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1 Article

2 Value of local offshore renewable resource diversity for network 3 hosting capacity

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11 **Abstract:** It is imperative to increase the connectable capacity (i.e. hosting capacity) of distributed
12 generation in order to decarbonise electricity distribution networks. Hybrid generation that exploits
13 complementarity in resource characteristics among different renewable types potentially provides
14 value for minimising technical constraints and increasing the effective use of the network. Tidal,
15 wave and wind energy are prominent offshore renewable energy sources. It is of importance to
16 explore their potential complementarity for increasing network integration. In this work, the novel
17 introduction of these distinct offshore renewable resources into hosting capacity evaluation enables
18 the quantification of the benefits of various resource combinations. A scenario reduction technique
19 is adapted to effectively consider variation of these renewables in an AC optimal power flow-based
20 NLP optimisation model. Moreover, the beneficial impact of Active Network Management (ANM)
21 on enhancing the renewable complementarity is also investigated. The combination of
22 complementary hybrid generation and ANM, specifically where the maxima of the generation
23 profiles rarely co-occur with each other and with the demand minimum, is found to make the best
24 use of the network components.

25 **Keywords:** hosting capacity; electricity distribution network; tidal; wave; offshore wind;
26 optimisation
27

28 1. Introduction

29 The rapid deployment of renewable generation in the last two decades has seen the introduction
30 of new power sources on the distribution network. Previously, power flowed strictly from supply to
31 demand but distributed generators (DG) have transformed the structure of distribution networks.
32 The installed capacity of DG on UK networks reached 26 GW in 2019, 24% of installed renewable
33 capacity, and is projected to increase to 36% by 2050 [1]. Although the integration of DG has
34 significant benefits in decarbonising the electricity industry [2], it also brings a series of challenges to
35 network operation due to the variability and uncertainty of renewable output. Bi-directional power
36 flow, voltage rise and increased fault level have been identified as key issues that DG poses to
37 network operation [3]. As the share of DG increases, the pressure on network capacity due to voltage
38 rise and reverse power flow will rise. Therefore, there is a critical need to fully utilise the network
39 capacity to connect DG by exploring the potential of different DG configurations and considering
40 new network management techniques. The research on how to locate and size renewable DGs to
41 maximise their overall connectable capacity is often referred to as ‘hosting capacity’ in the literature
42 [4,5].

43 Hybrid generation comprising different types of renewable generation offers a potentially
44 valuable route to better balance their output and increase their grid integration [6–8]. The time-

45 varying nature of renewable resources creates less predictable and uncontrollable generation peaks
46 and troughs. Generation peaks which coincide with periods of low demand define the worst-case
47 scenarios that drive voltage rise and increased reverse power flow on distribution networks.
48 Ultimately, these conditions determine the capacity that Distribution Network Operators (DNOs) are
49 willing to connect. If generation is based on resources with different profiles, either resulting from
50 temporal or spatial differences, then individual extreme peaks may be suppressed, and network
51 constraints might be avoided or reduced. A DNO could then connect more capacity.

52 The complementarity between different renewable resources seems to be highly dependent on
53 the location in which the study is made; however, in general, research has proven that a diversified
54 portfolio of renewables improves their output reliability. Many studies have focused on the analysis
55 of complementarity among wind, PV and hydroelectricity generation to facilitate grid integration.
56 These studies have reported valuable complementarity in different locations and time scales [9–11].
57 Hoicka et al. investigated wind and solar in Ontario, Canada and found complimentary resources
58 result in less variability of power output [12]. The solar and wind resources around China were
59 modelled using the MERRA-2 reanalysis dataset and the complementarity of wind and PV connected
60 more capacity than individual resources [13]. In [14], the strong temporal synergy of solar and wind
61 resource is found in Australia and their combination increases the use of existing transmission assets.
62 In [15], annual and interannual complementarities among wind, PV and hydropower are explored in
63 Colombia for stable power supply during the annual dry season and the El Nino Southern Oscillation.
64 The impact of complementarity on small scale hybrid wind-PV systems is studied in [16] and the
65 authors proposed a set of complementarity indices for power supply reliability. The work in [17]
66 found that the joint operation of PV and hydro stations helps to increase PV integration and also
67 raises their profit on the day-ahead market. Halamay et al. also identified the diversification of
68 resources at large scale as a way to reduce utility reserve requirements [18]. The value of local hybrid
69 solar-wind systems is examined in [19] and shows the benefit of the combination of the hybrid
70 generation and the value of selective curtailment of generation.

71 While the renewable complementarity for increasing grid-integration is an active research field,
72 studies on the complementarity involving both wave and tidal resources are sparse. There are a few
73 studies on combining wind only with wave. The complementarity of wind and wave resources at
74 locations around Europe have been compared, and sites that had two generation profiles with stable
75 behaviour and low correlation were found to reduce the variability of power output to the grid [20].
76 Similar studies include the evaluation of co-located wind and wave for the US west coast and the UK
77 North Sea [21], Latin America and Europe [22]. These works mainly look at the supply profile of the
78 combined resources but do not consider their feasibility regarding network capacity constraints.

79 Another popular route for increasing hosting capacity for renewables is through the use of
80 advanced network control schemes [23,24]. Historically, DNOs have connected DG with a ‘fit-and-
81 forget’ or ‘passive control’ approach where generator unit capacities are constrained at the planning
82 stage so that when connected they can operate without intervention. This hosting capacity is defined
83 according to often infrequent worst-case scenarios, where low demand coincides with high
84 generation output, making relatively inefficient use of the network. The downside of this approach
85 has been widely recognised and the potential to make better use of the network by using active
86 network management (ANM) techniques has been well articulated. Several different ANM control
87 schemes have been proposed. In a method referred to as co-ordinated voltage control (CVC), on-load
88 tap changers (OLTC) are used to change (lower) the set-point voltage on the secondary side of
89 transformers, mitigating voltage rise [25]. Power factor control (PFC) varies the DG power factor from
90 inductive to capacitive depending on the direction of required voltage control [26,27]. Alternatively,
91 DNOs may reserve the right to reduce power output via active curtailment control (ACC) during
92 periods that stretch the network capabilities [28,29]. ANM has been trialled on a distribution network
93 on the Orkney Islands, Scotland with power flow management through ACC used successfully to
94 keep network components within their thermal limits [30]. Optimal power flow (OPF) techniques
95 have been developed to understand how DG affects distribution network operation, the constraints
96 to deployment, and how connectable capacity may be enhanced [31–33]. Multi-period AC OPFs have

97 indicated that ANM schemes (notably ACC, CVC and PFC) increase the capacity of wind generation
98 connected to distribution networks [34].

99 Summarizing the research gap identified in the existing literature: firstly, regarding
100 complementarity of multiple renewable resources few – if any – consider the complementary
101 potential of offshore wind, wave and tidal energy sources to improve connectable capacity. Secondly,
102 few existing works on resource complementarity explicitly consider the reliable operation of
103 networks in terms of voltage and thermal limits in distribution network. In contrast, this study takes
104 a rigorous approach and thoroughly investigates the complementary benefits of these three offshore
105 renewable resources in alleviating network constraints and increasing the hosting capacity.
106 Moreover, the additional benefits from active network management are also studied in detail. The
107 main contribution of this work can be described as:

- 108 1. The novel introduction of three offshore renewable resources – offshore wind, wave and tidal
109 stream – to a hosting capacity study. A multivariate scenario reduction technique is adapted to
110 effectively consider variation and complementarity of renewables over a long time period.
- 111 2. The generic AC OPF based hosting capacity model is established to find the simultaneous
112 hosting capacity for various resource combinations considering their complementarity and a
113 suite of ANM control schemes. The hosting capacity problem is formulated as a Nonlinear
114 Optimisation model (NLP) to accurately model voltage and thermal constraints.
- 115 3. Comparative analysis is detailed in the case study in Scotland for different configurations of
116 renewable resources and control schemes. This identified which resources combine to offer
117 enhanced hosting capacity and energy delivery and which features constrain the performance
118 of network control schemes.

119 This paper is structured as follows: Section 2 introduces the optimisation model for hosting
120 capacity analysis. Section 3 introduces the case study and section 4 provides the resource evaluation
121 and hosting capacity analysis and discussion. The conclusion is provided as the last section.

122 2. AC OPF Model for Hosting Capacity Analysis

123 An AC OPF based approach is adopted here to model a hosting capacity problem with the
124 objective to maximise the overall connectable capacity of candidate DG located at specified locations
125 across the network. The OPF formulation is widely used to find the optimal control settings for a
126 power network to fulfil its objective function whilst remaining within network limits. An AC solution
127 is preferred as it accounts for active and reactive network components, both of which are known to
128 affect voltage levels, a key constraint to generation on distribution networks. While traditionally used
129 for operational analysis, it has found use in ‘planning’ analysis such as for hosting capacity analysis
130 where the capacity of generators are optimised [32,34].

131 The normal AC OPF is extended here to consider multiple resources and multiple time periods.
132 The multi-periodicity grasps the time-varying nature of demand and renewable generation profiles;
133 specifically the need to capture a wide range of conditions requires a large number of time periods
134 (at least a year) at relatively high time resolution (such as hourly). Hybrid generation configurations
135 can easily be analysed using a multi-period approach which account for their differing temporal
136 characteristics. The OPF-based nonlinear optimisation model is implemented in the modeling
137 language AIMMS [35] and solved using the CONOPT 4.0 NLP solver.

138 Before the formal mathematical description, it is worth explaining how the optimisation operates
139 in simple terms. The model uses the DG production and demand in each time period and determines
140 the resulting set of power flows. As the DG size(s) are increased, the production across all periods
141 will increase, changing the power flows and resulting in higher voltages and larger reverse power
142 flows. Where DG is not actively controlled, the DG(s) capacity will be increased until a voltage or
143 thermal constraint is reached in one or more periods (normally that with maximum production and
144 minimum demand). This defines the hosting capacity.

145 Where there are ANM controls in place and DG capacity and production increase, voltages and
146 reverse power flows increase. However, where a constraint is reached in a period the optimisation
147 will look to change the control setting (power factor, transformer voltage or curtailment) such that

148 the DG capacity can increase further. Each time period is treated separately but more periods will
 149 tend to see changes in control settings as the DG capacity increases. This continues until one or more
 150 of the control settings have reached their limit (e.g. power factor limits, transformer voltage limits or
 151 maximum curtailment), defining the hosting capacity.

152 2.1. Objective Function

153 More formally, the objective function of the optimisation is to maximise the total connectable
 154 capacity of potential DGs of different resource types located at specified locations in the network over
 155 all considered renewable resources:

$$\max \sum_{g \in G} \sum_{r \in R} p_{r,g} \quad (1)$$

156 where $p_{r,g}$ is the active power capacity of generator g for resource r .

157 2.2. Network Constraints

158 The three major constraints that the optimisation is subject to are: (1) active and reactive power
 159 balance, (2) voltage limits and (3) power flow limits.

160 2.2.1. Active and Reactive Nodal Power Balances

161 The active power balance equations are derived from Kirchhoff's Current Law and define the
 162 power flow into and out of each bus:

$$\sum_{l \in L | \beta_l^{1,2} = b} p_{b,m}^l + d_b^p \eta_m = \sum_{g \in G_b} \sum_{r \in R} p_{r,g} \omega_{r,m} + \sum_{x \in X_b} p_{x,m} \quad (2)$$

163 where $p_{b,m}^l$ is the active power injection into connecting lines L from bus b in period m ; η_m is
 164 demand in each period expressed relative to peak value d_b^p . $\omega_{r,m}$ is the generator output level for
 165 the resource r during period m and is defined as the instantaneous output as a fraction of the
 166 maximum/nominal output (i.e. capacity factor), and is determined by the resource characteristics
 167 such as wind speed in corresponding periods m . If the bus is connected to external connection x ,
 168 typically the grid supply point (GSP), any excess or deficit of production is met from exports/imports
 169 $p_{x,m}$ from the external network.

170 The reactive power balance constraints can be derived similarly:

$$\sum_{l \in L | \beta_l^{1,2} = b} q_{b,m}^l + d_b^q \eta_m = \sum_{g \in G_b} \sum_{r \in R} p_{r,g} \omega_{r,m} \tan(\phi_{r,g,m}) + \sum_{x \in X_b} q_{x,m} \quad (3)$$

171 where the reactive power output of DG is calculated based on its power factor angle $\phi_{r,g,m}$.

172 2.2.2. Voltage Limits

173 Network bus voltages $V_{b,m}$ over all time periods must be within defined limits described by
 174 lower and upper boundaries, V_b^-, V_b^+ :

$$V_b^- \leq V_{b,m} \leq V_b^+ \quad (4)$$

175 2.2.3. Power Flow Limits

176 Flow of power through each line and transformer has specified flow limits imposed by the
 177 equipment capabilities and described as:

$$\left(f_{l,m}^{(1,2),P}\right)^2 + \left(f_{l,m}^{(1,2),Q}\right)^2 \leq \left(f_l^+\right)^2 \quad (5)$$

178 where $f_{l,m}^{(1,2),P}$ and $f_{l,m}^{(1,2),Q}$ are, respectively, the active and reactive flows through line/transformer l
 179 and f_l^+ is the apparent power flow limit.

180 2.3. Active Network Management

181 ANM schemes are expected to complement the efforts of hybrid generation configurations for
 182 maximising DG production. Active network management aims to adapt control settings for network

183 components and DG on an ongoing basis in response to network constraints. Depending on the
 184 scheme these define target DG production levels and power factors as well as transformer set-points
 185 in each period that serve to allow larger generators and more energy production. The three schemes
 186 discussed in the introduction are simulated to investigate their benefit to networks.

187 2.3.1. Active Curtailment Control

188 Curtailment control selectively reduces DG active power output in periods when voltage or
 189 power flow limits would otherwise be breached, by reducing reverse power flows. In the model,
 190 curtailment $p_{r,g,m}^{curt}$ is considered as a variable, applied by the DNO when the network is constrained,
 191 that reduces the active power delivered in period m . The resulting power production in period m
 192 ($p_{r,g} - p_{r,g,m}^{curt}$) takes the place of the simple generator capacity previously included in Eq. 2:

$$\sum_{l \in L | \beta_l^{1,2} = b} p_{b,m}^l + d_b^p \eta_m = \sum_{g \in G_b} \sum_{r \in R} (p_{r,g} - p_{r,g,m}^{curt}) \omega_{r,m} + \sum_{x \in X_b} p_{x,m} \quad (6)$$

193 with a similar replacement required for Eq. 3. The amount of curtailment applied to each renewable
 194 DG is limited by its full potential output in the corresponding period:

$$p_{r,g,m}^{curt} \leq p_{r,g} \omega_{r,m} \quad (7)$$

195 To ensure a realistic level of curtailment that a developer might agree to, the level of curtailment of
 196 each DG is restricted by the curtailment factor $\lambda_{r,g}^{curt}$, a proportion of the total potential energy
 197 generation over the full study period M (e.g. over a whole year) as a global limit:

$$\sum_{m \in M} p_{r,g,m}^{curt} \tau_m \leq \lambda_{r,g}^{curt} \left[\sum_{m \in M} p_{r,g} \omega_{r,m} \tau_m \right] \quad (8)$$

198 where τ_m is the duration of period m , e.g. an hour.

199 2.3.2. Power Factor Control

200 Power factor control enables local voltage control close to the DG to alleviate voltage constraints.
 201 DGs are simulated with the capability to dispatch their power factor $\phi_{g,m}$ from period to period,
 202 within the inductive and capacitive limits of the DG (ϕ_g^-, ϕ_g^+):

$$\phi_g^- \leq \phi_{g,m} \leq \phi_g^+ \quad (9)$$

203 Making power factor $\phi_{g,m}$ more inductive will tend to reduce reverse power flows and limit voltage
 204 rise, enabling larger generators to be connected.

205 2.3.3. Coordinated Voltage Control

206 Coordinated voltage control allows the GSP transformer secondary voltage $V_{b_{OLTC},m}$ to be set to
 207 raise or lower overall voltage levels in the network. The secondary voltage is a variable in the model
 208 constrained within the range indicated by the transformer tap changer limits ($V_{b_{OLTC}}^-, V_{b_{OLTC}}^+$):

$$V_{b_{OLTC}}^- \leq V_{b_{OLTC},m} \leq V_{b_{OLTC}}^+ \quad (10)$$

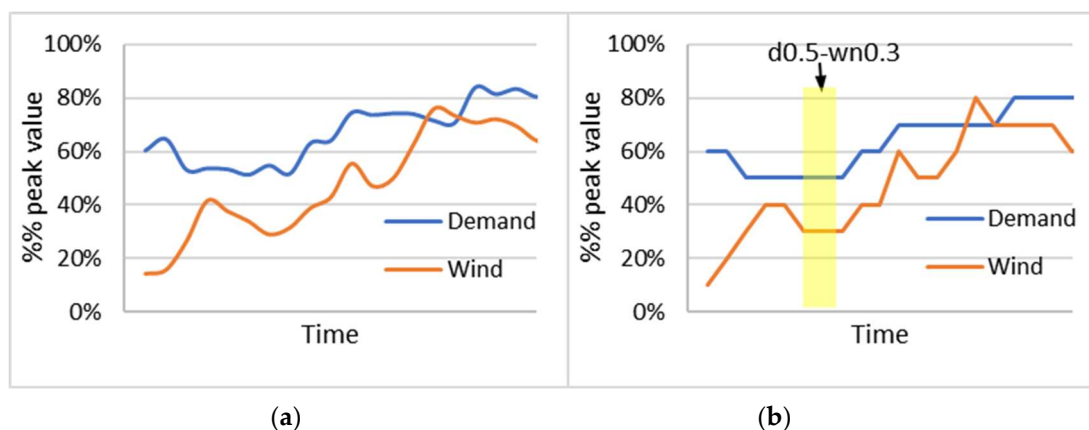
209 In general, setting a lower secondary voltage will tend to allow greater generation by enabling a
 210 greater degree of voltage rise relative to the substation.

211 2.4. Treatment of Long-term Time-series Data

212 It is important that the full variation of renewable resource and demand over an extended period
 213 (e.g. a year) is captured in the analysis, so that the obtained DG capacities satisfy all operational
 214 conditions. However, the non-convex nonlinear nature of the hosting capacity optimisation model
 215 makes this quite challenging. For example, the direct use of hourly data for one year in the
 216 optimisation will generate 8760 operational scenarios to be considered simultaneously, which means
 217 a significant number of time-varying variables and corresponding constraints, making the nonlinear
 218 optimisation problem laborious or intractable.

219 To address the computational challenge whilst effectively preserving the temporal
 220 interrelationships between resources and demand, scenario reduction is adopted here. The approach
 221 uses 'representative' combinations of demand and renewable resource level as inputs, rather than the

222 direct use of full time series. The first step is to discretize the original values, the illustration of which
 223 is shown in Figure 1 using the example of demand and wind data. After the discretization, the values
 224 are aggregated according to the occurrence of ‘similar’ periods and allocated into a series of bins
 225 covering specific intervals. Such treatment of long-term time-series data was previously detailed in
 226 [34], which also showed that discretisation only has a minor impact on accuracy. This paper further
 227 develops it to address the ‘coincidence’ of three different resources (i.e. tidal, wave and wind) and
 228 demand, essentially a four dimensional array.



229

230 **Figure 1.** (a) Normalised hourly demand and wind power time series; (b) discretised wind and demand
 231 time series. ‘d0.5-wn0.3’ is the period with demand at 50% of peak and wind at 30% of capacity.

232 3. Orkney Island Case Study

233 The case study considers application of the method to a representative location suitable for co-
 234 located offshore wind, wave and tidal resources. The resource data relates to part of Orkney off the
 235 north coast of Scotland which has a valuable combination of strong winds, an energetic wave climate
 236 and sites suitable for tidal stream by virtue of its position between the North Atlantic and the North
 237 Sea.

238 3.1. Resource Evaluation

239 Three resource profiles with hourly resolution are built from observational and modelled
 240 datasets from North Ronaldsay, Orkney using concurrent 2016 data. The location of the data sites is
 241 shown in Figure 2. Hourly offshore wind speed (m/s) and wave power density (per metre of wave
 242 crest) time series are based on the ECMWF ERA5 reanalysis dataset [36] which has been extensively
 243 validated. A tidal current velocity time series (m/s) is built from the FOAM Shelf Seas – Atlantic
 244 Margin Model (AMM7) coupled hydrodynamic-ecosystem model [37]. Due to the resolution of the
 245 model it slightly under-estimates current velocities so a scaling factor is applied to the tidal profile to
 246 raise the 25 highest current velocities to equal the observed local average peak spring velocity [38].

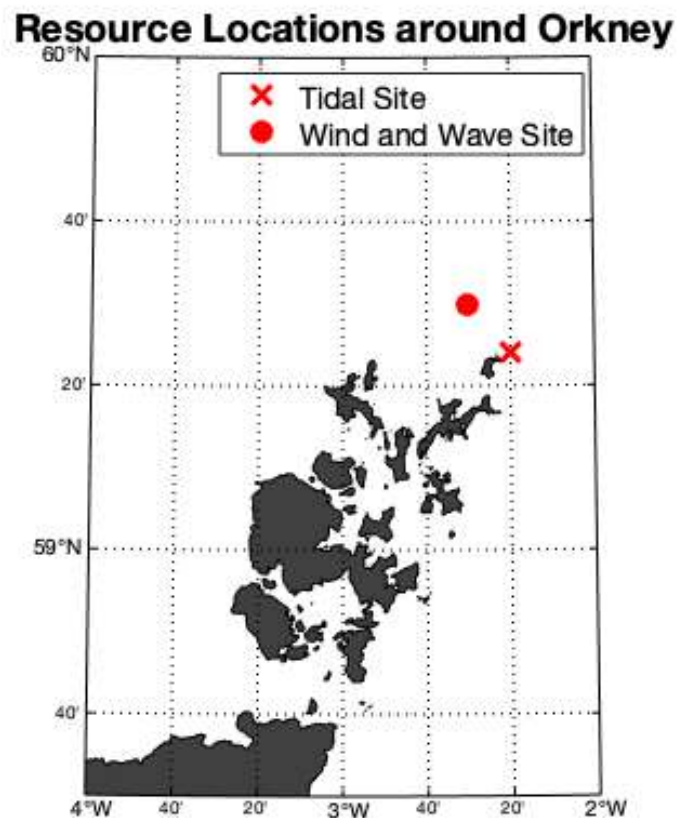
247 Three representative devices are used to convert the resource time series into production time
 248 series. A 1 MW, 18 m rotor diameter SeaGen tidal turbine [39] is chosen to convert tidal energy. The
 249 nature of the flow off the tip of North Ronaldsay is thought to be effectively captured by the bi-
 250 directional capability of the turbine. A Pelamis wave energy converter, scaled up from 750 kW to
 251 1500 kW as in [40], is chosen due to its wide coverage of energy period and wave height. Although
 252 this device is no longer being actively developed for commercialisation, it is well suited to the site
 253 characteristics around Orkney and is deemed appropriate to exhibit the benefits of hybrid generation.
 254 A generic wind power curve based on a 7.58 MW 127 m diameter direct-drive Enercon E-126 at 80m
 255 hub height is used to convert the wind resource. The resulting year-long hourly generation profiles
 256 are shown in Figure 3 along with the electricity load profile [40].

257 **Tidal:** The SeaGen capacity factor is 27.2%, a product of many hours spent at slack water
 258 between energetic flood and ebb flows typical of tidal turbines. The variation of tidal generation is
 259 dominated by semi-diurnal and fortnightly cycles determined by celestial orbits.

260 **Wave:** The scaled up Pelamis device achieves a capacity factor of 38%, which is comparable with
 261 some of the most efficient wave converter locations analysed in a recent study [41]. Figure 3 shows
 262 that the wave profile has a strong seasonal variation with calmer summers and more energetic
 263 winters.

264 **Wind:** Offshore wind generation has the highest capacity factor of the three generator types,
 265 reaching 51.2%. Wind exhibits a similar, but less pronounced seasonal distribution to the wave
 266 profile. Regular high production (relative to the generator capacity) will increase energy delivered
 267 but will also tend to stretch the limits of the network which may affect how wind is handled in the
 268 optimisation.

269



270

271 **Figure 2.** Resource sites co-located off North Ronaldsay, Orkney. Red markers indicate the location
 272 that data was collected from ECMWF ERA5 and FOAM AMM7 datasets for resource profiles.

273 To investigate the relationship among these generation types, and also between each generation
 274 type and load, their correlation coefficients are provided in Table 1. The peak cross-correlation
 275 coefficients and their associated lags are also calculated and given in Table 2.

276 A low correlation between the tidal profile and demand or other generation profiles is attributed
 277 to the misalignment of the production timescales with those for the others. Independence from other
 278 profiles could either support or suppress the inclusion of tidal generation in a hybrid configuration.
 279 Generation unrelated to the demand profile will cause frequent imbalance between generation and
 280 demand and tend to limit connectable capacity, as peaks of the two are not expected to co-occur.
 281 However, an opposite and beneficial impact can be expected with two unrelated generators, where
 282 the isolation of peaks reduces the overall generation peak and reduces the strain on the network.
 283 Wind and wave profiles are related by moderately high correlation (Table 1) with maximum cross-
 284 correlation occurring with a six-hour lag relative to the wind profile (Table 2). Large lags between
 285 wind and wave were attributed in [24] to sites where the mechanisms driving wind and wave

286 variation were isolated by the Atlantic fetch, seemingly appropriate for the site north of Orkney, and
 287 potentially describing the results. [42] also noted the benefit that lower correlation and higher peak
 288 lags offer hybrid generation configurations in the form of smoother power output with fewer zero
 289 hours. Table 1 and 2 suggest the wave and wind resource off North Ronaldsay may complement one
 290 another more than the same two resources analysed at other selected locations in Europe.

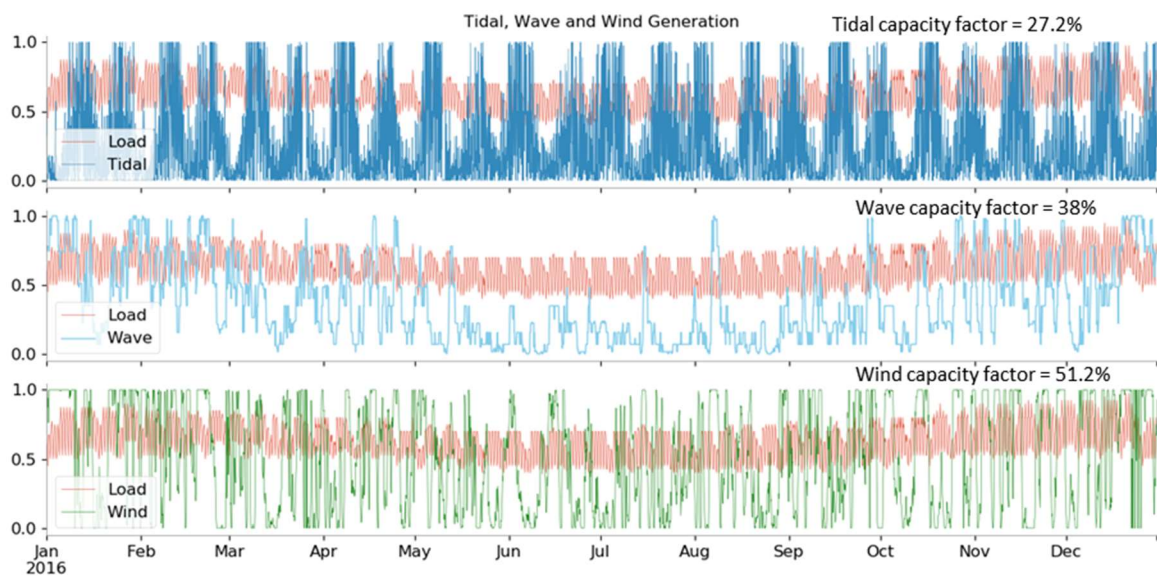
291 **Table 1.** Correlation coefficients (r) between load and generation profiles.

	Load	Tidal	Wave	Wind
Load	1.000	0.027	0.220	0.090
Tidal	-	1.000	-0.013	-0.017
Wave	-	-	1.000	0.595
Wind	-	-	-	1.000

292 **Table 2.** Peak cross-correlation coefficient (xR) and the associated lag (xL (hrs)) at which it occurs
 293 between generation profiles. Data is presented in the table in the form: xR/xL, where xL is positive
 294 when the signal on the left of the table lags the signal above. Cross correlations associated with a lag
 295 of more than 24 hours are thought to lack physical meaning.

	Tidal	Wave	Wind
Tidal	1.000/0	0.479/-277	0.494/-252
Wave	-	1.000/0	0.864/6
Wind	-	-	1.000/0

296



297

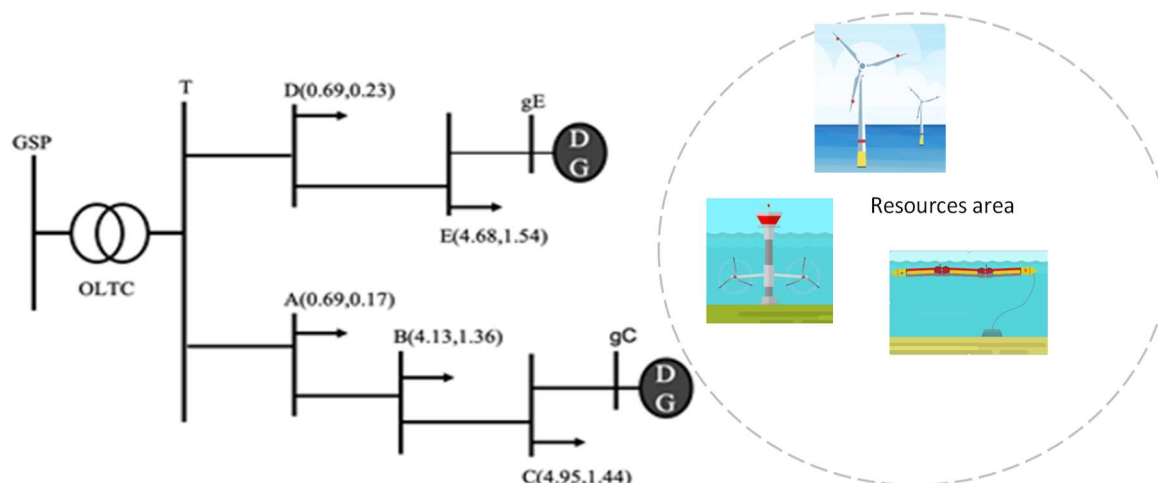
298 **Figure 3.** Generation profiles for resources located off North Ronaldsay for the year 2016. Generation
 299 is plotted as a proportion of maximum output. The load profile for the studied network is also plotted
 300 as a proportion of maximum demand (red dashed line).

301 **3.2. Network Description**

302 A typical but deliberately simple rural distribution network [43], outlined in Figure 4, is used to
 303 analyse the co-located offshore renewable resources. This is not the actual network constructed in
 304 Orkney but is used to enable comparison with earlier work using the same network [44]. The buses
 305 at the end of each feeder offer DG connection sites at bus C and bus E. The two sites have the potential

306 to harness any of the three resources considered in the optimisation due to the proximity of each
 307 resource's high energy regions.

308 Each bus is connected with local load, the sum of which has a maximum of 15.1 MW and
 309 minimum of 5.5 MW. The network is supplied by one 110/38 kV transformer at the grid supply point
 310 (GSP). Line and transformer information is given in Table 3. Voltage variation is limited to the range
 311 of $\pm 10\%$, and the transformer OLTC voltage target is fixed at 1.078 per unit when an ANM scheme is
 312 not considered. During the consideration of CVC, the tap changing potential at the GSP is $\pm 5\%$ – 15% .
 313 Power factor control is limited to power factors between ± 0.9 . The curtailment limit is set at 10% of
 314 the total potential energy output of each generation type throughout the study period.



315

316 **Figure 4.** Rural distribution network and local resource area during maximum loading. The maximum
 317 real and reactive powers are included with the bus label i.e. bus A: A (P, Q).

318 **Table 3.** Line and transformer parameters (resistance R, reactance X and maximum apparent power
 319 flow limit S_{max}) for the distribution network. All data are given as per unit values on a 100 MVA base.

Line	R	X	S_{max}
GSP - T	-	0.2500	0.3150
T - A	0.0296	0.0863	0.3817
A - B	0.5941	0.6244	0.1975
B - C	0.3875	0.4072	0.1975
T - D	1.126	1.193	0.3817
D - E	0.1550	0.1629	0.1975
C - gC	0.1292	0.1357	0.1975
E - gE	0.1292	0.1357	0.1975

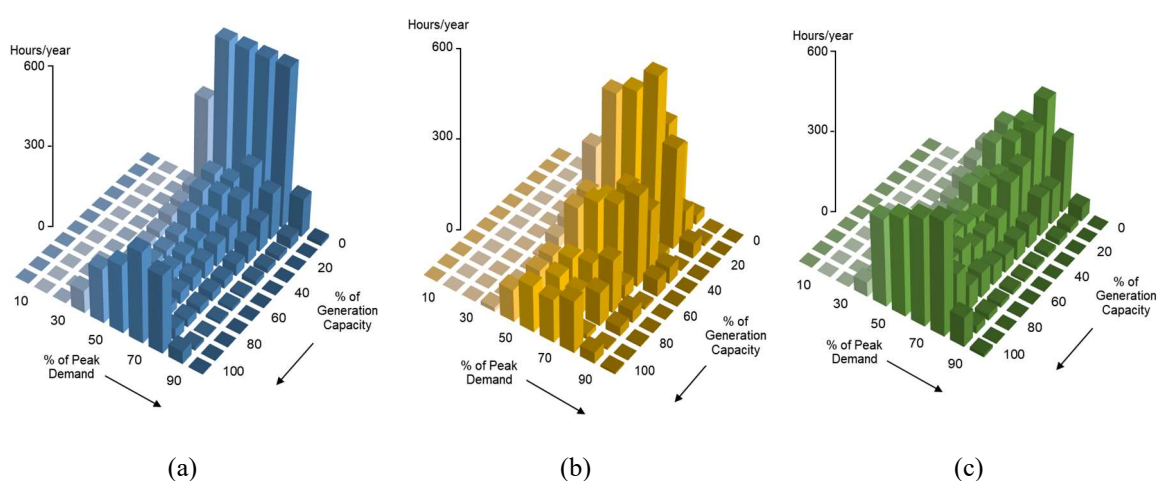
320 3.3. Resource-Demand Coincidence

321 In their original state, the demand and generation profiles take the form of four time-series each
 322 with 8760 hourly steps. The NLP optimisation program cannot directly account for such a large
 323 dataset, particularly with more than one bus location. Instead, the scenario reduction technique in
 324 Section 2.4 is applied to use the duration of coinciding demand-generation levels as input for the NLP
 325 to reduce the computational burden.

326 The hourly demand and generation data of each resource are fitted to various operating state
 327 bins, in percentage of its peak value, centered around 10% steps from 0 to 100%. Demand never falls
 328 into a bin lower than 40%, so only 7 of the 11 load states are considered. Periods can then be defined
 329 as every combination of demand and generation operating state that occurs in the dataset. The

330 duration of the period is simply the number of hourly occurrences. This unique combination is
 331 observed throughout the year.

332 A total of seven different resource configurations are considered in generating the profile of
 333 coincident hours: single resources, hybrids of any two, and all three resources together. Figure 5
 334 depicts the bivariate distributions of demand with each individual resource and their coincident
 335 hours. For brevity and also due to difficulty with visualization, the tri- and quadri-variate
 336 distributions are not shown for each case. However, the ‘worst-case’ scenarios are listed in Table 4
 337 which show the periods of high generation (100%) and low demand (40%) which are particularly
 338 restrictive to the connection of DG capacity. The coincident hours of these show that the occurrence
 339 of worst case periods varies considerably. Single resource tidal and wind cases exhibit the highest
 340 coincident hours, wave exhibits somewhat less and none of the 4 hybrid resource combinations
 341 exhibit more ‘worst-case’ hours than wave alone. This demonstrates that there is potential value in
 342 diverse combinations in terms of reducing the frequency of capacity limiting periods.
 343



344 **Figure 5.** Coincident hours of load and generation states for each offshore renewable. Bins are
 345 centered at 10% steps of the peak value of each profile: (a) tidal and demand; (b) wave and demand;
 346 (c) wind and demand.

347 **Table 4.** Annual duration of worst case scenarios expected to limit the connected capacity for each
 348 configuration of generation topology. The level of demand (d), and tidal (t), wave (wv), or wind (wn)
 349 generation is indicated as a percentage of its maximum, for example, d04t10 signifies a period with
 350 demand at 40% of peak and tidal at 10%.

Configuration	Period	Duration (hours)
Tidal	d04t10	87
Wave	d04wv10	15
Wind	d04wn10	56
Tidal+Wave	d04t09wv10	1
Tidal+Wind	d04t10wn10	6
Wave+Wind	d04wv10wn10	15
Tidal+Wave+Wind	d04t10wv08wn10	1
Tidal+Wave+Wind	d04t09wv10wn10	1

351

352

353 4. Results

354 Different combinations of resources and control schemes are studied to explore their ability to
355 maximise hosting capacity and the delivered energy. They are grouped into two subsections:

- 356 • Single resource cases
- 357 • Hybrid generation cases with combinations of two or three resources: tidal+wave, tidal+wind,
358 wave+wind, tidal+wave+wind.

359 Each resource case is examined subject to six different network control schemes: passive network
360 (i.e. No ANM) or actively managed network with either active curtailment control (ACC), Co-
361 ordinated Voltage Control (CVC) and Power Factor Control (PFC) applied individually or with ACC
362 combined with CVC or PFC.

363 Table 5 provides the results of hosting capacity for all studied cases and Table 6 is the
364 corresponding delivered energy. To aid comparison, the derived effective capacity factor, as the ratio
365 of actually delivered energy to the amount of energy that would have been produced at full capacity,
366 is given in Table 7.

367 To investigate the impact of different cases on network operation in terms of voltage and line
368 loading variations, the total hours during the year with *at least* one bus voltage actively constrained
369 by its upper limits are summarized and shown in Figure 6, with equivalent analyses for voltage lower
370 limits, line flow limits and average line loading given in Figures 7-9, respectively. The power injection
371 of DG would generally raise the voltage profiles and could also cause line overloading when the
372 injection largely exceeded local demand. The maximum voltage rise occurs during high generation-
373 low demand periods which ultimately determine the capacities of DG. While the voltages and line
374 loadings are constrained by the optimisation to prevent any limit violation, the frequency of them
375 reaching their limits and the average values over a whole year could indicate the effective use of the
376 network headroom for connecting renewable capacity.

377 4.1. Hosting Capacity for Single Renewable Type

378 Table 5.a shows that for all single resource cases in passive networks (i.e. no ANM) the capacity
379 is constrained to the same value due to the same worst case scenario event (maximum generation-
380 minimum demand), irrespective of the duration. There is however difference in the energy delivered
381 (Table 6.a) which reflects the variation in capacity factor of each generation type at the location
382 analysed.

383 Voltage rise during this scenario is the limiting factor to hosting capacity in this passive network
384 and which occur at the points of connection of the DG (i.e. buses gC and gE). It can be concluded that
385 voltage control schemes would release additional connectable capacity and CVC and PFC control are
386 successful for all renewable types. The increased capacity pushes the voltages in non-worst-case
387 periods towards the upper voltage limits, so the total hours where voltages reach the maximum
388 allowed values increase considerably, as shown in Figure 6.a. Additionally, the large reverse power
389 flows along the feeders result in lines' thermal limits being reached (Figure 8.a) in the lower rated
390 sections between buses A to gC and D to gE with overall loading levels raised considerably (Figure
391 9.a). The PFC controlled network cases record more hours constrained by voltage and reach the
392 inductive power factor limits (while attempting to lower voltage at the DG buses), but experience
393 fewer periods with constrained lines. CVC is the most successful single ANM scheme in increasing
394 DG capacity and energy delivery due to the highest line usage. The network wide effects of CVC are
395 more effective than the more localised impact of PFC.

396 Although the ACC cases do not enable as high connection capacity as the previous two control
397 cases, it does distinguish between resource types. By implementing ACC, the sporadic peaky nature
398 of the wave profile allows curtailment to remove its irregular peaks (as its maximum peak only
399 coincides with the low demand for 15 hours, as shown in Table 3) allowing greater capacity than the
400 tidal or wind cases. Curtailment is less effective for both the tidal and wind case which have more
401 regular maximum and other high production states. Despite the 22% extra capacity, the lower
402 capacity factor means wave still delivers 7% less energy (Table 6.a).

403 Combining ACC with another control scheme makes much more effective use of network
 404 capacity with the combination of ACC and CVC showing higher overall capacity and energy delivery
 405 than with PFC. The difference is particularly stark with the wave profile, where it is possible to
 406 connect almost six times the wave capacity than in the passive case, nearly matching the energy
 407 delivery by the equivalent wind case (Table 6.a). The combined control schemes stretch the power
 408 flow limits substantially and with PFC in particular, there is very frequent occurrence of upper
 409 voltage limits. Figure 7.a shows that lower voltage limits are occasionally met in the tidal and wind
 410 cases with ACC and CVC control, because high demand coincides with low generation and the range
 411 of the voltage set-point at the GSP OLTC restricts the network capacity. This does not occur with the
 412 wave case where maximum demand never coincides with zero generation.

413 The high overall capacity factor of the wind resource enables the wind cases to deliver the most
 414 energy in all cases. The choice of control is highly influential on the wave cases as outlined above and
 415 the tidal cases are consistently lower and the scope for capacity increases derived from ACC is
 416 lessened by the regular peaks and troughs associated with the resource. Despite differences in
 417 capacity and energy delivery among these single resources cases, their effective capacity factors in
 418 Table 7.a show the same trend: without ACC it is the same as the capacity factor of the resource; when
 419 ACC is involved, it is lower and the percentage reduction from its resource capacity factor is equal to
 420 the given curtailment limit, i.e. 10%.

421 **Table 5.** Connected generation capacity (MW) for a range of network control configurations. Rows
 422 indicate the generation types connected to the network. Columns indicate the network management
 423 scheme(s).

		No ANM	CVC	PFC	ACC	ACC CVC	ACC PFC
(a) single resource	Tidal	10.06	38.25	31.34	16.94	47.67	42.12
	Wave	10.06	38.25	31.34	21.37	58.83	52.43
	Wind	10.06	38.25	31.34	17.23	48.19	42.66
(b) hybrid resource	Tidal+Wave	10.78	39.20	32.51	27.30	76.15	67.59
	Tidal+Wind	10.06	38.25	31.34	23.51	67.48	59.40
	Wave+Wind	10.06	38.25	31.34	21.47	58.84	52.46
	Tidal+Wave+Wind	10.78	39.20	32.51	27.30	76.23	67.62

424 **Table 6.** Energy delivered (GWh/year) from different resource cases for a range of control
 425 configurations.

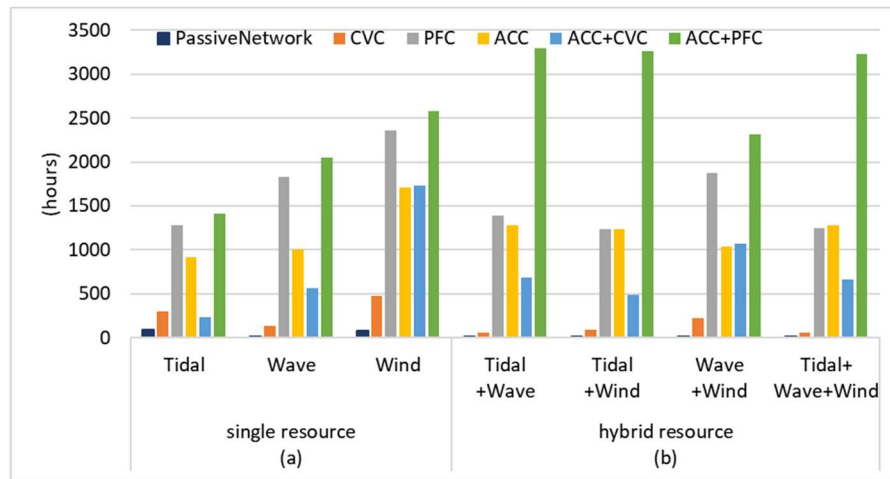
		No ANM	CVC	PFC	ACC	ACC CVC	ACC PFC
(a) single resource	Tidal	23.94	91.08	74.62	36.30	102.15	90.27
	Wave	33.49	127.40	104.38	64.05	176.34	157.15
	Wind	45.08	171.48	140.51	69.50	194.43	172.13
(b) hybrid resource	Tidal+Wave	29.06	118.85	83.64	72.66	202.11	178.99
	Tidal+Wind	34.96	142.78	80.86	72.46	213.45	187.64
	Wave+Wind	39.53	148.74	105.88	67.56	180.02	159.58
	Tidal+Wave+Wind	29.06	128.59	87.42	72.66	205.97	180.69

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Table 7. Effective capacity factor (delivered energy after curtailment) for a range of control configurations.

		No ANM	CVC	PFC	ACC	ACC CVC	ACC PFC
(a) single resource	Tidal	27.2%	27.2%	27.2%	24.5%	24.5%	24.5%
	Wave	38.0%	38.0%	38.0%	34.2%	34.2%	34.2%
	Wind	51.2%	51.2%	51.2%	46.1%	46.1%	46.1%
(b) hybrid resource	Tidal+Wave	30.8%	34.6%	29.4%	30.4%	30.3%	30.2%
	Tidal+Wind	39.7%	42.6%	29.5%	35.2%	36.1%	36.1%
	Wave+Wind	44.9%	44.4%	38.6%	35.9%	34.9%	34.7%
	Tidal+Wave+Wind	30.8%	37.4%	30.7%	30.4%	30.8%	30.5%

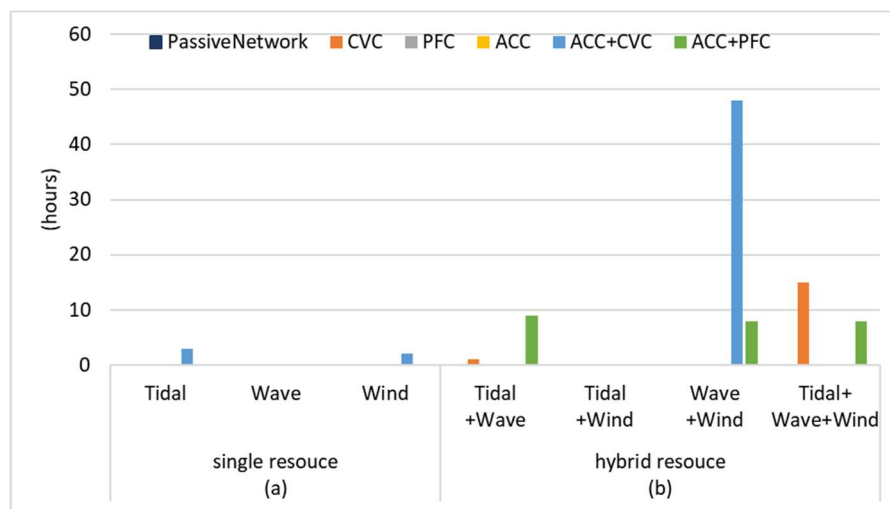
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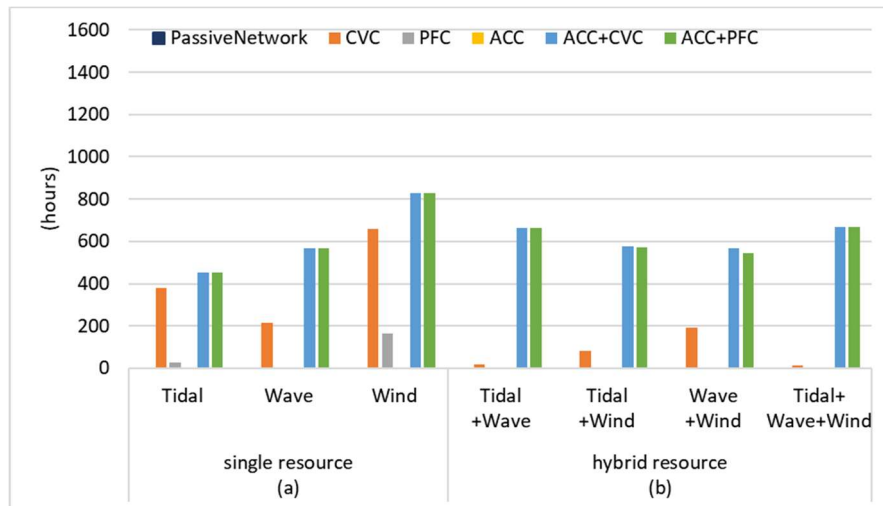
Figure 6. Total hours in the year when at least one bus voltage reaches its upper limits: (a) for single resource networks; (b) for hybrid resource networks.



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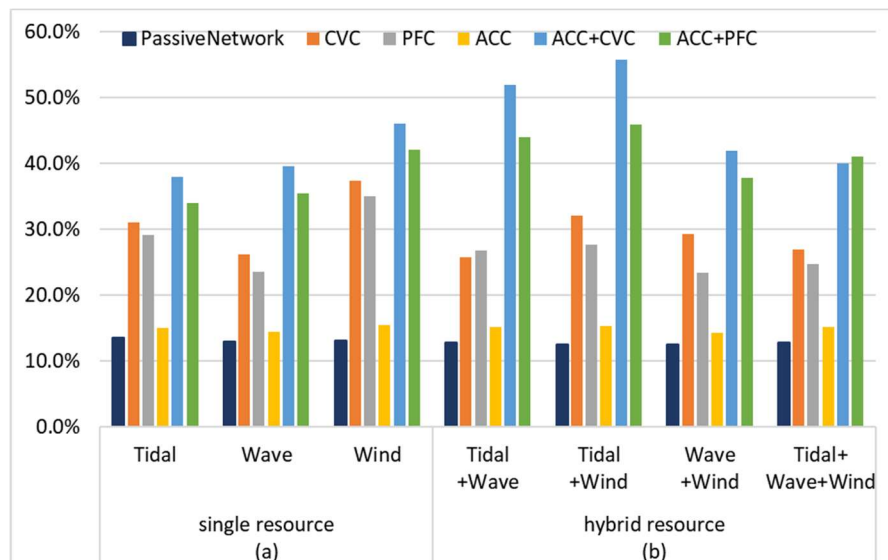
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Figure 7. Total hours in the year when at least one bus voltage reaches its lower limits: (a) for single resource networks; (b) for hybrid resource networks.



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Figure 8. Total hours in the year when the loading of at least one line reaches its full value: (a) for single resource networks; (b) for hybrid resource networks.



438
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Figure 9. Average line loading in the whole year as percentage of its full value: (a) for single resource networks; (b) for hybrid resource networks.

441 *4.2. Hosting Capacity for Hybrid Generation*

442 Tables 5.b and 6.b show the corresponding capacity and energy delivery for cases with multiple
 443 resources and Figure 10 shows the considerable variation in capacity split between resources in each
 444 case. In the passive cases, the tidal+wind and wave+wind combinations have overall capacity that
 445 precisely matches that of the individual resources; in both cases the wind represents 52% of the
 446 overall capacity suggesting the wind profile has the critical characteristic as far as limiting the hosting
 447 capacity. There is a small (~7%) capacity increase from connecting tidal+wave as the joint generation
 448 maximum never coincides with minimum demand; here the capacity split is 67% tidal meaning that
 449 the effective capacity factor is around 31%. The tidal+wave+wind case records an identical capacity
 450 split as no wind is allocated as this would introduce a further constraint due to the coincidence of
 451 maximum generation. The energy delivery from each combination is the weighted average of their
 452 resource capacity factors and all are lower than wind alone and higher than tidal alone. Overall, the
 453 passive network appears to be unable to exploit resource complementarity: neither capacity nor
 454 energy delivery fundamentally increases relative to single resources cases.

455 With CVC and to a lesser extent PFC there are considerable increases in capacity relative to the
 456 passive cases delivering higher capacity factors and energy delivery. Both control schemes are again

457 not able to fully exploit resource diversity as overall capacity increases are similar to single resource
458 cases, although the tidal+wave and triple resource cases again have marginally higher capacity (2 to
459 4%). There is more variation in capacity split between cases. With CVC wind becomes relatively more
460 significant in the tidal+wind case, marginally less in the wave+wind case and does considerably better
461 in the tidal+wind and triple resource cases. Wave improves its share while tidal decreases in all cases.
462 With PFC, tidal becomes more dominant with wind almost disappearing from the tidal+wind case
463 and not featuring in the triple resource case. The network-wide approach of CVC facilitates greater
464 exploitation of wind capacity than the more limited impact of PFC. The hosting capacity of hybrid
465 resources in passive and CVC/PFC hybrid networks is limited by the same constraining factors that
466 limit their single resource counterparts; the effect of CVC is clearly seen in Figure 7.b with the
467 occurrence of the low voltages at the GSP OLTC.

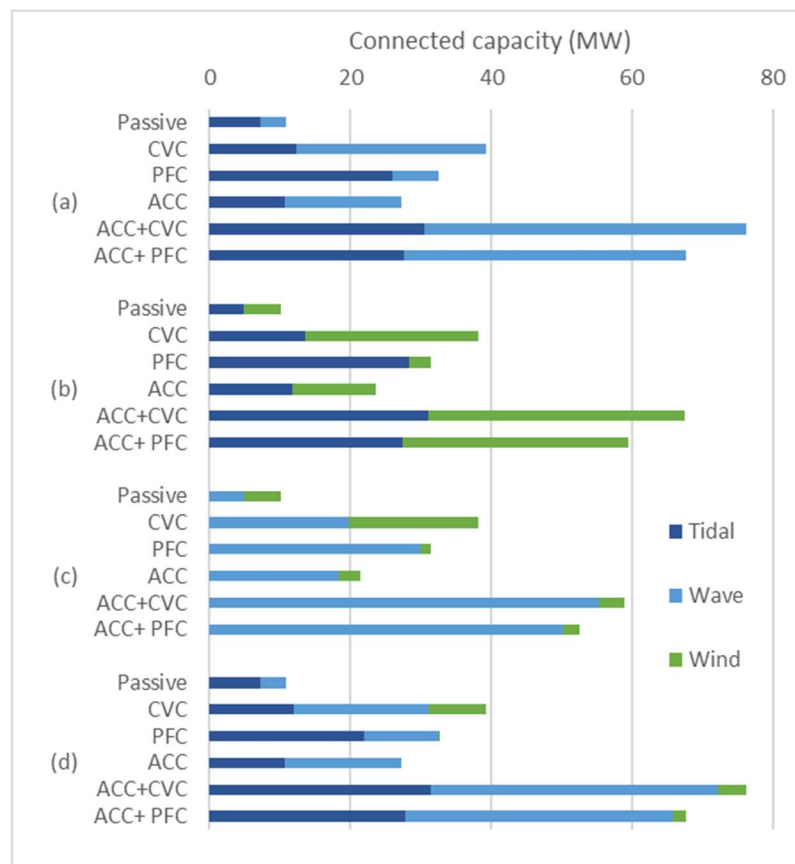
468 The first major benefit of hybrid generation is seen in the ACC cases. Complementarity is found
469 to support up to 60% increased capacity and energy delivery relative to single resource cases,
470 particularly the tidal+wave case. The worst performing hybrid case (wave+wind) has slightly greater
471 capacity than the highest for single resources (i.e. wave, Table 5.b) and its energy production is
472 around 5% higher (Table 6.b). Interestingly, with the exception of the wave+wind case, all other cases
473 produce more energy than the wind only case, albeit with considerably greater capacities. While the
474 increase in capacity relative to the passive case is lower for ACC than for either CVC or PFC case due
475 to less effective management of voltage constraints, selective curtailment delivers capacities and
476 energy production that are more balanced between resources (Figure 10); wave capacity becomes
477 dominant, particularly when combined with wind.

478 The combination of control schemes (ACC+CVC, ACC+PFC) facilitates greater exploitation of
479 the complementarity observed between resources. Both sets of cases see a similar pattern of capacity
480 split between resources with very balanced splits except in the triple resource and tidal+wind cases
481 where there is, respectively, little or no wind. The capacity gains over single resource cases is again
482 at most 60% (Table 5.b) with all but the wave+wind cases producing more energy than wind alone
483 (Table 6.b). The most effective is combining ACC with CVC: with ACC suppressing the peaks of the
484 wave profile and CVC managing voltage rise issues, the tidal+wave case makes greater use of
485 network line capacity than any other control configurations, pushing the average line loading closer
486 to its full value (Figure 9.b). With ACC+PFC, voltage limits constrain the network more than other
487 cases in Figure 6 and inductive power factor limits are regularly met as the generators attempt to
488 lower voltages.

489 While the capacity split between resources, as shown in Figure 10, indicates complex variation
490 between cases, it does allow indicative outcomes regarding complementarity among resource types.
491 The less similar the profiles, the better the complementarity with higher total capacity and a more
492 even split. Despite suggestions that wave and wind complementarity will smooth the power output
493 on useful timescales due to offsets of a number of hours [42], the regular co-occurrence of maximum
494 generation levels here means their complementarity is lower. In the case of wave+wind, considerably
495 more capacity is allocated to wave whose profile sees fewer worst-case periods and benefits more
496 from curtailment at peak output than wind. Alternatively, the combination of the more independent
497 tidal resource with either wave or wind supports higher capacity and a more even allocation between
498 generators due to the lower occurrence of high generation-low demand periods. Despite tidal+wind
499 connecting less capacity than tidal+wave, the large fraction of wind supports the largest energy
500 delivery of any case, almost 5 times more than the passive wind case (Table 5.b).

501 The cases with full hybrid (tidal+wave+wind) capacity replicate or rise slightly above the best
502 capacity obtained from the two-resource cases. Capacity is mainly allocated to tidal and wave, and a
503 small amount of wind capacity is only seen in the CVC, ACC+CVC and ACC+PFC cases (Figure 10.d).
504 This is because the complementarity between tidal and wave is better than with wind and
505 introducing wind adds undesirable periods of constraints. As a result, in terms of delivered energy,
506 the tidal+wave+wind case is outperformed by a two-resource combination in the ACC + CVC and
507 ACC+PFC cases. Overall, compared with the best performing two-resource cases, there was little
508 benefit seen from a combination of all three resources. Despite differences in capacity and energy

509 delivery, the same trend in constraining factors applies to the tidal+wave+wind case regarding the
 510 effectiveness of control configurations: ACC+CVC reaches voltage limits less than ACC+PFC (Figure
 511 6).
 512



513
 514 **Figure 10.** Capacity breakdown by resource type for hybrid cases with actively managed networks: (a)
 515 tidal+wave; (b) tidal+wind; (c) wind+wave; (d) tidal+wave+wind. Stack colour indicates the capacity of the
 516 individual resources.

517 5. Discussion

518 As far as we know this is the first analysis to consider these specific resources with regard to
 519 hosting capacity analysis and demonstrates some benefit from resource complementarity in terms of
 520 exploiting network capacity and energy delivery and very considerable benefits from active network
 521 management.

522 The complementarity level among resource types determines the level of capacity that can be
 523 connected. The less similar the profiles are the better. Despite suggestions that wave and wind
 524 complementarity will smooth the power output on useful timescales [42], offset from one another by
 525 a number of hours, this study finds the regular co-occurrence of both maximum generation levels
 526 would reduce the benefit from hybridisation. Instead, the combination of the independent tidal
 527 resource with either wave or wind supports higher capacity and energy delivery, due to their fewer
 528 occurrence of high generation-low demand periods.

529 The only comparator analysis is for solar and wind [19], and although the location, networks
 530 and specifics of the analysis were different, some qualitative comparison is possible. This showed
 531 that solar and wind exhibited greater complementarity and a more significant benefit in terms of
 532 additional hosting capacity and energy delivery. Further work looking at a wider portfolio of
 533 renewables would therefore be valuable.

534 While the focus here was very much on network capacity, recognising the value of resource
 535 diversity is a matter not just of local diversity in an individual network, but also the effect of
 536 geographical diversity as well as the operational and planning impacts on the wider power system.

537 This takes the value well beyond a view that more capacity is better towards a more nuanced
538 assessment of efficiency in terms of energy per unit of capacity and value for money, particularly
539 given the earlier developmental stage of tidal and wave. The application of this hybridisation
540 involving tidal, wave and offshore wind depends on the development of effective tidal and wave
541 generator arrays. While solar and wind currently offers a more mature alternative, for the best use of
542 hosting capacity, renewable combinations should be based on their complementary characteristics
543 and not simply their current industrial development.

544 There are a number of qualifications to the results that are worth stating. First, the analysis covers
545 only a year of data, meaning that it does not capture interannual variations in overall resource levels
546 nor the specific timings of each resource which do vary from weather system to weather system.
547 Some difference would be expected should a different year or longer period be used, although the
548 fundamental principles will hold. The framework is well set up to do a longer analysis. Secondly, the
549 resource levels and the statistical relationships between them will vary depending on the location
550 being affected by local geography as well as large scale wind, wave and tidal forcings. It would be
551 valuable to repeat the analysis at other locations to identify if the benefits of complementarity change
552 particularly as the relative level of capacity factors varies. Thirdly, the specific topology of the
553 network, local demand and the control systems will have a considerable impact on the local value of
554 complementarity.

555 5. Conclusions

556 In this work, the complementary value of three local offshore renewable resources – tidal, wave
557 and wind – for increasing network hosting capacity is evaluated. A generic AC OPF based hosting
558 capacity model is established to find the maximum connectable capacity for multiple renewable
559 resources. A scenario reduction technique is adapted to effectively consider long-term variation and
560 complementarity of the renewables in the NLP optimisation model.

561 The novel introduction of three resource types to the hosting capacity evaluation saw a complex
562 picture of increased network utilization through diversity. A second resource tended to increase
563 network hosting capacity and energy delivery but there was little benefit seen from a combination of
564 all three resources arising from co-occurrence of high generation with low demand that could not be
565 fully overcome by active network management. The analysis confirms that traditional passive control
566 schemes make inefficient use of network hosting capacity irrespective of the resource combination.
567 Although all active network control schemes made substantially more effective use of the network,
568 those involving active curtailment exploited coincidence characteristics among demand and multiple
569 renewable types well. Without curtailment the value of complementarity is quite modest for this
570 location although it should be emphasized that additional analysis is warranted to better understand
571 the phenomenon.

572 In future work, integration options such as energy storage and demand response can be
573 incorporated into the model to further assess the hosting capacity for the offshore renewable
574 resources. Considering that grid integration of variable renewable generation could also cause issues
575 with power quality, fault level and frequency, these technical challenges are worthy of further
576 research.

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579 G.P.H.; data curation, S.W.; writing—original draft preparation, S.H.; writing—review and editing, W.S., S.H.
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581 acquisition, G.P.H. All authors have read and agreed to the published version of the manuscript.

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