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# Instrument-model refinement in normalised reciprocal-vector space for X-ray Laue diffraction

Radosław Kamiński,<sup>a,\*</sup> Dariusz Szarejko,<sup>a</sup> Martin N. Pedersen,<sup>b</sup> Lauren E. Hatcher,<sup>c,d</sup> Piotr Łaski,<sup>a</sup> Paul R. Raithby,<sup>c</sup> Michael Wulff,<sup>e</sup> Katarzyna N. Jarzembska <sup>a,\*</sup>

<sup>*a*</sup> Department of Chemistry, University of Warsaw, Żwirki i Wigury 101, 02-089 Warsaw, Poland

<sup>b</sup> Niels Bohr Institute, University of Copenhagen, Universitetsparken 5, 2100 Copenhagen, Denmark

<sup>c</sup> Department of Chemistry, University of Bath, Claverton Down, Bath, BA2 7AY, United Kingdom

<sup>d</sup> School of Chemistry, Cardiff University, Main Building, Park Place, Cardiff, CF10 3AT, United Kingdom

<sup>e</sup> European Synchrotron Radiation Facility, 71 avenue des Martyrs, 38043 Grenoble, France

\* Corresponding authors: Radosław Kamiński (rkaminski85@uw.edu.pl) Katarzyna N. Jarzembska (katarzyna.jarzembska@uw.edu.pl)

**Abstract:** A simple yet efficient instrument-model refinement method for X-ray diffraction data is presented and discussed. The method is based on least-squares minimisation of differences between respective normalised refinement method on least-squares minimisation of differences between respective normalised refinement method is based on least-squares minimisation of differences between respective normalised. The method is based on least-squares minimisation of differences between the method works well on the method work of the method

**Synopsis:** Diffractometer instrument-model refinement method for X-ray Laue data is presented and tested. It is shown the approach works well even when the initial geometrical parameters deviate significantly from the target values.

**Keywords:** data processing, Laue diffraction, instrument model, refinement, X-ray

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#### 1. Introduction

Studies of short-lived light-induced excited states in crystals of small molecules are nt currently feasible almost exclusively at high-intensity X-ray sources, such as synchrotrons (Hatcher & Raithby, 2014, Coppens, 2011, Coppens et al., 2010). In this regard, the timeresolved (TR) X-ray diffraction Laue method, applied originally for macromolecular samples (<u>Ren et al., 1999, Hajdu et al., 1987</u>), constitutes the most efficient approach, as it allows effectively single-pulse diffraction experiments thanks to a superb X-ray flux. However, it that data processing in the case of a polychromatic X-ray beam is tonsiderably more difficult when compared to the monochromatic approach (<u>Coppens &</u> ncorrections which have to be applied. Such problems can be significantly reduced by provides only light-ON to light-OFF reflection intensity ratios (ION/IOFF). These in turn are <br/>further analysed so as to achieve electron-density photodifference maps and later structural models of transient species (Trzop et al., 2014, Jarzembska et al., 2014, Makal et al., 2012, Benedict et al., 2011, Jarzembska et al., 2019, Coppens et al., 2017, Vorontsov et al., 2010). nconsequently, the data processing pipeline concentrates here on the integration of diffraction determination. For small-molecule crystals the latter step is most efficiently achieved with the nt better software. Nevertheless, the success of this approach depends heavily on a proper n description of the used goniometer geometry, described with a mathematical instrument model (IM) including parameters of the experimental setup (e.g. detector distance, detector ncases, where sufficiently accurate instrument-model parameters are not available (an ்கள் பிரையில் பிருளியில் பிருளையில் பிருளையில் பிருளியில் பிருளியில் பிருளையில் பிருளையில் பிருளையில் பிருளையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிருளையில் பிருளையில் பிருளையில் பிருளையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிரையில் பிளையில் பிரையில் பிரையில் பிளையில் பிரையில் பிரையில் பிளையில் பிரையில ti s provided, for example, in the *PRECOGNITION* suite (<u>Šrajer *et al.*, 2000</u>) which, however, is ь войны ƴၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯၯ 

data processing is much more problematic. Hence, to fill-in this gap, in the current short data processing is much more problematic. Hence, to fill-in this gap, in the current short contribution a simple yet efficient *ab initio* method to refine instrument-model parameters is reported. Importantly, the algorithm relies only on diffraction spot positions, and does not require an orientation-matrix, wavelength spectrum, *etc.* 

# 2. Results and discussion

& A typical Laue X-ray diffraction experiment performed for a single-crystal sample is depicted schematically in Figure 1a. Diffraction experiment performed for a single-crystal sample being depicted within the single experiment of the typication of typication of the typication of the typication of typication of the typication of typication of the typication of typication of typication of the typication of the typication of the typication of the typication of typicati



 simplicity; this example data set consists of N frames; cross indicates the frame's centre). (b)
Overlay of two example data set consists of N frames; cross indicates the frame's centre). (b)
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Since in the Laue method a polychromatic X-ray beam is diffracted by a single-crystal sample, assigning a specific wavelength to a given recorded single diffracted by a single-crystal sample, assigning a specific wavelength to a given recorded single diffracted by a single-crystal sample, asmple, asmple, asmple, asmple, asmple diffraction sometimes and initially straightforward. Thus, before the orientation-matrix and indexing data processing steps, reconstruction of the reciprocal space is not feasible. (We note that such procedures are much easier when the unit cell parameters are a priori known, but become more cumbers and in the case of sparse diffraction patterns.) Nonetheless, it is possible to compute and is different easier with the compute different expersion. The compute different expersion of the compute expersion of the compute expersion. The compute expersion expersion

$$\mathbf{h}_{\sim} = \frac{\mathbf{s} - \mathbf{s}_0}{\|\mathbf{s} - \mathbf{s}_0\|} \tag{1}$$

where s and s and s and s and t mathematical domains domains

During the analysis of the available TR Laue data sets it appeared that, despite using an approximate IM parameters (*e.g.* detector distance is off by several millimetres), most of the approximate IM parameters (*e.g.* detector distance is off by several millimetres), most of the **h** proximate IM parameters (*e.g.* detector distance is off by several millimetres), most of the **h** proximate IM parameters (*e.g.* detector distance is off by several millimetres), most of the **h** proximate IM parameters (*e.g.* detector distance is off by several millimetres), most of the **h** proximate IM parameters (*e.g.* detector distance is detected by the several millimetres), most of the millimetres of the proximate is detected by the several millimetres of the several millimetres of the millimetres of the several millimetres of the several millimetres of the several millimetres of the millimetres of the several millimetres of the several

$$S = \sum_{j=1}^{N-1} \sum_{k(j)} \left\| \mathbf{h}_{0,k,j} - \mathbf{h}_{0,k,j+1} \right\|^2$$
(2)

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In our simple IM only three parameters are considered crucial for further data analysis with the RATIO method, namely the detector distance, the horizontal and vertical primary beam position on the detector surface: d,  $x_0$  and  $y_0$ , respectively. It is assumed that the detector is placed ideally perpendicularly at  $2\theta = 0^\circ$  with respect to the primary beam and there are no further goniometer misalignments. More details on the instrument model, used

ವೇಷ) ಹೊಡುತು ಹೊಡುತುತು ಹೊಡುತು ಹೊಡುತು ಹೊಡುತು ಹೊಡುತು ಹೊಡುತು ಹೊಡುತು ಹೊಡುತು ಹೊಡುತು ಹೊಡು

The algorithm was tested on a couple of model simulated and experimental data sets. The refinement of the instrument model on simulated X-ray Laue diffraction data sets for two crystal structures, *i.e.* of a small-molecule compound,  $Ag_2Cu_2L_4$  (L = 2-diphenylphosphino-3methylindole) (Koshevoy et al., 2011), and a pea lectin protein (Einspahr et al., 1986) constituted the primary benchmark. The silver(I)-copper(I) tetranuclear complex was studied by us using both TR Laue diffraction and high-pressure crystallography (triclinic space group  $P\overline{1}$ ) (Jarzembska et al., 2018, Jarzembska et al., 2014). In turn, the second simulated data set was generated for the pea lectin protein crystal structure, which was studied extensively with Laue diffraction by Helliwell and co-workers (orthorhombic space group  $P2_12_12_1$ ) (Cruickshank et al., 1991, Helliwell et al., 1989, Cruickshank et al., 1987, Machin, 1985). It should be noted that the simulated models account only for the diffraction geometry and not diffraction spot intensities (for details see the Supporting Information). Instead, experimental data sets of excellent quality collected for two copper(I) complexes are used as two further test cases. The first one,  $Cu(dppe)(dmp)PF_6$  (dppe = 1,2-bis(diphenylphosphino)ethane, dmp = 2,9-dimethyl-1,10-phenanthroline) (monoclinic space group  $P2_1/c$ ), was studied previously by Voronstsov et al. (Vorontsov et al., 2009) using the monochromatic TR technique and later by us using both Laue and in-house TR diffraction methods (Trzop et al., 2014, Coppens et al., 2016, Kaminski et al., 2014). The data set used here was measured at the 14-ID-B BioCARS beamline (Graber et al., 2011) at the Advanced Photon Source (APS). The data for the second compound, Cu(dppe)(dmdpp)PF<sub>6</sub> (dmdpp = 2,9-dimethyl-4,7-diphenyl-1,10-phenanthroline) (monoclinic space group  $P2_1/n$ ), were collected at the ID09 beamline (Wulff *et al.*, 2002) at the European Synchrotron Radiation Facility (ESRF). It should be noted that both data sets were initially integrated using our new 1-dimentional seed-skewness method (Szarejko et al., 2020), which resulted in a set of reflection intensities and positions. All data sets examined in this study are summarised in Table 1, including their abbreviations used hereafter. Exemplary simulated and experimental frames are shown in the Supporting Information.

Parameter	Simulated data		Experimental data	
Compound	Ag <sub>2</sub> Cu <sub>2</sub> L <sub>4</sub> complex	Pea lectin protein	Cu(dppe)(dmp)	Cu(dppe)(dmdpp)
			PF <sub>6</sub> complex	PF <sub>6</sub> complex
Data set abbreviation	simAgCu	simPeaL	expCuDppe	expCuDmdpp
X-ray source	-	-	14-ID-B at APS	ID09 at ESRF
Space group	<i>P</i> 1̄ (No. 2)	<i>P</i> 2 <sub>1</sub> 2 <sub>1</sub> 2 <sub>1</sub> (No. 19) <sup>£</sup>	<i>P</i> 2 <sub>1</sub> / <i>c</i> (No. 14)	<i>P</i> 2 <sub>1</sub> / <i>n</i> (No. 14)
a / Å	12.6106(2)	50.73(2)	20.2099(4)	14.1511(6)
<i>b /</i> Å	14.1988(3)	61.16(2)	13.6740(3)	14.2212(5)
<i>c /</i> Å	22.0662(4)	136.59(8)	26.5809(5)	27.3870(10)
α / °	76.3912(3)	90	90	90
β/°	81.5811(3)	90	95.5178(2)	98.373(3)
γ / °	66.8814(3)	90	90	90
Detector distance, d / mm	65.0 ¶	95.0 ¶	100.0 #	50.0 #
Beam position,				
$x_0$ / pix	1954.0 ¶	1215.0 ¶	1986.0 \$	1910.0 &
<i>y</i> <sub>0</sub> / pix	1973.0 ¶	1286.0 ¶	1964.0 \$	1924.0 &
Detector shape	square	square	square †	square ‡
Detector dimensions <sup>¥</sup> / mm	340.0	120.0 §	340.0 <sup>+</sup>	170.0 ‡
Frame dimensions $^{\text{F}}$ / pix	3840	2400 §	3840 <sup>†</sup>	3840 ‡
Pixel size <sup>¥</sup> / μm	89.0	20.0 §	<b>89.0</b> <sup>†</sup>	44.0 <sup>‡</sup>
Wavelength range				
$\lambda_{\min}$ / Å	0.8	0.5	0.8 €	0.75 €
$\lambda_{\rm max}$ / Å	1.1	2.6	1.1 €	1.1 €
Number of frames	91	91	91	91
Angular increment, $\Delta \phi$ / °	1.0	1.0	1.0	1.0
Angular coverage, $\phi_{ m tot}$ / °	91.0	91.0	91.0	91.0

**Table 1.** Selected parameters for simulated and experimental data sets used in this study.

<sup>¥</sup> Both dimensions (vertical and horizontal) are the same. <sup>£</sup> For simplicity systematic absences' conditions are omitted in this contribution. <sup>¶</sup> Values used in the simulation. <sup>§</sup> Parameters as close as possible to mimic the CEA reflex emulsion films (<u>Helliwell *et al.*</u>, 1989). <sup>#</sup> As assumed to be correct in the data collection software. <sup>§</sup> Primary beam position measured with the *ADXV* program (<u>Arvai, 2019</u>) from the reference frame with direct beam image (appropriate filters were used to maximally attenuate the beam). <sup>&</sup> Primary beam position was assumed to be close to the beamstop shadow centre. <sup>†</sup> Rayonix MX340-HS detector mounted at the 14-ID-B BioCARS beamline at APS (<u>Graber *et al.*</u>, 2011). <sup>‡</sup> Rayonix MX170-HS detector mounted at the ID09 beamline at ESRF (<u>Wulff *et al.*</u>, 2002). <sup>€</sup> Limiting values estimated from the  $\lambda$ -curve plots.

Results of the instrument-model refinement are shown in Table 2. In the case of simulated data, simulation with entities the instrument-model refinement are shown in Table 2. In the case of simulated data, simulated metator metat

In turn, regarding the data collected at the 14-ID-B beamline at APS, expCuDppe, the instrument geometry was tested with the PYP crystal and *PRECOGNITION* software. The primary beam position was determined by collecting its direct image by attenuating X-rays,

In the second case of the **expCuDmdpp** data set, collected at the ID09 beamline of the ESRF, we encountered some problems when indexing the measured data using the method of Kalinowski et al. without any IM refinement. As such, this data set presented a challenge for our software. The final step of the indexing method is to cluster the points in the Euler-angle space, each representing a single determined orientation matrix (the method is based on testing multiple orientation matrices). The final orientation matrix is considered to be an average of all matrices belonging to a single cluster. For the ESRF data, the detector distance was initially set and calibrated to 50 mm. The detector centre was not directly measured, but instead it was assumed to be very close to the centre of the X-ray beamstop shadow area ( $x_0$  = 1910 pix,  $y_0 = 1924$  pix; see the Supporting Information). However, starting from these values the orientation matrix hampered considerably further data processing. We ascribe these difficulties to imperfect instrument-model parameters, which tend to drift from their starting positions (properly calibrated initially) over the very long experiment time (ca. 5 days of constant data collection). The refinement of the IM parameters (final values: d = 47.25(2) mm,  $x_0 = 1904.1507(9)$  pix,  $y_0 = 1923.046(1)$  pix) with our new approach enabled us to find the orientation matrix readily and reliably. The total number of determined clusters increased considerably (to 268), which indicated correct determination of the crystal orientation. It is also worth noting the refined beam centre stayed in the beamstop shadow area, which constituted additional confirmation of the IM refinement method's validity.

 **Table 2.** Refinement of selected parameters for the studied Laue data sets. Note d is expressed in mm, whereas x<sub>0</sub> and y<sub>0</sub> in native detector pixel coordinates (see the Supporting Information). In certain cases the errors are so small that a non-standard notation for values and their e.s.d.

Data sat	Initial values			Final values			
Dulu sel	d	$x_0$	$y_0$	d	$x_0$	${\mathcal Y}_0$	
simAgCu¶	70.0	1954.0	1973.0	65.00 ± 8·10 <sup>-5</sup>	$1954.00 \pm 1.10^{-5}$	1973.00 ± 2·10 <sup>-5</sup>	
	65.0	1920.0	1973.0	65.00 ± 8·10 <sup>-5</sup>	1954.00 ± 1·10 <sup>-5</sup>	1973.00 ± 2·10 <sup>-5</sup>	
	80.0	1920.0	1985.0	65.00 ± 8·10 <sup>-5</sup>	$1954.00 \pm 1.10^{-5}$	$1973.00 \pm 1.10^{-5}$	
simPeaL <sup>\$</sup>	105.0	1215.0	1286.0	95.00 ± 3·10 <sup>-5</sup>	$1215.00 \pm 1.10^{-6}$	$1286.00 \pm 1.10^{-6}$	
	95.0	1240.0	1286.0	95.00 ± 3·10 <sup>-5</sup>	$1215.00 \pm 1.10^{-6}$	$1286.00 \pm 1.10^{-6}$	
	100.0	1240.0	1250.0	95.00 ± 3·10 <sup>-5</sup>	$1215.00 \pm 1.10^{-6}$	$1286.00 \pm 1.10^{-6}$	
expCuDppe ¥	120.0	1986.0	1964.0	100.80(7)	1986.174(5)	1965.013(7)	
	100.0	1950.0	1964.0	100.80(7)	1986.174(5)	1965.013(7)	
	120.0	1950.0	1950.0	100.80(7)	1986.177(5)	1965.020(7)	
expCuDmdpp	50	1910	1924	47.25(2)	1904.1507(9)	1923.046(1)	
	55	1900	1900	47.25(2)	1904.1497(9)	1923.044(1)	
	70	1920	1950	47.25(2)	1904.1504(9)	1923.047(1)	
<sup>¶</sup> Target values for <b>simAgCu</b> : $d = 65.0$ mm, $x_0 = 1954.0$ pix, $y_0 = 1973.0$ pix (Table 1). <sup>\$</sup> Target							
values for <b>simPeaL</b> : $d = 95.0$ mm, $x_0 = 1215.0$ pix, $y_0 = 1286.0$ pix (Table 1). * Target values for							
expCuDppe: d =	= 100.0 r	nm, $x_0 = 1$	986.0 pix,	$y_0 = 1964.0$ pix (	Table 1).		

Finally, it should be stressed that the main assumption of the method is that the crystal remains fixed during the stressed that the main assumption of the method is that the crystal or stressed that the method is remains fixed during the entire experiment, thus any irregular movements during the tata collection are eliminated. This is most efficiently realised us processed us the standard processed that the method is respectively in the crystal to crystal to the cr

#### 3. Conclusions and summary

A new algorithm to refine the diffractometer instrument model using normalised reciprocal space vectors has been developed and tested for use in the analysis of synchrotron-multiple consecutive frames are recorded for different crystal orientations and no irregular <br/>spot positions and frame angular setting angles. As it has been proved for both model <br/>simulated and experimental data sets, the method provides very good results. The refinement <br/>Most importantly, the method allows for determination of the IM parameters which had been previously unknown or had been known with low accuracy (which significantly hampered the orientation matrix determination). This constitutes a major improvement in the smallmolecule X-ray Laue diffraction processing pipeline. The algorithm is implemented in our new (Kalinowski et al., 2011, Kalinowski et al., 2012), is available from the authors upon request (the program code will be available publicly open-source shortly).

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### **Associated content**

## Supporting information:

The Supporting Information is available free of charge and contains definitions of all parameters indispensable to describe the Laue diffraction geometry and the instrument model together with equations needed for least-squares refinement. It also contains all information about simulation of the Laue data sets, as well as example frames of both simulated and experimental data sets.

#### Author information

### Corresponding authors:

Radosław Kamiński (rkaminski85@uw.edu.pl)

Katarzyna N. Jarzembska (katarzyna.jarzembska@uw.edu.pl)

# **ORCID:**

Radosław Kamiński: 0000-0002-8450-0955 Dariusz Szarejko: 0000-0003-2624-5551 Martin N. Pedersen: 0000-0001-6975-5071 Lauren E. Hatcher: 0000-0002-1549-9727 Piotr Łaski: 0000-0002-6410-5587 Paul R. Raithby: 0000-0002-2944-0662 Michael Wulff: 0000-0003-3784-9019 Katarzyna N. Jarzembska: 0000-0003-4026-1849 **Notes:** 

The authors declare no competing financial interest.

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# SUPPORTING INFORMATION

# Instrument-model refinement in normalised reciprocal-vector space for X-ray Laue diffraction

Radosław Kamiński,<sup>*a*,\*</sup> Dariusz Szarejko,<sup>*a*</sup> Martin N. Pedersen,<sup>*b*</sup> Lauren E. Hatcher,<sup>*c,d*</sup> Piotr Łaski,<sup>*a*</sup> Paul R. Raithby,<sup>*c*</sup> Michael Wulff,<sup>*e*</sup> Katarzyna N. Jarzembska <sup>*a*,\*</sup>

<sup>a</sup> Department of Chemistry, University of Warsaw, Żwirki i Wigury 101, 02-089 Warsaw, Poland

<sup>b</sup> Niels Bohr Institute, University of Copenhagen, Universitetsparken 5, 2100 Copenhagen, Denmark

<sup>c</sup> Department of Chemistry, University of Bath, Claverton Down, Bath, BA2 7AY, United Kingdom

<sup>d</sup> School of Chemistry, Cardiff University, Main Building, Park Place, Cardiff, CF10 3AT, United Kingdom

<sup>e</sup> European Synchrotron Radiation Facility, 71 avenue des Martyrs, 38043 Grenoble, France

\* Corresponding authors: Radosław Kamiński (rkaminski85@uw.edu.pl) Katarzyna N. Jarzembska (katarzyna.jarzembska@uw.edu.pl)

#### 1S. Instrument model and refinement details

Matrix notation for vectors is used; a<sup>T</sup> stands for a transpose of the matrix **a**; scalar product in Cartesian basis is a vectors is used; **a**<sup>T</sup> stands for a transpose of the matrix **a**; scalar product in to not transpose of the sisten is used; **b** is use; **b** is use;

$$\mathbf{x} = d \cdot \mathbf{s}_0 + \Delta \mathbf{r} = \begin{bmatrix} d \\ -(x - x_0) \\ y - y_0 \end{bmatrix}_L$$
(S1)

$$\mathbf{s} = \frac{\mathbf{x}}{\|\mathbf{x}\|}$$
,  $\mathbf{y} = \mathbf{s} - \mathbf{s}_0$ ,  $\mathbf{h} = \frac{\mathbf{y}}{\|\mathbf{y}\|}$  (S2)

where  $\|\cdot\|$  is the vector norm. See Figure 1S for visualisation of respective vectors and coordinate systems. Finally, vector  $\mathbf{h}$  rotated to the goniometer-head-fixed coordinate system  $G = (\mathbf{g}_x, \mathbf{g}_y, \mathbf{g}_z)$  is obtained by application of the rotation matrix  $\mathbf{R}$ , different for each frame:  $\mathbf{h}_0 = \mathbf{R}^T \mathbf{h}$  (where  $\mathbf{R}^{-1} = \mathbf{R}^T$ ). Note that G and L coordinate systems overlay for all goniometer angles set to zero.



**Figure 1S.** Detector and laboratory coordinate systems,  $D_0 = (\mathbf{d}_x, \mathbf{d}_y, \mathbf{d}_z)$  and  $L = (\mathbf{e}_x, \mathbf{e}_y, \mathbf{e}_z)$ , and vectors needed in the calculations.

Native ('raw') spot position on the detector is expressed in  $D_2 = (\mathbf{i}, \mathbf{j}, \mathbf{k})$  pixel-based coordinate system anchored in the centre of the top left detector pixel (right-handed,  $\mathbf{i}$  points down,  $\mathbf{j}$  right); this is a basic definition used in majority of image processing applications. We introduce real-valued coordinate system  $D_1 = (\boldsymbol{\delta}_x, \boldsymbol{\delta}_y, \boldsymbol{\delta}_z)$  centred on top left detector corner (orientation the same as for  $D_2$ ). Relations of spot coordinates in  $D_0$  and these two coordinate systems are expressed by the following formulas:

$$\begin{bmatrix} x \\ y \\ 0 \end{bmatrix}_{D_0} = \begin{bmatrix} x_{\delta} - \frac{1}{2} p_{h} n_{h} \\ \frac{1}{2} p_{v} n_{v} - y_{\delta} \\ 0 \end{bmatrix}_{D_1} = \begin{bmatrix} j + \frac{1}{2} p_{h} (1 - n_{h}) \\ \frac{1}{2} p_{v} (n_{v} - 1) - i \\ 0 \end{bmatrix}_{D_2}$$
(S3)

where  $n_h$  and  $n_v$  are number of detector pixels, and  $p_h$  and  $p_v$  are pixel sizes, for horizontal and vertical directions, respectively.

To perform a least-squares minimisation the derivatives of the norm of the difference of two computed  $\mathbf{h}_{0}$  vectors for the same spot appearing for two consecutive frames (*i.e.*  $\Delta \mathbf{h}_{0,k,j} = \mathbf{h}_{0,k,j} - \mathbf{h}_{0,k,j+1}$ ) are needed. The derivatives are computed as follows:

$$\frac{\partial}{\partial p} \left\| \Delta_{\widetilde{\nu}^{0,k,j}} \right\| = \frac{\Delta_{\widetilde{\nu}^{0,k,j}}^T}{\left\| \Delta_{\widetilde{\nu}^{0,k,j}} \right\|} \left( \frac{\partial}{\partial p} \mathbf{h}_{0,k,j} - \frac{\partial}{\partial p} \mathbf{h}_{0,k,j+1} \right)$$
(S4)

where  $\mathbf{h}_{o,k,j}$  is vector for the *k*-pair of  $\mathbf{h}_0$  vectors matched for frames *j* and *j* + 1; *p* is selected refined parameter. Accordingly (for clarity we drop indexes *k* and *j*; note matrices **R** depend on frame index *j*):

$$\frac{\partial}{\partial p} \underset{\sim}{\mathbf{h}}_{0} = \mathbf{R}^{\mathrm{T}} \left( \frac{1}{\|\mathbf{y}\|} \left( \frac{\partial \mathbf{y}}{\partial p} \right) - \frac{\mathbf{y}}{\|\mathbf{y}\|^{3}} \left[ \mathbf{y}^{\mathrm{T}} \left( \frac{\partial \mathbf{y}}{\partial p} \right) \right] \right)$$
(S5)

$$\frac{\partial \mathbf{y}}{\partial p} = \frac{1}{\|\mathbf{x}\|} \left( \frac{\partial \mathbf{x}}{\partial p} \right) - \frac{\mathbf{x}}{\|\mathbf{x}\|^3} \left[ \mathbf{x}^{\mathrm{T}} \left( \frac{\partial \mathbf{x}}{\partial p} \right) \right]$$
(S6)

Since  $\mathbf{x} = \begin{bmatrix} d & -(x - x_0) & y - y_0 \end{bmatrix}_L^T$  its derivatives simply equal to:

$$\frac{\partial \mathbf{x}}{\partial d} = \begin{bmatrix} 1\\0\\0 \end{bmatrix}_{L} , \quad \frac{\partial \mathbf{x}}{\partial x_{0}} = \begin{bmatrix} 0\\1\\0 \end{bmatrix}_{L} , \quad \frac{\partial \mathbf{x}}{\partial y_{0}} = \begin{bmatrix} 0\\0\\-1 \end{bmatrix}_{L}$$
(S7)

Please note the actual implementation of the procedure works in native detector pixel coordinates, as denoted above in the equation S3. Therefore, inside the program source code the last component of the third derivative in S7 (*i.e.*  $\partial \mathbf{x} / \partial y_0$ ) is in fact positive.

Reflections from two consecutive frames j and j + 1 are considered to form a pair k when the simple geometrical criterion,

$$\arccos\left(\mathbf{h}_{0,k,j}^{\mathrm{T}}\mathbf{h}_{0,k,j+1}\right) = \theta \le \theta_0$$
(S8)

is fulfilled, where  $\theta_0$  is the specified threshold (note here both vectors are of unit length, thus obviously  $\|\mathbf{h}_{0,k,j}\| \cdot \|\mathbf{h}_{0,k,j+1}\| = 1$ ).

#### 2S. Simulation of X-ray Laue patterns

Instrument model used in simulations is more general, which provides more flexibility for future applications. In addition to coordinate systems *L* and *G*, presented in the previous section, we define also extra coordinate systems  $K^* = (\mathbf{a}^*, \mathbf{b}^*, \mathbf{c}^*)$  (non-Cartesian reciprocal crystal coordinate system) and  $C = (\mathbf{c}_x, \mathbf{c}_y, \mathbf{c}_z)$  (introduced to easily decompose the orientation matrix into 'orientation' and 'unit-cell shape' parts). The transformation between  $K^*$  and *C* systems is defined with the following matrix **B** (expressed in reciprocal lattice unit cell parameters):

$$\mathbf{B} = \begin{bmatrix} a^* & 0 & 0 \\ b^* \cos(\gamma^*) & b^* \sin(\gamma^*) & 0 \\ c^* \cos(\beta^*) & c^* \frac{\cos(\alpha^*) - \cos(\gamma^*)\cos(\beta^*)}{\sin(\gamma^*)} & c^* \left[ 1 - \cos(\beta^*) - \frac{\cos(\alpha^*) - \cos(\gamma^*)\cos(\beta^*)}{\sin(\gamma^*)} \right] \end{bmatrix}$$
(S9)

where the transformation takes the form:

$$\mathbf{h}_{C} = \mathbf{B}^{\mathrm{T}} \cdot \mathbf{h}_{K^{*}} \tag{S10}$$

in which  $\mathbf{h} = h\mathbf{a}^* + k\mathbf{b}^* + l\mathbf{c}^* = x_c\mathbf{c}_x + y_c\mathbf{c}_y + z_c\mathbf{c}_z$ . The relationship between  $K^*$  and C frames is depicted in Figure 2S.



**Figure 2S.** Relationship between  $C = (\mathbf{c}_x, \mathbf{c}_y, \mathbf{c}_z)$  and  $K^* = (\mathbf{a}^*, \mathbf{b}^*, \mathbf{c}^*)$  coordinate systems. Vector  $\mathbf{a}^*$  is along  $\mathbf{c}_x$ , and  $\mathbf{b}^*$  lies in the plane formed by  $\mathbf{c}_x$  and  $\mathbf{c}_y$  vectors.

For computational purposes the matrix **B** is expressed in direct lattice unit-cell parameters using the very well-known formulas:

$$a^{*} = \frac{bc \sin \alpha}{V} \qquad b^{*} = \frac{ac \sin \beta}{V} \qquad c^{*} = \frac{ab \sin \gamma}{V}$$

$$\cos(\alpha^{*}) = \frac{\cos \beta \cos \gamma - \cos \alpha}{\sin \beta \sin \gamma} \qquad \cos(\beta^{*}) = \frac{\cos \alpha \cos \gamma - \cos \beta}{\sin \alpha \sin \gamma} \qquad \cos(\gamma^{*}) = \frac{\cos \alpha \cos \beta - \cos \gamma}{\sin \alpha \sin \beta} \qquad (S11)$$

$$\sin(\gamma^{*}) = \frac{V}{abc \sin \alpha \sin \beta} \qquad V = abc\sqrt{1 - \cos^{2} \alpha - \cos^{2} \beta - \cos^{2} \gamma + 2 \cos \alpha \cos \beta \cos \gamma}$$

Orientation matrix **U** describes how the crystal reciprocal axes are related to the goniometer-head-fixed coordinate system (*i.e.* relation between  $K^*$  and G coordinate systems). We define the matrix **U** as follows:

$$\mathbf{h}_G = \mathbf{U} \cdot \mathbf{h}_{K^*} \tag{S12}$$

where for any vector we have  $\mathbf{h} = h\mathbf{a}^* + k\mathbf{b}^* + l\mathbf{c}^* = x_g\mathbf{g}_x + y_g\mathbf{g}_y + z_g\mathbf{g}_z$ . This definition is identical to the one used by Kalinowski *et al.* (Kalinowski *et al.*, 2011) and closely related to the definitions used in the seminal paper by Busing & Levy (Busing & Levy, 1967). The relation between *G* and *C* coordinate systems (both are Cartesian) is then expressed with matrix **C** as follows:

$$\mathbf{h}_G = \mathbf{C}^{\mathrm{T}} \cdot \mathbf{h}_C \tag{S13}$$

From this definition it follows that  $\mathbf{h}_G = \mathbf{C}^T \mathbf{B}^T \cdot \mathbf{h}_{K^*} = (\mathbf{B}\mathbf{C})^T \cdot \mathbf{h}_{K^*}$ . Rotation matrix **C** is expressed via Euler angles ( $\theta_1$ ,  $\theta_2$  and  $\theta_3$ ) in the following way:

$$\mathbf{C} = \mathbf{R}_1(\theta_1) \cdot \mathbf{R}_2(\theta_2) \cdot \mathbf{R}_3(\theta_3)$$
(S14)

where

$$\mathbf{R}_{1}(\theta_{1}) = \mathbf{R}_{2}(\theta_{2}) = \mathbf{R}_{3}(\theta_{3}) = \\
= \begin{bmatrix} \cos(\theta_{1}) & -\sin(\theta_{1}) & 0\\ \sin(\theta_{1}) & \cos(\theta_{1}) & 0\\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0\\ 0 & \cos(\theta_{2}) & -\sin(\theta_{2})\\ 0 & \sin(\theta_{2}) & \cos(\theta_{2}) \end{bmatrix} = \begin{bmatrix} \cos(\theta_{3}) & -\sin(\theta_{3}) & 0\\ \sin(\theta_{3}) & \cos(\theta_{3}) & 0\\ 0 & 0 & 1 \end{bmatrix}$$
(S15)

Finally, every crystal is appropriately rotated on the goniometer. We assume all rotations of the goniometer are defined as counter-clockwise. When the goniometer angles are rotated, the goniometer are defined as counter-clockwise. When the goniometer angles are rotated, the selected h vector are defined as counter-clockwise. When the goniometer angles are rotated, the selected h vector h coordinates in G remain constant). General scheme angles are rotated alongside with the goniometer hender angles are rotated alongside with the goniometer-head-fixed rotated and the selected h vector is rotated alongside with the goniometer hender angles are rotated, the selected h vector hender and selected h vector is rotated alongside with the goniometer hender angles are rotated alongside with the goniometer between the goniometer angles are rotated along and meter angles are rotated as the selected with the goniometer angles are rotated as the selected with the goniometer angles are rotated as the selected with the goniometer angles are rotated as the selected with the goniometer and the selected with the sel

$$\mathbf{h}_L = \mathbf{R}_z(\omega) \cdot \mathbf{h}_0 \tag{S16}$$

$$\mathbf{h}_{O} = \mathbf{R}_{\chi}(\chi) \cdot \mathbf{h}_{M} \tag{S17}$$

$$\mathbf{h}_M = \mathbf{R}_z(\phi) \cdot \mathbf{h}_G \tag{S18}$$

This, finally, yields a total rotation as:

$$\mathbf{h}_L = \mathbf{R} \cdot \mathbf{h}_G \tag{S19}$$

where the matrix **R** takes the form:

$$\mathbf{R} = \mathbf{R}_{z}(\omega) \cdot \mathbf{R}_{x}(\chi) \cdot \mathbf{R}_{z}(\phi)$$
(S20)

and

$$\mathbf{R}_{z}(\omega) = \mathbf{R}_{x}(\chi) = \mathbf{R}_{z}(\phi) =$$

$$= \begin{bmatrix} \cos \omega & -\sin \omega & 0\\ \sin \omega & \cos \omega & 0\\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0\\ 0 & \cos \chi & -\sin \chi\\ 0 & \sin \chi & \cos \chi \end{bmatrix} = \begin{bmatrix} \cos \phi & -\sin \phi & 0\\ \sin \phi & \cos \phi & 0\\ 0 & 0 & 1 \end{bmatrix}$$
(S21)



**Figure 3S.** Schematic representation of the 4-circle Euler-type goniometer. (*a*) The instrument with all angles set to zero. (*b*) Instrument with all angles departed from zero position (all rotations are defined as positive then counter-clockwise; for clarity of the figure the  $\omega$  is shown as negative).

Finally, the equation allowing to compute the coordinates of vector  $\mathbf{h}$  in laboratory frame *L* given all the matrices and transformation is as follows:

$$\mathbf{h}_{L} = \mathbf{R} \cdot \mathbf{h}_{G} = \mathbf{R} \cdot (\mathbf{B}\mathbf{C})^{\mathrm{T}} \cdot \mathbf{h}_{K^{*}}$$
(S22)

Where we introduced vector  $\mathbf{h}_0 = \mathbf{h}_G = (\mathbf{B}\mathbf{C})^T \mathbf{h}_{K^*}$  (*i.e.* vector  $\mathbf{h}$  before goniometer rotation angles applied, as in the previous section; notation  $\mathbf{h}_0$  is used in the main text for convenience).

For Laue diffraction every spot falling into the region between two extreme Ewald spheres is recorded. For each  $\mathbf{h}$  vector its wavelength is calculated using a well-known formula:

$$\lambda = -2\frac{\mathbf{h} \cdot \mathbf{s}_0}{\|\mathbf{h}\|^2} = -2\frac{\mathbf{h} \cdot \mathbf{s}_0}{\mathbf{h} \cdot \mathbf{h}}$$
(S23)

The implemented algorithm follows then a simple path:

(i) Generation of the allowed  $\mathbf{h}_{K^*}$  vector indices (*i.e. h*, *k* and *l*) in reciprocal crystal basis  $K^*$ . Limiting values are estimated from the larger Ewald sphere radius  $(1/\lambda_{\min})$ . Additional  $\sin \theta / \lambda$  cut-off can be taken into account. At this point the systematic absences can also omitted (not implemented yet).

(ii) Generated  $\mathbf{h}_{K^*}$  vectors are transformed to the goniometer-head-fixed Cartesian reference frame of *G* using the  $\mathbf{h}_G = (\mathbf{BC})^T \mathbf{h}_{K^*}$ . This set is used in the next steps.

(iii) For every frame (with known frame rotation angles) all  $\mathbf{h}_G$  are rotated to the laboratory frame *L*:  $\mathbf{h}_L = \mathbf{R} \cdot \mathbf{h}_0$ .

(iv) For each h<sub>L</sub> the wavelength at which the diffraction would occur for this particular (iv) For each h<sub>L</sub> the wavelength at which the diffraction would occur for this particular (iv) For each h<sub>L</sub> the wavelength at which the diffraction would occur for this particular vector is computed. At this step we check which the diffraction would occur for this particular vector is computed. At this step we check which the diffraction would occur for this particular vector is computed. At this step we check which the diffraction would occur for this particular vector is computed. At this step we check which the diffraction would occur for the difference vector is computed. At this step we check which the diffraction would occur for the difference vector is computed. At this step we check which the diffraction would occur for the difference vector is computed. At this step we check which the diffraction would occur for the difference vector is computed. At this step we check which the difference vector is computed. At this step we check which the difference vector is computed. At this step we check we check which the difference vector is computed. At this step we check we check

(v) Diffraction equation is used to compute the scattering vector  $\mathbf{s} = \mathbf{s}_0 + \lambda \cdot \mathbf{h}_L$ , and it is checked whether the detector surface intersects the line along this vector (i.e. we check if the spot lies in the detector area). If the last is true, the coordinates of the spot on the detector are computed and saved into the HDF5 file.

(vi) Steps (iii)-(v) are repeated for all frames (a number specified by the user).



**Figure 4S.** Overlay of two adjacent frames (angular interval  $\Delta \phi = 1^{\circ}$ ) shown for simulated data (silver(I)-copper(I) complex quoted in the main text) – green spots: frame for  $\phi = 0^{\circ}$ , red spots: frame for  $\phi = 1^{\circ}$  (crystal horizontal rotation). Large dots represent selected reflections shown in Figure 1*b*.



Figure 5S. Example simulated frames. (a) Single frame generated for the simAgCu test sample. (b) Single frame generated for the simPeaL test sample. For simulation details see Table 1 in the manuscript text.

