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# Influence of DPSS Laser on Polymerization Shrinkage and Mass Change of Resin Composites

Dong-Hee Shin, D.D.S., M.S.<sup>1</sup> Dong-In Yun, D.D.S., M.S.<sup>1</sup> Mi-Gyong Park, Ph.D.<sup>2</sup> Ching-Chang Ko, D.D.S., Ph.D.,<sup>3</sup> Franklin García-Godoy, D.D.S., M.S.,<sup>4</sup> Hyung-II Kim, D.D.S., Ph.D.<sup>1</sup> and Yong Hoon Kwon, Ph.D.<sup>1</sup>

# Abstract

Objectives: This study evaluated the effectiveness of the diode-pumped solid state (DPSS) laser as a light source for light-curing dental resin composites. Background data: A DPSS laser of 473 nm may be useful because of its match with the absorption peak of camphorquinone (CQ), the photoinitiator. *Materials and methods:* A DPSS laser (LAS) of 473 nm and a quartz–tungsten–halogen (QTH) light-curing unit (OP) were used as the light sources for light curing six different resin composites (four nanocomposites and two hybrid composites). Polymerization shrinkage and mass change (water sorption and solubility) were measured during and after light curing to determine the degree of polymerization. Mass change was evaluated by following the ISO 4049 standard. Results: According to the evaluation, the specimens light cured using LAS showed similar maximum polymerization shrinkage (12.3  $\sim$  18.1  $\mu$ m for LAS; 13.2  $\sim$  16.2  $\mu$ m for OP) and water sorption (11.4  $\sim$  24.1  $\mu$ g/  $\text{mm}^3$  for LAS; 11.3 ~ 22.8  $\mu$ g/  $\text{mm}^3$  for OP) to the cases light cured using OP. The specimens light cured using LAS showed a significantly higher solubility than the cases light cured using OP  $(2.4 \sim 6.6 \,\mu g/\,\text{mm}^3$  for LAS;  $0.8 \sim 1.6 \,\mu$ g/ mm<sup>3</sup> for OP). However, the maximum water sorption and solubility obtained from the specimens were lower than the values permitted by the ISO 4049 standard. Conclusions: The results may suggest that the DPSS laser with an emission wavelength of 473 nm can be used as a light source for light-curing dental resin composites.

# Introduction

REGARDLESS OF THE TYPES AND USES, all light-curing dental<br>restorative materials are polymerized by blue light. The process of polymerization involves the following: activation of the photoinitiator camphorquinone (CQ) by blue light, conversion of the monomers to a polymer network, and termination of the process. During the conversion process, the larger van der Waals intermolecular spacing in the monomers changes to a smaller covalent bond intramolecular spacing of a polymer network.<sup>1,2</sup> Polymerization shrinkage inevitability occurs during this process. Because monomers do not completely convert into a polymer network during the conversion process, any unreacted molecules can form the walls of pores within the materials structure.<sup>3</sup>

Dental materials used to fill in a tooth cavity are continuously exposed to water. The water on the surface absorbs into the subsurface with time, which makes the material swell and soften. Subsequent deterioration of the physical/ mechanical properties occurs because of bond breakdown between the silane and filler particles, debonding in the fillermatrix interfaces, and leaching of the unreacted monomers and water-soluble elements.<sup>4</sup> The ISO 4049 standard states that the maximum water sorption and solubility are <40 and 7.5  $\mu$ g/mm<sup>3</sup>, respectively.<sup>5</sup>

The role of blue light is crucial because it initiates the polymerization process. Thus far, several types of light sources have been introduced for the light curing of dental restorative materials. $6-9$  One common feature in these light sources is the overlap of their emission spectrum to the absorption spectrum of CQ. The conventional quartz–tungsten– halogen (QTH) and xenon-based plasma arc light sources match the CQ spectrum most widely. On the other hand, light emit diodes (LEDs) match only at the absorption peak of CQ, and the argon laser matches only at the tail part of the absorption peak of CQ. Among the light sources, the

<sup>&</sup>lt;sup>1</sup>Department of Dental Materials, College of Dentistry and Pusan National University Hospital Medical Research Institute, Pusan National University, Yangsan, Korea. <sup>2</sup>

<sup>&</sup>lt;sup>2</sup>Department of Dental Laboratory Science, Catholic University of Pusan, Pusan, Korea.

<sup>3</sup> Department of Orthodontics, School of Dentistry, University of North Carolina, Chapel Hill, North Carolina.

<sup>4</sup> College of Dentistry, University of Tennessee, Memphis, Tennessee.

argon laser showed the narrowest emission width. Recently, diode-pumped solid state (DPSS) lasers have become widely used, as laser pointers and as a light source for the excitation of phycoerythrins (PE) in flow cytometers.<sup>10–12</sup> The advantages of DPSS lasers over argon lasers are their compactness and price. However, there are few reports on the application of DPSS lasers to the light curing of dental restorative materials in dentistry.<sup>13–16</sup>

The purpose of this study was to evaluate the polymerization shrinkage and mass change in dental resin composites that were light cured using the DPSS laser. The testing hypothesis was that the DPSS laser of 473 nm can light cure resin composites to the level that was achieved by the QTH light source through the effective activation of CQ.

#### Materials and Methods

#### Specimens and light sources

For the study, four different resin nanocomposites [Ceram X (CX), Grandio (GD), Premise (PE), and Filtek Z350 (Z3)] and two hybrid resin composites [Filtek P60 (P60) and Tetric Ceram (TC)] were examined. All have the shade, A3. A conventional QTH light [Optilux 501 (OP), Kerr, Danbury, Connecticut] and a DPSS laser (LAS) (LVI Technology, Seoul, Korea) of 473 nm were used as the light sources. The output power and spot size of LAS were  $\sim$  140 mW (PM3/FIELD-MAX, Coherent, Portland, Oregon) and 7 mm, respectively. The raw beam was expanded to 7 mm using a beam expander. The output light intensity of OP was measured using a radiometer, which was internally set in the OP. The light intensities of OP and LAS were  $\sim 800$  and  $400 \,\mathrm{mW/cm^2}$ , respectively. Table 1 lists the characteristics of the specimens used. The emission spectrum of the light sources and the absorption spectrum of CQ (Figure 1) were measured using a photodiode array detector (M1420, EG&G PARC, Princeton, New Jersey) connected to a spectrometer (SpectroPro-500, Acton Research, Acton, Massachusetts).

#### Measurement of polymerization shrinkage

The amount of polymerization shrinkage ( $n = 5$  for each condition) during the light-curing process was measured using a linometer (RB 404, R&B Inc., Daejon, Korea). The resin was located between the covering slide glass and aluminum disc (the specimen stage over the shrinkage sensing part). A metal mold (inner diameter, 4 mm; thickness, 2 mm) was placed over the aluminum disc and filled with resin. After being completely filled with resin, the metal mold was removed (at this time one resin cylinder was made). A slide glass was then secured over the resin. The end of the lightguide (OP) made contact with the top surface of the slide glass. The resin was irradiated for 40 sec with the previously mentioned light intensities. As the resin polymerized, it shrank toward the light source and the aluminum disc under the resin and then moved toward the light source. The polymerization shrinkage was measured automatically for 130 sec using the non-contacting inductive gauge. The resolution and measuring range of the shrinkage sensor were 0.1 and  $100 \mu m$ , respectively.

## Measurement of mass change (water sorption and solubility)

For the mass change measurements (water sorption and solubility), the specimens  $(n = 10$  for each case from each product) were prepared according to the ISO 4049 standards.<sup>5</sup> A ring-type metal mold (inner diameter, 15 mm; thickness, 1 mm) was placed over the thin slide glass. Each resin was placed in the mold and the top surface was covered with a thin slide glass. After pressing the top surface, light curing was performed for 40 sec. According to ISO 4049 standard, each specimen received nine overlapping steps of light irradiation for 360 sec on one side. The reverse side was then treated in a similar manner. The wall of the metal mold was pasted with a resin separator to allow easy removal of the specimen from the mold after light curing.

The specimens were removed from the mold and placed in a desiccator for 22h at  $37^{\circ}$ C and then for 2h at 24 $^{\circ}$ C. Subsequently, the weight was measured to an accuracy of  $\pm 0.001\,\text{mg}$  (according to ISO 4049 standard, accuracy of  $\pm$  0.1 mg is adequate) using an analytical balance (Sartorius CP2P, Goettingen, Germany). This cycle was repeated until a constant mass  $m_1$  was obtained (in this study, a deviation <0.001 mg was assumed to be constant). The specimens were then immersed in distilled water  $(37^{\circ}C)$  for 7 days. At this time, each specimen was placed in a tube filled with 15 ml of

Material	Composition	Filler type	Filler content <sup>a</sup> $vol\%$ / $wt\%$	Company
CX.	Methacrylate modified polysiloxane, Dimethacrylate resin,	Ba-Al-borosilicate glass, Methacrylate functionalized SiO <sub>2</sub> nanofiller	57/76	Dentsply/ Detrey
GD	Bis-GMA, TEGDMA, UDMA	Ba-Al-Borosilicate glass filler, $SiO2$ nonofillers	71.4/87	VOCO
<b>PM</b>	Bis-EMA, TEGDMA	Prepolymerized resin fillers, barium glass, silica nanoparticles	69/84	Kerr
Z3	Bis-GMA, UDMA, TEGDMA, Bis-EMA	Non-aggregated silica, Zirconia/silica	59.5/78.5	3M ESPE
<b>P60</b>	Bis-GMA, UDMA, Bis-EMA	Zirconia/silica	61/83	3M ESPE
TC.	Bis-GMA, UDMA, TEGDMA	Ba-Al-F-silicateglass, Ba glass, YbF <sub>3</sub>	60/78	Vivadent

Table 1. Characteristics of the Tested Resin Composites

CX, Ceram X; GD, Grandio; PM, Premise; Z3, Z350; P60, Filtek P60; TC, Tetric Ceram.

Bis-EMA, Bisphenol A ethoxylated dimethacrylates; Bis-GMA, Bisphenol A digycidyl methacrylate; TEGDMA, Triethylene glycol dimethacrylate; UDMA, Urethane dimethacrylate.

<sup>a</sup>According to the manufacturers.



FIG. 1. Emission spectrum of the light sources (LAS, OP) and the absorption spectrum of the photoinitiator (CQ).

water. After 7 days, the specimens were removed from the tube, and the water on the surfaces was blotted away until there was no visible moisture. The specimen was then waved in air for 15 sec, and weighed  $(m<sub>2</sub>)$  1 min after removal from the tube. Subsequently, the specimens were placed in a  $37^{\circ}$ C desiccator and weighed every 24 h until a constant mass  $(m_3)$ was obtained. The specimen volume (V) was determined by measuring the specimen diameter at right angles to each other and the thickness at the center of the specimen as well as at four equally spaced points on the circumference using Vernier calipers (series 530, Mitutoyo, Tokyo, Japan) with an accuracy of 0.02 mm. The level of water sorption (Wsp) and solubility (Wsl) were calculated using the formula  $Wsp = (m<sub>2</sub>)$ –  $m_3$ /V and Wsl =  $(m_1 - m_3)/V$ , respectively, where V (mm<sup>3</sup>) is the specimen volume, and m<sub>1</sub> ( $\mu$ g), m<sub>2</sub> ( $\mu$ g) and and  $m<sub>3</sub>$  are: the mass of the specimen prior to immersion, its mass after immersion for 7 days at  $37^{\circ}$ C, and its mass after immersion and drying, respectively.

## Statistical analysis

The data for polymerization shrinkage, water sorption, and solubility was analyzed by ANOVA at the 95% confidence level. A Tukey's test was then used for a multiple comparison when deemed necessary.

## **Results**

Figure 1 shows the emission spectrum of the light sources used in this study along with the absorption spectrum of CQ, which is commonly included in light-curing dental resin composites. The emission spectrum of OP matched completely with the absorption spectrum of CQ, whereas the emission spectrum of LAS matched the absorption peak of CQ only at its tail part.

Table 2 shows the maximum polymerization shrinkage  $(\mu m)$  during light curing. Among the specimens, TC and P60 (hybrid composite resins) showed the highest  $(18.1 \pm 1.0 \text{ or }$  $16.4 \pm 1.3$  depending upon the light source) and lowest  $(12.3 \pm 0.9 \text{ or } 13.1 \pm 0.7 \text{ depending upon the light source})$ shrinkage, respectively, whereas the remaining nanocomposite resins (CX, GD, PM, and Z3) showed similar shrinkage between the two maximum and minimum values.

TABLE 2. POLYMERIZATION SHRINKAGE  $(\mu M)$  of the Specimens Light Cured Using Different Light Sources

	Light source		
Material	LAS	OP	p Value
$CX^{AD}$	15.8(0.3)	16.2(0.8)	
$\mathrm{GD}^\mathrm{AB}$	14.8(0.3)	15.9(0.2)	
$PM^B$	14.8(0.3)	14.0(0.6)	$\beta$ < 0.001
$Z3^{\mathrm{AB}}$	14.8(0.6)	15.0(0.6)	
$P60^{\circ}$	12.3(0.9)	13.2(0.8)	
$TC^D$	18.1(1.0)	16.2(1.3)	

CX, Ceram X; GD, Grandio; PM, Premise; Z3, Z350; P60, Filtek P60; TC, Tetric Ceram.

Statistically significant difference on product is shown by superscript letters<sup> $A,B$ </sup>. Same letters are not significantly different ( $p > 0.05$ ). For the light source, no post hoc test was performed because there is no significant difference between values obtained from the different light sources.

On *p*-value, the letter  $\beta$  denotes product.

The amount of polymerization shrinkage obtained using the two light sources was similar ( $p > 0.05$ ).

Figure 2 shows the polymerization shrinkage profile of the specimens light cured using LAS (Fig. 2a) and OP (Fig. 2b). Immediately after light curing for 40 sec, the specimens light



FIG. 2. Polymerization shrinkage profile of the specimens during and after the light curing using LAS (a) and OP (b).

cured using OP showed a more apparent second peak than that obtained using LAS.

Table 3 shows the water sorption ( $\mu$ g/mm<sup>3</sup>) and solubility  $(\mu g/mm^3)$  of the specimens light cured using either LAS or OP. The specimens light cured using the different light sources showed similar water sorption. Among the specimens, Z3 and GD showed the highest (24.1  $\pm$  0.8) and lowest  $(11.3 \pm 0.6)$  water sorption, respectively, depending upon the light source used. In the case of solubility, the specimens light cured using LAS showed a significantly higher solubility than those cured using OP. The maximum solubility was ranked from PE (6.6 $\pm\,0.3$  or  $1.6\pm0.1$  depending upon the light source). P60 showed the lowest solubility (2.4  $\pm$  0.4) when light cured using LAS, whereas a negative  $(-1.3 \pm 0.6)$ solubility was observed when they were light cured with OP.

# **Discussion**

The polymerization of dental resin composites is initiated by irradiating the material with blue light. Blue light is essential for light curing because it activates the CQ contained in the resin matrix. Thus far, several different light sources have been used to generate blue light: QTH units, xenon lamp-based plasma arc units, LED units, and argon lasers. The QTH light used in this study emits a blue light at wavelength of 400–500 nm by filtering the white light emitted from the bulb. The light emitted from the QTH unit easily diverges in a similar manner to normal light. Such divergence significantly attenuates the initial light intensity with increasing distance between the light guide and specimen. During light curing, the light intensity can easily change if the distance is not kept constant. The advantage of QTH light is its excellent match with the absorption spectrum of CQ. According to the report by Rueggeberg et al.<sup>17</sup>, light irradiation with  $400 \text{ mW/cm}^2$  for  $40 \text{ sec}$  is sufficient to cure the composite resins to a 2-mm thickness.17 Most QTH lights available on the dental market emit a much stronger light than this critical value. Nevertheless, because QTH light-curing units use a lifetime limited bulb, they require frequent replacement and maintenance to maintain reliable light quality.

The superiority of lasers over other types of lights is a result of their monochromaticity and coherence. In the case of the argon laser (the same as the DPSS laser), one of its emission frequencies (488 nm) matches the absorption peak of CQ at its tail part. Because all the photons emitting from the argon laser have the same wavelength, they can effectively activate the photoinitiator. The usefulness and efficiency of an argon laser in the polymerization of dental restorative materials has been demonstrated.18–20 Nevertheless, its high price and bulkiness precludes its routine use in dental clinics. A DPSS laser with an emission at 473 nm has many similarities to the argon laser. The wavelength of the DPSS laser matches the absorption peak of CQ more closely than does that of the argon laser. The advantages of DPSS lasers over argon laser are their price and compactness. However, only a few studies have evaluated the applicability of 473 nm in the polymerization of light-curing dental restorative materials.<sup>13–16</sup>

Polymerization shrinkage occurs when the monomers convert to a polymer network. At that time, the molecular spacing reduces as a result of polymerization. Generally, polymerization shrinkage depends upon a variety of factors, such as the filler loading, filler type, and composition of the resin matrix.21–24 According to studies, the total shrinkage of the specimens (or degree of conversion) increased with decreasing molecular weight of the monomers. $25-27$  Among the monomers used in this study, Bisphenol A ethoxylated dimethacrylates (bis-EMA and triethylene glycol dimethacrylate (TEGDMA) had the highest and lowest molecular weight, respectively [bis-EMA, 540; bisphenol A digycidyl methacrylate (bis-GMA), 512.6; urethane dimethacrylate (UDMA), 470; TEGDMA, 286.2]. Therefore, the total shrinkage of the specimens increases (or decreases) as a percentage of TEGDMA (bis-EMA) in the specimen increases. Both the filler loading and composition of the monomers may influence the result. GD and PM contain the highest amount of filler in their resin. On the other hand, CX and Z3 contain the lowest filler content (vol %) among the specimens tested in this study. The reason for the similar shrinkage in this contrasting situation is unclear. Both the filler loading and composition (content) of the monomers may be related in some complicated manner to the results obtained. Immediately after light curing for 40 sec, the specimens light cured using OP showed the initiation of a more apparent

Table 3. Water Sorption  $(\mu G/\mathrm{Mm^3})$  and Solubility  $(\mu G/\mathrm{Mm^3})$ of the Specimens After Light Curing Using Different Light Sources

	Sorption $(\mu g/mm^3)$			Solubility $(\mu g/mm^3)$		
Material	LAS	ΟP		LAS <sup>1</sup>	$OP^2$	
$CX^A$	15.3(0.6)	15.4(0.6)	$CX^A$	4.6 $(0.1)$	0.9(0.2)	
$GD^B$	11.4(0.5)	11.3(0.6)	$GD^B$	3.1(0.2)	0.8(0.1)	
PE <sup>C</sup>	20.7(0.6)	21.0(0.9)	PE <sup>C</sup>	6.6(0.3)	1.6(0.1)	
$Z3^D$	24.1(0.8)	22.8(0.5)	$Z3^D$	6.3(0.3)	1.0(0.5)	
P60 <sup>E</sup>	17.4(0.1)	18.1(0.7)	P60 <sup>E</sup>	2.4(0.4)	$-1.4(0.6)$	
TC <sup>F</sup>	16.6(0.5)	15.7(0.8)	TC <sup>F</sup>	5.2(0.2)	1.2(0.2)	
$p$ -value	$\beta < 0.001$		$p$ -value		$\alpha$ < 0.001, $\beta$ < 0.001	

CX, Ceram X; GD, Grandio; PM, Premise; Z3, Z350; P60, Filtek P60; TC, Tetric Ceram.

Statistically significant difference on product is shown by superscript letters<sup>A,B</sup>. Same letters are not significantly different ( $p > 0.05$ ). For the light source in the water sorption, no post hoc test was performed because there is no significant difference between values obtained from the different light sources.

On *p*-values, the letters  $\alpha$  and  $\beta$  denote light source and product, respectively.

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second peak in the 40–60 sec interval. The reason for such increase in the shrinkage profile may be related to the thermal expansion of the specimen by the heat from the light source and the exothermic heat of the specimen during the light curing. According to reports, the temperature rise on the composite resins reaches to the point that feels hotness.<sup>28,29</sup> Because of the heat from the QTH bulb, the heat is transmitted through the light guide, and through exothermic reaction, the specimen can expand during the light curing while the specimen undergoes polymerization shrinkage. However, if there is no light, the heat supply from the QTH bulb and the exothermic reaction will cease, and then shrinkage will occur dominantly without suppression.

When the filled dental materials come in contact with water (oral fluids) in the oral cavity, water sorption from the surface occurs mainly through the resin matrix. Within the resin matrix, the absorbed water can fill the pores made from the unreacted molecules. $3$  In addition, water on the specimen surface and within the pores softens the resin matrix, resulting in the leaching of unreacted monomers, unbound components, and water-soluble elements.<sup>30,31</sup> The strength, volume, color stability, and biocompatibility of the dental filling materials can be adversely affected by this water sorption and solubility, even though some positive effects, such as marginal sealing by hygroscopic expansion, can be expected.<sup>32–34</sup> ISO 4049 standard requires light-curing dental materials to have a maximum water sorption and solubility  $<$ 40 and 7.5  $\mu$ g/mm<sup>3</sup>, respectively. The materials tested in this study satisfy this guideline. The fact that GD had the lowest water sorption was attributed to its highest filler volume. However, an explanation for the fact that Z3, which has the lowest filler volume, had the highest water sorption, may not possible. Generally, the amount of water sorption depends upon the monomer composition, surface condition, degree of polymerization, pore size, and volume within the resin matrix. $34-37$  A generally high (low) solubility was observed in the specimens showing high (low) water sorption. The relatively high solubility of TC may be partly caused by the leaching of the contained fluoride. TC contains Ba-Al-Fsilicate glass and  $YbF_3$  as part of its fillers. It is unclear why there was a significantly higher solubility in the specimens light cured with LAS than in those light cured with OP, despite their similar water sorption. It might be related to the lower degree of polymerization. As the light intensity of LAS was 50% that of OP, the lower degree of conversion and more retention of the unreacted monomers would be natural. Such a state can increase the solubility of the LAS-cured specimens compared to those of the OP-cured specimens. The negative value from P60 suggests an increase in the resulting mass than before the immersion in distilled water. One of the possible reasons is the formation of a new compound within the structure. The glass filler and metal oxides are known to form metal hydroxides as reaction products when they interact with water.<sup>4,38</sup> The absorption of any substance or incomplete dehydration was not possible because the specimens were immersed in distilled water and fully dried.

# **Conclusions**

The specimens light cured using LAS showed similar maximum polymerization shrinkage and water sorption to those cured using OP. In the case of solubility, the specimens light cured using LAS showed significantly higher values than those cured using OP. However, the maximum water sorption and solubility obtained using LAS were lower than the maximum values set by the ISO 4049 standard. The DPSS laser of 473 nm appears to have high potential as a light source for the light curing of dental restorative materials. For more concrete conclusions, future studies estimating the degree of polymerization by the DPSS laser, using various mechanical tests, will be needed.

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#### Author Disclosure Statement

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#### **References**

- 1. Watts, D.C. (2005). Reaction kinetics and mechanics in photo-polymerised networks. Dent. Mater. 21, 27–35.
- 2. Asmussen, E., and Peutzfeldt, A. (1997). Direction of shrinkage of light-curing resin composites. Acta Odontol. Scand. 57, 310–315.
- 3. Anusavice, K.J. (1996). Phillips' science of dental materials, 10th ed. Philadelphia: WB Saunders, pp. 52–83.
- 4. Soderholm, K.J., Zigan, M., Ragan, M., Fischlschweiger, W., and Bergman, M. (1984). Hydrolytic degradation of dental composites. J. Dent. Res. 63, 1248–1254.
- 5. EN ISO 4049 Dentistry-Polymer-based filling, restorative and luting materials. Geneva: International Organization for Standardization.
- 6. Lopes, L.G., Moraes, B.R., Souza, R.M., Jardim Filho Ada, V., Moreira Fdo, C., Campos, R.E., and de Souza, J.B. (2010). How light sources and distance of the light tip influence water sorption, solubility, and biaxial flexural strength of a composite resin. Gen. Dent. 58, e162–e167.
- 7. Topcu, F.T., Erdemir, U., Sahinkesen, G., Yildiz, E., Uslan, I., and Acikel, C. (2010). Evaluation of microhardness, surface roughness, and wear behavior of different types of resin composites polymerized with two different light sources. J. Biomed. Mater. Res. B Appl. Biomater. 92, 470–478.
- 8. Komori, P.C., de Paula, A.B., Martin, A.A., Tango, R.N., Sinhoreti, M.A., and Correr-Sobrinho, L. (2010). Effect of light energy density on conversion degree and hardness of dual-cured resin cement. Oper. Dent. 35, 120–124.
- 9. Price, R.B., Fahey, J., and Felix, C.M. (2010). Knoop microhardness mapping used to compare the efficacy of LED, QTH and PAC curing lights. Oper. Dent. 35, 58–68.
- 10. Kapoor, V., Karpov, V., Linton, C., Subach, F.V., Verkhusha, V.V., and Telford, W.G. (2008). Solid state yellow and orange lasers for flow cytometry. Cytometry A 73, 570–577.
- 11. Habbersett, R.C., Naivar, M.A., Woods, T.A., Goddard, G.R., and Graves, S.W. (2007). Evaluation of a green laser pointer for flow cytometry. Cytometry A. 71, 809–817.
- 12. Telford, W.G., Murga, M., Hawley, T., Hawley, R.G., Packard, B.Z., Komoriya, A., Haas, F., and Hubert, C. (2005). DPSS yellow-green 561 nm lasers for improved fluorochrome detection by flow cytometry. Cytometry A. 68, 36– 44.
- 13. Kwon, Y.H., Jang, C.M., Shin, D.H., Seol, H.J., and Kim, H.I. (2008). The applicability of DPSS laser for light curing of composite resins. Lasers Med. Sci. 23, 407–414.
- 14. Knezevic, A., Ristic, M., Demoli, N., Tarle, Z., Music, S., and Negovetic Mandic, V. (2007). Composite polymerization with diode laser. Oper. Dent. 32, 279–284.
- 15. Jang, C.M., Seol, H.J., Kim, H.I., and Kwon, Y.H. (2009). Effect of blue light-curing systems on the polymerization of nanocomposite resins. Photomed. Laser Surg. 27, 871–876.
- 16. Jung, Y.H., Cho, B.H., Nah, K.S., Kim, H.I., and Kwon, Y.H. (2010). Effect of diode-pumped solid state laser on polymerization shrinkage and color change in composite resins. Lasers Med. Sci. 25, 339–343.
- 17. Rueggeberg, F.A., Eagle, J.W., and Mettenburg, D.J. (2000). Polymerization depths of contemporary light-curing units using microhardness. J. Esthet. Dent. 12, 340–349.
- 18. Voltarelli, F.R., Dos Santos-Daroz, C.B., Alves, M.C., Peris, A.R., and Marchi, G.M. (2009). Effectiveness of resin composite polymerization when cured at different depths and with different curing lights. Gen. Dent. 57, 314–319.
- 19. Cassoni, A., Ferla Jde, O., Albino, L.G., Youssef, M.N., Shibli, J.A., and Rodrigues, J.A. (2010). Argon ion laser and halogen lamp activation of a dark and light resin composite: microhardness after long-term storage. Lasers Med. Sci. 25, 829– 834.
- 20. Rode, K.M., de Freitas, P.M., Lloret, P.R., Powell, L.G., and Turbino, M.L. (2009). Micro-hardness evaluation of a microhybrid composite resin light cured with halogen light, lightemitting diode and argon ion laser. Lasers Med. Sci. 24, 87–92.
- 21. Li, Y., Swartz, M.L., Phillips, R.W., Moore, B.K., and Roberts, T.A. (1985). Effect of filler content and size on properties of composites. J. Dent. Res. 64, 1396–1401.
- 22. Tarumi, H., Torii, M., and Tsuchitani, Y. (1995). Relationship between particle size of barium glass filler and water sorption of light-cured composite resin. Dent. Mater. J. 14, 37–44.
- 23. Uhl, A., Mills, R.W., Rzanny, A.E., and Jandt, K.D. (2005). Time dependence of composite shrinkage using halogen and LED light curing. Dent. Mater. 21, 278–286.
- 24. Aw, T.C., and Nicholls, J.I. (2006). Polymerization shrinkage of densely filled resin composites. Oper. Dent. 26, 498–504.
- 25. Alvarez-Gayosso, C., Barcelo-Santana, F., Guerrero-Ibarra, J., Saez-Espinola, G., and Canseco-Martinez, M.A. (2004). Calculation of contraction rates due to shrinkage in lightcured composites. Dent. Mater. 20, 228–235.
- 26. Atai, M., Watts, D.C., and Atai, Z. (2005). Shrinkage strainrates of dental resin-monomer and composite systems. Biomaterials. 26, 5015–5020.
- 27. Sideridou, I.D., Achilias, D.S., and Karabela, M.M. (2007). Sorption kinetics of ethanol/water solution by dimethacrylate-based dental resins and resin composites. J. Biomed. Mater. Res. B Appl. Biomater. 81B, 207–218.
- 28. Knezević, A., Tarle, Z., Meniga, A., Sutalo, J., and Pichler, G. (2005). Influence of light intensity from different curing units

upon composite temperature rise. J. Oral Rehabil. 32, 362– 327.

- 29. Hofmann, N., Markert, T., Hugo, B., and Klaiber, B. (2003). Effect of high intensity vs. soft-start halogen irradiation on light-cured resin-based composites. Part I. Temperature rise and polymerization shrinkage. Am. J. Dent. 16, 421–430.
- 30. Cesar, P.F., Miranda, W.G. Junior, and Braga, R.R. (2001). Influence of shade and storage time on the flexural strength, flexural modulus and hardness of composites used for indirect restorations. J. Prosthet. Dent. 86, 289–296.
- 31. Mante, F., Saleh, N., and Mante, M. (1993). Softening patterns of post-cure heat-treated dental composites. Dent. Mater. 9, 325–331.
- 32. Mortier, E., Gerdolle, D.A., Jacquot, B., and Panighi, M.M. (2004). Importance of water sorption and solubility studies for couple bonding agent-resin-based filling material. Oper. Dent. 29, 669–676.
- 33. Sideridou, I., Tserki, V., and Papanastasiou, G. (2003). Study of water sorption, solubility and modulus of elasticity of light-cured dimethacrylate-based dental resins. Biomaterials. 24, 655–665.
- 34. Ortengren, U., Wellendort, H., Karlsson, S., and Ruyter, I.E. (2001). Water sorption and solubility of dental composites and identification of monomers released in an aqueous environment. J. Oral Rehabil. 28, 1106–1115.
- 35. Hofmann, N., Renner, J., Hugo, B., and Klaiber, B. (2002). Elution of leachable components from resin composites after plasma arc vs standard or soft-start halogen light irradiation. J. Dent. 30, 223–232.
- 36. Sideridou, I., Achilias, D.S., Spyroudi, C., and Karabela, M. (2004). Water sorption characteristics of light-cured dental resins and composites based on Bis-EMA/PCDMA. Biomaterials. 25, 367–376.
- 37. Oysaed, H., and Ruyter, I.E. (1986). Composites for use in posterior teeth: mechanical properties tested under dry and wet conditions. J. Biomed. Mater. Res. 20, 261–271.
- 38. Kildal, K.K., and Ruyter, I.E. (1997). How different curing methods affect mechanical properties of composites for inlays when tested in dry and wet conditions. Eur. J. Oral Sci. 105, 353–361.

Address correspondence to: Yong Hoon Kwon Department of Dental Materials School of Dentistry and Medical Research Institute, Pusan National University Yangsan 626-870 Korea

E-mail: y0k0916@pusan.ac.kr