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Investigation of the Impact on Tungsten of Transient Heat Loads induced by Laser Irradiation, Electron Beams and Plasma Guns

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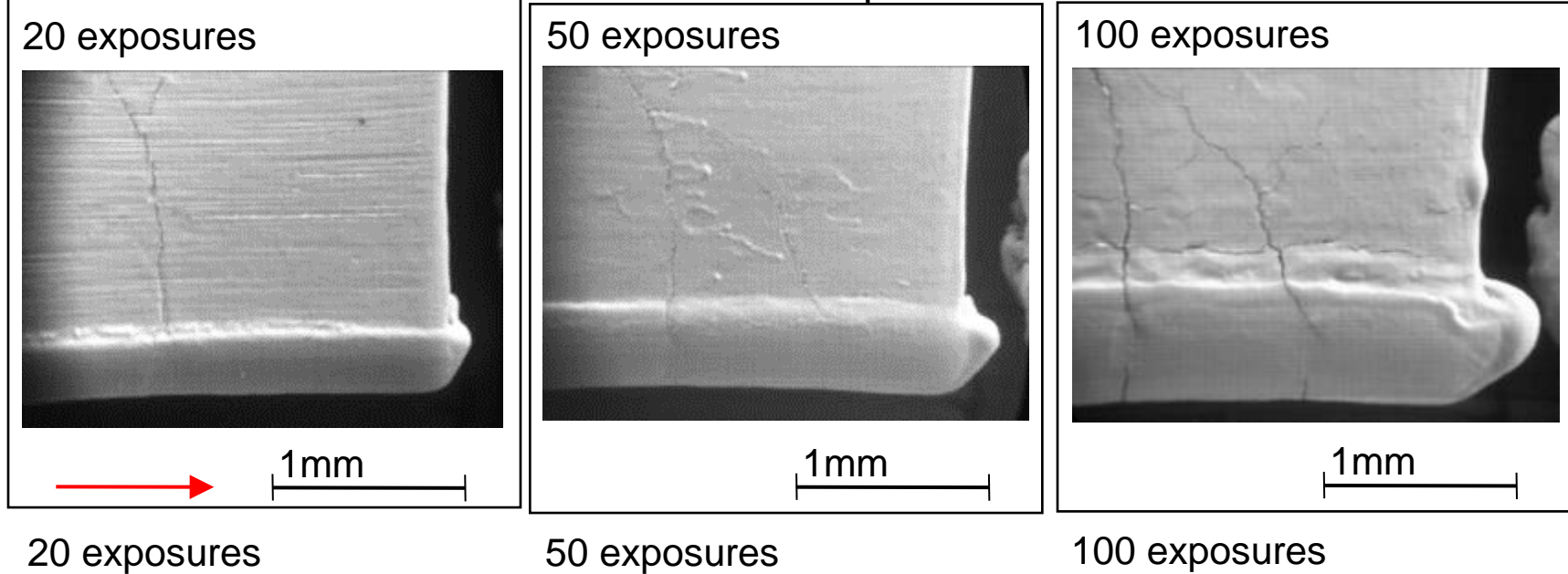
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- **Motivation**
- **Methods for simulation of transient thermal shock events**
- **Comparison of different methods**
 - Parameters relevant to cracks
 - Surface Morphology after transient heat loads
- **Future Plans and experiments**
 - Laser heat load experiments (without plasma background)
 - Transient heat load experiments with plasma background.
- **Summary**

N. Klimov, SRC RF TRINITI, QSPA ELM experiment $Q=0.7\text{MJ/m}^2$

Pure tungsten

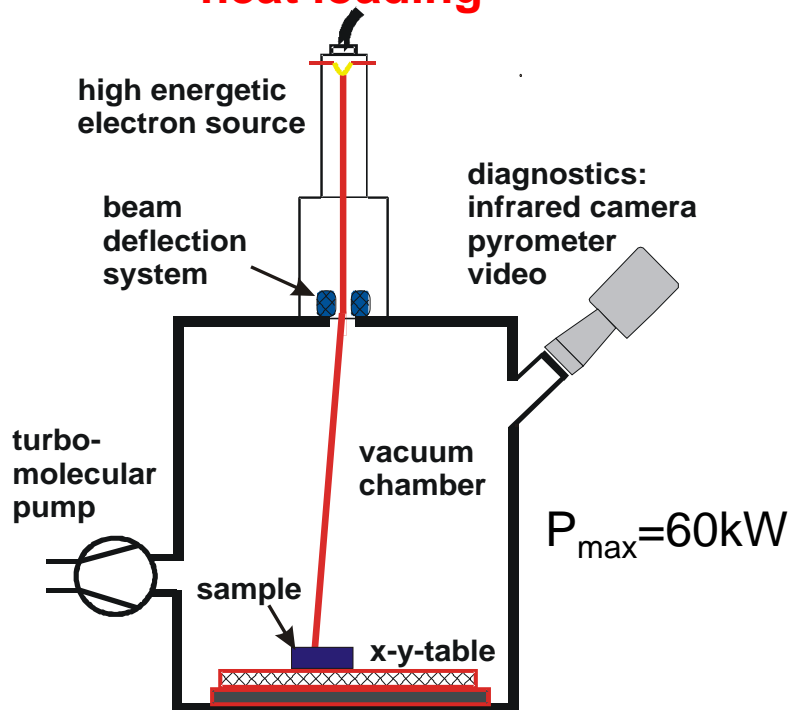


Strong Erosion for Energies beyond 0.5 MJ/m^2 for 0.5ms heat pulse duration

Estimates indicate that the ELM energy fluxes must remain below $\sim 0.5 \text{ MJm}^{-2} / \text{ELM}$ at the ITER divertor targets. This implies an ELM energy loss, $\Delta W_{\text{ELM}} \sim 1 \text{ MJ} \rightarrow \sim 0.3\%$ of the stored energy in an ITER $Q_{\text{DT}} = 10$ burning plasma!

A. Loarte et al., "Power and particle fluxes at the plasma edge of ITER : Specifications and Physics Basis", Nuclear Fusion... [Proc. 22nd IAEA Fusion Energy Conference, Geneva, Switzerland (2008)]

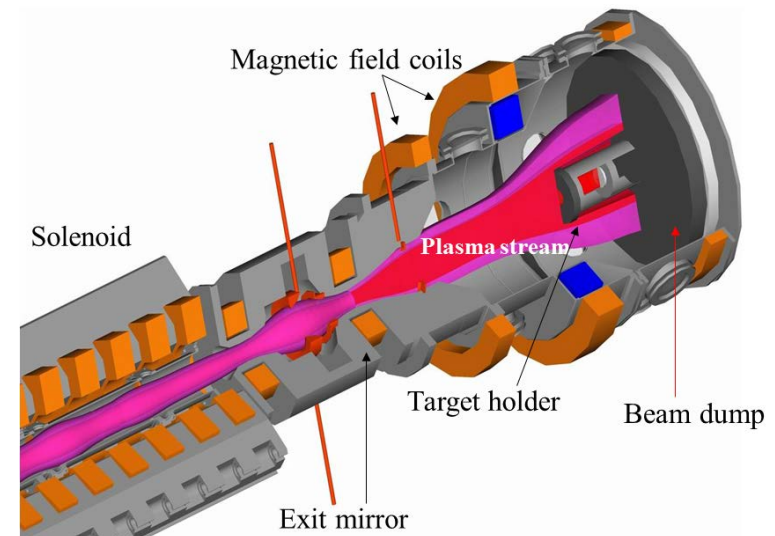
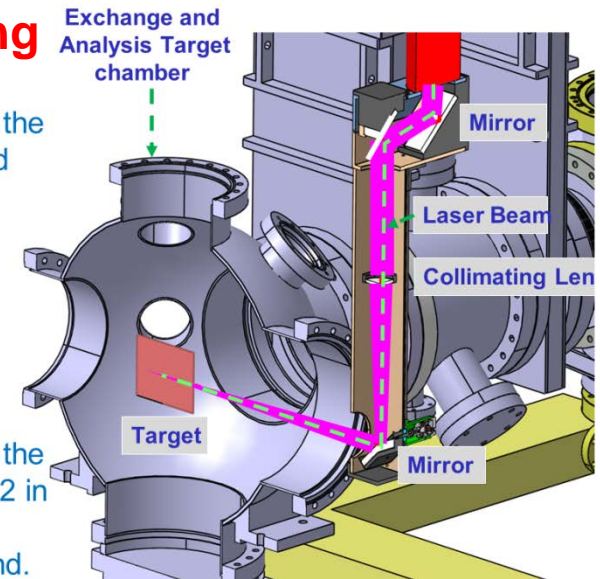
JUDITH 1 facility: volumetric (several μm) heat loading



$P = 0.19 \div 1.51 \text{ GW/m}^2$, pulse duration of 1ms. (ITER: max. $W_{\text{th}}^{\text{ELM}} = 0.5\text{MJ/m}^2$)

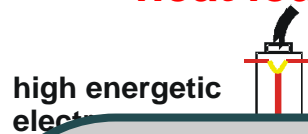
LASER System: surface heat loading

- Measurements of the transient heat load without plasma background
- Measurements of the heat loads in PSI-2 in the presence of a plasma background.



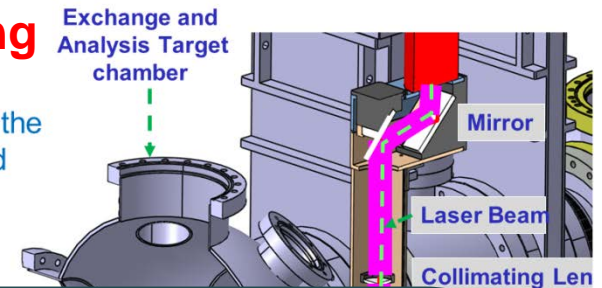
JUDITH 1 facility:

**volumetric (several μm)
heat loading**



**LASER System:
surface heat loading**

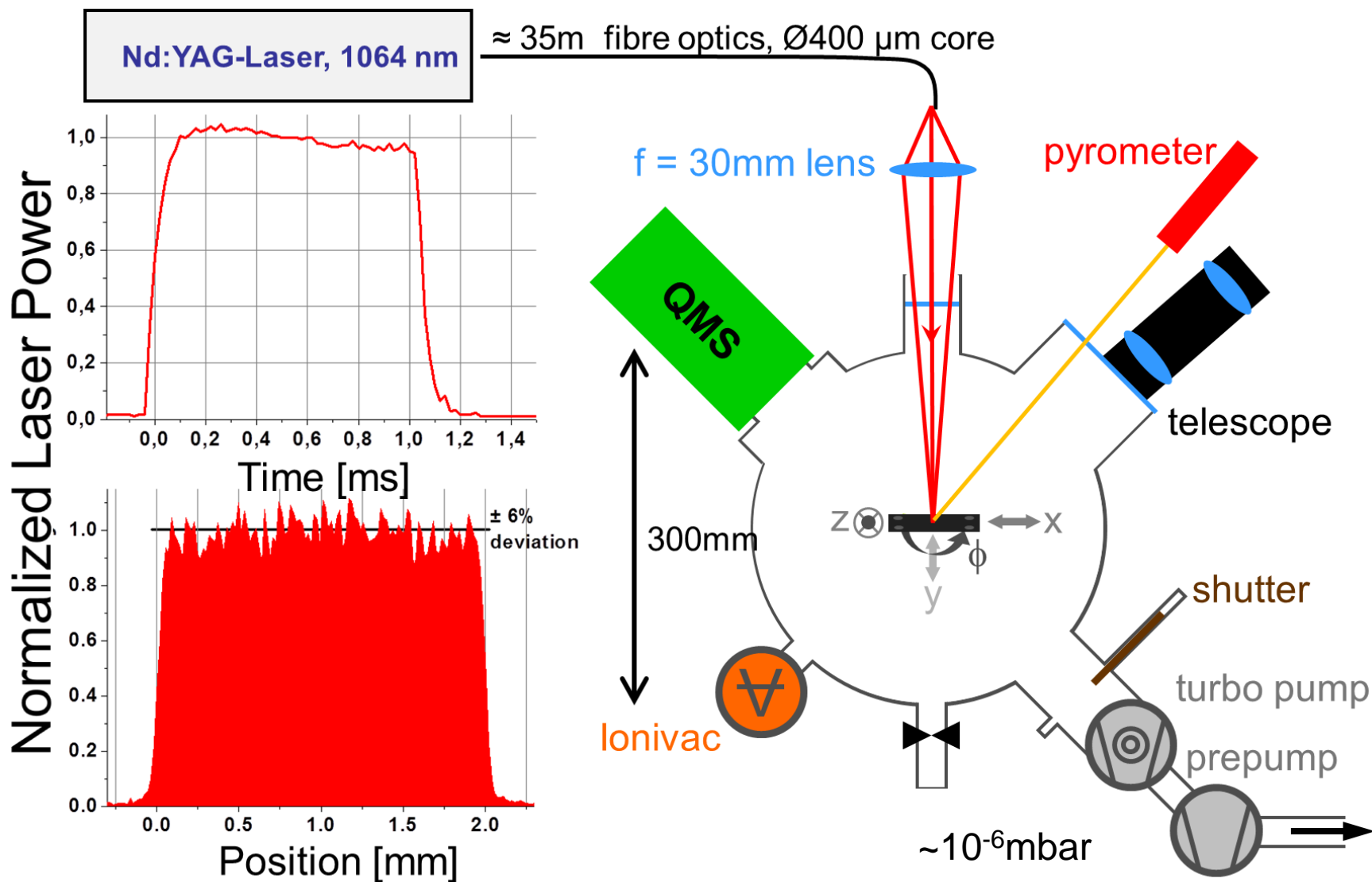
- Measurements of the transient heat load without plasma background



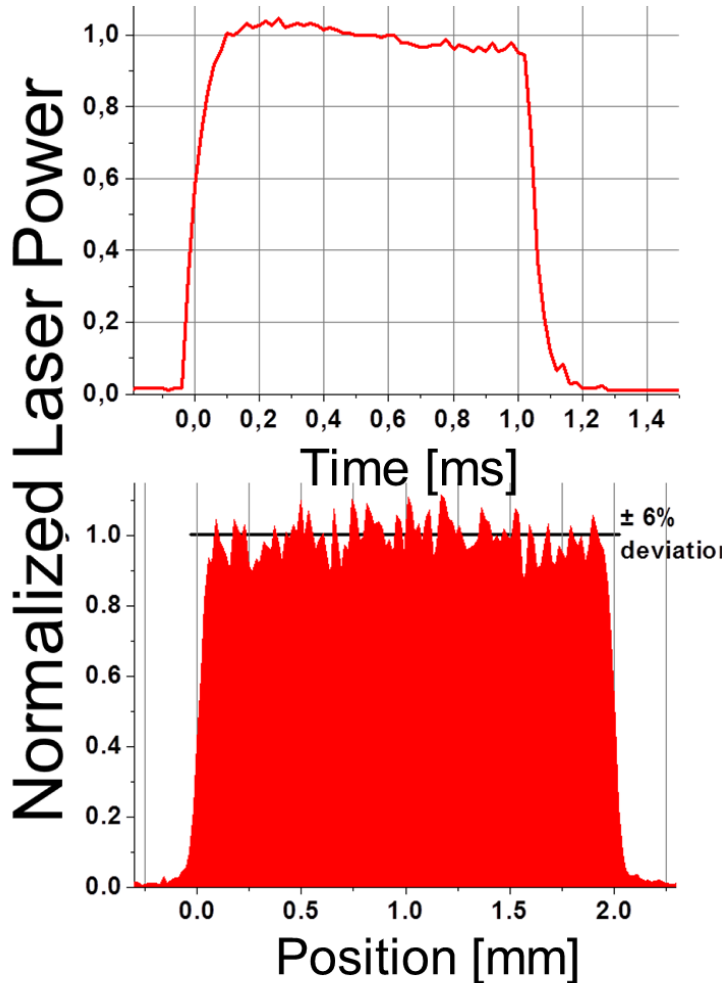
We wanted to know whether the laser method is comparable with the other ones

- the laser **pulse rate** can indeed be **much higher** and there is practically **no limit** to the overall **number of pulses**.
- Moreover, it is possible with the laser to **combine the transient heat loads with a steady state plasma exposure**.





Nd:YAG-Laser, 1064 nm $\approx 35\text{m}$

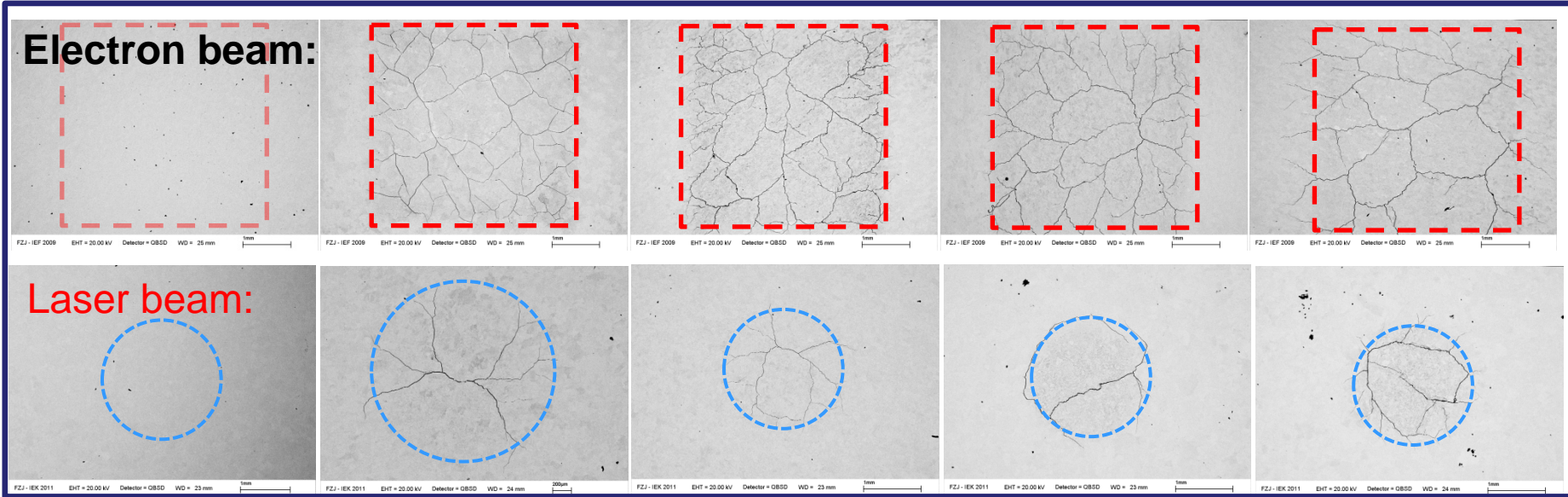


Standard settings for thermal loads:

1 ms pulse duration:
nearly square function

2 mm laser beam diameter
nearly hat top shape

0.5 Hz repetition rate
Heat power up to 1.5 GW/m^2
heat flux factor: $I\sqrt{t} = 47$
 $\text{MW}\sqrt{\text{s/m}^2}$



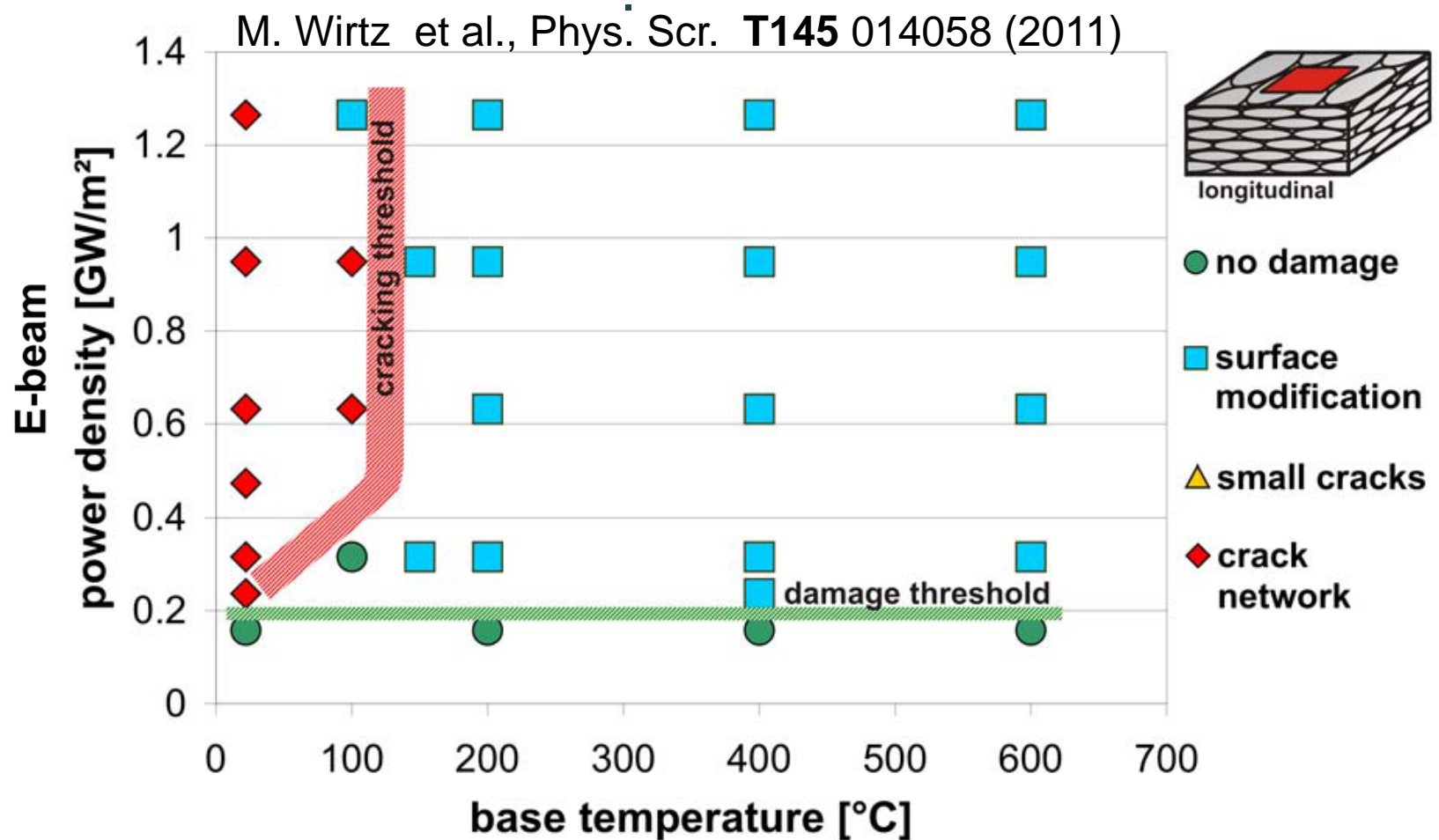
0.19 GW/m² 0.38 GW/m² 0.76 GW/m² 1.14 GW/m² 1.51 GW/m²
 (absorbed intensity)

Cracking patterns are very similar !!!

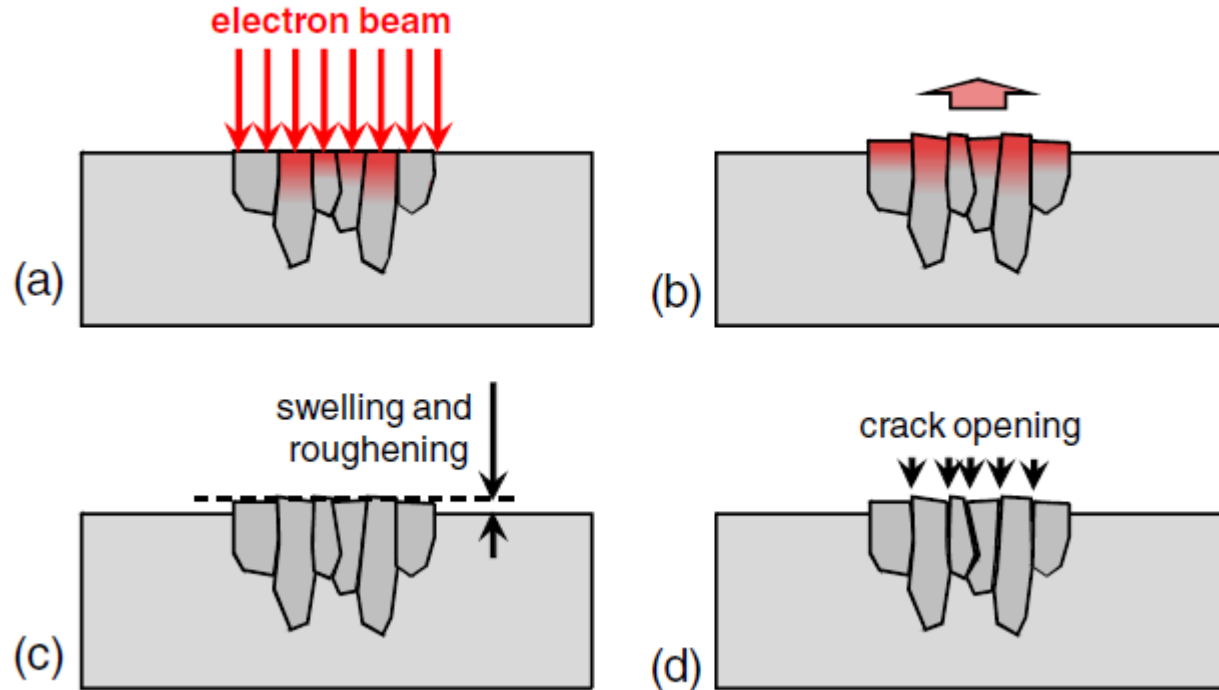
- At $P = 0.19 \text{ GW/m}^2$ there are no cracks after repetitive electron as well laser loadings.
- Cracks network for $P \geq 0.38 \text{ GW/m}^2$ for both methods

Samples:

- Industrially manufactured single forged tungsten grade W-UHP (ultra-high-purity tungsten) with a purity of 99.9999 wt%.
- The base temperature of W samples around room temperature

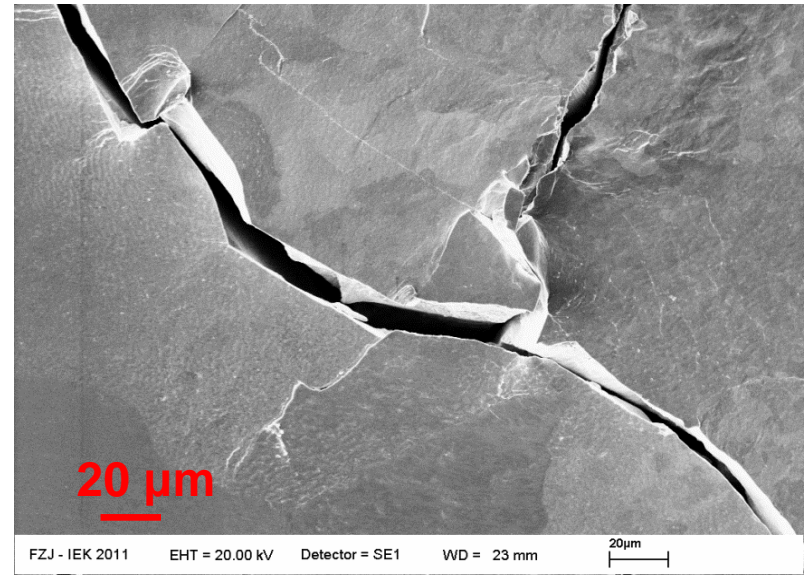
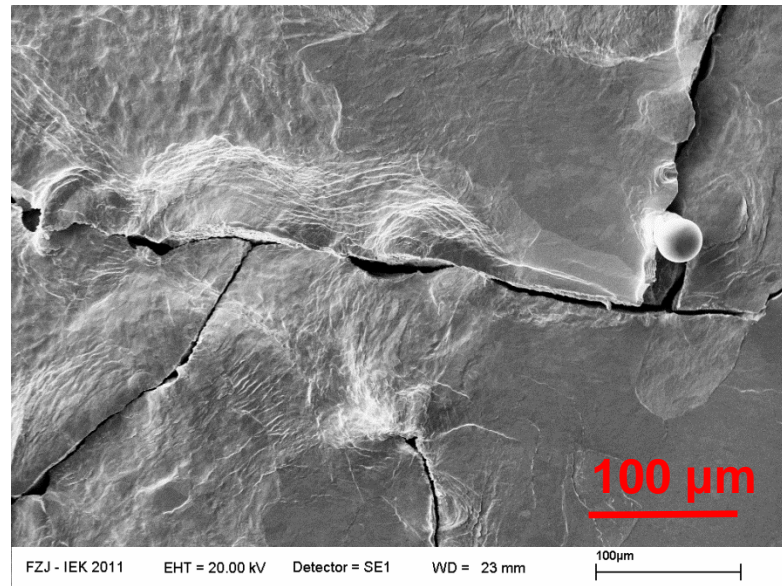
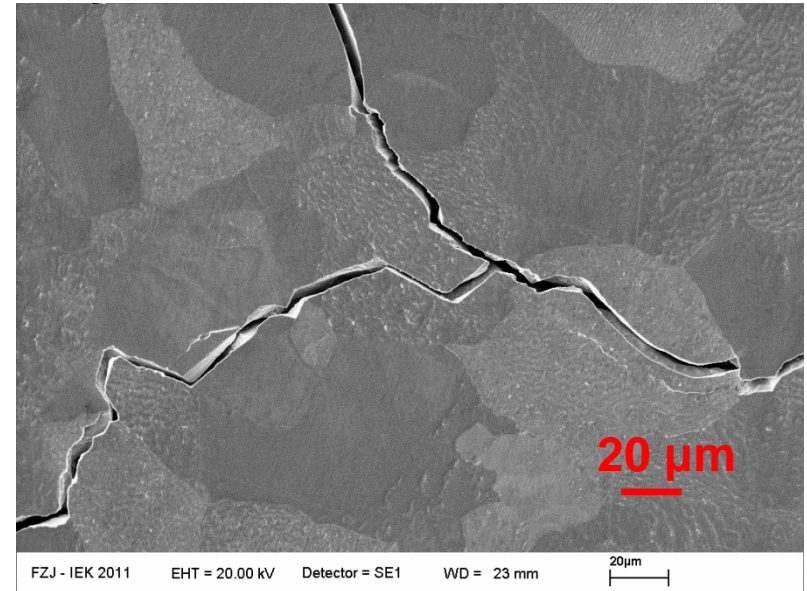
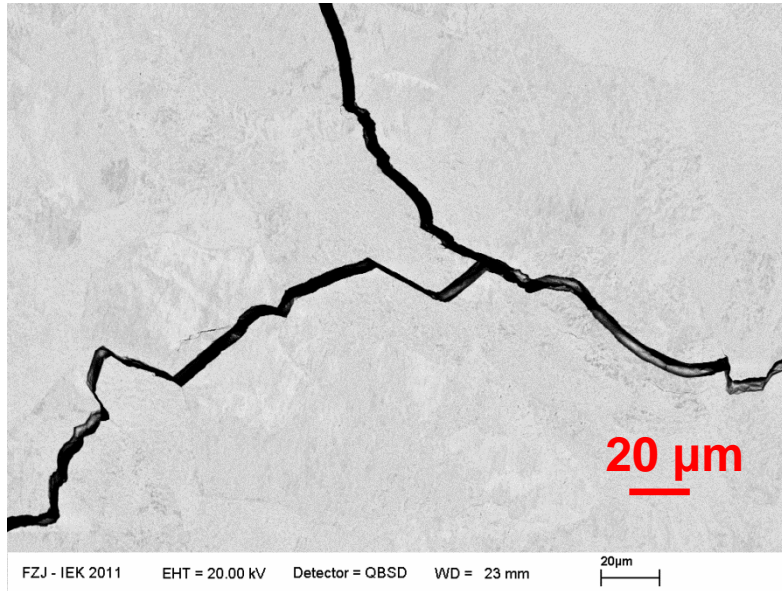


Below 0.16 GWm⁻² no visible damage appears. Above a base temperature of 100 °C only surface modification occurs.



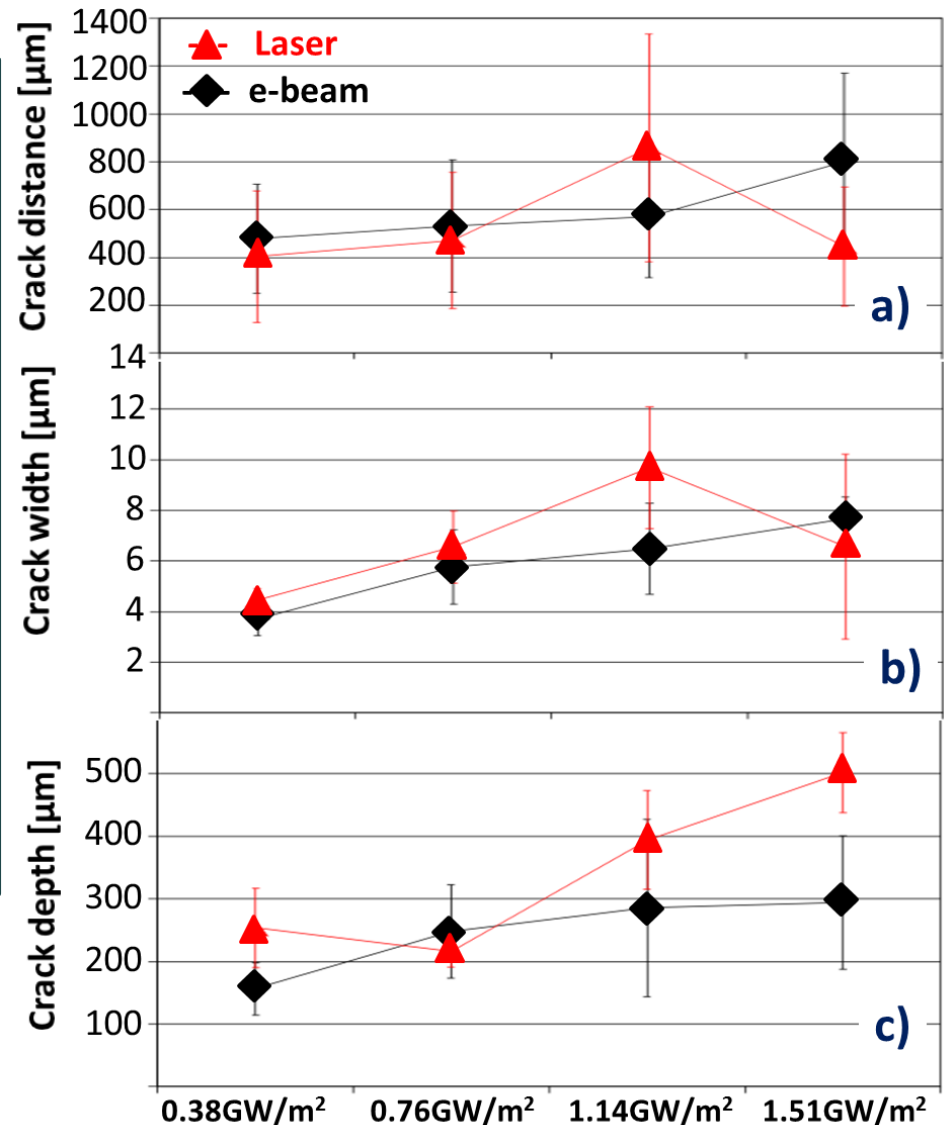
J. Linke et al. Nucl. Fusion 51 (2011) 073017

**Cracks with an orientation parallel to the heated surface =>
subsequent delamination effects =>
overheating, melting and complete loss of the detached layer.**



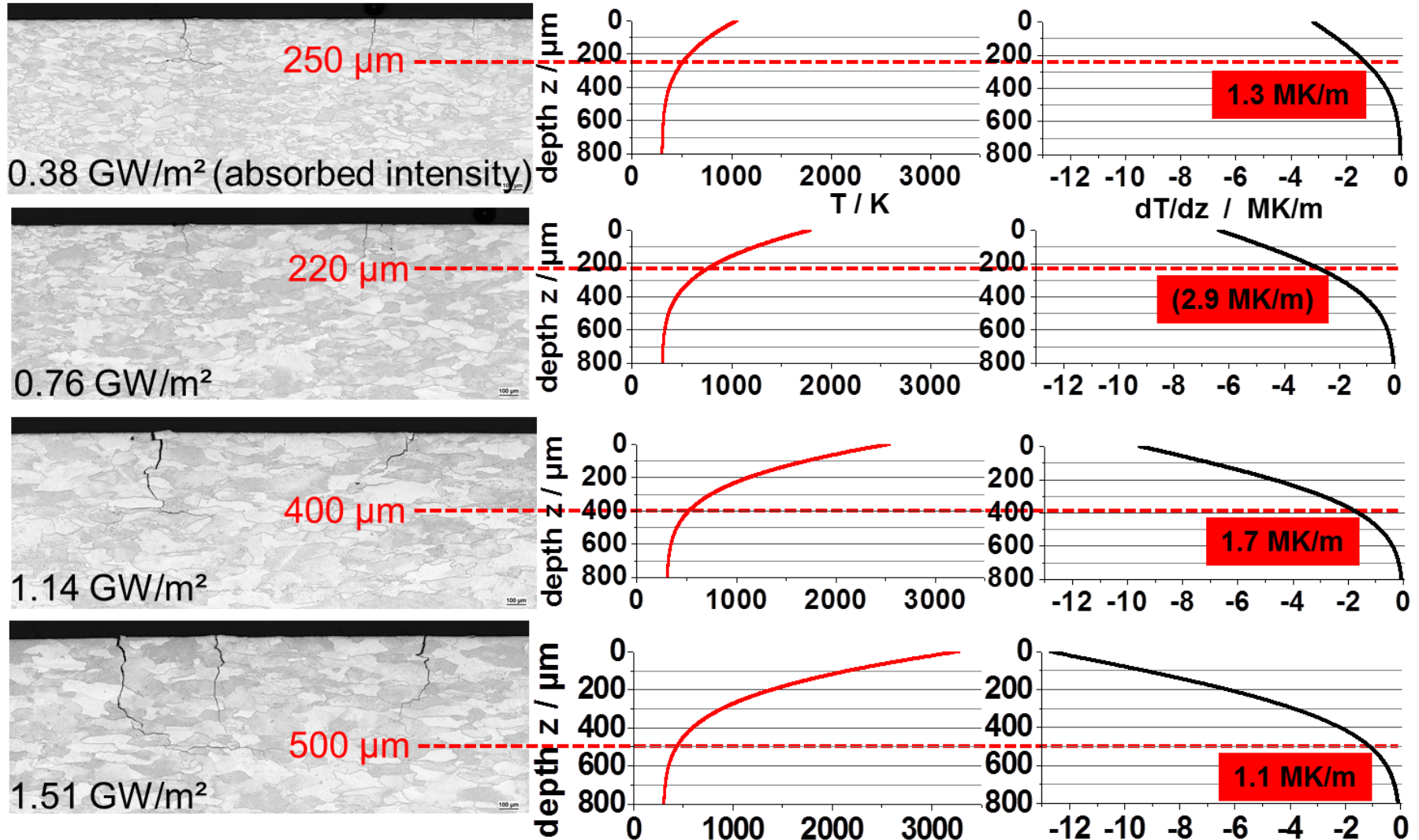
- Independently of loading methods, all observed crack parameter values increase with power density.
- Cracks extend perpendicularly to the irradiated surface to a depth of 100-500 μm .
- The observed crack width varied between 4 and 10 μm .
- The cracks form a network with a distance between cracks in the order of 0.4-1.0 mm.

**Cracking patterns parameters
are very similar !!!**



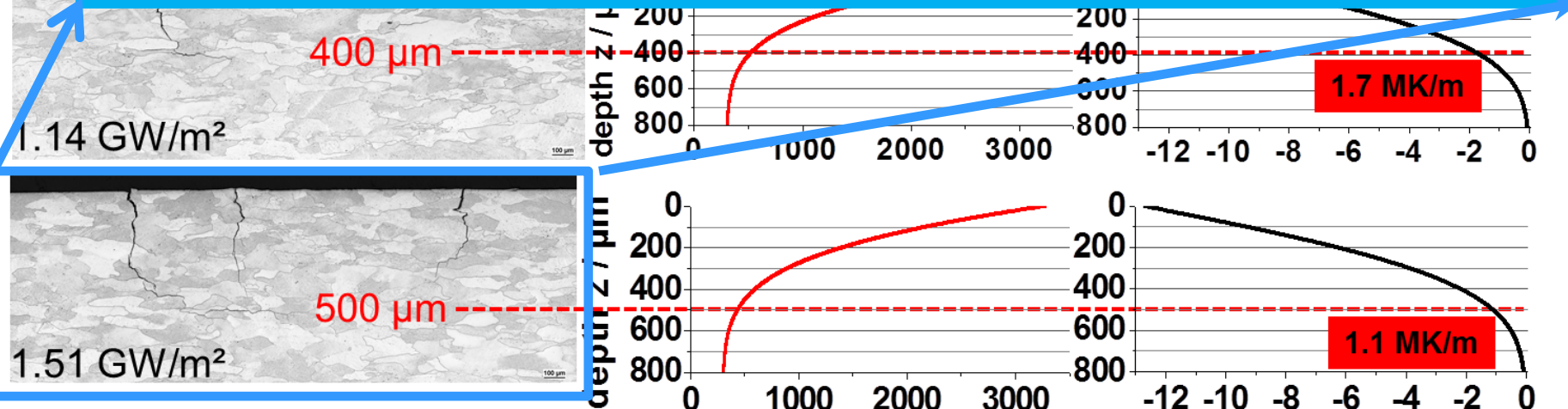
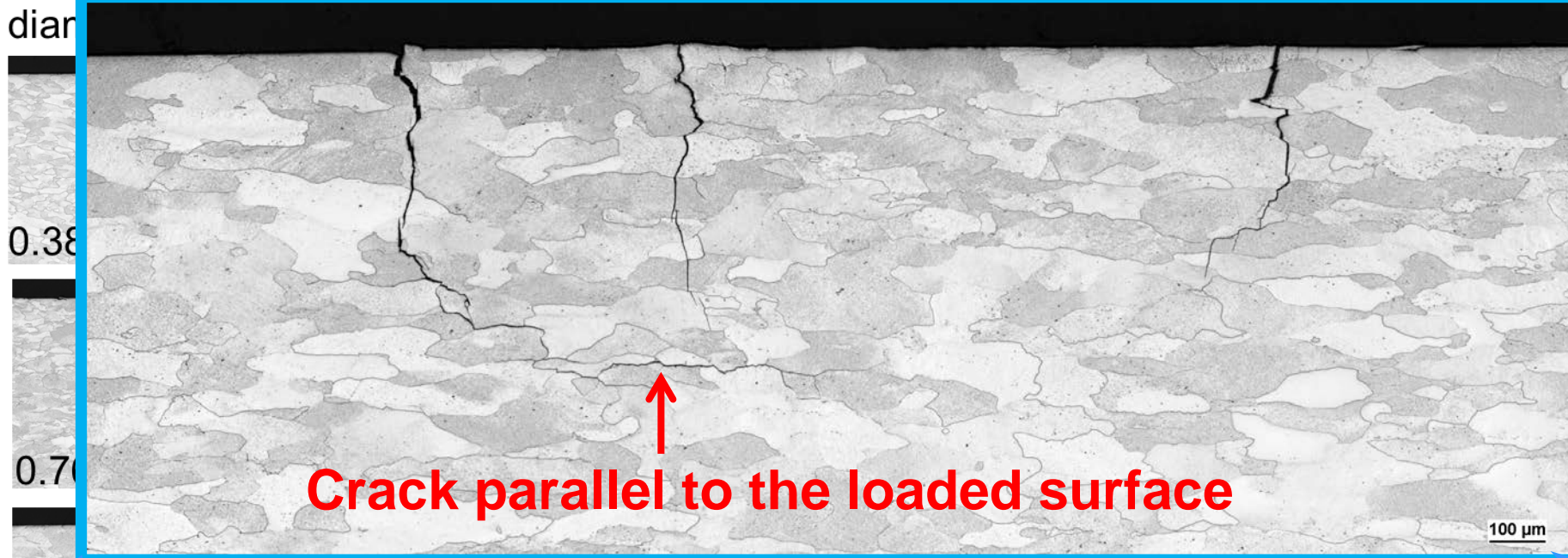
100 laser pulses of 1 ms, 2 mm diameter, 0.5 Hz, polished W (Plansee)

explanation: crack formation in an area with temperature gradient $< -1.3 \text{ MK/m}$



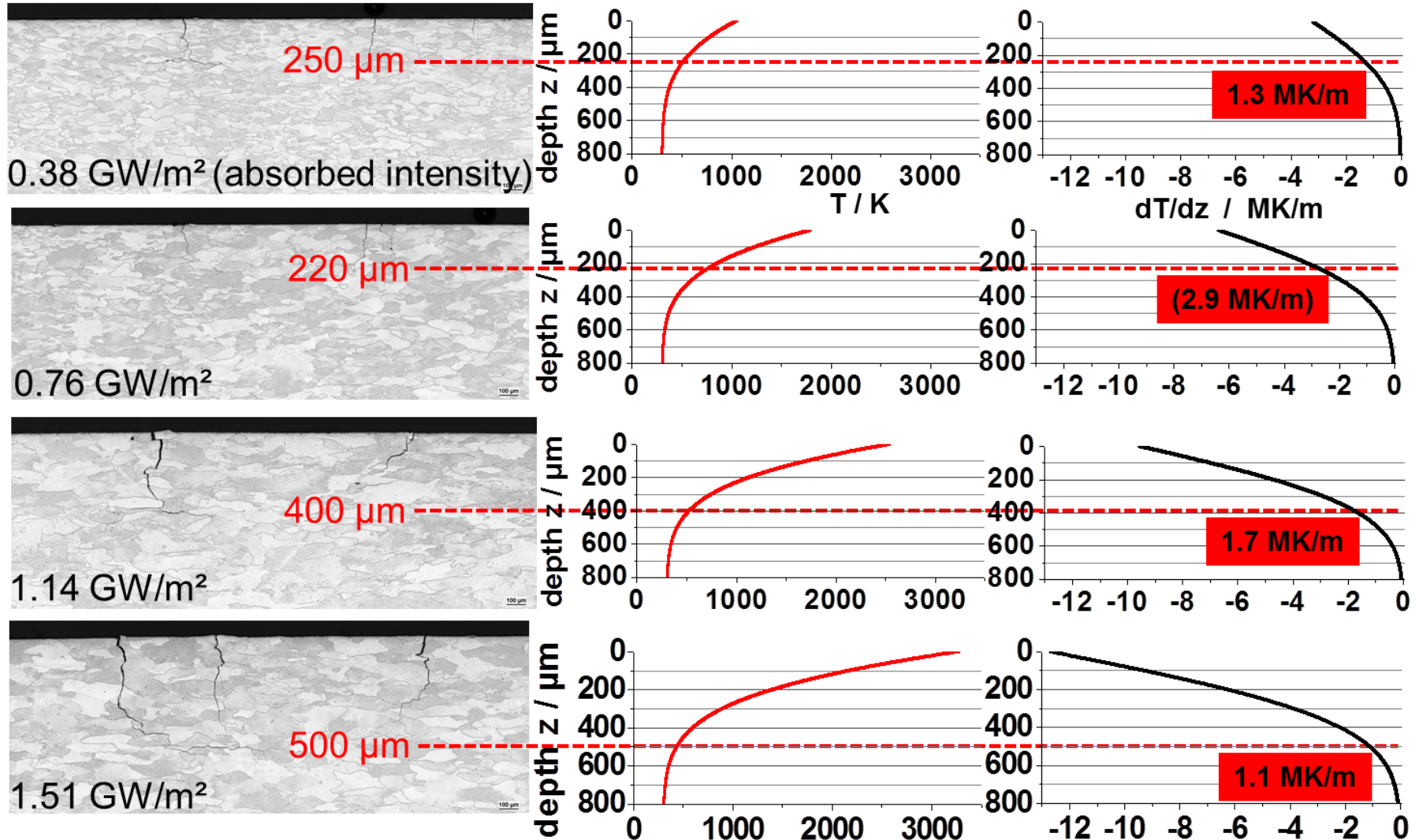
100 laser pulses of 1 ms, 2 mm

explanation: crack formation in an area

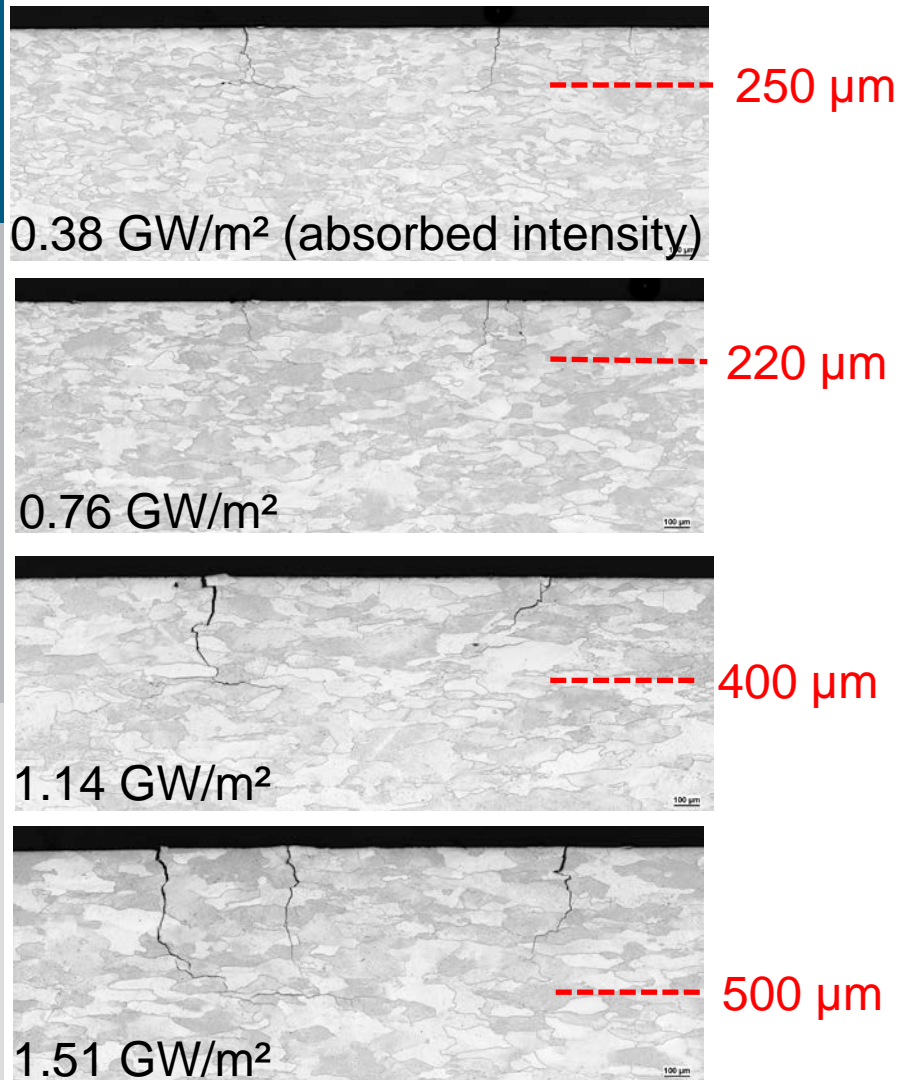


100 laser pulses of 1 ms, 2 mm diameter, 0.5 Hz, polished W (Plansee)

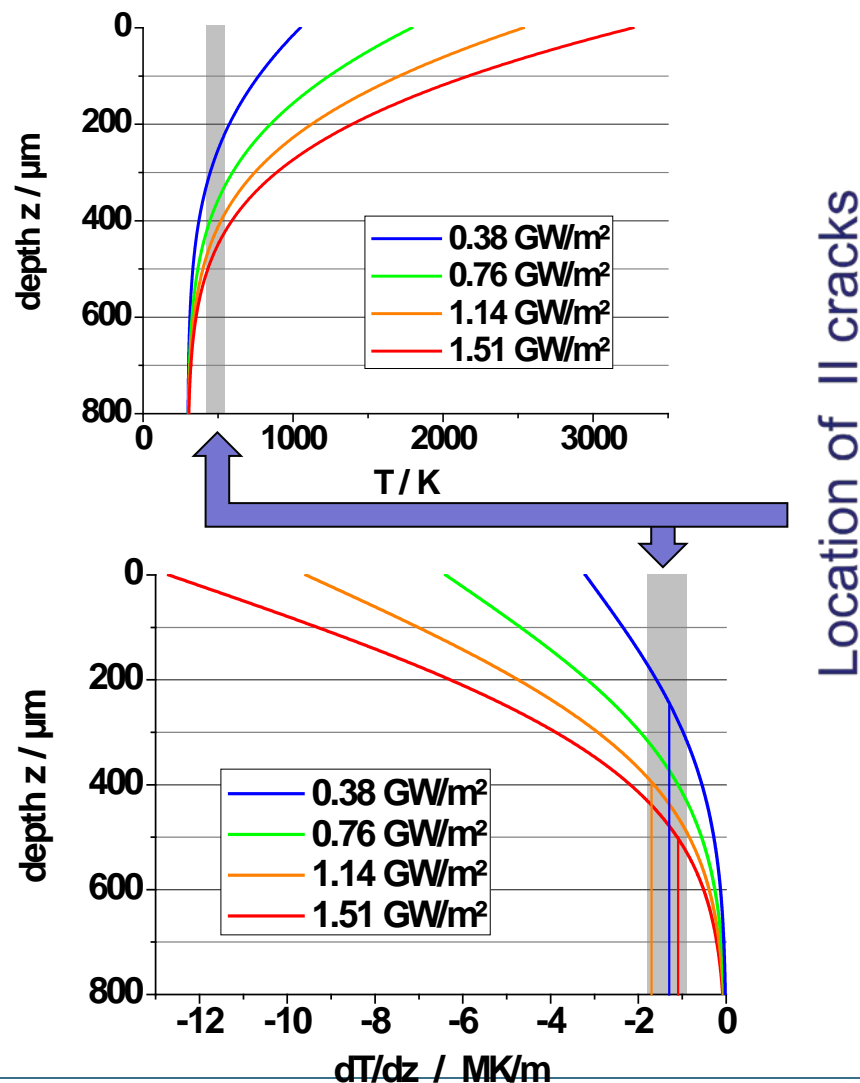
explanation: crack formation in an area with temperature gradient $< -1.3 \text{ MK/m}$

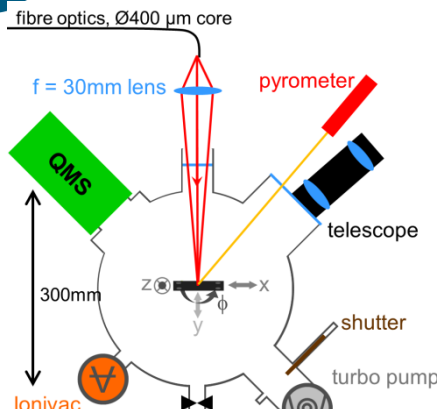


100 laser pulses of 1 ms, 2 mm diameter, 0.5 Hz, polished W (Plansee)

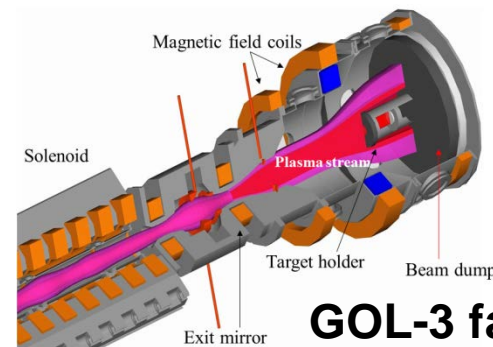


explanation: crack formation II to the surface in an area with $T \sim 500$ K –around DBTT – and a temperature gradient of 1.3-1.7 MK/m.

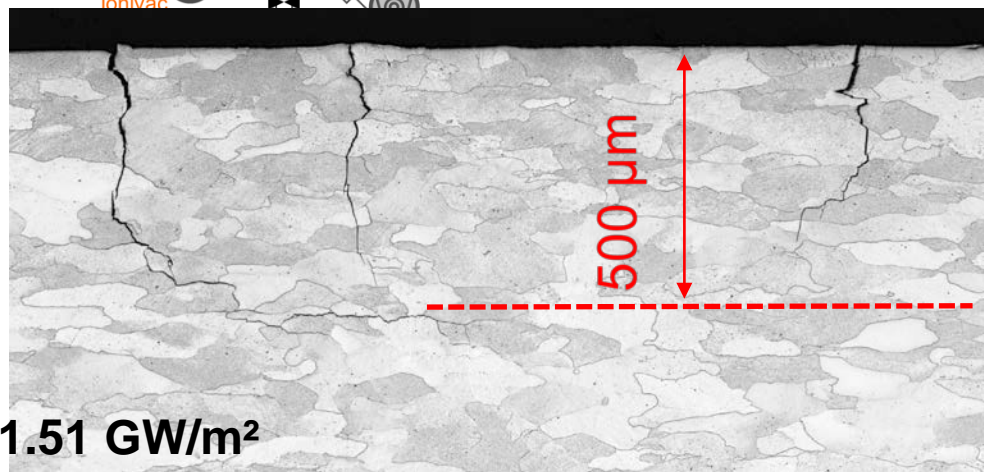




Laser irradiation

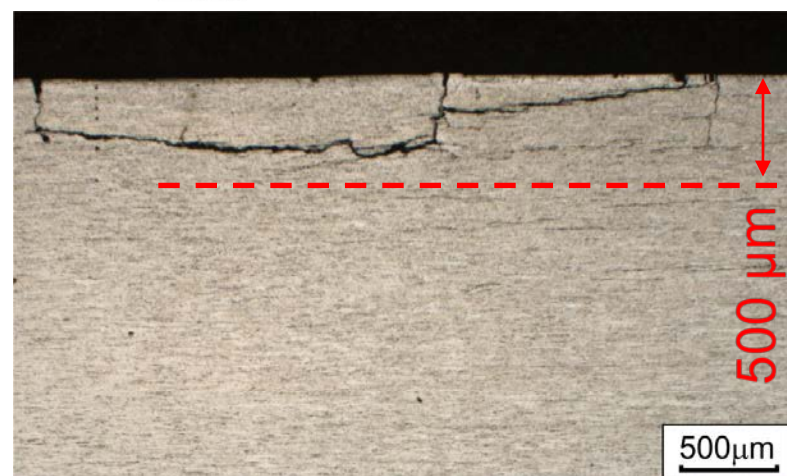


GOL-3 facility



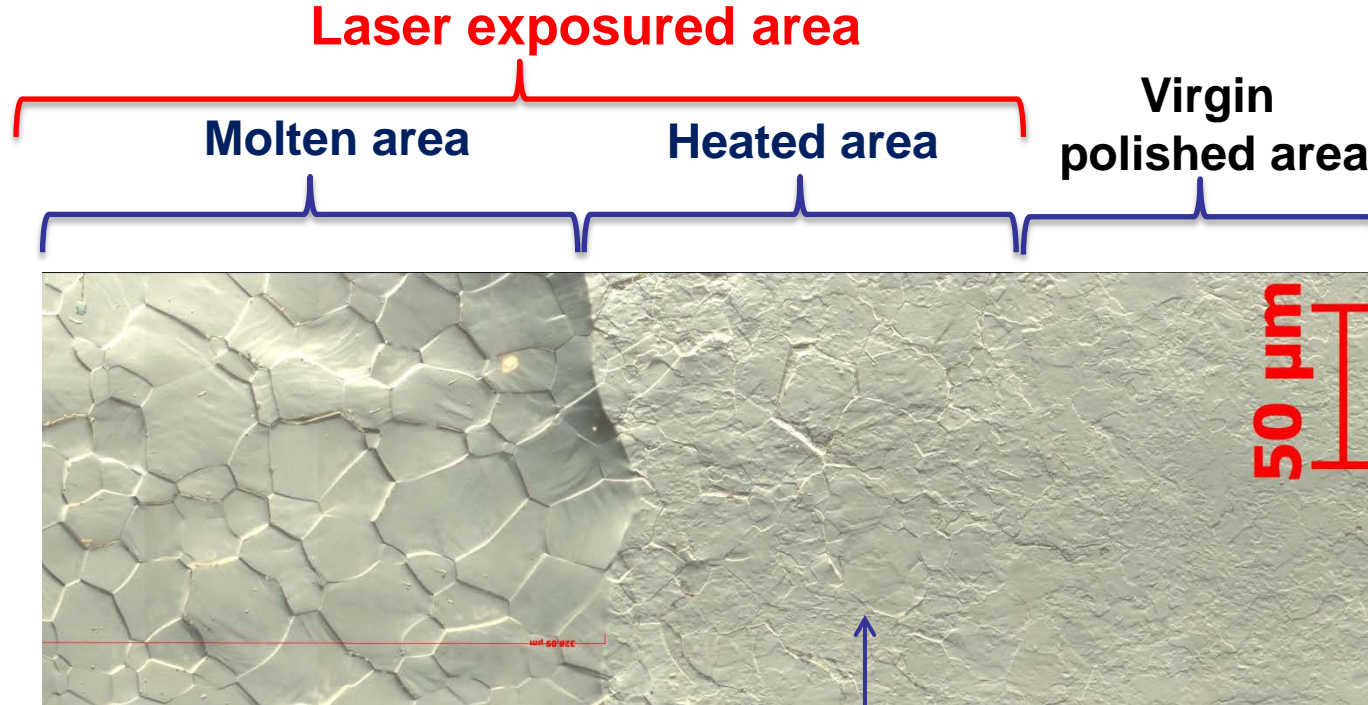
1.51 GW/m²

100 laser pulses of 1 ms, 2 mm diameter, 0.5 Hz, polished W (Plansee)



Crack propagation in the surface layer of the irradiated tungsten sample in GOL-3 2MJ/m²

Similar crack parameters have been observed by transient heat loads simulations in the linear plasma device GOL-3



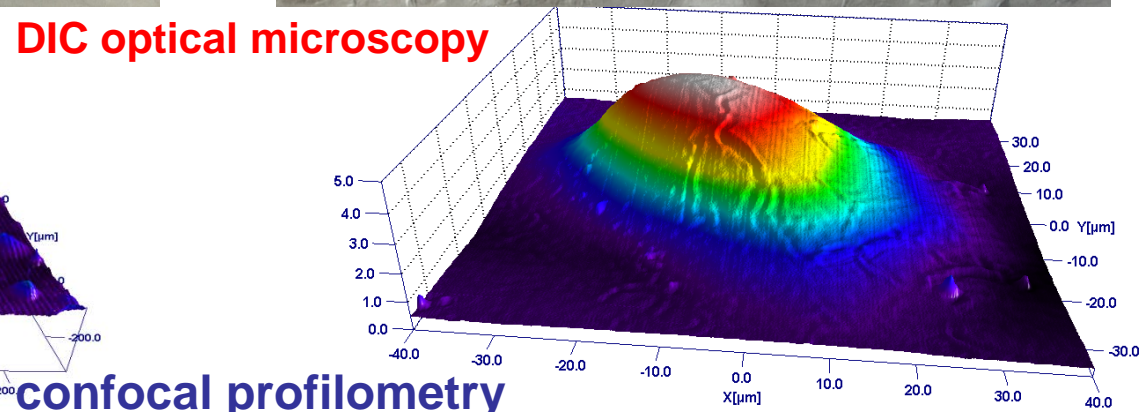
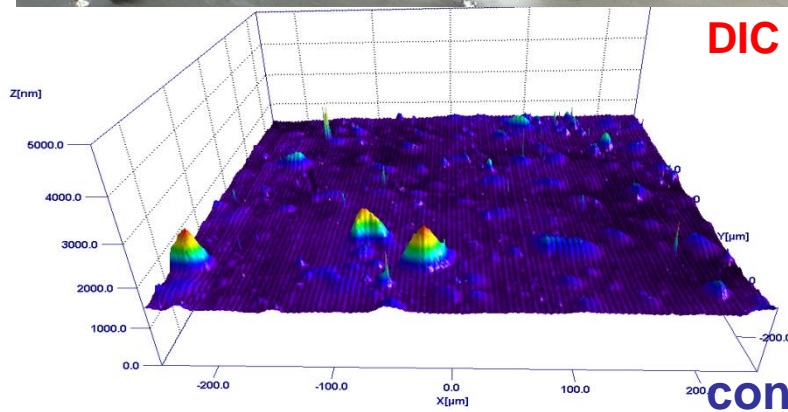
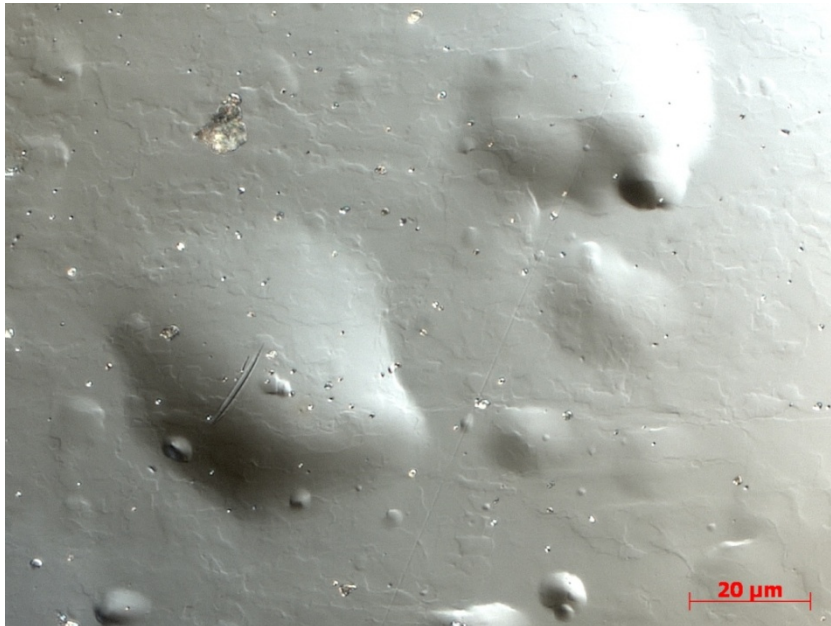
Polycrystalline, rolled tungsten
(Goodfellow, 99.95 wt.% purity)

DIC optical microscopy

- Roughness increased by thermal shock loads: rougher in the melted area
- Roughness formation is independent of the loading methods.
- At $P = 0.19 \text{ GW/m}^2$ there are no formation of roughness structure
- Beyond 0.2 GW/m^2 : the surface roughening increase up to $2 \mu\text{m}$ with $P \uparrow$

Before laser pulse: W with blisters due to D implantation: (fluence $6 \times 10^{24}/\text{m}^2$, 480 K) up to 1 μm blister height

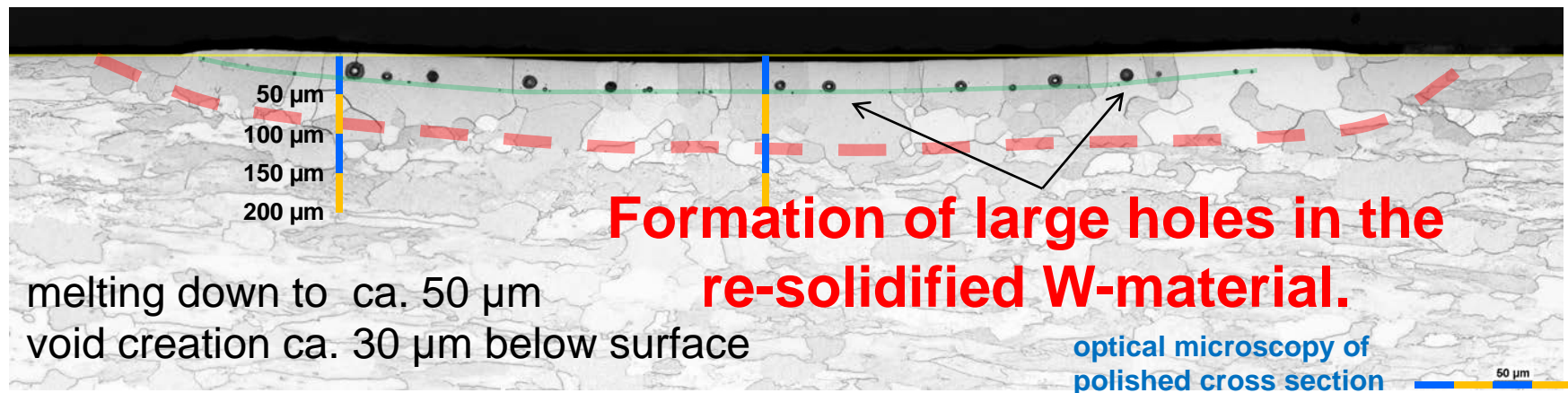
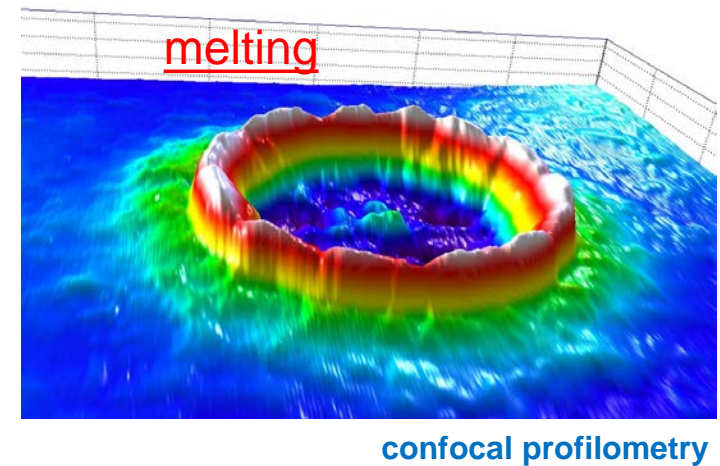
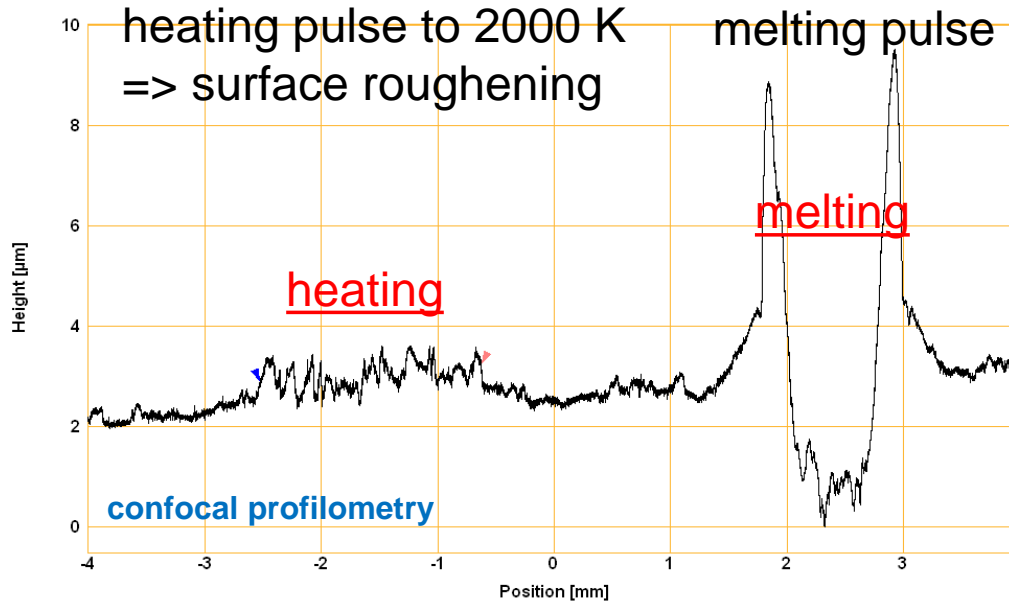
After laser heating pulse ($500\text{MW}/\text{m}^2$, 3ms duration, 2 pulses): blisters grow up to 4 μm , grain swelling due to thermal expansion



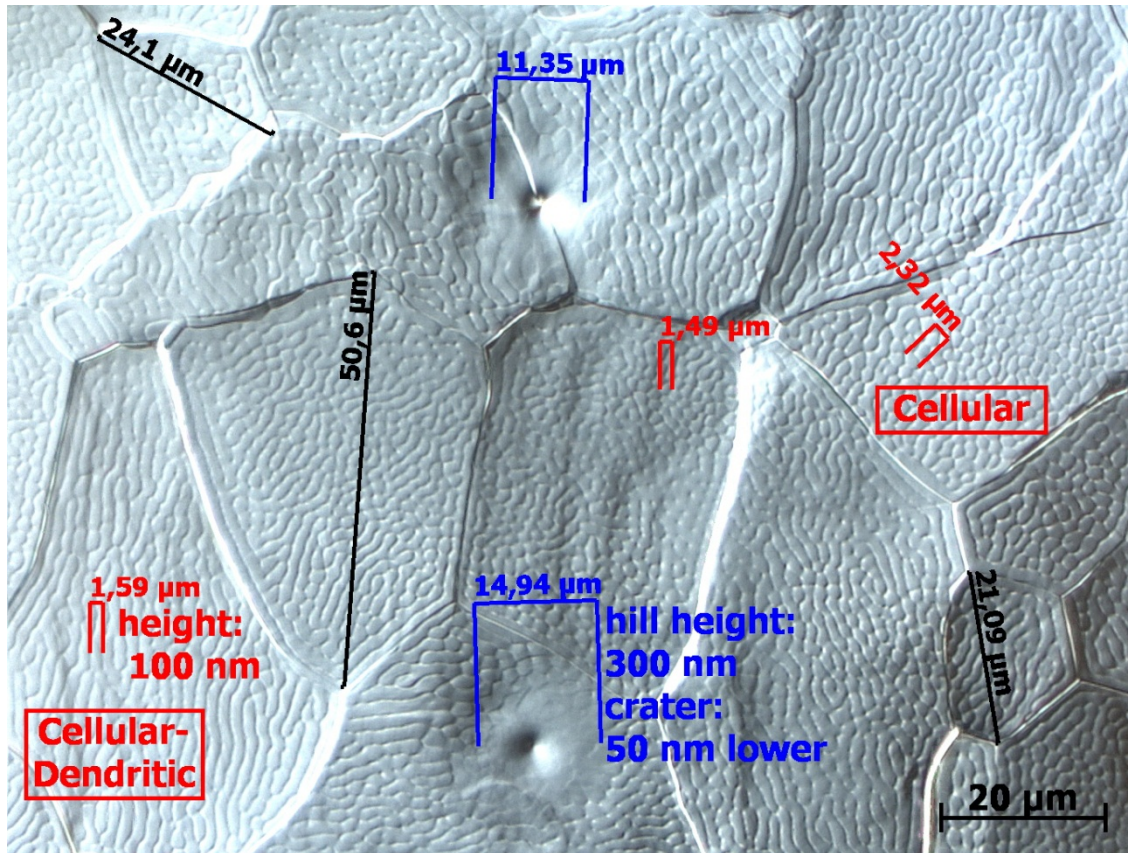
DIC optical microscopy

confocal profilometry

Surface profile of polished W after heating pulse (left) and melting pulse (right)



The area after the melted laser pulse



DIC optical Microscopy

- The surface exhibits predominantly cellular structures inside the grains (due to surface stresses)

Rapid cooling of thin melted layers

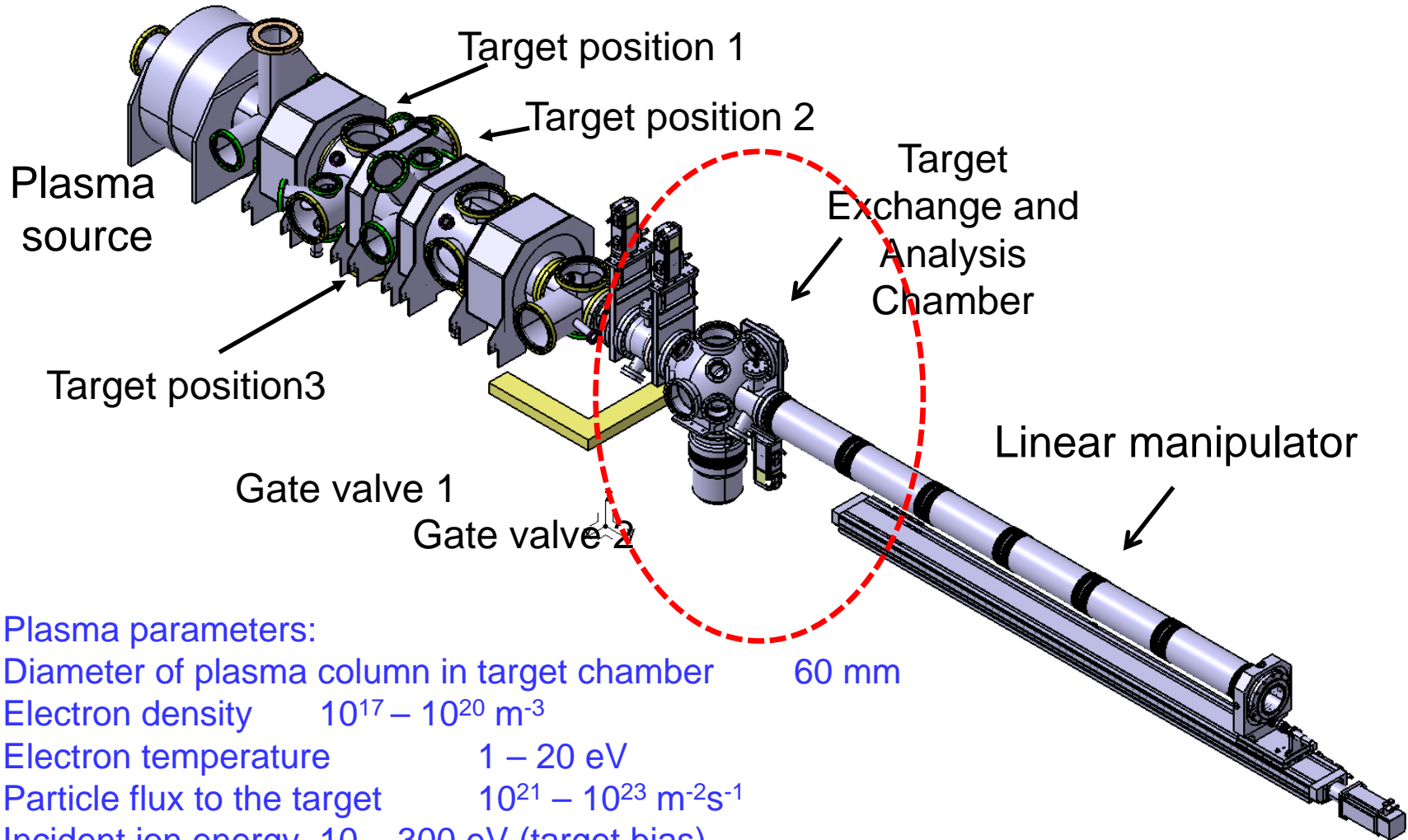


The surface material turns into a solid very quickly.



Rapid Solidification

Future plans for ELM simulation Experiments in PSI-2

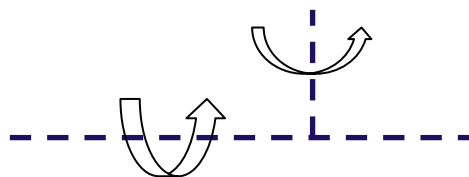


Plasma parameters:

Diameter of plasma column in target chamber	60 mm
Electron density	$10^{17} - 10^{20} \text{ m}^{-3}$
Electron temperature	1 – 20 eV
Particle flux to the target	$10^{21} - 10^{23} \text{ m}^{-2}\text{s}^{-1}$
Incident ion energy	10 – 300 eV (target bias)
Min. neutral gas pressure in target chamber	10^{-2} Pa

Target Holder:

- rotatable
- heatable up to 600 °C
- with active cooling
- exchangeable

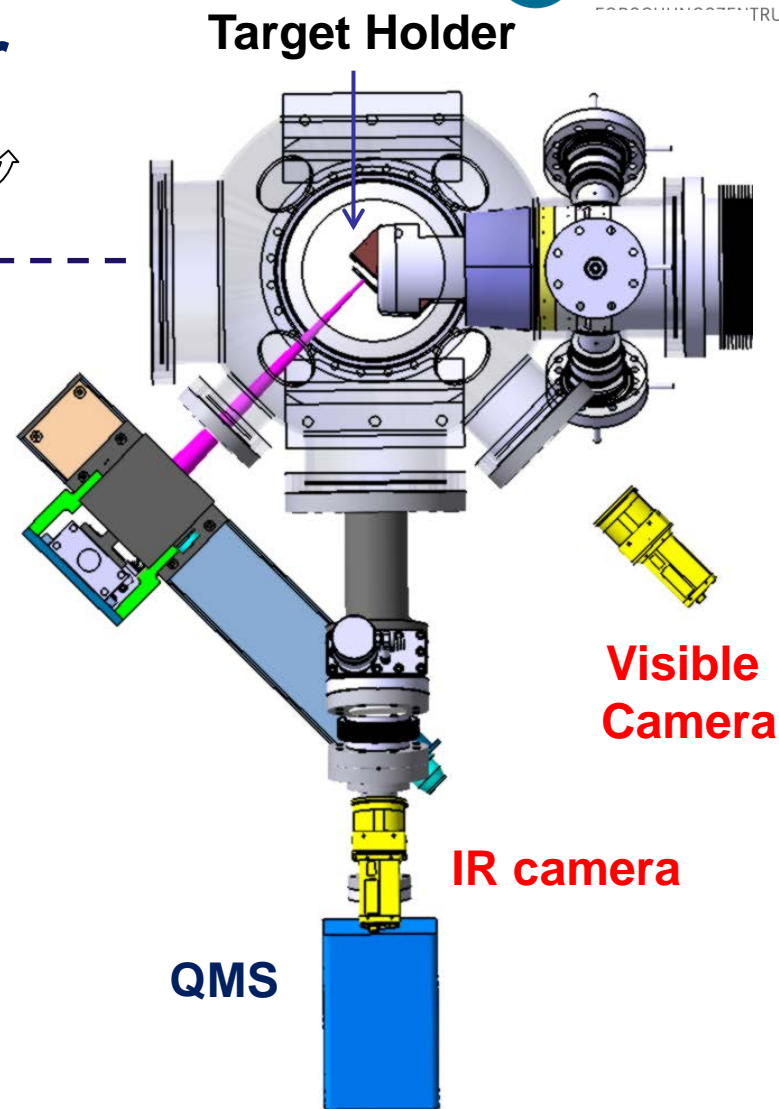


Laser injection unit

Laser heat load experiments:

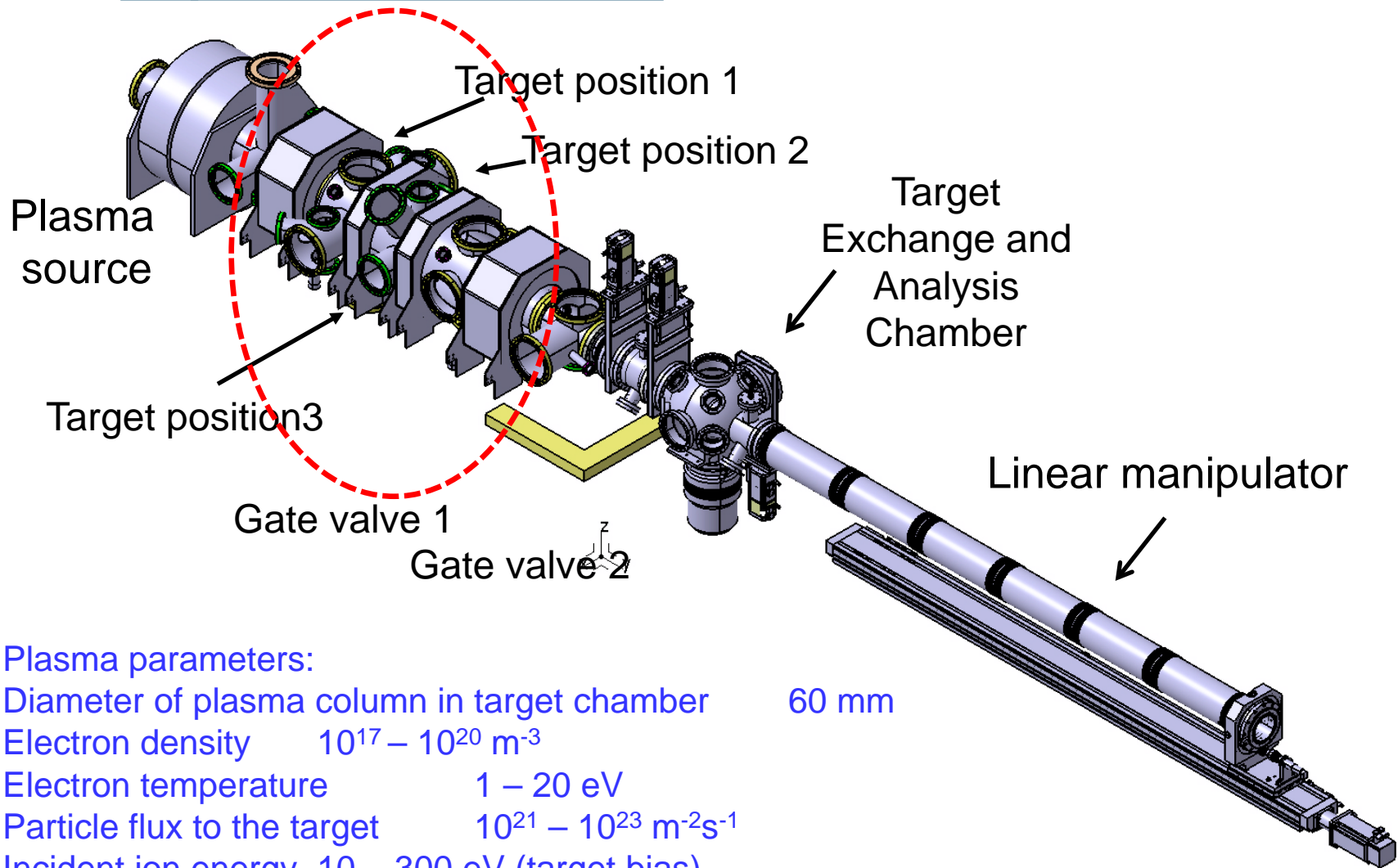
- Unexposed and
- Plasma pre-exposed samples

(without plasma background)



Without breaking the vacuum in the plasma chamber the probes can be removed easily for post mortem analysis.

Future plans for ELM simulation Experiments in PSI-2

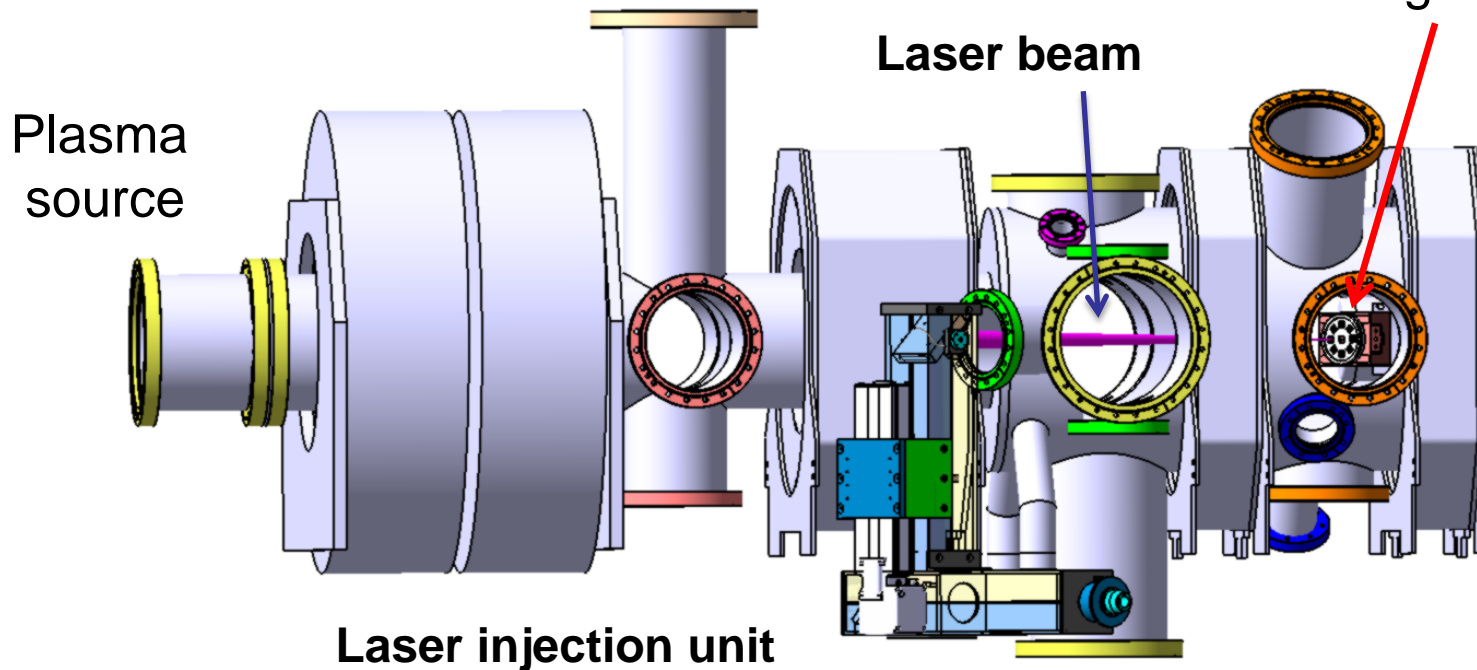


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Incident ion energy	10 – 300 eV (target bias)
Min. neutral gas pressure in target chamber	10^{-2} Pa

Target Holder:

- rotatable
- heatable up to 1600 °C
- with active cooling
- exchangeable



- Transient heat load experiments in the PSI-2 facility simultaneously to a steady state plasma exposure **(with plasma background)**.



- Volumetric loading with the electron beam (penetration depth in W in the μm range) has been compared with surface loading with the laser beam (22 nm light decay length) and plasma gun

- Results indicate that the different techniques show, in general, similar damage behaviours and the same damage thresholds

- The laser simulation is comparable to e-beam and plasma methods.

- Since the laser method is successful, one can use its advantages:
 - - no restrictions on pulse number (can be much higher than in other methods)
 - - can be applied simultaneously to a steady state plasma exposure



➤ Physics results:

- ❑ Independently of loading methods, observed crack parameter values increase with power density
- ❑ Cracks \perp to the irradiated surface: to a depth of 100-500 μm . width varied between 4 and 10 μm , distance between cracks in the order of 0.4-1.0 mm.
- ❑ Cracks \parallel to the loaded surface: formation in areas with $T \sim 500\text{K}$ –around DBTT – and a temperature gradient of 1.3-1.7 MK/m.
- ❑ surface roughness after heat loading
- ❑ Surface Morphology after laser melt Pulse: predominantly the cellular structures, holes in the re-solidified W-material