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# Transport, survival and modification of xenoliths and xenocrysts from source to surface

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**Abstract:** A wide variety of magmas entrain, transport and erupt mantle material in the form of xenoliths and xenocrysts. The host magmas are often low viscosity in nature and range from basalt to more esoteric compositions such as kimberlite, nephelinite and basanite. Here we focus on kimberlite magmas which are particularly successful at transporting deep mantle cargo to the surface, including economically important quantities of diamond. Collections of mantle-derived xenoliths and xenocrysts are critical to our understanding of the structure, stability, composition, thermal state, age, and origin of the lithosphere. However, they also inform on magma transport conditions. Through a series of scaled analogue experiments, we document the relative mechanical stability of olivine, garnet, orthopyroxene, clinopyroxene and diamond xenocrysts during magma ascent. Our experiments fluidized these mantle minerals at a constant gas flux for variable amounts of time approximating transport in a high velocity, turbulent, fluid-rich (supercritical fluid or gas, depending on depth) magma. The evolution of mineral surface features, morphology and grain size distributions is analyzed as a function of residence time. We show that on timescales consistent with magma ascent, each mantle mineral is subject to mechanical modification resulting in mass loss and reshaping (rounding) by grain size reduction and surface pitting. We further discuss the chemical consequences of producing fine particle chips that are highly susceptible to dissolution. Lastly, we utilize an empirical model that relates textural observations (e.g. impact pit size) on xenocrysts to differential

particle velocities. Our approach applied to natural kimberlitic olivine and garnet xenocrysts indicates differential velocities of  $\sim 4$  m s<sup>-1</sup> – the first direct estimate for velocity in an ascending kimberlite magma.

### 1. Introduction

Kimberlites are bodies of volcanic rock preserved at surface as shallow pipes, sheets, dykes and sills across the Earth's cratons (Brown and Valentine, 2013; Dawson, 1971; Russell et al., 2019; Sparks, 2013). Subaerial deposits such as lava and pyroclastic edifices also characterize kimberlite, but are rare due to their poor preservation potential (Brown et al., 2012; Brown and Valentine, 2013). These low viscosity, volatile rich magmas originate deep within the Earth, in excess of 150 km, and are proposed to ascend at anomalously high speeds estimated to be between 1 and 20 m s<sup>-1</sup> (Eggler, 1989; McGetchin et al., 1973; Russell et al., 2012; Sparks et al., 2006; Wilson and Head, 2007). Transit to the surface through the cratonic mantle lithosphere is attended by entrainment of mantlederived xenoliths and decompression-induced liberation of xenocrysts (Brett et al., 2015); all of which occur on timescales of hours to days (Sparks et al., 2006). The resulting rock, kimberlite, therefore comprises abundant (≤ 50% volume; Moss et al., 2010; Smith, 2008) mantle cargo, all encoded with information pertaining to the dynamics of kimberlite transport, ascent and eruption. However, natural samples are often pervasively altered post-emplacement and only limited deposits are fresh enough for quantitative insights to be drawn.

Kimberlite magmas ascend in fractures (dykes), facilitated by buoyancy arising from a critical

Kimberlite magmas ascend in fractures (dykes), facilitated by buoyancy arising from a critical density difference between the magma and surrounding country rock (Russell et al., 2012; Sparks, 2013; Sparks et al., 2006). During magma ascent, the overlying mantle is fractured due to overpressures at the crack-tip, leading to the entrainment of wall rocks as mantle xenoliths (Brett et al., 2015). Fast upward transport subjects xenoliths to rapid depressurization, causing their disaggregation and the subsequent release of xenocrysts into the turbulent, volatile-rich magma (Brett et al., 2015; Jones et al., 2019). Once entrained the mantle xenocrysts may be affected by: (1) chemical dissolution (Arndt et al., 2010; Kamenetsky et al., 2008; Pilbeam et al., 2013) potentially expressed as etch pits and embayments, and (2) mechanical modification (Arndt et al., 2010; Brett et al., 2015; Jones et al.,

2019, 2014) by 'attrition' (cf. Jones and Russell, 2018) expressed by grain rounding, breakage and pitting. Textural evidence for these processes is commonly preserved in the properties of kimberlite-hosted xenocrysts. Mechanical modification dominates the surface textures of many mantle xenocrysts within kimberlite, implying that it is particularly important during the later stages of ascent (Arndt et al., 2010; Jones et al., 2019).

Previous studies have proposed that beneath the dyke/crack tip there is a low viscosity, volatile-rich region comprising supercritical fluid and/or gas (depending on depth) that turbulently suspends high volume fractions of mantle cargo (Arndt et al., 2010; Brett et al., 2015; Russell et al., 2019). This is followed stratigraphically by a denser, melt-dominated region in the dyke tail (Brett et al., 2015). Mechanical attrition of the mantle cargo within these rapidly ascending (i.e. turbulent) magmas is expressed by reshaping (rounding) and resurfacing of xenoliths and xenocrysts (Arndt et al., 2010, 2006; Barton Jr and Gerya, 2003; Jones et al., 2019, 2014; Kurszlaukis and Barnett, 2003; Peltonen et al., 2002; Peterson and LeCheminant, 1993; Smith and Griffin, 2005). Transport-induced rounding is particularly evident in olivine xenocrysts which volumetrically dominate most kimberlites.

Here, we present a series of attrition experiments at scaled conditions relevant to kimberlite ascent for mantle-derived minerals typical of kimberlite cargo (olivine, garnet, orthopyroxene, clinopyroxene, diamond and mixtures thereof). The experiments involve suspending mantle minerals in a turbulent, gas fluidized state for prescribed amounts of time. Our experimental set-up is most relevant to the gas/supercritical fluid-rich (depth dependent) crack-tip environment where ideal conditions are met for sustained and energetic particle-particle interactions supporting attrition (e.g. Brett et al., 2015; Jones et al., 2019). Our experiments inform on the mechanical stability of each mineral and establish quantitative rates of mechanical breakdown (i.e. attrition) for each. We conclude by combining experimental data and observations on natural kimberlite samples to provide quantitative constraints on the timescales and velocities of kimberlite ascent.

### 2. Methods & Materials

## 2.1 Characterization of starting materials

Fresh (i.e. unaltered) minerals for this project were sourced from a variety of companies mostly specializing in abrasives or gemstone sales. Forsterite (olivine) sand derived from crushed dunite is from Ashwani Industrial Minerals Corp.; pyrope (garnet) sand is from Zhangjiakou Xuanhua Ju Hong Abrasion Resistant Material Distribution Co., Ltd.; chrome diopside (clinopyroxene) from Sovtube, an unaffiliated seller; and natural rough diamond sand from CDL FINESHINE. The clinopyroxene and orthopyroxene could only be obtained as large (i.e. >5 mm) crystals and were manually crushed using a corundum mortar and pestle. Before using the minerals for experimental purposes, all mineral sands were sieved to the desired, restricted grain size of 600-710 µm and washed using deionized water to remove any adhering fine particles. This size range was selected as it the largest grain size available for all minerals and is therefore the closest to those observed in the natural system. Photographs of representative mineral grains used in the experiments are shown in Figure S1.

The density of each mineral was calculated using an analytical balance to measure mass and a Micrometrics Accupyc II 1340 Helium pycnometer to measure volume. Three aliquots of each mineral sample were measured for mass and volume, then plotted as mass [g] against volume [cm³]. A linear regression was then fitted through the three data points and the origin, with the slope determining the density [g cm³] of the mineral (Table S1). Additionally, a number of grains were imaged using a Philips XL30 scanning electron microscope (SEM) in secondary electron mode with a 15-kV accelerating voltage and a 35  $\mu$ A beam current. Images were taken at various magnifications to document the overall morphology and the surfaces of the starting material prior to experimentation.

# 2.2 Attrition Experiments

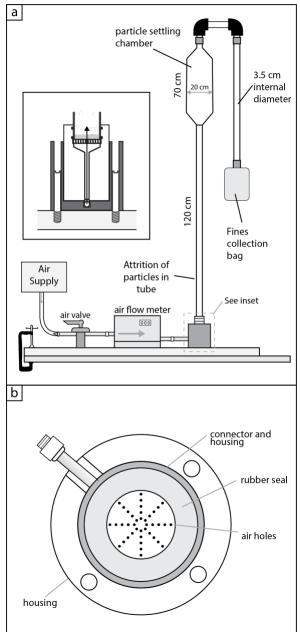
Experiments were performed at standard laboratory conditions wherein mineral grains (i.e. particles) were suspended in an air-jet. The apparatus (Figure 1) features a compressed air feed that passes through a calibrated FMA 5526 Omega gas flow meter (measuring gas flux, 105 L min<sup>-1</sup> for all experiments), and into to the base of a 3.5 cm diameter, 120 cm long vertical attrition tube. The gas enters the base of the tube via a distributor plate which features 41 evenly spaced holes (Figure 1). On top of the distributor plate 15 g of input mineral grains (initially 600-710 µm in diameter, termed

parent particles) are loaded to an initial bed height,  $h_0$ . The distributor plate ensures an equally distributed gas flux, which suspends particles effectively to height,  $h_p$  which was measured after the start of each experiment. As particle interactions occur within the attrition tube, fine particles are elutriated from the bed, passing up the attrition tube and into a 70 cm long, 20 cm diameter settling chamber which serves two primary purposes. Firstly, a lower gas flux in the settling chamber allows particles 23-135  $\mu$ m in diameter to be recycled back into the attrition tube which would otherwise leave the attrition process. Secondly, ultrafine particles (<23  $\mu$ m) can be elutriated from the settling chamber, passing through an elbow joint, down a tube and into a nylon filter bag (1  $\mu$ m mesh) where the fines are collected for processing. For each experiment, we recorded the initial bed height ( $h_0$ ) and the fluidized column height ( $h_p$ ). Particle concentration ( $\varphi$ ) is calculated from values of  $h_p$  relative to a model initial dense (pore space free) bed height ( $h_0$  calculated seconds) as:

$$\varphi = \frac{h_{0 calc}}{h_p} = \frac{m_0}{\pi r^2 \rho_p h_p} \tag{1}$$

where  $\rho_p$  [kg m<sup>-3</sup>] is the particle density,  $m_0$  [kg] is the input mass is particles and r [m] is the attrition tube radius.

The key modifications to this apparatus, relative to the previous work of Jones and Russell (2018) and Jones et al. (2019), is the addition of a settling chamber that allows re-entrainment of particles and the fines collection filter bag which ensures retention of the finest particles whist allowing free flow-through (i.e. no back pressure) of gas. Table S2 (online supplementary information), summarizes the experimental conditions and characterization performed for each experiment in this study.



**Figure 1:** Attrition apparatus used in this study. (a) Schematic diagram of apparatus with inset showing sample resting on the distributor plate to be fluidized by the gas jet (solid arrow). (b) A plan view of the distributor plate upon which the input sample is loaded.

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We used videography to study and quantify the nature of fluidization and particle interactions. We recorded 20 seconds of select experiments at 1,050 frames per second using a Chronos 1.4 high-speed camera; image collection began ~ two minutes after the gas flux was initiated. To ensure that individual particles could be manually tracked with accuracy, a Godox QT600II high speed flash strobe light was used to illuminate the experiment. For all filming the camera was positioned at a 50 cm horizontal distance from the attrition tube. We varied the camera's vertical position between the

different mineral experiments to ensure that film captured 50 - 90 % of the total column height. For each mineral type we tracked between 140 and 165 particles over 2-10 frames in a representative experiment. The dataset comprised ~140 particles tracked from the central region of the attrition tube and 30 particles from the margins. This ratio of tracked particles (centre *vs.* margins) is proportional to distribution of particles across the width of the tube; approximately 70% of the tube is occupied by particles moving upward within the central jet and 30% downwelling at the margins.

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#### 2.3 Post-experiment sample characterization

At the end of a prescribed time, the gas flow was switched off marking the end of the experiment and the apparatus was left for at least 1 hour to ensure fine particles had settled. At that point, the attrition apparatus was carefully disassembled and washed with deionized water over a standard stack of ASTM E11 mechanical sieves with a mesh size range of 125 µm to 600 µm and a collection pan below the 125 µm sieve. The sieves were then left to dry in a 70°C oven overnight. The following day the material was dry sieved and the contents of each sieve were weighed using an analytical balance ( $\pm 0.1$  mg). All material collected below the input parent size ( $600 - 710 \,\mu\text{m}$ ) represents particle sizes derived from the attrition process, which we term 'daughter' particles' herein. Grain size distributions of material caught in the pan (i.e. <125 µm) were measured by Laser Particle Size Analysis (LPSA). A Malvern Mastersizer 2000 laser diffraction device with a hydro 2000 Mu water dispersion module attached was used for LPSA in this study. The pump speed, absorption coefficient and refractive index were varied for each mineral (see Table S3). Each aliquot of sample added to the dispersion module was measured three times. To prevent particle aggregation, an ultrasonic pulse was applied for 2 seconds immediately before measurement. This process was repeated three times for a total of nine measurements. To obtain the final particle size distribution of the powder, the nine measurements were averaged for a mean grain size distribution. The experimental run products were also characterized for morphology and surface features using the SEM as reported above (cf. Section 2.1).

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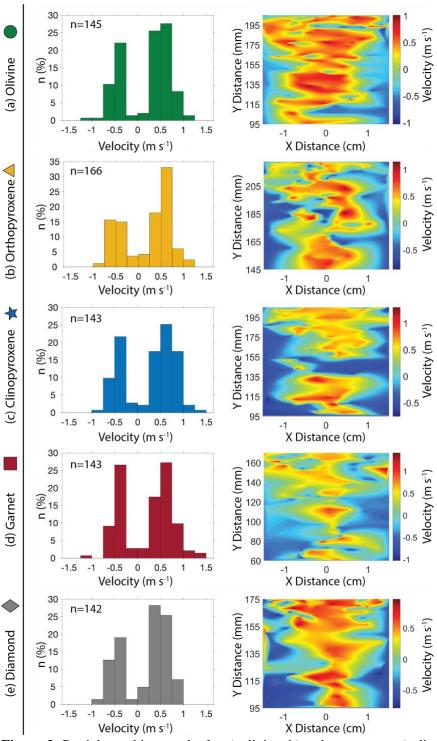
#### 3. Results and Analysis

Our experimental campaign consisted of a total of 43 experiments that fluidized an initial mass ( $m_0$ ) of 15 g of one of the minerals olivine, garnet, clinopyroxene, orthopyroxene, or diamond with a gas flux of 105 L min<sup>-1</sup>.

#### 3.1 Experimental Observations

Throughout all experiments, particles were distributed throughout the column and able to move freely relative to neighboring particles indicating a pneumatic flow regime (Bi and Grace, 1995; Jones et al., 2019). As would be expected, column height and the particle's density are negatively correlated whereas particle concentration and particle density are positively correlated. Specifically, at fixed gas flux (105 L min<sup>-1</sup>), orthopyroxene had the largest mean column height of  $218.0 \pm 2.7$ , followed by olivine, clinopyroxene, diamond and garnet with  $h_p$  values of  $209.4 \pm 5.3$  mm,  $209.3 \pm 3.9$ ,  $189.3 \pm 3.5$  and  $172.3 \pm 3.4$  mm respectively. This resulted in similar average particle concentrations of,  $0.02214 \pm 0.00028$ ,  $0.02295 \pm 0.00058$ ,  $0.02265 \pm 0.00043$ ,  $0.02348 \pm 0.00043$  and  $0.02327 \pm 0.00047$  (cf. Table S4).

Particle motion within the tube is not entirely random, the central region of the tube is dominated by an upward stream of relatively fast-moving particles, which contrasts the slower, predominantly downward, particle motion at the tube margins. The particle tracking results for each mineral are visualized in Figure 2. The histogram plots for each mineral show a bimodal distribution with one mode at a positive velocity and another mode at a negative velocity. The differential velocity  $(\Delta v)$  is approximated by taking the difference between the two velocity modes. This is 1.0 m s<sup>-1</sup> for all experiments apart from orthopyroxene and diamond, where  $\Delta v = 1.25$  m s<sup>-1</sup> and 0.75 m s<sup>-1</sup>, respectively. The velocity contours for each mineral show a central jet characterized by relatively large, positive velocities ('hot' colors) and negative velocities ('cold' colors) at the margins of the tube.



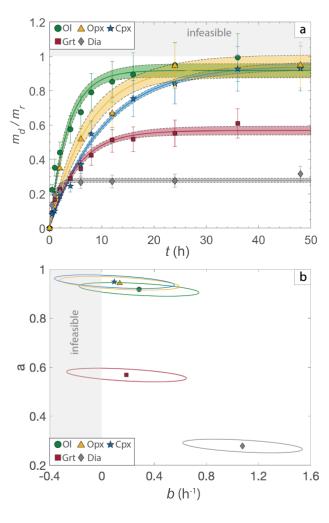
**Figure 2:** Particle tracking results for a) olivine, b) orthopyroxene, c) clinopyroxene, d) garnet, e) diamond. Left column: velocity values plotted as histograms with a 0.25 m s<sup>-1</sup> bin width. Right column: velocity distributions within the attrition tube where Y is the distance above the base of the tube and X is the distance across the tube. Accompanying videos can be found in the online supporting information and are labelled S1 through S5 corresponding to the panels (a) through (e) respectively.

#### 3.2 Fines production datasets and models

The production of daughter particles serves as an effective and simple measure to quantify the attrition process (Gwyn, 1969). The mass of daughter particles ( $m_d$ ) relative to the total mass recovered ( $m_r$ ), as a function of time t [h] for each mineral is shown in Figure 3. Each suite of experiments shows an initial, rapid rise in the production of daughter particles followed by a highly reduced rate ultimately forming a plateau and indicating little further attrition. In the literature this plateau is recognized as a stable state where production of daughter particles becomes limited with increased residence time (Jones et al., 2017; Knight et al., 2014). The time-dependent trends are well modelled by the empirical function:

$$\frac{m_d}{m_r} = a(1 - e^{-bt}) \tag{2}$$

(Jones et al., 2017). The two adjustable parameters, a and b, represent the infinite time attrition limit (i.e. the plateau) and the attrition rate constant [ $h^{-1}$ ] dictating the rate (i.e. initial slope) at which that limit is reached, respectively.



**Figure 3:** (a) Proportion of daughter products  $(m_d)$  normalized to the mass recovered  $(m_r)$  plotted against time for each mineral series. Error bars represent two relative standard deviations obtained from repeating experiment 1-F three times. Dashed lines bounding the coloured region for each mineral series are 95% confidence limits for the optimal fit (solid line). The accompanying mass loss data can be found in Table S5. (b) Model values of a, the infinite time limit of attrition and b, the attrition rate constant for all minerals. The ellipses represent 95% confidence envelopes on the optimal solution (i.e. a and b; Eq. 2). See Table 1 for fit parameters.

Mineral	а	<b>b</b> (h <sup>-1</sup> )	RMSE of fit
Olivine	0.9179	0.2840	0.0708
Orthopyroxene	0.9427	0.1355	0.0793
Clinopyroxene	0.9492	0.0955	0.0312
Garnet	0.5682	0.1884	0.0381
Diamond	0.2784	1.0770	0.0231

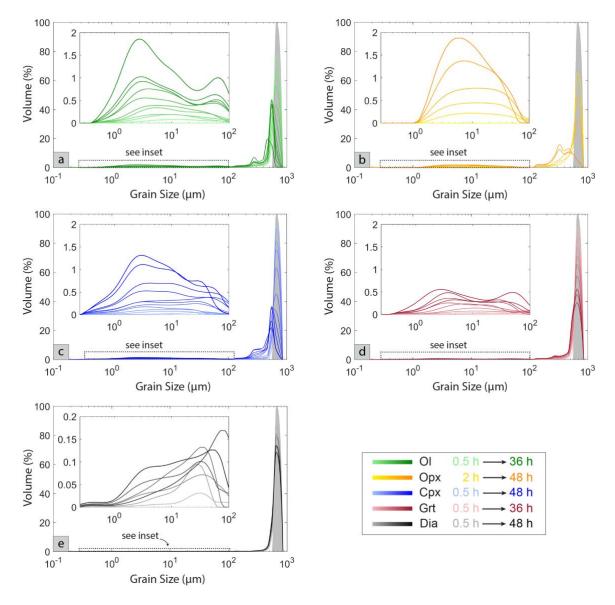
**Table 1:** Modelled fit parameters for Eq.2 for each mineral series. RMSE = Root Mean Square Error.

The model functions (Equation 2; Table 1) describe the experiment data well and the 95% confidence limits establish the range of a and b values that are consistent with the individual datasets and their measurement uncertainties (Figure 3). We distinguish two groups of minerals that form similar shaped trends (1) olivine, garnet and diamond; (2) clinopyroxene and orthopyroxene. For set (1), the attrition plateau is reached within 16 hours, but minerals are characterized by different attrition limits (a) and rates (b). Specifically, olivine has the highest a value of 0.9179 followed by garnet and diamond with values of 0.5682 and 0.2784 respectively. Diamond approaches its attrition limit the fastest followed by olivine and garnet. For set (2), the two pyroxene minerals, orthopyroxene and clinopyroxene, the attrition limit (i.e. a) is only just met within the experimental timescale, but this attrition limit is similar to olivine at the 95% confidence limits. The largest difference between sets (1) and (2) is in the rate at which the attrition limit is approached (b); the pyroxenes have slower rates (0.1355 h<sup>-1</sup> and 0.09554 h<sup>-1</sup>) relative to olivine (0.2840 h<sup>-1</sup>).

### 3.3 Total grain-size distributions

The experiments show a characteristic rapid initial drop in abundance of the parent grain population (grey mode; Figure 4) over short times. This decrease in the parent population is accompanied by the development of secondary grain-size modes representing the daughter products resulting from attrition. Interestingly, the grain size distributions for each mineral type feature a number of modes

and mode positions unique to that mineral. These characteristic distributions directly reflect the physical properties of each mineral.



**Figure 4:** Grain size distributions for each mineral series: (a) olivine; (b) orthopyroxene; (c) clinopyroxene; (d) garnet; (e) diamond. The input distribution is shaded in grey and presents the initial parent mode that evolves with time. The experiment run products are plotted as continuous lines which become darker with increasing experiment duration (see legend). Experiment durations for each mineral series are shown in Table S2. Insets show the finer daughter products measured by laser particle size analysis (LPSA), at an enlarged scale. For the reader's ease the diamond inset y-axis scale is an order of magnitude lower than the other plots to account for the low abundances of diamond daughter products.

The parent mode for olivine (Figure 4a) decreases from 655  $\mu$ m to 500  $\mu$ m with increased residence time up to 6 h. At the longest duration (36 h), the mode position changes again to ~ 463  $\mu$ m. After 6 h a secondary daughter mode at 275  $\mu$ m begins to form. Two finer modes below 100  $\mu$ m at 3

μm and 65 μm exist (see inset) for a total of four modes. Orthopyroxene shows an initial rapid decline in the parent mode which moves towards a position of 463 µm at 24 h. At 24 h a secondary mode at 328 µm becomes very noticeable (Figure 4b). Unlike the other minerals, orthopyroxene below 100 μm is characterized by a broad unimodal distribution centered on 6 μm for a total of three modes. Another peak may occur at 26 µm but is obscured by the breadth of the distribution. Clinopyroxene shows a parent population that shifts towards a peak position of 500 µm with increased residence time (Figure 4c). Development of a secondary mode at 275 µm is evident after 24 h. At long times (> 24 h) the parent mode broadens and is skewed to the finer grain sizes indicating possible emergence of another mode at 463 µm. Below 100 µm, two modes are identified, one at 3 µm and another at 31µm. The latter migrates towards 48 µm at long times (> 16 h). A total of four modes are identified for clinopyroxene. Garnet shows a declining parent peak which, unlike the other minerals, does not change grain-size position (Figure 4d). A secondary mode is observed at 275 µm starting at 16 h. Below 100 µm there exists a bimodal fines population with modes at 3 µm and 52 µm for a total of four modes. Lastly, diamond shows far less attrition than the other minerals. This is indicated by a persistent parent mode which, as seen in garnet, does not shift towards a smaller mode (Figure 4e). No secondary mode is observed and a relatively low volume of fines (<100 µm) is produced (note that the inset volume % scale has been lowered by an order of magnitude). Below 100 µm a bimodal population is observed, with one peak at 4 µm and another at 31µm shifting towards 78 µm at longer (24 h) residence times. A total of three modes are observed for diamond.

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### 3.4 Xenocryst morphologies and surfaces

Initially all mineral grains have angular morphologies, sharp edges and smooth surfaces.

Grains of pyroxene start with slightly higher aspect ratios (long axis: short axis) due to their inherent cleavage. With increased residence times all parent mineral grains transition towards rounded morphologies with micro-rough surfaces (Figure 5). In general, morphological changes to the parent particles are most profound in the first two hours of attrition, where particles rapidly lose asperities and the overall morphologies round. Further changes in particle shape slow as residence time increases.

Olivine undergoes the most efficient modification expressed by highly rounded grain morphologies and rough surfaces. Orthopyroxene and clinopyroxene show distinct cleavage-controlled disruption with planar breakage surfaces resulting in high aspect ratio products (Figure 5). These higher aspect ratios might make pyroxenes more susceptible to further attrition. Garnet shows conchoidal fracture and a morphology similar to olivine after long (≥ 12 h) residence times. Both minerals evolve to aspect ratios close to 1, however, garnet grain surfaces sometimes show less pitting relative to olivine. The diamond input particles (i.e. 0 h) show perfectly straight and sharp edges and flawless surfaces controlled by the perfect cleavage. The rounding and surface modification of diamond is much less than the other minerals, yet they still round and become pitted.

Higher magnification images of milled grains (Figure 5) show a range of surface features from small scale ( $<20~\mu m$ ) surface depressions resulting from lower energy, more frequent collisions to larger scale ( $>100~\mu m$ ) impact features resulting from higher energy collisions. The nature of the impact features varies by mineral type and, to an extent, is controlled by cleavage. Olivine and garnet have impact depressions and excavations that are hemispherical in shape, have a smooth interior surface, and are randomly oriented. By contrast, orthopyroxene, clinopyroxene and diamond show a higher degree of flaking and layering with impact pits appearing more elongated. Flaking at, and beneath, the exterior surface is not restricted to cleavage and is also observed, although less frequently, in both olivine and garnet. Other authors have identified these subsurface textures and flaky surfaces as a stress release mechanism in response to either decompression or heating (Campbell et al., 2013; Jones et al., 2014; Little et al., 2017). Furthermore, subsurface layering/flaking has also been documented in natural diamonds and interpreted as brittle fracturing during both magma transport and post emplacement (Win et al., 2001).

**Figure 5:** SEM images (in secondary electron mode) of representative parent particle morphology and surface features at select experiment durations. Rows represent different minerals and columns denote experiment duration. White scale bars denote 300  $\mu$ m for the morphology images and 100  $\mu$ m for the surface images. Further imagery can be found in Figure S2.

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## 4. Discussion

## 4.1 Relating experiments to nature

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**Figure 6:** Scanning electron microscope images of the morphology and surface features of xenocrysts from Diavik A154N coherent kimberlite taken in secondary electron mode. Top row shows rounded shapes of clinopyroxene, garnet and olivine mineral grains. Surfaces of these minerals are rough (middle row) and, in detail, are micro-chipped and flaked (bottom row).

To compare the products of our experiments to natural samples, xenocrysts were analysed from the Diavik kimberlite deposit located in the Northwest Territories, Canada, part of an economic ore body within the Lac de Gras kimberlite field. Specifically, clinopyroxene, garnet and olivine grains from coherent kimberlite of the A154N pipe (~650 m drill depth) were carefully extracted and imaged under the SEM (Figure 6). First, we used a diamond drill tip to extract an area of groundmass encasing the grain. Then the grains were carefully rinsed under water to remove the attached groundmass.

Images of xenocrysts recovered from natural samples of kimberlite show a remarkable resemblance to the experiment products (Figure 6 vs. 5). The kimberlitic xenocrysts display rounded morphologies and rough surfaces dominated by impact pits. The creation of surface textures in kimberlite can broadly be divided into 'chemical' and 'mechanical' processes (Jones et al., 2019, 2014). Chemical textures can originate from either magmatic melt and/or fluid dissolution or

crystallization (Fedortchouk, 2019; Giuliani, 2018; Kamenetsky et al., 2008; Pilbeam et al., 2013) whereas mechanical textures originate from attrition driven by particle-particle collisions (Arndt et al., 2010, 2006; Brett et al., 2015; Jones et al., 2019, 2014; Jones and Russell, 2018). A comparison of features resulting from these contrasting modes of surface modification are illustrated in Figure S3. Cavities formed by chemical etching appear strongly controlled by crystallography, having sharp edges and regular geometry (Figure S3). In contrast, impact pits have convex outlines and hemispherical morphologies (Figure S3). Importantly the surface features observed on natural kimberlite xenocrysts (Figure 6 and S3) are dominantly mechanical in nature and thus, at a minimum, mechanical processes dominate during the final stages (i.e. < 100 km) of ascent (Arndt et al., 2010; Brett et al., 2015; Jones et al., 2019, 2014; Jones and Russell, 2018).

Mechanical modification, or attrition, creates new grain size populations and surface textures by both fragmentation and abrasion (e.g. Bemrose and Bridgwater, 1987). Fragmentation is a high-energy process resulting in wholesale breakage of the parent particles often producing a small number of similarly sized daughter particles (e.g. Dufek et al., 2012; Jones et al., 2017; Jones and Russell, 2017; King, 2001). Sometimes fragmentation can occur through the incremental breakage of particles as expressed in the olivine experiments by the appearance of a secondary daughter mode at 275 μm after 6 h (Bonfils et al., 2016). Abrasion is a lower energy process generating a large number of small chips through the rounding of parent particles (e.g. Jones et al., 2016; King, 2001; Kueppers et al., 2012; Manga et al., 2011). Fragmentation processes operating on kimberlite xenocrysts have been discussed in detail by Jones et al. (2019). They showed that fragmentation occurs at, or above, a critical impact velocity. For olivine, garnet and diamond parent particles the critical fragmentation velocities are 0.54, 0.96 and 1.2 m s<sup>-1</sup> respectively.

The average differential velocities (i.e. impact velocity) in each experiment are ~1.0 m s<sup>-1</sup> supporting fragmentation of olivine and garnet, whereas fragmentation of diamond should be rare or unlikely. This is in excellent agreement with our grain size distributions (Figure 4) which showed an intermediate daughter (fragmentation) mode for both olivine and garnet, but not for diamond. A lack of literature values for fracture surface energies for diopside and enstatite precluded calculation of their critical fragmentation velocities (Table S1). However, their relatively weak physical properties

(Table S1) imply that the intermediate peaks observed in the grain size distributions result from fragmentation. Abrasion processes will be discussed further in Section 4.3.

When ascending in a multiphase mixture (i.e. not monomineralic), we hypothesize that the minerals with cleavage, most importantly orthopyroxene, will experience a relatively higher rate of attrition. The high surface area to volume ratios of these fine-grained attrition products of orthopyroxene (Figure 5) would be particularly susceptible to chemical assimilation by the melt (Mitchell, 1986; Mitchell et al., 2019) thereby changing melt composition, decreasing CO<sub>2</sub> solubility and increasing the potential for assimilation fueled buoyant ascent driven by CO<sub>2</sub> fluid exsolution (e.g. Russell et al., 2012; 2019). This creates a positive feedback cycle in which CO<sub>2</sub> exsolution increases magma ascent velocity, leading to more breakage and assimilation, continually supporting turbulent ascent. A corollary of assimilation is that a limited record of attrition processes, particularly the production of daughter fragments, will be preserved in the deposits.

#### 4.2 Transport duration and velocity of kimberlite ascent

Kimberlite magmas have been ascribed higher than average ascent rates relative to other mafic magmas (e.g. Eggler, 1989; Sparks et al., 2006; Wilson and Head, 2007; Russell et al., 2012). The rapid ascent (10's of m s<sup>-1</sup>) of kimberlite is a concept that has been investigated by many authors (Brett et al., 2015; Eggler, 1989; Jones et al., 2019, 2014; Jones and Russell, 2018; Kavanagh and Sparks, 2009; McGetchin et al., 1973; Russell et al., 2019, 2012; Sparks et al., 2006; Sparks, 2013; Wilson and Head, 2007). However, the dynamics remain a highly debated topic. Specifically, the timescales and velocities associated with magma ascent are poorly constrained; velocity estimates range from 1-20 m s<sup>-1</sup> (Sparks et al., 2006; Wilson and Head, 2007) resulting in transport timescales of days to hours.

Our experiments are shown to be correctly scaled for the natural system, in that, they fall within the same dynamical regime (e.g. turbulent flow) and dimensionless space best estimated for kimberlite magmas. Flow regimes are quantified by using the Reynolds number (Re) and specifically for kimberlite ( $Re_k$ ) is expressed as:

$$Re_{k} = \frac{Dv\rho}{u}$$
 [3]

- where D [m] is the dyke width, v [m s<sup>-1</sup>] is the velocity of the ascending magma,  $\rho$  [kg m<sup>-3</sup>] is the bulk
- density and  $\mu$  [Pa s] is the bulk viscosity of the three-phase fluidized mixture (melt, crystals,
- volatiles). The associated range of values of  $Re_k$  for kimberlite is ~  $10^2 10^6$  (see Table S6).
- Similarly, the Reynolds number of the flow in our experiments (Re<sub>exp</sub>) is given by:

$$Re_{exp} = \frac{Lv^*\rho^*}{\mu^*}$$
 [4]

- where L is the attrition tube internal diameter [m],  $v^*$  [m s<sup>-1</sup>] is the bulk velocity [m s<sup>-1</sup>],  $\rho^*$  is the bulk
- density [kg m<sup>-3</sup>] and  $\mu^*$  [Pa s] is the bulk viscosity. We adopt a mixture-based approach (Weit et al.,
- 387 2018) for calculation of bulk (denoted by the \* superscript) velocity, density and viscosity of the
- fluidized mixture of gas and particles. The bulk velocity  $(v^*)$  is given by:

$$v^* = \varphi v_p + (1 - \varphi) v_q \tag{5}$$

- where  $\varphi$  is the particle concentration,  $v_p$  [m s<sup>-1</sup>] is the average absolute particle velocity, recorded by
- high-speed videography and  $v_g$  [m s<sup>-1</sup>] is the superficial gas velocity. The bulk density (solid + gas) of
- 391 the mixture  $(\rho^*)$  is given by:

$$\rho^* = \varphi \rho_p + (1 - \varphi)\rho_q \tag{6}$$

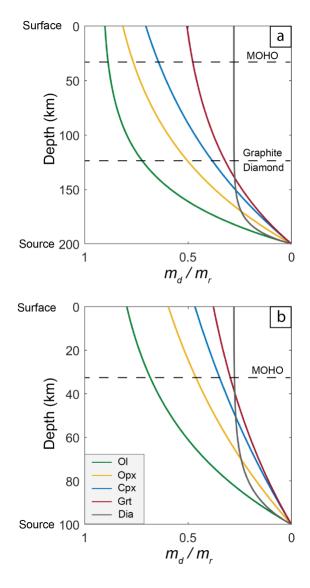
- where  $\rho_p$  [kg m<sup>-3</sup>] is the particle density and  $\rho_g$  [kg m<sup>-3</sup>] is the gas density. Lastly, the bulk viscosity
- 393  $(\mu^*)$  of the two-phase mixture is given by (Mader et al., 2013):

$$\mu^* = \mu_g (1 + \frac{5}{2}\varphi) \tag{7}$$

- where  $\mu_g$  [Pa s] is the gas viscosity. The parameters (i.e.  $\varphi$ ,  $\rho_p$ ,  $\nu_p$ ) vary for experiments using different
- 395 minerals and, thus, Re<sub>exp</sub> will vary slightly. For each mineral the calculated values of Re<sub>exp</sub> are well
- within the range of Re<sub>k</sub> values expected for kimberlite transport (i.e.  $\sim 10^2 10^6$ ): olivine (2.46 × 10<sup>5</sup>),
- orthopyroxene (2.37  $\times$  10<sup>5</sup>), clinopyroxene (2.47  $\times$  10<sup>5</sup>), garnet (2.98  $\times$  10<sup>5</sup>), and diamond (2.71  $\times$
- $398 10^5$ ).
- Equating Re<sub>k</sub> and Re<sub>exp</sub> for each mineral experiment series and rearranging yields the velocity
- of the kimberlite magma:  $v = \text{Re}_{\text{exp}} \mu / \rho D$ . For example, a 1.5 m wide dyke containing a magma
- with bulk density ( $\rho$ ) of 2100 kg m<sup>-3</sup> and a viscosity ( $\mu$ ) of 0.05 Pa s suggests corresponding velocities

for the olivine, orthopyroxene, clinopyroxene, garnet and diamond experiments of 3.91, 3.77, 3.91, 4.74 and 4.31 m s<sup>-1</sup>, respectively. To relate the model attrition rates (cf. Figure 3) to kimberlite ascent, the time axis is converted to distance using the characteristic velocities estimated above (Figure 7). The resulting curves now show attrition-related mass loss as a function of transport distance once the kimberlite magma is in a fluidized, turbulent state. We note that the exact distances will vary upon changing the assumed kimberlite dyke width, density and viscosity, however broad insights can be drawn.

At the transport conditions described above, all minerals, except diamond, suffer continual mass loss over 200 km of transport (Fig. 7a). Over this distance olivine shows the largest magnitude of mass loss and therefore serves as the best mineral to document the transport distance in a vigorous, turbulent state. Milling of olivine is highly sensitive to transport distance relative to the other mantle minerals investigated especially over short (< 50 km) distances, thus is the best mineral to resolve short transport distances (Fig. 7b). Diamond reaches the plateau faster than all other minerals mainly because, after  $\sim$ 30 km of transport, diamond ceases to break down at a measurable rate. The mechanical modification of diamond, therefore, can only be used to discriminate between short ( $\lesssim$  30 km) and long  $\gtrsim$  30 km) transport distances. These mass loss relationships are also dependent on the gas flux and mass input used in the experiments (Jones et al., 2019). This means that in application of these models to the ascending kimberlite dyke, the choice of particle concentrations and energy (velocity) needs to be chosen with caution.



**Figure 7:** Mineral series attrition curves where the x-axis is converted to distance using calculated ascent velocities. (a) Vigorous, high Re ascent (onset of attrition) begins at the source depth of 200 km. (b) Fluidization begins at a depth of 100 km. The Mohorovičić discontinuity (MOHO) and the top of the diamond window have been marked for reference.

#### 4.3 Impact pits on xenocrysts record transport velocities

Surface textures on xenoliths and xenocrysts (e.g., impact pits, striae, flaking) entrained by low viscosity magmas have been long been recognised as hallmarks of abrasion processes (Arndt et al., 2010; Jones et al., 2014; Jones and Russell, 2018; Kurszlaukis and Barnett, 2003; Peltonen et al., 2002). These mechanical processes are thought to occur at the volatile-rich dyke head under turbulent flow conditions (e.g., Brett et al., 2015) – the same conditions that our experiments are scaled for (Figure 8a). Here we use surface features on natural and experimental xenocrysts, especially the

impact pits, to characterize the environment and to quantify internal velocities within the magmafilled dyke during transport (Figure 8a).

Abrasion is a localized stress release mechanism and can be divided into surface wear and chipping (Boerefijn et al., 2007; Ghadiri and Zhang, 2002). Surface wear takes place at the micron scale, releasing ultra-fine particles and is associated with plastic deformation and shear stress at the surface of the grain (Hutchings, 1993). In the case of chipping, a fracture propagates from the site of impact, extending laterally and curving to towards the surface (Ghadiri and Zhang, 2002). This produces chips, often larger in size than those produced by surface wear. Our abrasion products typically show a bimodal distribution (insets; Figure 4), in which the coarser mode is produced by chipping exclusively and the finer mode can be produced by both chipping and surface wear, although likely dominated by the latter.

Surface abrasive wear of materials is commonly linked to hardness (Archard, 1953; Hutchings, 1993). The model proposed by Archard (1953) relates the extent of breakage by surface wear ( $\zeta_{wear}$ ) to the normal compressive force acting on the particle (F [mN]), the sliding distance ( $\Delta$ s [m]) and the material hardness (H [Pa]):

$$\zeta_{wear} = \alpha_w \frac{F\Delta s}{H}$$
 [8]

where  $\alpha_w$  [m<sup>-3</sup>] is a material-dependent proportionality factor. In kimberlite magmas, we would expect the harder minerals (e.g., diamond) to be less prone to surface wear relative to, for example, olivine (Table S1). The extent of breakage by chipping ( $\zeta_{chip}$ ) has been described by Zhang and Ghadiri (2002):

$$\zeta_{chip} = \alpha_c \frac{H}{K_c^2} \rho_p v_i^2 d_p$$
 [9]

where  $K_c$  [Pa m<sup>-0.5</sup>] is the fracture toughness,  $\rho_p$  [kg m<sup>-3</sup>] is the particle density,  $v_i$  [m s<sup>-1</sup>] the impact velocity and  $d_p$  [µm] is the particle diameter. The variable  $\alpha_c$  [kg m<sup>-0.5</sup> s<sup>2</sup>] is a material-dependent proportionality factor. The relationship is strongly dependent on the brittleness factor (Ghadiri and Zhang, 2002; Zhang and Ghadiri, 2002), a ratio of the hardness to the fracture toughness ( $H K_c$ <sup>-2</sup>). This implies that, in kimberlite, more brittle materials (e.g. diamond, garnet; Table S1) are more prone

to chipping. Equations 8 and 9 explain the relative peak sizes (cf. Figure 4) of the abrasion products ( $<100~\mu m$ ). Surface wear is limited to the finer mode ( $<20~\mu m$ ) and chipping contributes to both the coarser mode ( $80-100~\mu m$ ) and the finer mode.

Impact pit geometries produced by chipping have been related to the impact velocity (Ghadiri and Zhang, 2002; Zhang and Ghadiri, 2002):

$$i = k l v_i^{\frac{1}{2}} \left(\frac{\rho_p}{H}\right)^{1/4} \tag{10}$$

where i [m] is the impact pit diameter, k is a proportionality constant and l [m] is the particle diameter. Equation 10 assumes hemispherical impact geometry and an equant particle morphology. In natural kimberlite xenocrysts and in our experimental run products, surfaces of olivine and garnet grains exhibit hemispherical impact pits (cf. Jones et al., 2014). Twenty pit-diameters were measured on both olivine and garnet grains collected from short (2h), intermediate (12h) and long duration (36h) experiments yielding a total of 60 measurements per mineral (Table S7). These pit measurements were then used in conjunction with our well-constrained experimental data,  $v_i = 1 \text{ m s}^{-1}$  (differential particle velocities; Fig. 3) and modal grain sizes from Fig. 4 to fit for the corresponding proportionality constants (k) for olivine and garnet: 0.62 ( $1\sigma = 0.170$ ) and 0.46 ( $1\sigma = 0.117$ ), respectively.

Equation 10 can be rearranged to solve for impact velocity from measurements of impact pits on natural kimberlite xenocrysts using our experimentally derived proportionality constants:

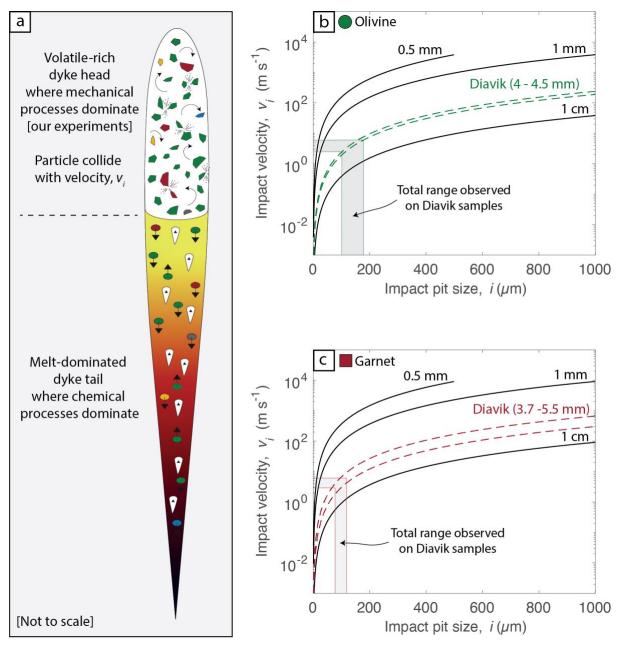
$$v_i = \left(\frac{i}{kl\left(\frac{\rho_p}{H}\right)^{1/4}}\right)^2 \tag{11}$$

This provides a valuable quantitative tool to directly relate textures observed on natural kimberlite xenocrysts to their differential velocities within the ascending magma. Furthermore, our approach is clearly portable to other systems where impact pits are preserved on magma-transported solids.

As an illustration of the method, two olivine grains and two garnet grains from Diavik A154N coherent kimberlite were carefully extracted and had their impact pits measured (Figure S4).

Measurements (n = 16) on the two olivine grains ( $k_{olivine} = 0.62$ ) corresponds to impact velocities in the

range of  $2.6 - 6.0 \text{ m s}^{-1}$  and  $2.5 - 5.0 \text{ m s}^{-1}$  (Figure 8b). Similarly, measurements (n = 11) on the two garnet grains ( $k_{garnet} = 0.46$ ) corresponds to impact velocities of  $2.9 - 4.2 \text{ m s}^{-1}$  and  $4.0 - 6.2 \text{ m s}^{-1}$  (Figure 8c). These velocities obtained independently from olivine and garnet xenocrysts hosted in coherent kimberlite show remarkable agreement. These impact velocities of ~4 m s<sup>-1</sup> are in excellent agreement with kimberlite dyke ascent models (e.g. Sparks et al., 2006). However, it is important to note that these velocities are subject to coupling between the xenocryst and the ascending magma. Furthermore, the internal flow velocity within the dyke is not necessarily the same as the dyke propagation velocity (Kavanagh et al., 2018).



**Figure 8:** (a) Schematic model diagram of the ascending dyke after Brett et al., (2015) and Russell et al., (2019). Model relationships between impact velocity and pit size for different size grains of (b) olivine and (c) garnet using k values of 0.62 and 0.46 respectively. Pit sizes were measured for two grains of olivine and two grains of garnet from the Diavik A154N pipe are shown by the dashed curves (with the grain size listed). The total range of impact pit sizes and the corresponding, calculated impact velocities are shown by the grey shaded regions.

### 5. Conclusions

A diverse range of magmas erupt carrying abundant mantle xenolithic cargo in the form of xenoliths and xenocrysts. The common xenolith-bearing magma types include alkaline basalt, basanite, nephelinite and, especially, lamprophyre and kimberlites. These magmas sample mantle material at

depth from the base of the mantle lithosphere to the Moho. The successful entrainment and transport of the dense mantle cargo is likely indicative of magmas fluidized by supercritical fluids or gas (depending on depth) and high ascent velocities capable of turbulent flow. Where this environment is sustained it creates the ideal environment for mechanical modification (i.e. attrition) of the solid cargo.

In this study we showed that all mantle xenocrysts are susceptible to mechanical modification on the timescales expected for kimberlite transport. The different mantle minerals are variably susceptible to mechanical modification with olivine breaking down at the fastest rate and diamond the slowest. With further study, xenocryst mass loss could be inverted to better constrain source melt compositions. Lastly, we develop an empirical model to relate the impact pits observed on both our experimental products and natural kimberlitic xenocrysts to the differential velocities of xenocrysts during transport. Applying this concept to garnet and olivine xenocrysts extracted from samples of coherent kimberlite we independently arrive at xenocryst velocities of ~4 m s<sup>-1</sup>, thereby providing a direct estimate of transport velocity for these enigmatic cargo-laden magmas. The concept of converting impact pits preserved on magma-transported solids is clearly portable to other systems.

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