

# A Microelectrode-Cell Sensor Model for Real Time Monitoring

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**Abstract--** In this paper the application of a cell-microelectrode model to cell biometry experiments is proposed, using the cell-electrode area overlap as main parameter. The model can be applied to cell size identification, cell count, and their extension to cell growth and dosimetry protocols. Experimental results using AA8 cell line are presented, obtaining promising results.

**Keywords-** Microelectrode; ECIS; bio-impedance; impedance sensor; cell culture; dosimetry.

## I. INTRODUCTION

Many biological parameters and processes can be sensed and monitored using its impedance as marker [1-5], with the advantage of being a non-invasive and relatively cheap technique. Cell growth and activity, changes in cell composition and shape, or in cell location are examples of how processes can be detected with microelectrode-cell impedance sensors [6-9]. Among Impedance Spectroscopy (IS) techniques, Electrical Cell-substrate Impedance Spectroscopy (ECIS) [7,8], based on two-electrode setups, allows the measure of cell-culture impedances and the definition of the biological nature (material, internal activity, motility and size) of a kind of cell and its relationship with the environment [11]. One of the drawbacks of ECIS technique is the need of efficient models to decode the full system electrical performance composed by the electrodes, medium and cells. Several works have been developed in this field. In [8], magnitude and phase impedance are deduced from electric field equation solution at the cell-electrode interface, giving a three parameter based model.  $h$ , the cell-electrode distance,  $R_b$ , cell-to-cell barrier resistance and  $r_{cell}$ , cell radius. In [9,10], finite element simulation (FEM) are executed to solve electrical field considering the whole structure. This method gives one parameter model ( $R_{gap}$ ) to describe the gap or cell-electrode region resistance. In both, the model considers cells are in confluent phase [7] or a fixed area over the electrode [9]. The latest was extended in [10] to several cell sizes, allowing to define the cell-electrode covered area as the main model parameter. In this work is considered a model extension of  $R_{gap}$  based model, to incorporate the variable cell-microelectrode area overlap [10]. Impedance sensor sensitivity curves based on the cell size and density will be presented and applied to measure the growth-tax in cell-cultures and to describe cell toxicity experiments.

In this paper, section II resumes the electrode solution model for cell-electrode characterization. The process to extract practical models is included at section III, illustrating the simulations on a simplified system leading to cell size

detection. Section IV relies on real time cell culture monitoring and its application to dosimetry experiments. Conclusions will be highlighted at section V.

## II. ELECTRODE-ELECTROLYTE MODEL

The impedance of electrodes in ionic liquids has been rather extensively investigated. An excellent review can be found at [6]. The main components describing the electrical performance of an electrode metal inside a solution are four: the double layer capacitance,  $C_1$ , the current flowing through the electrified interface will encounter a resistance  $R_{ct}$  caused by the electron transfer at the electrode surface and Warburg impedance  $Z_w$  due to limited mass diffusion from the electrode surface to the solution. The electron transfer resistance  $R_{ct}$  is in series with the mass diffusion limited impedance  $Z_w$ . As the current spreads out to the bulk solution, the electrode has a solution conductivity determined by series resistance, represented as spreading resistance  $R_s$  in the equivalent circuit. These four parameters depend on technology, medium and geometry.

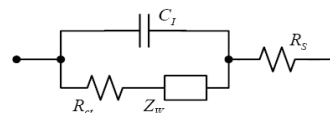


Figure 1. Equivalent circuit of electrode-solution interface.  $C_1$  is the double layer capacitance. Faradic impedance includes  $Z_w$ , the Warburg impedance and  $R_{ct}$ , the charge-transfer resistance.  $R_s$  is the spreading resistance.

## III. CELL-ELECTRODE MODEL

The Fig. 2 illustrates a two-electrode impedance sensor useful for ECIS technique:  $e_1$  is the sensing electrode and  $e_2$  the reference one. Electrodes can be manufactured in CMOS process with metal layers [9] or using post-processing steps [13]. The cell location and size on  $e_1$  top must be detected.

The model in Fig. 3 considers the sensing surface of  $e_1$  could be total or partially filled by cells. For the two-electrode sensor in Fig. 2,  $e_1$  is the sensing area  $A$ ,  $Z(\omega)$  is the impedance by unit area of the empty electrode (without cells on top). When  $e_1$  is partially covered by cells in a surface  $A_c$ ,  $Z(\omega)/(A-A_c)$  is the electrode impedance associated to non-covered area by cells, and  $Z(\omega)/A_c$  the impedance of the covered area.  $R_{gap}$  models the current flowing laterally in the electrode-cell interface, which depends on the electrode-cell distance at the interface (in the range of 15-150nm).  $R_s$  is the spreading resistance through the conductive solution. For an empty electrode, the impedance model  $Z(\omega)$  is represented by the circuit in Fig. 1. It has been considered for  $e_2$  the model in Fig 3a, not covered by cells. The  $e_2$  electrode is commonly large

and ground connected, being its resistance small enough to be rejected. Figure 4 represents the impedance magnitude,  $Z_c$ , for the sensor system in Fig. 2, considering that  $e_1$  could be either empty, partially or totally covered by cells. The parameter  $ff$ , called *fill factor*, can be zero for  $A_c=0$  ( $e_1$  electrode empty), and 1 for  $A_c=A$  ( $e_1$  electrode full). It is defined  $Z_c(ff=0)=Z_{nc}$  as the impedance magnitude of the sensor without cells.

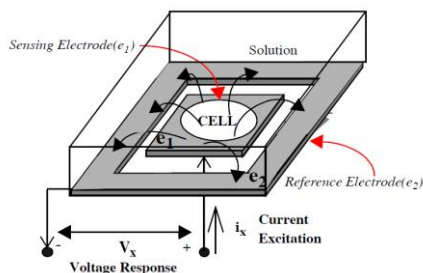


Figure 2. Two electrodes for ECIS:  $e_1$  (sensing) and  $e_2$  (reference). AC current  $i_x$  is injected between  $e_1$ - $e_2$ , and voltage response  $V_x$  is measured.

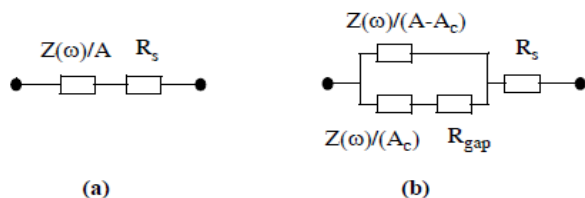


Figure 3. Proposed model for the an electrode-solution-cell model with area  $A$ , uncovered with cells (a) and covered and area  $A_c$  (b).

The relative changes at impedance magnitude, defined as,

$$r = \frac{Z_c - Z_{nc}}{Z_{nc}} \quad (1)$$

inform more accurate from these variations, being  $r$  the change of impedance magnitude for the two-electrode with cells ( $Z_c$ ) with respect to the system without them ( $Z_{nc}$ ). The graphics of  $r$  versus frequency is plotted in Fig. 5, for a cell-to-electrode coverage  $ff$  from 0.1 to 0.9 in steps of 0.1, using a  $R_{gap}=90$  k $\Omega$ . The size of the electrode is  $32 \times 32 \mu m^2$  [9,10]. It can be identified again the frequency range where the sensitivity to cells is high at 100kHz, represented by  $r$  increments. For a given frequency, each normalized impedance value of  $r$  can be linked with its  $ff$ , being possible the cell detection and estimation of the covered area  $A_c$ . Even more, area covered can be interpreted as consequence than two or more cells, allowing cell count for a given cell size.

From Fig. 5, it can be deduced that models of electrode-cell electrical performance can be used to derive the overlapping area in cell-electrode systems, useful for biological studies. It can be observed how the curve fits well with the frequency range, placing the maximum  $r$  value around 100 kHz, as predicts the FEM simulations [9, 10]. A value of  $R_{gap}=90$  k $\Omega$  was selected for this curve, representing a maximum value of the  $r$  curve with  $ff=0.69$ , which represents the ratio ( $A_c/A$ ), for a cell size of  $30 \mu m$  diameter represented at figure obtained using FEM simulations [10]. Impedance sensor curves at figures 4 and 5 were obtained using SpectreHDL [15] mixed-

mode simulator, with Analog Hardware Description Language (AHDL) for circuits in Fig. 3. An advantage of using AHDL models is the possibility of including non-linear performance of circuit elements, in our case, the frequency squared-root function at the Warburg impedance.

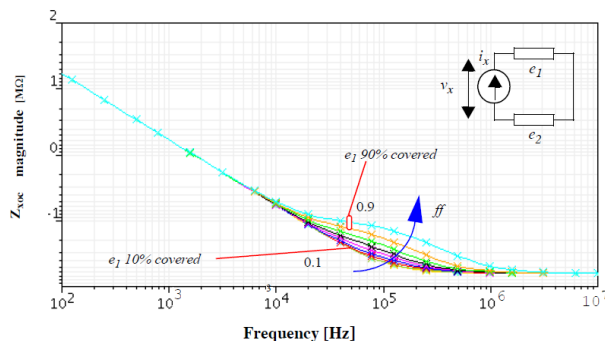


Figure 4. Impedance evolution when fill factor increases  $32 \times 32 \mu m^2$ .

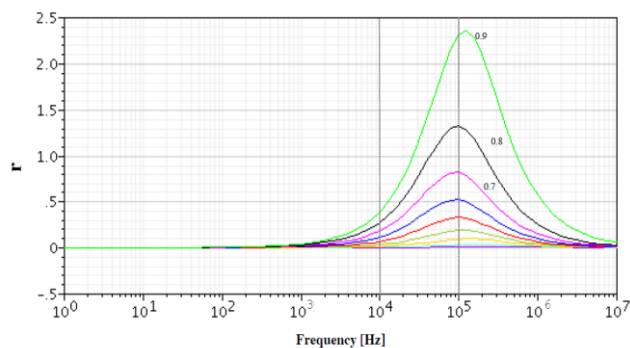


Figure 5. Normalized impedance  $r$  versus frequency derived from Fig. 4. Curves correspond to  $ff$  in the range of 0.1 (near empty) to 0.9 (near full).

#### IV. CELL CULTURE APPLICATIONS

##### A: Electrode Model

The proposed model based in Fig 3 has three main parameters: the electrode area ( $A$ ), the fill-factor ( $ff$ ), and the resistance of the gap region ( $R_{gap}$ ). Technology data were included and simulation results obtained to model a commercial electrode: 8W10E, from Applied Biophysics [12]. It is composed by eight wells; each one contains ten circular gold microelectrodes, with  $250 \mu m$  diameter. Ten sensing electrodes, in parallel, were used for  $e_1$  and only one common reference electrode, much larger than sensing ones. Figure 6 represents the normalized impedance  $r$  expected for these electrodes, for  $R_{gap}=22$  k $\Omega$ , if fill factor changes from electrodes without cell on top ( $ff=0.1$ ) to near those fully covered ( $ff=0.9$ ). Values of  $R_{gap}$  can be used to match the models to observed performance. In Fig. 7,  $R_{gap}$  values were changed for  $ff=0.9$ , observing large  $r$  changes. Finally, it was also modified the electrode area for  $R_{gap}=22$  k $\Omega$  and  $ff=0.9$ , showing the results at Fig. 8. It can be observed that optimal working frequency is near the proposed by the electrode factory (around 4 kHz), and that electrode area covered by cells can be approximated by using the fill factor parameters. The performance curves obtained before can be used to fit experimental results to proposed model and find relevant biometric characteristics.

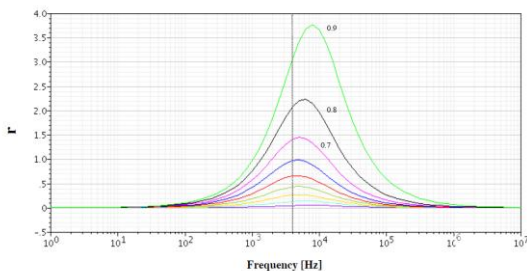


Figure 6. Obtained curves for  $r$  vs frequency, for  $ff \in [0.1,0.9]$  and  $R_{gap} = 22k\Omega$ , using 8W10E electrodes.

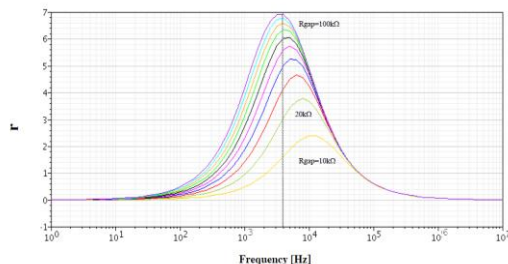


Figure 7. Obtained curves for  $r$  vs frequency, for  $R_{gap} \in [10k\Omega,100k\Omega]$  in steps of  $10k\Omega$ , for  $ff=0.9$ , using 8W10E electrodes.

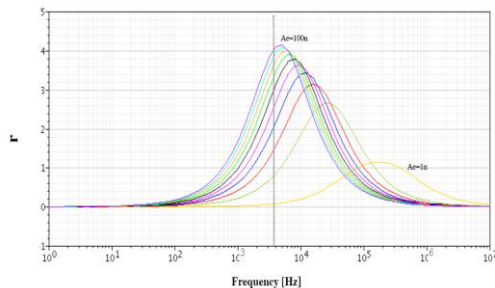


Figure 8. Obtained curves for the  $r$  vs frequency, for  $R_{gap}=22k\Omega$  and  $ff=0.9$ , for different electrode areas ( $1n$  to  $100n$ ).  $49n$  ( $49 \cdot 10^{-9}m^2$ ) corresponds to a circular electrode with a  $250\mu m$  diameter.

**B: Cell growth**

In Fig. 9a it is shown the growth curve obtained by us during seven days using 8W10E sensors with a similar setup in [8]. AA8 cells for chinese hamster were seeded initially, in an approximated number of 5000. The impedance range is around  $1220\Omega$  ( $380\Omega-1600\Omega$ ). Considering an initial cell number of 5000 very low, we take the initial impedance as due to no-cell impedance value ( $Z_{nc}$ ). At  $t=6000$  min, the medium was changed, and the confluent phase was achieved at  $t = 8500$  min approximately. The maximum experimental value given from eq. (1) is around  $r = 3.1$ , as illustrates Fig. 9b. We consider in our model that the electrodes are aproximately fully covered by cells for  $ff=0.9$ , the value of  $R_{gap}$  that better fits is  $22k\Omega$ . System response corresponds to  $r$ -values illustrated in Fig. 6. From these curves, it can be obtained the fill factor at different times. Table I summarized the relative normalized impedance values  $r$  at several times. Using Fig. 6 for the sensor response, fill factor is calculated at every instant. For a well area of  $0.8\text{ cm}^2$ , the maximum cell number goes from  $0.8 \times 10^6$  to  $1.6 \times 10^6$ . Number of cells,  $n_{cell}$ , in Table I, is obtained from  $0.8 \times 10^6$  expected final cell number. A value of  $Z_{nc}=380\Omega$  for  $r$  calculus in eq. (1) was considered.

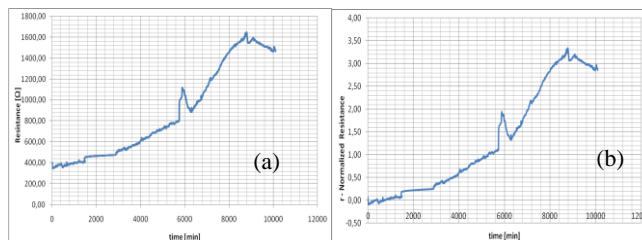


Figure 9. (a) Impedance evolution of the cell growth experiment. (b) The normalised impedance  $r$  evolution obtained.

TABLE ME: CELL NUMBER ( $n_{cell}$ ) OBTAINED FROM IMPEDANCE  $Z_c$  MEASURE IN Fig. 9, AND USING THE  $r$  CURVES PROPOSED FOR 8W10E SENSORS.

| t (min) | r     | ff    | $n_{cell}$ |
|---------|-------|-------|------------|
| 0       | 0     | -     | 5000       |
| 500     | 0.024 | 0.020 | 18000      |
| 1000    | 0.050 | 0.050 | 44000      |
| 1500    | 0.072 | 0.070 | 63000      |
| 2000    | n.a.  | n.a.  | n.a.       |
| 2500    | n.a.  | n.a.  | n.a.       |
| 3000    | 0.374 | 0.362 | 322000     |
| 3500    | 0.437 | 0.395 | 351000     |
| 4000    | 0.615 | 0.475 | 422000     |
| 4500    | 0.777 | 0.530 | 471000     |
| 5000    | 0.903 | 0.581 | 516000     |
| 5500    | 1.033 | 0.602 | 535000     |
| 6000    | 1.074 | 0.620 | 551000     |
| 6500    | 1.507 | 0.710 | 631000     |
| 7000    | 1.970 | 0.775 | 689000     |
| 7500    | 2.353 | 0.810 | 720000     |
| 8000    | 2.837 | 0.860 | 764000     |
| 8500    | 3.113 | 0.890 | 791000     |
| 9000    | 3.134 | 0.900 | 800000     |
| 9500    | 3.010 | 0.875 | 778000     |
| 10000   | 2.857 | 0.864 | 768000     |

**C: Dosimetry**

Experiments to characterize the influence of some drugs in cell growth were done. The objective is to proof that proposed model allows counting cell number at different dosis. It was considered the AA8 cell line and as drug, six different doses of MG132 for growth inhibition (from  $0.2\mu M$  to  $50\mu M$ ). After 72 hours normal cell growth, the medium was changed and the drug added at different doses: 0.2, 0.5, 1, 5, 10 and  $50\mu M$  for wells 3 to 8 respectively. Well 2 is the control.

Measured impedances for the 8 wells are at Fig. 10, for 4kHz working frequency. At the end of the experiment can be observed that impedance decreases as drug dosis increases. Control (W2) is full of cells with the maximum impedance, while maximum dosis (W8) has the lowest resistance, at the botton. The black line (W1) represents the electrode-solution impedance. After the medium change ( $t=4000$ min), it is observed a decreasing impedance below the initial baseline level ( $400\Omega$ ) that we cannot explain. Final impedance values at 8000min,  $Z_c$ , were considered, at Table II. From  $Z_{nc}$  and  $Z_c$ ,  $r$  values are calculated in third column. Using curves for  $r$  versus frequency in Fig. 6,  $ff$  estimated values from proposed model are obtained. The cell number at the end of the experiment was also count and shown at the last column for each well. Considering  $ff_{max}=0.9$  for a measured cell number of  $8.06 \times 10^5$ , the expected values for  $ff$  are calculated.

The same data are summarized at Table III for 2, 4 and 10kHz frequencies respectively. The better agreement it is obtained at 4kHz in fill factor ( $ff$ ). It is observed that the impedance baseline,  $Z_{nc}$ , for  $r$  calculus decreases with frequency due probably to electrode impedance dependence.



For medium resistance (W1) and high drug concentrations wells (W6-W8), the resistance measured is below to  $Z_{nc}$ , so eq. (1) can no be applied for r calculation.

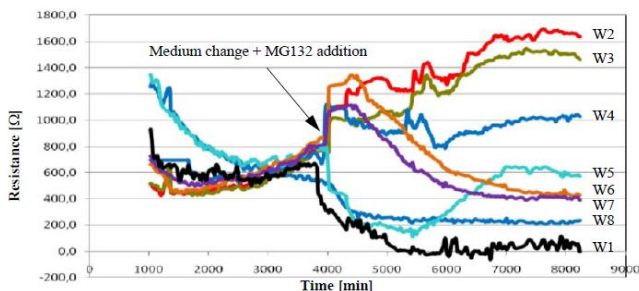


Figure 10. Impedance measure in dosimetry at 8 wells for 4kHz frequency. W1: Medium. W2: Control. W3: 0.2μM. W4: 0.5 μM. W5: 1 μM. W6: 5 μM. W7: 10 μM and W8: 50 μM.

TABLE II: EXPERIMENTAL VALUES FOR RELATIVE IMPEDANCE (r) AND FILL-FACTOR (ff) FOR  $Z_{nc} = 400 \Omega$ . FREQUENCY = 4 KHZ.

| Well | $Z_c$<br>t=8000min | r              |           | ff       |                      | n <sub>cell</sub><br>measured |
|------|--------------------|----------------|-----------|----------|----------------------|-------------------------------|
|      |                    | $Z_c / Z_{nc}$ | estimated | expected |                      |                               |
| 1    | 259.2              | -              | -         | -        | -                    | Medium                        |
| 2    | 1631.7             | 3.1            | 0.90      | 0.900    | 8.06x10 <sup>5</sup> |                               |
| 3    | 1454.7             | 2.6            | 0.85      | 0.690    | 6.13x10 <sup>5</sup> |                               |
| 4    | 1030.6             | 1.5            | 0.72      | 0.610    | 5.41x10 <sup>5</sup> |                               |
| 5    | 625.8              | 0.5            | 0.44      | 0.410    | 3.60x10 <sup>5</sup> |                               |
| 6    | 417.4              | 0.05           | 0.037     | 0.036    | 3.20x10 <sup>4</sup> |                               |
| 7    | 406.8              | 0.015          | 0.016     | 0.024    | 2.10x10 <sup>4</sup> |                               |
| 8    | 99.6               | < 0            | -         | 0.005    | 4.00x10 <sup>3</sup> |                               |

TABLE III: EXPERIMENTAL VALUES FOR RELATIVE IMPEDANCE (r) AND FILL FACTOR (ff) AT VARIOUS FREQUENCIES.  $Z_{nc} = 480 \Omega$ , 400Ω, AND 315Ω FOR 2, 4 AND 10 KHZ WORKING FREQUENCY RESPECTIVELY.

| Well | r (from $Z_c$ and $Z_{nc}$ ) |       |       | ff (from model) |       |       | ff expect. |
|------|------------------------------|-------|-------|-----------------|-------|-------|------------|
|      | 2kHz                         | 4kHz  | 10kHz | 2kHz            | 4kHz  | 10kHz |            |
| 1    | -                            | -     | -     | -               | -     | -     | Medium     |
| 2    | 2.43                         | 3.1   | 3.76  | 0.98            | 0.90  | 0.90  | 0.900      |
| 3    | 2.18                         | 2.6   | 3.24  | 0.94            | 0.85  | 0.88  | 0.690      |
| 4    | 1.17                         | 1.5   | 2.21  | 0.82            | 0.72  | 0.82  | 0.610      |
| 5    | 0.21                         | 0.5   | 0.84  | 0.32            | 0.44  | 0.44  | 0.410      |
| 6    | -                            | 0.05  | -     | -               | 0.037 | -     | 0.036      |
| 7    | -                            | 0.015 | -     | -               | 0.016 | -     | 0.024      |
| 8    | -                            | -     | -     | -               | -     | -     | 0.005      |

V. DISCUSSION AND CONCLUSIONS

This work describes an area dependent model for cell-electrode systems and its application to measure and identify cells during cell culture protocols. A practical circuit for electrode-solution-cell simulation was employed, using an AHDL description for commercial electrodes, obtaining a good matching. Optimal measurement frequency was identified near 4 kHz. It was proposed the cell growth evolution study based on 8W10E electrode models. Curves obtained experimentally, allows the real time growth monitoring by fitting the  $R_{gap}$  parameter. An estimation of the number of cells was obtained by using sensor curves calculated from electrical model proposed. Dosimetry experiments reproduce similar conditions than cell growth, but in this case, it is added a growth inhibitor at different dosis. There is observed a decreasing impedance, below the baseline expected ( $Z_{nc}$ ) that we can not explain.

However, for the control and small drug dosis, impedance curves are perfectly aligned. It was fitted a proposed model with  $R_{gap}=22k\Omega$  to explain experimental data. Deviations from data are over 10-20% in fill factor, more accurate for 4 kHz.

The deviations in fill factors measured are not small, being required to analyze the influence of error sources to increase the system performance. First, Signal-to-Noise Ratio (SNR) should be increased at the setup. Second, proposed model has the advantage that need only one parameter ( $R_{gap}$ ), versus other reported model using three parameters [8]. One parameter model makes easy to fit experimental data, but can introduce inaccuracy. The possibility to add more parameters to the model should be considered in the future.

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REFERENCES

- [1] S. Grimnes and O. Martinsen, "Bio-impedance and Bioelectricity Basics," Second edition. Academic Press, Elsevier. 2008.
- [2] R. D. Beach et al., "Towards a Miniature In Vivo Telemetry Monitoring System Dynamically Configurable as a Potentiostat or Galvanostat for Two- and Three- Electrode Biosensors," IEEE transaction on Instrumentation and Measurement, vol 54, n°1, pp:61-72. 2005.
- [3] A. Yúfera et al., "A Tissue Impedance Measurement Chip for Myocardial Ischemia Detection," IEEE transaction on Circuits and Systems: Part I. vol.52, n°:12 pp:2620-2628. 2005.
- [4] S. Radke et al., "Design and Fabrication of a Microimpedance Biosensor for Bacterial Detection," IEEE Sensor J. vol 4,n° 4,434-440. 2004.
- [5] A. Yúfera et al., "A Method for Bioimpedance Measure With Four- and Two-Electrode Sensor Systems," 30th Annual International IEEE EMBS Conference, pp: 2318-2321. 2008.
- [6] D. A. Borkholder. Cell-Based Biosensors Using Microelectrodes. PhD Thesis, Stanford University. 1998.
- [7] I. Giaever, et al., "Use of Electric Fields to Monitor the Dynamical Aspect of Cell Behaviour in Tissue Cultures," IEEE Transaction on Biomedical Engineering, vol. BME-33, No. 2, pp. 242-247. 1986.
- [8] I. Giaever and C. R. Keese, "Micromotion of mammalian cells measured electrically," Proc. Nail. Acad. Sci. USA. Cell Biology, vol. 88, pp: 7896-7900, Sep. 1991.
- [9] X. Huang et al., "Simulation of Microelectrode Impedance Changes Due to Cell Growth," IEEE Sensors J., vol.4, n°5, pp: 576-583. 2004.
- [10] A. Olmo et al., "Computer Simulation of Microelectrode Based Bio-Impedance Measurements With COMSOL," BIODEVICES 2010. pp: 178-182. Valencia (Spain), 20-23, Jan. 2010.
- [11] P. Wang and Q. Liu, editors. Cell-Based Biosensors: Principles and Applications, Artech House Series. 2010.
- [12] Applied Biophysics. Http://www.biophysics.com/.
- [13] A. Manickam, A. Chevalier, M. McDermott, A. D. Ellington, and A. Hassibi, "A CMOS Electrochemical Impedance Spectroscopy (EIS) Biosensor Array," IEEE Transactions on Biomedical Circuits and Systems, vol 4, n° 6. pp: 379-390. 2010.
- [14] A. Yúfera and A. Rueda, "A Real-Time Cell Culture Monitoring CMOS System Based on Bio-impedance Measurements," Kluwer Academic P.. Analog Integrated Circuits and Signal Processing. 2011. (accepted)
- [15] A. Yúfera A. and E. Gallego, "Generation of HDL Models for Bioimpedance Sensor Simulation Based on Microelectrodes," Sensors and Transducers Journal, pp: 160-170. vol. 10. Feb. 2011.