



## Attitude Control System Design NEUDOSE's PMAC system is comprised of a permanent magnet along the satellite's y axis, with hysteresis rods along the z and x axes. The main design constraints are: Pointing error, $\beta$ , must be < 60° 2. PMAC must be successful up to an initial angular velocity, $\omega = 5^{\circ}/s$ , on each axis Bar magnetic moment m < 0.51 A $\cdot$ m<sup>2</sup> Preliminary mounting of hysteresis rods along the satellite's x axis. The hysteresis rod housing will be mounted tot the bottom of the payload enclosure support tray.

Passive magnetic attitude control proved to be a simple solution to McMaster NEUDOSE's pointing requirements, after changing to a 2U CubeSat, with the new design requiring no power and occupying very little volume. CubeSatellite missions should consider passive attitude control systems when their of a passive system can decrease mission risks and allow for more freedom in designing a successful CubeSat mission.

### Acknowledgements

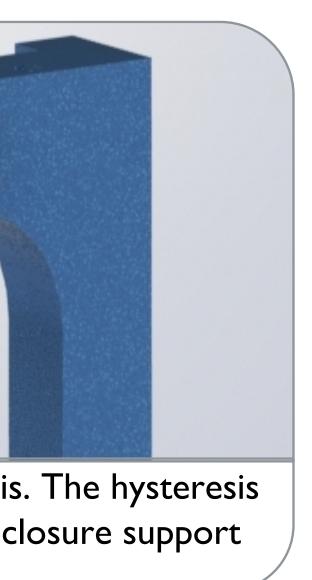
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# Passive Attitude Control to \*Alexander Barovier, Devan Wagner, Andrei Hanu\*\*, Eric Johnston, Soo Hyun Byun\*\*

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#### Motivation

McMaster NEUDOSE was initially a 3U CubeSat, which required an active ADCS. After some design alterations, NEUDOSE changed to a 2U CubeSat, which no longer had space or a need for an active ADCS. A passive magnetic attitude control system (PMAC) was chosen for the 2U design due to it's simplicity and small volume requirement.



#### Attitude Simulation

A simulation was developed using a combination of Matlab and STK, to model the PMAC system.

External Torque	Ma
Source	
Gravity Gradient	3.3
Aerodynamic	4.8
Solar Pressure	4.8
Eddy Current	6.7

Above is the worst case environmental disturbance torques simulated. These torques are calculated at each timestep as part of the attitude simulation, using input from STK. This simulation was used to run a variety of test cases, with varying hysteresis volumes, to determine their impact on the PMAC system's settling time and steady state error.

#### Conclusion

#### aximum Torque

 $3 \times 10^{-8} \text{ N} \cdot \text{m}$  $8 \times 10^{-8} \, \text{N} \cdot \text{m}$  $8 \times 10^{-10} \text{ N} \cdot \text{m}$  $7 \times 10^{-8} \text{ N} \cdot \text{m}$ 

Pictured below is a simulation of the PMAC system using  $2 \times 10^{-7} \text{m}^3$  of hysteresis material per axis, and a bar magnetic moment of 0.45  $\text{A} \cdot \text{m}^2$ .

This simulation/ also included the worst case initial angular velocities, showing the PMAC system can meet the mission's pointing goals.

Varying hysteresis volumes were simulated, and yielded the expected effect of decreasing settling times with increasing amount of hysteresis material.

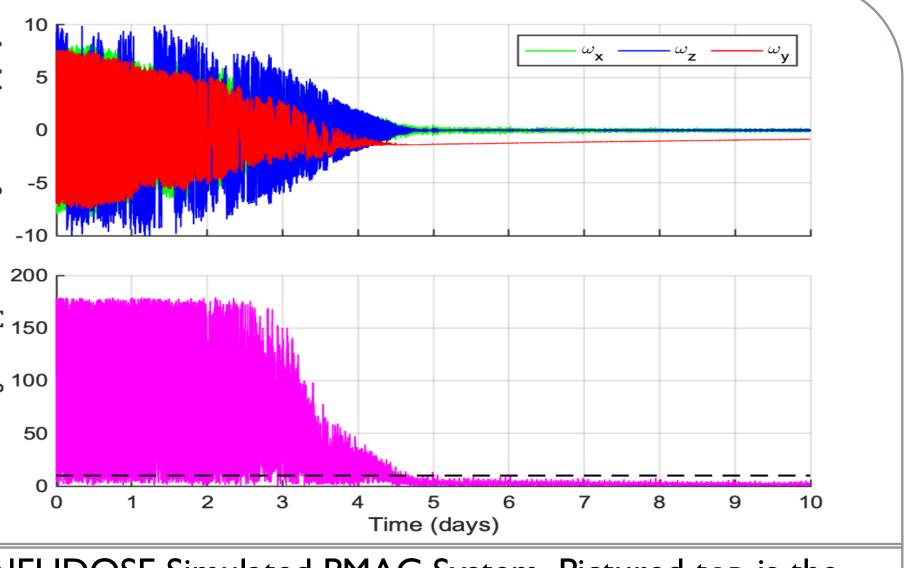
#### References

- D.T. Gerhardt. Small Satellite Passive Magnetic Attitude Control. PhD thesis, University of Colorado, 2014
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#### Results



NEUDOSE Simulated PMAC System. Pictured top is the satellite angular velocities. Pictured bottom is the pointing error