

The Use of Natural Fibers in Repairing and Strengthening of Cultural Heritage Buildings

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Abstract

Natural fibers are getting a huge interest amongst researchers due to their green, economical and good mechanical properties when employed in different composites as reinforcements. In this work we present a review on the applications of natural fibers, essentially as composites, for structural purposes with focus on repairing and strengthening of cultural built heritage. Different testing methods with their results combined with the studying of the enhancements attained by applying natural fiber composites, e.g. textile reinforced mortar (TRM), to weak masonry are discussed. Durability challenges mainly due to the hydrophilic nature of the natural fibers are discussed together with some possible solutions.

Keywords: Natural Fibers Composites; Built Heritage; Seismic Retrofitting; Surface Treatments; Masonry

1. Introduction

Masonry structures are widespread around the Mediterranean area and Europe. With the various materials used for masonry structures, e.g. clay bricks, tuff and stones, masonry is considered as one of the most used building materials that humans ever used.

The old masonry structures were constructed mainly to resist vertical and gravitational loads, mainly the dead loads [1]. However, historical constructions, in general, are likely to be subjected to various hazards, either natural or man-made, that may threaten their functions, behavior and even the continuity of their existence. Various catastrophic natural hazards, namely earthquakes, have happened through time and caused severe casualties and losses. Under such lateral loads, masonry structures showed a vulnerable seismic response [2]. Thus, this problem highlights the necessity to approach scientific interventions to preserve the built heritage against earthquakes.

Amongst the different strengthening systems based on the external retrofitting of historical constructions, the use of external reinforcements embedded into inorganic matrices has had an important consensus among researchers. These composites are employed as textile reinforced mortar/fiber reinforced cementitious matrices, the so-called TRM/FRCM composites, and have been studied and proved a high capability to enhance lateral stiffness and load carrying capacity of historical masonry constructions.

Different types of synthetic fibers have been used as reinforcements, such as basalt, glass and carbon, typically embedded within lime or cement matrices and applied to masonry panels. Consequently, very interesting mechanical enhancements have been attained in terms of both in-plane shear capacity and out-of-plane flexural performance. However, the manufacturing process of synthetic fibers composites, their application and the disposal at end-of-life phase have a harsh impact to the environment. Moreover, compatibility problems pointed out by the over stiffening of masonry substrates combined with the premature cracks occurring before reaching the ultimate capacity of these fibers appeared as drawbacks. Hence, researchers have been motivated to direct their studies to green, economical, and innovative solutions.

Given their environmental-friendly trait, economic feasibility and good mechanical properties, natural fibers have emerged as an alternative solution to many synthetic fibers. The applications of this environmental-friendly solution have spread to major industries such as automobiles, biomedicines and mechanical engineering.

45 All the advantageous characteristics corresponding to the use of natural fibers drew the attention to the possibility
 46 of engaging them in the structural repairing of the historical constructions. This paper presents an overview on the
 47 strengthening and repairing works resorting to natural fibers with a major focus on the cultural built heritage and the
 48 challenges corresponded to.

49 **2. Natural Fibers and Civil Engineering**

50 Due to the aforementioned significant benefits provided by natural fibers, their applications were widened to be
 51 exploited in civil engineering purposes. Among different natural fibers, such as animal (wool, silk. etc.), cotton and
 52 processed cellulosic fibers, bast fibers derived from plants are most widely investigated and used for building materials
 53 purposes [3]. Flax, hemp, sisal and kenaf have good mechanical properties if compared to synthetic fibers, as shown
 54 in Table 1 described by author [4].

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 56 Table 1-Bast natural fibers mechanical properties [4].

Fiber	Density	Diameter	Tensile Strength	Young's modulus	Elongation at break	References
	g/cm ³	μm	MPa	GPa	%	
Cotton	1.5-1.6	-	287-800	5.5-12.6	7.0-8.0	45, 49
Jute	1.3-1.45	25-200	393-773	13-26.5	1.16-1.5	22, 23, 37, 45, 49
Flax	1.50	-	345-1100	27.6	2.7-3.2	22, 23, 37, 49
Hemp	-	-	690	-	1.6	22 37
Ramie	1.50	-	400-938	61.4-128	1.2-3.8	22 37 46 49
Sisal	1.45	50-200	468-640	9.4-22.0	3-7	22 23 37 45 49
PALF	-	20-80	413-1627	34.5-82.51	1.6	45
Coir	1.15	100-450	131-175	4-6	15-40	22, 45
E-glass	2.5	-	2000-3500	70	2.5	22, 47
S-glass	2.5	-	4570	86	2.8	22, 23, 47
Aramid	1.4	-	3000-3150	63-67	3.3-3.7	22, 47
Carbon	1.7	-	4000	230-240	1.4-1.8	22, 47

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 58 One of the most significant applications of natural fibers in construction field is the use of short fibers as internal
 59 reinforcements mainly to increase the tensile and flexural properties. When reinforced with randomly distributed short
 60 natural fibers, cement concrete showed a higher toughness after the occurring of cracking [5]. The crossed fibers along
 61 the crack width demonstrated the so-called bridging phenomena, see Figure 1, an issue that highlights the capacity of
 62 natural fibers to transfer stresses. For instance, Li et al. [6] employed 20 mm-long hemp fibers when casting reinforced
 63 concrete and detected increase of flexural toughness by 144 %, combined with increased flexural toughness index by
 64 214 %. These results were in consensus with results acquired with author [7], where a set of different natural fibers
 65 were used to reinforce concrete prismatic samples, see Figure 2. Hemp fibers showed the highest fracture energy
 66 increment of 70 % when compared to non-reinforced concrete samples.

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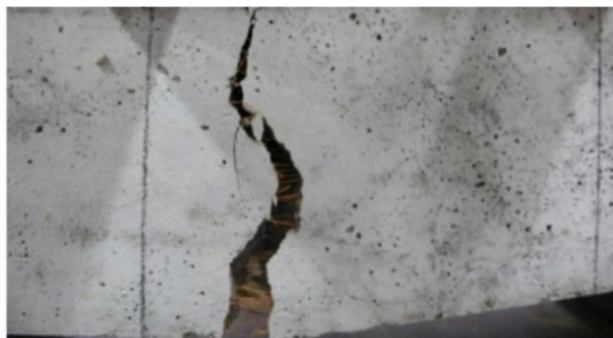


Figure 1-Coconut fibers-reinforced concrete [5].



Figure 2-Hemp, wheat straw, and elephant grass, respectively [7]

69 Natural fibers can also be studied as possible reinforcements for polymeric concrete resulting in increased flexural
70 strength [8]. Depending on the kind and the proportion of natural fibers, mechanical behavior improvements of the
71 reinforced samples can be achieved without compromising the compressive characteristics of the concrete. B. Hu et
72 al [9] studied short sisal and ramie fibers, independently, as possible reinforcements for epoxy polymer concrete and
73 the flexural strength was increased by 10% and 25% for both fibers respectively. Also, Reis [10] studied a set of
74 natural fibers to reinforce epoxy resins polymer concrete with banana, coconuts and bagasse fibers. Subsequently, it
75 was stated that increments in both fracture toughness and fracture energy (16% and 41% respectively) when using
76 coconut and bagasse fibers were observed.

77 For non-cementitious materials, such as rammed earth [11], natural fibers were examined in literature as apt
78 reinforcements when fabricating adobe bricks [12]. Given the brittle properties of adobe bricks, the addition of natural
79 fibers resulted in improving their breaking behavior. Millogo et al. [13] observed that the addition of short hemp fibers
80 (30mm) at proportion of 0.2-0.6 wt% led to limitations of the porosity of the bricks that resulted in better mechanical
81 characteristics. Moreover, the high adhesion with clay matrix ensued in higher durability, according to abrasion tests,
82 as well as improved flexural strength because of the high tensile strength of the fibers. The addition of 1 wt% of straw
83 fibers to mud adobe contributed to developments in energy absorption and ultimate load capacities by acting as shear
84 reinforcements [14]. The stabilization with coconut husk, bagasse and oil palm fibres in the production of red and
85 brown clayey soil blocks was studied by Danso et al. [15]. The results revealed that a 0.5 wt% content of the fibers to
86 soil improved significantly the compressive strength (up to 57% with palm oil fibers), erosion resistance and reduced
87 shrinkage cracking. Considerable ductility [11], resistance (around 24% increment) and elasto-plastic behavior were
88 also obtained by Jové-sandoval et al. [16], who added different kinds of pine needles to adobe blocks (65.48% and
89 9.28% silt and 26.24% clay) in framework of comparative study with straw fibers, see Figure 3.

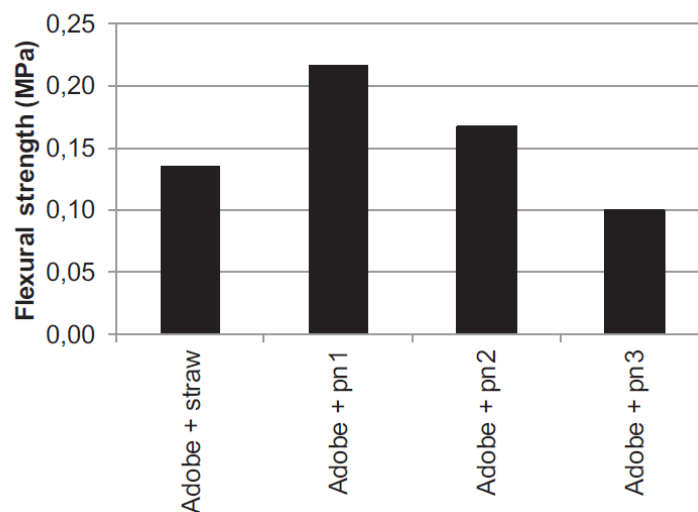


Figure 3-Resistance of adobe bricks reinforced with vegetable fibers [16]

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When embedded in thermosetting, thermoplastic or cementitious matrices [17], important composite materials can be crafted out of natural fibers. For construction fields, thermosetting matrices are the mostly applied ones, mainly epoxy resin-based matrices [18][19]. As composites used for external reinforcement, Yan et al. [20] studied flax fiber reinforced polymers FFRP under flat coupon tensile tests as a candidate for concrete confinement. In this study, a set of confined concrete cylinders from different strength rates (27.5 MPa and 32.8MPa) with bidirectional flax woven with different thicknesses were tested under uniaxial compression. Tests results exhibited remarkable enhancements in the ductility as well as the ultimate strength, around 51% increase in case of using 9 layers of FFRP with 32.8MPa-cylinders. Similar outcome was attained when Sen et al. [21] performed a comparative study between sisal/jute composites and carbon/glass composites to confine concrete cylinders. Indications stated in this study demonstrated that it is fairly comparable the axial load capacity increment obtained by sisal (66%) to that of carbon's (83%); especially since natural fibers FRP showed higher ductility and very similar confinement strength of GFRP's (17-18 MPa). The latter research coincided with the findings of Yan et al. [22], whom examined flax FRP comparatively with glass/carbon FRP, regarding the enhancements of the compressive strength and fracture energy [23] of concrete cylinders externally strengthened with.

In another trend of application, researchers suggested using natural fibers combined with synthetic fibers in hybrid composites, through which good mechanical properties, less footprint of carbon and economic advantages can be guaranteed [24][25][26]. In a study carried out by Padanattil et al. [27], concrete cylinders with compressive strength of 23 MPa confined with epoxy-based hybrid sisal-glass reinforced polymers were studied under axial compressive loading. Thereafter, the results were compared with different synthetic fibers composites and yet demonstrated better behavior, if compared with GFRP-confined samples, in terms of deformability, ductility and resistance, Figure 4.

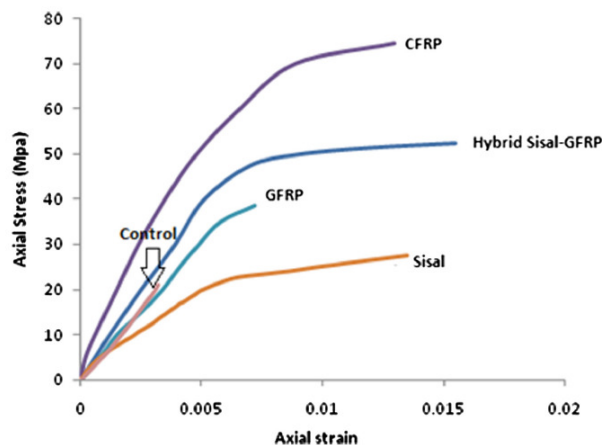


Figure 4-Stress-strain diagram of FRP strengthened samples [27]

3. Natural fibers composites and the strengthening of the built heritage

As the natural fibers provide good but limited enhancements to materials of high stiffness, such as concrete, see Figure 4, a new trend of research focusing on using them for external strengthening for weak structures has emerged.

3.1. Historical masonry behavior

Masonry structures show a significant behavior under axial compression loading, however, when masonry undergoes eccentric loads, seismic and out-of-plane loading, vulnerability owing to tensile stresses arises as a serious threat. For instance, Marcari et al. [28] studied the in-plane shear behavior of unreinforced masonry walls and observed sharp post-peak softening, limited ductility and low load carrying capacity, Figure 5. This trait might conditionally vary depending on the homogeneity, the variability of the different types of constituent materials and the structural function of the masonry (arch, walls, columns. etc.) [29].

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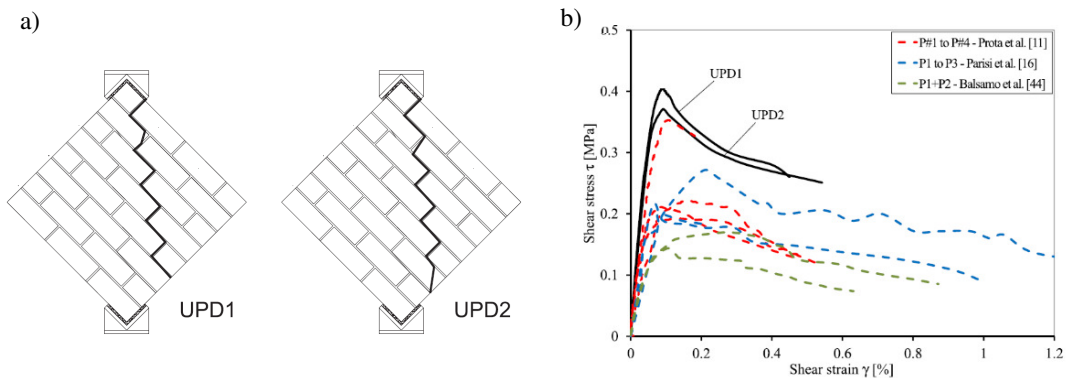


Figure 5- a) Masonry in-plane damage pattern, b) unreinforced masonry in-plane behavior [28]

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In addition to the significant results, in terms of tensile strength and energy absorption achieved by natural fibers composites (NFCs), the aptness of employment of these sustainable fibers for strengthening of built heritage and existing buildings is significantly growing. Further, their meeting to the compatibility criterion required for built heritage interventions by Venice Charter [30] and Cracow Charter [31] presents them as an appealing alternative to synthetic fibers.

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The practical implementation of NFCs as external-based reinforcement systems has been limitedly employed in a frame of TRM/FRCM [32] when embedded into lime [33][34] or cement matrices [35][36] to strengthen masonry walls [37] [38]. Yet, this solution showed significant developments of mechanical properties. Such solution was also studied as a hybrid composite materials conducted by consequent layers of natural fiber meshes and non-organic fabrics (sisal /glass) embedded into 10 wt% cement particles and achieved high flexural strength [39].

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3.2. Mechanical Improvements of structural components strengthened with NFCs

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Aiming at a better understanding of the contribution of NFCs to promote the mechanical behavior of structural elements strengthened with, researchers conducted different testing methodologies to accomplish so. When used as a seismic retrofitting system, the contribution of NFCs to improve the in-plane shear response of masonry was experimentally studied throughout shear tests, such as diagonal compression test (DCT). Both clay brick and tuff masonry have shown significant performance when strengthened with NFCs, e.g. hemp fibers [40]. In the latter study, Menna et al. [40], Figure 6, assessed the adequacy of hemp grids embedded into two different matrices (lime and

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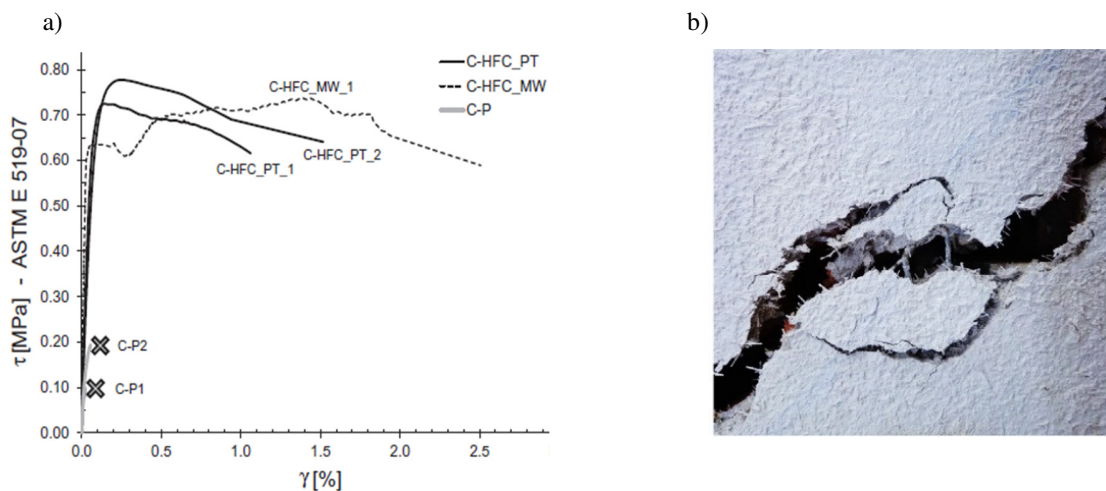


Figure 6- a) Strength increase of clay masonry, b) fibers rupture [40]

199 pozzolanic) to strengthen such masonry panels and consequently they added significant increments in the shear
200 strength and ductile behavior. Furthermore, bridging phenomena and fibers rupture along the diagonal crack pointed
201 out that the fibers reached their maximum tensile capacity.

202 Similarly, Olivito et al. [41] studied the effectiveness of NFCs casted from hemp, flax and glass fibers into cement
203 matrices throughout different typologies (grid and unidirectional diagonal strips) as reinforcements for clay masonry
204 walls. Afterward, it was observed that the load carrying capacity, ductility and deformability differ correspondingly
205 to the matrix kind also that flax grid endowed the highest increment of strength (around 90%), Figure 7. On the other
206 hand, in spite of glass-TRM provided higher ductility than flax-TRM, masonry strengthened with glass-TRM
207 experienced delamination phenomena and sudden collapse of the reinforcements. These results are in a good
208 agreement with numerical results of sisal fibers based-TRM solution, according to [42], where a macro-model was
209 developed and validated to predict the shear performance of masonry panels retrofitted with sisal-TRM.

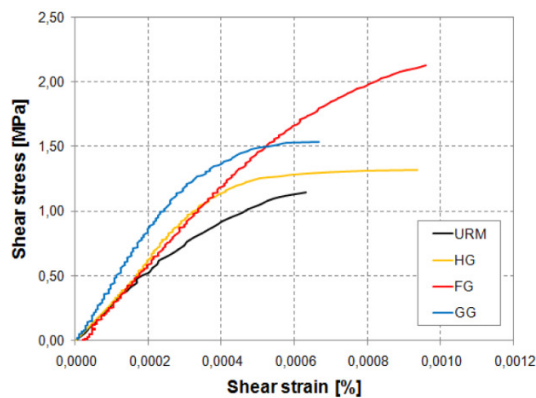


Figure 7-Shear stress-strain diagram [41]

226 The upgraded out-of-plane response of masonry walling elements repaired or strengthened with NFCs was also
227 detected under eccentric compression tests. In a study by Cevallos et al. [43], woven flax grids and PBO
228 (polyparaphenylene benzobisoxazole) fibers were independently impregnated in lime-based matrix and employed as
229 TRM. Consequently, the results delivered proposed that even though flax fibers have weaker mechanical properties
230 than PBO, their composites outperformed the PBO composites and showed more sufficiency to strengthen historical
231 masonry walls. That conclusion was reliant on the higher strength attained (more than 25% over PBO-strengthened
232 walls), higher ultimate strains and absence of debonding if compared to PBO-TRM. Another concordant results,
233 considering the study of [44], assured that the capacity of flax-FRCM to transfer the loading to the substrate to release
234 the stored energy, is a preferential aspect that highlights their compatibility to repair damaged masonry. Additionally,
235 the higher bending moment under eccentric loading, good deformability and the ability to restore stiffness might
236 extend the possibility of applying this repairing system to different kinds of loads [43] [44].

237 The capability of NFCs to sustain the tensile stresses when applied as external reinforcements for masonry arches
238 revealed important promotions in their global behavior if compared to FRP systems. Loccarini [45] characterized the
239 behavior of earthen masonry arches strengthened with jute-TRM along their extrados and intrados simultaneously
240 with specimens anchored with the jute fabrics wraps. Consequently, the reinforcement strips were capable to convey
241 the loading and modify the failure mechanisms by preventing the four-hinge mechanism, enhancing by that the load
242 bearing capacity over 100%.

243 The diversity of the mechanical enhancements that are possible to gain by NFCs might vary according to
244 reinforcements configurations [41]; as well as the conditions of application, e.g. matrix layers thicknesses [36];
245 reinforcements layers numbers. etc. This issue has been confirmed in framework of actual case studies [46] where
246 different levels of stability and ductility were delivered through using different typologies.

247 3.3. Tensile and bonding behavior of NFCs

248 Generally, the mechanical properties of natural fibers composites, namely tensile, bond strength and Young's
249 modulus, significantly increase by including the fibers, since they have much higher tensile strength than the matrices
250 themselves. However, the fact that the fiber content up to an optimum value or beyond combined with the several

251 technical processes conditions, such as fibers direction, are important factors that control the efficiency of the NFCs
 252 and may compromise the global performance of the composites [18].

253 In order to assess the competency of TRM tensile characteristics to improve the mechanical response of masonry
 254 panels, researchers performed uniaxial direct tensile tests, according to standards [47][48]. These tests have provided
 255 a considerable insight in composites tensile properties. By conducting tensile tests on NFCs manufactured from (sisal,
 256 jute and hemp) and separately embedded in different matrices (pozzolanic-lime and resins), Codispoti et al [37]
 257 characterized the efficiency of this system to resist tensile stresses. Subsequently, they concluded by that even if lime
 258 mortar-based NFCs showed lower tensile strength than resins-based NFCs, they have delivered higher ductility and
 259 deformability. As a result, this issue requires further investigation especially when applied to weak masonry substrates.
 260 A comparable study was performed by authors [34] and reported different tensile strengths when they applied lime
 261 matrix in different thicknesses. Thus, the main trait observed was the higher the thickness is, the less ability to
 262 distribute the stress along the composites and the lower tensile strength. In terms of failure mechanisms, researchers
 263 detected a similar trend of developing the matrix cracking patterns that occur in a gradual manner starting by the
 264 formation of the first crack and later ending up by several regular cracks in parallel to the stiffness losing [49] [34]
 265 [50]. The characterization of the adhesion stresses in fiber-to-matrix level is usually achieved throughout pull-out tests
 266 carried out on a fiber (mostly yarn) embedded into the matrix specimen [51]. Asprone et al. [52] performed pull-out
 267 tests on hemp strings and bundles, with different embedment lengths, coated with latex and resins and impregnated
 268 into pozzolana-based matrix. The results obtained revealed that latex delivered good degradation protection to the
 269 fibers and improved the bond strength, especially in case of short-embedded fibers. According to [53], the three tested
 270 fibers (sisal, curauà and jute) as reinforcements for cement-based matrix exhibited various behaviors depending on
 271 the length (5, 10 and 25 mm) especially in the post peak phase, namely in terms of ductility, see Figure 8.
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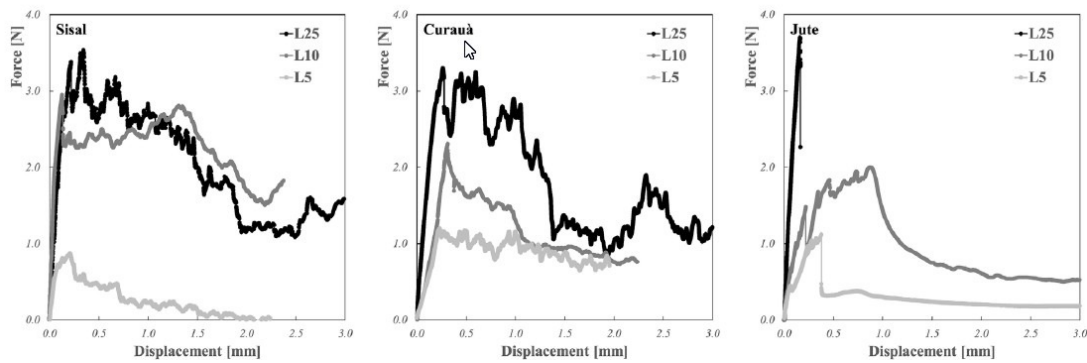


Figure 8- Typical pull-out behavior of natural fibers [53].

273 Essentially, the bond behavior at matrix-to-substrate level is governed by the two main factors of the adhesive
 274 nature and the mechanical characteristics of the substrate. Failure mechanisms can vary therefore, as depicted in Figure
 275 9 [50]. When the adhesive has lower strength than the substrate, a probable fracture in smooth surfaces within the
 276 interface in between might occur under so-called adhesive fracture. The cohesive failure takes place through the
 277 material (either the adhesive or the substrate). When this type of failure is combined with smooth fracture within the
 278 interfacial surface, it results in mixed fracture. To investigate the bond behavior within the interfaces between NFCs
 279 and masonry substrates, single or double lap shear bond tests have been employed through literature. In a comparative
 280 study between PBO and flax lime-based TRM, Olivito et al [54] observed through double-lap test that bond stress
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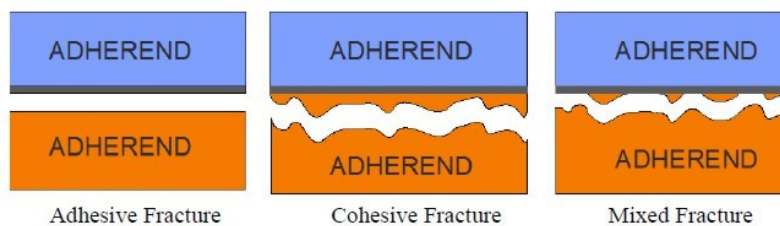


Figure 9-Possible failure mechanisms at adhesive-substrate level [50]

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290 values of flax composites are similar to the ones of PBO, which indicated that PBO fibers exploited less than 30% of
 291 their mechanical capacity unlike flax fibers. Moreover, the progressive cracking detected with flax-TRM
 292 demonstrated better ductile behavior than PBO that had a sudden delamination, see Figure 10, which is concordant
 293 with what other studies reported [43] [44].

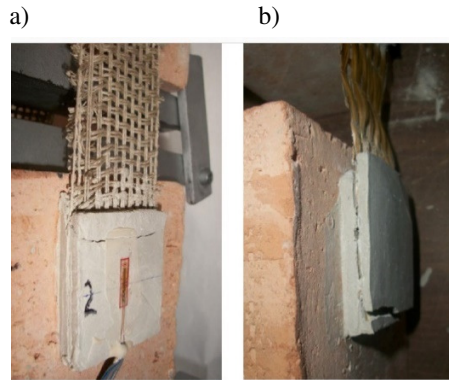


Figure 10-Failure modes of: a) Flax-TRM, b) PBO-TRM [54]

309 4. NFCs and challenges

310 In spite of natural fibers enable good bonding strength in the interface with matrices, their life cycle can be severely
 311 affected when embedded into inorganic matrices such as lime mortar or cement. Natural fibers have polar nature
 312 whereas the matrices have nonpolar nature, an issue that can interduce incompatibility problems when manufacturing
 313 the NFCs [55]. Every single natural fiber constitutes of several elementary natural fibrils joined together by means of
 314 a matrix of pectin [56], which is a complex structure [57]. In turn, every elementary fibril has an essential structure of
 315 three successive areas, as depicted in Figure 11. These areas are: the middle lamella that contains lignin, pectin,
 316 hemicellulose; the primary cell wall containing hemicellulose and cellulose; the secondary cell walls (S1, S2 and S3)
 317 contain mainly cellulose [56- 61].

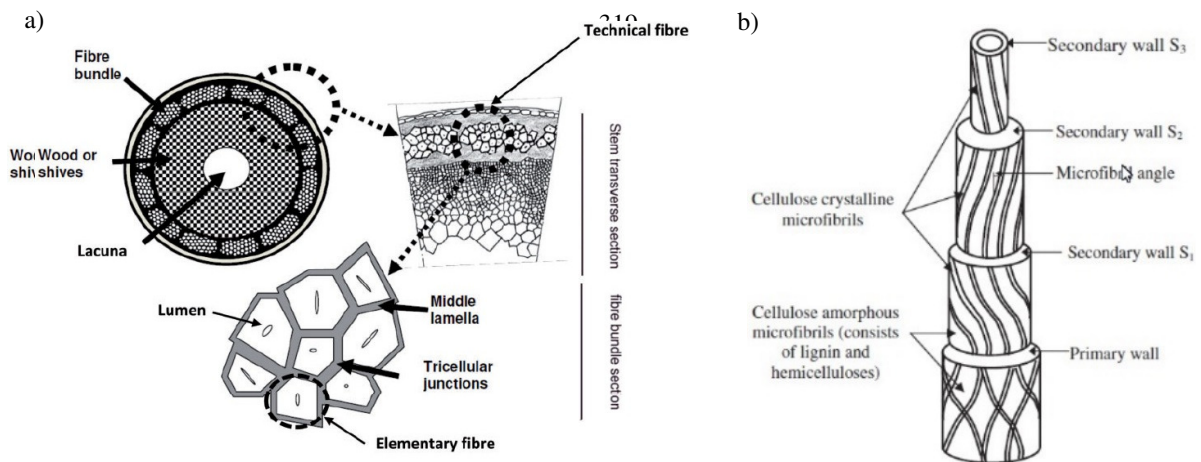


Figure 11-a) the structure of the technical natural fiber [57] , b) natural elementary fibril structure [72]

333 The crystalline materials, namely cellulose, are responsible for the good mechanical properties of the fibers, i.e. the
 334 tensile strength and Young's modulus. On the other hand, the other materials, hemicellulose acts as compatibilizer,
 335 lignin, pectin and waxes provide adhesives and matrices, are amorphous and have many irregularities [60]. These
 336 amorphous materials are rich with hydroxyl groups (OH) that result in a hydrophilic nature in the most of the natural
 337 plant fibers. These hydroxylic groups have extreme affinity to water molecules and tend to intensively bond with
 338 them. Accordingly, when embedding these fibers into inorganic matrices and especially the hydrophobic lime-based

339 matrices, serious impairments in their mechanical performance emerge as an actual challenge. These challenges are
340 due to the high-rate water uptake, represented by the diminishing of the efficiency to transfer tensile stresses.

341 Generally, the bond behavior between the fiber and the matrix occurs by means of mechanisms of mechanical
342 interlocking, electrostatic bonding, chemical bonding and inter-diffusion bonding [61][55]. In case of NFCs for
343 strengthening purposes, the mechanical interlocking governs the bonding phenomena relying to a high extent on the
344 roughness of the interface within the fiber-to-matrix surface. However, bonding strengths might be compromised
345 when the fibers absorb moisture from the matrix resulting in fibers swelling and diameter expanding. Thereafter, that
346 leads to micro cracking in the surrounding matrix to end up by total debonding or local delaminations [59].
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348 To overcome the aforementioned drawbacks, researchers proposed various solutions and treatments either at matrix
349 level, by including additive materials, or by subjecting the fibers themselves to a chain of treatments that can be
350 physical, thermal or chemical [62]. In this paper, the chemical treatments of low cost and easy application are of a
351 main focus prompted by the aim of possible applications to natural fibers for structural strengthening of historical
352 constructions. Moreover, since the lime mortar used for this field has shown significant compatibility to masonry
353 panels, the treatments derived from additive materials to the matrix may dilute this key trait.
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355 Through literature, various chemical treatments were exploited to reduce the hydrophilic nature of the natural
356 fibers. Hence, the chemical modification targets on degrading of the hydroxylic groups or/and occupying these groups
357 by their grafting with different reagents. The reagents have free radicals that have affinity to (OH) functional groups
358 as so a weak reactivity with water molecules is achieved. Different hydrophobic treatments were used [58-62] such as
359 acetylation [63], alkylation [64], silanization, acrylation, benzylation; treatments with isocyanate, permanganate,
360 peroxide, titanate, zirconate; maleated anhydride (MA) grafted coupling agents. Among these treatments, alkali
361 treatments, MA grafting, acetylation and silane treatments are the most common and studied with plant fibers as
362 surface modifiers. Alkaline treatment is usually conducted using NaOH that degrades the non-cellulosic compounds
363 (hemicellulose the most hydrophilic, lignin, etc.) exposing by that cellulosic materials that have better crystallinity
364 index. Fiore et al [64] applied alkali treatment on kenaf fibers for 48 hs and 144 hs and reported that the treatment
365 with 6% NaOH for 48 hs improved the compatibility to the hydrophobic resin matrix and mechanical properties.
366 However, after 144 h-treatment, the tensile strength of the treated fibers was less than that of the untreated ones. When
367 applying acetylation to flax fibers, Bledzki et al [63] observed high tensile strength and moisture absorption resistance
368 due to extraction of the waxy and non-cellulosic components. Though, the increase of the acetylation degree (beyond
369 18 wt%) led to an excessive degradation of cellulose which in turn resulted in decrease of the mechanical behavior.
370 In addition to increasing the mechanical properties of natural fibers, maleic anhydride has been noticed to improve
371 the hydrophobicity of natural fiber surfaces. In parallel, Stamboulis et al. [65] reported that when applying MA
372 treatment to flax fiber composites, they experienced 30% less moisture uptake than that with the green flax fibers. A
373 concordant hydrophobicity was also attained in a study by authors [66] where they used silane treatment for hemp
374 fibers, where a condensation reaction between hydrolyzed silane and hydroxyl groups of hemp resulted in low affinity
375 to water.
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377 Nevertheless, to comply with the sustainability of natural fibers, many researchers have recommended sustainable
378 and bio-based remedies that may afford considerable enhancements to natural fibers hydrophobicity, such as fatty
379 acids, plants oil, waxes [67], etc. For instance, Wei et al. [68] studied fatty acids derived from canola vegetable oil to
380 improve the hydrophobicity of cellulosic nanofibers, and accordingly they reported good hydrophobic behavior
381 through contact angle test (increase from 23° to 62°). Stearic acid is another fatty acid that has been studied for long
382 time and showed considerable hydrophobic trait when grafted onto different bio-plant-based surfaces [69]. Ye et al.
383 [70] also examined the efficiency of stearic acid grafted onto bio-based film of soy beans proteins to enhance water
384 absorption resistance and subsequently, good hydrophobicity (74%-increment) was attained, however, the tensile
385 strength decreased if compared to the non-grafted samples. Most recently, a promising bio-based remedial approach
386 depending on using enzymes to deliver higher water absorption resistance has been studied [3] [60] [71]. Enzymes
387 play a crucial role as a catalyst, mediator and non-cellulosic materials degrader. It is known that enzymes such as
388 xylanase, laccase, lipase and oxidases have good capability for the delignification. These bio-based treatments can be
389 found commercialized or prepared through fungal treatments [72], e.g. white rot fungus and taramites hirsute. For
390 example, not only noticeable increase in moisture absorption resistance (20-45%) and mechanical properties were
391 obtained when authors [73] treated abaca fibers by fungamix and natural enzyme, but also the improvements acquired
392 by these bio-based modifiers exceeded those perceived by MA.

393 **5. Conclusion**

394 Natural fibers are getting a huge interest amongst researchers owing to their sustainable, economical and good
395 mechanical properties when employed in different composites. For applications in strengthening and repairing of weak
396 structures, such as historical masonry, natural fibers composites (NFCs) may outperform synthetic fibers composites
397 in terms of compatibility and deformability under seismic loads. Nevertheless, many factors might affect the
398 performance and durability of NFCs; environmental factors represented mainly in weathering and aging; thermo-
399 chemo-physical characteristics, i.e. hydrophilicity. Therefore, apart from the non-bio-based coating systems, many
400 bio-based treatments were recommended by researchers to overcome such drawbacks. Hence, the effects of treatments
401 application procedures and conditions, the dependency between fiber content and mechanical behavior of the
402 composites and long-term durability have denoted the need for further studies.
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