

# Evaluation and Parameter Analysis of Burn up Calculations for the Assessment of Radioactive Waste

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The purpose of this work is to define and verify the range of validity and limitations of correlations used for nuclear waste characterization and to scrutinize the dependencies and propagation of uncertainties that affect the waste inventory declarations and their independent verification. This is accomplished by numerical assessment and simulation of waste production using well accepted codes SCALE 6.0 and 6.1 to simulate the cooling time and burn up of a spent fuel element. The simulations are benchmarked against spent fuel from the pressurized water reactor Obrigheim in Germany for which sufficiently precise experimental reference data are available.

Table I. Calculation vector: from SFCOMPPO data base [1]

Variable	Unit
1. Cs-134/Cs-137	Bq/Bq
2. Cs-137/U-238 <sup>1</sup>	mol/mol
3. Eu-154/Cs-137 <sup>1</sup>	Bq/Bq
4. K-85/K-86 <sup>2</sup>	mol/mol
5. K-84/K-86 <sup>2</sup>	mol/mol
6. K-85/K-86 <sup>2</sup>	mol/mol
7. Nd-148/U-238	mol/mol
8. Pu-238/total Pu	kg/kg
9. Pu-239/total Pu	kg/kg
10. Pu-238/U-238	mol/mol
11. Pu-240/total Pu	mol/mol
12. Pu-240/total Pu	kg/kg
13. Pu-240/Pu-239	mol/mol
14. Pu-240/total Pu	kg/kg
15. Pu-242/total Pu	mol/mol
16. Pu-242/total Pu	kg/kg
17. total Pu/total U	mol/mol
18. total Pu/total U	kg/kg
19. U-235/total U	kg/kg
20. U-235/total U/(U-235/total U min)	kg/kg
21. U-235/U-238	mol/mol
22. U-235/total U	kg/kg
23. U-238/U-238	mol/mol
24. U-238/total U	kg/kg
25. Xe-137/Xe-134 <sup>2</sup>	mol/mol
26. Xe-137/Xe-134 <sup>2</sup>	mol/mol
27. Xe-135/Xe-134 <sup>2</sup>	mol/mol
28. Burn up (by Cs-137 (destructive method)) <sup>1</sup>	GWD/MTU
29. Burn up (by Cs-137 (non-destructive method)) <sup>1</sup>	GWD/MTU
30. Burn up (by Nd-148 (method))	GWD/MTU
31. Burn up (by theoretical)	GWD/MTU
32. Am-241	kg
33. Cm-242	kg
34. Cm-244	kg
35. Cs-134	kg
36. Cs-137	kg
37. Eu-154 <sup>1</sup>	kg
38. Pu-238	kg
39. Pu-239	kg
40. Pu-240	kg
41. Pu-241	kg
42. Pu-242	kg
43. total Pu	kg
44. total Pu, U	kg
45. total U	kg
46. U-235	kg
47. U-235 Depletion	kg
48. U-238 Build-up	kg
49. U-238	kg
50. U-235 Depletion	kg

## BENCHMARK

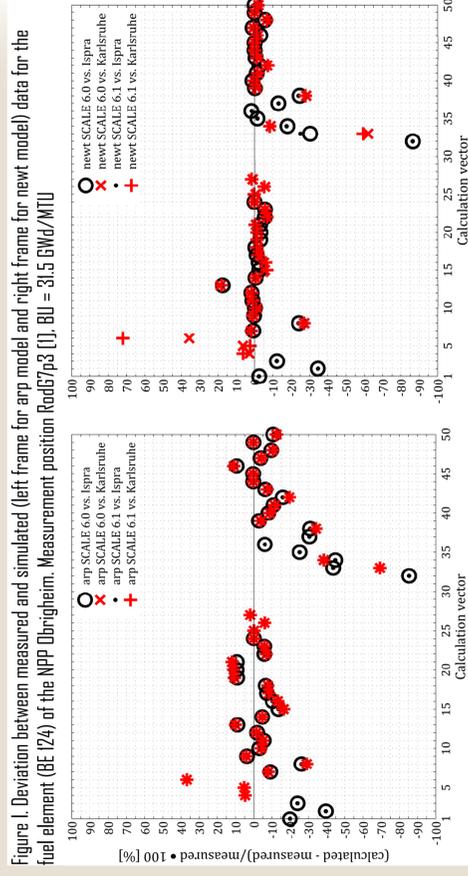


Figure I. Deviation between measured and simulated (left frame for arp model and right frame for newt model) data for the fuel element (BE 124) of the NPP Obrigheim. Measurement position Rod67p3 [1]. BU = 31.5 GWD/MTU

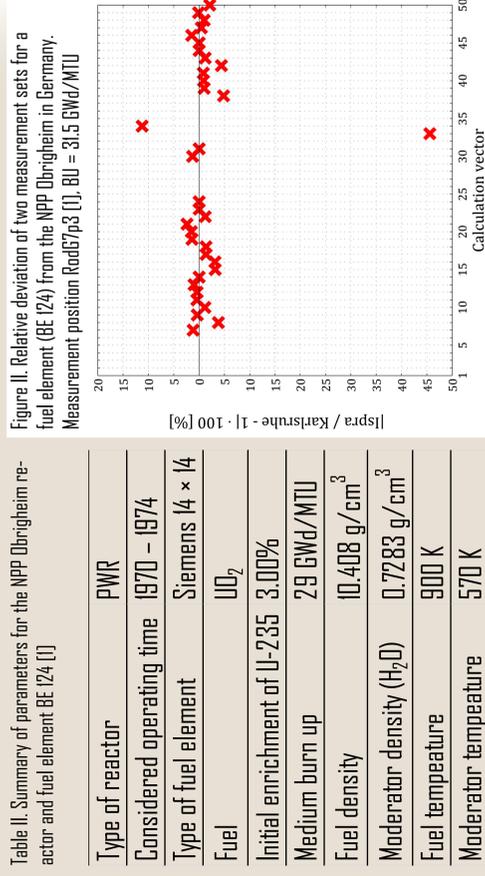


Figure II. Relative deviation of two measurement sets for a fuel element (BE 124) from the NPP Obrigheim in Germany. Measurement position Rod67p3 [1]. BU = 31.5 GWD/MTU

Table II. Summary of parameters for the NPP Obrigheim reactor and fuel element BE 124 [1]

Type of reactor	PWR
Considered operating time	1970 – 1974
Type of fuel element	Siemens 14 x 14
Fuel	UO <sub>2</sub>
Initial enrichment of U-235	3.00%
Medium burn up	29 GWD/MTU
Fuel density	10,408 g/cm <sup>3</sup>
Moderator density (H <sub>2</sub> O)	0.7283 g/cm <sup>3</sup>
Fuel temperature	900 K
Moderator temperature	570 K

References:

[1] <http://www.oecd-nea.org/stcomppo/Ver.2/Eng/Obrigheim/index.html>, Online 2013

<sup>1</sup> Only from "Joint Research Center" (Ispra)  
<sup>2</sup> Only from Karlsruhe Institute of Technology (Karlsruhe)

## VARIATIONAL ANALYSIS OF THE CORRELATION BANDWIDTH

**SECONDARY REACTOR PARAMETERS**

- Fuel properties: initial enrichment: density, temperature
- Moderator properties: density, temperature

**MODEL FOR VARIATIONAL ANALYSIS**

- Fuel element: NPP Obrigheim BE 124
- Burn up: 60 GWD/MTU
- Initial enrichment: 1.5%, 3%, 4.5%
- Fuel temperature: 900 K, 1800 K
- Moderator temperature: 556 K, 586 K
- Fuel density: 90%, 100% respective of the physical fuel density (Table II)
- Moderator density: 90%, 100% respective of the physical moderator density (Table II)

**KEY NUCLIDE** is such a radionuclide that can be detected easily through its characteristic gamma rays by means of non-destructive methodology (Cs-134, Cs-137, Eu-154).

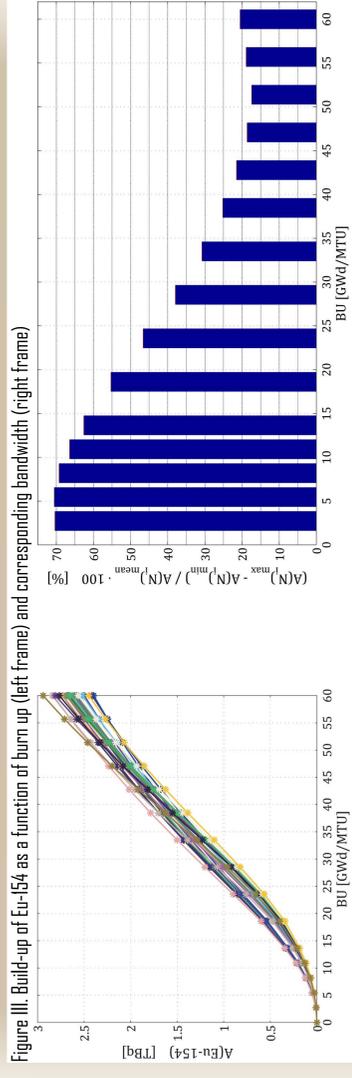


Figure III. Build-up of Eu-154 as a function of burn up (left frame) and corresponding bandwidth (right frame)

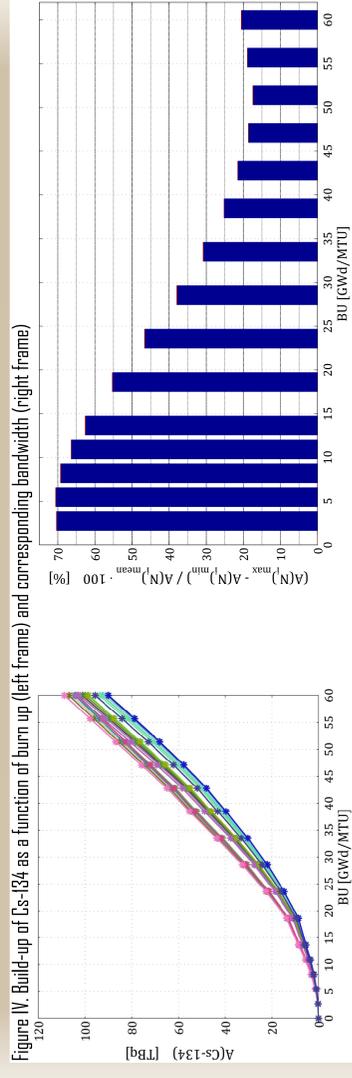


Figure IV. Build-up of Cs-134 as a function of burn up (left frame) and corresponding bandwidth (right frame)

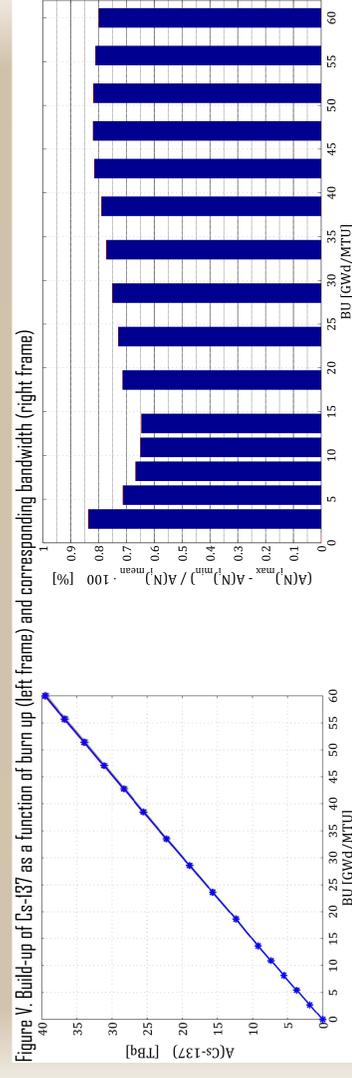


Figure V. Build-up of Cs-137 as a function of burn up (left frame) and corresponding bandwidth (right frame)

## BURN UP CORRELATION

### Eu-154/Cs-137

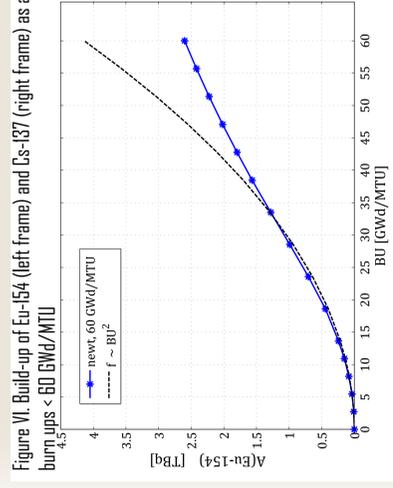


Figure VI. Build-up of Eu-154 (left frame) and Cs-137 (right frame) as a function of burn up. Calculations are performed with SCALE 6.1 using newt model for burn ups < 60 GWD/MTU

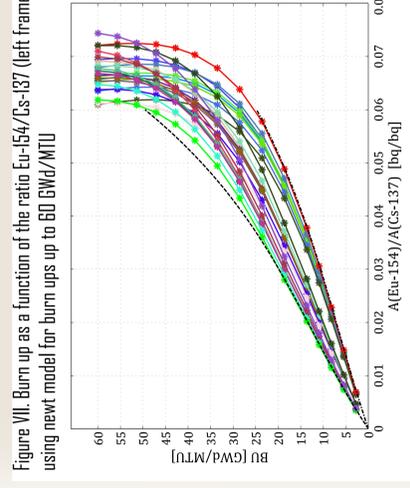


Figure VII. Burn up as a function of the ratio Eu-154/Cs-137 (left frame) and the corresponding bandwidth (right frame). Calculations are performed with SCALE 6.1 using newt model for burn ups up to 60 GWD/MTU

## COOLING TIME CORRELATION

### Eu-154/Cs-134

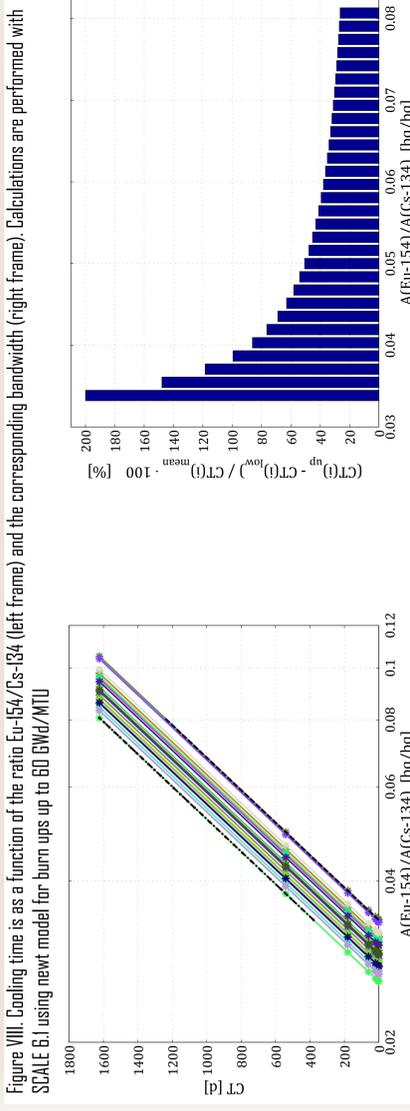


Figure VIII. Cooling time as a function of the ratio Eu-154/Cs-134 (left frame) and the corresponding bandwidth (right frame). Calculations are performed with SCALE 6.1 using newt model for burn ups up to 60 GWD/MTU