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Mechanical Properties and Free Formaldehyde Content of Particleboards Produced using Ammonium Sulphate-Based Hardener Partially Replaced with Tartaric Acid

Mehanička svojstva i sadržaj slobodnog formaldehida ploča iverica izrađenih primjenom katalizatora na bazi amonijeva sulfata djelomično zamijenjenoga vinskom kiselinom

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ABSTRACT • The use of resins, whose curing reaction takes place by high temperature and hardener addition, is inevitably involved in particleboard manufacturing process. In addition to commercial hardeners, such as ammonium sulphate, with the aim of optimizing the production process and reducing the production costs, a certain percentage of hardener can, among other things, be replaced with price affordable bio-based materials. Tartaric acid, that is its salts (tartrates), which are commercially produced for the needs of wine and food industries, are a part of the aforementioned group of products. Since tartaric acid is a relatively inexpensive, readily available, weak diprotic and aldaric acid, the question arises whether it can be used as a component of the hardener system for curing urea-formaldehyde resins that are commercially used in particleboard production. For that reason, in this paper, the influence of partial replacement of ammonium sulphate hardener with tartaric acid on the mechanical properties (bending strength, modulus of elasticity and internal bond) and free formaldehyde content of experimentally produced particleboards was examined. Boards thickness, density and moisture content were also determined. The test results suggest that tartaric acid has a beneficial effect on the above particleboard properties, but they also indicate that the extent of that effect is strongly dependent on panel press time.

Key words: particleboards; hardener; tartaric acid; mechanical properties; free formaldehyde content

SAŽETAK • Proces proizvodnje ploča iverica neminovno podrazumijeva upotrebu smola čija se reakcija otvrdnjavanja ostvaruje uz pomoć povišene temperature i katalizatora. Uz komercijalne katalizatore poput amonijeva

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sulfata, radi optimizacije procesa i racionalizacije troškova proizvodnje ploča, katalizatore je u određenom postotku moguće zamijeniti, među ostalim, i cijenom prihvatljivim proizvodima na biobazi. U navedenu se skupinu proizvoda svrstava i vinska kiselina, točnije njezine soli (tartarati), komercijalno proizvedene za potrebe vinske i prehrambene industrije. S obzirom na to da je vinska kiselina relativno jeftina, lako dostupna, slaba diprotonska, aldarna kiselina, postavlja se pitanje potencijala njezine primjene u sustavima katalizatora za otvrdnjavanje ureaformaldehidne smole koja se upotrebljava u proizvodnji ploča iverica. Upravo je zato u ovom radu ispitano kako se zamjena dijela amonijeva sulfata tartaratnom kiselinom odražava na mehanička svojstva (savojnu čvrstoću, modul elastičnosti, vlačnu čvrstoću) i na koncentraciju slobodnog formaldehida eksperimentalno proizvedenih ploča iverica. Usto, u eksperimentu su određene debljina i gustoća ploča te sadržaj vode u njima. Rezultati ispitivanja upućuju na to da dodatak vinske kiseline povoljno utječe na navedena svojstva ploča, ali i na činjenicu kako taj učinak iznimno ovisi o vremenu prešanja ploča.

Ključne riječi: ploče iverice; katalizator; vinska kiselina; mehanička svojstva; koncentracija slobodnog formaldehida

1 INTRODUCTION

1. UVOD

The urea-formaldehyde (UF) resin is the predominant resin in today's modern particleboard production. This is due to its low price, water solubility, fire resistance, good thermal conductivity, absence of colour of cured resin and its easy adaptation to different curing conditions (Pizzi, 2003). Commonly, UF resins are cured at elevated temperatures using acidic hardeners (catalyst), such as ammonium sulphate $((NH_4)_2SO_4)$. As resin curing depends on the type of hardener, its addition, pH value and solid content (Uner and Olgun, 2017; Xing et al., 2007), the use of various hardeners, other than the above mentioned, is also possible. Such hardeners include ammonium chloride (Xing et al., 2007), sodium chloride, sodium chlorite and borax (Uner and Olgun, 2017), ammonium citrate and zinc nitrate (Park et al., 2003), aluminium chloride and aluminium sulphate (Aizat et al., 2019), ammonium formate for melamine-urea-formaldehyde resins (Čuk et al., 2011) and ammonium persulfate and ferrum (III) chloride if UF resins are used for plywood bonding (Bekhta et al., 2016).

As for the natural acids, attempts were made to use citric and oxalic acids as hardeners in crude state after the wood particles were blended with adhesive mixtures. The use of such hardeners for curing commercial UF resins resulted in a slight rise in the free formaldehyde content (to the upper limit of the E1 emission class). However, if oxalic acid was used neat or in combination with ammonium sulphate for curing low formaldehyde to urea molar ratio UF resin, produced particleboards had high values of internal bond (IB) with free formaldehyde values $\leq 4.5 \text{ mg}/100 \text{ g}$ oven dry board (Costa *et* al., 2014). The use of citric acid-sucrose mixtures as binders for particleboard production was also attempted. The results showed that although citric acid and sucrose mixtures have great potential as binders for particleboards, the final effect of their use is highly dependent on targeted board density and press temperature. Boards pressed at 200 °C with targeted density of 0.8 g/cm³ had values of mechanical (bending strength (MOR) and modulus of elasticity (MOR)) and physical properties (water absorption and swelling in thickness) in the range or above those minimum required by the applicable

standards (Widyorini *et al.*, 2016; Umemura *et al.*, 2013, 2015). As for the low density, when insulating particleboards were pressed using the same binder mixtures, the MOR and swelling in thickness values increased with increasing the board density, and boards with targeted density of 0.4 g/cm³ pressed by adding 15 % binder met the standards requirements (Liao *et al.*, 2016).

Given that our earlier work, in which we have examined the neat resin-catalyst systems (Španić *et al.*, 2017), showed that tartaric acid ($C_4H_6O_6$) could be successfully used as a part of hardener for UF resin curing, and taking into consideration the above mentioned results of other authors, in this paper the experimental particleboards were produced and their mechanical properties and free formaldehyde content were determined. Boards with nominal thickness of 15 mm were made using ammonium sulphate hardener, partially replaced with tartaric acid, with pressing temperature set at 175 °C and pressing time varying from 240 to 300 seconds.

2 MATERIALS AND METHODS 2. MATERIJALI I METODE

In this study, four series (8 boards in total) of three-layer particleboards sized $45 \times 37 \times 15$ (mm) were produced using industrial particles of various wood species and commercial urea-formaldehyde resin. Paraffin emulsion was used as hydrophobic agent and ammonium sulphate-based catalyst partially modified with tartaric acid (1 % addition) was used as hardener. Face and core particles, urea-formaldehyde resin, industrial grade ammonium sulphate and paraffin emulsion were obtained from Kronospan CRO Ltd. Industrial grade tartaric acid (L-(+)-tartaric acid) for oenological purposes was obtained from Begerow GmbH & Co. Deionised water used for catalyst preparation was ASTM type II, and prepared using TKA MicroMed system.

2.1 Particleboard production

2.1. Izrada ploča iverica

The moisture content for face layer and core layer particles was 7 % and 5 %, respectively, as determined gravimetrically. Such particles were used to make 16 mm thick particleboards with target density of 0.75 g/

| Panel series | Press temperature | Press pressure | Pressing time | Hardener type |
|--------------|----------------------|-------------------|------------------|----------------------------|
| Serija ploča | Temperatura prešanja | Tlak prešanja | Vrijeme prešanja | Vrsta katalizatora |
| | °C | N/mm ² | S | |
| А | 175 | 3.2 | 300 | neat $(NH_4)_2SO_4$ |
| В | 175 | 3.2 | 300 | $(NH_4)_2SO_4 + C_4H_6O_6$ |
| С | 175 | 3.2 | 270 | $(NH_4)_2SO_4 + C_4H_6O_6$ |
| D | 175 | 3.2 | 240 | $(NH_4)_2SO_4 + C_4H_6O_6$ |

Table 1 Experimental design for produced particleboards**Tablica 1.** Parametri za izradu eksperimentalnih ploča iverica

cm³. Panels were made by adding 11 % (face) and 8.5 % (core) of urea-formaldehyde adhesive with 66 % solid content, based on oven dry weight of particles. For the first series of panels (marked A), neat ammonium sulphate was used as hardener, while in other three series (marked B, C and D), the catalyst consisted of ammonium sulphate and tartaric acid. The hardener was added based on the solid content of the resin, 3 % being added for the core layer and 0.2 % for the face layer. In all series of particleboards, solid content of the catalyst was 20 %. In modified catalyst systems, 1 % (based on solid content of resin) of ammonium sulphate was replaced with the same amount of solid tartaric acid, in accordance with the findings of our prior work (Spanić et al., 2017). Paraffin emulsion solid content was 46 % and was added to face layer (3 %) and core layer (4 %), respectively, based on resin weight.

All series of panels were pressed at 175 $^{\circ}$ C and 3.2 N/mm² pressure, with pressing time and hardener used depending on the panel series (Table 1).

In each panel series, two boards were made and conditioned at 65 % relative humidity and 20 °C, before being sawn into test samples.

2.2 Particleboard testing

2.2. Ispitivanje ploča iverica

Prepared particleboards were tested in order to determine bending strength (MOR) and modulus of elasticity (MOE) according to EN 310:1993 and internal bond (IB) according to EN 319:1993. Mechanical properties were determined using a Schenck Trebel universal testing machine (model UPM 20T). The dimensions of the test samples were determined according to EN 325:1993 using an INSIZE digital calliper (model 1137-150; 0.01mm precision) and an INSIZE digital micrometre (model 3100-25; 0.001mm precision). Board density was determined according to EN 323:1993 and their moisture content using a Memmert laboratory drying oven (model UF 110 plus) according to EN 322:1993. The weight of the test specimens was determined using a Sartorius digital laboratory balance (model TE 612-L; 0.01g precision). Free formaldehyde content was determined according to EN 120:1992, using a Shimadzu UV-VIS spectrophotometer (model UV mini 1240). For each panel series and each property examined, 10 samples were prepared and tested. Free formaldehyde content was determined on one sample per board series.

Data obtained for each property examined was statistically analysed. The influence of partial replacement of ammonium sulphate hardener with tartaric acid on properties of particleboards was evaluated by analysis of variance (ANOVA). Tukey's HSD post hoc test was performed in order to identify which group (data for each property examined for each board series) was significantly different from other groups at 95 % confidence level. Statistical analysis was performed using Statistica Ver.13.3 software (Tibco Software Inc.).

3 RESULTS AND DISCUSSION 3. REZULTATI I RASPRAVA

The results of mechanical properties of experimentally produced particleboards are given in Table 2, namely their thickness, density and moisture content.

EN 312:2010 defines values of 0.35 N/mm², 11 N/mm² and 1600 N/mm² as minimum requirements for IB, MOR and MOE, respectively, for Type P2 particleboards (boards for interior fitments, including furniture; for use in dry conditions). The same standard permits the value of $\leq 8 \text{ mg}/100 \text{ g}$ oven dry board, for the free formaldehyde content (CH₂O). The results in Table 2 show that 1 % replacement of ammonium sulphate with tartaric acid resulted in only minor changes in mechanical properties, if the board pressing time stayed the same (300 s). This is also the case regarding the free formaldehyde, whose content is 6.49 mg/100 g oven dry board for boards from series A and 6.54 mg/100 g oven dry board for boards from series B (Figure 1). Both the boards from series A and B fulfil the minimum requirements, implying that tartaric acid has a positive effect on resin curing if the pressing time is not altered. However, this is not the case regarding the IB of boards from series C and D, which were pressed for 270 and 240 seconds, respectively. Although those values are lower, MOR and MOE values are still above the minimum required. The same is with the free formaldehyde content, which rises up to 7.6 mg/100 g oven dry board for boards from series C and then drops back to 6.62 mg/100 g oven dry board for boards from series D (Figure 1).

Relative increase of MOR and MOE values accompanied by the decrease of IB values of boards hot pressed for 270 and 240 seconds is common. That is due to the fact that the shorter press time influences the relationship between board density and strength, thus leading to higher densification of outer layers, which highly contributes to the increase of MOR and MOE values and decrease of IB values (Moslemi, 1974). More precisely, due to short press time, the heat transfer to inner layers was insufficient, causing improper

| Property | Panel series | N | Mean ± STD | Median | Min | Max |
|--|--------------|----|-----------------------------|--------|--------|--------|
| Svojstvo | Serija ploča | | | | | |
| | Α | 10 | 15.16±0.15 ^{ab} | 15.15 | 14.97 | 15.43 |
| Thislenses / dabling mm | В | 10 | 15.22±0.44 ^{ab} | 15.38 | 14.56 | 15.73 |
| Thickness / <i>debljina</i> , mm | С | 10 | 15.61±0.26ª | 15.42 | 15.31 | 15.96 |
| | D | 10 | 15.15±0.40 ^b | 14.97 | 14.71 | 15.91 |
| | Α | 10 | 0.75±0.04 ^{abc} | 0.76 | 0.66 | 0.79 |
| Density / gustoća, g/cm ³ | В | 10 | 0.71±0.03° | 0.71 | 0.65 | 0.75 |
| | С | 10 | 0.73±0.02ª | 0.73 | 0.70 | 0.78 |
| | D | 10 | 0.77±0.04 ^{ab} | 0.78 | 0.67 | 0.82 |
| | Α | 10 | 7.23±0.26ª | 7.25 | 6.76 | 7.59 |
| Maisture contant / and žni us da 0/ | В | 10 | 7.02±0.11ª | 7.02 | 6.87 | 7.22 |
| Moisture content / <i>sadržaj vode</i> , % | С | 10 | 7.21±0.17ª | 7.21 | 6.90 | 7.49 |
| | D | 10 | 7.17±0.15ª | 7.13 | 6.98 | 7.50 |
| | Α | 10 | 0.35±0.04ª | 0.34 | 0.27 | 0.39 |
| IB / vlačna čvrstoća okomito na površinu ploče, | В | 10 | 0.38±0.04ª | 0.40 | 0.31 | 0.45 |
| N/mm ² | С | 10 | 0.16±0.01 ^b | 0.17 | 0.14 | 0.18 |
| | D | 10 | 0.18±0.06 ^b | 0.17 | 0.04 | 0.28 |
| | А | 10 | 11.9±1.39 ^a | 11.8 | 9.7 | 14.1 |
| MOR (aquain a čunato ća N/mm² | В | 10 | 13.4±1.38 ^{ab} | 13.2 | 11.6 | 15.9 |
| <i>MOR / savojna čvrstoća</i> , N/mm ² | С | 10 | 13.9±1.83 ^{ab} | 14.1 | 11.2 | 16.7 |
| | D | 10 | 15.5±2.43 ^b | 15.3 | 11.7 | 19.0 |
| | А | 10 | 2423.8±232.02ª | 2451.3 | 2081.0 | 2699.6 |
| MOE / modul alastičnosti sausino čunstoćo N/mm² | В | 10 | 2503.7±256.97 ^{ab} | 2535.6 | 2129.0 | 2892.2 |
| MOE / modul elastičnosti savojne čvrstoće, N/mm ² | С | 10 | 2502.7±256.31ab | 2504.2 | 2092.7 | 2857.7 |
| | D | 10 | 2841.0±345.07b | 2881.6 | 2594.2 | 3087.9 |

| Table 2 Mechanical properties of experimentally produced particleboards | |
|---|--|
| Tablica 2. Mehanička svojstva ploča iverica izrađenih za eksperiment | |

* Means sharing the same superscript are not significantly different from each other (Tukey's HSD, p < 0.05)

* Srednje vrijednosti koje imaju istu slovnu oznaku međusobno se znatno ne razlikuju (Tukey's HSD, p < 0.05)

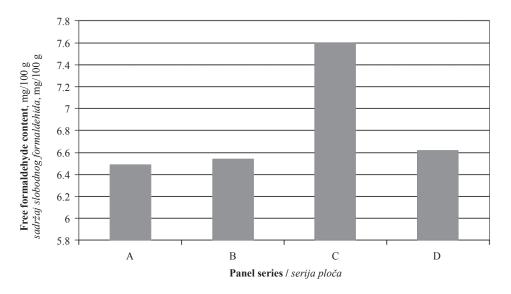


Figure 1 Free formaldehyde content of experimentally produced particleboards **Slika 1.** Sadržaj slobodnog formaldehida ploča iverica izrađenih za eksperiment

resin polymerization in the core layers. The slight rise of free formaldehyde content in case of boards from series C and D is also an indication of improper resin polymerization in inner layers.

As already mentioned, the mechanical properties of boards from second series (B) are only slightly affected by the addition of tartaric acid, if compared with the results obtained for the boards made using neat ammonium sulphate (series A). Such results are likely due to the hardener pKa (acid dissociation change) that shifts to lower values as the temperature of wood particle mat increases. With the increase of temperature, tartaric acid pKa changed, thus lowering the pH value of the catalyst system, which resulted in somewhat faster resin curing time. Faster curing consequently helped the development of *IB*, *MOR* and *MOE* values (Wang and Winistorfer, 2003) in case of boards from the second series (B). The results given in Table 2 reveal that there are no significant differences in moisture content between individual panel series. Small differences in terms of board thickness could be associated with unevenness of metal sheets on which the wet mats were formed. The density drop from 0.75 g/cm³ (series A) to 0.71 g/ cm³ (series B) and its rise in series C and D (to 0.73 g/ cm³ and 0.77 g/cm³, respectively) could be an indication that, in case of the use of tartaric acid, the catalytic mechanism is independent of the free formaldehyde (Costa *et al.*, 2014).

4 CONCLUSION 4. ZAKLJUČAK

This study showed that it is possible to use ammonium sulphate-based hardener partially replaced with tartaric acid for particleboard production. However, this is possible only if the panel press time is not too short (less than 300 s), as results showed that the IB, MOR and MOE values, as well as free formaldehyde content, are under the influence of set press time. The results also imply that the hardener system and consequently the board properties are influenced by the addition of tartaric acid (pKa values), leading to the conclusion that the particleboards could be produced using neat tartaric acid as hardener for UF resin. Still, this should be examined in further studies.

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