

Sliding-Mode Controller Based on Fractional Order Calculus For a Class of Nonlinear Systems

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Article Info

Article history:

Received Apr 12, 2016

Revised July 18, 2016

Accepted Aug 7, 2016

Keyword:

fractional order calculus

SMC

FOSMC

inverted pendulum

ABSTRACT

This paper presents a new approach of fractional order sliding mode controllers (FOSMC) for a class of nonlinear systems which have a single input and two outputs (SITO). Firstly, two fractional order sliding surfaces S_1 and S_2 were proposed with an intermediate variable z transferred from S_2 to S_1 in order to hierarchy the two sliding surfaces. Secondly, a control law was determined in order to control the two outputs. A sliding control stability condition was obtained by using the properties of the fractional order calculus. Finally, the effectiveness and robustness of the proposed approach were demonstrated by comparing its performance with the one of the conventional sliding mode controller (SMC), which is based on integer order derivatives. Simulation results were provided for the case of controlling an inverted pendulum system.

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1. INTRODUCTION

Sliding mode control has largely proved its effectiveness in numerous applications, see, e.g., the studies by Utkin [1] and Slotine [2]. The first step of the SMC design is to select a sliding surface that models the desired closed-loop performance in state variable space. In the second step, equivalent and hitting control laws are designed such that the system state trajectories are forced towards the sliding surface and slide along it to the desired attitude.

An advantage of these methods of control (SMC) is their robustness to parameters variation and bounded external disturbances. The robustness is attributed to the discontinuous term in the control input. However, this discontinuous term also causes an undesirable effect called chattering. Sometimes this discontinuous control action can even cause instability of the system. This effect can be alleviated by, for example, introducing a sat function and taking off the sgn function in the hitting control law of the SMC.

In the last years, the control of single-input-two output non-linear dynamical systems has risen some interest in the control research community; in general, the controller (input) is done for the trajectory tracking of the two outputs. PID controllers were applied in [3] to the stabilization and tracking control of three types of inverted pendulum. A PID+LQR method was given in [4], in which the LQR was added negatively to the PID in order to have a resultant optimal control. A fuzzy controller with estimation of scaling factors was studied in [5]. An intelligent control system based on an interval type-2 fuzzy PD controller was studied in [6]. The SMC design for this kind of systems is a very challenging task. Such developed controllers include the decoupled SMC shown in [7], a Fuzzy Sliding Mode Control (FSMC) that was tuned using ant colony optimization [8], [9] and a decoupled SM with a fuzzy-neural network controller [10] where the fuzzy-neural network was used to approximate an ideal computational controller. All these developed approaches are based on the standard integer order calculus.

The fractional order differentiation theory, which has 300 years of history and deals with derivatives and integrals of non-integer order, has recently been rediscovered by scientists and engineering, being applied in many fields and, among them, the field of control. One of the first applications of fractional order derivatives/integrals to the control of dynamic systems was given by Oustaloup, who developed the so called Commande Robuste d'Ordre Non Entier (CRONE), which is described in [11, 12], along with examples of application in various fields. Fractional order

PID (FOPID) controllers have been studied in [13]. A fuzzy FOPID controller, which uses the error and its fractional order derivative as its input, and has a fractional order integrator in its output, has been proposed in [14].

Also in the SMC field, some researchers have introduced the fractional order calculus to design a fractional order sliding mode control (FOSMC). The first application using the technique of fractional order SMC returns to Calderon [15, 16] on a DC-DC power converter; where the authors defined switching surfaces based on the structures of fractional order PI (FOPI) and FOPID controllers. The approach which uses the FOPID sliding surface was also studied in [17, 18]. A FOSMC based on a fractional order PD (FOPD) sliding surface was studied in [19, 20] and a Fractional Order Terminal Sliding Mode Control (FOTSMC) was proposed in [21].

Motivated by the above discussion, this paper proposes a FOSMC for a class of single input two outputs non-linear systems. The control law is derived from these proposed fractional order sliding surfaces and its purpose is to drive the two outputs of the system to their desired trajectories. The stability is guaranteed by using the Lyapunov theorem. Simulation results illustrate that the proposed control design method applied to the inverted pendulum plant yield controller that can rapidly stabilize these system compared with the conventional integer order controller. This performance is guaranteed through the added extra parameter α (fractional order).

The rest of this article is organized as follows. A brief introduction to fractional calculus is described in Section 2. System description and control design are developed in Section 3. Simulation results and some conclusions are given in Sections 4 and 5 respectively.

2. A BRIEF INTRODUCTION TO FRACTIONAL CALCULUS

The fractional differo-integral operators are denoted by ${}_a D_t^\alpha f(t)$ (fractional calculus), where a and t , are the bounds of the operation and $\alpha \in \mathcal{R}$ is a generalization of the standard integration and differentiation to non-integer order operators.

The continuous differo-integral operator is given by the following:

$${}_a D_t^\alpha = \begin{cases} \frac{d^\alpha}{dt^\alpha} & \text{for } \alpha > 0 \\ 1 & \text{for } \alpha = 0 \\ \int_a^t (d\tau)^\alpha & \text{for } \alpha < 0 \end{cases} \quad (1)$$

In the literature We can find different definitions of the fractional differ-integral operator. But the most commonly used definitions of fractional order derivatives are:

The Riemann-Liouville (RL) definition:

$${}_a D_t^\alpha f(t) = \frac{1}{\Gamma(m-\alpha)} \left(\frac{d}{dt} \right)^m \int_a^t \frac{f(\tau)}{(t-\tau)^{1-(m-\alpha)}} d\tau \quad (2)$$

The Caputos definition:

$${}_a D_t^\alpha f(t) = \frac{1}{\Gamma(m-\alpha)} \int_a^t \frac{f^m(\tau)}{(t-\tau)^{1-(m-\alpha)}} d\tau \quad (3)$$

In these expressions, $m-1 < \alpha < m$, and $\Gamma(\cdot)$ is the well-known Eulers gamma function:

$$\Gamma(x) = \int_0^\infty e^{-t} t^{(x-1)} dt, \quad x > 0 \quad (4)$$

On the other hand, Grunwald-Letnikov (GL) reformulated the definition of the fractional order differ-integral operator as follows:

$${}_a D_t^\alpha f(t) = \lim_{h \rightarrow 0} \frac{1}{h^\alpha} \sum_{k=0}^{(t-a)/h} (-1)^k \binom{\alpha}{k} f(t-kh) \quad (5)$$

Since the numerical simulation of a fractional differential equation is not as simple as an ordinary differential equation, the Laplace transform method is often used as a tool for solving fractional order differential equations that arise in engineering applications [22], [23].

The Laplace transforms of the previous fractional order derivatives are given below.

The Laplace transform of the (RL) definition is as follows [22], [24]:

$$L \{ {}_0D_t^\alpha f(t); s \} = s^\alpha F(s) - \sum_{k=0}^{(m-1)} s^k \left[{}_0D_t^{(\alpha-k-1)} f(t) \right]_{t=0} \quad (6)$$

The Laplace transform of the Caputos definition is given by [24]:

$$L \{ {}_0D_t^\alpha f(t); s \} = s^\alpha F(s) - \sum_{k=0}^{(m-1)} s^{(\alpha-k-1)} f^k(0) \quad (7)$$

Where s denotes the Laplace operator. For zero initial conditions, the Laplace transforms of the fractional order derivatives of Riemann-Liouville and Caputo are reduced to (8) [24], [25].

$$L ({}_0D_t^\alpha f(t)) = s^\alpha F(s) \quad (8)$$

In this paper, the fractional order element s^α is approximated by the Oustaloups filter. The Oustaloups filter [26] approximates

$$G(s) = s^\alpha, \quad \alpha \in R \quad (9)$$

by a rational function of the form

$$\hat{G}(s) = K \prod_{k=-N}^N \frac{s + w'_k}{s + w_k} \quad (10)$$

where its parameters (zeros, poles, and gain) are determined by the following formulas:

$$\begin{aligned} w'_k &= w_b \cdot \left(\frac{w_h/w_b}{w_b/w_h} \right)^{(k+N+0.5(1-\alpha))/(2N+1)} \\ w_k &= w_b \cdot \left(\frac{w_h/w_b}{w_b/w_h} \right)^{(k+N+0.5(1+\alpha))/(2N+1)} \\ K &= w_h^\alpha \end{aligned} \quad (11)$$

In these expressions, $(2N + 1)$ is the order of the filter and w_b and w_h are respectively the low and high transient-frequencies.

In the following, some properties of the Caputos definition of fractional order derivatives that will be used in this paper are given. The below desirable properties are valid under causality and when the function is differ-integrated taking as starting point the point when the function starts [24]:

- Fractional order derivative of the fractional order integration of the function $f(t)$:

$${}_aD_t^\alpha ({}_aD_t^{-\alpha} f(t)) = f(t) \quad (12)$$

- Fractional order integration of the fractional order derivative of the function $f(t)$:

$${}_aD_t^{-\alpha} ({}_aD_t^\alpha f(t)) = f(t) - \sum_{k=0}^{m-1} \frac{f^k(a)}{k!} (t-a)^k \quad (13)$$

- The fractional order derivative is a linear operator:

$${}_aD_t^\alpha (f(t) + g(t)) = {}_aD_t^\alpha f(t) + {}_aD_t^\alpha g(t) \quad (14)$$

- The fractional order integration is a linear operator:

$${}_aD_t^{-\alpha} (f(t) + g(t)) = {}_aD_t^{-\alpha} f(t) + {}_aD_t^{-\alpha} g(t) \quad (15)$$

3. SYSTEM DESCRIPTION AND CONTROL DESIGN

3.1. System description

Consider the single-input two-output non-linear system, which can be represented in the following state space form:

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= f_1(x) + b_1(x)u + d_1(t) \\ \dot{x}_3 &= x_4 \\ \dot{x}_4 &= f_2(x) + b_2(x)u + d_2(t)\end{aligned}\quad (16)$$

Where $X = [x_1, x_2, x_3, x_4]^T$ is the state vector, $f_1(x)$, $f_2(x)$ and $b_1(x)$, $b_2(x)$ are nonlinear functions, u is the control input, $d_1(t)$, $d_2(t)$ are bounded external disturbances. Moreover assume that $y = [x_1, x_3]^T$ is the output vector.

Assumption 1: The bounded external disturbances satisfy the following inequalities:

$$|d_1(t)| \leq \delta_1 \quad (17)$$

$$|d_2(t)| \leq \delta_2 \quad (18)$$

$$\left| D_t^{(\alpha-1)} d_1(t) \right| \leq \psi_1 \quad (19)$$

$$\left| D_t^{(\alpha-1)} d_2(t) \right| \leq \psi_2 \quad (20)$$

Where δ_1 , δ_2 , ψ_1 and ψ_2 are known positive constants.

3.2. Sliding Mode Controller (SMC) Design

The principle of the proposed methodology to design the SMC for system (16) is the following:

- Decouple the global system into two subsystems. The first one contains the states x_1 , x_2 , and a sliding surface $S_1 = \dot{e}_1 + \lambda_1 e_1$ is defined for it, where $e_1 = x_1 - x_{1d}$ and λ_1 is a positive constant. The second subsystem contains the states x_3 , x_4 , and a sliding surface $S_2 = \dot{e}_3 + \lambda_2 e_3$ is also defined for it, where $e_3 = x_3 - x_{3d}$ and λ_2 is another positive constant. Note that the control objective is to force a motion of the states of the first subsystem towards the sliding surface $S_1 = 0$, converging therefore to $x_1 = x_{1d}$, $x_2 = \dot{x}_{1d}$. The second objective is to force a motion of the states of the second subsystem towards the sliding surface $S_2 = 0$, converging therefore to $x_3 = x_{3d}$, $x_4 = \dot{x}_{3d}$.

- The use of a control signal $u = u_1$ calculated from the sliding surface S_1 causes the convergence of only the states x_1 , x_2 to their desired values. And the use of a control signal $u = u_2$ calculated from the sliding surface S_2 causes the convergence of only the states x_3 , x_4 to their desired values. In order to achieve simultaneous control of all the states, we take into account the idea of [8] that consists in using an intermediate variable z between the sliding surfaces. This variable represents the information transferred from S_2 to S_1 , and saturates the error e_1 to k_2 . Thus the sliding surface S_1 is modified to

$$S_1 = \dot{e}_1 + \lambda_1 \cdot (e_1 - z) \quad (21)$$

While the sliding surface S_2 keeps its standard form

$$S_2 = \dot{e}_3 + \lambda_2 \cdot e_3 \quad (22)$$

- This modification changes the control objective from making $X = X_d = [x_{1d}, x_{2d}, x_{3d}, x_{4d}]^T$ to making $X = \hat{X}_d = [x_{1d} + z, x_{2d}, x_{3d}, x_{4d}]^T$ where

$$z = \text{sat}(S_2/\phi_2) \cdot k_2, \quad 0 < k_2 < 1 \quad (23)$$

And the definition of the $\text{sat}(\cdot)$ function is:

$$\text{sat}(S_2/\phi_2) = \begin{cases} (S_2/\phi_2) & \text{if } |S_2/\phi_2| < 1 \\ \text{sgn}(S_2/\phi_2) & \text{if } |S_2/\phi_2| \geq 1 \end{cases} \quad (24)$$

Being ϕ_2 is the boundary layer of the sliding surface S_2 .

Remark: If $S_1 = 0$, then we obtain from equation (21) that $x_1 = x_{1d} + z$ and $x_2 = \dot{x}_{1d}$. On the other hand, if $S_2 \neq 0$, equation (23) shows that then we have $z \neq 0$. Consequently, we must pursue that the control system

decreases the value of S_2 , which implies that the value of z decreases too. In such case, if $z \rightarrow 0$ and $S_1 \rightarrow 0$ too, we would have that $x_1 \rightarrow x_{1d}$. In summary, we can state that when $S_2 \rightarrow 0$ and $S_1 \rightarrow 0$, then $x_3 \rightarrow x_{3d}$, $z \rightarrow 0$ and $x_1 \rightarrow x_{1d}$, and the control objectives would be achieved.

Keeping the system states (x_1, x_3) on the sliding surfaces $S_1, S_2, \forall t > 0$ guarantees that the tracking errors vector (e_1, e_3) asymptotically approaches to zero. The corresponding sliding condition is [10]:

$$\begin{cases} V = \frac{1}{2}S_1^2 \geq 0 \\ \dot{V} = S_1\dot{S}_1 \leq 0 \end{cases} \quad (25)$$

The general control structure that satisfies the stability condition of the sliding motion can be written as:

$$u = u_{eq} + u_{sw} \quad (26)$$

Where u_{eq} is called the equivalent control law that is derived by setting $\dot{S}_1 = 0$ and u_{sw} is the switching control law.

Taking the time derivative of (21) gives:

$$\begin{aligned} \dot{S}_1 &= \ddot{e}_1 + \lambda_1(\dot{e}_1 - \dot{z}) \\ &= (\ddot{x}_1 - \ddot{x}_{1d}) + \lambda_1(\dot{e}_1 - \dot{z}) \\ &= (f_1(x) + b_1(x)u + d_1 - \ddot{x}_{1d}) + \lambda_1(\dot{e}_1 - \dot{z}) \end{aligned} \quad (27)$$

Where, \dot{z} is given as follows:

$$\dot{z} = \begin{cases} \frac{k_2}{\phi_2} \cdot \dot{S}_2 & \text{if } \left| \frac{S_2}{\phi_2} \right| < 1 \\ 0 & \text{if } \left| \frac{S_2}{\phi_2} \right| \geq 1 \end{cases} \quad (28)$$

And:

$$\begin{aligned} \dot{S}_2 &= \ddot{e}_3 + \lambda_2 \cdot \dot{e}_3 \\ &= (\ddot{x}_3 - \ddot{x}_{3d}) + \lambda_2 \cdot \dot{e}_3 \\ &= (f_2(x) + b_2(x)u + d_2 - \ddot{x}_{3d}) + \lambda_2 \cdot \dot{e}_3 \end{aligned} \quad (29)$$

Substituting equations (29), and (28) into (27), and setting $\dot{S}_1 = 0$ in this last equation, the equivalent control is obtained:

$$u_{eq} = \frac{-1}{(b_1 - \lambda_1 \frac{k_2}{\phi_2} b_2)} [f_1 - \ddot{x}_{1d} - \lambda_1 \frac{k_2}{\phi_2} \cdot (f_2 - \ddot{x}_{3d}) + (\lambda_1 \cdot \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3)] \quad (30)$$

Then the global control input u is given by the expression:

$$u = \frac{-1}{(b_1 - \lambda_1 \frac{k_2}{\phi_2} b_2)} [f_1 - \ddot{x}_{1d} - \lambda_1 \frac{k_2}{\phi_2} \cdot (f_2 - \ddot{x}_{3d}) + (\lambda_1 \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3) + (k_1 \cdot \text{sgn}(\frac{S_1}{\phi_1}))] \quad (31)$$

where k_1 is a positive constant and ϕ_1 is the boundary layer of the sliding surface S_1 . Substituting (31) into (27) yields

$$\begin{aligned} \dot{S}_1 &= \left(d_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot d_2 \right) - k_1 \text{sgn}(\frac{S_1}{\phi_1}) \\ &\leq \left(\delta_1 \cdot \text{sgn}(\frac{S_1}{\phi_1}) - \lambda_1 \frac{k_2}{\phi_2} \cdot \delta_2 \cdot \text{sgn}(\frac{S_1}{\phi_1}) \right) - k_1 \cdot \text{sgn}(\frac{S_1}{\phi_1}) \end{aligned} \quad (32)$$

Then simply:

$$S_1 \dot{S}_1 \leq \phi_1 \cdot \left(\delta_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot \delta_2 - k_1 \right) \cdot \left| \frac{S_1}{\phi_1} \right| \quad (33)$$

From Eq(33) it can be concluded that the reaching condition is obtained from $k_1 > (\delta_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot \delta_2)$.

But, Eq(31) will have high-frequency switching near the sliding surface ($S_1 = 0$) due to the sgn function involved. Thus, in order to reduce the chattering phenomenon, we replace $\text{sgn}(S_1/\phi_1)$ by $\text{sat}(S_1/\phi_1)$ as follows:

$$u = \frac{-1}{(b_1 - \lambda_1 \frac{k_2}{\phi_2} b_2)} [f_1 - \ddot{x}_{1d} - \lambda_1 \frac{k_2}{\phi_2} \cdot (f_2 - \ddot{x}_{3d}) + (\lambda_1 \cdot \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3) + (k_1 \cdot \text{sat}(\frac{S_1}{\phi_1}))] \quad (34)$$

3.3. Fractional Order Sliding Mode Controller (FOSMC) Design

In this section we will develop a fractional-order sliding mode control for trajectory tracking of the system of Eq(16). For this purpose, the forms introduced in the previous section are used.

Let the two sliding surfaces to be defined as follows:

$$S_1 = D_t^\alpha e_1 + \lambda_1 \cdot (e_1 - z) \quad (35)$$

$$S_2 = D_t^\alpha e_3 + \lambda_2 \cdot e_3 \quad (36)$$

With respect the property of Caputos derivative $D_t^\alpha(f(t)) = D_t^{(\alpha-m)} \frac{d^m}{dt^m}(f(t))$, S_1 and S_2 can be rewritten as :

$$S_1 = D_t^{(\alpha-1)} \dot{e}_1 + \lambda_1 \cdot (e_1 - z) \quad (37)$$

$$S_2 = D_t^{(\alpha-1)} \dot{e}_3 + \lambda_2 \cdot e_3 \quad (38)$$

Taking derivative of both sides of Eq(37) with respect to time, we have.

$$\begin{aligned} \dot{S}_1 &= D_t^{(\alpha-1)} \ddot{e}_1 + \lambda_1 \cdot (\dot{e}_1 - \dot{z}) \\ &= D_t^{(\alpha-1)} (\ddot{x}_1 - \ddot{x}_{1d}) + \lambda_1 \cdot (\dot{e}_1 - \dot{z}) \\ &= D_t^{(\alpha-1)} (f_1(x) + b_1(x)u + d_1 - \ddot{x}_{1d}) + \lambda_1 \cdot (\dot{e}_1 - \dot{z}) \end{aligned} \quad (39)$$

Where, \dot{z} has the same form as in Eq(28), and:

$$\begin{aligned} \dot{S}_2 &= D_t^{(\alpha-1)} \ddot{e}_3 + \lambda_2 \cdot \dot{e}_3 \\ &= D_t^{(\alpha-1)} (\ddot{x}_3 - \ddot{x}_{3d}) + \lambda_2 \cdot \dot{e}_3 \\ &= D_t^{(\alpha-1)} (f_2(x) + b_2(x)u + d_2 - \ddot{x}_{3d}) + \lambda_2 \cdot \dot{e}_3 \end{aligned} \quad (40)$$

By setting $\dot{S}_1 = 0$ and respect the properties of fractional derivative given in section II; the equivalent control is obtained and it has the flowing formula:

$$u_{eq} = \frac{-1}{(b_1 - \lambda_1 \frac{k_2}{\phi_2} b_2)} [f_1 - \ddot{x}_{1d} - \lambda_1 \frac{k_2}{\phi_2} \cdot (f_2 - \ddot{x}_{3d}) + D_t^{(1-\alpha)} (\lambda_1 \cdot \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3)] \quad (41)$$

Then the global control input u is given by:

$$u = \frac{-1}{(b_1 - \lambda_1 \frac{k_2}{\phi_2} b_2)} [f_1 - \ddot{x}_{1d} - \lambda_1 \frac{k_2}{\phi_2} \cdot (f_2 - \ddot{x}_{3d}) + D_t^{(1-\alpha)} (\lambda_1 \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3) + D_t^{(1-\alpha)} (k_1 \cdot \text{sgn}(\frac{S_1}{\phi_1}))] \quad (42)$$

Where u_{sw} is given by its proper formula in Eq(42) to satisfy the existence condition of sliding mode. For the stability condition, substituting Eq(42) into Eq(39); results in:

$$\begin{aligned} \dot{S}_1 &= -D_t^{(\alpha-1)} D_t^{(1-\alpha)} (\lambda_1 \cdot \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3) - D_t^{(\alpha-1)} D_t^{(1-\alpha)} (k_1 \cdot \text{sgn}(\frac{S_1}{\phi_1})) + (\lambda_1 \cdot \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3) \\ &\quad + D_t^{(\alpha-1)} d_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot D_t^{(\alpha-1)} d_2 \end{aligned} \quad (43)$$

Taking into account the property of Caputos derivative ${}_a D_t^{-\alpha} ({}_a D_t^\alpha f(t)) = f(t) - \sum_{k=0}^{m-1} \frac{f^{(k)}(a)}{k!} (t-a)^k$, where $m = 1$.

This lets us have:

$$\dot{S}_1 = -k_1 \cdot (\text{sgn}(\frac{S_1}{\phi_1})) + k_1 \cdot (\text{sgn}(\frac{S_1(0)}{\phi_1})) + (\lambda_1 \cdot \dot{e}_1(0) - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3(0)) + D_t^{(\alpha-1)} d_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot D_t^{(\alpha-1)} d_2 \quad (44)$$

If one assume that $k_1 \cdot (\text{sgn}(\frac{S_1(0)}{\phi_1})) + (\lambda_1 \dot{e}_1(0) - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \dot{e}_3(0)) = 0$, Eq (44) will be:

$$\begin{aligned}\dot{S}_1 &= -k_1(\operatorname{sgn}(\frac{S_1}{\phi_1})) + D_t^{(\alpha-1)}d_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot D_t^{(\alpha-1)}d_2 \\ &= -k_1(\operatorname{sgn}(\frac{S_1}{\phi_1})) + \psi_1(\operatorname{sgn}(\frac{S_1}{\phi_1})) - \lambda_1 \frac{k_2}{\phi_2} \cdot \psi_2(\operatorname{sgn}(\frac{S_1}{\phi_1}))\end{aligned}\quad (45)$$

Then simply:

$$S_1 \dot{S}_1 \leq \phi_1 \cdot \left(\psi_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot \psi_2 - k_1 \right) \cdot \left| \frac{S_1}{\phi_1} \right| \quad (46)$$

From Eq(46) the reaching condition can be obtained from $k_1 \succ (\psi_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot \psi_2)$.

Otherwise, if $\left| k_1 \cdot (\operatorname{sgn}(\frac{S_1(0)}{\phi_1})) + (\lambda_1 \dot{e}_1(0) - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \dot{e}_3(0)) \right| \prec \xi \prec \infty$, this lets us have:

$$S_1 \dot{S}_1 \leq \phi_1 \cdot \left(\psi_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot \psi_2 - k_1 + \xi \right) \cdot \left| \frac{S_1}{\phi_1} \right| \quad (47)$$

For $k_1 \succ (\psi_1 - \lambda_1 \frac{k_2}{\phi_2} \cdot \psi_2 + \xi)$ then reaching condition of Eq(25) is also valid. Eq(48) represent the control input with sat function to avoid the problem of chattering.

$$u = \frac{-1}{(b_1 - \lambda_1 \frac{k_2}{\phi_2} b_2)} \left[f_1 - \ddot{x}_{1d} - \lambda_1 \frac{k_2}{\phi_2} \cdot (f_2 - \ddot{x}_{3d}) + D_t^{(1-\alpha)}(\lambda_1 \cdot \dot{e}_1 - \lambda_1 \lambda_2 \frac{k_2}{\phi_2} \cdot \dot{e}_3) + D_t^{(1-\alpha)}(k_1 \cdot \operatorname{sat}(\frac{S_1}{\phi_1})) \right] \quad (48)$$

Figure 1 summarizes the proposed FOSMC for a single-input two output non-linear system.

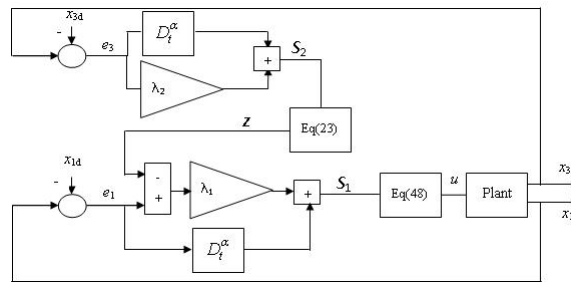


Figure 1. Scheme of proposed FOSMC

4. SIMULATION RESULTS

In this section, we shall demonstrate that the proposed FOSMC is applicable to the problem of trajectory tracking of single input two output (SITO) system described in Eq (16) in order to verify the theoretical development by using Matlab/simulink tools. We choose as example, the single-inverted pendulum system.

The structure of a single-inverted pendulum is illustrated in figure 2 and its dynamic is described below (Eq 49):

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= \frac{m_t g \sin x_1 - m_p L \sin x_1 \cos x_1 \cdot x_2^2}{L(\frac{4}{3}m_t - m_p \cos^2 x_1)} + \frac{\cos x_1}{L(\frac{4}{3}m_t - m_p \cos^2 x_1)} u + d \\ \dot{x}_3 &= x_4 \\ \dot{x}_4 &= \frac{\frac{4}{3}m_p L x_2^2 \sin x_1 + m_p g \sin x_1 \cos x_1}{\frac{4}{3}m_t - m_p \cos^2 x_1} + \frac{4}{3(\frac{4}{3}m_t - m_p \cos^2 x_1)} u + d\end{aligned}\quad (49)$$

And assuming that the control signal u and the external disturbance d are as follows:

$$\begin{aligned}d(t) &= 0.05 \sin(t) \\ \max(abs(u)) &\leq 10N\end{aligned}\quad (50)$$

Where $x_1 = \theta$, the angle of the pole with respect to the vertical axis, $x_2 = \dot{\theta}$ the angle velocity of the pole with respect to the vertical axis; $x_3 = x$, the position of the cart; $x_4 = \dot{x}$, the velocity of the cart.

Due to its behaviour, the trajectory tracking problem for this system is generally carried for x_3 and save the verticality of the pole ($x_1=0$); in our study we have discussed the following two cases:

Case 1: the both desired states x_{1d} and x_{3d} are set to 0.

Case 2: the desired states x_{1d} and x_{3d} are set to 0 and $x_{3d}(t) = 0.3 \sin(\frac{\pi t}{25})$ respectively.

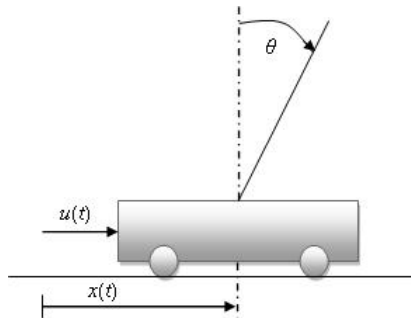


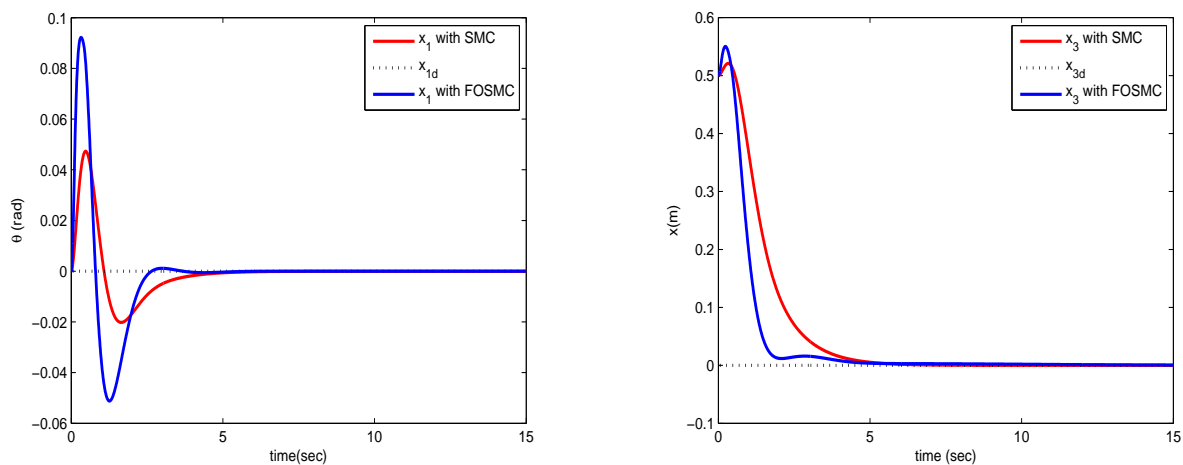
Figure 2. Single-inverted pendulum system

For the simulation, the initial conditions are set to $[x_{10}, x_{20}, x_{30}, x_{40}] = [0, 0, 0.5, 0]$, and the following specifications are used:

- For inverted pendulum system: $m_p = 0.1\text{kg}$, $m_c = 1\text{kg}$, $L = 0.5\text{m}$, $g = 9.81\text{m/s}^2$, $m_t = m_c + m_p$.

- As given below, the parameters of both SMC and FOSMC are equivalent (but for FOSMC we have $\alpha=0.56$)
 $\lambda_1 = 1.05$, $\lambda_2 = 1.05$, $\phi_1 = 0.24$, $\phi_2 = 0.95$, $k_1 = 0.91$, $k_2 = 0.35$

The simulation results are given by figures 3 to 10.



a)

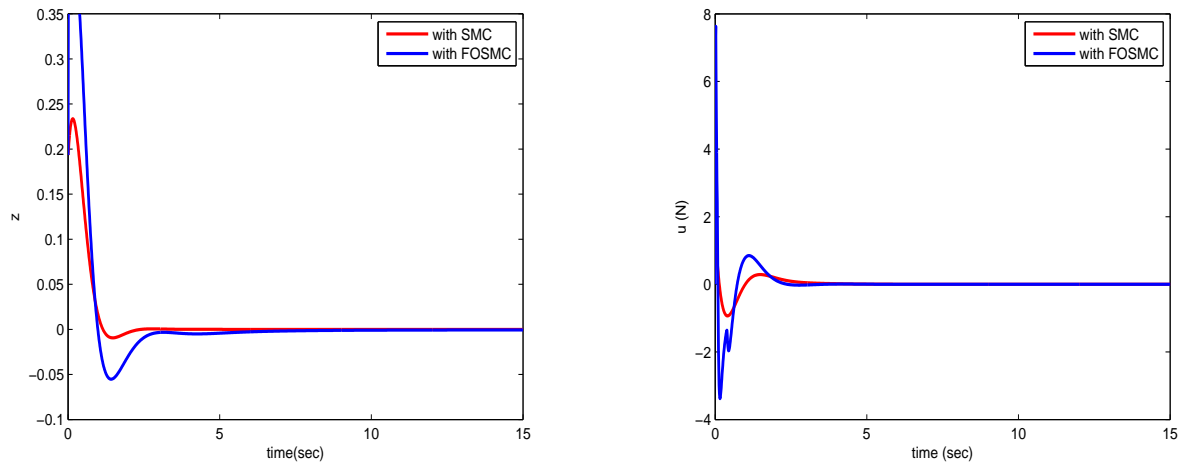
b)

Figure 3. Simulation results of case 1 without any disturbance, a) Angle evolution θ , b) displacement x

It can be seen from figures, that x_1 and x_3 converge respectively to the desired trajectories x_{1d} and x_{3d} . Also, the convergence of these states using the proposed FOSMC is faster than that of classical SMC, this is obtained under considerable magnitude of x_1 and control signal (u) in the transition state for the first one. With adding external disturbance, the system is still stable.

5. CONCLUSION

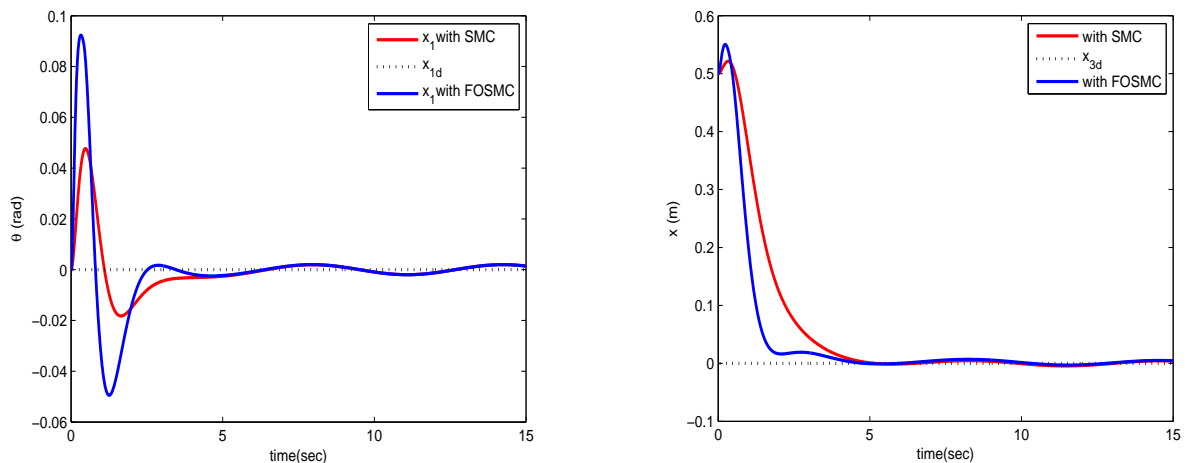
In this paper a sliding mode control scheme based on fractional order calculus was proposed for a class of non-linear systems, which is characterized by a single input and two outputs (SITO). The proposed approach used two fractional order sliding surfaces with intermediate variable between them; in which the control law was calculated to control the two system outputs. The Lyapunov theorem is used to prove the stability condition. Finally the simulation



a)

b)

Figure 4. Simulation results of case 1 without any disturbance, a) intermediate variable z , b) control signal u



a)

b)

Figure 5. Simulation results of case 1 with adding external disturbance, a) Angle evolution θ , b) displacement x

for inverted pendulum system have shown that the proposed FOSMC give the best control specification compared with the conventional one based on integer order.

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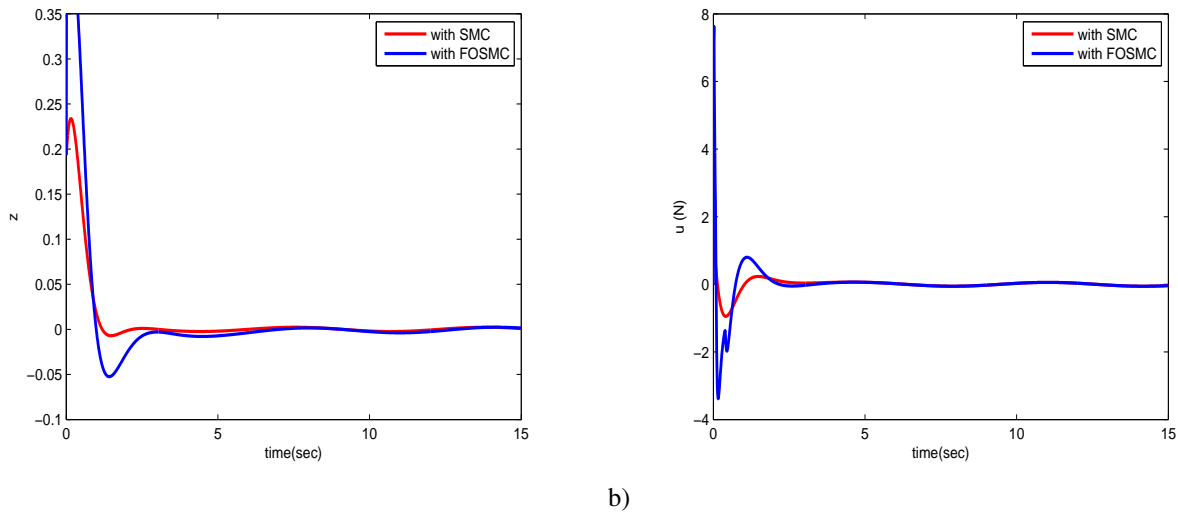


Figure 6. Simulation results of case 1 with adding external disturbance, a) intermediate variable z , b) control signal u

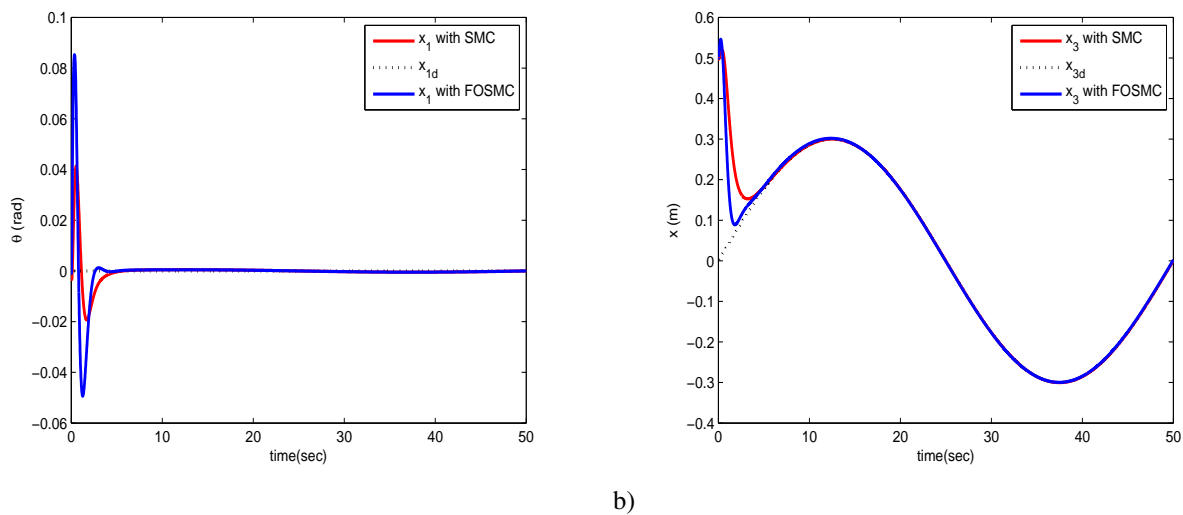
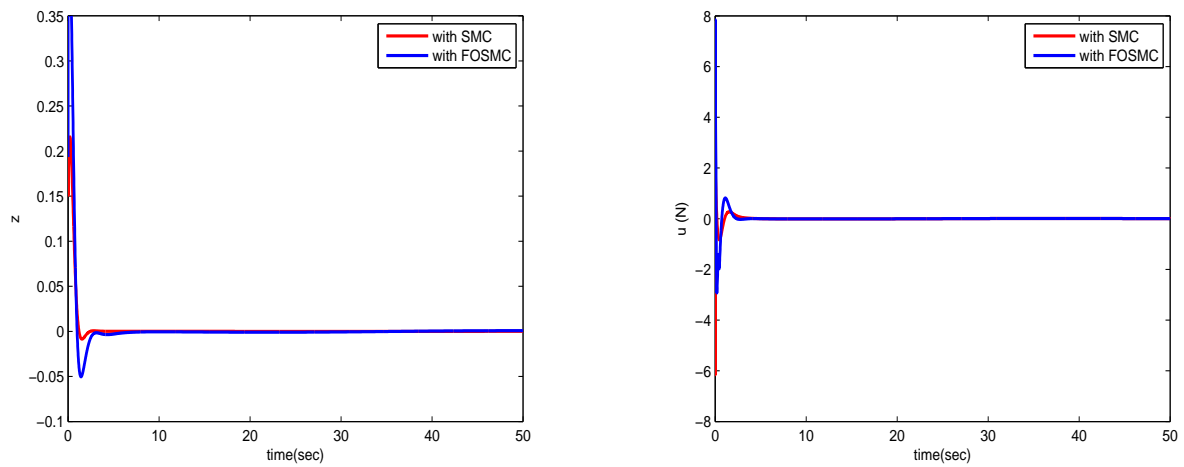


Figure 7. Simulation results of case 2 without any disturbance, a) Angle evolution θ , b) displacement x

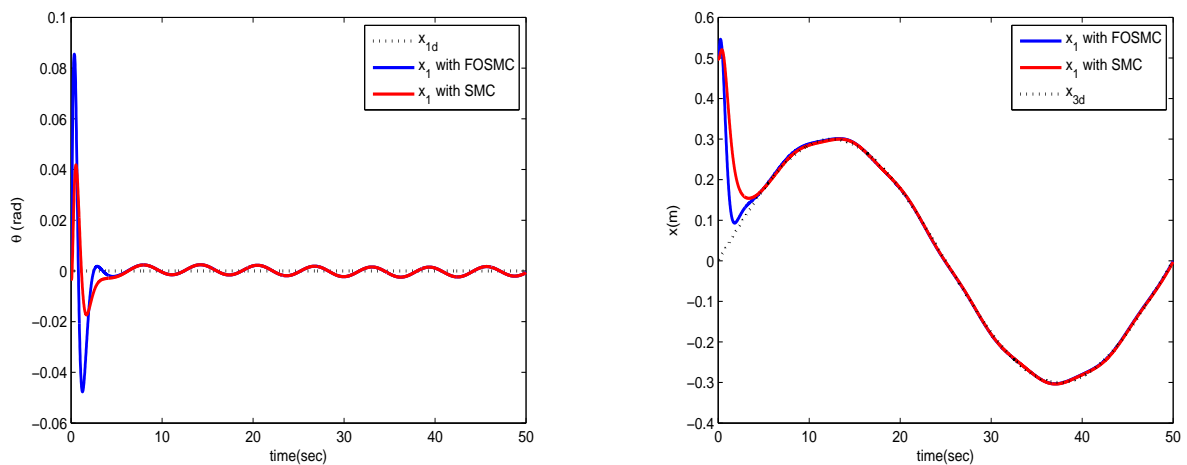
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a)

b)

Figure 8. Simulation results of case 2 without any disturbance, a) intermediate variable z , b) control signal u



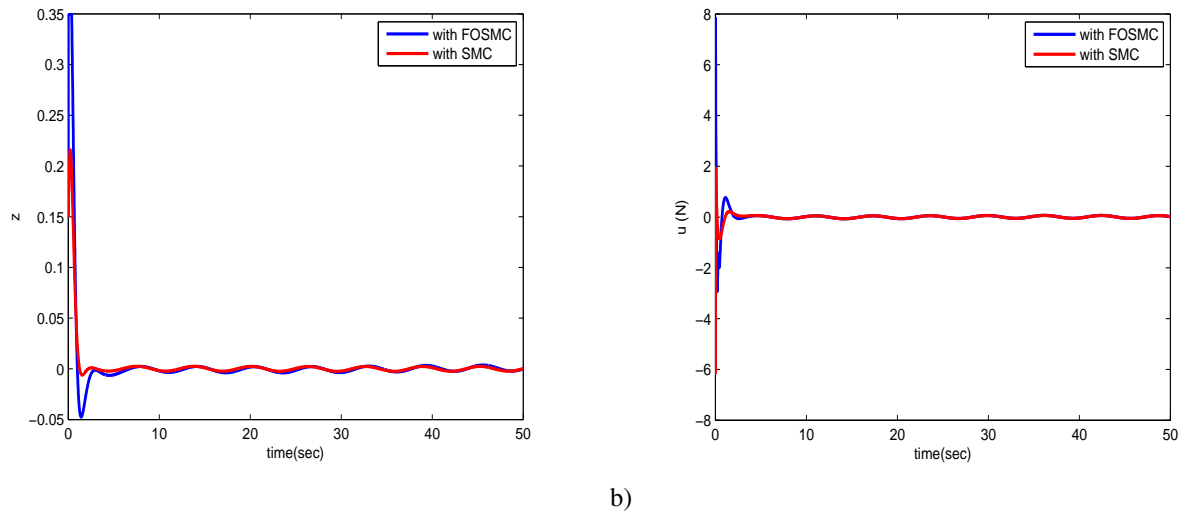
a)

b)

Figure 9. Simulation results of case 2 with adding external disturbance, a) Angle evolution θ , b) displacement x

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a) b)
Figure 10. Simulation results of case 2 with adding external disturbance, a) intermediate variable z , b) control signal u

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