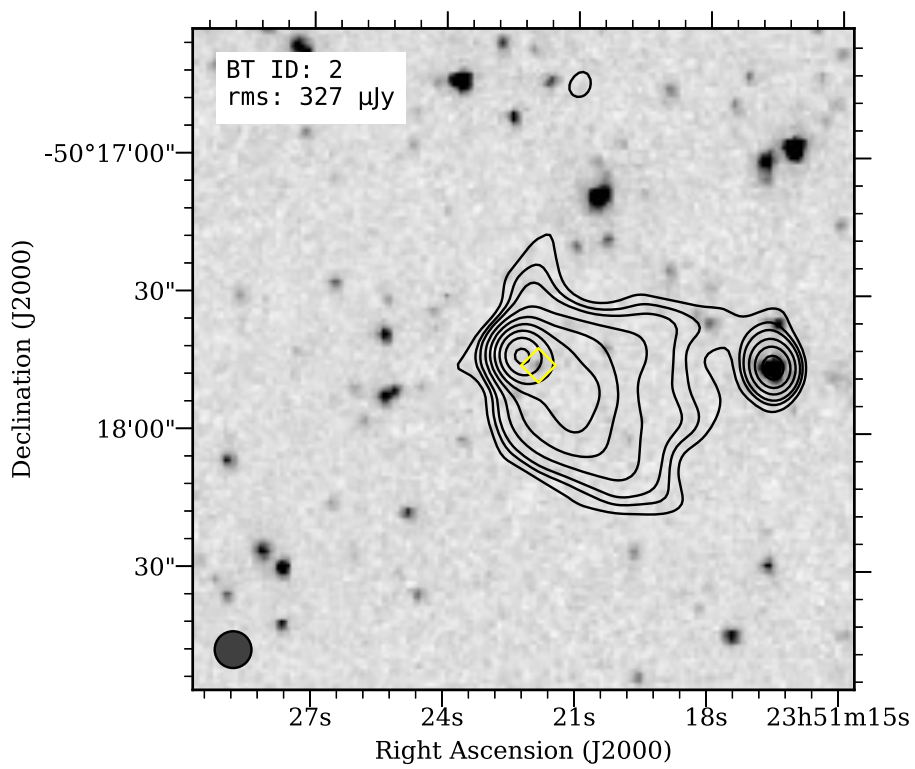
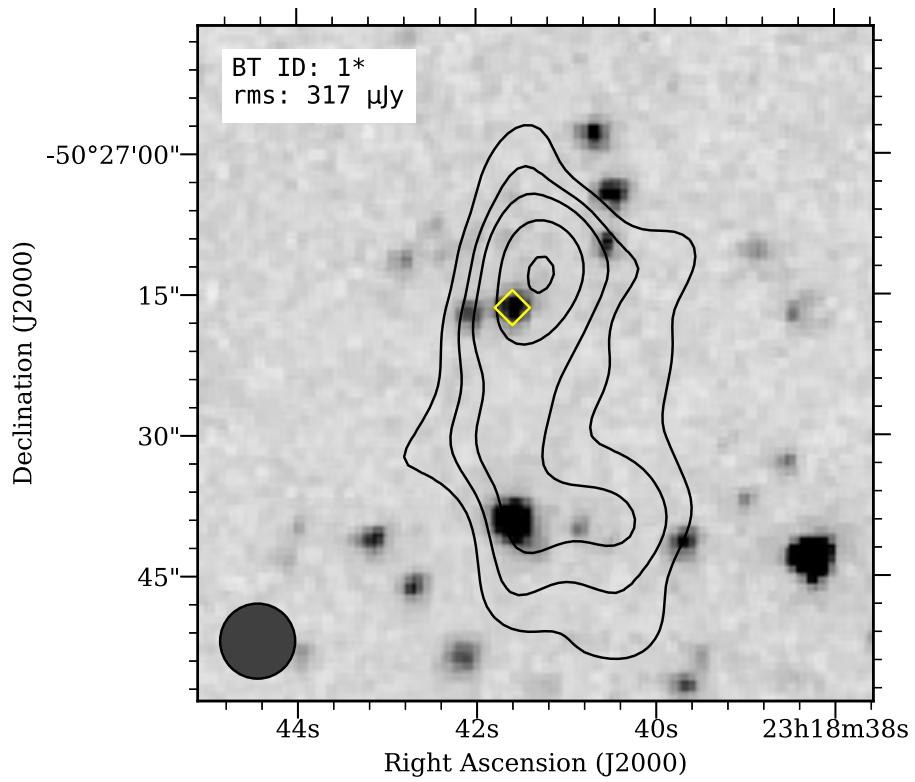
## 4.4 Conclusions

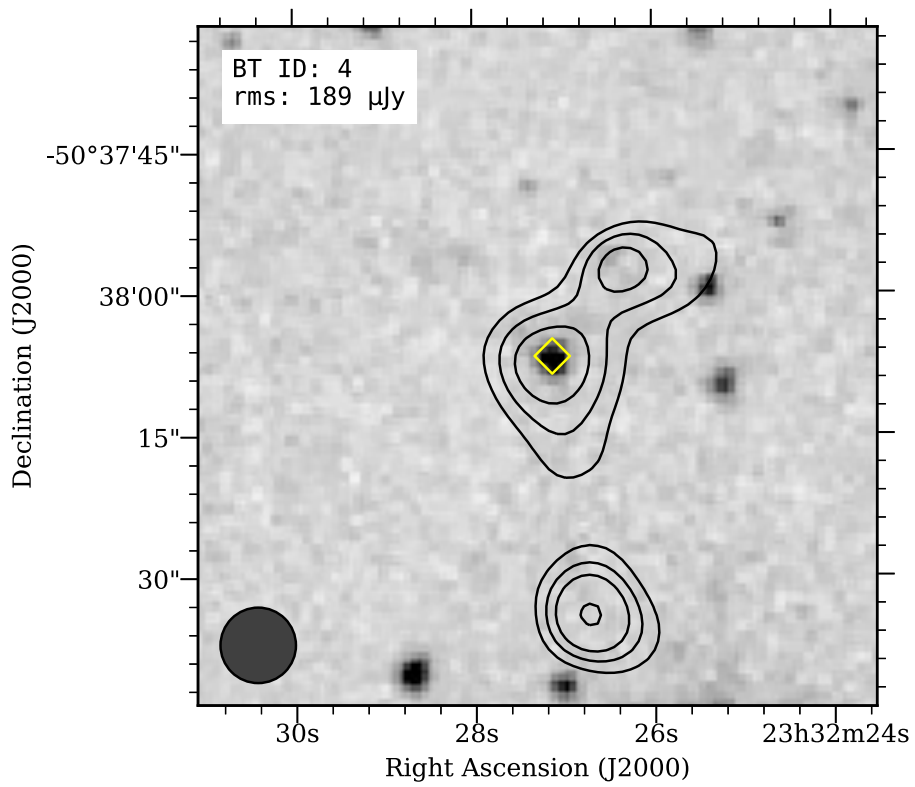
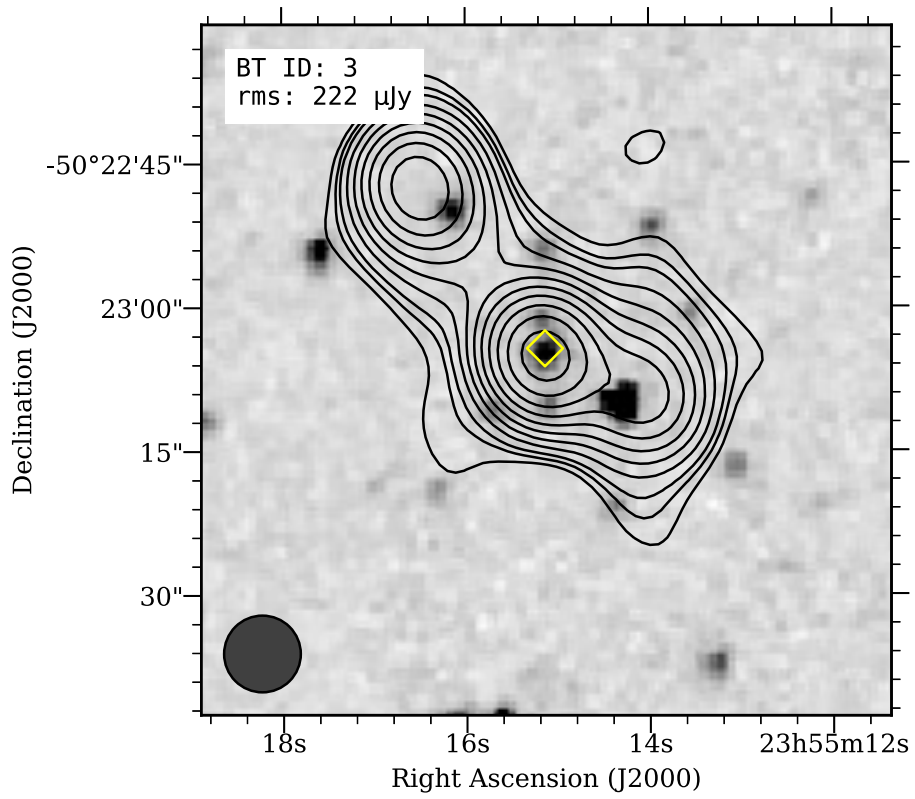
Bent-tail galaxies are expected to be associated with high-mass clusters. We present a new catalogue of 46 BT galaxies detected in the ATLAS-SPT field and compare the 16 BT galaxies with photometric redshifts with the 546 clusters detected using other techniques. We find that only 4 of our 16 BT galaxies are associated with known clusters. This raises two questions: (i) why don't we see BT sources in known clusters? (ii) why don't most BT sources reside in clusters? The first of these may be caused by selection effects which means our sample of BT galaxies may be incomplete. The second question is more problematic, and our data suggests that BT galaxies may be found in lower-mass clusters (or lower-density environments) than expected from models.

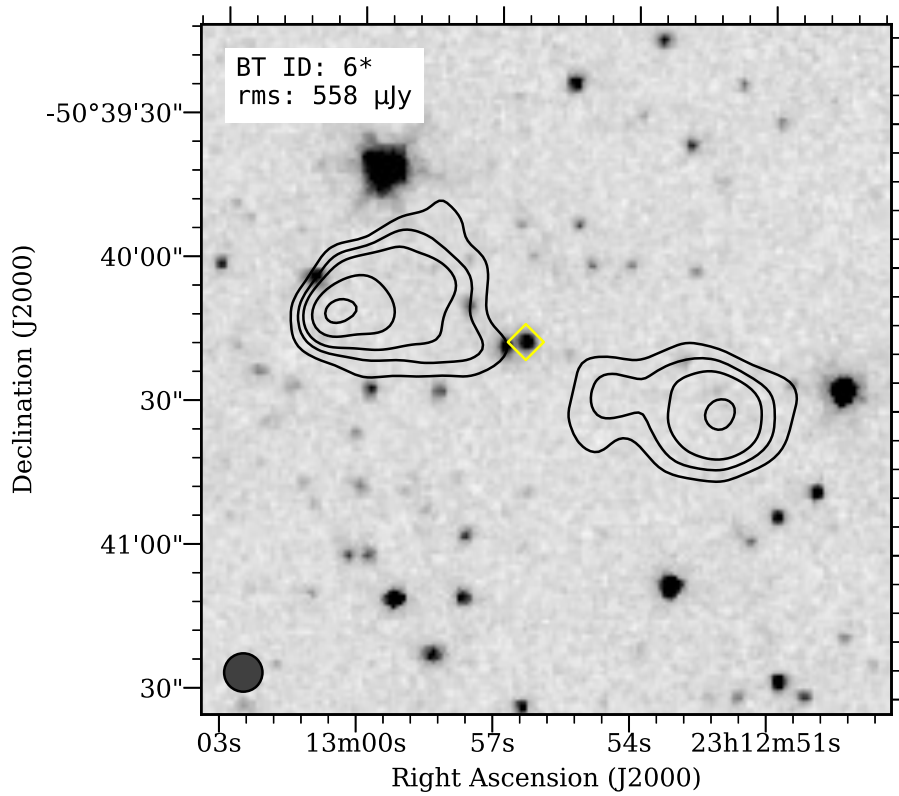
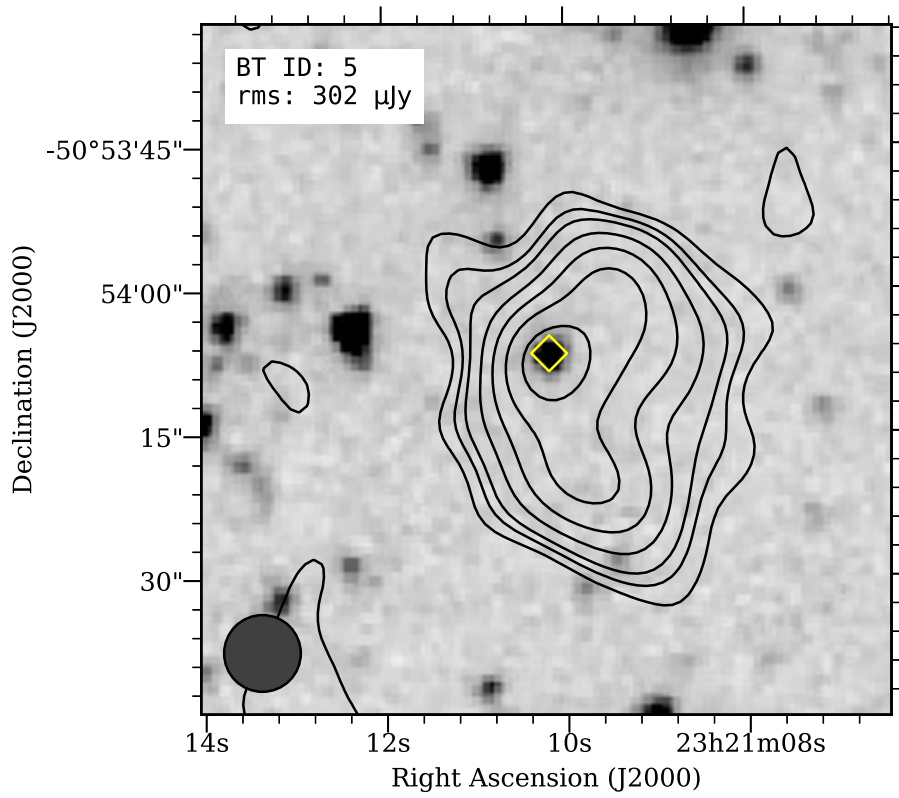
## Appendix 4.A Cutout Images of Bent-tail Sources

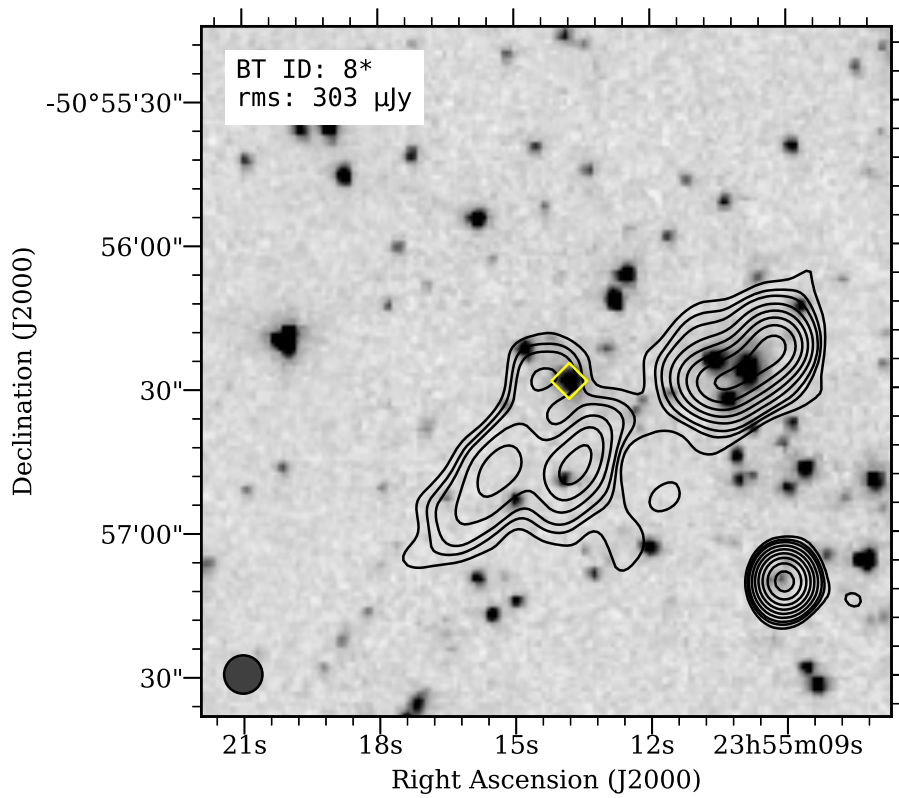
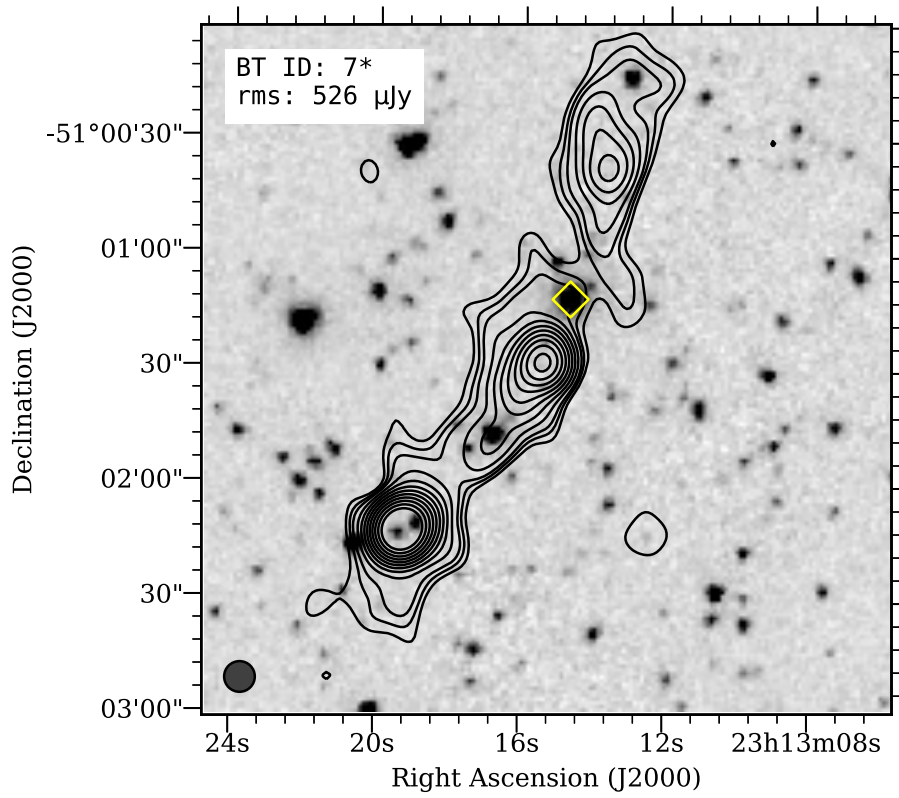
Each bent-tail candidate in the ATLAS-SPT survey is shown in the following figures. Radio structure from this study is shown in black contours overlaid on 3.6  $\mu\text{m}$  images from the SSDF.

Contours are drawn at  $3, 4, 5\sigma$  and then increase by factors of  $\sqrt{2}^n$  where  $n \in \mathbb{N}$ . Additional radio contours of higher resolution from the ATCA-XXL survey (Butler et al., 2017) are overlaid as dashed contours when available. Radio synthesised beam sizes for the ATLAS-SPT and ATCA-XXL data are shown in the bottom left and right corners, respectively. SSDF sources identified as the likely host galaxy are marked with a yellow diamond. Optical cross-identifications are indicated with a cyan X.

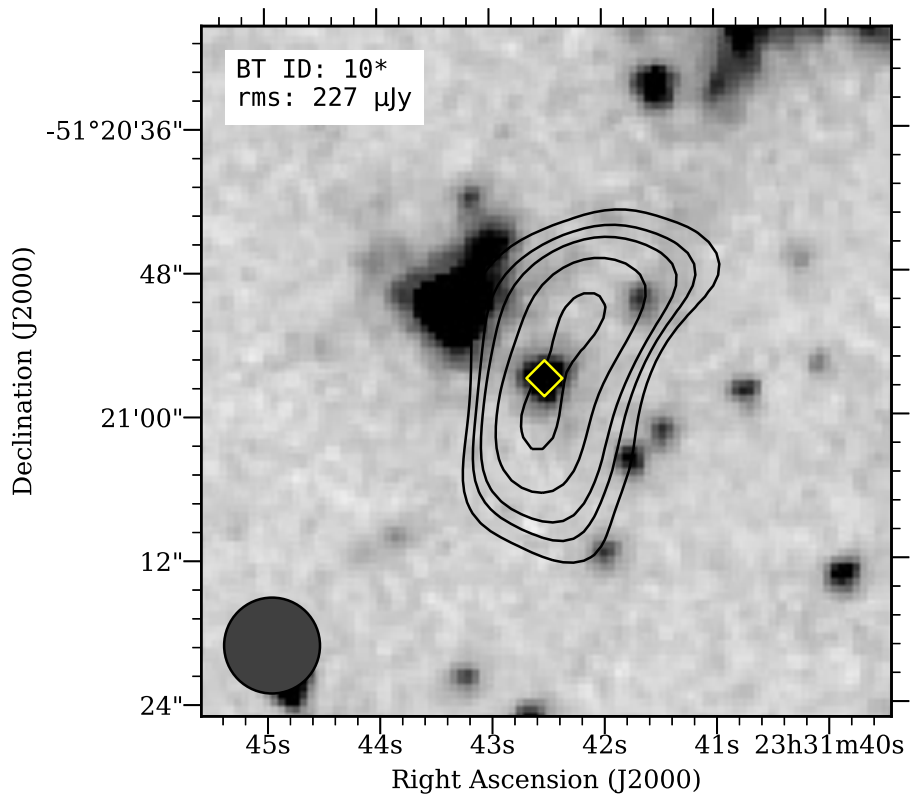
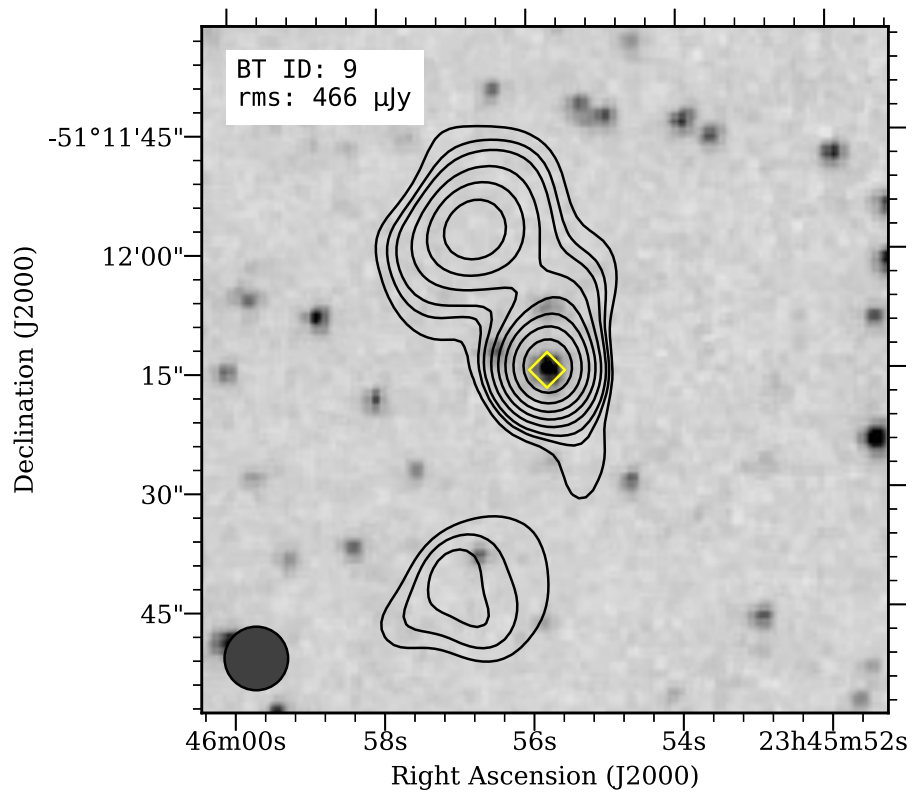


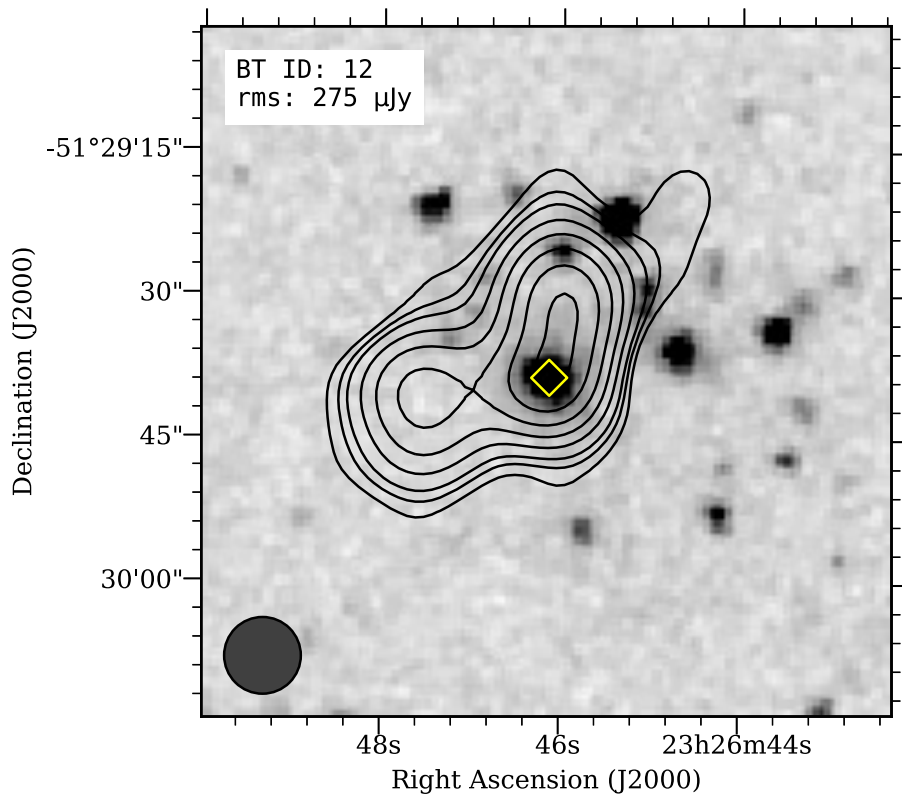
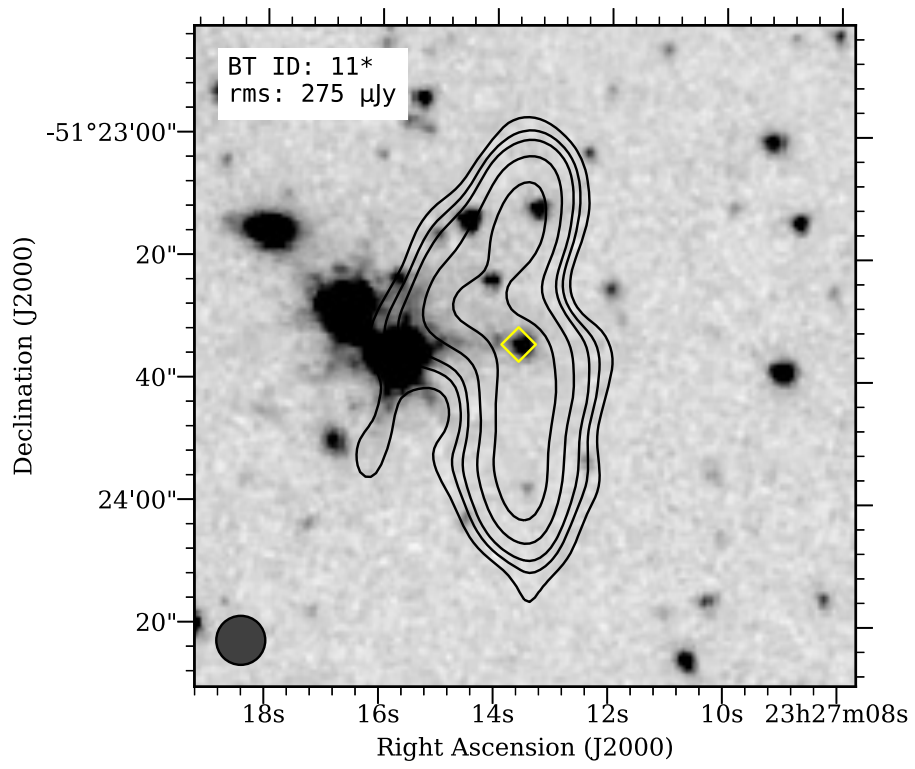


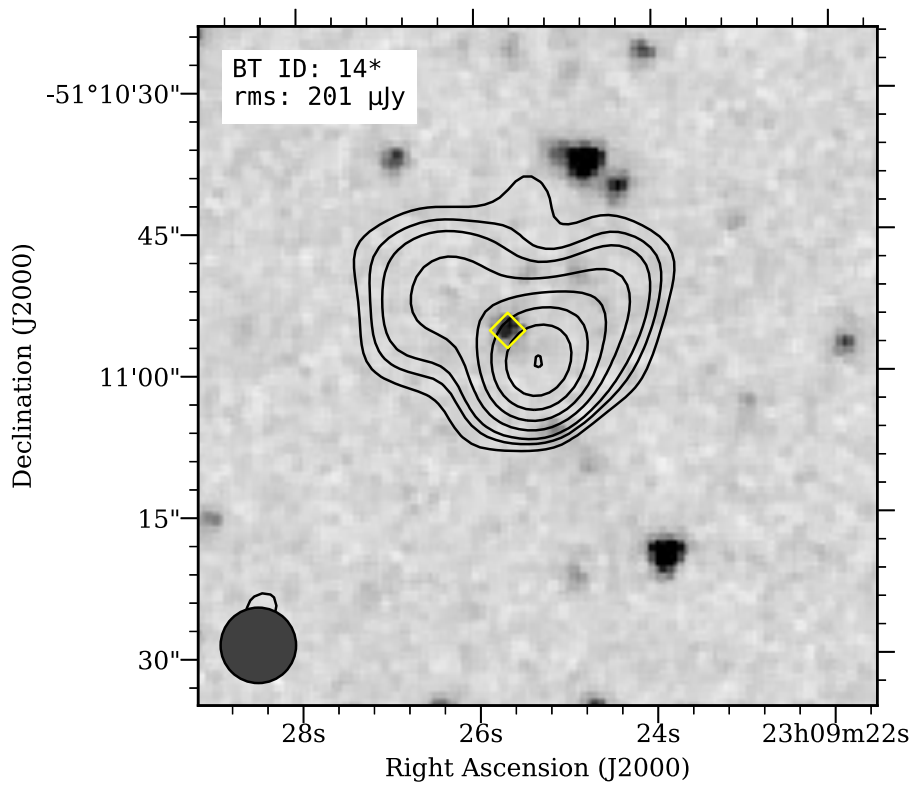
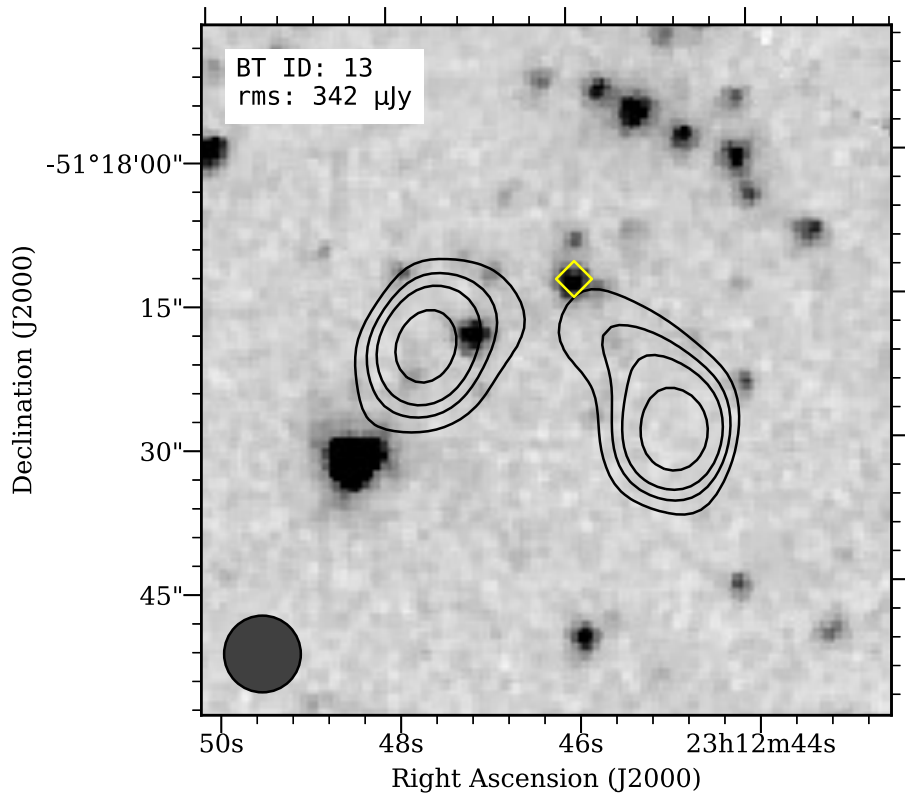


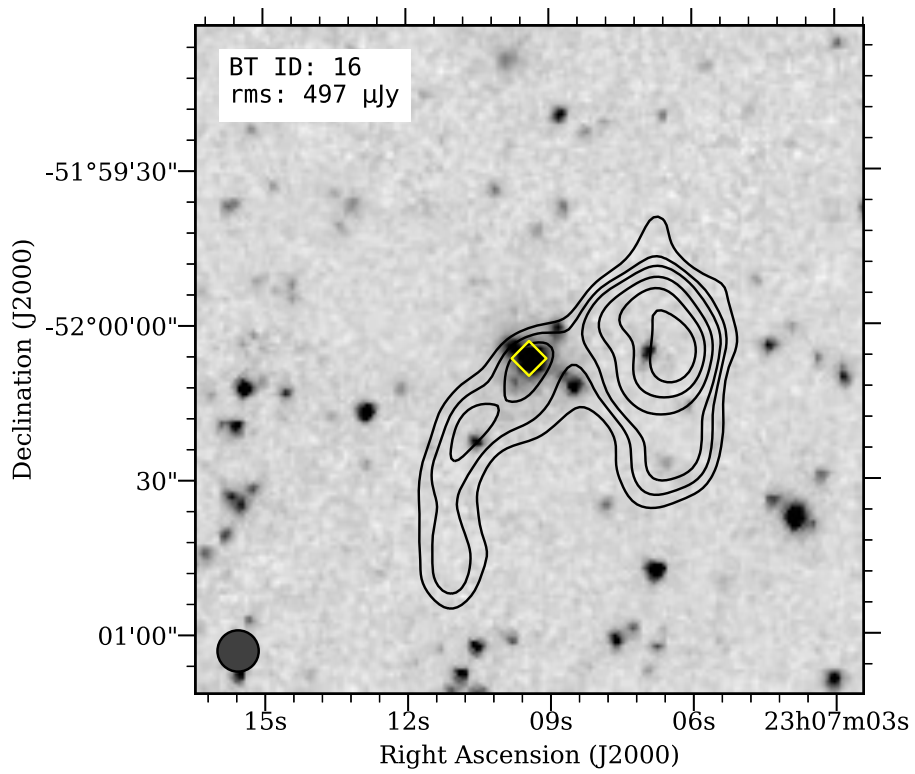
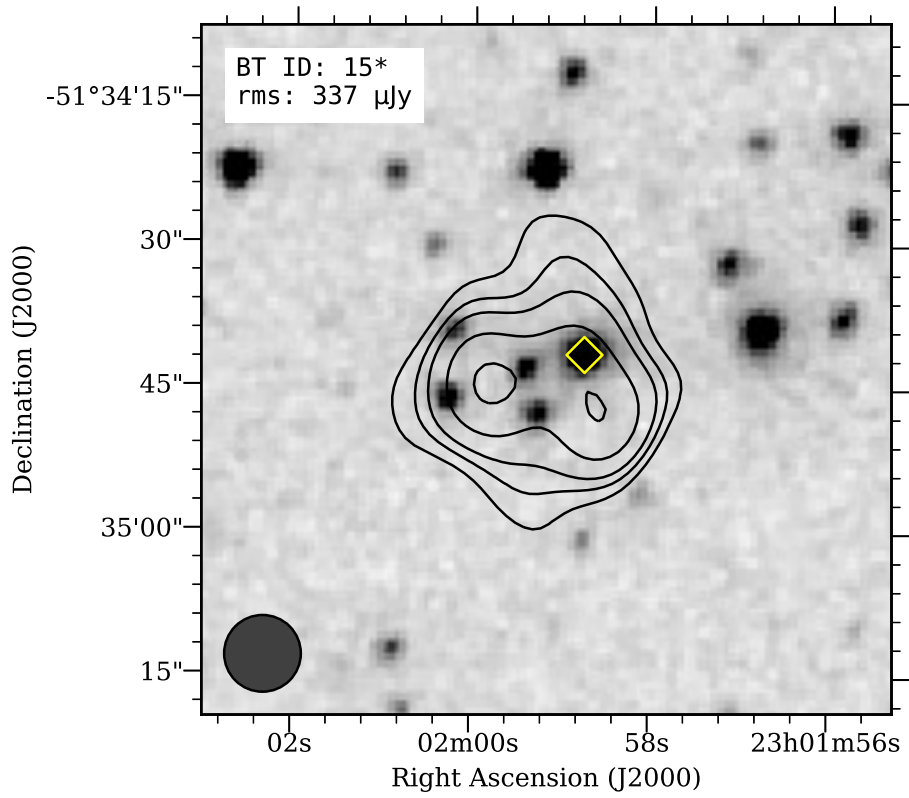


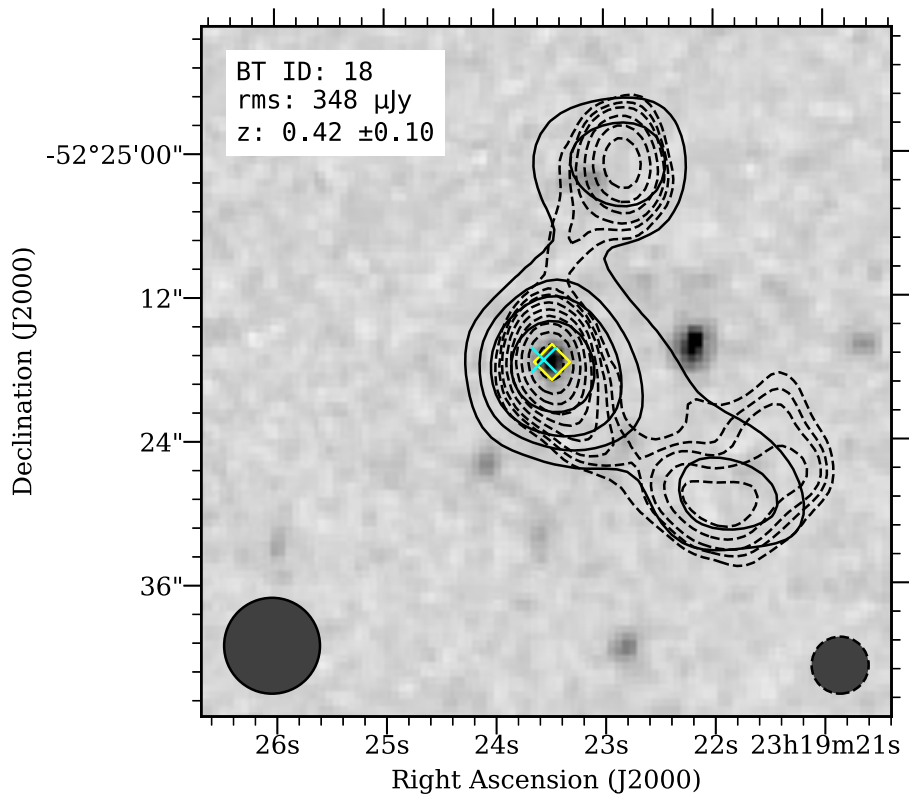
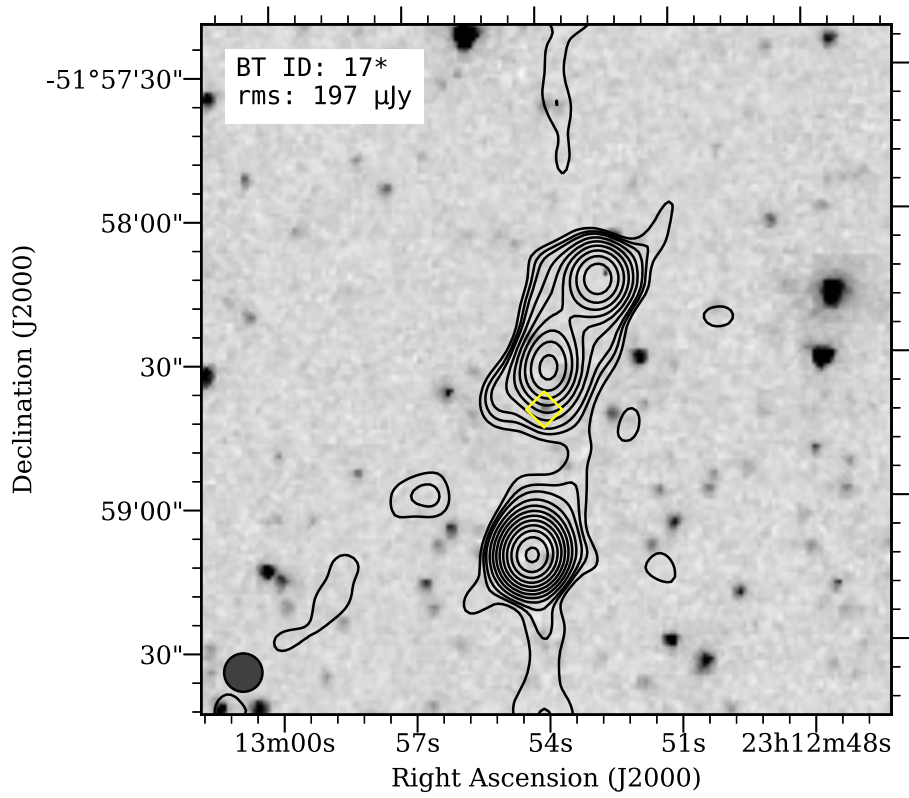


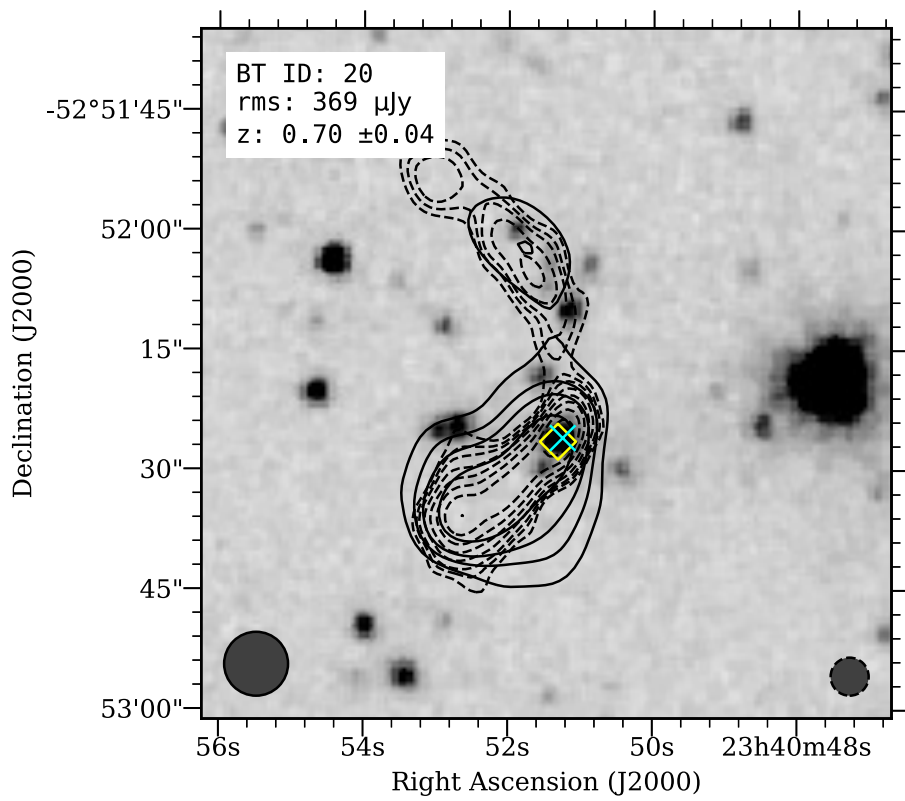
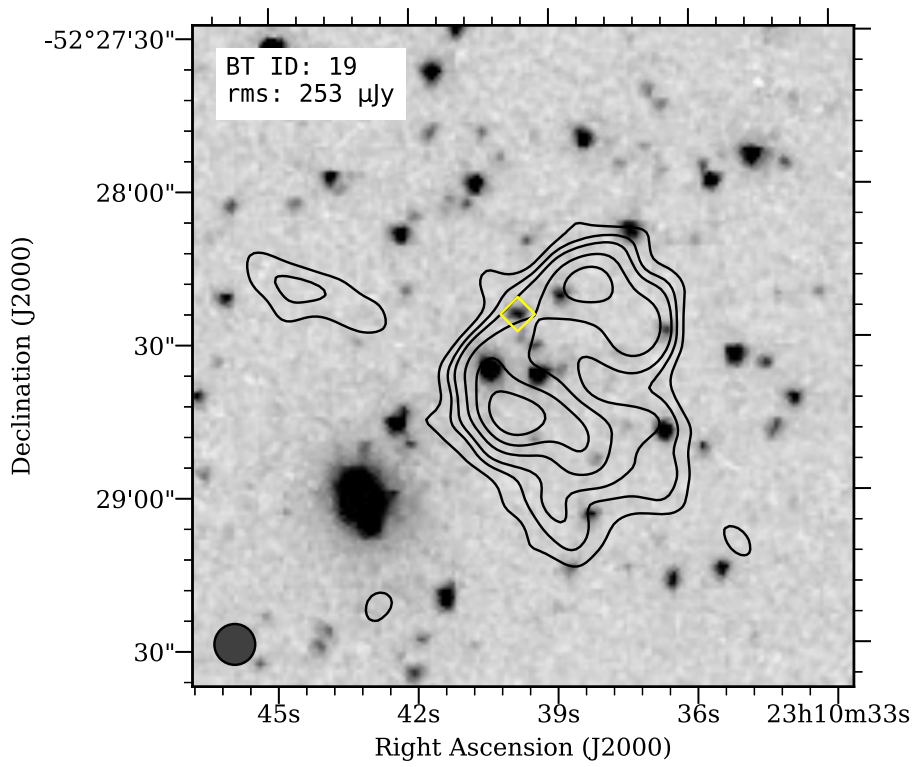




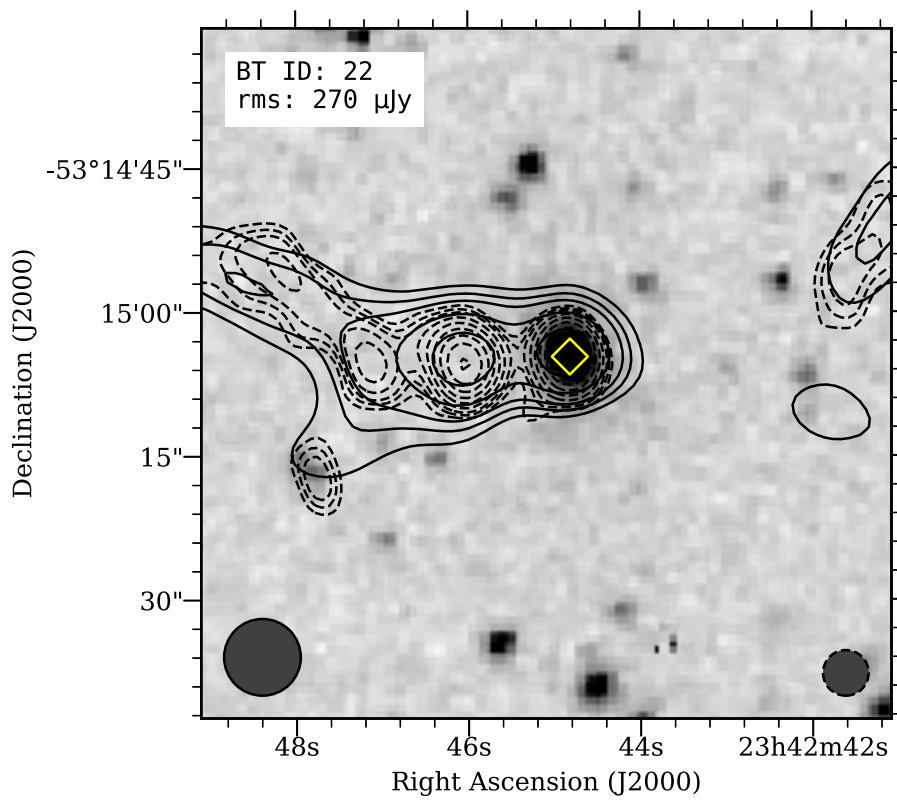
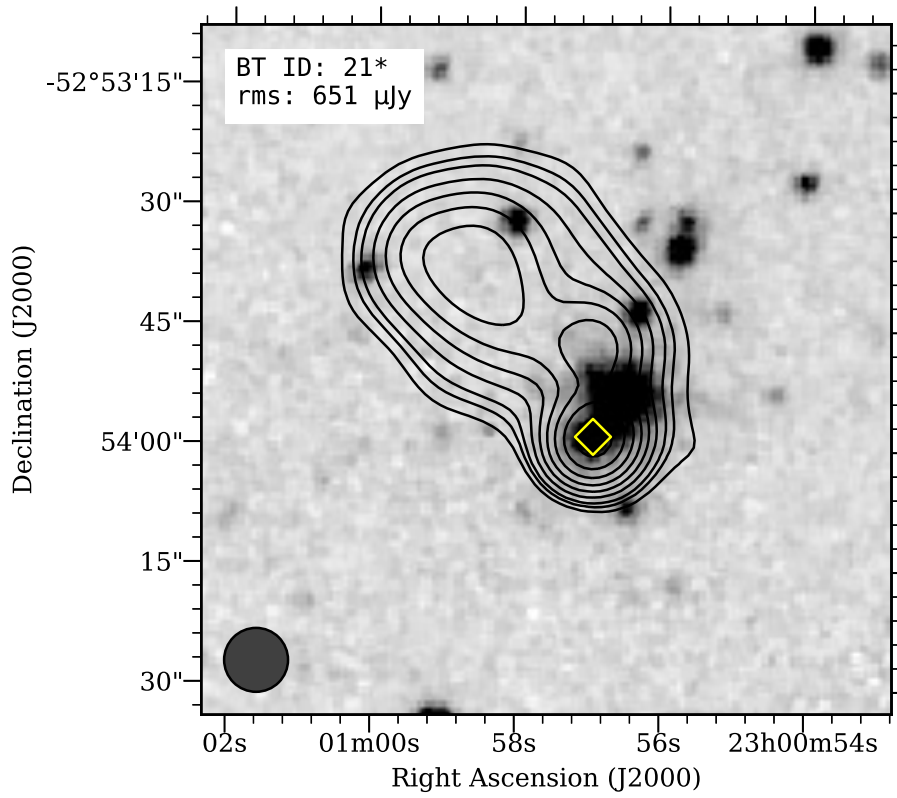


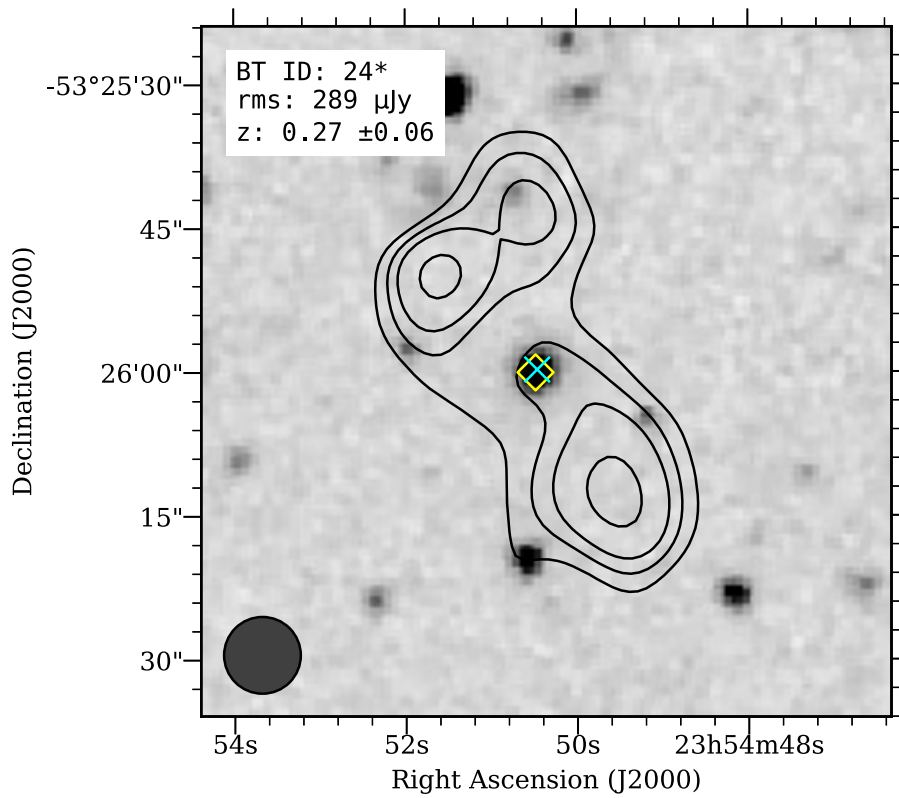
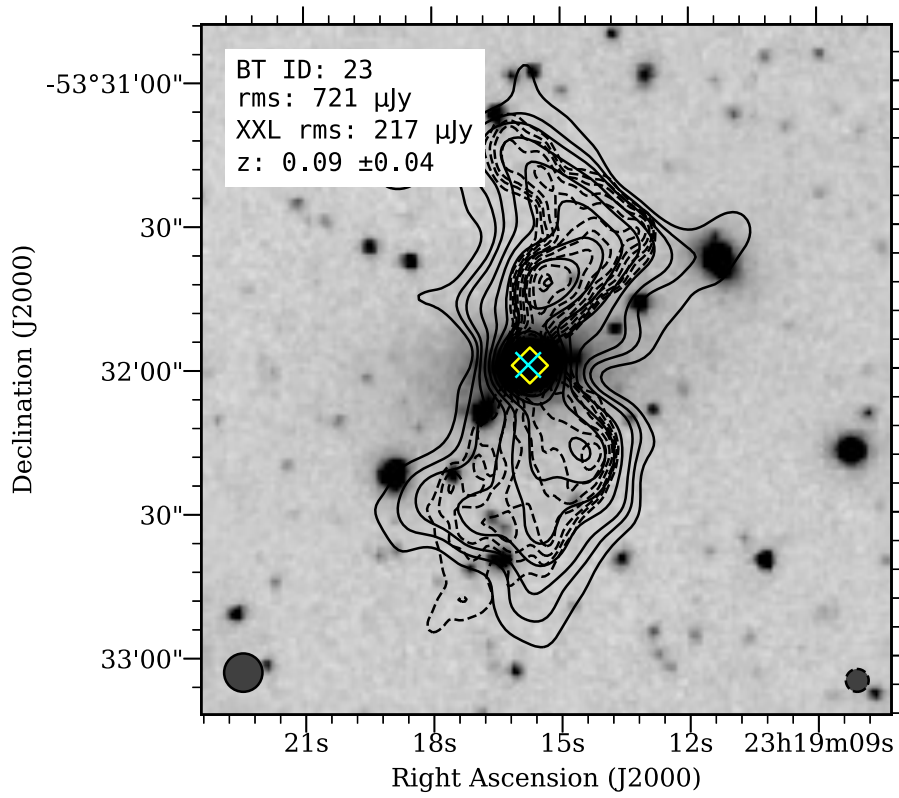




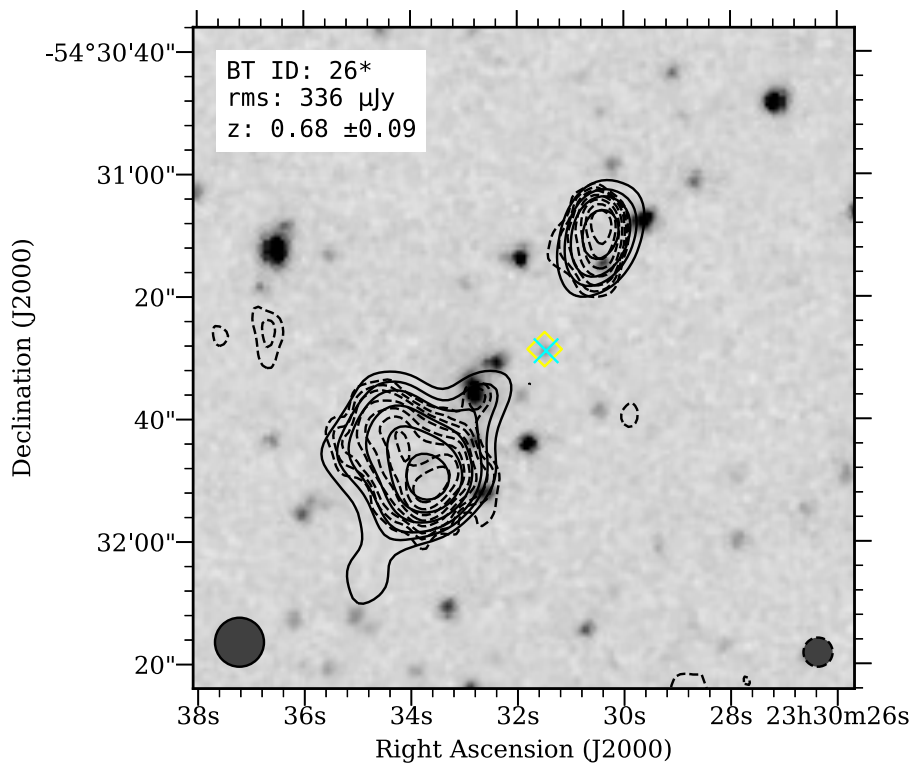
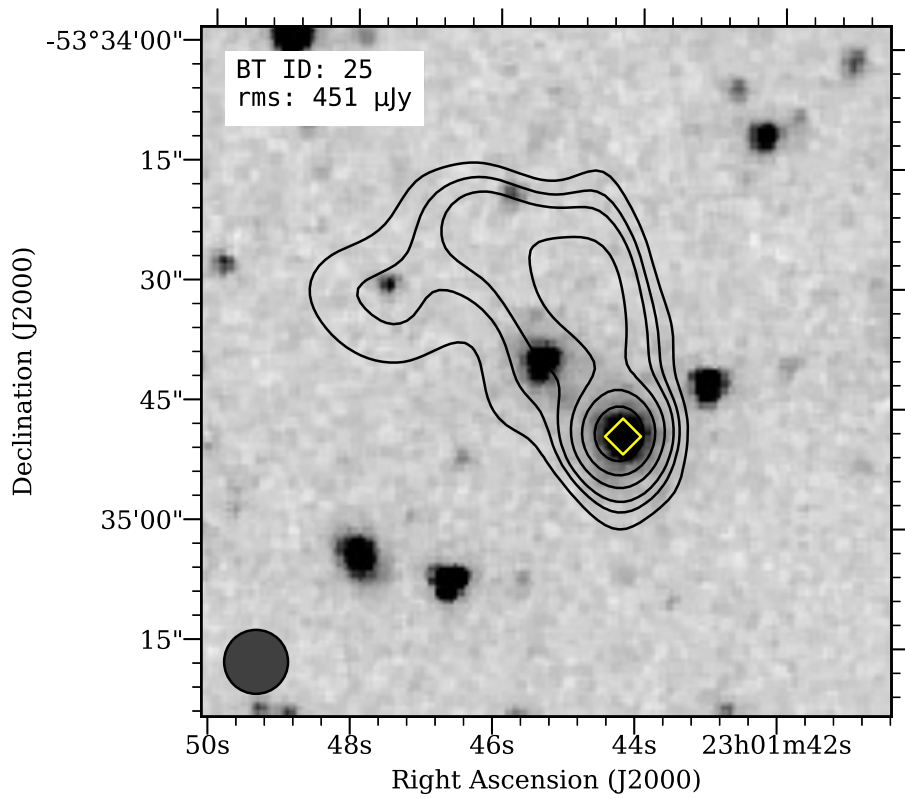


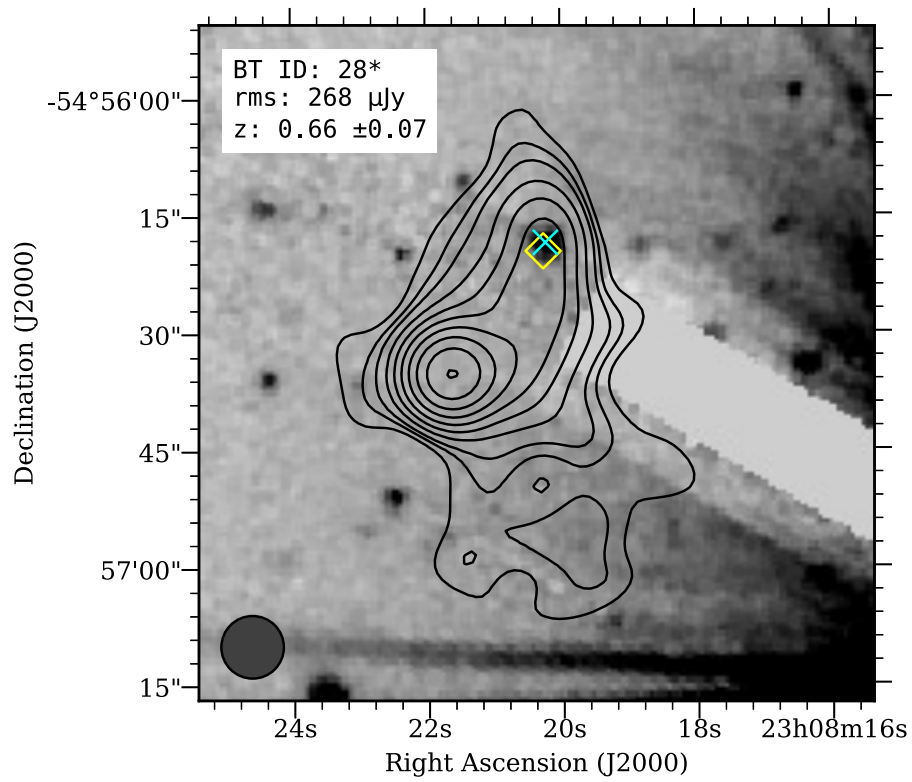
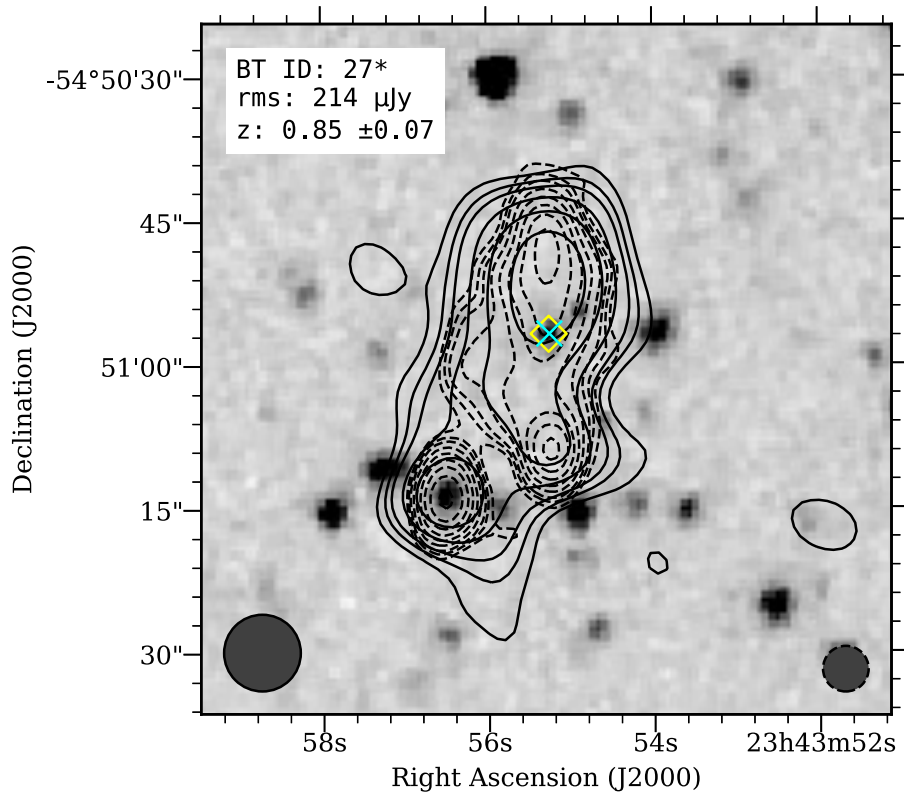


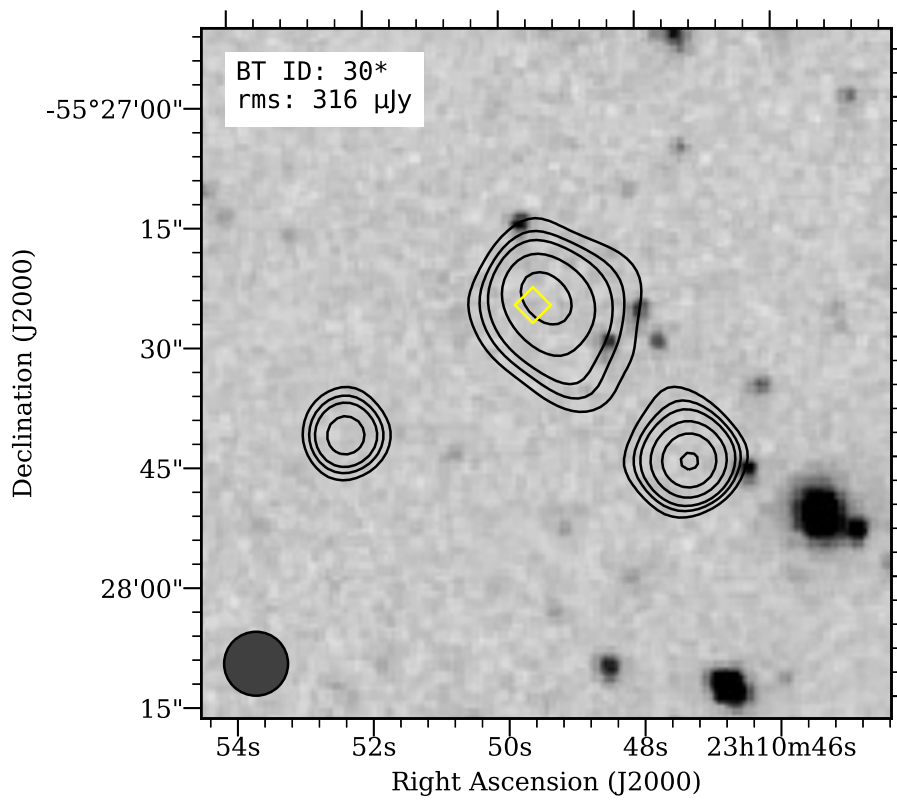
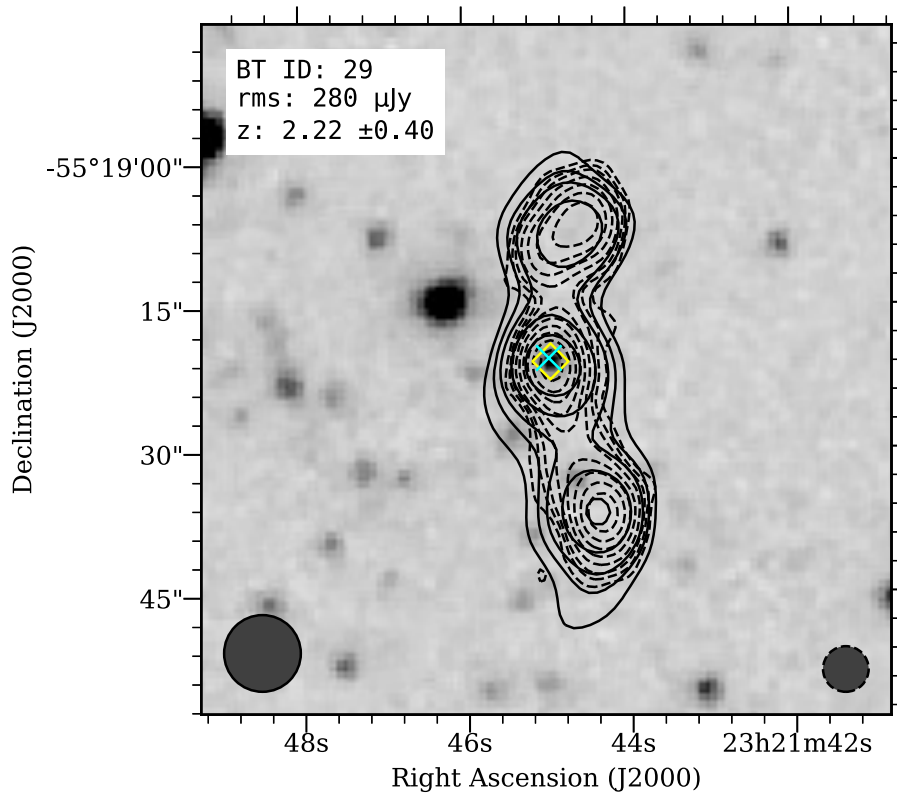


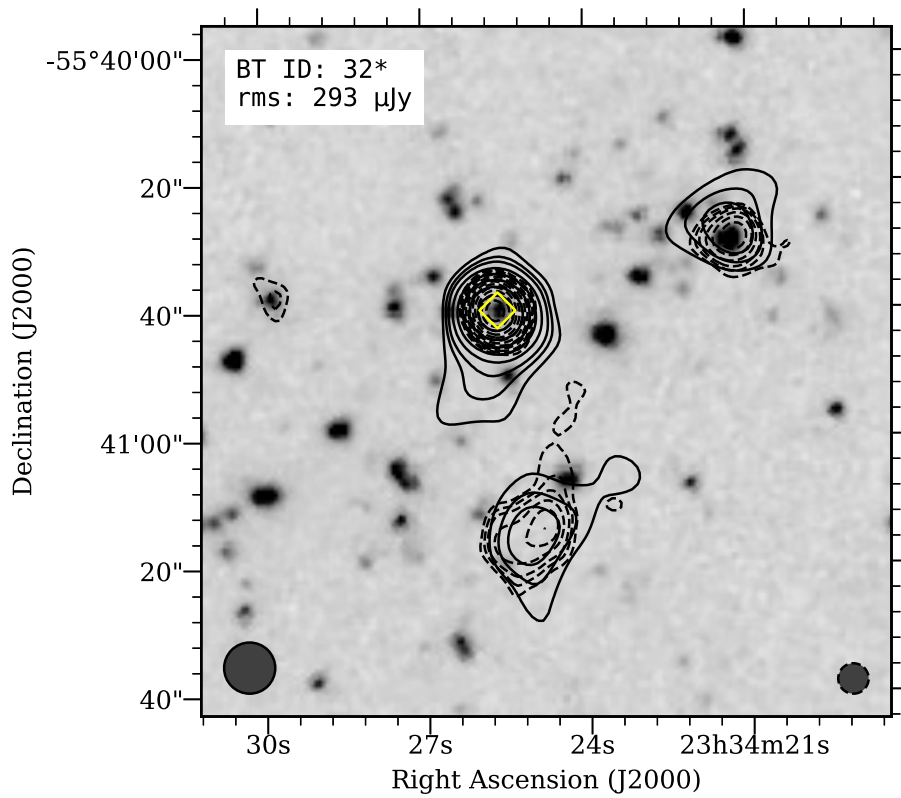
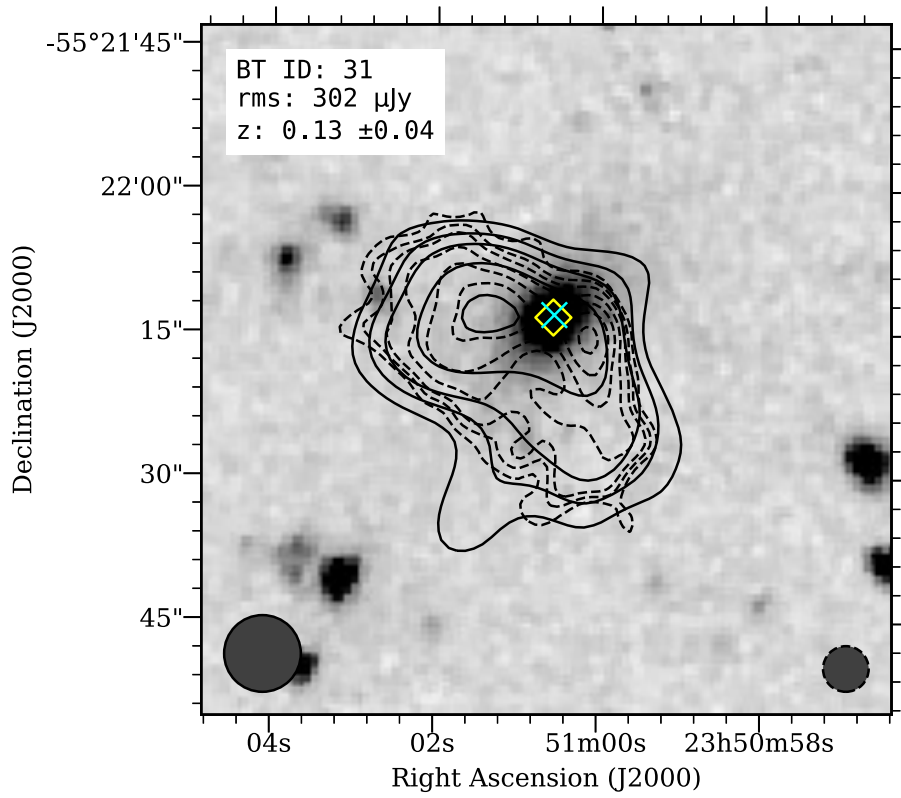


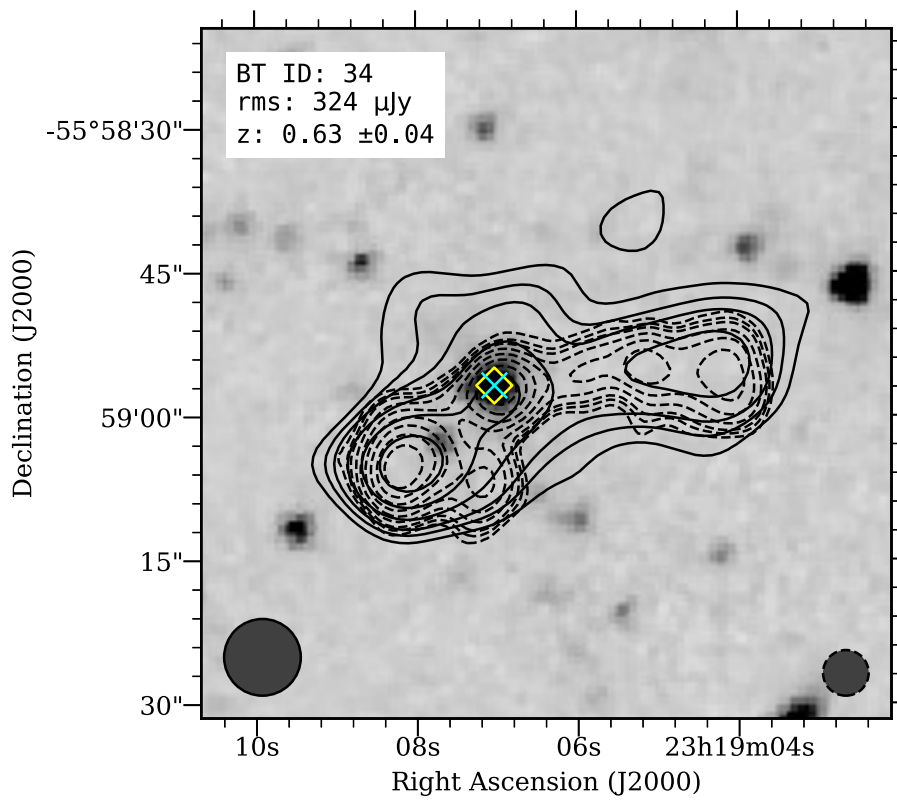
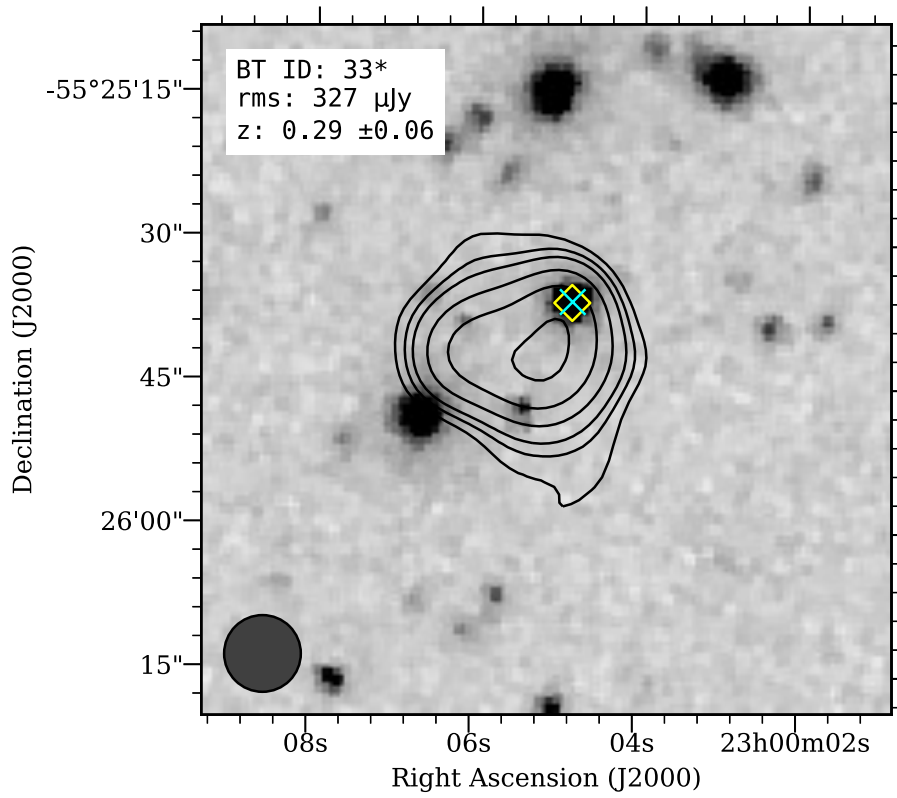


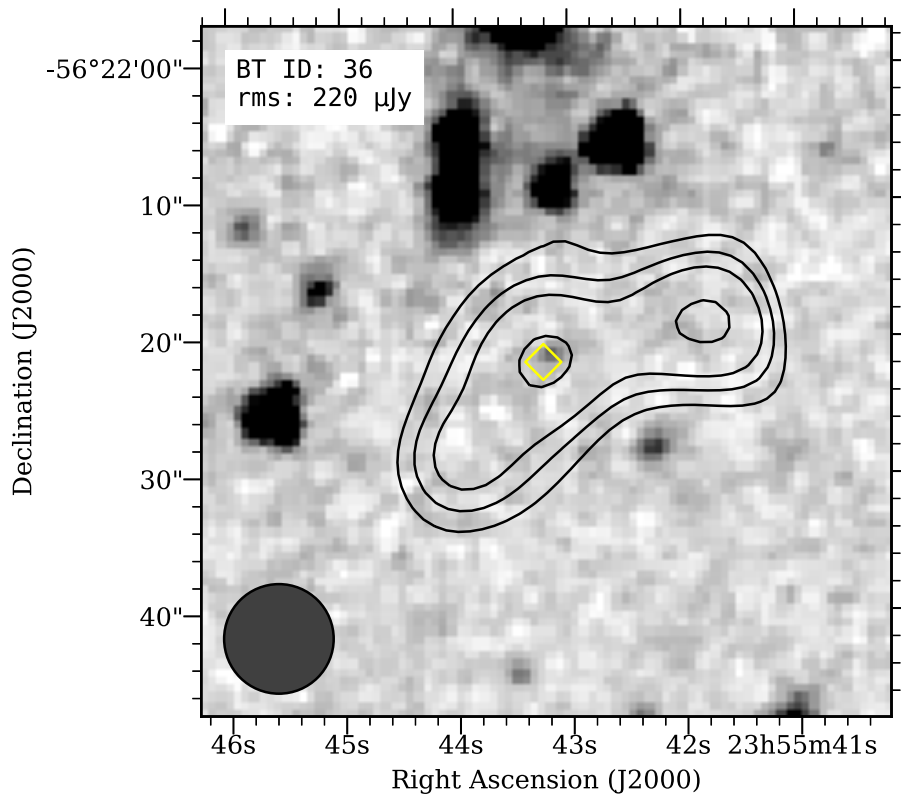
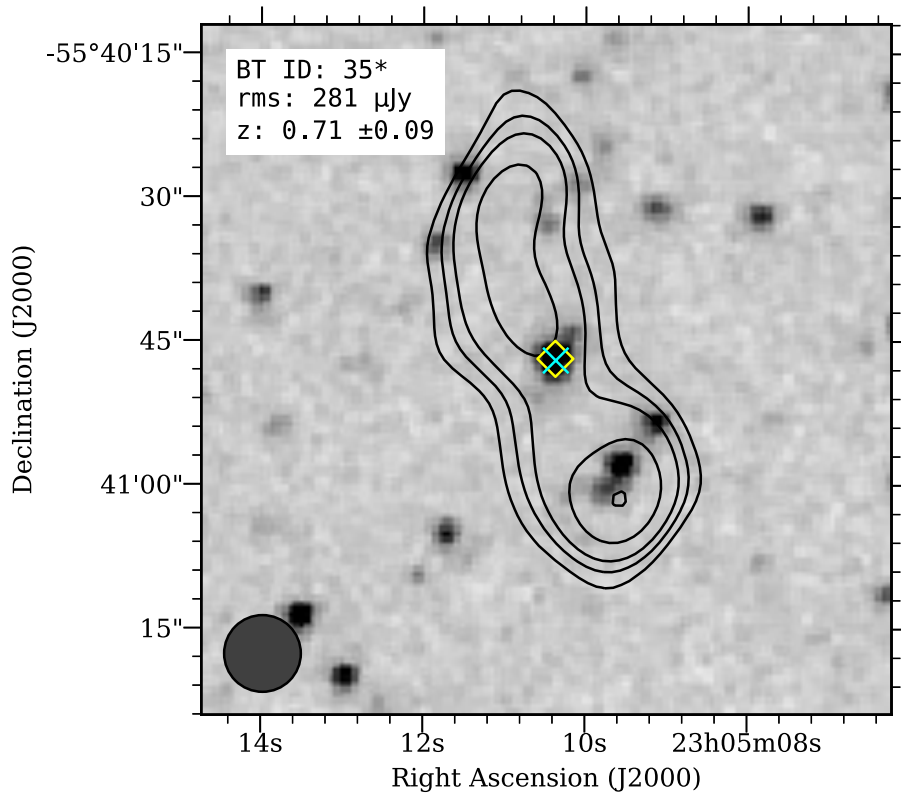




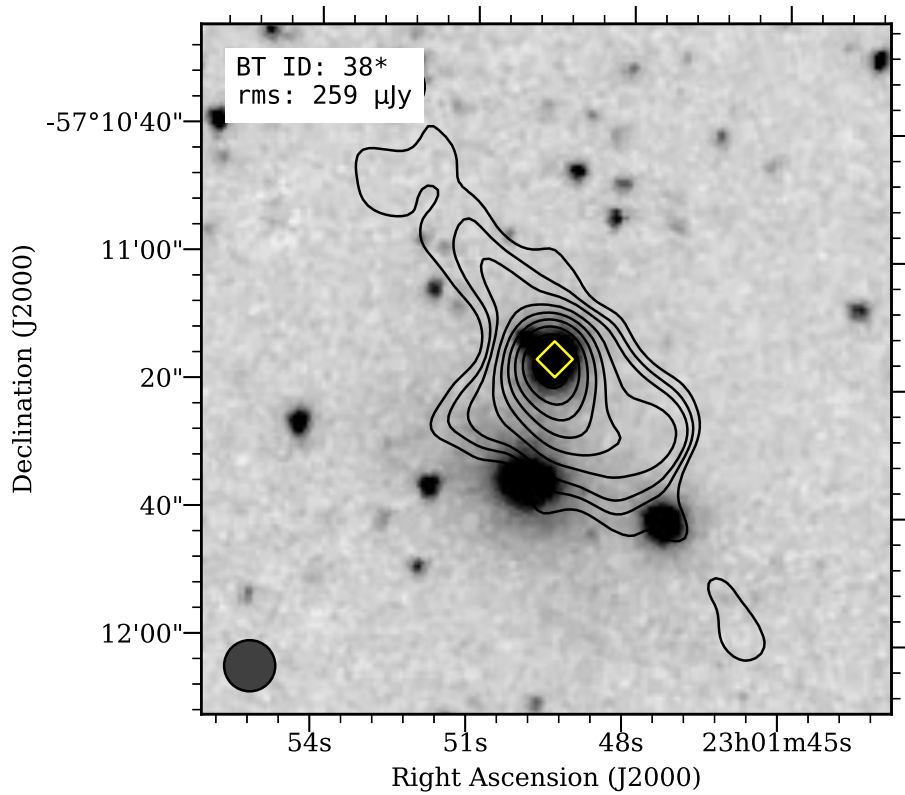
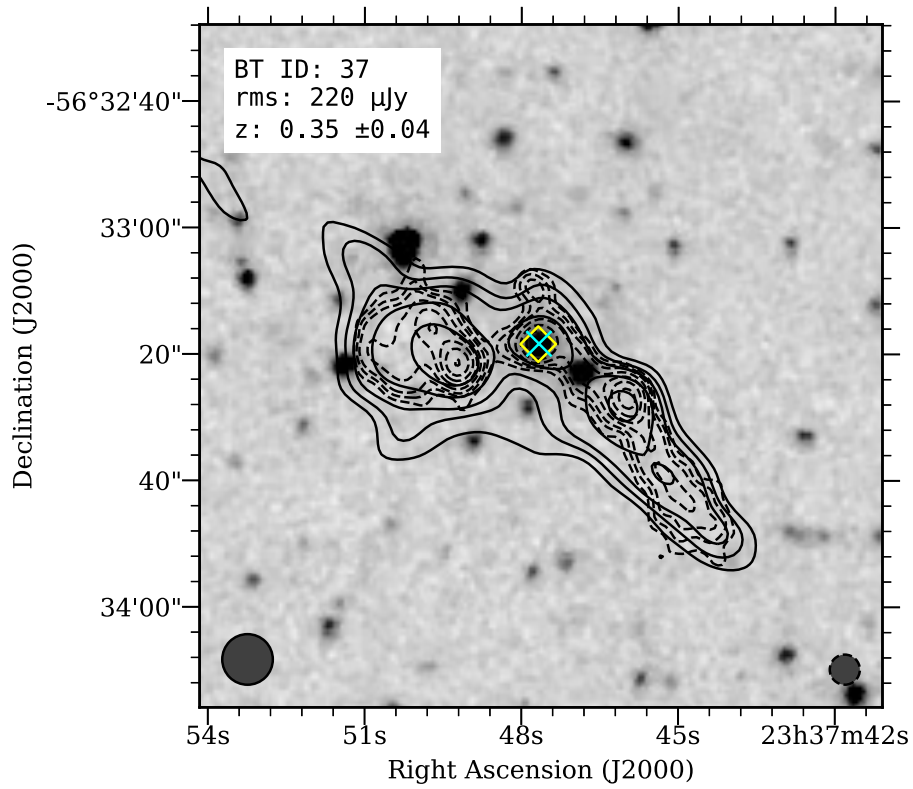


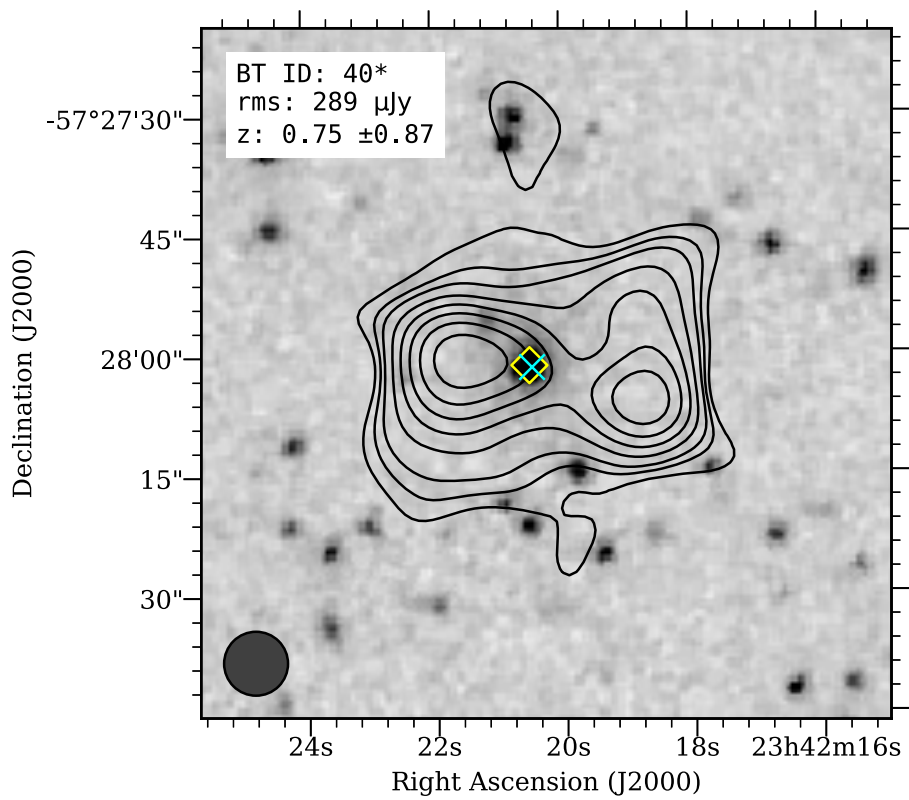
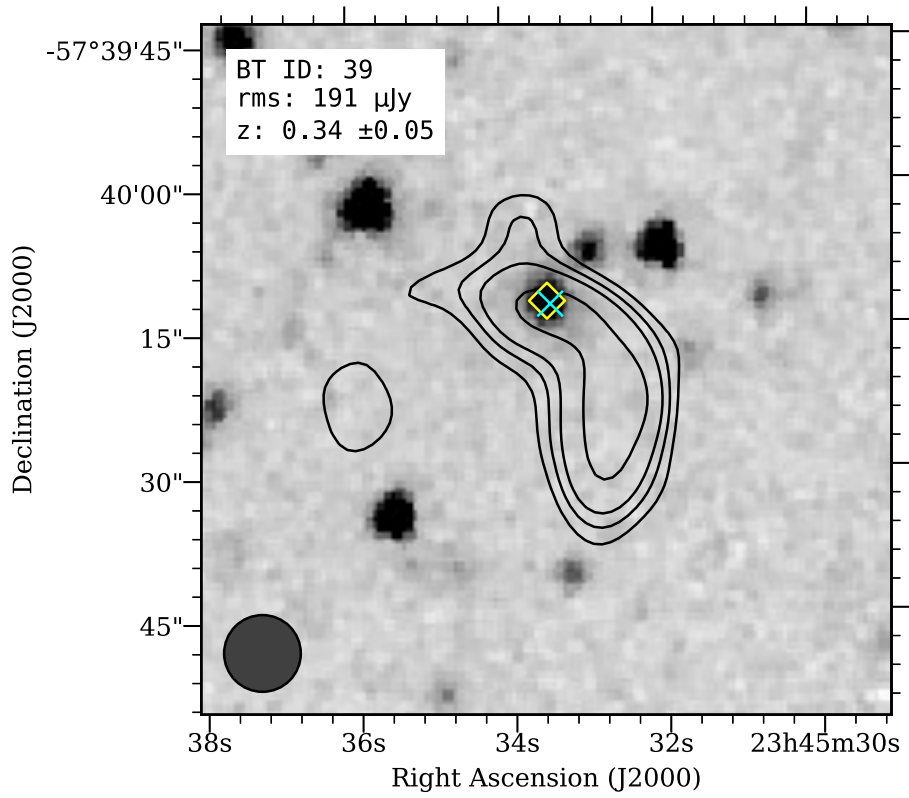




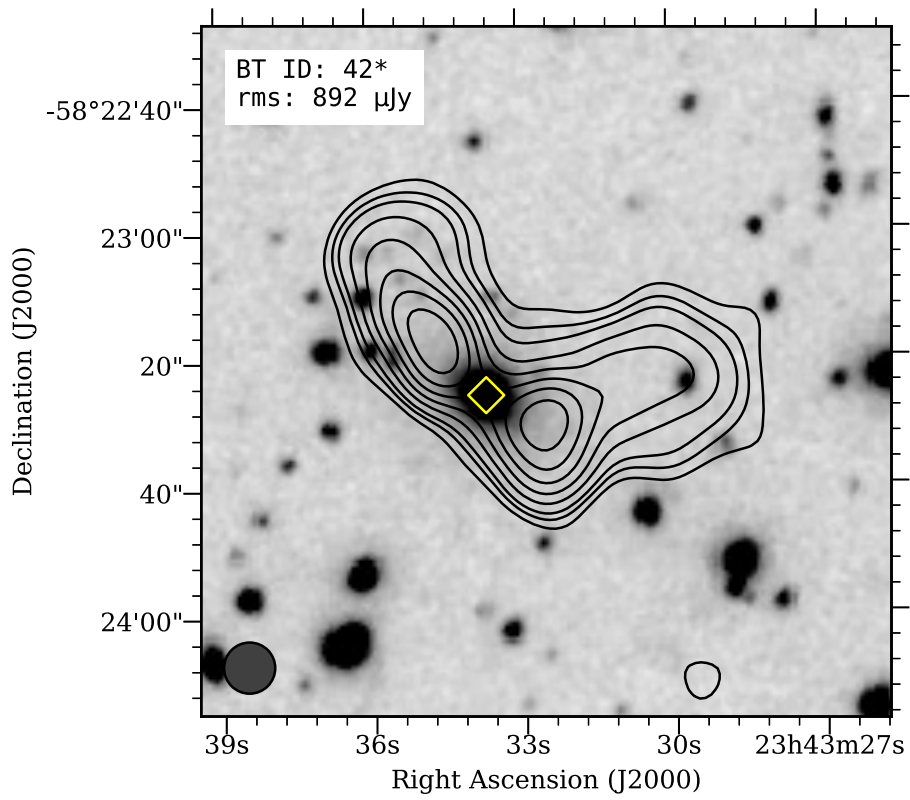
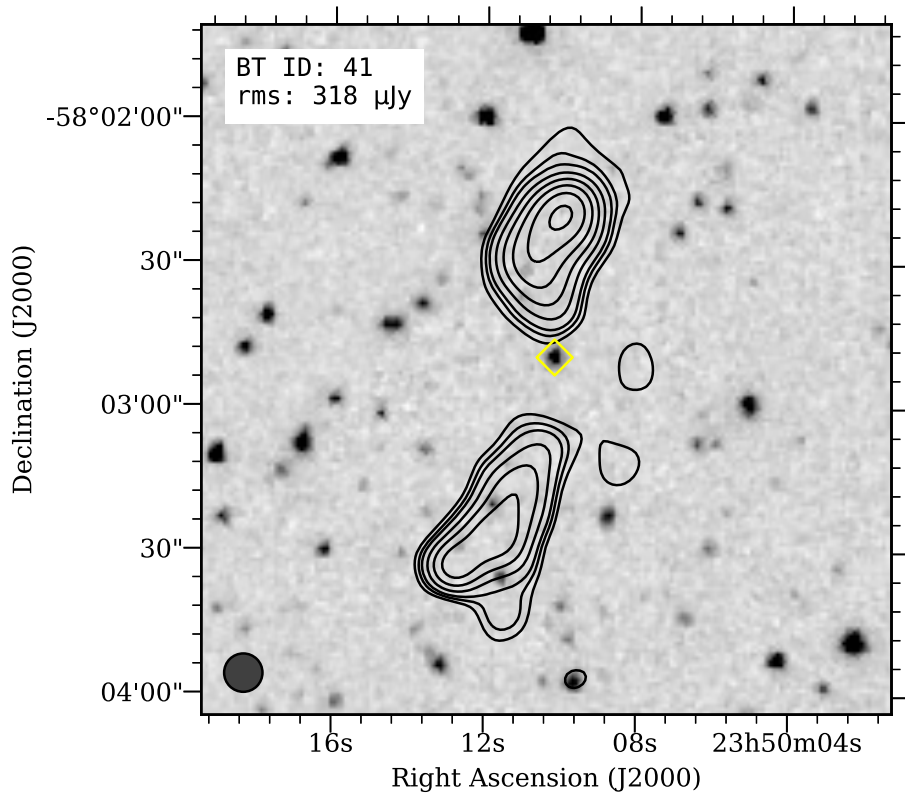


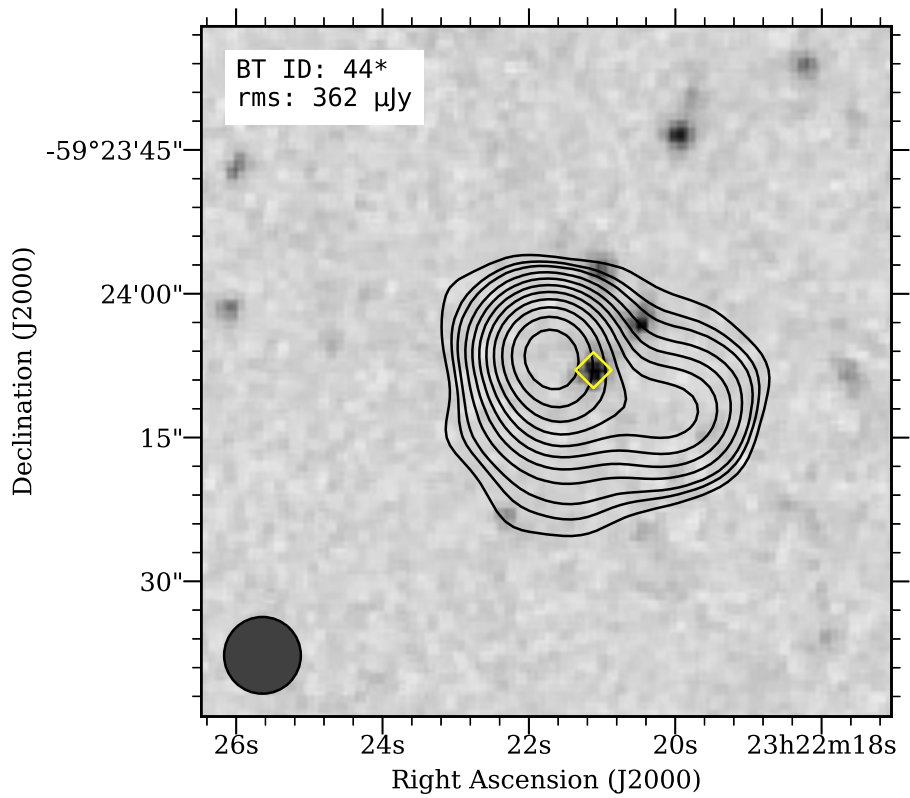
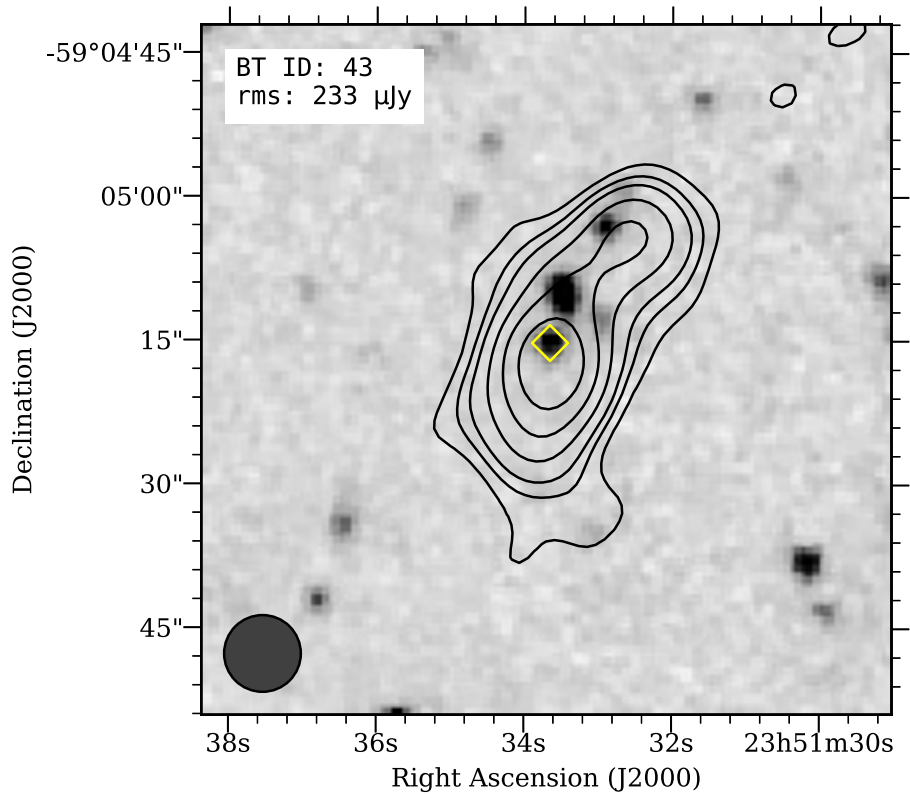


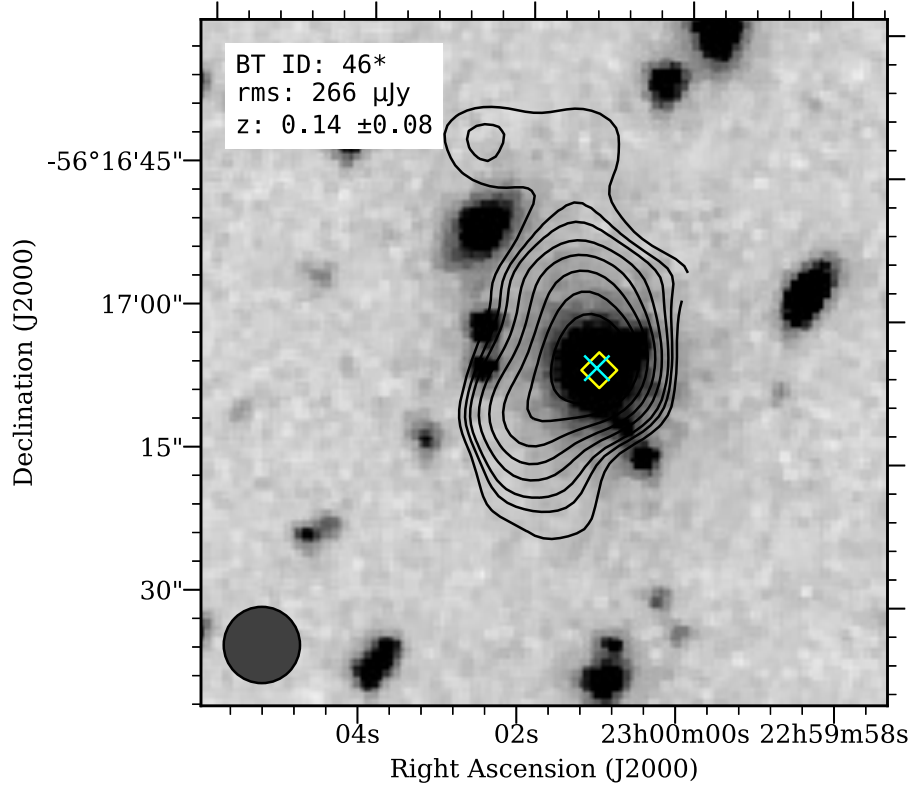
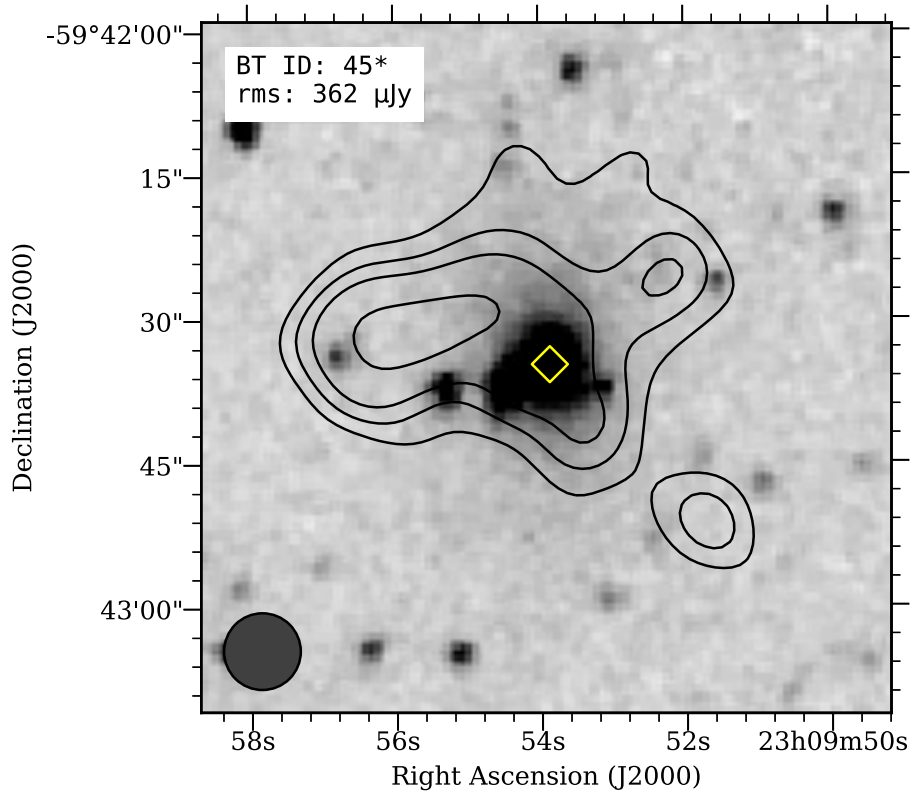












## Chapter 5

# Conclusions and Future Work

Planning, conducting and processing the data from large-area radio surveys is a gargantuan task. Most of my PhD project has been spent devising strategies for the observations, carrying out those observations, and then developing work-arounds to overcome the limitations in the available software to enable the processing of large volumes of data.

There is no doubt that the future of radio surveys is to produce sensitive all-sky maps as many of the latest instruments have been (or are being) optimised to do so. In particular, EMU, the main continuum survey for ASKAP, is estimated to detect about 70 million galaxies over 75% of the sky to a resolution of  $10''$  (Norris et al., 2011). The work presented in this thesis forms an important part of the preparation for the observation planning and data processing of both EMU and the currently underway ATCA legacy projects.

The observation strategies presented in this thesis have already been used when planning the observations for the ATCA legacy project observing the GAMA23 field. Once complete, the imaging strategies presented here will be used to make the imaging more automated and efficient. The automated outlier source subtraction will be useful for future surveys consisting of several pointings with restricted  $u, v$  coverage. A parallel computing approach to imaging is already in use for the processing of ASKAP data, and the work presented in this thesis provides a method of using similar techniques for data recorded with older instruments such as the ATCA.

The radio source catalogue presented in Chapter 3 provides accurate positions and flux densities for 6067 radio sources at a central frequency of 2.1 GHz. This catalogue will be used as priors to de-blend sources in confused maps covering the ATLAS-SPT field from the SPT and *Herschel* space telescope.

Using the ATLAS-SPT radio source catalogue and the various galaxy cluster catalogues covering the same field, I was able to test the efficacy of using bent-tail radio sources to detect

galaxy clusters. Surprisingly, I found only a small fraction (4 of 17) of bent-tails were associated with known galaxy clusters, and only one bent-tail was found to reside within an SZ detected cluster which is from a mass-limited sample. This casts doubt upon models that predict the number of bent-tails as a function of cluster mass.

A summary of my achievements from my candidature is given below.

1. I planned and executed the observation of  $\sim 86 \text{ deg}^2$  with the ATCA.
2. I devised strategies for reducing large datasets and processed the data to produce an image covering the  $\sim 86 \text{ deg}^2$  field.
3. I have generated a catalogue of 6067 radio sources in the field, measuring their position and flux densities.
4. I have produced differential source counts of flux density, which shows that the catalogue data has excellent signal-to-noise ratio in the region depicting AGN evolution, and also indicates the flattening due to star-forming galaxies.
5. I have measured spectral indices for the 722 sources strong enough to yield a reliable spectral index which conforms to the expected distribution for a survey predominantly sensitive to AGN.
6. I have compared the positions of bent-tail radio galaxies with known galaxy clusters, and shown that they fail to confirm the predictions of theoretical models of the distribution of bent-tail galaxies.

## 5.1 Future Work

The ATLAS-SPT survey is currently being extended to include a study of diffuse radio emission. This complementary survey uses the same survey strategy but with a more compact array configuration to target diffuse emission. It aims to detect more galaxy clusters through the detection of the ICM or by locating radio relics (see Section 1.1). The observations have been completed and data processing is currently underway.

The visibility data from this work will be used to subtract the compact sources from the lower resolution diffuse study data so that only the diffuse emission that was resolved out by the work presented in this thesis remains. This study will be the first large-area diffuse radio emission survey for clusters and will be also be an important pathfinder for diffuse emission processing for future surveys such as EMU. Additionally, the compact configuration data can also be merged with the high-resolution data from this thesis to increase sensitivity by a factor of  $\sqrt{2}$ .

Early science commissioning ASKAP observations of the ATLAS-SPT field have also been completed and data processing is currently underway. The radio catalogue presented in this thesis has been included in the quality assurance pipeline to provide indicators of instrumentation or imaging issues within the ASKAP pipeline. Once complete, the ASKAP data will provide extra spectral information at  $\lambda = 20$  cm, filling the gap between this work and lower radio frequency studies such as SUMSS.

The investigation of the spatial correlation between bent-tail radio galaxies and galaxy clusters within the ATLAS-SPT survey area used existing cluster catalogues. At the time this study was conducted, the optical data coverage for the field was incomplete. Since the conclusion of this work, more optical data from DES has been released which now covers the entire field. I intend to use this dataset to search for more optical hosts for the bent-tails identified in Chapter 4 to obtain photometric redshifts which may permit more of these sources to be matched to known clusters. The more complete optical survey data may also be used to find previously unknown clusters by searching for galaxy overdensities.

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