

LABORATORY OF PHARMACEUTICAL PROCESS ANALYTICAL TECHNOLOGY

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PRACTICAL IMPLEMENTATION OF DYNAMIC PRIMARY DRYING SETTINGS IN A CONTINUOUS FREEZE-DRYING PROCESS

INTRODUCTION

- Continuous freeze-drying = 1) Spin freezing vials with N₂-gas (→ thin product layer) + 2) Perpetual vacuum chamber with radiation as energy supply method (→ more uniform)
- Mechanistic model of the continuous drying step¹ → most optimal dynamic dryer settings: chamber pressure (P_c) & radiator temperature (T_{rad}).
- Continuous processing → unit doses processed one by one → enables individualised process settings per vial → reducing effects of uncontrolled factors → uniform quality

AIM: Supercooling = uncontrolled factor → vial-to-vial dry product resistance (R_p) variability → adjust dynamic dryer settings per unit dose based on supercooling temperature (T_{sc})

SPINFREEZING

Material & methods:

- Spinfrozen at 2000 RPM with 50 l/min nitrogen gas of -30±3 °C
- 3,9 ml solution (5 % mannitol) in 10R Schott vial
- Experimental groups: scratched vial wall (Scored) vs (Regular)
- Vial Temperature (T_{vial}) with Infrared (IR) thermometer
- T_{sc} = temperature just before nucleation (1A at Graph 1)

Results:

- Nucleation → Appearance of clear white ice (Figure 1: 1A vs 1B) → Simultaneous rise in T_{vial} towards 0 °C (Graph 1)
- Wide range of T_{sc} were observed (i.e. between -4 °C and -12 °C)

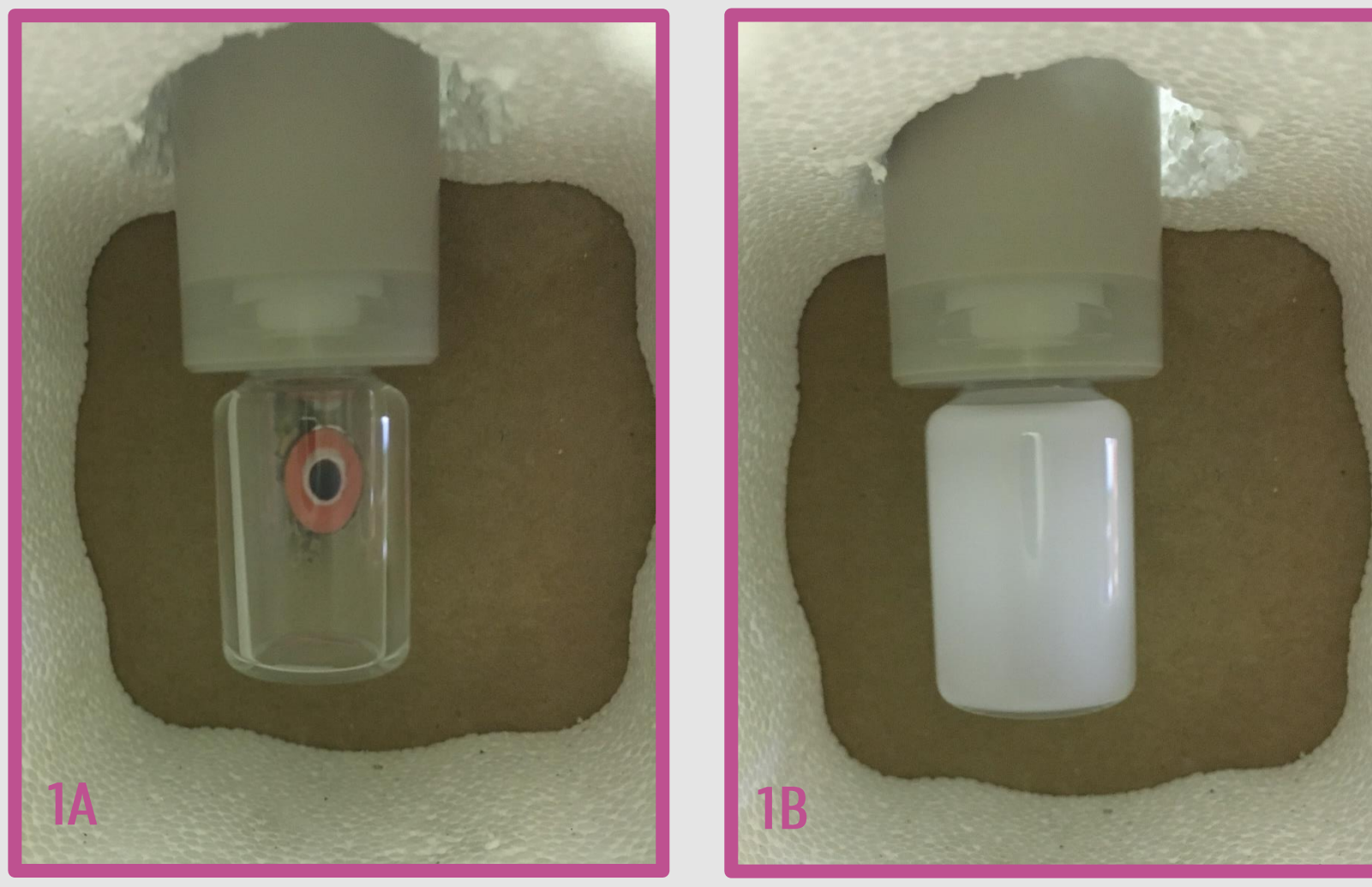
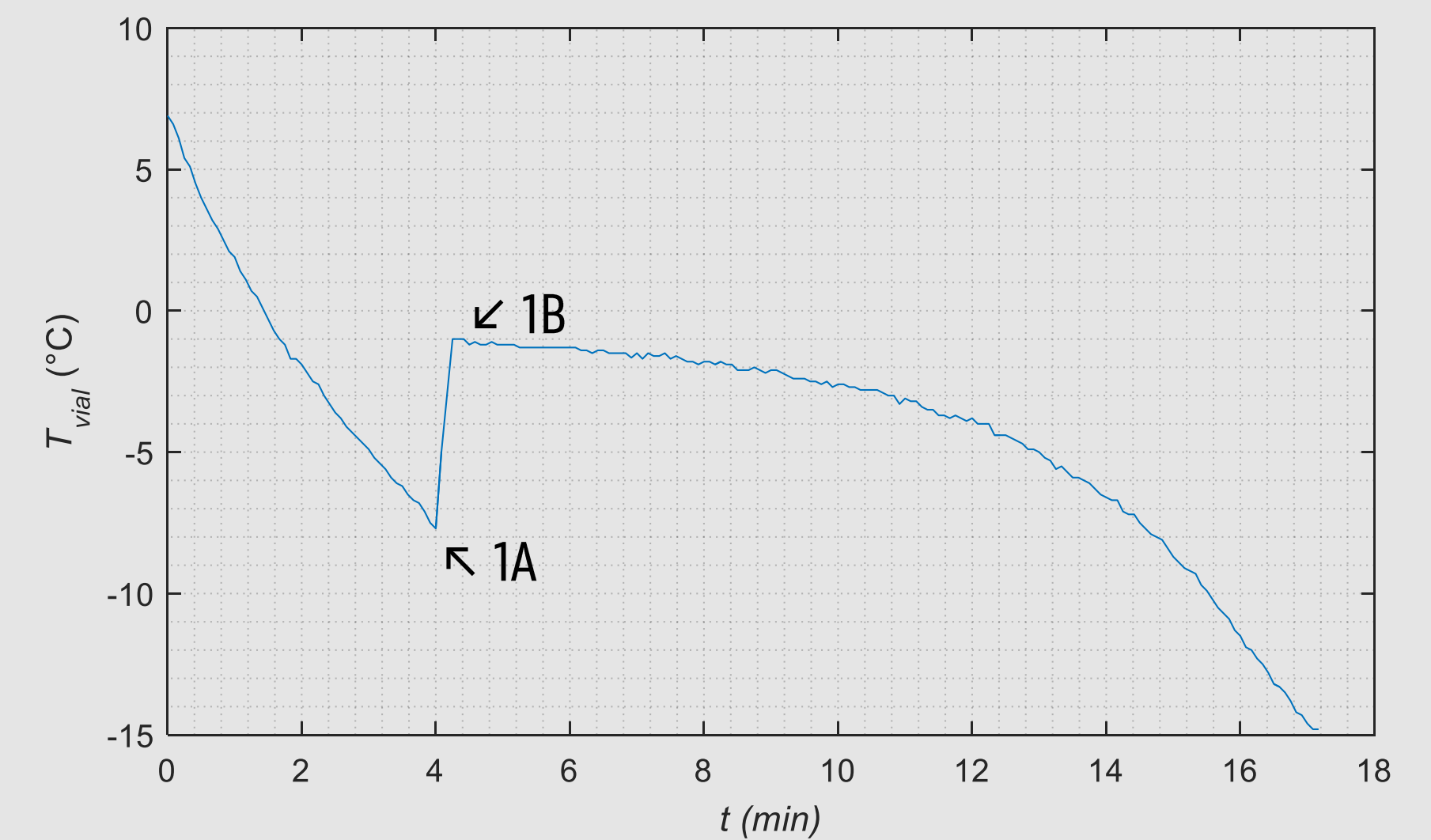
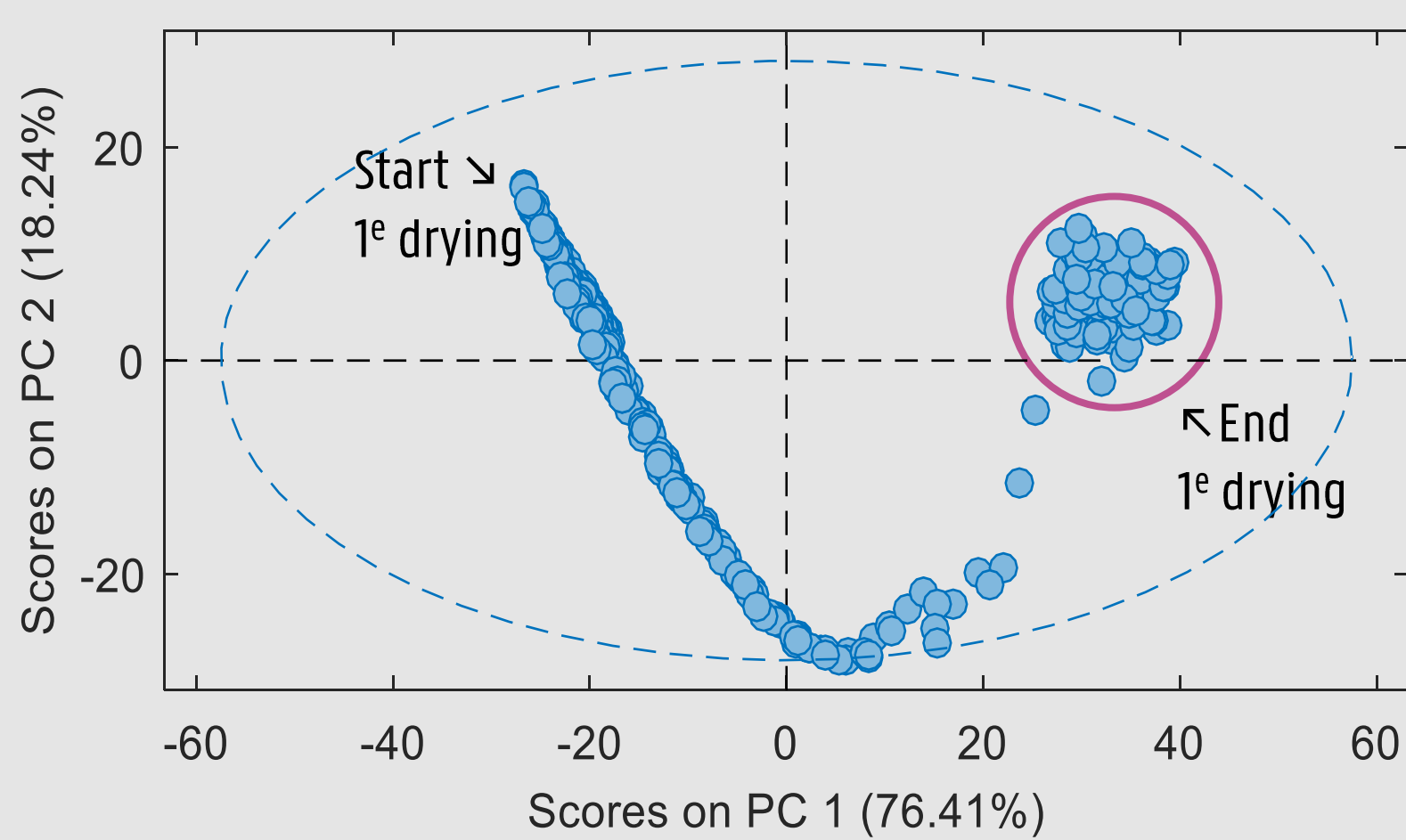


Figure 1: Spinned vial just before (1A) and right after (1B) nucleation

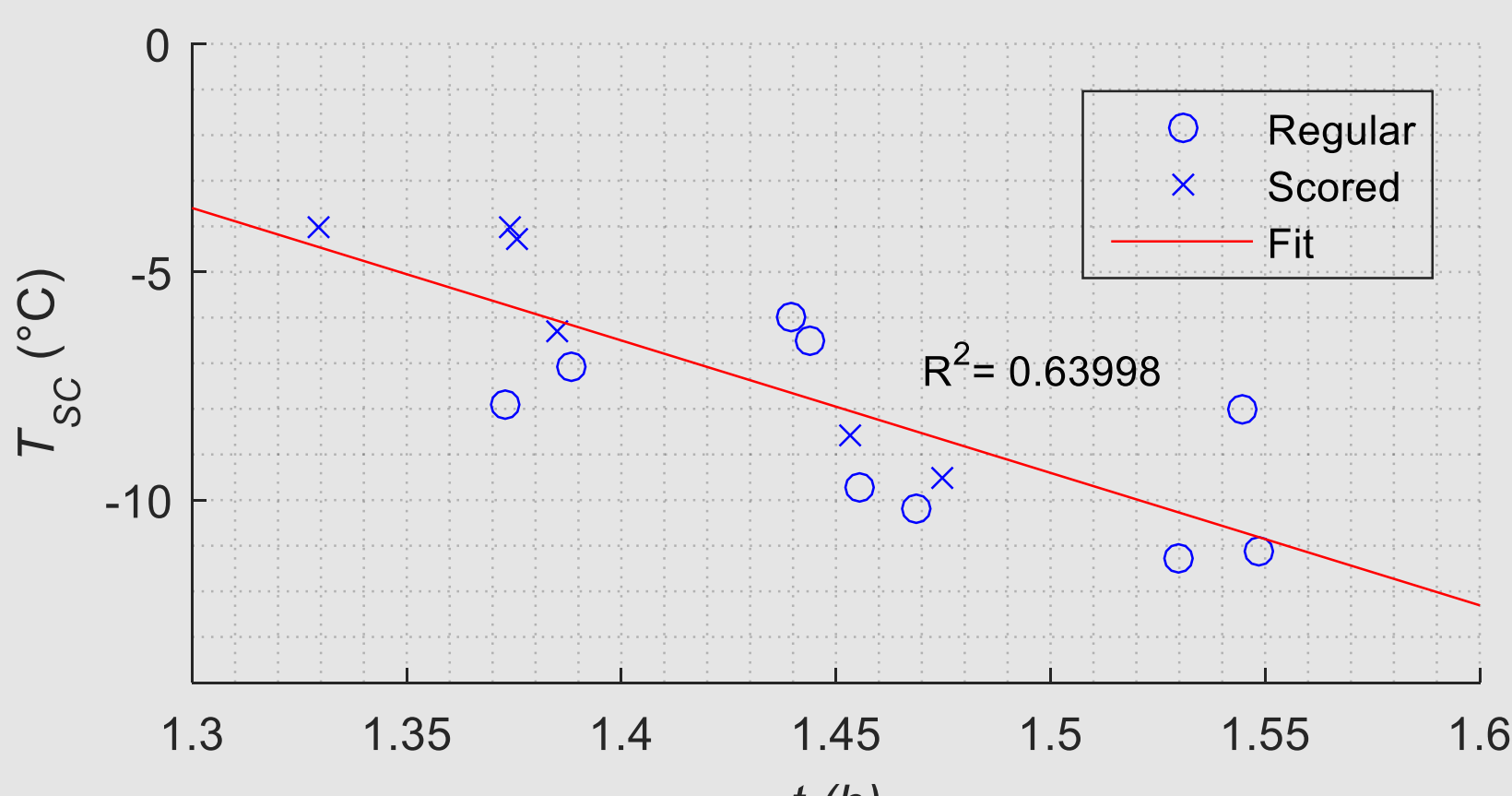


Graph 1: Observed vial temperature with infrared thermometer during spinfreezing

PRIMARY DRYING



Graph 2: Scores plot from PCA analysis: primary drying end point



Graph 3: Observed T_{sc} versus primary drying time by NIR

Material & methods:

- 15 vials with a T_{sc}: -4 to -12 °C dried by radiation (18W) at 55 Pa (Figure 2)
- Every 20 s NIR spectra → Savitzky-Golay smoothing and SNV preprocessing
- Principal component analysis (PCA) → primary drying end point (Graph 2)
- 1e Derivative → peak shifts at 5250 & 7074 cm⁻¹ → product temp (T_p)

$$(1) P_i = e^{\frac{-6140.4}{T_p} + 28.916} \quad (2) R_p = \frac{(P_i - P_c) \times A}{\dot{m}_{sub}} \quad (3) R_p = R_{p0} + \frac{A_{Rp} \times l}{1 + B_{Rp} \times l}$$

- Average sublimation rate (\dot{m}_{sub}) = filling volume / 1st drying time (by NIR)
- R_p estimated using (1) and (2) and plotted against dry layer thickness (l)
- Parameters in (3) fitted → A_{Rp} & B_{Rp} linearly regressed to the observed T_{sc}

Results:

- Linear relation between T_{sc} and 1st drying time with R² of 0.64 (Graph 3) → similar observation by Searles in regular frozen vials²
- For 7 out of 15 vials the T_p prediction (RMSE: 4°C): reasonably feasible → R_p calculated and plotted against l (Graph 4)
- Linear relation between A_{Rp} and T_{sc} observed with R² of 0.76 → similar observation by Rambhatla with controlled nucleation³
- Unclear regression of B_{Rp} to T_{sc} with R² of 0.31
- T_p dominant in R_p calculation → error on T_p prediction to big for reasonable R_p predictions

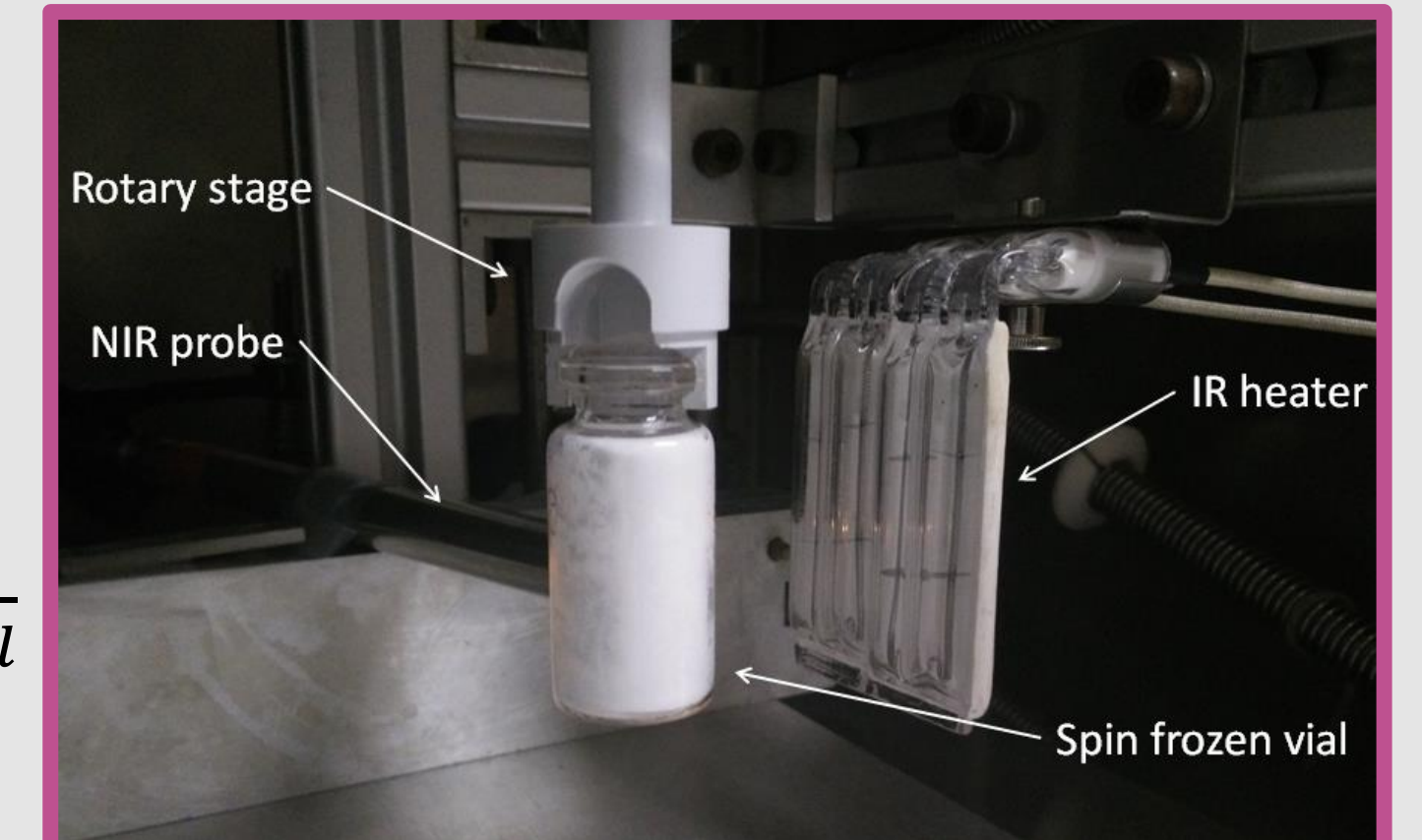
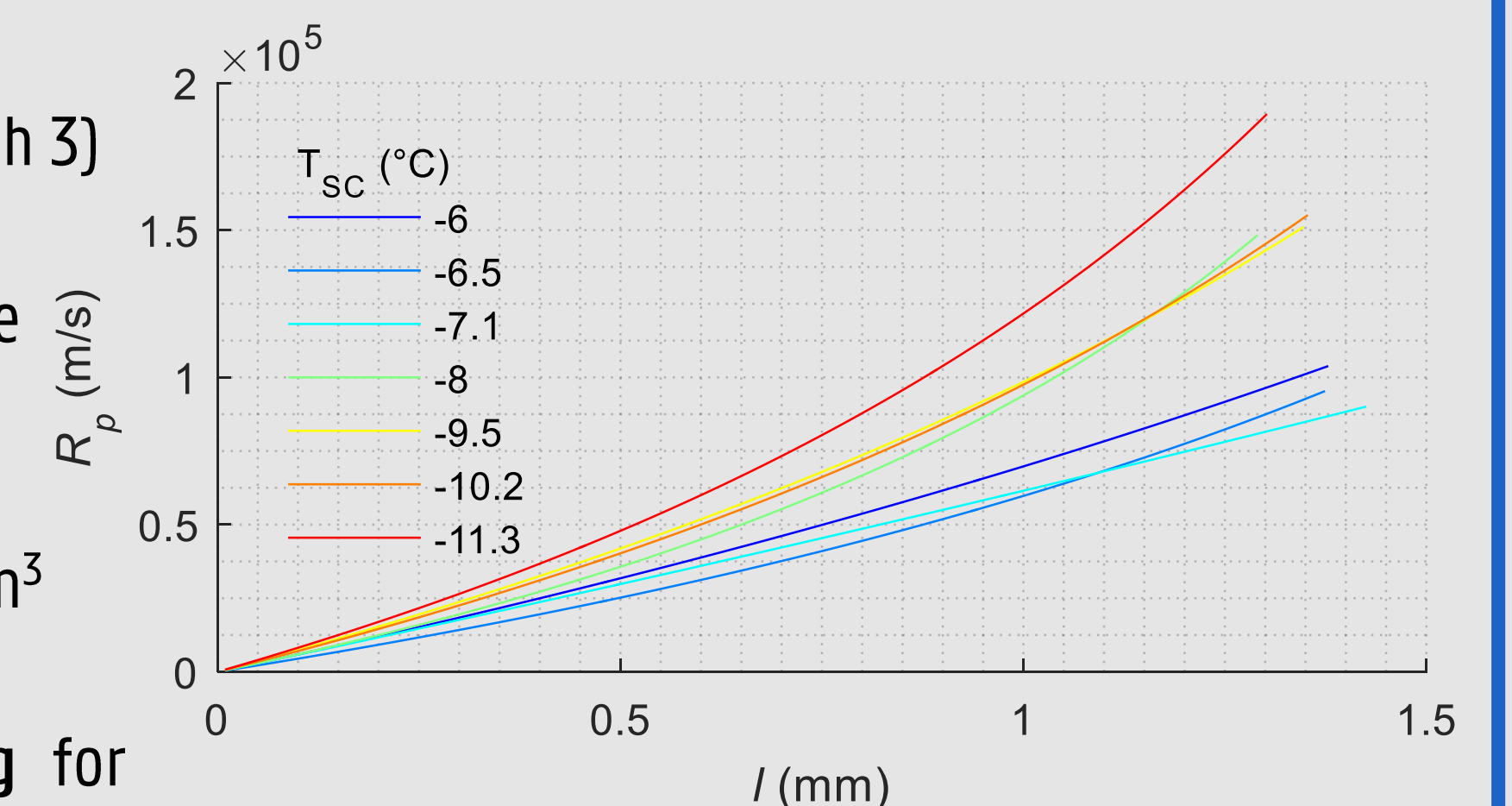


Figure 2: Radiation primary drying stage with NIR probe



Graph 4: Fitted dry layer resistance versus dry layer thickness

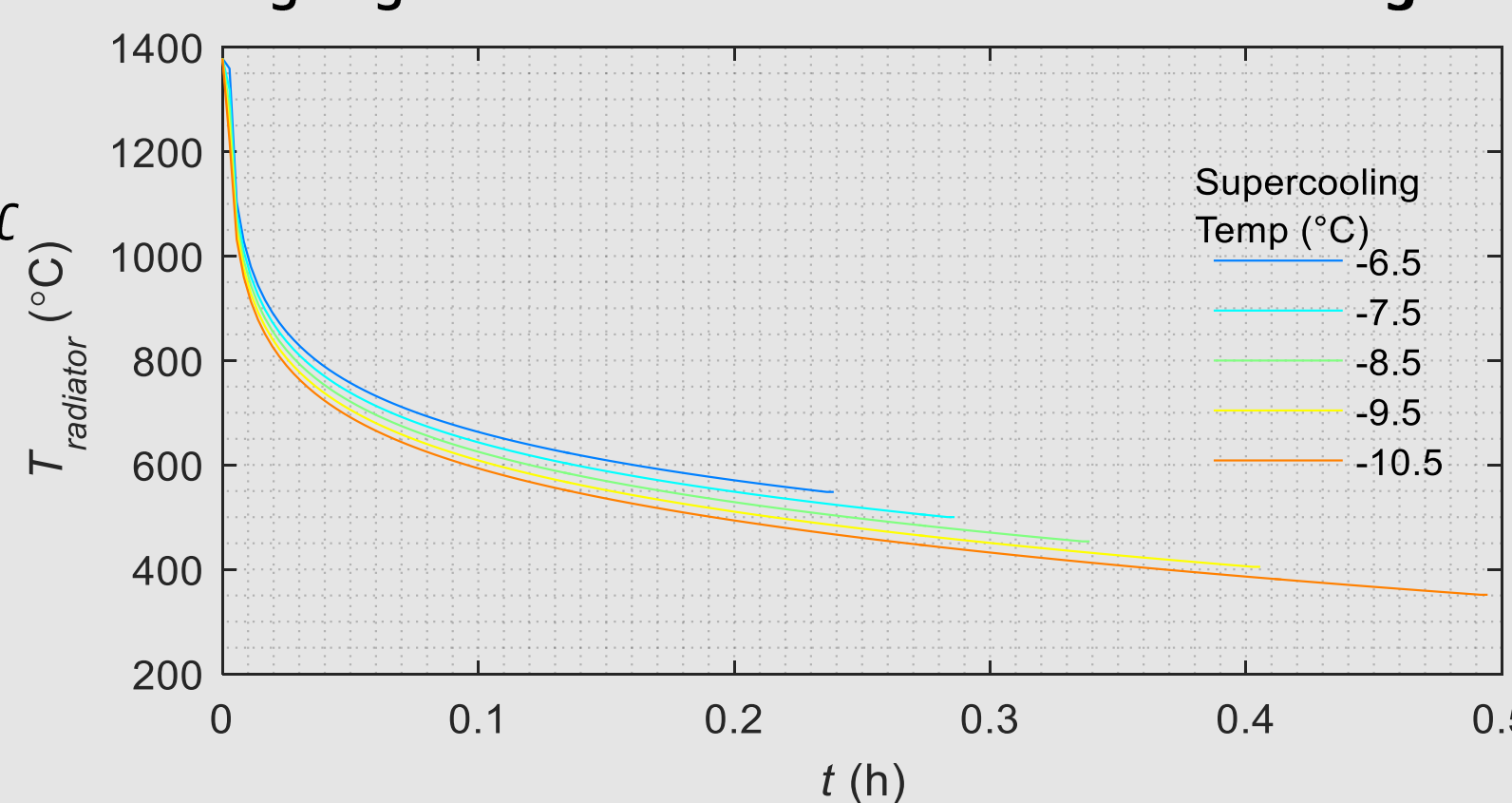
DYNAMIC SETTINGS

Material & methods: A full integrated Labview 2015SP1 application was developed containing (Figure 3):

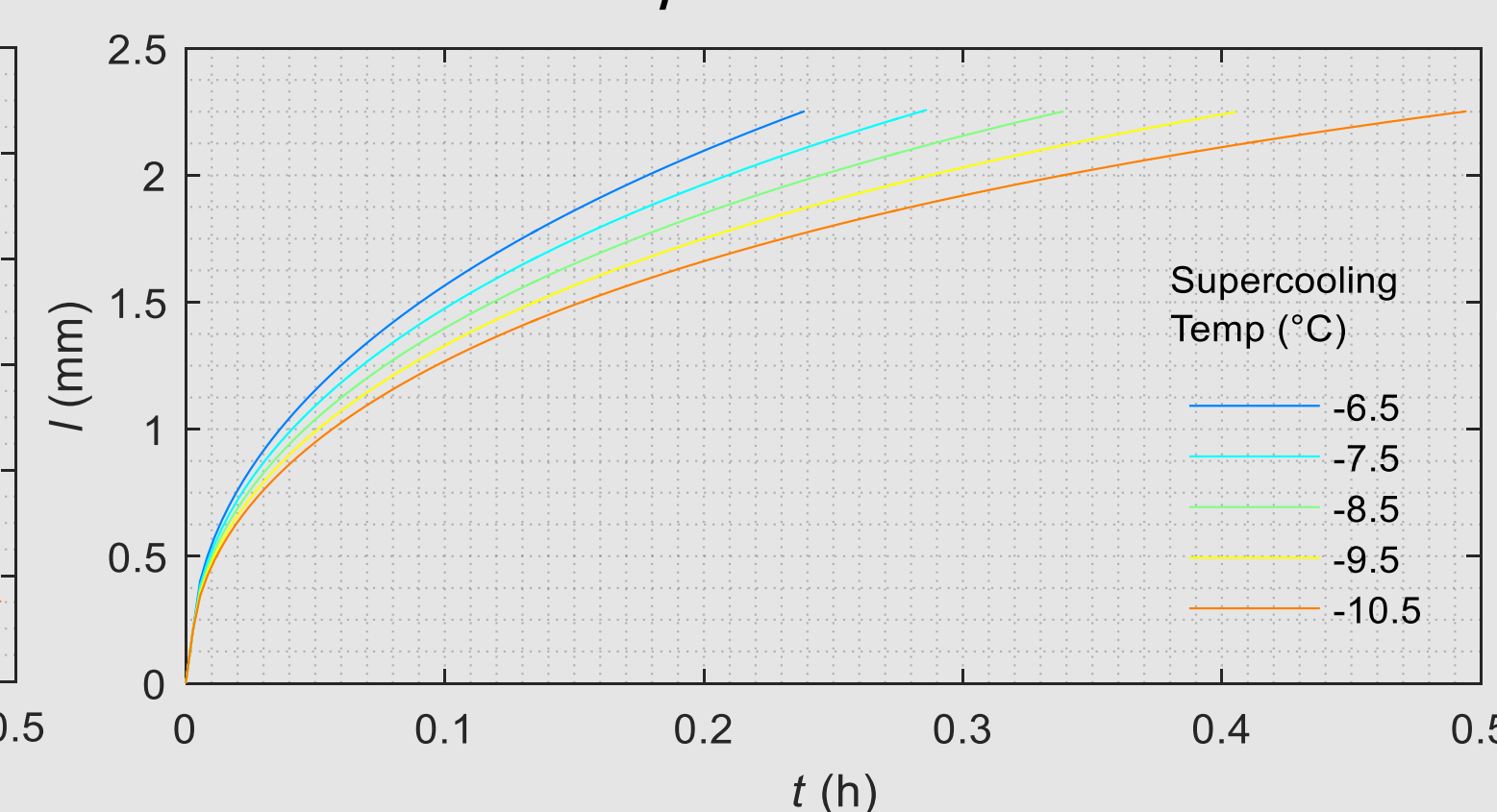
- Primary drying mechanistic model developed in Matlab R2015b¹ → prediction of most optimal dryer settings (P_c & T_{rad})
- Capturing all model input variables: formulation properties (i.e. R_{p0}, A_{Rp} & B_{Rp}); vial dimension, freeze dryer configuration, filling volume ...
- Data acquisition from the Pirani vacuum gauge and Actuator drivers: Gas dosing valve and NIR radiator by the Power source

Results:

- A_{Rp} & B_{Rp} predicted for several T_{sc}
- Safe T_p of -10 °C assumed
- Labview → most optimal drying trajectories (graph 5 and 6)
- considerable difference in 1e drying time → unrealistic A_{Rp}



Graph 5: Simulated T_{rad} versus primary drying time



Graph 6: Simulated dry layer thickness versus primary drying time

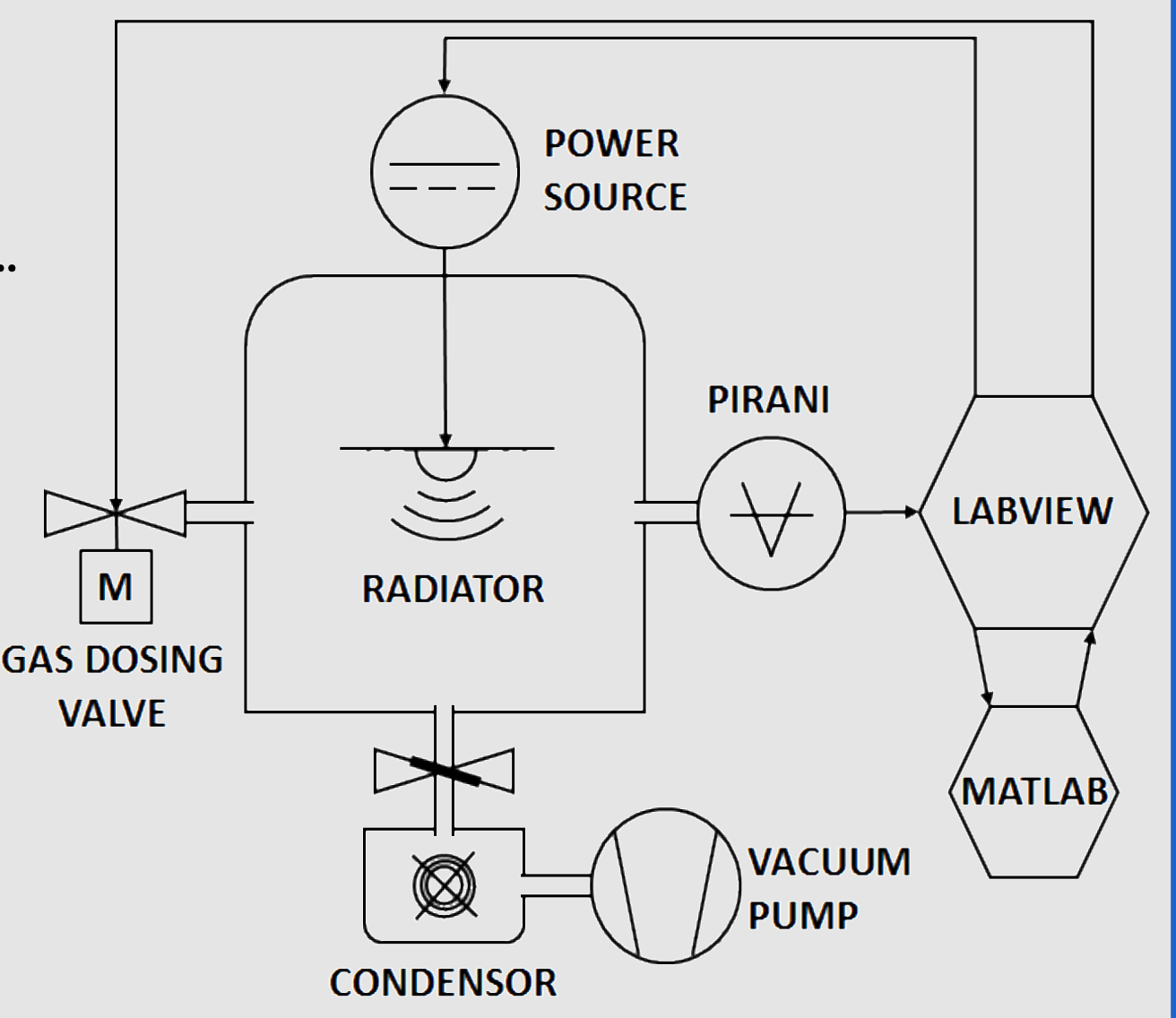


Figure 3: Piping and instrumentation diagram of primary drying set-up; M: motor actuated

CONCLUSION

- Supercooling temperature (T_{sc}) effect upon the primary drying of spinfrozen vials observed; similar to reports by literature^{2,3}
- NIR spectra → Primary drying end point detection by PCA; T_p prediction by peak shift of the 5250 & 7074 cm⁻¹ waterbands
- R_p calculations overestimated due to the inaccuracy of the product temperature (T_p) predictions → unrealistic A_{Rp} parameters
- Full integrated controlled drying system developed, capable of individualised optimal drying settings to compensate for uncontrolled factors: i.e. supercooling temperature → more uniform batch quality

- 1: Van Bockstal (2017). J. Pharm. Sci. (106) 71-82;
- 2: Searles (2001). J. Pharm. Sci. (90) 872-887;
- 3: Rambhatla (2004). AAPS PharmSciTech, (5) 1-9;

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