

Ultra-Fast Low-Temperature Crystallization of Solar Cell Graded Formamidinium-Cesium Mixed-Cation Lead Mixed-Halide Perovskites Using a Reproducible Microwave-Based Process

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ABSTRACT

The control of morphology and crystallinity of solution-processed perovskite thin-films for solar cells is the key for further enhancement of the devices' power conversion efficiency and stability. Improving crystallinity and increasing grain size of perovskite films is a proven way to boost the devices' performance and operational robustness, nevertheless this has only been achieved with high temperature processes. Here, we present an unprecedented low temperature (<80 °C) and ultra-fast microwave (MW) annealing process to yield uniform, compact and crystalline $\text{FA}_{0.83}\text{Cs}_{0.17}\text{Pb}(\text{I}_{(1-x)}\text{Br}_x)_3$ perovskite films with full coverage and micrometer-scale grains. We demonstrate that the nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite films annealed at 100 W MW power present the same band gap, similar morphology and crystallinity of conventionally annealed films, with the advantage of being produced at a lower temperature (below 80 °C vs 185 °C) and during a very short period of time (~2.5 min vs 60 minutes). These results open new avenues to fabricate band gap tunable perovskite films at low temperatures, which is of utmost importance for mechanically flexible perovskite cells and monolithic perovskite based tandem cells applications.

KEYWORDS: Microwave annealing, fast low-temperature processing, micrometer-scale grains, mixed-cation lead mixed-halide perovskites, perovskite chemical composition.

1 INTRODUCTION

2 Organo-metal halide perovskites have emerged as an extremely promising photovoltaic (PV)
3 technology due to high power conversion efficiencies (PCE) and low fabrication cost. In a span of a
4 few years, the record single-junction efficiency of perovskite solar cells has reached 22.7%¹ making
5 it the most efficient solution-processed PV technology. Furthermore, their wide tunable band gap²
6 makes perovskites highly attractive for use in tandem solar cells, i.e. as top cells of narrower-band
7 gap absorbers such as silicon (Si) and copper indium gallium selenide (CIGS).³⁻⁵

8 One of the main challenges in the perovskite field is the fabrication of high quality films with controlled
9 morphology, high surface coverage and minimum pinholes.^{6,7} Factors such as charge dissociation
10 efficiency, charge transport and diffusion length of charge species are strongly dependent on the
11 film crystallinity. Therefore, the control of the crystallization and, thus, the kinetics of film formation
12 during deposition and annealing are the key to boost the performance of solution-processed
13 perovskite solar cells.⁸⁻¹¹ For this purpose, approaches such as solvent engineering,¹² inclusion of
14 additives into the precursor solution,¹³⁻¹⁷ substrate temperature,^{18,19} thermal annealing,²⁰ and
15 solution-processed methods²¹⁻²³ have been investigated by several research groups.

16 Recently, it has been shown that improvements in crystallinity and larger grain sizes can impact the
17 stability of the perovskite film^{19,24,25} and several solution-processed approaches to achieve
18 micrometer-sized perovskite grains have been reported.^{18,19} Usually, these approaches involve hot-
19 casting of the perovskite precursor solution onto a substrate maintained above the crystallization
20 temperature of the perovskite phase (i.e. between 145 °C up to 180 °C depending on the perovskite
21 chemical composition), which allows to extend the perovskite crystals growth, yielding large
22 crystalline grains. Clearly, a lower temperature annealing process that allows full crystallization of
23 the perovskite, keeping the morphological, structural, and optoelectronic quality of the films
24 processed at higher temperatures, can be of major importance for the entire field of perovskite-based
25 PV. In particular, it is crucial to enable novel device architectures such as perovskite tandem solar
26 cells, and to allow integration in mechanically flexible substrates.²⁶⁻²⁸ In this context, microwave-
27 driven annealing is a promising approach, as it is known that its processing temperature and time
28 can be lower when compared to conventional thermal annealing.^{29,30}

1 Microwave heating uses the ability of some compounds (liquids or solids) to transform
2 electromagnetic energy into heat (coupling at the molecular level).³¹ Energy transmission is
3 produced by dielectric losses, and the magnitude of heating depends on the dielectric properties of
4 the molecules, which means that the absorption of radiation and consequent heating may be
5 performed selectively. In contrast to conventional heating (which is slow and relies on surface
6 heating), microwave irradiation is rapid and volumetric, with the whole material heated
7 simultaneously.³² In many processes of industrial interest the volumetric heating provides significant
8 reductions in the processing time and energy savings.

9 Mamun *et al.*³³ reported the use of microwave (MW) irradiation for rapid (≤ 8 min) and low
10 temperature (≤ 260 °C) production of nanocrystalline titanium dioxide (nc-TiO₂) films with similar
11 optical, morphological and structural properties of the conventionally annealed films. The rapid
12 fabrication time was not only attributed to direct absorption of MW energy by FTO coating in close
13 contact with the TiO₂ film, allowing effective and efficient heat transfer from FTO to nc-TiO₂, but also
14 to the ability of organic molecules (solvent and binders present in the TiO₂ paste) to absorb MW
15 radiation efficiently.

16 Recent studies related to MW annealing of methylammonium lead iodide perovskite films
17 (CH₃NH₃PbI₃) show that this technique provides a fast and less energy-intensive process for the
18 manufacture of perovskites,^{34,35} however under the conditions tested (fixed MW power and varying
19 the irradiation time) no advantage was observed regarding the processing temperature (i.e. the
20 crystallization temperature of MW annealing at ~ 100 °C was similar to that of thermal annealing
21 methods).

22 In this work, we report a versatile and ultra-fast microwave (MW) annealing process to produce highly
23 crystalline formamidinium-cesium mixed-cation lead mixed-halide perovskite films with micrometer-
24 scale grains and preferred crystal orientation, at low temperatures (< 80 °C), processed at ambient
25 atmosphere. Moreover, an innovative combined characterization toolset was developed to determine
26 the real composition of mixed-cation lead mixed-halide perovskite films, showing that the
27 stoichiometry can change with respect to the expected one (from the precursor solution preparation
28 used). This is crucial for the fabrication of perovskite films with reproducible opto-electronic
29 properties.

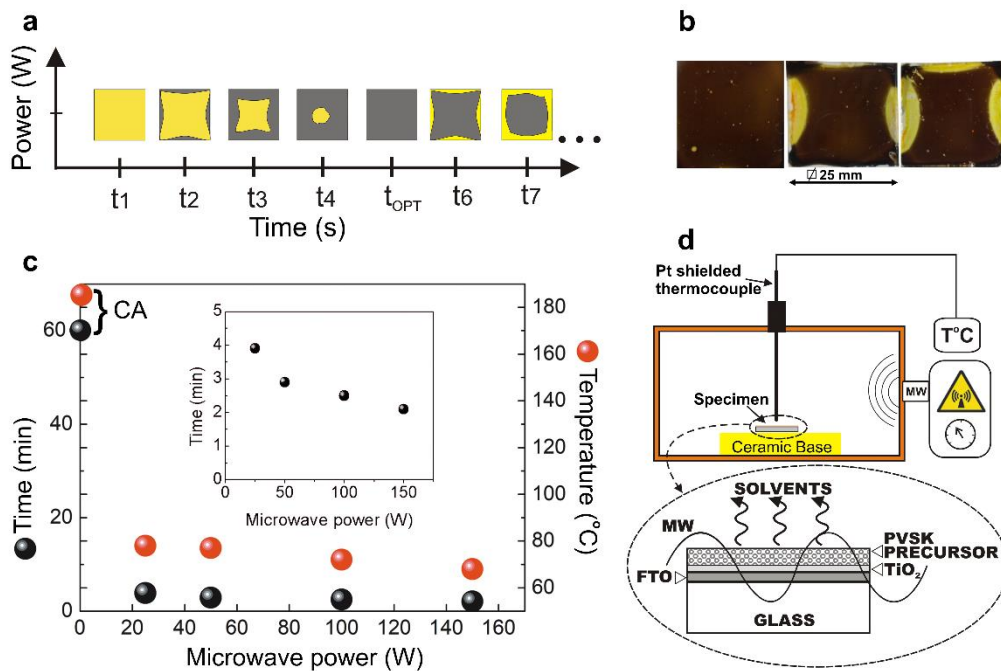
1 RESULTS AND DISCUSSION

2 Low-temperature crystallization of mixed-cation lead mixed-halide perovskite films

3 Here we test the MW annealing process with state-of-art perovskites using formamidinium (FA) and
4 cesium (Cs) mixed cation/ iodide-bromide mixed anion perovskites formulations of nominal
5 composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$.³⁶ The selection of this wide-bandgap perovskite as test bed is
6 based on its crystallization temperature (185 °C) and long crystallization time, improved photo-,
7 moisture and thermal stability, excellent opto-electronic properties (charge-carrier mobility exceeding
8 $20 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$) and its ideal band gap ($\sim 1.74 \text{ eV}$) for top sub-cells in double-junction tandem solar
9 cells.^{10,11,36,37}

10 The perovskite films with the nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ were deposited on compact
11 TiO_2 layer (prepared as described elsewhere³⁸) by spin coating a mixture of PbI_2 , PbBr_2 , FAI and CsI
12 in *N,N*-dimethylformamide (DMF) and using acidic additives (hydriodic acid, HI, and hydrobromic
13 acid, HBr).^{11,36} Microwave annealing was performed at powers of 25, 50, 100 and 150 W, and the
14 irradiation time (t_i) was set initially by visual inspection of the color change throughout the sample
15 surface during the crystallization process. For comparison sake, cycles in a conventional annealing
16 (CA) oven were performed. The annealing program followed a multi-step heating up to 185 °C, being
17 60 minutes the time from room temperature up to the end of the annealing plateau. In all cases, the
18 films were annealed in ambient atmosphere.

19 In Figure 1a we show a schematic representation of the perovskite crystallization evolution with MW
20 irradiation time at a fixed power. The crystallization starts on the near-edge region and continues
21 towards the sample's center. This is due to the edge effect that occurs when electromagnetic waves
22 diffract on the specimen's edge, rising locally the temperature, and consequently starting the
23 crystallization on that site.³⁹ The magnitude of the specific heating power depends on the polarization
24 and propagation direction of the incident electromagnetic waves. The spatial non-uniformity of the
25 absorbed power is noticeable when the wave vector is parallel to the sample surface but
26 perpendicular to the sample edge.



1

2 **Figure 1.** Microwave annealing of $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite. **a** Schematic representation of
 3 perovskite crystallization evolution with MW irradiation time (t). **b** photograph of a perovskite film for
 4 $t=t_{\text{opt}}$ (left photo); and $t > t_{\text{opt}}$ (center and right photos) where visible degradation starts to occur from
 5 the edges; **c** Optimum MW irradiation time (t_{opt}) (black) and maximum measured temperature at $t=t_{\text{opt}}$
 6 (red), as a function of MW power (inset: magnification on the range 0 to 5 min), compared with the
 7 CA time (60 min) and temperature (185 °C) of perovskite films with nominal composition
 8 $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ deposited on FT0/compact TiO_2 . **d** Schematic representation of perovskite
 9 MW annealing process.

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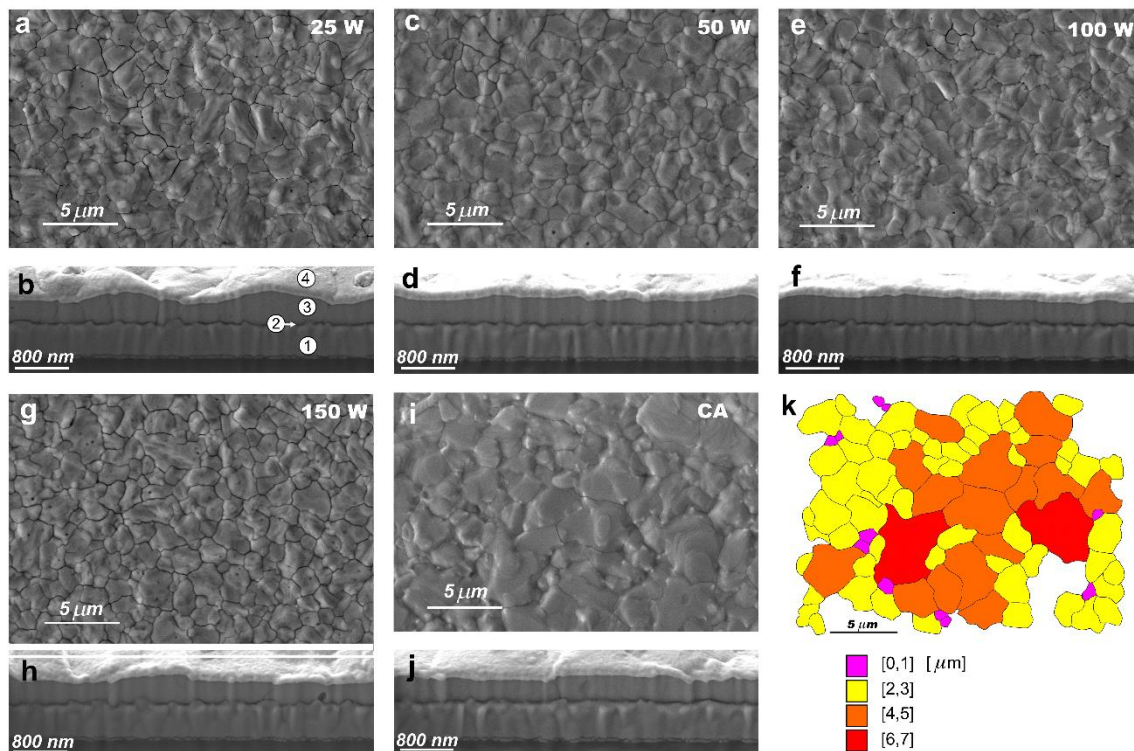
11 This edge effect can be overcome with the use of a shield for the incident waves, e.g. aluminum thin
 12 sheet (10 μm), positioned around the sample edges to attenuate the MW radiation, leading to an
 13 improvement of the temperature uniformity of the sample.³⁹ The consideration of the MW penetration
 14 depth into a material is of great significance to an efficient and uniform MW heating process. In order
 15 to have the whole material coupling with MW, the sample's dimension should be comparable to the
 16 penetration depth, so that the entire sample can be irradiated by MW radiation to get the maximal
 17 heating rate. In the present case, the stack thickness ($\sim 1 \mu\text{m}$) of FT0, TiO_2 and as-deposited
 18 perovskite film is within the dimension of the respective MW penetration depth (DMF penetration
 19 depth is 0.46 cm⁴⁰), allowing the materials to be heated by direct microwave dielectric heating.

20 For each MW power, there is an optimum irradiation time (t_{opt}) (Figure 1b, left photo), after which
 21 perovskite degradation begins to occur, also starting from the edges towards the sample center (as

1 shown in Figure 1b, center and right photos). As expected, t_{opt} decreases, from 4 to 2 min, with the
2 increase of MW power (Figure 1c), and for all the MW powers tested the perovskite crystallization
3 occurs at a temperature below 80 °C.

4 In Figure 1d a schematic representation of the perovskite MW annealing process is shown. The
5 residual polar solvent (DMF) present in the as-deposit perovskite film absorbs MW energy due to its
6 high dielectric constant ($\epsilon = 37.51$ at 25°C). The DMF's dipoles are sensitive to external electric fields
7 and will attempt to align themselves with the field by rotation. At the used frequency, 2.45 GHz, the
8 dipoles do not have enough time to be constantly aligned to the oscillating field, colliding to one
9 another and the power is dissipated by heat generation in the material. This MW heating will promote
10 the quick evaporation of the solvent and consequently the crystallization of perovskite material. The
11 constituents of the substrate, i.e. FTO and TiO₂, have also their own contribution to MW heating. The
12 TiO₂ showed moderate coupling to microwaves because it is a stoichiometric semiconductor having
13 both low electrical conductivity and low magnetic induction loss.⁴¹ On the other hand, knowing that
14 FTO is a non-stoichiometric semiconductor with high electrical conductivity, material-MW coupling
15 is possibly correlated with high concentration of conduction electrons and the temperature rise
16 attributed to induction losses from electron conduction. The two mentioned MW heating
17 mechanisms, i.e dipolar polarization and conductive mechanisms work together and are responsible
18 for the rapid, low temperature and controllable crystallization of perovskites films.

19 The top-view and cross section scanning electron microscope (SEM) images for each MW- and CA-
20 perovskite films are shown in Figures 2a-j. To evaluate the uniformity of surface morphology of each
21 MW- and CA-perovskite films, five different regions (an area of approximately 2 cm² in the center of
22 each sample) were chosen randomly to obtain SEM images at low magnification (5000 x). Figure S2
23 exemplifies the surface uniformity assessment for the 100 W-perovskite film.



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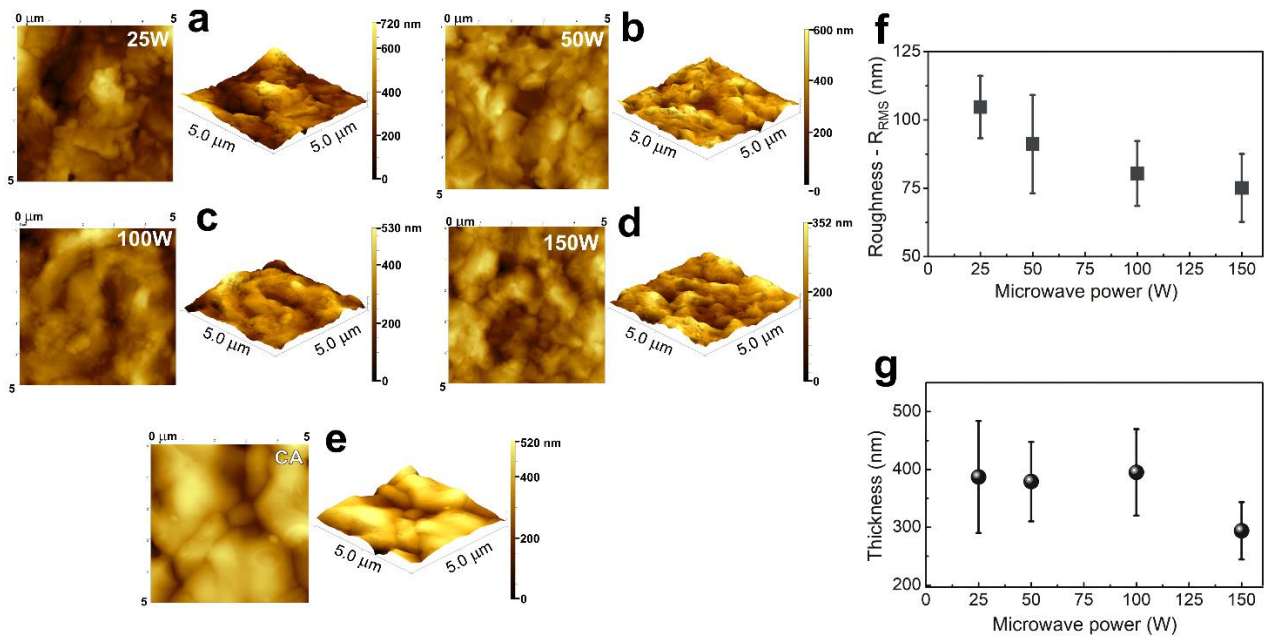
3 **Figure 2.** Characterization of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite films after
 4 different annealing conditions. The SEM analysis was performed with top-view images (upper ones)
 5 of the MW-perovskite films (**a** 25 W, **c** 50 W, **e** 100 W, **g** 150 W) and of the CA-perovskite film (**i**), as
 6 well as cross section images (bottom ones) of the same films (**b** 25 W, **d** 50 W, **f** 100 W, **h** 150 W
 7 and **j** CA). The layers indicated by the labels 1, 2, 3 and 4 in **b** correspond to FTO, compact TiO_2 ,
 8 perovskite and gold, respectively. **k** Grain boundary map of the CA-perovskite SEM image (**i**)
 9 obtained by Digital Image Analysis, showing the different grain size classes.

10

11 All perovskite films are compact and pinhole-free, which is highly desirable for efficient perovskite
 12 solar cell fabrication. As displayed in the cross-section SEM images (Figures 2d, f, h, j), perovskite
 13 films annealed at 50, 100 and 150 W MW power and conventionally annealed films show a uniform
 14 thickness (around 379, 395, 294 and 367 nm, respectively). At 25 W MW power, a significant film
 15 thickness variability is observed (Figure 2b, thickness variation between 270 and 565 nm), being the
 16 thickness average of 387 nm. The thickness decrease of the perovskite film annealed at 150 W is
 17 due to the degradation of the film, i.e. loss of mass associated to the organic cation, which is
 18 confirmed by the appearance of the peak of PbI_2 at $2\theta \sim 12.7^\circ$ in the XRD pattern (Figure 5a).

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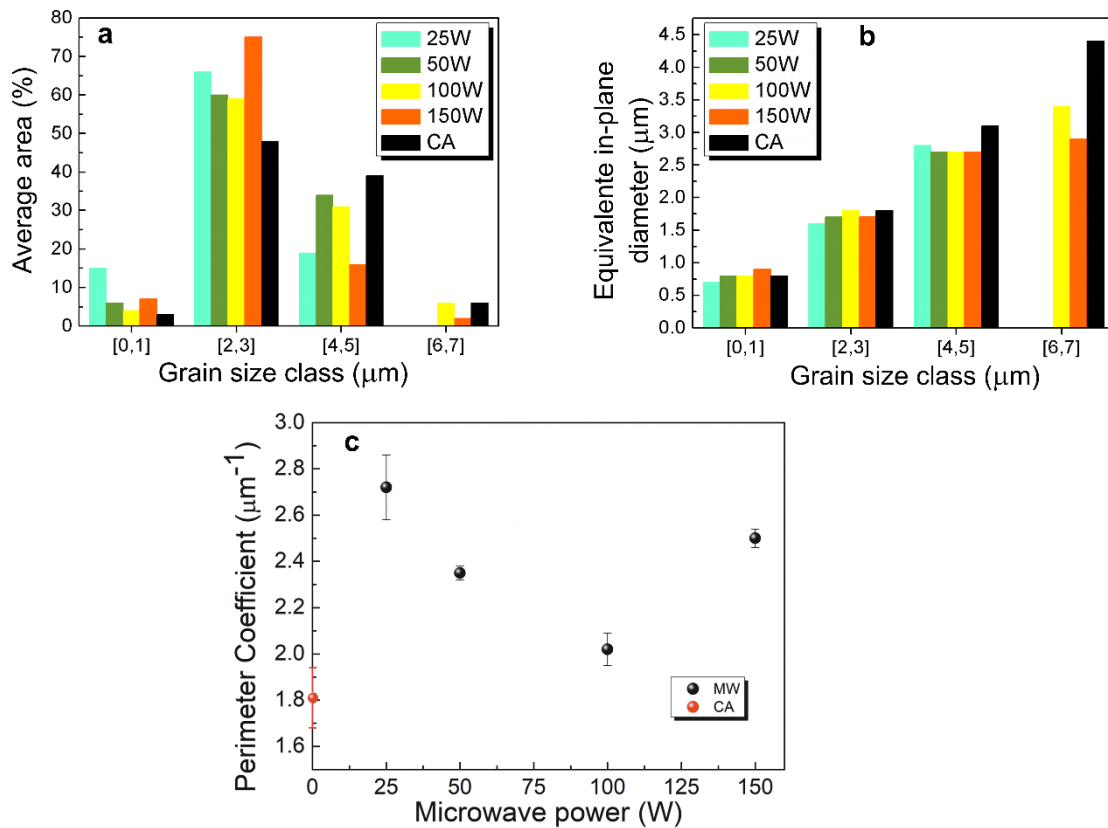
2 **Figure 3.** AFM images ($5 \times 5 \mu\text{m}^2$) of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{Pb}_{1.8}\text{Br}_{1.2}$ perovskite films after
 3 different annealing conditions (**a** 25 W, **b** 50 W, **c** 100 W, **d** 150 W and **e** CA) in an area of $5 \times 5 \mu\text{m}^2$.
 4 **f** Perovskite film root mean-square roughness (R_{RMS}) (average of 3 different film regions) and **g**
 5 thickness (average of 10 measurements by SEM-FIB cross section analysis) as a function of MW
 6 power. The error bars represent the standard deviation from the mean.

7

8 Top-view and 3D AFM images for each MW- and CA-perovskite films are shown in Figures 3a-e.
 9 The root-mean-square surface roughness (R_{RMS}) of the perovskite films was found to decrease with
 10 the increase of MW power (Figure 3f). Compared to the CA- perovskite film ($R_{\text{RMS}}=73.1 \text{ nm}$) the 100
 11 W processed specimens showed a slightly higher R_{RMS} (80.4 nm), whilst the 150 W ones showed a
 12 similar value (75.1 nm).

13 To help establishing the relationship between MW power and grain size of the MW-perovskite films,
 14 we studied the mean dimensions of the grains in the films, namely the equivalent in-plane diameter,
 15 average area and perimeter coefficient (ratio between the total perimeter and the total area of the
 16 grains), determined by a Digital Image Analysis in-house procedure (Figure 4k) described in
 17 supporting information (SI).

18



1

2 **Figure 4.** Digital image analysis of the perovskite grain size. **a** Average area percentage of each
 3 grain size class and, **b** Equivalent in-plane diameter of the grains in CA- and MW-perovskite films,
 4 for each grain size class, **c** Perimeter coefficient of the grains in CA- and MW-perovskite films as a
 5 function of MW power.

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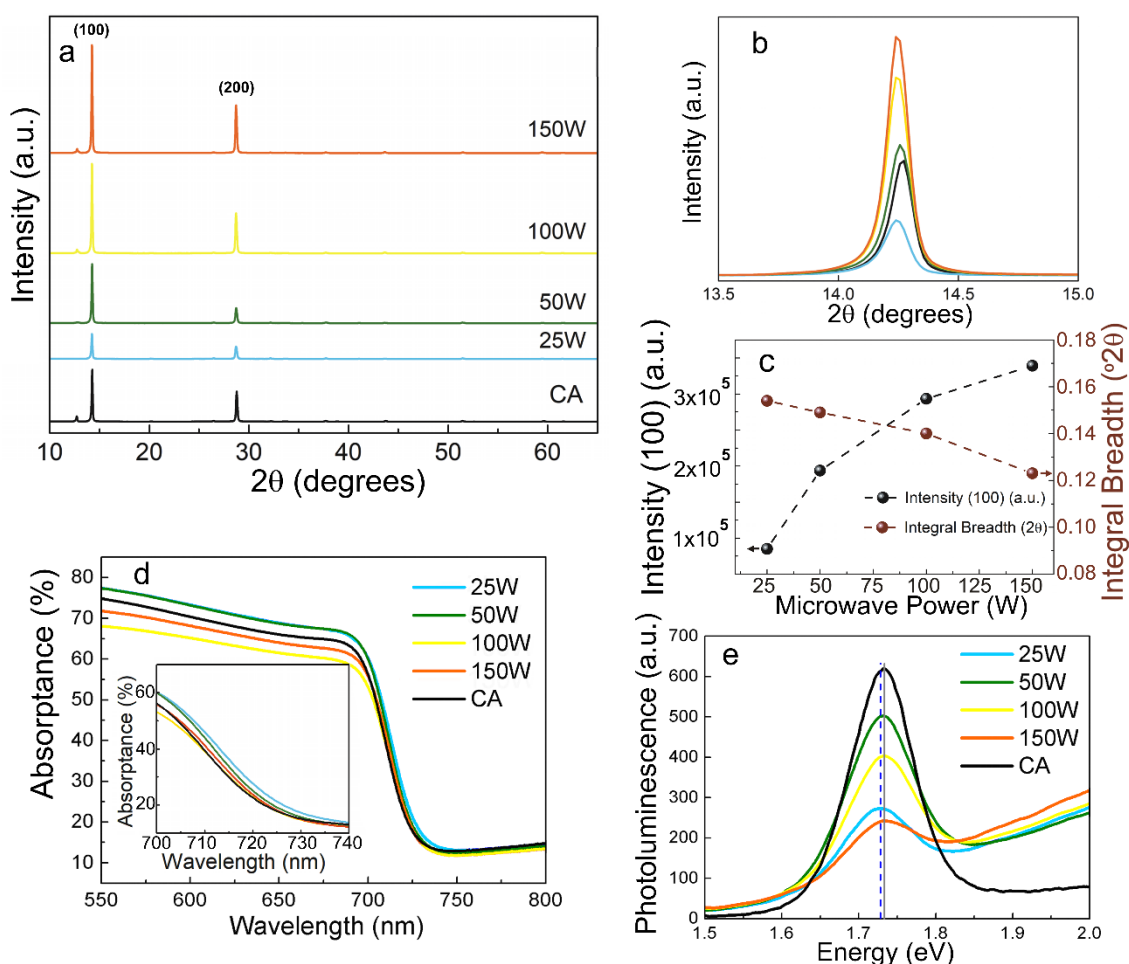
7 As shown in Figure 4a, for the perovskite films processed at 25, 50 and 100 W, the average area of
 8 the [0,1] and [2,3] grain size classes (i.e. the classes with smaller grain sizes) decreases with
 9 increasing power. On the other hand, the average area of the [4,5] and [6,7] classes seems to
 10 increase with MW power, being this at the expense of the immediately preceding grain size class,
 11 i.e. larger grains grow at the expense of smaller ones (Ostwald ripening).⁴² These findings are more
 12 noticeable in perovskite films processed at 100 W. In fact, the average area of the [0,1] class
 13 decreases from 15% to 4% when the MW power is increased from 25 to 100 W, and at the same
 14 time the average area of the [4,5] and [6,7] grain size class increases from 19% to 31% and from
 15 0% to 6%, respectively. As shown in Figure 4b, the equivalent in-plane diameter is approximately
 16 constant within each grain size class for all the specimens, regardless of the MW power used. On
 17 the other hand, regarding the values of the perimeter coefficient calculated for each specimen, Figure
 18 4c, there is a decreasing trend as the MW power increases from 25 to 100 W, due to the increase in

1 the particle size and consequent decrease in the total particles perimeter (see digital image analysis
2 procedure in SI). However, this trend changes for the specimens processed at 150 W, as such high
3 power seems to go beyond the maximum balanced MW power for the annealing of this type of
4 perovskite. Therefore, it is preferential to MW-anneal the perovskite films at applied powers around
5 100 W, yielding a similar perimeter coefficient value to that of CA-perovskite films, and presenting
6 an equivalent morphology.

7 To understand the impact of MW annealing on the formation and crystallization of perovskite phases,
8 we performed X-ray diffraction (XRD) measurements on the perovskite films. As presented in Figure
9 5a, all XRD patterns show high intensity peaks, corresponding to the (100) and (200) reflections from
10 characteristic planes of the cubic perovskite, indicating a highly preferred orientation along these
11 directions. In Figure 5b, we show the XRD pattern zoomed around the (100) peak of perovskite films
12 at $2\theta \sim 14.25^\circ$, processed at 50 W, 100 W and 150 W MW power and for CA films.

13 In the case of 25 W-perovskite films, a small shift to lower angles is observed ($2\theta \sim 14.23^\circ$) for the
14 (100) peak (Figure 5b) when compared with the other MW annealed samples, suggesting a
15 perovskite composition with higher content of iodine.^{10,36} Peak profile deconvolution was used to
16 assess the $K\alpha_1$ peak position. From Figure 5c, we observe that the intensity of the peaks increases
17 with increasing MW power, and the integral breadth values of the (100) peak decrease with
18 increasing MW power, indicating a higher crystallinity in the samples annealed at higher power.

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1

2 **Figure 5.** Structural and optical characterization of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$
 3 perovskite films deposited on FTO/compact TiO_2 substrates. **a** XRD patterns for CA- and MW-
 4 perovskite films. **b** Detail of the XRD patterns of the films for 2θ from 13° to 15° ; **c** Intensity and
 5 integral breadth ($^\circ 2\theta$) of the (100) diffraction peak as a function of MW power; **d** UV-Vis absorbance
 6 spectra (inset: magnification on the range 700 to 740 nm) and **e** Steady-state photoluminescence
 7 (PL) spectra.

8

9 The absorbance spectra of CA and MW-perovskite films exhibit comparable optical properties with
 10 a strong absorption in the range of 550–700 nm, as shown in Figure 5d. From the absorption profile,
 11 a slight red-shift of the band edge is visible for the 25W-perovskite. The band gap energy (E_g) was
 12 estimated from the reflectance measurements by applying the modified Kubelka–Munk ($F(R)$)
 13 method using the equation: $F(R) = (1-R)^2/2R$ and plotting $(F(R) \times h\nu)^2$, as a function of the photon
 14 energy ($h\nu$) in eV, where R is the reflectance, h is the Planck's constant (J.s) and ν is the light
 15 frequency (s^{-1}).⁴³ An E_g of ~ 1.72 eV was obtained for CA and MW-perovskite films (Figure S1 of SI),
 16 with the exception of the 25 W-perovskite that shows a slightly lower band gap (E_g 1.71 eV),

1 indicating a slightly higher content of iodine in the perovskite's composition.³⁶ This band gap shift
2 was also detected using the photoluminescence (PL) emission spectra, as presented in Figure 4e.
3 The slight red-shift of the band edge observed in the absorptance spectra of 25 W-perovskite film
4 and the lower band gap value obtained ($E_g = 1.71$ eV) are also in agreement with the small shift to
5 lower angles observed ($2\theta \sim 14.23^\circ$) for the (100) peak in the XRD pattern (Figure 5b).
6 It is noteworthy that the perovskite films annealed at 100 W microwave power present the same
7 band gap ($E_g = 1.72$ eV) and similar morphology and crystallinity of conventionally annealed films,
8 with the advantage of being produced at a lower temperature (below 80 °C vs 185 °C) and during a
9 very short period of time (~2.5 min vs 60 minutes). As demonstrated here, the ultra-fast MW
10 annealing process not only entails a low temperature fabrication of full coverage, crystalline
11 perovskite films with micrometer-scale grains and preferred crystal orientations, but also allows
12 simultaneously improving crystallinity and increasing grain size, through optimization of MW settings,
13 such as power and irradiation time.

14

15 **Perovskite chemical composition upon crystallization**

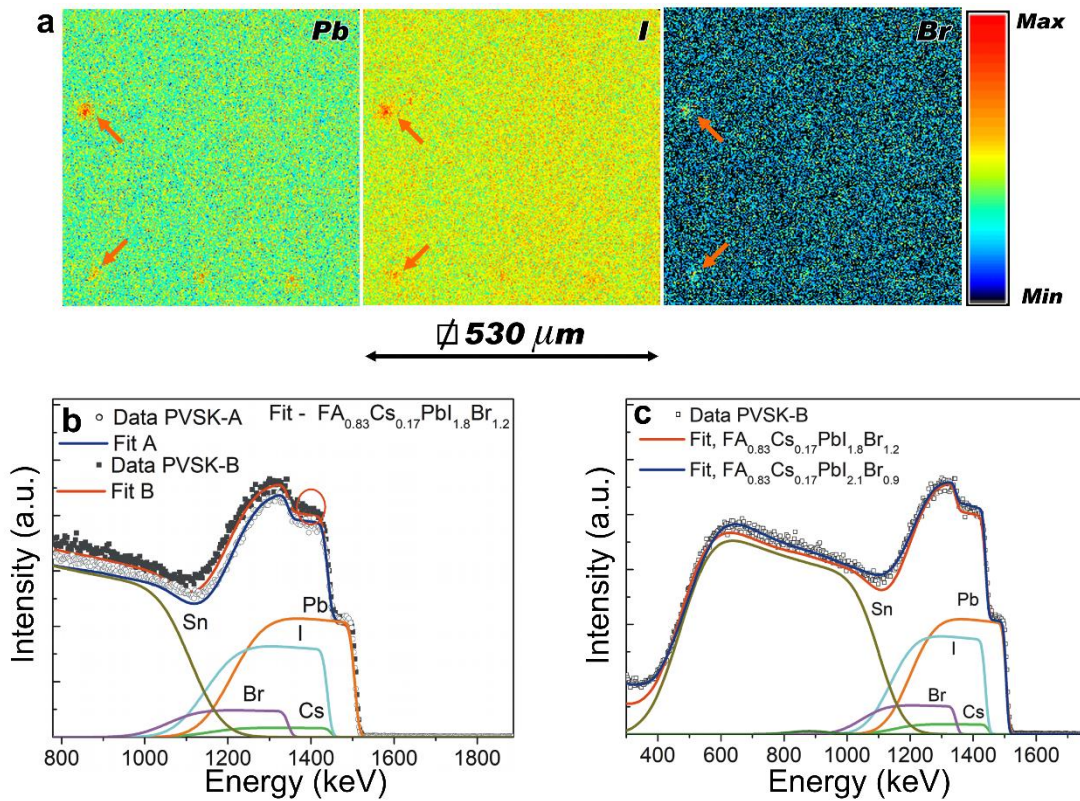
16 The estimated band gap values of both MW (100 W) and CA $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ films ($E_g = 1.72$
17 eV for both films) are lower than the previous reported band gap ($E_g = 1.74$ eV) for this particular
18 nominal composition.³⁶ This can be attributed to the fact that the perovskite chemical composition in
19 the fabricated films may differ from that which is estimated upon mixing the perovskite precursor
20 compounds in the precursor solution. Therefore, we set out to investigate this aspect, as it is of major
21 relevance for all perovskite applications.

22 To this end, we used Ion Beam Analysis (IBA) techniques⁴⁴ to assess the lateral and in-depth
23 elemental composition of the perovskite films (see supporting information, SI) by means of 2D
24 Particle Induced X-ray Emission (2D-PIXE) maps⁴⁵ and Rutherford Backscattering Spectrometry
25 (RBS)⁴⁶ following the Total IBA approach.⁴⁴

26 For this study, two sets of five conventionally-annealed perovskite films³⁶ were prepared from two
27 independent perovskite precursor solutions (solution A and B) with nominal composition
28 $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$, and the band gap was determined for all films based on diffuse reflectance
29 measurements, as described previously (Table S1). Two films were then selected, one from each

1 precursor solution (solution A and B), that presented a band gap similar to that previously reported
 2 in the literature for this particular nominal composition³⁶ (Figure S3). IBA measurements were carried
 3 out on the selected films, referred here as PVSK-A ($E_g = 1.74$ eV) and PVSK-B ($E_g = 1.73$ eV) (Table
 4 S1 and Figure S3), which were also characterized by SEM, Energy Dispersive Spectrometry (EDS),
 5 Digital Image Analysis and XRD techniques (see Figures. S4, S5, S6 and Table S2 in SI).
 6 For illustration, Figure 6a shows the 2D-PIXE elemental distribution maps obtained for PVSK-A using
 7 a 2 MeV proton beam (equivalent maps for PVSK-B are presented in Figure S7).

8



9

10 **Figure 6.** Elemental analysis and depth profile of CA perovskite films. **a** 2 MeV H^+ 2D-PIXE elemental
 11 distribution maps of PVSK-A for Pb (left), I (middle) and Br (right). Red arrows indicate local
 12 heterogeneities; **b** 1.6 MeV He^+ RBS experimental data and fits of PVSK-A (open grey circles and
 13 blue line) and PVSK-B (black squares and red line) films (elemental contributions to the fits are also
 14 shown), using nominal composition. The difference between film thicknesses is given by the different
 15 widths of the spectra. The red circle marks an underestimation of I content. **c** 1.6 MeV He^+ RBS data
 16 (open circles) and fits assuming nominal composition (red line) or composition obtained from PIXE
 17 (blue line) for PVSK-B. Also shown are the individual elemental contributions for the blue line fit.

18

1 The multi-elemental distribution over the surface presents a quite large uniform area, pointing
 2 towards an overall homogeneous chemical composition of the film. Small local heterogeneities can
 3 be observed (red arrows), concerning regions of higher intensity for the three elements shown, that
 4 were found to be related to thicker perovskite crystals.

5 From similar maps obtained for the PVSK-A and PVSK-B films, three homogeneous areas (~90x90
 6 μm^2) were chosen to simultaneously record the PIXE and RBS spectra. PIXE and EDS results of Pb,
 7 I and Br are expressed in atomic fraction normalized to the Pb content (Table 1). Although probing
 8 different sample depths (i.e. the entire material layer is probed by the 2 MeV proton beam, whereas
 9 EDS information is gathered over a shallow sample depth), and in spite of the higher uncertainty of
 10 EDS, the results are consistent. PIXE and EDS provided similar Br values, indicating a chemical
 11 composition different from the nominal one ($\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$) and still different between PVSK-
 12 A and PVSK-B films, as expected.

13

14 **Table 1.** EDS and PIXE analysis of Pb, I and Br in perovskites PVSK-A and PVSK-B. The results
 15 are expressed in atomic fraction normalized to the Pb content.

Sample	Eg (eV)	PIXE atomic fraction			EDS atomic fraction		
		I	Br	I/Br	I	Br	I/Br
PVSK-A	1.74	2.02 ± 0.08	0.98 ± 0.02	2.0	1.99 ± 0.09	0.95 ± 0.04	2.0
PVSK-B	1.73	2.14 ± 0.03	0.91 ± 0.03	2.3	2.0 ± 0.2	0.9 ± 0.1	2.2

16

17 Although the band gap value of PVSK-A is consistent with previous reports,³⁶ the I/Br ratio obtained
 18 is higher than that of the precursor perovskite solution (I/Br ratio 1.5), corresponding to a real
 19 composition in the film of $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{2.0}\text{Br}_{1.0}$. As shown in Fig S5, the PVSK-A XRD pattern
 20 exhibits the two characteristic peaks of perovskite at 14.31° and 28.84° which are assigned to the
 21 (100) and (200) crystal planes, respectively. The slight variation in chemical composition of PVSK-A
 22 and PVSK-B films is in accordance with XRD results (Table S2) and with the different measured
 23 band gaps (Figure S3), since lower Br content in the perovskite chemical composition decreases the
 24 band gap and shifts the diffraction peaks to lower 2θ values.^{10,36}

1 Figure 6b shows the RBS experimental spectra obtained for PVSK-A and PVSK-B, using 1.6 MeV
2 alpha beam together with the best fits, considering: a) a single layer of perovskite with the nominal
3 composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$, followed by a TiO_2 compact layer, a F-doped SnO_2 (FTO) and
4 glass layers and b) the interface roughness to increase the energy spread resolution as a function
5 of depth.⁴⁷

6 The RBS results show that a single layer of perovskite is enough to achieve good fits, indicating an
7 in-depth uniform material composition which contrasts to that previously found for MAPbI_3
8 perovskites⁴⁸. Moreover, the different width of the Cs, Br, I and Pb signals observed in the RBS
9 spectra correspond to a ~4% thickness difference between PVSK-A and PVSK-B films (2434×10^{15}
10 at/cm^2 and $2534 \times 10^{15} \text{at}/\text{cm}^2$, respectively). Also comparing the fit curves with experimental data it
11 is noticeable that the I surface barrier height (proportional to the I content) is slightly underestimated,
12 being this difference more evident for PVSK-B (red circle in Figure 6b). This finding indicates the
13 need to consider a higher value of I in the perovskite film to achieve a better fit, which is in agreement
14 with PIXE results (Table 1).

15 As shown in Figure 5c, for PVSK-B, when considering a single layer of perovskite with the chemical
16 composition obtained by PIXE ($\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{2.1}\text{Br}_{0.9}$), the corresponding RBS fit (blue line) displays
17 a closer agreement with the experimental data than that obtained for the nominal composition (red
18 line). Using the same approach for PVSK-A films (Figure S8), a better RBS fit was also achieved
19 considering the chemical composition obtained by PIXE analysis ($\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{2.0}\text{Br}_{1.0}$). These
20 results show that, through a total IBA approach it is possible to set and measure the difference
21 between the real composition of the crystallized perovskite and the nominal content in its precursor
22 solution, confirming at the same time the perovskite in-depth composition uniformity.

23 This study demonstrates that $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite precursor solution, prepared as
24 previously reported,³⁶ crystallizes with a Br content lower than the nominal value with an in-depth
25 uniform composition. Moreover, it was found that the PVSK-A ($E_g = 1.74 \text{ eV}$) and PVSK-B ($E_g =$
26 1.73 eV) have the real composition of $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{2.0}\text{Br}_{1.0}$ and $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{2.1}\text{Br}_{0.9}$, respectively,
27 being the slight difference of the band gap of these films in accordance with variations of Br content
28 in the chemical composition of the perovskite that occur during its self-organization upon
29 crystallization.

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CONCLUSIONS

In summary, we have demonstrated that microwave annealing process is an efficient and ultra-fast method for low-temperature fabrication of compact, pinhole-free and highly crystalline formamidinium-cesium mixed-cation lead mixed-halide perovskite films with micrometer-scale grains and preferred crystal orientation. It was also found that the improvement in crystallinity and enhancement in perovskite grain sizes can be achieved by optimization of microwave output power and irradiation time. Perovskite films prepared from $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ precursor solution and annealed at 100 W microwave power present the same band gap, similar morphology and crystallinity of conventionally annealed films. Moreover, the used IBA techniques allowed establishing the dependence of band gap variation of the perovskite films with the changes in the perovskite chemical composition upon the crystallization process. This work is the first to show that mixed-cation mixed-halide $\text{FA}_{0.83}\text{Cs}_{0.17}\text{Pb}(\text{I}_{(1-x)}\text{Br}_x)_3$ perovskite with an optical band gap of ~ 1.74 eV has the real composition of $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_2\text{Br}$.

In view of photovoltaic applications, the perovskite films analysed here were formed on glass substrates coated with the typical *n*-contact layers (FTO/compact TiO_2) of state-of-the-art perovskite solar cells composed of the conventional superstrate device architecture. As demonstrated here, microwave annealing opens new avenues to fabricate band gap tuneable perovskite films at low temperatures, which is of utmost importance for their integration in mechanically-flexible perovskite cells and/or monolithic perovskite based tandem cells.

EXPERIMENTAL SECTION

Materials. Cesium iodide (CsI, 99.9%), Lead(II) bromide (PbBr_2 , 98%), Lead(II) iodide (PbI_2 , 99%) and Hydrobromic acid (HBr, 48wt%) were purchased from Sigma-Aldrich, and Hydriodic acid (HI, 57wt%) was purchased from Alfa Aesar. All chemicals were used as received without further purification.

Perovskite precursor solution. The perovskite precursor solution (0.95 M) with nominal composition of $\text{FA}_{0.83}\text{Cs}_{0.17}\text{Pb}(\text{I}_{0.6}\text{Br}_{0.4})_3$ was prepared by dissolving FAI (272 mg), CsI (83.4 mg), PbI_2

1 (350 mg) and PbBr_2 (418 mg) in *N,N*-dimethylformamide (2 ml). 109.4 μl of HI and 54.6 μl HBr was
2 added and the solution was stirred for 48 hours at room temperature.

3 **Perovskite film preparation.** The compact TiO_2 layer (c- TiO_2) was coated onto an F-doped SnO_2
4 (FTO, Pilkington, TEC8) substrate by spin coating a 0.15M titanium diisopropoxide
5 bis(acetylacetonate) in 1-butanol, at 2000 rpm for 20 s³⁶. The c- TiO_2 films were annealed at 500 °C,
6 for 30 min. The perovskite precursor solutions were filtered with 0.20 μm PTFE filters and spin-
7 coated at 2000 rpm for 45 s on a c- TiO_2 /FTO substrate pre-heated at 70 °C. The films were dried on
8 a hotplate at 70 °C for 5 min, and then annealed in microwave oven at different power levels, or in a
9 conventional oven in air atmosphere following a multi-step temperature ramp up to 185 °C (room
10 temperature, 10 °C/min; 100 °C, 10 min, 10 °C/min; 185 °C, 30 min).

11 **Microwave annealing of perovskite films.** The microwave annealing tests were performed in a
12 Microwave Research Applications Inc. USA oven, with multimodal cavity, 1 kW nominal power and
13 2.45 GHz frequency magnetron. During irradiation, temperatures were measured by a platinum
14 shielded type-S thermocouple placed 2 mm above the specimens. At the end of the MW cycle
15 temperatures were measured by an external thermocouple in contact with the samples. All the
16 annealing tests were performed in air at microwave power of 25, 50, 100 and 150 W. The MW
17 irradiation time was initially set by visual control, which allowed to estimate the irradiation time for
18 each MW power. The estimated values were subsequently used and adjusted in the several MW-
19 annealing tests, allowing the determination of the optimum irradiation time for each MW power.

20 **Perovskite film characterization.** Scanning electron microscopy (SEM) was performed on a Philips
21 XL30 FEG (field emission electron source). SEM secondary electron top-view images were obtained
22 at an acceleration voltage of 10 kV. For this study, the samples were not coated with any conductive
23 surface layer. Semi-quantitative elemental composition was obtained with an EDS (EDAX) system
24 equipped with a Si(Li) detector and a 3 μm super ultra-thin window (SUTW). Spectra were collected
25 at an acceleration voltage of 30 kV for 300 s acquisition time. The same samples analysed by SEM
26 were gold-coated to obtain cross section images with the Zeiss Auriga CrossBeam system, and the
27 cross section was done by focused ion beam (FIB) milling with the Ga liquid metal ion source (LMIS)
28 at 30 kV acceleration voltage. SEM imaging was done at 5 kV acceleration voltage of the electron
29 beam. Atomic force microscopy (AFM) analysis was performed using an Asylum Research MFP-3D

1 Stand Alone AFM system. Measurements were performed in tapping (alternate contact) mode in air,
2 using commercially available silicon AFM probes (Olympus AC160TS; $k = 26$ N/m; $f_0 = 300$ kHz).
3 AFM topography images ($5 \times 5 \mu\text{m}^2$) were obtained in three different zones, with a minimum
4 resolution of 256×1024 points, and in an area of approximately 1 mm^2 . The X-ray diffraction (XRD)
5 patterns were recorded using a Panalytical MPD XPert Pro diffractometer in Bragg-Brentano
6 configuration and using a $\text{CuK}\alpha$ radiation source. The data were collected using a X'Celerator 1D
7 detector with a step size of 0.02° and was analysed with HighScore plus Software. The total
8 transmittance (T) and reflectance (R) spectra of perovskite films were acquired using an ultraviolet-
9 visible-near double beam infrared spectrophotometer (Perkin-Elmer Lambda 950) equipped with an
10 integrating sphere. Steady state photoluminescence was measured using a Perkin Elmer LS 55
11 fluorescence spectrometer, with a xenon flash lamp as the luminous source. An excitation
12 wavelength of 400 nm was used for all samples. The emission spectra were measured from 600 nm
13 to 900 nm in steps of 1 nm and with the scanning speed of 100 nm/min .

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15 **ASSOCIATED CONTENT**

16 **Supporting Information**

17 Supporting Information accompanies this paper and includes Tauc plots, scanning electron
18 microscope images, X-ray diffraction patterns, 2D-PIXE elemental distribution maps and RBS data
19 of perovskite films. Details on the Digital Image Analysis method and IBA techniques.

20

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SUPPORTING INFORMATION

Ultra-Fast Low-Temperature Crystallization of Solar Cell Graded Formamidinium-Cesium Mixed-Cation Lead Mixed-Halide Perovskites Using a Reproducible Microwave-Based Process

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Figures and Tables

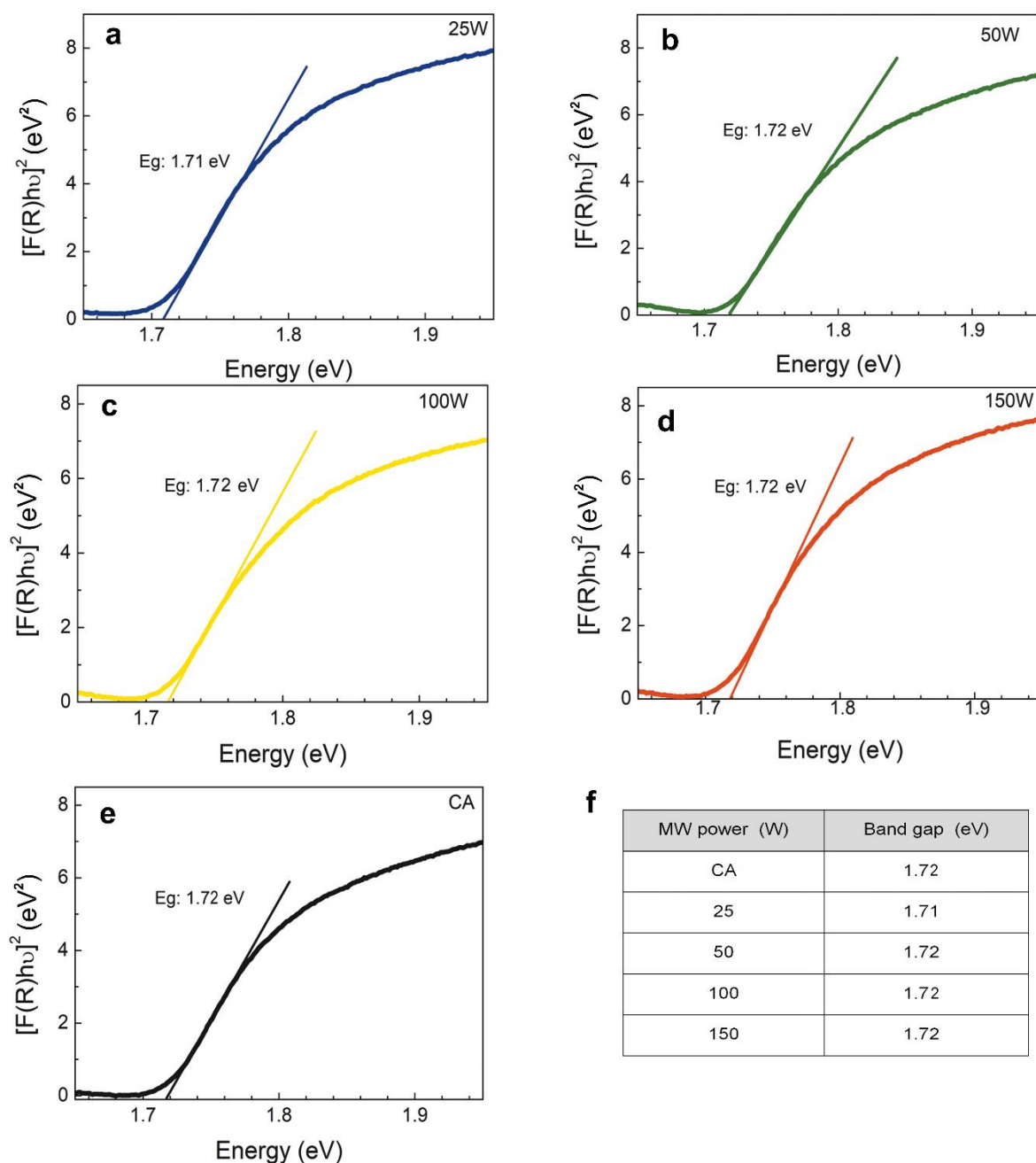


Figure S1 – Tauc plots of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite films formed on FTO/compact TiO_2 coated glass substrates showing determination of optical band gap from interception with horizontal axis. Perovskite films annealed at, **a** 25 W, **b** 50 W, **c** 100 W, **d** 150 W microwave power and **e** 185 °C referred as CA, **f** band gap values obtained for MW- and CA-perovskite films.

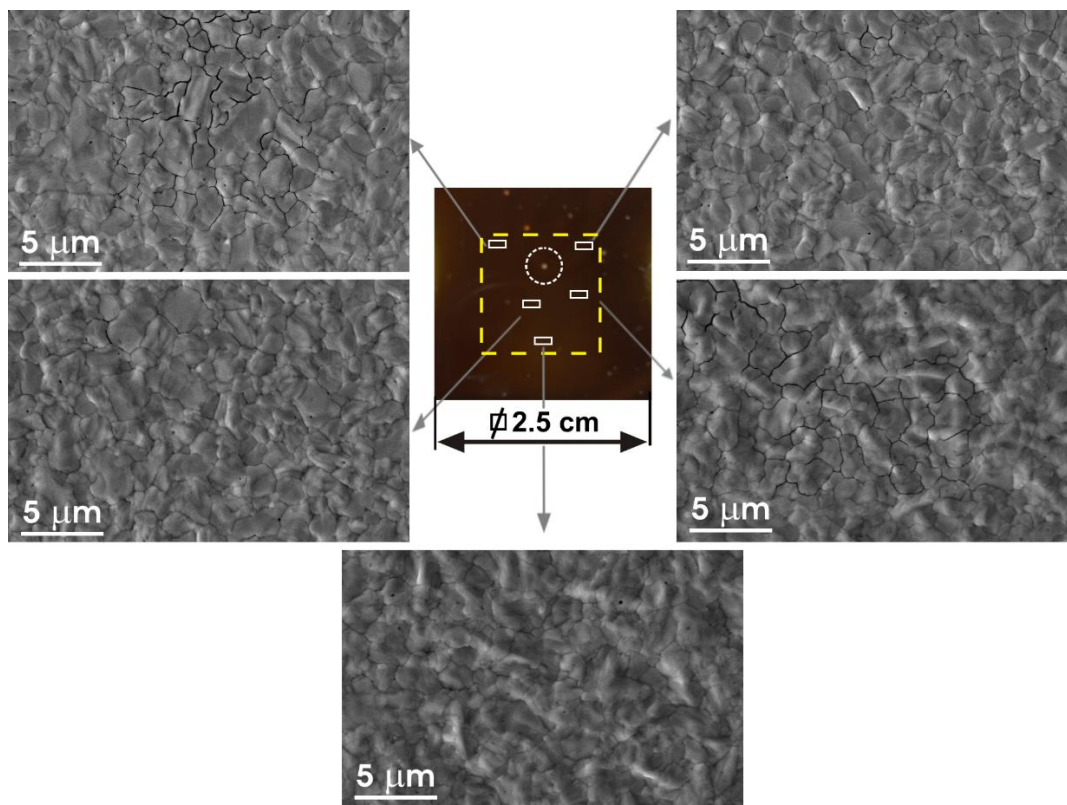


Figure S2 – Photograph of a perovskite film annealed at 100 W MW power (in the center) and SEM morphology images (magnification 5000 x) obtained on 5 surface regions (area of 1.5 x1.5 cm² highlighted in yellow) close to the white rectangles. The brighter points on the film (one of them indicated with a dashed circle) do not correspond to defects due to MW perovskite crystallization, but refer to defects already visible in the as deposit perovskite film, i.e before perovskite MW annealing process.

Table S1 – Band gap values of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite films, prepared from two independent precursor solutions (solution A and B). The perovskite films were conventionally annealed at 185 °C.

Precursor Solution A		Precursor Solution B	
Sample	Band gap (eV)	Sample	Band gap (eV)
#1	1.72	#1	1.72
#2	1.73	#2	1.73
#3 (PVSK-A)	1.74	#3 (PVSK-B)	1.73
#4	1.73	#4	1.72
#5	1.74	#5	1.72

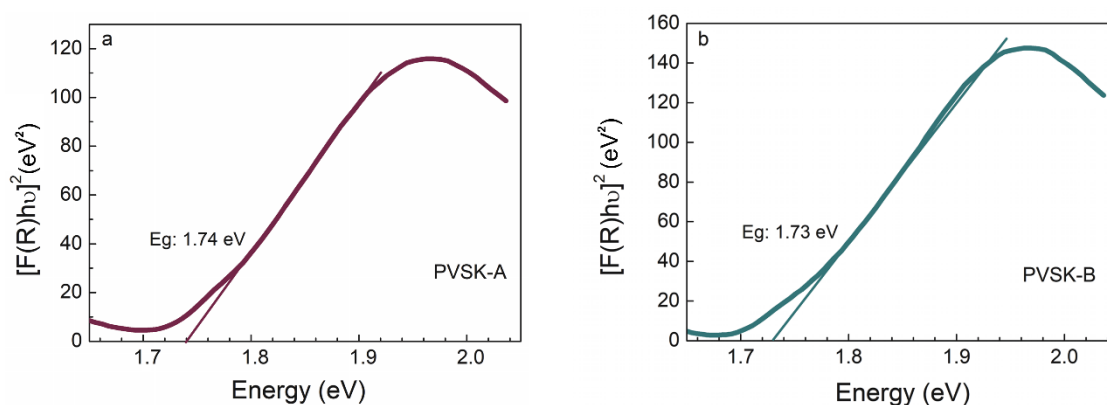


Figure S3 – Tauc plots of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite films (a. PVSK-A; b. PVSK-B) formed on FTO/compact TiO_2 coated glass substrates, showing the determination of the optical band gap from interception of the bottom axis. The perovskite films were conventionally annealed at 185 °C.

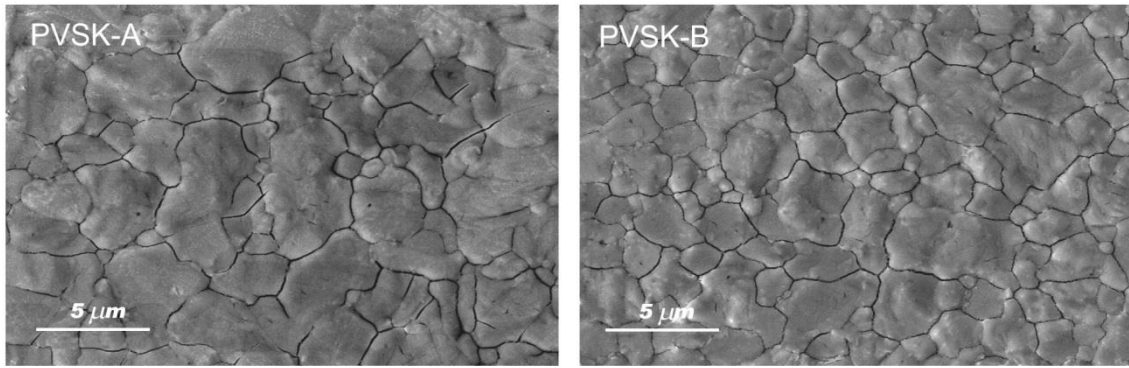


Figure S4. Scanning electron microscope images (SEM) of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{Pb}_{1.8}\text{Br}_{1.2}$ perovskite films. (A) PVSK-A film. (B) PVSK-B film.

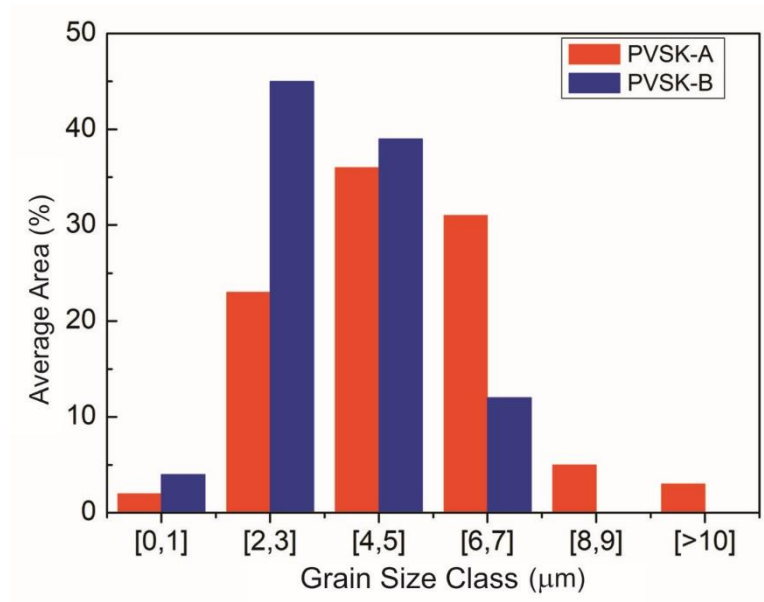


Figure S5 - Average area of each grain size class for PVSK-A and PVSK-B perovskite films.

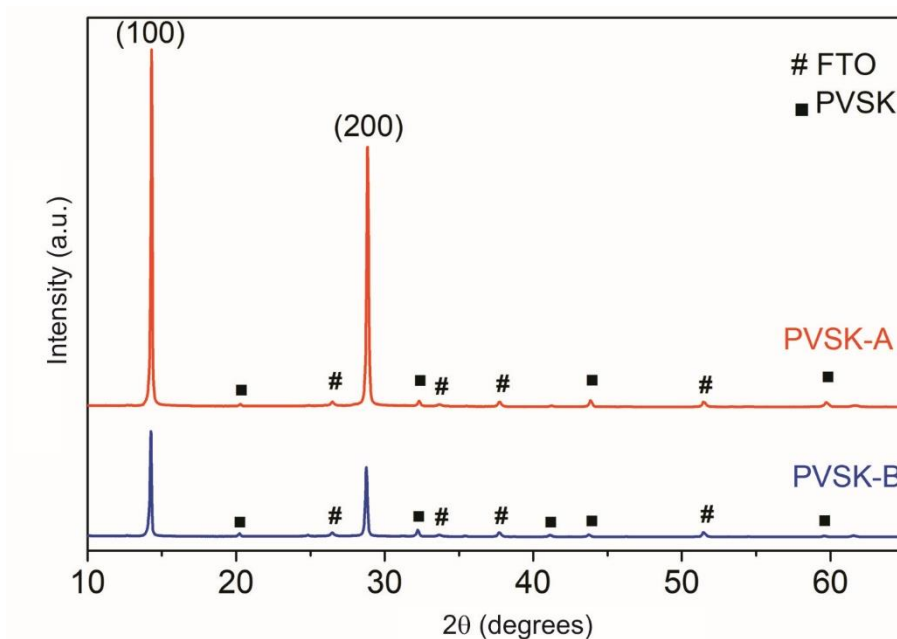


Figure S6. X-ray diffraction patterns (XRD) of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite films formed on FTO/Compact TiO_2 coated glass substrates when annealed at 185 °C. PVSK-A (red line) and PVSK-B (blue line). Peaks labelled with black squares are assigned to less intense perovskite peaks. Peaks labelled with # are assigned to the FTO substrate.

Table S2 – XRD results of nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$ perovskite films (PVSK-A and PVSK-B) formed on FTO/Compact TiO_2 coated glass substrates, and annealed at 185°C.

PVSK	XRD peak position [$^{\circ}2\theta$] planes (100) / (200)	XRD distance between (100) and (200) peaks [$^{\circ}2\theta$]	XRD (100) peak intensity / integral breadth [$^{\circ}2\theta$]
A	14.31 / 28.84	14.53	2.7×10^5 / 0.134
B	14.27 / 28.76	14.49	8.1×10^4 / 0.145

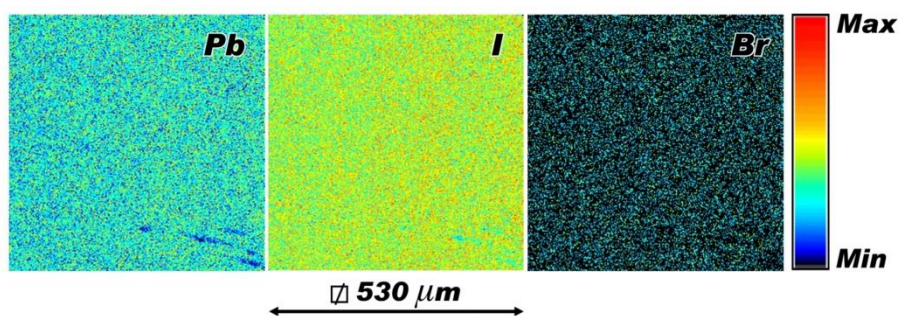


Figure S7 2 MeV H⁺ PIXE elemental mapping of PVSK-B. 2D elemental distribution maps for Pb (left), I (middle) and Br (right).

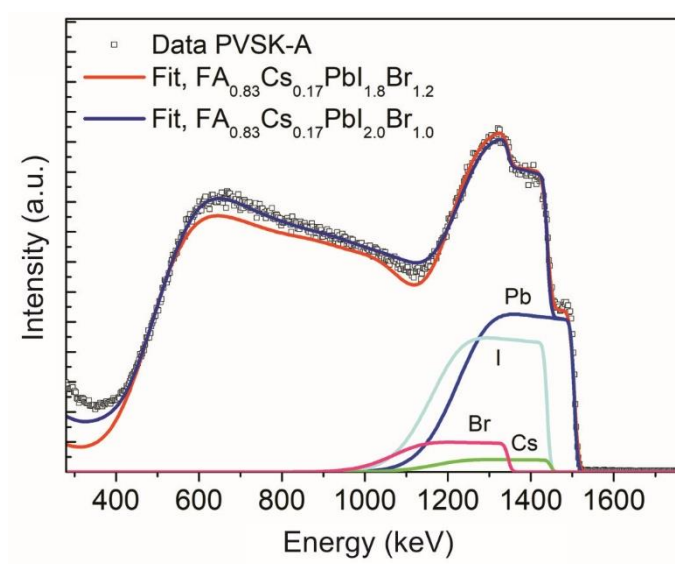


Figure S8 1.6 MeV He⁺ RBS data (open squares) and fits for PVSK-A assuming nominal concentration (red line) or composition obtained from PIXE (blue line). Elemental contributions to the fits are also shown.

Supplementary methods

Digital Image Analysis: Grain size, Average of equivalent in plane grain diameter and Perimeter coefficient were determined by Digital Image Analysis in-house procedures. The process is based on the acquisition of several SEM images (Figure S8a) taken with the same magnification from each specimen in different regions. These images are handled in order to enhance grain boundaries (Figure S8b). Then the maximum grain length is measured for each grain, and classified accordingly to previously defined size classes, e.g. [1,2], [3,4]... μm (Figure S8c).

The total area and number of grains for each size class is determined by the image analysis program. Hence, the grain average area is calculated for each class and the diameter of the equivalent circle computed (referred to as equivalent in-plane diameter). With this, the total specimen perimeter is determined, being the sum of each class value. Finally, a Perimeter Coefficient is computed, being the ratio between the Total Perimeter [μm] and the Total Area [μm^2] for each specimen. The lower the coefficient value the bigger the average grain size.

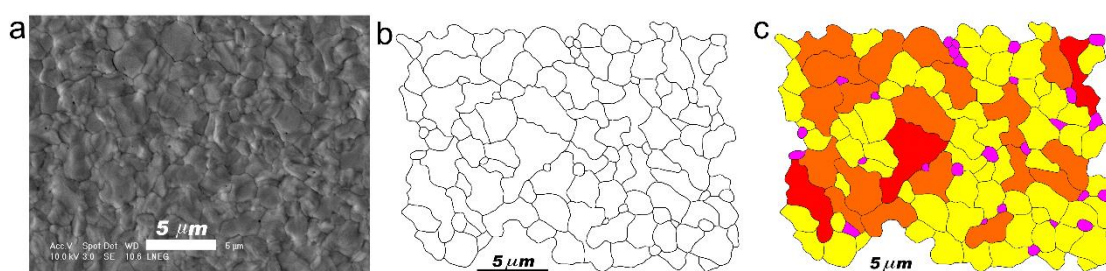


Figure S9 – Illustration of Digital Image Analysis procedures. **a** SEM image of a perovskite film. **b** digital image processing in order to enhance grain boundaries. **c** grain size classes (μm): [0,1] (pink), [2,3] (yellow), [4,5] (orange), [6,7] (red).

IBA techniques: Ion beam analysis (IBA) was carried out with an Oxford Microbeams Nuclear Microprobe installed at one of the beam lines of the CTN 2.5 MV Van de Graaff accelerator ¹. The microprobe comprises an OM150 quadrupole triplet to focus the beam, and the experimental chamber includes an X-ray and a backscattered particle detection system for PIXE and RBS measurements, respectively.

Typical ion beam spatial resolution is of $3 \times 4 \mu\text{m}^2$ for a 2 MeV proton beam with ~ 100 pA beam current and $5 \times 6 \mu\text{m}^2$ for a 1.6 MeV alpha particle beam with ~ 100 pA beam current. X-rays are detected with a 70 mm^2 Si(Li) detector with 155 eV resolution and positioned at 135° with the beam direction. Backscattered particles were detected by means of a 300 mm^2 PIPS detector, positioned at 140° with the beam direction in Cornell geometry.

Voltage amplitude signals resulting from the interaction of radiation (or beam particles) with the used detectors are proportional to the energy of the incoming radiation (or particles) and are sampled in a MCA (Multichannel Analyzer) originating spectra showing the energy of the incoming X-rays (PIXE spectra) or the energy of the backscattered particles (RBS spectra). An energy calibration allows establishing correspondence between channel and X-ray energy (for PIXE) or particle backscattered energy (for RBS). X-rays energy are a fingerprint of the detected element and are independent on the sample depth where they were induced. Rutherford backscattering is dealt as an elastic collision between the projectile ion and an atomic nucleus and the backscattered particle energy ruled by the kinematic factor (defined as the ratio of the interacting particle energy before and after being scattered ², that is shown to be only dependent on the mass of the impinging particle, the mass of the interacting nuclei and the scattering angle). This allows establishing a relation between measured backscattered energy of the scattered particle and sample nuclei mass with a clear identification of the sample surface scattering nuclei (elemental surface barrier (depicted in Figures 5 b and c, S7 and S9). The differential scattering cross-section² permits establishing correspondence between intensity of the detected signal and concentration of the scattering nuclei. Together with

the knowledge of the matrix stopping power (dE/dx) the analysis can be extended to the sample depth, allowing the study of in-depth heterogeneous samples whether due to elemental diffusion or to layered structured samples. Samples with similar layer composition but different layer thicknesses can easily be identified through the differences in width of the recorded scattering energy values (thicker layer will scatter particles with a larger range of energies).

Thickness values in units of at/cm^2 (or in the straightforward conversion to area mass density values) are the natural units in RBS analysis and usually the ones presented, as in the case of this work. They render the obtained results, independently of the physical state of the analyzed samples. An accurate conversion to length units (nm, μm ...) depends only on the accurate knowledge of sample density. Also notice that the value of $10^{15} \text{ at}/\text{cm}^2$ is of the order of magnitude of the lattice constant of most solid materials. IBA techniques allow to obtain the surface elemental distribution, by means of the 2D maps as well as to determine the layers thickness, uniformity and composition depth profile combining PIXE ³ and RBS ⁴ data in a Total IBA approach ⁵.

Different beams (2 MeV protons and 1.6 MeV alpha particles), chosen according to previously adjusted conditions ⁶, were used to gather sample information over different depths (see Figures 5a, 5b and S7, S9 of supporting information).

2D-PIXE elemental distribution maps (Figures 5a and S6) were obtained in a $530 \times 530 \mu\text{m}^2$ area for PVSK-A and PVSK-B, using a 2 MeV proton beam and the $\text{Pb-M}\alpha$, $\text{I-L}\alpha$ and $\text{Br-K}\alpha$ X-ray emission lines (see Figure S10).

RBS experimental data and fits for PVSK-A and PVSK-B obtained with 2 MeV proton beam and 1.6 MeV alpha beam are shown in Figures S9 and 5b, respectively. The fitting model in these samples considers a single layer of perovskite with the nominal composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$, followed by a multi-layered target configuration of a TiO_2 compact layer / F-doped SnO_2 (FTO) / glass with the fitting algorithm only allowing layers thickness and surface and interface sample roughness to change ⁷. When using a 2 MeV proton beam, it is possible to register the signal coming from the entire structure

(perovskite film, TiO₂ layer, FTO coating and glass substrate) but we cannot separate signals from Pb and I atoms in the RBS spectrum (Figure S9). The use of alpha particles increases the elemental mass resolution and in-depth sensitivity, enabling to separate signals from Pb and I atoms in the RBS spectrum (Figure 5b). On the other hand, the 2 MeV proton beam provides good PIXE yield (Figure S10), allowing an efficient check of the lateral composition homogeneity through 2D elemental distribution maps.

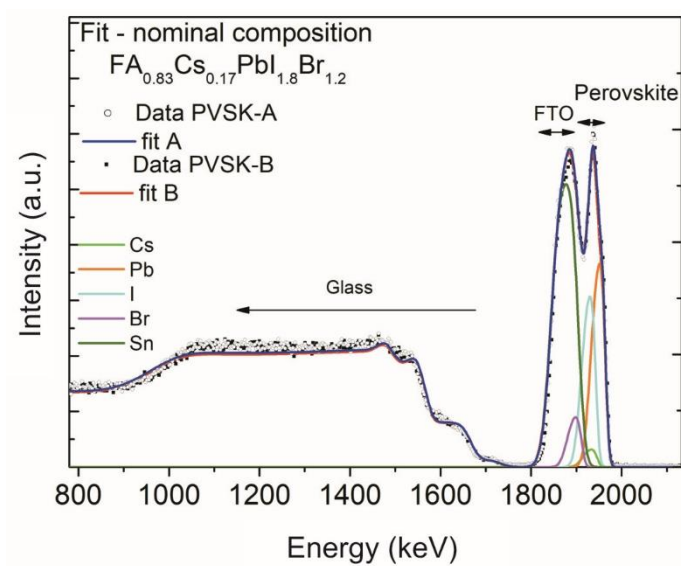


Figure S10. RBS experimental data and fits for PVSK-A and PVSK-B obtained with 2 MeV H⁺ ion beam. The fitting model in these multi-layered targets includes sample surface roughness and nominal perovskite composition $\text{FA}_{0.83}\text{Cs}_{0.17}\text{PbI}_{1.8}\text{Br}_{1.2}$.

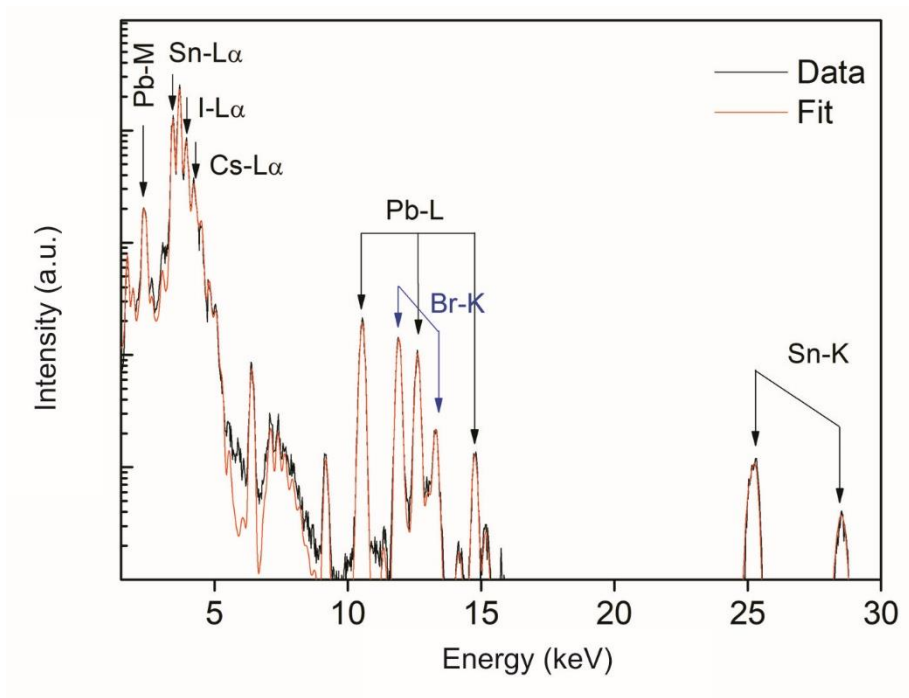


Figure S11. PIXE spectrum of PVSK-A using 2 MeV proton beam, showing good sensitivity and detection yield for the elements present in this multi-layered target.

Methodology for spectra analysis: PIXE spectra were analysed by the GUPIX⁸ code using multi-layered structure option. The software code provides mass concentration results for each element, and the corresponding elemental peak areas, which were used as input data to the NDF v9.6a code⁹.

NDF code allows a self-consistent fit of all the RBS and PIXE data obtained for each of the analysed samples (in total four spectra per area analysed) providing a unique solution, based on the concept of Total IBA approach¹⁰. More details about the fit procedure can be found in previous work⁶.

The RBS fits also consider the double scattering contribution, the pulse pile-up effect (considering the Molodtsov and Gurbich algorithm¹¹ collected with the 2 MeV proton), and the non-Rutherford cross sections for C, N, O and Si for RBS spectra beam¹². The RBS analysis of “ideal layered samples” with well-defined and flat surfaces and interfaces (implies well-defined geometry for the incident and scattered beam) are commonly managed by most of RBS fitting algorithms. Surface and interface roughness

result in the broadening of the obtained spectra, as can be observed in Figure 4 of Barreiros and Figure 11 of Barradas works ^{6,13}, where experimental data and simulation of the “ideal layered sample” are presented. Modelling the roughness contribution as a beam energy spread with the same layer composition of the “ideal layered sample” results in a proper fit to the experimental data as also shown ¹³. The extra contribution of sample roughness was also considered to the fitted spectra in this work, being more noticeable when dealing with He beam. The Gamma roughness algorithm, which contributes for the energy spread, was considered ¹³ with a value of 0.21.

Supplementary references

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