## Short communication

# On the stress tensor in Vrancea region 

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## Introduction

Vrancea region (Romania) is a complex tectonic zone characterized by a clustered but intense intermediate-depth seismic activity and by a 'continent-continent-like' collision between three tectonic units (East-European Platform, Moesian Sub-plate and Inter-Alpine Sub-plate) which leads also to moderate-size crustal earthquakes. Both crustal and sub-crustal events present some diversity in focal mechanisms that made early seismotectonic interpretation difficult (Roman, 1970; Ritsema, 1974).

As was shown by McKenzie (1969), if there are preexisting zones of weakness on which slip can occur, the directions of the principal stresses $\sigma_{1}, \sigma_{2}, \sigma_{3}$ may not be close to the $P, B$ and $T$ axes from focal mechanisms. In such cases, only the direction and sense of resolved shear stress on the fault plane, as indicated by the slip vector, can be used to constrain the stresses. Assuming that the variety of focal mechanisms are consistent with a single regional stress tensor, Gephart and Forsyth (1984) developed a new inverse technique to seek a uniform stress field that predicts directions and senses of slip in agreement with the observations.

The aim of this short note is (1) to present a new application of this attractive method, (2) to point out that in Vrancea region the compression axis acts in a NE-SW direction and not in a SE-NW direction, as is commonly thought from focal mechanism results, and (3) to give additional evidence that the stresses in the crust are decoupled from those in the subducted slab.

## Method and data

Gephart and Forsyth (1984) chose to describe the deviatoric part of the model stress tensor by four independent parameters, the directions of the principal stress axes $\sigma_{1}<\sigma_{2}<\sigma_{3}$ and the ratio $R=\left(\sigma_{2}-\sigma_{1}\right) /\left(\sigma_{3}-\sigma_{1}\right)$, thus dealing only with shear-stress directions on the fault planes and neglecting shear-stress magnitudes and hydrostatic stress. This parameterization is particularly useful for data sets for which $P$ and $T$ axes from focal mechanism (principal strain axes) are not well clustered. The ratio $R$ specifies the magnitude of $\sigma_{2}$ relative to $\sigma_{1}$ and $\sigma_{3}$, and is defined between 0 and 1, both situations describing a bi-axial stress state.

The inversion is performed by a grid search over the three stress directions (characterized by three independent angles) and $R$, looking for the minimization of the sum of absolute values of the rotation angles about any axis needed to bring the observed and predicted slip direction and senses into coincidence. When the fault plane is not known 'a priori', there are two rotation angles for the two nodal planes. Thus, in performing the inversion, one selects the plane that is more consistent with the stress model. The inversion is performed in two steps: first, the whole stress model space is searched, on a $10^{\circ}-15^{\circ}$ grid for angles and 0.1 units for $R$, using an approximate method (the rotation axes were pre-specified to be the poles of the two nodal planes and the null vector); second, the exact method (with the much more time-consuming determination of the minimum rotation axes) was applied in the vicinity of the isolated minima.

The data set consists of two sub-sets: one is formed by 27 intermediate-depth earthquakes (see Table 1) which occurred between 1934 and 1986 with magnitudes in the range $5.0 \leq M \leq 7.4$ (with one exception, and $M 4.0$ event on May 16, 1982 at about 200 km depth); the other sub-set is formed by 12 crustal events (see Table 2) which occurred between 1959 and 1986 with $4.0 \leq M \leq 5.4$ (with one exception, an M3.0 event on April 27, 1986 in Vrancea foredeep). The first sub-set consists of fault-plane solutions obtained with a minimum of 20 and an average of $65 P$-wave first motion signs (Fig. 1); the solutions of the second sub-set were obtained with a minimum of 15 and an average of 39 signs (Fig. 2). The fault-plane solutions were determined with short-period $P$-wave first motion signs with good azimuthal coverage using a grid search of all possible orientations of the two nodal planes and finally inspecting the first ten top-score solutions that best separate dilatational from compressional quadrants. The input data were taken from national, international or station bulletins, except for the March 4, 1977 main event whose solution was not redetermined and corresponds to shock $E_{1}$ from Räkers and Müller (1982).

## Results

## Intermediate-depth earthquakes

After searching the stress model space in two steps, we found the best-fitting model presented in Fig. 3, with relative values of principal stresses $\sigma_{1}=-0.67 \sigma_{3}$ and $\sigma_{2}=-$

Table 1. Intermediate-depth earthquakes used in this study. $\gamma$ is the smallest misfit angle for the two nodal planes, and $\varphi_{s}$ and $\delta$ are their strike and dip angles, respectively

| No. | Date | Origin time | Lat.N <br> $\left({ }^{\circ}\right)$ | Lon.E <br> $\left({ }^{\circ}\right)$ | $h$ (km) | M | Nodal planes |  |  |  |  | Source ${ }^{\text {a }}$ | No. of $P$ sings | Score <br> (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | $\begin{aligned} & \varphi_{s} \\ & \left({ }^{\circ}\right) \end{aligned}$ | $\begin{aligned} & \delta \\ & \left({ }^{\circ}\right) \end{aligned}$ | $\begin{aligned} & \|\gamma\| \\ & \left({ }^{\circ}\right) \end{aligned}$ |  |  |  |
| 1 | 340329 | 20:06 | 45.8 | 26.5 | 90 | 6.2 | 200 | 66 | 317 | 45 | 4 | $\mathrm{RO}^{\prime} 80$ | 33 | 97 |
| 2 | 400624 | 09:17 | 45.9 | 26.6 | 115 | 5.5 | 220 | 58 | 32 | 32 | 1 | RO'80 | 27 | 100 |
| 3 | 401022 | 06:37 | 45.8 | 26.4 | 122 | 6.5 | 223 | 61 | 49 | 30 | 3 | RO'80 | 57 | 97 |
| 4 | 401110 | 01:39 | 45.8 | 26.7 | 133 | 7.4 | 224 | 62 | 73 | 31 | 8 | RO'80 | 58 | 93 |
| 5 | 450907 | 15:48 | 45.9 | 26.5 | 75 | 6.5 | 224 | 60 | 39 | 30 | 0 | $\mathrm{RO}^{\prime} 80$ | 30 | 93 |
| 6 | 451209 | 06:08 | 45.7 | 26.8 | 80 | 6.0 | 134 | 63 | 359 | 36 | 24 | $\mathrm{RO}^{\prime} 80$ | 24 | 96 |
| 7 | 480529 | 04:48 | 45.8 | 26.5 | 140 | 5.7 | 196 | 48 | 25 | 42 | 1 | RO'80 | 33 | 91 |
| 8 | 550501 | 21:22 | 45.5 | 26.3 | 135 | 5.4 | 103 | 51 | 347 | 61 | 22 | RO'80 | 28 | 86 |
| 9 | 600126 | 20:27 | 45.8 | 26.8 | 140 | 5.0 | 155 | 32 | 332 | 58 | 2 | RO'80 | 53 | 83 |
| 10 | 601013 | 02:21 | 45.7 | 26.4 | 160 | 5.5 | 163 | 40 | 343 | 50 | 5 | RO'80 | 47 | 89 |
| 11 | 630114 | 18:33 | 45.7 | 26.6 | 133 | 5.4 | 146 | 36 | 326 | 54 | 2 | RO'80 | 54 | 80 |
| 12 | 650110 | 02:52 | 45.8 | 26.6 | 120 | 5.4 | 348 | 50 | 156 | 41 | 9 | RO'80 | 54 | 83 |
| 13 | 661015 | 06:59 | 45.6 | 26.4 | 140 | 5.1 | 134 | 84 | 286 | 7 | 3 | RO'80 | 39 | 80 |
| 14 | 730820 | 15:18 | 45.7 | 26.5 | 73 | 5.5 | 262 | 23 | 27 | 80 | 11 | RO'80 | 49 | 82 |
| 15 | 731023 | 10:50 | 45.7 | 26.5 | 170 | 5.1 | 117 | 56 | 331 | 39 | 5 | RO'80 | 34 | 82 |
| 16 | 740717 | 05:09 | 45.8 | 26.5 | 145 | 5.4 | 216 | 26 | 82 | 72 | 21 | RO'80 | 55 | 84 |
| 17 | 761001 | 17:50 | 45.7 | 26.5 | 146 | 5.5 | 169 | 43 | 333 | 48 | 2 | RO'80 | 85 | 85 |
| 18 | 770304 | 19:21 | 45.8 | 26.8 | 93 | 5.0 | 275 | 78 | 78 | 12 | 8 | RO'80 | 61 | 87 |
| 19 | 770304 | 19:26 | 45.8 | 26.8 | 93 | 7.2 | 238 | 76 | 8 | 21 | 10 | RM'82 | 78 | 99 |
| 20 | 781002 | 20:28 | 45.7 | 26.7 | 140 | 5.3 | 131 | 34 | 316 | 56 | 5 | RO'80 | 108 | 85 |
| 21 | 790531 | 07:28 | 45.6 | 26.4 | 120 | 5.4 | 233 | 80 | 124 | 27 | 5 | RO'80 | 89 | 83 |
| 22 | 790911 | 15:36 | 45.6 | 26.5 | 158 | 5.4 | 210 | 13 | 12 | 77 | 2 | RO'80 | 100 | 87 |
| 23 | 810718 | 00:03 | 45.7 | 26.4 | 146 | 5.3 | 184 | 46 | 92 | 88 | 15 | RCO'81 | 106 | 78 |
| 24 | 820516 | 04:03 | 45.4 | 26.4 | 201 | 4.0 | 206 | 81 | 298 | 75 | 15 | $\mathrm{RO}^{\prime} 82$ | 20 | 82 |
| 25 | 830125 | 07:34 | 45.7 | 26.7 | 156 | 5.3 | 84 | 50 | 323 | 58 | 18 | This paper | 72 | 86 |
| 26 | 850801 | 14:35 | 45.8 | 26.5 | 107 | 5.3 | 200 | 76 | 298 | 61 | 0 | OA'85 | 86 | 86 |
| 27 | 860830 | 21:28 | 45.5 | 26.5 | 134 | 6.8 | 235 | 65 | 73 | 24 | 5 | RO'87 | 232 | 87 |

${ }^{\text {a }} R O^{\prime} 80$ Radu and Oncescu (1980); $R M^{\prime} 82$ Räkers and Müller (1982); $R C^{\prime} O^{\prime} 81$ Radu et al. (1981); $R O^{\prime} 82$ Radu and Oncescu (1982); $O A^{\prime} 85$ Oncescu and Apolozan (1985); $R O^{\prime} 87$ Radu and Oncescu (1987)

Table 2. Crustal earthquakes used in this study. $\gamma$ is the smallest misfit angle for the two nodal planes, and $\varphi_{s}$ and $\delta$ are their strike and dip angles, respectively

| No. | Date | Origin time | Lat.N <br> $\left({ }^{\circ}\right)$ | Lon.E <br> $\left({ }^{\circ}\right)$ | $h$$(\mathrm{km})$ | M | Nodal planes |  |  |  |  | Source ${ }^{\text {a }}$ | No. of $P$ signs | Score <br> (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | $\begin{aligned} & \delta \\ & \left({ }^{\circ}\right) \end{aligned}$ | $\begin{aligned} & \varphi_{s} \\ & \left({ }^{\circ}\right) \end{aligned}$ | $\begin{aligned} & \delta \\ & \left({ }^{\circ}\right) \end{aligned}$ | $\begin{aligned} & \|\gamma\| \\ & \left({ }^{\circ}\right) \end{aligned}$ |  |  |  |
| 1 | 590531 | 12:15 | 45.7 | 27.2 | 35 | 5.2 | 40 | 17 | 149 | 84 | 24 | $\mathrm{RO}^{\prime} 80$ | 41 | 88 |
| 2 | 600104 | 12:21 | 44.6 | 27.0 | 41 | 5.4 | 138 | 40 | 271 | 60 | 18 | RO'80 | 35 | 74 |
| 3 | 690418 | 20:38 | 45.3 | 25.1 | 10 | 5.2 | 137 | 83 | 231 | 60 | 14 | RO'80 | 38 | 79 |
| 4 | 750208 | 08:21 | 45.1 | 26.0 | 23 | 4.7 | 144 | 74 | 48 | 70 | 12 | RO'80 | 20 | 80 |
| 5 | 750307 | 04:13 | 45.9 | 26.6 | 21 | 5.1 | 237 | 83 | 143 | 60 | 3 | RO'80 | 39 | 77 |
| 6 | 770305 | 00:00 | 45.3 | 27.1 | 10 | 4.3 | 106 | 86 | 13 | 53 | 2 | $\mathrm{RO}^{\prime} 80$ | 20 | 88 |
| 7 | 800911 | 23:24 | 45.4 | 28.2 | 15 | 4.7 | 282 | 89 | 12 | 90 | 8 | RO'80 | 45 | 76 |
| 8 | 801208 | 19:51 | 44.4 | 27.2 | 15 | 4.0 | 331 | 89 | 240 | 45 | 1 | RCO'81 | 23 | 96 |
| 9 | 811113 | 09:07 | 45.2 | 29.0 | 10 | 5.2 | 314 | 57 | 171 | 39 | 4 | RCO'81 | 81 | 73 |
| 10 | 830221 | 18:03 | 45.3 | 27.1 | 19 | 4.5 | 234 | 63 | 18 | 32 | 2 | OA'84 | 20 | 95 |
| 11 | 860427 | 00:04 | 45.5 | 27.1 | 26 | 5.0 | 226 | 44 | 30 | 47 | 2 | OT'87 | 95 | 90 |
| 12 | 860427 | 00:47 | 45.5 | 27.1 | 19 | 3.0 | 294 | 62 | 159 | 37 | 10 | OT'87 | 15 | 93 |

[^0]$0.33 \sigma_{3}\left(\sigma_{2}=0.5 \sigma_{1}\right)$. This model has an average misfit (absolute value of rotation angle about any axis) of $7.7^{\circ}$ with a $95 \%$ confidence limit of $11.6^{\circ}$. If the three events that do not fit the model (with misfits greater than $20^{\circ}$ and marked with a rectangle in Fig. 1) are removed, the average misfit is reduced to $5.3^{\circ}$. Of the other 24 events, 5 have misfits between $10^{\circ}$ and $20^{\circ}$ and the remaining 19 fit the stress model within a few degrees. Errors of only several
degrees are less than the uncertainty of the focal mechanism determinations, which in this case are estimated to be of the order of $10^{\circ}$.

## Crustal events

Again, after searching the stress model space in two steps, we found the best-fitting model presented in Fig. 4, with


Fig. 1. Stereographic projections of the lower hemisphere of faultplane solutions for 27 intermediate-depth earthquakes. Magnitudes are indicated near each solution, as well as the corresponding sequene numbers from Table 1. Within each depth interval the earthquakes are ordered with decreasing magnitude; the first column may be regarded as a variation of maximum magnitude with depth. Thick curves denote identified fault planes (see text)


Fig. 3. Principal stress axes (triangles), individual $P$ axes (open circles) and $T$ axes (full circles) for Vrancea intermediate-depth region. Stereographic projections of the lower hemisphere are used. Contours indicate $95 \%$ confidence regions for $\sigma_{1}$ (dotted line) and $\sigma_{3}$ (solid line) axes
relative values of principal stresses $\sigma_{1}=\sigma_{2}=-0.5 \sigma_{3}$. This model has an average misfit of $8.4^{\circ}$ with a $95 \%$ confidence limit of $17.9^{\circ}$. One event has a misfit greater than $20^{\circ}$; if this one is removed, the average misfit is reduced to $6.3^{\circ}$. Of the remaining 11 events, three have misfits between $10^{\circ}$ and $20^{\circ}$. The uncertainty of focal mechanism determinations for these crustal events is estimated to be about $15^{\circ}-20^{\circ}$, so that the fit seems reasonably good.

## Discussion

On the basis of this analysis we arrive at the following interpretation concerning the intermediate-depth seismic re-


Fig. 2. Stereographic projections of the lower hemisphere of faultplane solutions for 12 crustal earthquakes. The projections are centred on the epicentres, except where otherwise indicated. Thick curves denote identified fault planes (see text). Numbers correspond to those from Table 2


Fig. 4. Same as Fig. 3, but for crustal earthquakes
gion. (1) the minimum compression axis ( $\sigma_{3}$ ) acts vertically, as was observed by all previous investigators. (2) The maximum compression axis $\left(\sigma_{1}\right)$ acts in a NE-SW direction, the direction of the paleo-subduction in Eastern Carpathians, as was pointed out by Bleahu et al. (1973) from volcanological data and by Oncescu et al. (1984) from seismological data. (3) The intermediate stress axis $\left(\sigma_{2}\right)$ has also a negative sign and acts in a SE-NW direction, the direction of $P$ axes of all strong and most moderate earthquakes; it follows that there are pre-existing planes of weakness on which at least strong and moderate events occur, as suggested by Constantinescu and Enescu (1984). On the other hand, small events with the same orientation of the principal strain axes tend to have high values of fracture energy per unit area of the fault (Oncescu, 1986), a feature generally associated with fresh fracture of rocks. The pattern is not very far from a bi-axial state of stress, as was
first observed by Oncescu and Trifu (1987b) from a statistical analysis of principal strain axes of 120 small earthquakes. A cause of compression along the $\sigma_{2}$ axis (SE-NW) could be the advancement of the Black Sea or Moesian platelet. (4) There is no strong requirement that the stresses are heterogeneous; the few events that do not fit the model are of moderate magnitudes and scattered in space. Following Gephart (1985), we tried to discriminate between the two nodal planes exploiting the fact that the null $(B)$ axes from focal mechanisms are generally not parallel to the $\sigma_{2}$ axis. The choice was made only when the differences in misfits were greater than $10^{\circ}$. For two events, the identified fault planes are coincident with those independently determined by Müller et al. (1978) for the March 4, 1977 M7.2 earthquake and by Trifu and Oncescu (1987) for the August 30, 1986 M6.8 earthquake. These two cases give significance to the other fault-plane identifications, so that one can conclude that (5) when the nodal planes strike $\mathrm{NE}-\mathrm{SW}$ the rupture plane is that one dipping toward NW, and when the nodal planes strike NW-SE the rupture planes plane is that one dipping toward SW (with two exceptions, the $M 6.5$ and $M 5.8$ events between 120 and 140 km depth).

As to the crustal earthquakes, we obtained that: (1) the most vertical prinicpal stress is the maximum compression ( $\sigma_{1}$ ) axis. (2) The intermediate stress axis ( $\sigma_{2}$ ) equals the $\sigma_{1}$ axis in magnitude (a pure bi-axial stress state), so that their orientation is difficult to determine. Moreover, it is in this situation that the greatest diversity in nodal plane orientations is observed (Harmsen and Rogers, 1986), a feature that can be noticed from Fig. 2. (3) The stress tensor within the crust appears to be quite homogeneous. (4) The clear difference between the stress tensor within the crust and the stress tensor in the intermediate-depth region supports the hypothesis of the existence of a gravitationally sinking slab now decoupled from the crust. Again, following Gephart (1985) and observing that $B$ axes from focal mechanisms are generally not coplanar with the equal principal stress axes, we tried to identify the rupture plane in cases where the differences in misfits were greater than $10^{\circ}$. In all five cases where the fault plane was known independently (although not introduced specifically in the stress inversion), the agreement was perfect.

In conclusion, although this method does not take into consideration stress magnitudes, many interesting new results were obtained (and old results confirmed or proved) about the stress tensor in Vrancea region, which on the basis of $P, B, T$ axes alone could not be inferred, at least not so elegantly and straightforwardly.
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[^0]:    ${ }^{\text {a }} R O^{\prime} 80$ Radu and Oncescu (1980); $R C^{\prime} O^{\prime} 81$ Radu et al. (1981); $O A^{\prime} 84$ Oncescu and Apolozan (1984); $O T^{\prime} 87$ Oncescu and Trifu (1987a)

