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CLASSIFICATION CHARACTERISTICS OF CARBON NANOTUBE POLYMER COMPOSITE CHEMICAL VAPOR DETECTORS

THESIS

Huynh A. Hinshaw, Captain, USAF AFIT/GOR/ENS/06-10

DEPARTMENT OF THE AIR FORCE AIR UNIVERSITY

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Wright-Patterson Air Force Base, Ohio

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CLASSIFICATION CHARACTERISTICS OF CARBON NANOTUBE POLYMER COMPOSITE CHEMICAL VAPOR DETECTORS

THESIS

Presented to the Faculty

Department of Operational Sciences

Graduate School of Engineering and Management

Air Force Institute of Technology

Air University

Air Education and Training Command

In Partial Fulfillment of the Requirements for the

Degree of Master of Science in Operations Research

Huynh A. Hinshaw, B.S.

Captain, USAF

March 2006

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| Dr. Kenneth W. Bauer Thesis Advisor | date |
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Abstract

The first step in combating a chemical weapons threat is contamination avoidance. This is accomplished by the detection and identification of chemical agents. The Air Force has several instruments to detect chemical vapors, but is always looking for lighter, faster, and more accurate technology for a better capability.

This research is focused on using carbon nanotube polymer composite sensors for chemical detection. More specifically, models are developed to classify three sets of sensor data according to vapor using various multivariate techniques. Also, prediction models of a mixed sensor output are developed using neural networks and regression analysis. The classifiers developed are able to accurately classify three vapors for a specific set of data, but have problems when tested against data from aged sensors as well as data generated from a different set of new sensors. These results indicate that further research should be conducted to ensure accuracy in identifying chemical vapors using these types of sensors.

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Huynh A. Hinshaw

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CLASSIFICATION CHARACTERISTICS OF CARBON NANOTUBE POLYMER COMPOSITE CHEMICAL VAPOR DETECTORS

1. Introduction

1.1 Background

Chemicals have been used in warfare for centuries. The earliest use of chemical gases against an enemy was seen during the Peloponnesian War when the Spartans gained control of an Athenian fort by directing smoke into it through "hollowed out" beams (Langford, 2004:211). Ancient Chinese writings describe the use of smoke, from burning mustard and toxic vegetable matter, to deter an enemy (Langford, 2004:212). Chemical weapons use was also witnessed in World War I, where mustard gas caused more deaths than any other chemical agent (Langford, 2004:216).

After viewing the effects of such weapons, the international community placed a stigma on the use of chemical weapons in conflict. In 1993, the Chemical Weapons Convention was opened for signature and has been signed by 186 countries, including the United States. The organization established to monitor the progress of the Convention is the Organization for the Prohibition of Chemical Weapons (OPCW). According to the OPCW:

The Convention prohibits all development, production, acquisition, stockpiling, transfer, and use of chemical weapons. It requires each State Party to destroy chemical weapons and chemical weapons production facilities it possesses, as well as any chemical weapons it may have abandoned on the territory of another State Party (OPCW, 2005).

There are 8 countries, including Egypt, North Korea, and Syria, that have not signed the Convention.

While there is progress in disarmament, open source intelligence indicates that over twenty countries have either chemical weapons programs or stockpiles. The international community has taken a stand on this issue through the Convention, but it currently only addresses nation-states. The problem with this is that waging war has changed since the days of the World Wars. We are no longer fighting nation-states, but insurgents and international terrorist groups. Now, when we go into combat, we are engaging with a sometimes unknown enemy that does not fight conventionally. Terrorist groups have already shown their willingness to use chemical weapons to induce fear in a civilian population, as seen in the sarin attack on the Tokyo subway system in 1995. If they are willing to attack civilians in this fashion, they will have no qualms about using this same method to harm our military forces.

Chemical weapons can be blood, choking, nerve, blister, tear, vomiting, or incapacitating agents. They can be easily manufactured and specific chemicals, such as hydrogen cyanide and phosgene, can be purchased commercially. Due to the proliferation of chemical weapons, it is inevitable that our forces will encounter them. Senior leaders have shown that they believe this to be a significant threat, as seen by their increase in budget for weapons of mass destruction (WMD) countermeasures by \$2.1 billion for FY06-11 (DoD, 2005).

The first step in battling the chemical weapons threat is "contamination avoidance" (DoD, 2005). Contamination avoidance includes the ability to detect a

chemical agent and identify it. This thesis focuses on chemical agent vapor detection.

The military has several devices that it currently uses to accomplish this. The Chemical Agent Monitor (CAM), Improved Chemical Agent Monitor (ICAM), Automatic Chemical Agent Detection Alarm (ACADA), HAPSITE, MINICAMS, TVA-1000, and various colorimetric devices are the current fielded capabilities. A device called the Joint Chemical Agent Detector (JCAD) was developed to provide a handheld detection capability to the warfighter and the Joint NBC Reconnaissance System (JNBCRS) was developed to provide reconnaissance in areas where NBC employment is suspected.

These technologies will be fully discussed in Chapter 2.

An emerging technology that could also be used to address this issue is the use of carbon nanotube polymer composite sensors for detection. Their small size, low power consumption, and low cost make them a good option for research and development in this area. Figure 1 shows examples of how this technology could be potentially employed.



Figure 1. Potential carbon nanotube polymer composite sensor detector platforms (AFRL, 2005).

This research focuses on carbon nanotube polymer composite sensors, more specifically, identifying classifiers that will discriminate between different chemicals. The result is a study into whether this technology is a viable option for detecting and identifying chemical vapors.

1.2 Research Problem

While the Air Force has several capabilities available for chemical vapor detection, it continues to search for faster, lighter, and lower cost alternatives that provide better accuracy in the field. This thesis considered carbon nanotube polymer composite sensor technology as a possible alternative.

1.3 Research Objective

The objective of this thesis was to take existing sensor data for a number of chemicals that have interacted with different polymer sensors and develop algorithms to identify the chemical. The data was also used to investigate whether individual polymer sensor data sets can be used to predict the behavior of a mixed polymer sensor. Several multivariate analysis techniques, such as discriminant/classification analysis, neural networks, and regression analysis were considered.

1.4 Overview

Chapter 2 provides a literature review discussing current Air Force capabilities and previous research on the chemical detection capability of carbon nanotube polymer composite sensors. Chapter 3 discusses the methods used to classify and analyze the sensor data, while Chapter 4 provides the numerical analysis and results of the study. Chapter 5 presents the conclusion of the study, how this research is relevant to the Air Force, and recommendations for further research.

2. Literature Review

This chapter presents a literature review that focuses on chemical vapor detection technologies and multivariate analysis techniques. Section 2.1 focuses on the technologies currently being used or developed by the U.S. Air Force (USAF). Section 2.2 includes information on carbon nanotube polymer composite detectors and previous research into their chemical detection capability. Section 2.3 reviews discriminant analysis, Section 2.4 neural network techniques, and Section 2.5 regression analysis, and how they can be used to identify different chemicals.

2.1 Current and Developing Military Technology for Chemical Vapor Detection

Current detection devices are bulky and subject to false readings. Also, most do not provide information on the concentration of a detected chemical agent. Developing technology has attempted to resolve these issues, but several difficulties continue to exist.

2.1.1 Current Fielded Capability

The U.S. Air Force (USAF) currently uses the following technologies for chemical vapor detection: colorimetry, ion mobility spectrometry (IMS), gas chromatography with mass spectrometry (GC/MS), and photoionization/flame ionization.

Colorimetric sensors consist of litmus paper, or color spot, tests. This is the least expensive method, although rather slow for early warning detection, taking about 15-20

minutes to detect various agents (Hill and Martin, 2002:2283). These sensors are also lightweight and easy to use. They detect chemicals through the reaction of reagents, impregnated on the paper sensor, with the air. When a chemical agent is present, the reagent and chemical react and change the color of the paper. Since different reagents react to specific chemicals, a different sensor is required for each chemical to be detected. This is the main disadvantage of this technology, but it is also an advantage due to less false positives. The detector requires the human eye to act as the "signal (color) processor" (Sun and Ong, 2005:198). The problem with this is that each person's eye has a different sensitivity to color and some people have a degree of colorblindness (Sun and Ong, 2005:198). In addition, environmental factors, such as dim or bright light can inhibit the effectiveness of the sensor (Sun and Ong, 2005:198). This is why colorimetric detectors can, at best, be used for qualitative or semiqualitative analysis (Sun and Ong, 2005:198).

The current colorimetric detectors in use for vapor detection are the M256A1 Kit and the Draeger Civil Defense Simultest (CDS) Kit. The M256A1 Kit consists of M8 paper for liquid detection and M256A1 sampler detectors for vapor detection (DAF, 2003:43). The sampler detectors have pretreated test spots capable of detecting blister, blood, and nerve agents (DoD, 1999). There are two ampoules, filled with reagent, connected to each test spot via channels. When testing, the ampoules are broken and the reagents run down the channels to the pretreated test spots. The presence or absence of chemical agents can be seen by changes to the color of the test spots (DoD, 2005:A5).

The Draeger CDS Kit consists of a pump and two sets of detector tubes (Draeger, 2005). The pump is connected to the test sets and used to draw air into them. Each set

contains "five different specially designed and calibrated detector tubes" (Drager, 2005).

Specific color changes in the tubes will identify the presence of a chemical agent. The kit can detect nerve, blood, blister, and choking agents.

In IMS, ions are separated based on their drift velocity through an electric field (Sun and Ong, 2005:113). This detection process consists of "sample introduction, ionization, ionic drift, collision and diffusion, ion collection, and signal generation" (Sun and Ong, 2005:114). An IMS device usually contains a weak radioactive source to ionize a vapor sample once it has entered the system (Sun and Ong, 2005:118). These ions then enter the "drift region" where they move through an electric field. The time it takes them to move through the drift region depends on their shape, mass, and charge (Sun and Ong, 2005:113). While in the drift tube, ions collide with other molecules in the drift flow, which is opposite the ion flow. These collisions slow them down, but they are once again accelerated by the electric field gradient. Ions also undergo diffusion which causes the ions to disperse while in the drift tube. The ions eventually reach the ion collector where they lose their charges and a drift time is recorded. The drift time is the time it takes an ion to get to the ion collector after it has entered the drift region (Sun and Ong, 2005:121). At this time, an electrical current is generated, which is processed into a "signature" that correlates to the specific relative drift time (Sun and Ong, 2005:121). The detector compares this information to target information stored in its library and if it matches a target, an alarm is generated signifying detection of a chemical agent (Sun and Ong, 2005:115).

The advantages of IMS technology are that it can detect a chemical agent within seconds and at concentration levels as low as parts-per-billion (ppb) (Sun and Ong,

2005:113). It also can detect and identify many different vapors, even those not targeted, which can be a disadvantage due to false alarms (Sun and Ong, 2005:122). In addition, IMS devices can be small and lightweight, easy to operate since the microprocessor does most of the analysis, and purchased at low cost (Prelas and Ghosh, 2002:384).

Current IMS devices used by the USAF are the Chemical Agent Monitor (CAM), Improved Chemical Agent Monitor (ICAM), and Automatic Chemical Agent Detection Alarm (ACADA). The CAM and ICAM are both handheld devices that can detect and identify specific classes of nerve and blister agents, but ICAM is "300% more reliable, starts up 10 times faster, and the modular design is much less expensive to repair" (DoD, 2005:A2). ACADA is a man-portable system that can detect and identify all nerve agents, mustard, and lewisite (DoD, 2005:A7). It provides simultaneous detection of nerve and blister agents and can operate independently after start-up (JPEO-CBD, 2005).

GC/MS technology "uses a gas chromatograph to separate the materials in a sample into relatively pure chemical compounds, and then uses the mass spectrometer to identify the specific substance" (Langford, 2004:296). After the material is separated into different components by the GC, it will be ionized by an electron beam in the MS (EPA, 1998:iv). The ions are then subjected to an electric or magnetic field where they are further separated by mass (Langford, 2004:296). The resulting mass spectrum "serves as a molecular fingerprint that identifies the structure of the compound" (Langford, 2004:296). This technology allows for quick detection of chemical agents in the ppb to ppm range.

The HAPSITE Chemical Detection System is a portable GC/MS that is used by USAF. An agent is identified by its GC retention time and the comparison of its mass

spectrum to a target compound library (EPA, 1998:6). The HAPSITE can detect, identify, and quantify chemical agents in the ppb to ppm range, but the cost of the device is in the tens of thousands and operational costs are hundreds of dollars a day (EPA, 1998:iv).

Another device used by the AF is the MINICAMS, which is a near real-time gas chromatography system. It operates by alternating between sampling, when air is pulled into the system, and analysis, when nitrogen is forced through the system to send captured analytes to the capillary column for separation (Utah, 1996:1). The separated analytes are then sent to the detector where the signal is analyzed to identify and quantify the chemical present (Utah, 1996:1). This process takes approximately three to ten minutes depending on system configuration (Utah, 1996:1). The MINICAMS can detect all nerve agents and specific blister agents in the ppb to ppm range (MINICAMS, 2006).

Lastly, photoionization/flame ionization detectors (PID/FID) identify the presence of a chemical agent by measuring the current generated by an ionized molecule (Sun and Ong, 2005:209). The difference in the two techniques is how they ionize the molecules. Photoionization does this through ultraviolet (UV) radiation, while flame ionization uses a hydrogen flame to burn molecules and produce ions (Sun and Ong, 2005:209). In both methods, the ions are subjected to an electrical field which forces them toward electrodes, where the ions release their charges on contact (Sun and Ong, 2005:209). This produces an electric current that is proportional to the amount of substance that enters the detector (Sun and Ong, 2005:212).

The USAF uses a dual PID/FID system called the TVA-1000 produced by the Foxboro Company. This equipment is used for gas survey monitoring through the sampling and measurement of the concentration of known gases. Before use, it must first

be calibrated to the gas being measured (Foxboro, 1995). If the gas to be measured is different than the gas used to calibrate the system, a response factor must be used to calculate an accurate concentration reading (Foxboro, 1995). The disadvantage of this system is that it does not identify unknown gases, although a user can get an idea of what type of gas is being detected based on the different readings from the PID and FID (Foxboro, 1995).

2.1.2 Developing Capability

The Air Force has developed a sensor that makes use of Surface Acoustic Wave (SAW) technology. A piezoelectric plate is central to SAW technology. An electric field is applied to one end of the plate, which generates an acoustic wave on the surface of the plate (Hill and Martin, 2002:2282). The wave is detected at the other end of the plate and measured by the electric voltage it produces (Hill and Martin, 2002:2282). The plate itself is not capable of attracting chemicals to its surface, so a thin polymer film provides sorption sites for chemical agents (Sun and Ong, 2005:178). When a chemical sorbs onto the plate's surface, the acoustic wave's amplitude and phase changes (Hill and Martin, 2002:2282). This change is used to determine the amount of chemical deposited on the sensor. A detector can have several sensors, each with a different polymer on its surface. Each sensor will have a different response when exposed to a vapor. The chemical can be identified based on the response pattern generated from all the sensors (Sun and Ong, 2005:185). When a pattern matches one stored in the detector, the device will indicate the presence of a chemical agent (Sun and Ong, 2005:182). The SAW device is then

subjected to flash heat, so the sorbed chemicals can be released and the process can start again (Sun and Ong, 2005:182).

The major advantages of this technology are that it can be made "small and portable" (Hill and Martin, 2002:2283), manufactured at low cost, and is able to detect chemicals at the ppb level (Sun and Ong, 2005:187). It is also very fast, developing a response to a detected chemical vapor within seconds (Sun and Ong, 2005:187).

A device developed that uses SAW technology is the Joint Chemical Agent Detector (JCAD). This detector uses a chemical sensor array made up of specific polymers that detect nerve, blister, and blood agent vapors (Laljer, 2005:5). It then uses a neural network algorithm to identify and quantify the detected agent (Laljer, 2005:5). When new chemical agents are discovered, the neural network algorithm can be updated with the new information to increase detection capability (Laljer, 2005:5).

Another new system, the Joint NBC Reconnaissance System (JNBCRS), is expected to be fielded in FY06. The JNBCRS detects chemical, as well as biological, radiological, and nuclear hazards and requires 3 people to operate: a driver, sensor operator, and surveyor (AFCESA, 2006). It is to be fielded as a reconnaissance system in areas where NBC weapons and toxic chemicals are suspected to have been employed (MCTSSA, 2006). The system currently carries the ACADA for chemical detection (Huber, 2006). The disadvantages of the JNBCRS are size and cost: a large vehicle is required and is costs have been quoted at approximately \$900K per system and \$138K for annual sustainment (AFCESA, 2006).

2.2 Carbon Nanotube Polymer Composite Sensors

Carbon nanotubes are "rolled up sheets of carbon atoms" (Nanotube, 2005). They were discovered in 1991 when Sumio Iijima was studying the deposits on a graphite cathode after arc evaporation (Harris, 1999:4). Since then, they have been involved in various research in several fields from physics to material science. Research in their use for chemical detection has been conducted since the early 2000s and continues today in various forms. Their unique electrical properties and high sensitivity allow them to detect gases and volatile organic compounds (Carbon, 2005).

Before delving into research concerning carbon nanotubes, another form of carbon must be discussed due to its contribution to chemical detection research. Carbon black is a form of carbon that is produced when materials containing carbon, such as oil or gas, are not burned completely due to lack of oxygen during the combustion process. Early research conducted with carbon black organic polymer sensors provided evidence that they had the potential to detect, identify, and quantify different organic vapors.

Research from Lonergan and associates showed that carbon black sensors could resolve common organic solvents. Their tests included taking "thin films of carbon black organic polymer composites" and placing them across two metallic leads to produce individual sensors (Lonergan et al., 1996:2298). Sensor arrays were constructed by using sensors made up of several different organic polymers to provide as much chemical diversity as possible. The carbon black supplied the electrical conductivity while the organic polymer provided the diversity to allow for detected chemical classification (Lonergan et al., 1996:2299). When a sensor was exposed to a vapor, the polymer would swell causing a change in resistance, but most interesting were the patterns in resistance

change created by different vapors (Lonergan et al., 1996:2298). These patterns led to a fingerprint for each chemical that would allow for definitive classification and identification (Lonergan et al., 1996:2298). Before analysis, the team "normalized and autoscaled" the data (Lonergan et al., 1996:2305). The data was first normalized to correct for the differences in concentrations between exposures by calculating S_{ij} , the normalized signal

$$S_{ij} = \Delta R_{ij,\text{max}} / \sum_{i} \Delta R_{ij,\text{max}}$$
 (1)

where $\Delta R_{ij,\text{max}}$ is the maximum differential resistance change for the *j*th sensor to the *i*th exposure (Lonergan et al., 1996:2305). The normalized data was then autoscaled to account for the "differences in the dynamic ranges of the sensors" (Lonergan et al., 1996:2305). This resulted in features d_{ij} defined by

$$d_{ij} = (S_{ij} - \overline{S}_j) / \sigma_j \tag{2}$$

where \overline{S}_j and σ_j are the mean and standard deviation of the normalized responses (Lonergan et al., 1996:2305). The features were then analyzed using principal component analysis demonstrating that the sensors could effectively distinguish between different chemicals and their concentrations, as seen in Figure 2 (Lonergan et al., 1996:2307). Neural networks were identified as another possible option for differentiating the data.

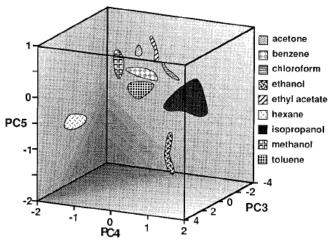


Figure 2. Results from the exposure of the 17-element array to nine solvents as represented in the third, fourth, and fifth dimensions of principal component space (Lonergan et al., 1996:2305).

Further research in 1998 focused on the sensor arrays and how they could be modified for better detection. Doleman and his team studied three areas (Doleman et al., 1998:4178):

- What vapors were not well-resolved by specific detector arrays, allowing for the change of array components to improve performance
- Optimal number of detectors needed in an array for the best performance in a specific task
- Performance of various types of detectors (bulk organic conducting polymers vs. carbon black polymer composites vs. tin oxide detectors)

Using the Fisher discriminant method, they found that the carbon black polymer composite type sensors performed best for the specific vapors tested and that for an unknown task, increasing the number of different detectors in the array will increase the array's ability to distinguish between different analytes (Doleman et al., 1998:4190).

Hopkins and Lewis also conducted tests using carbon black organic polymer composite sensors. They tested against the nerve agent simulants dimethylmethylphosphonate (DMMP) and diisopropylmethylphosponate (DIMP).

DMMP is considered a simulant for sarin and DIMP a simulant for soman (Hopkins and Lewis, 2001:887). Hopkins and Lewis found that the sensors could differentiate between these agents and other background analytes (benzene, toluene, diesel fuel, etc.) at limits of detection lower than the EC₅₀ value for the nerve agents sarin and soman (Hopkins and Lewis, 2001:884). (EC₅₀ is the concentration that would cause severe effects in 50% of a population exposed to the agents for 30 minutes.) They showed this was possible by performing principal component analysis, shown in Figure 3, as well as analyzing the data by pairs using Fisher linear discriminant analysis (Hopkins and Lewis, 2001:887).

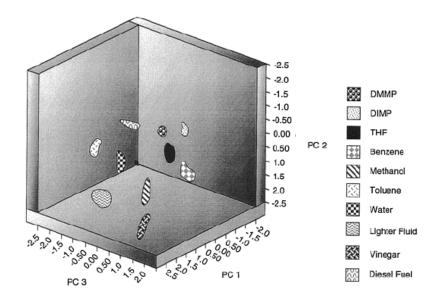


Figure 3. Data in principal component space of $\Delta R/R_b$ values produced when an eight-detector carbon black/polymer composite array was exposed to DMMP, DIMP, THF, benzene, methanol, toluene, water, lighter fluid, vinegar, or diesel fuel in an air background (Hopkins and Lewis, 2001:888).

Additionally, the Jet Propulsion Laboratory at the California Institute of Technology developed an electronic nose (ENose) using polymer-carbon black composite sensors to identify and quantify target compounds in the recycled air of spacecraft (Ryan et al., 2004:714). The ENose was composed of a 32-element sensor

array with polymers chosen that could detect a set of specific compounds at exposure levels set by the National Aeronautics and Space Administration (NASA) (Ryan et al., 2004:714). The first-generation ENose used an algorithm based on Levenburg-Marquart nonlinear least-squares fitting to identify and quantify chemicals with a success rate of 85% for a single gas event (Ryan et al., 2004:719). This system was successfully tested on a space shuttle mission in 1998, but research has continued on optimizing the sensors and sensor array, as well as developing models to identify compounds the sensing arrays have not been trained for (Ryan et al., 2004:719).

In early 2000, the idea of using carbon nanotubes for chemical detection was introduced. Kong and associates showed that sensors composed of individual single-walled carbon nanotubes (SWNTs) could detect specific gases. Once exposed to nitrogen dioxide (NO₂) or ammonia (NH₃), the electrical resistance of the SWNT either dramatically increased, Figure 4a, or decreased, Figure 4b (Kong et al., 2000:622).

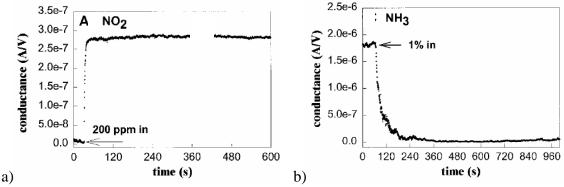


Figure 4. Electrical resistance of a semiconducting SWNT to gas molecules. (a) Conductance versus time in a 200-ppm flow. (b) Conductance versus time recorded with the same SWNT in a flow of argon (Ar) containing 1% NH₃ (Kong et al., 2000:624).

Shortly after, in 2003, a sensor platform that consisted of a network of SWNTs on interdigited electrodes (IDE) was developed for the detection of gases and organic vapors (Li et al., 2003:929). The sensors were exposed to NO₂ and nitrotoluene at different

concentrations resulting in noticeable changes in resistance. Because these responses were linearly dependent on the concentrations, the detection limit of the sensors for each vapor was easily calculated by extrapolating the linear calibration curve to the point where the sensor response is considered to be the true signal, or when the signal equals three times the noise, shown in Figure 5 (Li et al., 2003:932). These sensors were found to be able to detect NO_2 and nitrotoluene to the ppb level (Li et al., 2003:932).

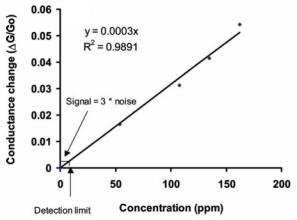


Figure 5. Calibration curve for nitrotoluene (Li et al., 2003:931).

Most recently, perpendicularly aligned carbon nanotube arrays have shown their worth as sensing materials. Wei and associates developed the sensors by dropping a polymer solution along the tube length of the aligned multiwall carbon nanotubes, as shown in Figure 6a (I) (Wei et al., 2006). The nanotube polymer composite film was then inverted (Figure 6a (II)) and gold electrodes were placed across the nanotube arrays (Figure 6a (III)) (Wei et al., 2006). The devices were then used to detect chemical vapors "through monitoring conductivity changes (Figure 6b) caused by charge-transfer interaction with gas molecules and/or inter-tube distance change induced by polymer swelling via gas adsorption" (Wei et al., 2006). Experiments conducted with these

sensors showed that when exposed to various chemical vapors resistance changes occurred. The data from these tests were used for the classification studies in this thesis.

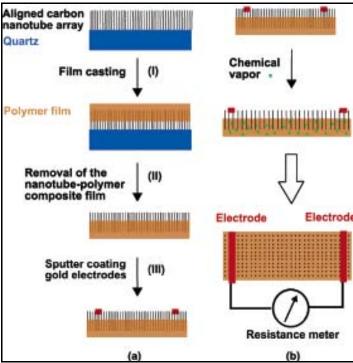


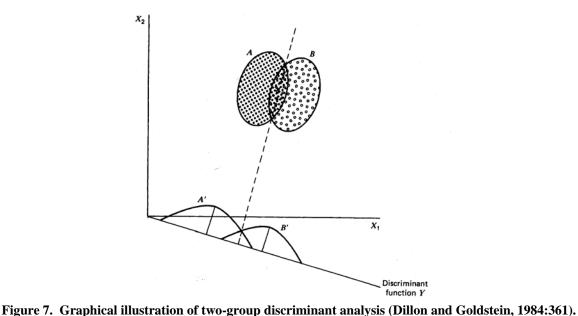
Figure 6. Schematic illustration of the procedures for (a) fabricating and (b) characterizing the aligned carbon nanotube-polymer composite chemical vapor sensor (Wei et al., 2006).

2.3 Discriminant Analysis

Discriminant Analysis is a technique for differentiating between individual observations based on their features. This is accomplished by developing a mathematical function and applying it to the features to separate the observations into mutually exclusive and exhaustive groups (Bauer, 2005a:58). The function assigns a score to each observation, so that each score (Bauer, 2005a:58)

- is a linear combination of the observation's attributes
- has average scores from the two groups as far apart as possible
- has a variance as small as possible

For the discrimination of two groups, A and B, a discriminant function \mathbf{Y} is used to separate the groups. The discriminant score, Y, for each observation is calculated by multiplying the discriminant weight, b, by the observation's value on each independent variable, X_1 and X_2 : $\mathbf{Y} = \mathbf{b}'\mathbf{X}$, where \mathbf{Y} is a 1 x n vector of discriminant scores, \mathbf{b}' is a 1 x p vector of discriminant weights, and \mathbf{X} is a p x n matrix containing the values for each of the n observations on the p independent variables (Dillon and Goldstein, 1984:361). Figure 7 shows a scatterplot of groups A, denoted by the dots, and B, denoted by the circles (Dillon and Goldstein, 1984:362). The straight line through the ellipses represents the smallest overlap between the univariate distributions A' and B' on the discriminant function graph (Dillon and Goldstein, 1984:362).



The classification rules that allow the function to distinguish between groups are developed from a training set of data in which their groupings are known. This data is

examined for differences and rules are developed so as to minimize misclassification

(Johnson and Wichern, 2002:583).

2.3.1 Discriminant Analysis Methodology

There are several methods that can be used in discriminant analysis. For most methods, the populations are assumed to be multivariate normal. To test whether a data set originated from a multivariate normal population, each variable can be tested separately for univariate normality because if one variable is not normal, the entire vector is not multivariate normal (Rencher, 2002:92). Although this should not be the only approach since the normality of the individual variables does not ensure joint normality (Rencher, 2002:92).

The assumption of univariate normality can be tested by first putting the data in order according to magnitude, $x_{(1)} \le x_{(2)} \le ... \le x_{(n)}$. Next, the probability levels (p) for the jth observation and the corresponding standard normal quantiles (q) can be calculated by (Johnson and Wichern, 2002:179):

$$P[Z \le q_{(j)}] = p_{(j)} = \frac{j - \frac{1}{2}}{n}$$
(3)

where n is the total number of observations. The ordered data $x_{(j)}$ and the normal quantiles $q_{(j)}$ can then be plotted on a Q-Q plot and the "straightness" of the resulting plot should be examined. This can be measured by calculating the correlation coefficient, r_Q , of all points in the Q-Q plot (Johnson and Wichern, 2002:182):

$$r_{Q} = \frac{\sum_{j=1}^{n} \left(x_{(j)} - \overline{x}\right) \left(q_{(j)} - \overline{q}\right)}{\sqrt{\sum_{j=1}^{n} \left(x_{(j)} - \overline{x}\right)^{2}} \sqrt{\sum_{j=1}^{n} \left(q_{(j)} - \overline{q}\right)^{2}}}$$
(4)

If r_Q is less than the appropriate level of significance, α , we can reject the hypothesis of normality (Johnson and Wichern, 2002:182).

Testing multivariate normality is not as straightforward as testing univariate normality. If the sample is not large enough, it may not provide a good estimate of the actual distribution of the population (Rencher, 2002:97). Also, these tests may not be very powerful due to the sparseness of the data in space (Rencher, 2002:97).

One method that can be used to test multivariate normality is to calculate the standardized distance from each \mathbf{x}_j to \mathbf{x} (Rencher, 2002:97; Johnson and Wichern, 2002:187):

$$d_j^2 = \left(\mathbf{x}_j - \overline{\mathbf{x}}\right)' \mathbf{S}^{-1} \left(\mathbf{x}_j - \overline{\mathbf{x}}\right)$$
 (5)

If the data is multivariate normal, then

$$u_i = \frac{nD_i^2}{\left(n - 1\right)^2} \tag{6}$$

has a beta distribution (Rencher, 2002:97). A Q-Q plot can also be constructed in this method, but the u_i values will instead be ranked in ascending order $u_{(1)} \le u_{(2)} \le ... \le u_{(n)}$ and plotted against the quantiles v_i

$$v_i = \frac{i - \alpha}{n - \alpha - \beta + 1} \tag{7}$$

where

$$\alpha = \frac{p-2}{2p} \tag{8}$$

$$\beta = \frac{n - p - 3}{2(n - p - 1)} \tag{9}$$

If the Q-Q plot has a nonlinear pattern, it is an indication that the data is not multivariate normal.

Once multivariate normality is established, it is necessary to determine whether the population covariance matrices are homogeneous. The covariance matrices (S) of each group should be calculated using (Bauer, 2005a:42):

$$S = \frac{1}{N-1} \left(\underline{X}' \underline{X} - \frac{1}{N} \underline{X}' 1 1' \underline{X} \right)$$
 (10)

where N is the number of observations and \underline{X} is the data matrix. These covariance matrices can then be tested for equality using Box's M-test. The hypothesis of all covariances being equal is tested by calculating (Rencher, 2002:257):

$$u = -2(1 - c_1) \ln M \tag{11}$$

$$c_1 = \frac{(k+1)(2p^2 + 3p - 1)}{6kv(p+1)} \tag{12}$$

$$\ln M = \frac{1}{2} \sum_{i=1}^{k} v_i \ln |S_i| - \frac{1}{2} \left(\sum_{i=1}^{k} v_i \right) \ln |S_{pl}|$$
 (13)

where v = n - 1, p is the number of features in the covariance matrix, k is the number of groups to be separated, v_i is v of the ith sample, \mathbf{S}_i is the covariance matrix of the ith sample, and \mathbf{S}_{pl} is the pooled sample covariance matrix (Rencher, 2002:256)

$$\mathbf{S}_{pl} = \frac{\sum_{i=1}^{k} v_i \mathbf{S}_i}{\sum_{i=1}^{k} v_i} \tag{14}$$

If $u > \chi_{\alpha}^2$, we can reject the hypothesis of all covariances being equal.

If the covariance matrices are equal, Fisher's Discriminant Function can be used to classify the data (Johnson and Wichern, 2002:609). The population does not need to be multivariate normal to use this method. Fisher's discriminant function finds a linear combination of the characteristics of a population so that the difference in means is maximized and the variance is minimized (Dillon and Goldstein, 1984:364). The linear combination in Equation 15 meets these requirements (Johnson and Wichern, 2002:610)

$$\hat{y} = (\bar{\mathbf{x}}_1 - \bar{\mathbf{x}}_2)' \mathbf{S}_{pooled}^{-1} \mathbf{x}$$
 (15)

where \mathbf{S}_{pooled} is the pooled sample covariance matrix. The midpoint of the maximal separation between the two populations $\hat{m} = \frac{1}{2} (\mathbf{x}_1 - \mathbf{x}_2)' \mathbf{S}_{pooled}^{-1} (\mathbf{x}_1 + \mathbf{x}_2)$ is used as the rule to classify new observations (Johnson and Wichern, 2002:611).

If the covariance matrices are not equal, quadratic discrimination scores should be calculated to identify classification rules. "Quadratic discriminant scores (D_q scores) are an approximation of the natural log of the likelihood estimators (Young, 2002:28)". The D_q scores are calculated using (Johnson and Wichern, 2002:617):

$$d_i^{\mathcal{Q}}(\mathbf{x}) = -\frac{1}{2} \ln |\mathbf{S}_i| - \frac{1}{2} (\mathbf{x} - \overline{\mathbf{x}_i})' \mathbf{S}_i^{-1} (\mathbf{x} - \overline{\mathbf{x}_i})$$
(16)

where \mathbf{x}_i is the sample mean vector and \mathbf{S}_i is the sample covariance matrix. Once the discriminant scores are calculated for each individual, the highest D_q score will determine which group the individual should be classified in.

After classification is accomplished, a confusion matrix can be created for n_1 observations from π_1 and n_2 observations from π_2 in the form (Johnson and Wichern, 2002:601)

Predicted membership

Actual membership

| | π_1 | π_2 |
|---------|----------|----------|
| π_1 | N_{1C} | N_{1M} |
| π_2 | N_{2M} | N_{2C} |

where

 N_{1C} = number of π_1 items correctly classified as π_1 items N_{1M} = number of π_1 items misclassified as π_2 items N_{2C} = number of π_2 items correctly classified as π_2 items N_{2M} = number of π_2 items misclassified as π_1 items

From the confusion matrix, the apparent error rate (APER) can be easily calculated

$$APER = \frac{N_{1M} + N_{2M}}{n_1 + n_2} \tag{17}$$

The APER is based on the training set and therefore tends to underestimate the Actual Error Rate (AER) (Bauer, 2005a:85). To find a better estimate, the total sample is usually split into a training sample and a validation sample leading to separate confusion matrices (Johnson and Wichern, 2002:602). The training sample is used to construct the discriminant function while the validation data is used to evaluate it (Johnson and Wichern, 2002:602).

2.4 Artificial Neural Networks

Artificial Neural Networks (ANNs) are another method for classifying data. This technique was developed when scientists attempted to imitate the simple neuron functions that occur in the brain. A neuron, Figure 8, consists of a nucleus, dendrites that carry signals to the nucleus, and axons which carry signals away (Nelson and Illingworth, 1991:37). A synapse is the point where a neuron passes an impulse to another neuron,

which allows for a "network" of communication throughout the brain. When a neuron receives an input, the input is "weighted" to either excite or inhibit the neuron to forward the signal (Nelson and Illingworth, 1991:39). Once the sum of the weighted inputs reaches a certain level, the neuron fires its output. This process is modeled in an ANN, which is "trained" to produce a specific output through the adjustment of the weights and network architecture.

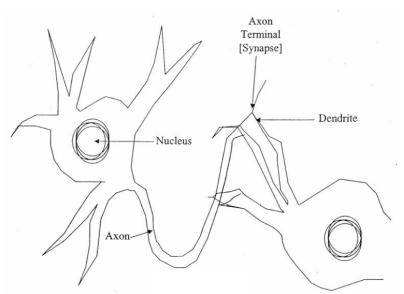


Figure 8. Biological neuron (Bauer, 2005b:1).

2.4.1 Artificial Neural Networks Definitions

The following are definitions of terms normally used when discussing ANNs (Bauer, 2005b:3):

- Artificial Neural Networks (ANN). An information processing system (algorithm) that operates on inputs to extract information and produces outputs corresponding to the extracted information.
- Architecture. The topological arrangements of neurons, layers, and connections which define the set of modeling equations available to the ANN.

- Backpropagation. A learning algorithm for updating weights in a feedforward multilayer perceptron (MLP) ANN that minimizes the mean squared mapping error.
- Epoch. A complete presentation of the data set being used to train the MLP, or equivalently called a training cycle.
- Feature. In neural networks, features refer to the input vectors of information which are presumed to have some relation that might be helpful in distinguishing the various output classes. The vector of features is often called an Exemplar.
- Feed-forward Neural Networks. Multilayer ANNs whose connections exclusively feed inputs from lower to higher levels. In contrast to a feedback or recurrent ANN, a feed-forward ANN operates only until all the inputs propagate to the output layer. An example of a feed-forward ANN is the MLP.
- Hidden Units. The processing elements in MLP ANNs that are not included in the input or output layers. This is the part of the neural network located between the input and output layers.
- Neuron. The fundamental building block of an ANN. Normally, each neuron takes a weighted sum of its inputs to determine its net input. The net is then processed through its transfer function to produce a single valued output that is broadcast to "downstream" neurons.
- Training. The iterative process of updating the weights of each node to better fit the data.
- Weight: The values, associated with each connection, which signify its strength. The weights are combined to calculate the activations.

2.4.2 Artificial Neural Networks Paradigms

In the 1940s, the first neural network model was developed by Warren McCulloch and Walter Pitts. Their model, though, did not include the weighting of the inputs to the neuron. This was corrected in the 1950s when Frank Rosenblatt introduced the first perceptron model, Figure 9. This model was made up of three layers: sensory,

association, and response (Smith, 1996:4). The sensory layer was connected to the association layer and the association layer to the response layer in a random manner (Smith, 1996:4). The response neuron with the strongest input would inhibit the other neurons and therefore provide the output for the network (Smith, 1996:5). The model was successful at "learning", but could only classify data correctly if it was linearly separable (Nelson and Illingworth, 1991:116).

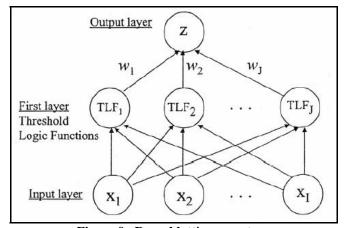


Figure 9. Rosenblatt's perceptron

Rosenblatt's Perceptron had a significant impact despite its problems. Several other models followed his, which led to the feedforward multilayer perceptron (MLP) in Figure 10. The output from one layer is fed forward to activate the next layer.

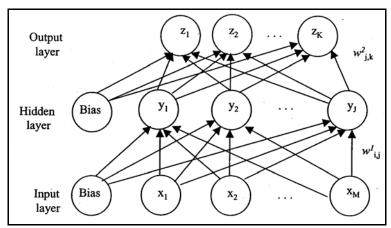


Figure 10. MLP ANN with bias

The first layer of the MLP is the input layer where the data is applied to the network. The last layer is the final output of the network. Between these two layers, there are hidden nodes. This research will include only one layer of hidden nodes in the network. The bias nodes, with values between zero and one, may be used to further inhibit the activity of certain neurons (Schalkoff, 1997:86).

The following equation describes the output for the n^{th} exemplar (z^n) of the MLP ANN above (Bauer, 2005b:15):

$$k^{\text{th}}$$
 neural network output $=z_k^n = f\left(\sum_{j=1}^J w_{j,k}^2 x_j^1\right)$ (18)

where

- J is the number of hidden nodes
- f(a) = 1/(1+e-a) for sigmoidal activation functions
- f(a) = a for linear activation functions
- $w_{j,k}^2$ is the weight from the hidden node j to output node k
- x_0^1 is the hidden layer bias term
- $x_j^1 = f\left(\sum_{i=1}^M w_{i,j}^1 x_i^n\right)$ is the output of hidden node j
- M is the number of input features
- $w_{i,j}^1$ is the weight from input node I to hidden node j
- x_0^n is the input layer bias term and is set equal to 1
- x_i^n is the *i*th input feature of the *n*th input vector

For the MLP to be useful, it must be able to learn patterns. Training algorithms such as the backwards propagation of errors method, or backpropagation, can accomplish this. Introduced in the mid-80s, it calculates the difference between the network output and the desired output and adjusts the weights of the neurons so as to minimize error. The instantaneous backpropagation algorithm for a single hidden layer feedforward network follows (Bauer, 2005b:19):

- 1. Randomly partition data into *training*, *training-test*, and *validation* sets.
- 2. Normalize the feature input data.
- 3. Initialize weights to small random values.
- 4. Present the network with a randomly selected vector from the training set, denoted x^n .
- 5. Calculate the network output z^n associated with the n^{th} training vector.
- 6. Update the weights.
- 7. If the training-test set error does not indicate sufficient convergence, go to Step 4.

Overfitting is training the data too closely and can become a problem while training an ANN. The problem is that it models the noise along with the actual population (Smith, 1996:113). This can be prevented by increasing the training sample size, by limiting the number of hidden nodes, by preventing the weights from getting too large, or by simply stopping training when overfitting begins (Smith, 1996:25). Limiting the training is the preferred method because of decreased computation time (Smith, 1996:117). This can be accomplished through early stopping. In early stopping, the data set is divided into a training set and a validation set. The training data error will continue to decrease as the training time increases, so the validation set error must be measured

simultaneously. When the error on the validation set increases, overfitting has begun (Smith, 1996:126). At this time, training is stopped and the weights and biases that produced the lowest error on the validation set are used for the model (Smith, 1996:126).

2.4.3 Signal-to-Noise Ratios

The signal-to-noise ratio (SNR) saliency measure provides even more insight into the architecture of an ANN. This measure allows for the ranking of a population's features based on their usefulness to the network (Bauer et al., 2000:31). The SNR "directly compares the saliency of a feature to that of an injected noise feature":

$$SNR_{i} = 10\log_{base10} \left(\frac{\sum_{j=1}^{J} (w_{i,j}^{1})^{2}}{\sum_{j=1}^{J} (w_{N,j}^{1})^{2}} \right)$$
(19)

where SNR_i is the value of the SNR saliency measure for feature i, J is the number of hidden nodes, $w_{i,j}^1$ is the first layer weight from node i to node j, and $w_{N,j}^1$ is the first layer weight from the injected noise node N to node j (Bauer et al., 2000:32). The injected noise feature is a Uniform (0, 1) random variable. If a feature is important to the network, the SNR saliency measure will be significantly larger than 0.0. If not, then the SNR will be close to or less than 0.0. The advantage of this method is that it may be completed in only one training run, whereas other methods require several.

2.5 Regression Analysis

Regression analysis is a statistical technique for modeling the relationship between predictor and response variables (Montgomery et al., 2001:1). A simple linear

regression model consists of the mean function, $E(Y|X=x) = \beta_0 + \beta_1 x$, and the variance function, $Var(Y|X=x) = \sigma^2$ (Weisburg, 2005:19). The variance, σ^2 , is usually a positive value, so the expected value of the *i*th response usually does not equal the observed value, y_i (Weisburg, 2005:19). The difference between the observed value and the expected value is the statistical error, ε_i , defined by $\varepsilon_i = y_i - E(Y|X=x_i)$ (Weisburg, 2005:19).

A model with more than one predictor variable is a multiple linear regression model $y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + ... + \beta_k x_k + \varepsilon$ (Montgomery et al., 2001:68). The regression coefficients, β_k , can be estimated using several methods. One such method is the method of least squares, where the error term is assumed to have $E(\varepsilon) = 0$, $Var(\varepsilon) = \sigma^2$ and they are also assumed to be uncorrelated (Montgomery et al., 2001:71). Multiple regression models are easily expressed in matrix notation by

$$\mathbf{y} = \mathbf{X}\boldsymbol{\beta} + \boldsymbol{\varepsilon} \tag{20}$$

where **y** is an *n* x 1 vector of observations, $\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_k \end{bmatrix}$, **X** is an *n* x *p* matrix of regressor

variables,
$$\mathbf{X} = \begin{bmatrix} 1 & x_{11} & x_{12} & \cdots & x_{1k} \\ 1 & x_{21} & x_{22} & \cdots & x_{2k} \\ \vdots & \vdots & & \vdots & & \vdots \\ 1 & x_{n1} & x_{n2} & \cdots & x_{nk} \end{bmatrix}$$
, $\boldsymbol{\beta}$ is a $p \times 1$ vector of regression coefficients,

$$\boldsymbol{\beta} = \begin{bmatrix} \beta_0 \\ \beta_1 \\ \vdots \\ \beta_k \end{bmatrix}, \text{ and } \boldsymbol{\varepsilon} \text{ is an n x 1 vector of random errors, } \boldsymbol{\varepsilon} = \begin{bmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \vdots \\ \varepsilon_k \end{bmatrix}, \text{ for } n \text{ observations and } p = \boldsymbol{\varepsilon}$$

k+1 (Montgomery et al., 2001:73). The observations, \mathbf{y} , and the values of the regressor variables, \mathbf{X} , are known, but the regressor coefficients, $\boldsymbol{\beta}$, are unknown. The $\boldsymbol{\beta}$'s can be estimated by finding least-squares estimators, $\hat{\boldsymbol{\beta}}$, that minimize the least-squares function $S(\boldsymbol{\beta}) = \sum_{i=1}^{n} \varepsilon_i^2$ (Montgomery et al., 2001:74). Once the least-squares estimators are found, fitted values, \hat{y}_i , corresponding to the observed values, y_i , can be found using $\hat{\mathbf{y}} = \mathbf{X}\hat{\boldsymbol{\beta}}$ (Montgomery et al., 2001:75). The difference between these two values is called the residual, e_i , which can be expressed in matrix notation as $\mathbf{e} = \mathbf{y} - \hat{\mathbf{y}}$ (Montgomery et al., 2001:75).

2.5.1 Hypothesis Testing

Once the model has been estimated, a significance of regression test should be conducted to measure the accuracy of the model. The hypotheses used in this test are (Montgomery et al., 2001:87)

$$H_0: \beta_1 = \beta_2 = \dots = \beta_k = 0$$

 $H_1: \beta_i \neq 0 \text{ for at least one j}$ (21)

Rejection of the null hypothesis indicates that at least one regressor variable significantly contributes to the model (Montgomery et al., 2001:87). To test this, an analysis of variance (ANOVA) can be accomplished. An ANOVA table, in Table 1, is usually used to summarize the results of the test (Montgomery et al., 2001:88).

Table 1. ANOVA for Significance of Regression in Multiple Regression (Montgomery et al., 2001:88)

| Source of | | Degrees of | | |
|------------|----------------|-------------|---------------------|---------------------------|
| Variation | Sum of Squares | Freedom | Mean Square | F_0 |
| Regression | $SS_{ m R}$ | k | $MS_{ m R}$ | $MS_{\rm R}/MS_{\rm Res}$ |
| Residual | $SS_{ m Res}$ | n-k-1 | MS_{Res} | |
| Total | $SS_{ m T}$ | <i>n</i> -1 | | |

The total sum of squares, SST, measures the total variability in the observations and is made up of the sum of squares due to regression, SS_R , and the residual sum of squares, SS_{Res} (Montgomery et al., 2001:87)

$$SS_T = SS_R + SS_{Res} (22)$$

It can also be calculated with the following equation (Montgomery et al., 2001:89):

$$SS_T = \mathbf{y}'\mathbf{y} - \frac{\left(\sum_{i=1}^n y_i\right)^2}{n}$$
 (23)

The regression sum of squares is defined as

$$SS_{R} = \hat{\boldsymbol{\beta}} \mathbf{X}' \mathbf{y} - \frac{\left(\sum_{i=1}^{n} y_{i}\right)^{2}}{n}$$
(24)

and the residual sum of squares is (Montgomery et al., 2001:89)

$$SS_{Res} = \mathbf{y}'\mathbf{y} - \hat{\boldsymbol{\beta}}'\mathbf{X}'\mathbf{y}$$
 (25)

The regression mean square is found by dividing the regression sum of squares by its degrees of freedom

$$MS_R = SS_R/k \tag{26}$$

and the residual mean square, which is an unbiased estimator of the variance, is calculated by dividing the residual sum of squares by its degrees of freedom

$$MS_{\text{Res}} = SS_{\text{Res}}/n - p \tag{27}$$

where p = k + 1 (Perry, 2005). To test the null hypothesis, the test statistic F_0 must be calculated (Montgomery et al., 2001:90)

$$F_0 = MS_R / MS_{\text{Res}} \tag{28}$$

If $F_0 > F_{\alpha,k,n-p}$, then the null hypothesis would be rejected implying that the regressor variables are related to the response, although this does not imply that the model is the best prediction of the relationship between the regressors and the response (Montgomery et al., 2001:90).

The above hypothesis test determines if at least one regressor is important to the model. To find which regressors are important, the significance of an individual regression coefficient can be tested. The hypotheses and test statistic are

$$H_0: \beta_j = 0$$

$$H_1: \beta_i \neq 0$$
(29)

$$t_0 = \frac{\hat{\beta}_j}{\sqrt{\hat{\sigma}^2 C_{jj}}} \tag{30}$$

where C_{jj} is the diagonal element of $(\mathbf{X}^{*}\mathbf{X})^{-1}$ corresponding to $\hat{\boldsymbol{\beta}}_{j}$ (Montgomery et al., 2001:91). The null hypothesis can be rejected if $|t_{0}| > t_{\alpha/2,n-k-1}$ (Montgomery et al., 2001:91). If it cannot be rejected, the regressor x_{j} can be removed from the model (Montgomery et al., 2001:91). The above procedure tests the contribution of x_{j} given all the other regressors are in the model (Montgomery et al., 2001:91).

To test the contribution of a specific subset of r regressors on a regression model with k regressors, the extra-sum-of-squares method can be used. In this method, the regression coefficients are partitioned into two sets

$$\beta = \left[\frac{\beta_1}{\beta_2} \right]$$

where β_1 is $(p-r) \times 1$ and β_2 is $r \times 1$ (Montgomery et al., 2001:92). This partitioning leads to the following model (Montgomery et al., 2001:92)

$$\mathbf{y} = \mathbf{X}_1 \, \mathbf{\beta}_1 + \mathbf{X}_2 \, \mathbf{\beta}_2 + \mathbf{\epsilon} \tag{31}$$

The hypotheses and test statistic are

$$H_0: \mathbf{\beta}_2 = 0$$

$$H_1: \mathbf{\beta}_2 \neq 0$$
(32)

$$F_0 = \frac{SS_R \left(\beta_2 \middle| \beta_1 \right) / r}{MS_{\text{Res}}}$$
 (33)

where $SS_R(\beta_2|\beta_1) = SS_R(\beta) - SS_R(\beta_1)$ (Montgomery et al., 2001:94). If $F_0 > F_{\alpha,r,n-p}$, the null hypothesis can be rejected implying that at least one of the regressors in $\mathbf{X_2}$ contributes significantly to the model (Montgomery et al., 2001:94).

2.5.2 *Model Adequacy*

After a model has been developed, the adequacy of the model should be examined. One way to do this is through residual analysis. It is good to use scaled residuals, as well as the original residuals, in this analysis because scaled residuals, such as studentized residuals, highlight observations that are outliers or extreme values.

Since the hypothesis tests depend on the normality of the errors, it is important to check on the validity of this assumption. This can be done by constructing normal probability plots of the residuals. The residuals should be ranked in increasing order $e_{[1]} < e_{[2]} < \cdots < e_{[n]}$ and then plotted against their cumulative probabilities $P_i = \left(i - \frac{1}{2}\right) / n$, $i = 1, 2, \ldots, n$ (Montgomery et al., 2001:138-139). If the resulting plotted points substantially depart from a straight line, the distribution is not normal (Montgomery et al., 2001:139). Figure 11 shows an example of an ideal normal probability plot.

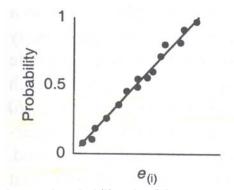


Figure 11. Ideal normal probability plot (Montgomery et al., 2001:139).

Another graphical analysis technique is to plot the residuals versus their corresponding fitted values \hat{y}_i , which allows for the detection of non-constant variance and nonlinearity. Figure 12 shows examples of an ideal residual plot (a) and those that indicate model deficiencies (b-d).

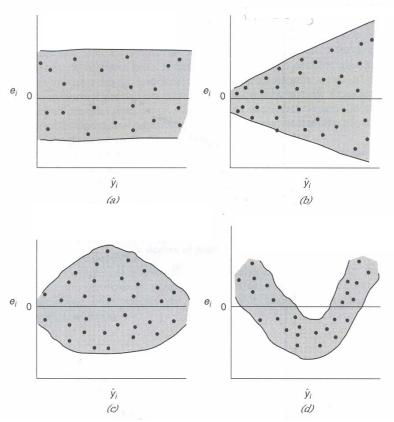


Figure 12. Patterns for residual plots: (a) satisfactory, constant variance; (b) increasing variance; (c) non-constant variance; (d) may indicate nonlinearity (Montgomery et al., 2001:142; Perry, 2005).

If residual analysis indicates non-constant variance or nonnormality in the error terms, or nonlinearity of the model, data transformations can be used to correct these problems. Analytical methods, such as Box-Cox and Box-Tidwell, can be used to select the correct transformation needed.

The Box-Cox method can be used to correct nonnormality and/or nonconstant variance (Montgomery et al., 2001:186). The power transformation y^{λ} is used in this method where λ is to be determined (Montgomery et al., 2001:186). The procedure for the Box-Cox method follows (Perry, 2005; Montgomery et al., 2001:187)):

- 1. Select a value for λ .
 - a. Compute the temporary scaled response $\boldsymbol{y}^{(\lambda)}$

$$y^{(\lambda)} = \begin{cases} \frac{y^{\lambda} - 1}{\lambda \dot{y}^{\lambda - 1}}, & \lambda \neq 0\\ \dot{y} \ln y, & \lambda = 0 \end{cases}$$
 (34)

$$\dot{y} = \exp\left[\frac{1}{n}\left(\sum_{i=1}^{n} \ln y_i\right)\right] \tag{35}$$

b. Use the scaled response to fit the model

$$\mathbf{y}^{(\lambda)} = \mathbf{X}\boldsymbol{\beta} + \boldsymbol{\varepsilon} \tag{36}$$

- c. Calculate $SS_{Res}(\lambda)$
- 2. Repeat Step 1 for various λ 's. Typically, 10-20 values are needed to estimate an optimum value.
- 3. Plot the $SS_{Res}(\lambda)$ versus λ to find the value of λ that minimizes $SS_{Res}(\lambda)$.
- 4. Fit the model using y^{λ} as the response if $\lambda \neq 0$. If $\lambda = 0$, then use $\ln y$.

If the relationship between y and its regressors is nonlinear, but the assumptions of normality and constant variance are satisfied, the Box-Tidwell method can be used to select a transformation on the regressor variables (Montgomery et al., 2001:190). The steps for the Box-Tidwell method are as follows (Perry, 2005; Montgomery et al., 2001:191):

0. Assume that the response y is related to a power of the regressor x', where

$$x' = \begin{cases} \ln x, & \alpha = 0 \\ x^{\alpha}, & \alpha \neq 0 \end{cases}$$
 (37)

- 1. Fit $\hat{y} = \hat{\beta}_0 + \hat{\beta}_1 x$ by least squares.
- 2. Define another regressor $w = x \ln x$ and fit $\hat{y} = \hat{\beta}_0 + \hat{\beta}_1 x + \hat{\gamma} w$ by least squares.
- 3. Define $\hat{\alpha}_j = \frac{\hat{\gamma}}{\hat{\beta}_1} + 1$, where *j* is the number of iterations.
- 4. Replace x with $x' = x^{\hat{\alpha}}$ and w with $w' = x' \ln x'$. Return to Step 1.

This procedure usually converges quickly, so a single iteration often gives a satisfactory estimate of α (Montgomery, 2001:192).

The nonconstant variance problem can also be addressed by fitting the model using the weighted least squares method. The variance of the errors are said to be uncorrelated and unequal with a covariance matrix of (Montgomery et al., 2001:195)

$$\sigma^{2}V = \sigma^{2} \begin{bmatrix} \frac{1}{w_{1}} & 0 \\ \frac{1}{w_{2}} & \\ 0 & \frac{1}{w_{n}} \end{bmatrix}$$

$$(38)$$

The weighted least-squares estimator is (Montgomery et al., 2001:196)

$$\hat{\boldsymbol{\beta}} = (\mathbf{X}'\mathbf{W}\mathbf{X})^{-1}\mathbf{X}'\mathbf{W}\mathbf{y} \tag{39}$$

where $\mathbf{W} = \mathbf{V}^{-1}$. The weights w_i must be known and residual analysis can sometimes give an indication of what they are (Montgomery et al., 2001:196). For example, the

variance could be a function of one of the regressors, $Var(\varepsilon_i) = \sigma^2 x_{ij}$, so that $w_i = 1/x_{ij}$ (Montgomery et al., 2001:196). Most often, the weights will have to be estimated, the analysis performed, and the weights reestimated based on the results, which may take several iterations (Montgomery et al., 2001:196).

3. Methodology

This chapter describes the methods used to detect and identify chemical agents.

Section 3.1 provides background information on the data used for this study. Section 3.2 outlines the different phases of analysis and the assumptions used. Section 3.3 presents the specific methods used to classify the data.

3.1 Background Information

The data used for this study was generated through several experiments conducted at The University of Dayton by Dr. Wei Chen. These chemical detection experiments were conducted on carbon nanotube polymer composite sensors composed of multiwalled carbon nanotubes embedded in a polymer film, as seen in Figure 13.

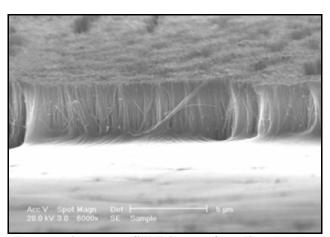


Figure 13. Scanning electron microscope (SEM) image of an aligned carbon nanotube array in a polymer matrix (Wei et al., 1006)

Three different sensors, made of the following polymers, were used: (1) polyisopropene (PI), (2) poly(vinyl acetate) (PVAc), and (3) a 1:1, by weight, mixture of the two (PI-

PVAc). These 3 sensors were individually exposed to 3 different chemical vapors: (1) cyclohexane, (2) ethanol, and (3) tetrahydrofuran (THF).

Once the chemical was exposed to the sensor, the resistance was measured by a multimeter and a change in relative resistance was calculated with the following equation:

$$\frac{(R - R_0)}{R_0} *100 \tag{40}$$

where R is the resistance after exposure in kiloohms (k Ω) and R_0 is the initial resistance in k Ω (Wei, 2006). The experimental error was about 5% in terms of relative resistance (Wei, 2006).

The experiment began by exposing each sensor to air for 110 seconds. Each sensor was then exposed to a chemical from 120 to 230 seconds. After this, the sensor was once again exposed to air for another 120 seconds thus beginning the cycle of exposure to air and chemical. This cycle continued for approximately 30 minutes.

3.2 Phases of Analysis and Assumptions

Three different sets of data were used in this research. The initial set was from sensors that had approximately 20 experiments conducted on them. The second data set was from identical sensors that had been "aged" seven to nine months and had about 50 experiments conducted on them. The last data set was from a new set of sensors that had no experiments conducted on them. Because of this, analysis consisted of four phases, as shown in Figure 14:

- Phase one: initial data set classified by vapor
- Phase two: initial data set sensor three predicted from sensors one and two
- Phase three: models developed from initial data set and validated by second data set
- Phase four: same models developed in phase three validated by last data set

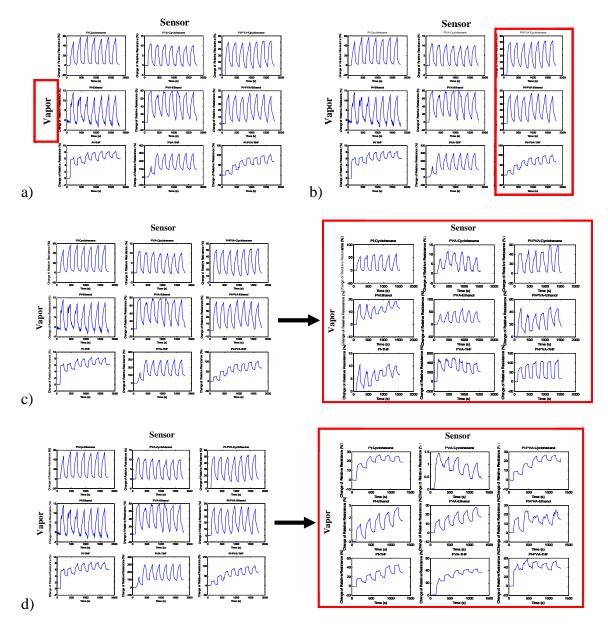


Figure 14. Phases of analysis (a) phase one, (b) phase two, (c) phase three, (d) phase four.

In the first phase Fisher's discriminant method, the quadratic discriminant scores method, and neural networks were used to classify the data by vapor. This would allow for the identification of an unknown vapor. During this phase, the sensors were assumed to be independent. Also, to use the quadratic discriminant scores method, we must assume the populations are multivariate normal. The second phase dealt with predicting

the output of the mixture sensor from the poly(vinyl acetate) and polyisopropene sensor data using linear regression and neural networks. At this point, it was assumed that the output of the mixture was dependent on the interactions of the pure polymer data. Since a linear regression was used for prediction, it was also assumed that the relationship between the response and the regressors was approximately linear. Also, the errors were assumed to be independent random variables with a mean of zero and a constant variance. The same assumptions from phase one and two were applied to phases three and four.

3.3 Methods of Analysis

Analysis was split up into four phases with a specific methodology for each.

3.3.1 Phase One

For phase one, the initial set of data was used and classified according to vapor. All the data was split up by vapor and features (F) were calculated for each vapor i, sensor j, and exposure k using the following equation (Doleman et al., 1998:4180):

$$F_{ijk} = \left[\left(\frac{\left(R_{\text{max}} - R_0 \right)}{R_0} * 100 \right)_{ijk} - \frac{1}{x_{ijk}} \right] / S_{ijk}$$
 (41)

$$\frac{\left(R_{\text{max}} - R_0\right)}{R_0} * 100 = maximum \ relative \ change \ in \ resistance$$

$$\overline{x}_{ijk} = \frac{1}{n} \sum_{m=1}^{n} x_{ijk_m} = average \ relative \ change \ in \ resistance$$

$$S_{ijk} = \sqrt{\frac{\sum_{m=1}^{n} \left(x_{ijk_m} - \overline{x}_{ijk}\right)^2}{n-1}} = standard \ deviation \ of \ relative \ change \ in \ resistance$$

The classifier was trained against the first six exposures and the last exposure was used to test the prediction capability of the function.

The covariance matrices were equal, so Fisher's approach was used for classification. Quadratic discriminant scores were also calculated, using Equation 16, for comparison. Three scores, correlating to each vapor, were calculated for each observation. The scores were the discriminating feature of the vapors. For Fisher's approach, the same equations were used, but the individual covariance matrices for each vapor were replaced with the pooled covariance matrix.

Following this, a neural network analysis was performed using the Statistical Neural Network Analysis Package (SNNAP) software to validate the quadratic discriminate score method. A tutorial for using SNNAP is in Section 3.4 of this chapter.

After classification was completed, confusion matrices were created, for both methods, for n_1 observations from π_1 , n_2 observations from π_2 , and n_3 observations from π_3 in the form (Johnson, 2002:601)

Predicted membership

Actual membership

| | π_1 | π_2 | π_3 |
|---------|-----------|-----------|-----------|
| π_1 | n_{1C} | n_{1M2} | n_{1M3} |
| π_2 | n_{2M1} | n_{2C} | n_{2M3} |
| π_3 | n_{3M1} | n_{3M2} | n_{3C} |

where

 n_{1C} = number of π_1 items correctly classified as π_1 items n_{1M2} = number of π_1 items misclassified as π_2 items n_{1M3} = number of π_1 items misclassified as π_3 items n_{2C} = number of π_2 items correctly classified as π_2 items n_{2M1} = number of π_2 items misclassified as π_1 items n_{2M3} = number of π_2 items misclassified as π_3 items n_{3C} = number of π_3 items correctly classified as π_3 items n_{3M1} = number of π_3 items misclassified as π_1 items n_{3M2} = number of π_3 items misclassified as π_2 items

From the confusion matrix, the apparent error rate (APER) was calculated (Bauer, 2005a:85)

APER =
$$\frac{n_{1M2} + n_{1M3} + n_{2M1} + n_{2M3} + n_{3M1} + n_{3M2}}{n_1 + n_2 + n_3}$$
(42)

Since the amount of data available was small, Lachenbruch's Holdout procedure was used to find an average error rate in classifying the data. To do this, the neural network was trained several times, each time leaving a different observation out of the training data set. For example, instead of using observation seven for validation,

observation one and so on were held out and used. Once the procedure was completed, an expected actual error rate was calculated (Bauer, 2005a:86)

$$E(AER) = \frac{\sum_{h} \sum_{g} I_{hg}}{HG}$$
 (43)

where H is the total number of holdout procedures, G is the total number of gases classified, and

$$I_{hg} = \begin{cases} 1 \text{ if misclassified for holdout } h, \text{ gas } g \\ 0 \text{ if classified correctly} \end{cases}$$

3.3.2 Phase Two

In phase two, rather than using features, the raw data from the initial data set was used to try to predict the output of sensor three. A linear regression of the data using the method of least squares was first used to accomplish this. The third sensor's data was used as the response, while the other two sensors' data represented the regressor variables. The coefficients of the model were found by calculating the least-squares estimator of β , for each gas, with (Montgomery, 2001:74)

$$\hat{\boldsymbol{\beta}} = (\mathbf{X}'\mathbf{X})^{-1}\mathbf{X}'\mathbf{y} \tag{44}$$

where

 $y = response \ vector$

 $X = regressor\ variable\ matrix$

The predicted values of the third sensor, \hat{y}_i , were calculated by finding those $\hat{\mathbf{y}} = \mathbf{X}\hat{\boldsymbol{\beta}}$ that corresponded to the actual values y_i (Montgomery, 2001:75). To assess the validity of

the model, an ANOVA table was constructed and the adjusted R^2 (R^2_{Adj}) was calculated (Montgomery, 2001:90):

$$R_{Adj}^{2} = 1 - \frac{SS_{\text{Re}s}/(n-p)}{SS_{T}/(n-1)}$$
(45)

where n is the number of observations and p is the number of parameters estimated.

Since normality of the errors was assumed, a normal probability plot was developed to check this assumption. An analysis of the model residuals was then conducted to assess the validity of the constant variance and linear assumptions and examine the model's adequacy. To do this, the studentized residuals, r_i , were calculated with (Montgomery, 2001:134):

$$r_i = \frac{e_i}{\sqrt{MS_{\text{Re}s}(1 - h_{ii})}}$$
 $i = 1, 2, ..., n$ (46)

where

 h_{ii} = ith diagonal element of the hat matrix

The studentized residuals were plotted against the fitted values \hat{y}_i to detect any model defects.

A neural network analysis, through SNNAP, was used to find better predictions of the sensor three data. In both methods, the first six observations were used to train and the last observation was used to test the algorithms. After both approaches were completed, a root mean square error (RMSE) was calculated to help identify which model performed best

$$RMSE = \sqrt{\frac{\sum_{i=1}^{n} (y_i - \hat{y}_i)^2}{N}}$$
 (47)

3.3.3 Phases three and four

In phase three of the analysis, new data from the same sensors used in the initial data set was used to validate the models based on the initial data set. The same methods used in phases one and two were used to develop the classification and prediction models. In phase four, data from new sensors was compared to the initial data set to observe if different sensors of the same type produced different readings. To do this, the data was tested against the same models used for validation in phase three.

3.4 SNNAP Tutorial

The following tutorial shows the steps that can be used to reproduce the neural networks acquired in this thesis. After the data is formatted in a .dat file, it is input into the SNNAP software by choosing New in the File Menu. Once the file is chosen, a Choose Model Variables window, Figure 15, appears where input and output variables are selected for the neural network analysis that is needed.

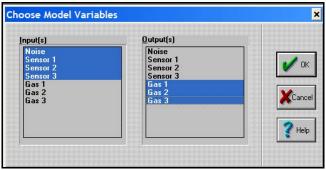


Figure 15. Choose Model Variables window

Once the model variables are accepted, a New Network window, Figure 16, will appear and Back Propagation should be used as the Network Type.

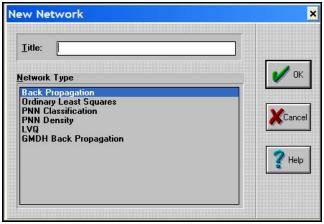


Figure 16. New Network window

After the Network type is chosen, a Structure window appears. Once the Suggest button is clicked, a Structure Suggest window will pop-up, Figure 17. After one of the output data options is selected, the Structure window, Figure 18, will appear again with the suggested structure that the program selected. The Input Layer should have a Linear Layer Type and the Layer 1 and Output Layer should be Sigmoid. Next, a Data Options window will appear where a validation sample can be chosen based on the current data using the modulus option. If modulus is selected, a Define Validation Sample box will pop-up, Figure 19, so size of the validation sample can be chosen. If separate file is selected, the software will allow the user to browse files for the data to be used for validation.

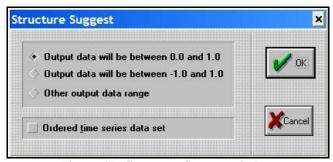


Figure 17. Structure Suggest window

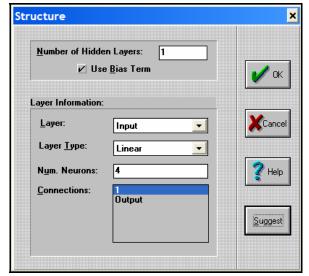


Figure 18. Structure window

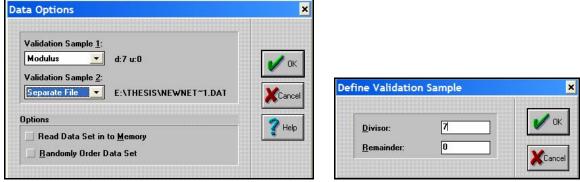


Figure 19. Data Options and Define Validation Sample windows

After data options are selected, a Data Scaling, Figure 20, window will appear where standardize input variables and no transformation on output variables should be chosen. Finally, a Parameters window, Figure 21, will appear and OK should be selected to accept the parameters given.

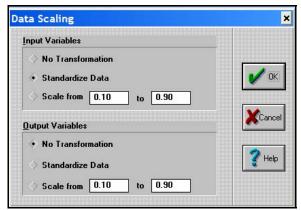


Figure 20. Data Scaling window

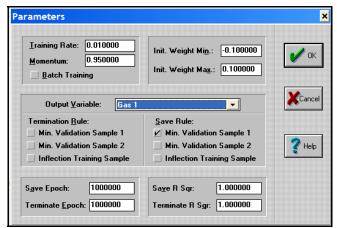


Figure 21. Parameters window

Before the neural network is trained, the weights should be saved by selecting

Text Save from the Network Menu. This will allow the user to save all node weights to a

specific file for use in future analysis. After this, the network can be trained by selecting

Train from the Train Menu. The Stop Training option in the Train Menu allows the user

to stop the training of the neural network. The Confusion Matrix option in the Network

menu will produce confusion matrices for the training and validation samples. The final

option needed to reproduce the outputs in this thesis is the Projection feature, Figure 22,

where the user can apply the trained neural network to another file and designate a file for
the output.

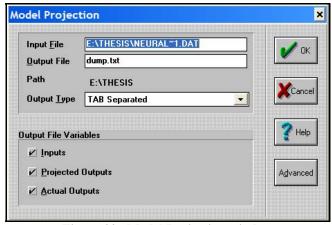


Figure 22. Model Projection window

4. Results and Analysis

In this chapter, the four phases outlined in Chapter 3 are used to analyze the experimental data. In Section 4.1, the sensor data is presented. Section 4.2 provides the numerical results of the analysis phases.

4.1 Data

During the experiment, change in relative resistance data was collected over time. Figure 23 shows the experimental data in a scaled graph matrix with equal y axes. From this set of plots, the range in the output between the gas/sensor combinations is obvious. The data was also graphed with different y axes proportional to each plot, in Figure 24, so that the changes in each gas/sensor output could be easily identified.

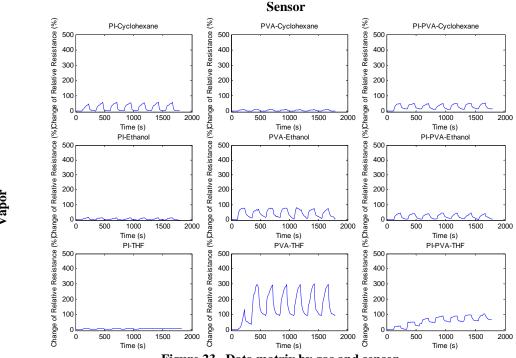


Figure 23. Data matrix by gas and sensor

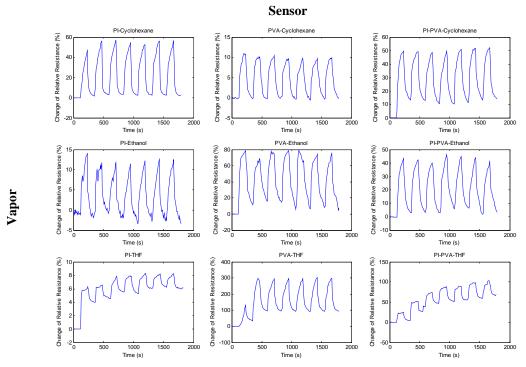


Figure 24. Scaled data matrix by gas and sensor

4.2 Analysis

Analysis was divided into four phases. The first phase consisted of taking vapor detection data from a specific set of sensors and using various techniques, including quadratic discriminant scores and neural networks, to classify the vapors. In phase two, the same data was used and sensor three data was predicted using sensor one and two data. Phase three involved using data from experiments conducted on the same set of sensors used in phases one and two. The difference was that the sensors were older at the time of these experiments and had several other experiments conducted on them. This data was used to validate classification and prediction models based on the initial data set. Finally, in phase four, data taken from new sensors of the same type were also used to validate the same models developed in phase three.

4.2.1 Phase One

During this phase, features calculated from the initial data set were used to classify the data by vapor. Table 2 shows the calculated features according to sensor and vapor. Exposures 1 through 6 were used to train the data, while exposure 7 was used to test the algorithm developed from the training.

Table 2. Data features

| | Table | 2. Data feati | ires | |
|----------|------------|---------------|------------|------------|
| | g 4 | | G 3 | T 7 |
| Exposure | Sensor 1 | Sensor 2 | Sensor 3 | Vapor |
| 1 | 1.3464947 | 0.83341224 | 0.80910072 | 1 |
| 2 | 1.21232127 | 0.60872578 | 0.95624728 | 1 |
| 3 | 1.06481227 | 0.87427116 | 1.00498005 | 1 |
| 4 | 1.0929826 | 0.79029322 | 1.25580843 | 1 |
| 5 | 1.04545194 | 1.07638323 | 0.85839787 | 1 |
| 6 | 1.08910891 | 0.90778385 | 0.73880252 | 1 |
| 7 | 1.18663325 | 0.82890241 | 0.81007631 | 1 |
| | | | | |
| 1 | 1.12964686 | 0.78237425 | 0.96890643 | 2 |
| 2 | 0.99238041 | 0.84638191 | 0.91405588 | 2 |
| 3 | 1.3438907 | 0.72138031 | 0.91118717 | 2 |
| 4 | 1.38655643 | 0.75648524 | 1.0764978 | 2 |
| 5 | 1.24568849 | 0.81968627 | 1.16606724 | 2 |
| 6 | 1.32177839 | 0.77493905 | 1.19758733 | 2 |
| 7 | 1.20693492 | 1.13712767 | 1.12664602 | 2 |
| | | | | |
| 1 | 0.51133845 | 1.79067543 | 0.70798521 | 3 |
| 2 | | 0.92720874 | | 3 |
| 3 | 1.12624714 | 1.08751899 | 0.71844641 | 3 |
| 4 | 0.80396293 | 1.18215031 | 1.32391398 | 3 |
| 5 | 0.93018531 | 1.09438993 | 0.73071483 | 3 |
| 6 | 0.87240143 | 1.05372458 | 0.91074049 | 3 |
| 7 | 1.24888628 | 1.03326901 | 1.07721608 | 3 |

These features were used to calculate discriminant scores. Three scores were calculated for each observation. If the largest score was score 1, then the vapor was predicted to be cyclohexane. If the largest was score 2, the predicted vapor was ethanol. Lastly, if the

largest was score 3, the vapor was predicted as THF. The Fisher's confusion matrices in Table 3 show that the training data classified fairly well with an APER of 27.8% and the method continued to perform similarly for the test data resulting in an APER of 33.3%. The quadratic analysis confusion matrices in Table 4 showed that the training data was fairly successful at identifying the correct vapor with an APER of 11.1%, performing better than Fisher's, but the test data performed poorly with an APER of 66.7%.

Table 3. Phase one Fisher's discriminant analysis confusion matrices Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 6 | 4 | 2 | 0 |
| V2 | 6 | 2 | 4 | 0 |
| V3 | 6 | 1 | 0 | 5 |

Test:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 0 | 1 | 0 |

Table 4. Phase one quadratic discriminant analysis confusion matrices Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 1 | 5 | 0 |
| V3 | 6 | 1 | 0 | 5 |

Test:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 0 | 1 |
| V3 | 1 | 1 | 0 | 0 |

For the neural network analysis, the data set was input in the same manner, training against the first six exposures and validating the network with the last exposure. The sensor features per vapor were the input variables and the output variables were the three vapors. The data was trained with 6 hidden nodes to 200 epochs and resulted in the confusion matrices in Table 5. These confusion matrices also showed that the neural network performed poorly for the validation sample with a similar APER of 66.7%.

Table 5. Phase one neural network analysis confusion matrices Training:

| Training. | | | | |
|-----------------|---------------|----|-----------|-----------|
| Actual Group | # of Cases | | Predicted | |
| | | V1 | V2 | V3 |
| V1 | 6 | 4 | 1 | 1 |
| V2 | 6 | 1 | 5 | 0 |
| V3 | 6 | 1 | 0 | 5 |

Test:

| Actual Group | # of Cases | | Predicted | |
|-----------------|---------------|-----------|-----------|-----------|
| | | V1 | V2 | V3 |
| V1 | 1 | 0 | 1 | 0 |
| V2 | 1 | 1 | 0 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Lachenbruch's Holdout procedure was used to find an average error rate in classifying the data. To do this, the neural network was trained six more times, each time leaving a different observation out of the training data set. For this instance, there were seven holdouts (H) and three gases (G). The expected actual error rate for the training data was 12.7% and for the test data it was 52.4%. This average error confirmed the poor performance of the data. Confusion matrices for all seven procedures can be found in Appendix D.

Because the above methods performed so poorly, the data itself was closely examined and it was discovered that the single feature was not enough information to accurately classify the gases. Another feature was created based on the slopes of the plots formed when a sensor was exposed to a chemical. The following feature was calculated based on the slope of the last six readings of each observation:

$$Fs_{ijk} = \frac{\left[\left(\frac{\left(R_{\text{max}} - R_0\right)}{R_0} * 100\right)_{ijk_l} - \left(\frac{\left(R_{\text{max}} - R_0\right)}{R_0} * 100\right)_{ijk_{l-5}}\right]}{t_l - t_{l-5}}$$
(48)

where l is the last reading during exposure. For example, in observation one, the difference in the resistance change at 230 seconds and 180 seconds divided by 50 seconds would result in the appropriate feature for observation one. Table 6 shows the new feature according to sensor and vapor.

Table 6. Data feature based on slope

| | | | • | |
|----------|-----------|------------|-----------|-------|
| Exposure | Sensor 1 | Sensor 2 | Sensor 3 | Vapor |
| 1 | 0.3065 | 0.0190996 | 0.0846064 | 1 |
| 2 | 0.2685 | 0.005457 | 0.0916568 | 1 |
| 3 | 0.211 | 0.0245566 | 0.1222092 | 1 |
| 4 | 0.215 | 0.021828 | 0.1903644 | 1 |
| 5 | 0.1995 | 0.0491134 | 0.094007 | 1 |
| 6 | 0.222 | 0.0300136 | 0.0376028 | 1 |
| 7 | 0.232 | 0.0245566 | 0.0775558 | 1 |
| | | | | |
| 1 | 0.0836502 | 0.1214098 | 0.1431924 | 2 |
| 2 | 0.0380228 | 0.1736292 | 0.1173708 | 2 |
| 3 | 0.0912548 | -0.0639686 | 0.1079814 | 2 |
| 4 | 0.0912546 | 0.113577 | 0.2253522 | 2 |
| 5 | 0.0912548 | -0.227154 | 0.2347418 | 2 |
| 6 | 0.0912548 | 0.1409922 | 0.2464788 | 2 |
| 7 | 0.068441 | 0.302872 | 0.1713616 | 2 |
| | | | | |
| 1 | 0.0063254 | 1.6802412 | 0.043423 | 3 |
| 2 | 0.0060576 | -0.325792 | 0.0434228 | 3 |
| 3 | 0.0160612 | 0.9170436 | 0.0374336 | 3 |
| 4 | 0.0031516 | 0.9773754 | 0.050161 | 3 |
| 5 | 0.011094 | 0.8687782 | 0.0449202 | 3 |
| 6 | 0.0064678 | 0.8325792 | 0.017968 | 3 |
| 7 | 0.0103678 | 0.8325792 | 0.074867 | 3 |

Discriminant scores were recalculated and the neural network retrained with this additional feature and the resulting confusion matrices in Tables 7, 8, and 9 show that the additional feature improves the performance of both the test and training data. Fisher's method resulted in a 0% APER for both the training and test data, while the quadratic scores method resulted in an APER of 0% for the training data and 33.3% for the test data. The neural network was trained with 10 nodes to 500 epochs and resulted in 0% APER for both data sets.

Table 7. Fisher's analysis confusion matrices for phase one with two features Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Table 8. Quadratic discriminant analysis confusion matrices for phase one with two features

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test:

| 1est. | | | | |
|-----------------|------------|----|-----------------|----|
| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 0 | 1 |
| V3 | 1 | 0 | 0 | 1 |

Table 9. Neural network confusion matrices for phase one with two features
Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test:

| Actual Group | # of Cases | | Predicted | |
|-----------------|------------|----|-----------|----|
| | | V1 | V2 | V3 |
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 0 | 0 | 1 |

For further analysis, noise was introduced into the data so signal-to-noise ratios could be computed. Signal to noise ratios were calculated with the following equation (Bauer, 2000:32):

$$SNR_{i} = 10\log_{base10} \left(\frac{\sum_{j=1}^{J} (w_{i,j}^{1})^{2}}{\sum_{j=1}^{J} (w_{N,j}^{1})^{2}} \right)$$
(49)

 $w_{i,j}^1 = hidden \ node \ weight$

 $w_{N,i}^1 = noise node weight$

J = number of hidden nodes connected to each feature i

Table 10 shows the hidden node weights of the neural network along with the signal to noise ratios (SNR). Most of the ratios are similar, indicating most of the sensor data is important in distinguishing between the gases. The feature two, sensor three SNR is smaller compared to the rest indicating it may have less influence on the neural network. Because of this, another neural network was trained with all other features except for

feature two of sensor three. This neural network resulted in less accuracy in classifying the data, indicating that feature two, sensor three data was needed to properly classify the vapors.

Table 10. Hidden node weights and signal-to-noise ratios for the neural network

| | | | Feature 1 | | | Feature 2 | 1 | |
|----------------------------------|--------|----------|-----------|----------|----------|-----------|----------|----------|
|] | Noise | Sensor 1 | Sensor 2 | Sensor 3 | Sensor 1 | Sensor 2 | Sensor 3 | Bias |
| 0.0 | 015476 | 0.058538 | 0.038078 | 0.025285 | 0.038231 | 0.000449 | -0.04065 | 0.035887 |
| 0.0 | 007016 | -0.07382 | -0.00946 | 0.09303 | -0.09808 | 0.090411 | 0.024747 | -0.05055 |
| -0 | .01109 | -0.05553 | 0.020847 | -0.07848 | -0.0941 | -0.08741 | 0.00698 | -0.01324 |
| -0 | .00542 | -0.00957 | 0.064129 | 0.025578 | 0.071697 | 0.034574 | -0.0665 | -0.07427 |
| -(| 0.0665 | -0.08816 | -0.00845 | -0.03133 | -0.0128 | -0.0229 | 0.03621 | 0.015983 |
| -0 | .09698 | 0.048296 | 0.02833 | -0.08473 | 0.080853 | -0.05238 | 0.031864 | 0.043675 |
| 0.0 | 024979 | -0.02271 | 0.096667 | 0.0082 | 0.020847 | -0.00103 | -0.07241 | 0.02136 |
| 0.0 | 007486 | 0.085345 | 0.083734 | -0.02903 | 0.039396 | 0.012864 | -0.04864 | -0.09716 |
| 0.0 | 031632 | -0.03593 | 0.034629 | -0.06489 | -0.01811 | -0.09142 | 0.007407 | -0.07703 |
| -0 | .03681 | 0.031285 | 0.070367 | 0.092547 | 0.081164 | 0.076519 | 0.056743 | -0.03742 |
| $\mathbf{sum} \ \mathbf{sq} 0.0$ | 017304 | 0.032225 | 0.029467 | 0.037956 | 0.04068 | 0.034658 | 0.019945 | 0.028927 |
| SNR | | 2.70041 | 2.311808 | 3.41119 | 3.712255 | 3.016482 | 0.616759 | 2.231443 |

Once again, Lachenbruch's Holdout procedure was conducted on the two data features to find an average error rate in classification. The expected actual error rate for the training data was 0% and for the test data it was 9.52%, so, on average, the data was able to be classified accurately. Confusion matrices for all seven holdouts can be found in Appendix D.

4.2.2 Phase Two

Phase two analysis began with a linear regression of the data to predict the sensor output of sensor three for each vapor. The \mathbf{X} matrices were set up as $\mathbf{X} = \begin{bmatrix} \mathbf{1}, \mathbf{x}_1, \mathbf{x}_2, \mathbf{t} \end{bmatrix}$.

The least-squares estimator of β for each vapor was

$$\hat{\boldsymbol{\beta}}_{1} = \begin{bmatrix} 11.4945 \\ 0.1979 \\ 2.3821 \\ 0.0045 \end{bmatrix} \qquad \hat{\boldsymbol{\beta}}_{2} = \begin{bmatrix} -2.5636 \\ 2.2863 \\ 0.1927 \\ 0.0047 \end{bmatrix} \qquad \hat{\boldsymbol{\beta}}_{3} = \begin{bmatrix} 10.2563 \\ 0.4618 \\ 0.0785 \\ 0.0491 \end{bmatrix}$$

where vapor one was cyclohexane, vapor two was ethanol, and vapor three was THF.

The following models were developed:

$$\hat{y}_1 = 11.4945 + 0.1979x_1 + 2.3821x_2 + 0.0045t \tag{50}$$

$$\hat{y}_2 = -2.5636 + 2.2863x_1 + 0.1927x_2 + 0.0047t \tag{51}$$

$$\hat{y}_3 = 10.2563 + 0.4618x_1 + 0.0785x_2 + 0.0491t \tag{52}$$

where \hat{y} is the predicted value of sensor three, x_1 is sensor one data, x_2 is sensor two data, and t is time. The first six exposures were used to build the models and the seventh exposure was used to validate them.

To test the significance of regression, the ANOVA tables shown in Tables 11-13, were developed.

Table 11. ANOVA table for cyclohexane

| Source of | | Degrees of | | |
|------------|----------------|------------|-------------|----------|
| Variation | Sum of Squares | Freedom | Mean Square | F_0 |
| Regression | 6.48E+03 | 3 | 2.16E+03 | 193.4223 |
| Residual | 7.60E+02 | 68 | 11.17 | |
| Total | 7.24E+03 | 71 | | |

Table 12. ANOVA table for ethanol

| Source of | | Degrees of | | |
|------------|----------------|------------|-------------|----------|
| Variation | Sum of Squares | Freedom | Mean Square | F_0 |
| Regression | 9.95E+03 | 4 | 3.32E+03 | 240.3473 |
| Residual | 9.38E+02 | 68 | 13.7957 | |
| Total | 1.09E+04 | 71 | | |

Table 13. ANOVA table for THF

| Source of | | Degrees of | | |
|------------|----------------|------------|-------------|----------|
| Variation | Sum of Squares | Freedom | Mean Square | F_0 |
| Regression | 4.52E+04 | 4 | 1.51E+04 | 330.1967 |
| Residual | 3.10E+03 | 68 | 45.5798 | |
| Total | 4.83E+04 | 71 | | |

The resulting p-values of approximately zero led to rejection of the null hypothesis indicating that at least one of the variables significantly contributed to all models. The R_{Adj}^2 of the models were 0.8905, 0.9100, and 0.9329, respectively. These values indicated that most of the variability in the y's was explained by the models.

Since normality of the errors is required to conduct the above significance test, normal probability plots (NPP) were constructed to ensure that this assumption could be made. The NPPs, in Figures 25-27, are basically linear with some outliers present, which led to the acceptance of the normality assumption.

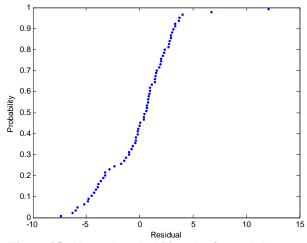
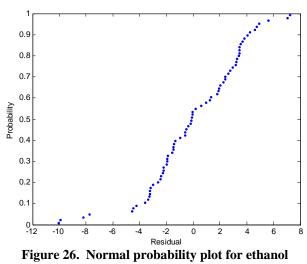
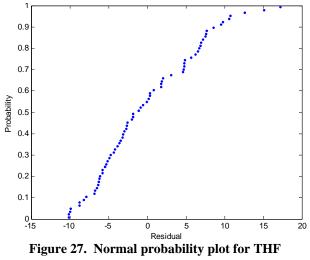


Figure 25. Normal probability plot for cyclohexane





To further assess the adequacy of the models, a residual analysis for each model was performed. The plots for cyclohexane and ethanol in Figures 28 and 29 indicated that the constant variance and linear relationship assumptions could be applied to these gases, but Figure 30 showed that they could not be applied to THF.

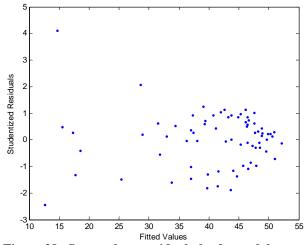


Figure 28. Sensor three residual plot for cyclohexane

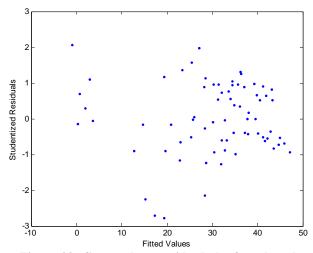


Figure 29. Sensor three residual plot for ethanol

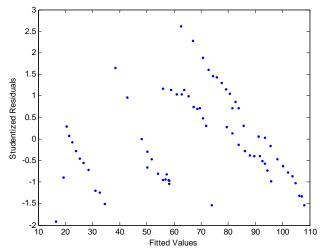


Figure 30. Sensor three residual plot for THF

Since the THF errors were found to have nonconstant variance, a weighted least squares was performed for model improvement. The variability was estimated using the moving range (MR) defined as (Montgomery, 2005:232)

$$MR_i = |y_i - y_{i-1}| \tag{53}$$

From this, the weights were calculated as $\frac{1}{MR}$ resulting in the following model:

$$y_3 = 23.3408 - 1.9601x_1 + 0.0752x_2 + 0.0535t$$
 (54)

The residual plot, though, still indicated nonconstant variance as seen in Figure 31.

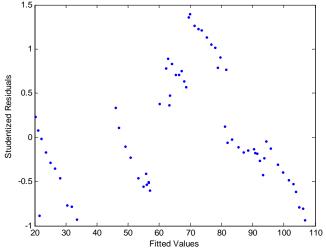
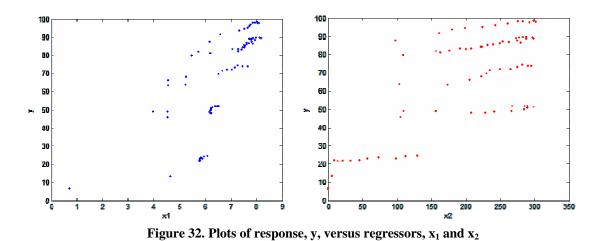


Figure 31. Weighted least squares plot for THF

Piecewise polynomial fitting (or splines) and a sinusoidal model were also used to develop a better model for THF. None of these methods succeeded in good estimates for sensor three data based on sensors one and two. This is due to the data, as seen in the y versus regressors plots in Figure 32, which would require nonlinear techniques for prediction. Because of this, the neural network served as the sole prediction method for THF.



Although the regression techniques led to adequate models for cyclohexane and ethanol, a neural network analysis was accomplished on all vapors to better predict the output of sensor three. The data of the first two sensors were used as inputs with the third sensor identified as the output. The neural network was trained with 5 nodes to 500 epochs.

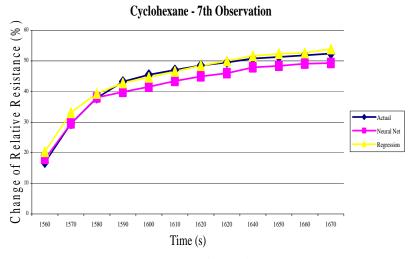
The predicted values of both methods were graphed, in Figure 33, with the actual data to compare prediction capability of both models. The RMSEs, in Table 14, showed that the regression performed better than the neural network in predicting the third sensor

for cyclohexane and ethanol. They also showed that the neural network performed fairly well in predicting all the vapors, including THF.

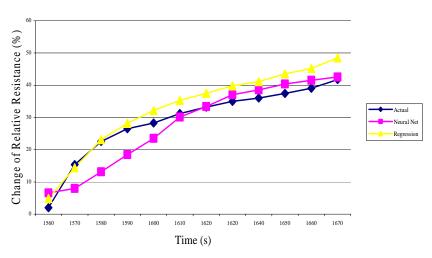
Table 14. RMSE's for sensor three models

RMSE

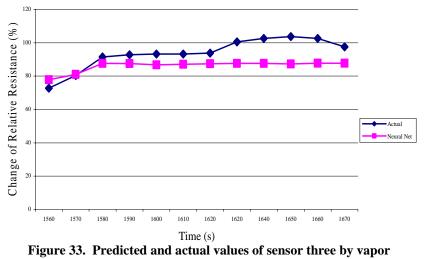
| Vapor | Neural Network | Regression |
|-------------|----------------|------------|
| Cyclohexane | 2.899 | 1.687 |
| Ethanol | 4.824 | 4.380 |
| THF | 9.857 | - |



Ethanol - 7th Observation



THF - 7th Observation



4.2.3 Phase Three

For phase three, data from a new set of sensors was used, as plotted in Figure 34. It was obvious that this data was different than the data in phase one, so it was not surprising if the models built on phase one data did not accurately classify this data. After discussions with Dr. Wei Chen, it was discovered that these differences were most likely due to the fact that the sensors during phase three experiments were months older than in phase one. During these months of aging, several experiments had been conducted on them which allowed for residual chemical build up in the sensors. This could have lead to different readings on specific sensors based on their chemical characteristics. Even though this was viewed as a potential issue, discriminant techniques were applied to the data to prove that sensor age impacted sensor classification.

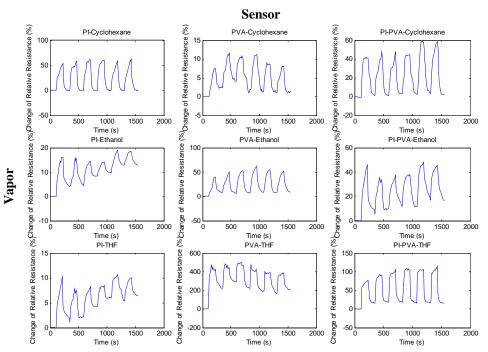


Figure 34. Phase three data matrix by vapor and sensor

Features, in Table 15, were once again calculated using Equations 41 and 48. They were then used to validate the models that were developed from the features in phase one.

Table 15. Phase three data features

| | | Feature 1 | | | Feature 2 | | | |
|----------|----------|-----------|----------|----------|-----------|----------|-------|--|
| Exposure | Sensor 1 | Sensor 2 | Sensor 3 | Sensor 1 | Sensor 2 | Sensor 3 | Vapor | |
| 1 | 1.175931 | 1.023003 | 0.56661 | 0.225396 | 0.020878 | 0.006088 | 1 | |
| 2 | 1.212669 | 1.084147 | 1.538628 | 0.225396 | 0.041647 | 0.346308 | 1 | |
| 3 | 0.971214 | 0.885291 | 1.419109 | 0.072459 | -0.00787 | 0.293008 | 1 | |
| 4 | 0.882484 | 0.978941 | 0.583188 | 0.126286 | 0.041264 | 0.021622 | 1 | |
| 5 | 1.373864 | 0.828139 | 0.883084 | 0.315626 | 0.004844 | 0.120299 | 1 | |
| 6 | 1.244025 | 0.989828 | 0.966607 | 0.290648 | 0.029388 | 0.180462 | 1 | |
| | | | | | | | | |
| 1 | 0.860175 | 1.141115 | 1.374607 | 0.032034 | 0.248222 | -0.31358 | 2 | |
| 2 | 1.236764 | 1.333025 | 1.132702 | 0.053152 | 0.284644 | 0.018756 | 2 | |
| 3 | 1.025822 | 0.88837 | 1.151288 | 0.027601 | 0.11329 | 0.110866 | 2 | |
| 4 | 1.063816 | 1.121701 | 0.833965 | 0.021488 | 0.242582 | 0.024657 | 2 | |
| 5 | 1.276944 | 0.912194 | 0.797551 | 0.049089 | 0.107429 | 0.055433 | 2 | |
| 6 | 0.879069 | 0.982816 | 0.944214 | 0.008892 | 0.123024 | 0.053349 | 2 | |
| | | | | | | | | |
| 1 | 1.465 | 1.395871 | 1.355226 | -0.06968 | -0.63253 | 0.145715 | 3 | |
| 2 | 1.132704 | 0.840745 | 0.635177 | 0.004168 | -0.0726 | 0.04204 | 3 | |
| 3 | 1.151289 | 1.246459 | 0.89028 | 0.024637 | -0.28996 | 0.189372 | 3 | |
| 4 | 0.833969 | 2.735958 | 0.506979 | 0.005479 | -0.16609 | -0.1009 | 3 | |
| 5 | 0.852657 | 0.507814 | 0.801067 | 0.012319 | 0.137248 | -0.01368 | 3 | |
| 6 | 0.944213 | 0.571045 | 0.679397 | 0.011855 | 0.194932 | 0.175784 | 3 | |

The results of classification using Fisher's and quadratic discriminant analysis are shown in Tables 16 and 17. The training data were classified perfectly for both methods, but the test data performed less accurately with an APER of 55.6% for Fisher's and 38.9% for the quadratic, which was expected since the data looked so different.

Table 16. Phase three Fisher's analysis confusion matrices Training Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 7 | 7 | 0 | 0 |
| V2 | 7 | 0 | 7 | 0 |
| V3 | 7 | 0 | 0 | 7 |

Test Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|-----|--------------|------------|
| | | V I | V 2 | V 3 |
| V1 | 6 | 4 | 2 | 0 |
| V2 | 6 | 0 | 1 | 5 |
| V3 | 6 | 0 | 3 | 3 |

Table 17. Phase three quadratic discriminant analysis confusion matrices
Training Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 7 | 7 | 0 | 0 |
| V2 | 7 | 0 | 7 | 0 |
| V3 | 7 | 0 | 0 | 7 |

Test Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 6 | 5 | 1 | 0 |
| V2 | 6 | 0 | 4 | 2 |
| V3 | 6 | 0 | 4 | 2 |

Table 18 shows that the neural network also performed well on the training data, but significantly misclassified the test data with an APER of 55.6%.

Table 18. Phase three neural network confusion matrices Training Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 7 | 7 | 0 | 0 |
| V2 | 7 | 0 | 7 | 0 |
| V3 | 7 | 0 | 0 | 7 |

Test Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 6 | 5 | 1 | 0 |
| V2 | 6 | 0 | 1 | 5 |
| V3 | 6 | 0 | 4 | 2 |

The above results showed that the age of the sensor impacted the classification of the vapors, especially ethanol and THF.

Next, the prediction techniques used in phase two were used to develop models on the full phase two data set with no holdouts. The phase three data was then used to validate these models. The new regression models for cyclohexane and ethanol were:

$$y_1 = 11.4133 + 0.2131x_1 + 2.3595x_2 + 0.0039t$$

$$y_2 = -1.9520 + 2.0608x_1 + 0.2277x_2 + 0.0029t$$
(55)

These models passed the checks for adequacy and had R_{Adj}^2 of 0.9052 and 0.9102, respectively. The neural network was once again trained with four nodes to 100 epochs using sensors one and two as the inputs and sensor three as the output. Table 16 shows the RMSE's of both the neural network and least squares regression for phase three data. The RMSE's show that phase one and two models were not the best prediction models for phase three data, which further shows the impact of the aged sensors. An example of

a predicted values versus actual data plot is shown in Figure 35. The rest of the plots are located in Appendix E.

Table 19. Phase three RMSE's

| | RMSE | | | | | | |
|-------------|-----------------------|------------|--|--|--|--|--|
| Vapor | Neural Network | Regression | | | | | |
| Cyclohexane | | | | | | | |
| Exposure 1 | 4.263 | 6.130 | | | | | |
| Exposure 2 | 14.880 | 12.403 | | | | | |
| Exposure 3 | 16.489 | 16.981 | | | | | |
| Exposure 4 | 7.902 | 7.349 | | | | | |
| Exposure 5 | 14.218 | 15.026 | | | | | |
| Exposure 6 | 6.392 | 7.876 | | | | | |
| Ethanol | | | | | | | |
| Exposure 1 | 8.795 | 7.016 | | | | | |
| Exposure 2 | 7.533 | 5.596 | | | | | |
| Exposure 3 | 5.311 | 4.661 | | | | | |
| Exposure 4 | 5.190 | 3.732 | | | | | |
| Exposure 5 | 4.065 | 6.873 | | | | | |
| Exposure 6 | 1.537 | 6.241 | | | | | |
| THF | | | | | | | |
| Exposure 1 | 13.250 | - | | | | | |
| Exposure 2 | 21.906 | - | | | | | |
| Exposure 3 | 28.437 | - | | | | | |
| Exposure 4 | 25.909 | - | | | | | |
| Exposure 5 | 12.298 | - | | | | | |
| Exposure 6 | 15.229 | - | | | | | |

Cyclohexane Exposure 1

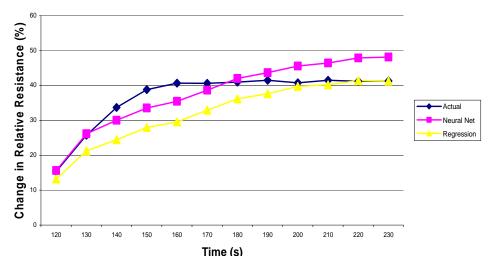


Figure 35. Predicted and actual values of sensor three for cyclohexane exposure one.

4.2.4 Phase Four

Phase four data, plotted in Figure 36, was also very different from the initial set of data. This data was collected from a newly manufactured set of PI, PVAc, and PI-PVAc sensors. It was expected that these data would also not be sufficiently classified and predicted by the models developed from the first set of data. The same methods used in phase three were used to show the inconsistencies between different sensor sets.

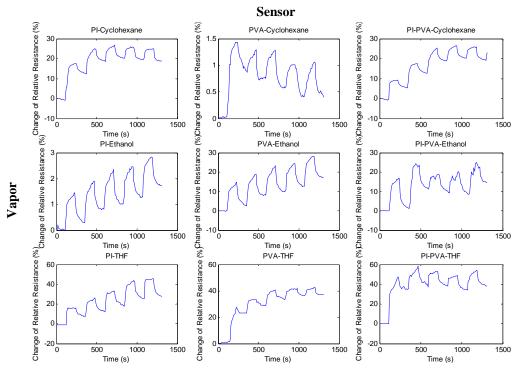


Figure 36. Phase four data matrix by vapor and sensor

Table 20 shows the data features that were calculated using Equations 41 and 48.

These features were used to validate the same models developed in phase three.

Table 20. Phase four data features

| | Feature 1 | | | Feature 2 | | | |
|-------------|-----------|----------|----------|-----------|----------|----------|-------|
| Observation | Sensor 1 | Sensor 2 | Sensor 3 | Sensor 1 | Sensor 2 | Sensor 3 | Vapor |
| 1 | 0.709334 | 0.780779 | 0.813902 | 0.017095 | 0.002395 | -0.02523 | 1 |
| 2 | 0.98102 | 1.426941 | 0.862241 | 0.051286 | 0.002928 | -0.02 | 1 |
| 3 | 0.819849 | 1.15167 | 1.282911 | 0.020083 | 0.001397 | -0.02954 | 1 |
| 4 | 0.684759 | 0.707817 | 1.247191 | 0.006141 | 0.000133 | -0.04913 | 1 |
| 5 | 0.588205 | 1.25645 | 0.640691 | 0.004149 | 0.003726 | -0.06888 | 1 |
| | | | | | | | |
| 1 | 1.119915 | 1.19082 | 0.861281 | 0.004009 | 0.047827 | 0.048989 | 2 |
| 2 | 1.066997 | 1.007185 | 0.820879 | 0.005065 | 0.052047 | -0.01243 | 2 |
| 3 | 1.303884 | 1.265177 | 1.022068 | 0.006682 | 0.068927 | 0.019174 | 2 |
| 4 | 0.889723 | 0.854844 | 1.288982 | 0.003869 | 0.037277 | 0.069532 | 2 |
| 5 | 0.934744 | 0.869599 | 1.102297 | 0.002814 | 0.02954 | 0.116308 | 2 |
| | | | | | | | |
| 1 | 0.420603 | 1.231845 | 1.383607 | -0.00148 | 0.18234 | 0.172004 | 3 |
| 2 | 0.872359 | 0.556045 | 1.755483 | 0.047163 | 0.0074 | 0.127032 | 3 |
| 3 | 0.717784 | 0.894251 | 1.192714 | 0.050779 | 0.01574 | 0.025969 | 3 |
| 4 | 0.78837 | 0.787867 | 1.704366 | 0.061628 | 0.00834 | 0.037089 | 3 |
| 5 | 0.50449 | 1.176451 | 1.170101 | 0.007793 | 0.03008 | 0.062496 | 3 |

Tables 21 and 22 show the results from Fisher's and quadratic analysis using the features in Table 20. Fisher's approach results in an APER of 66.7% and quadratic analysis results in an APER of 73.3%, which demonstrates that the models built on the initial data are insufficient in classifying this new data. The results of the neural network, in Table 23, show further inconsistencies with an APER of 60.0%.

Table 21. Phase four Fisher's analysis confusion matrices Training Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 7 | 7 | 0 | 0 |
| V2 | 7 | 0 | 7 | 0 |
| V3 | 7 | 0 | 0 | 7 |

Test Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 5 | 0 | 0 | 5 |
| V2 | 5 | 0 | 1 | 4 |
| V3 | 5 | 0 | 1 | 4 |

Table 22. Phase four quadratic discriminant analysis confusion matrices Training Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 7 | 7 | 0 | 0 |
| V2 | 7 | 0 | 7 | 0 |
| V3 | 7 | 0 | 0 | 7 |

Test Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 5 | 0 | 2 | 3 |
| V2 | 5 | 0 | 3 | 2 |
| V3 | 5 | 0 | 4 | 1 |

Table 23. Phase four neural network confusion matrices Training Data:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 7 | 7 | 0 | 0 |
| V2 | 7 | 0 | 7 | 0 |
| V3 | 7 | 0 | 0 | 7 |

Test Data:

| Actual Group | # of Cases | Predicted | | |
|-----------------|------------|-----------|----|-----------|
| | | V1 | V2 | V3 |
| V1 | 5 | 0 | 0 | 5 |
| V2 | 5 | 0 | 1 | 4 |
| V3 | 5 | 0 | 0 | 5 |

The phase two methods used to build models were also applied to this data.

Using Equation 55 and a neural network, the third sensor was predicted according to vapor. Once again, THF was only predicted using a neural network. The predicted versus actual data graphs are located in Appendix E.

Table 24 includes the RMSE's that resulted from the regression analysis and neural network. When these results are compared to the results of phase three, we see that the models' prediction performance for phase three cyclohexane and THF data and phase two ethanol data is good. On average, the models predicted phase four data better.

Table 24. Phase four RMSE's

| | RMSE | | |
|---------------|----------------|------------|--|
| Vapor | Neural Network | Regression | |
| Cyclohexane | | | |
| Observation 1 | 12.110 | 9.422 | |
| Observation 2 | 6.951 | 3.691 | |
| Observation 3 | 2.859 | 1.456 | |
| Observation 4 | 1.319 | 3.108 | |
| Observation 5 | 1.682 | 2.638 | |
| Ethanol | | | |
| Observation 1 | 7.278 | 9.649 | |
| Observation 2 | 12.572 | 13.238 | |
| Observation 3 | 8.933 | 8.461 | |
| Observation 4 | 7.546 | 5.910 | |
| Observation 5 | 10.674 | 7.338 | |
| THF | | | |
| Observation 1 | 18.398 | - | |
| Observation 2 | 7.062 | - | |
| Observation 3 | 6.339 | - | |
| Observation 4 | 10.405 | - | |
| Observation 5 | 8.218 | - | |

4.3 Summary

In phase one, Fisher's approach, quadratic discriminant scores, and neural networks were used to classify the initial data set by vapor. We were able to accurately classify the data using two data features. Phase two consisted of using the initial data set to predict sensor three output from sensors one and two. Least squares regression and neural networks were able to effectively predict the sensor three data using sensors one and two and time as variables. During phase three, the initial data set was once again used to develop classification and prediction models, but data from an "aged" sensor was used to

validate these models. The models based on the initial data set poorly classified and predicted the "aged" sensor data. Lastly, in phase four, the new sensor data was used to validate the models built in phase three. These models also performed poorly for the different sensor data set.

5. Conclusions

5.1 Introduction

The goal of this thesis was to develop models that could classify carbon nanotube polymer composite sensor data by vapor. Additionally, models were built to predict sensor three data based on two other sensors (sensors one and two). Three sets of detection data from three different sensor sets were used to accomplish this:

- PI, PVAc, PI-PVAc sensors with approximately 20 experiments conducted on them
- 2. Same set of sensors as 1., but seven to nine months older and about 50 experiments conducted on them
- 3. Different and new set of the three sensors

The data from the three sensors was generated by Dr. Wei Chen at The University of Dayton.

5.2 Literature Review Findings

The literature review began by describing the equipment that the Air Force currently uses for chemical detection, as well as the equipment that is being developed and will soon be fielded. It discussed the technology that each uses for detection along with its capability, advantages, and disadvantages.

The literature review continued with a short discussion on carbon nanotubes before moving into the topic of carbon black polymer composite sensors and their use in chemical detection research. Included in this section were several plots and other information that showed that the carbon black sensors could discriminate between

various gases. Next, carbon nanotubes as sensors with polymer composites were discussed. This portion described how they were manufactured and highlighted their ability to detect different chemicals.

The literature review then described various multivariate analysis techniques. It began by describing Fisher's discriminant function and quadratic discriminant scores along with the assumptions needed to use these techniques. It continued with a description of neural networks and signal-to-noise ratios.

The literature review ended with a discussion on regression analysis. This section focused on least squares fitting, methods to ensure model accuracy and adequacy, and concluded with a discussion on weighted least squares.

5.3 Methodologies Employed

The methodology was separated into four phases based on the data and analysis technique being applied. The first phase consisted of classifying the first set of data by vapor using Fisher's method, quadratic discriminant scores, and neural networks. This was done by calculating specific features that represented each observation. It was found that a single feature was not enough to classify the data, so another feature was developed to further explain the observations. This added feature allowed the above methods to accurately classify the vapors in most instances. In the second phase, sensor one and two data were used to predict sensor three using regression analysis and neural networks. Phase three included performing the same phase one and two analysis on the second set of data. During this phase, the data was used to validate the models developed from phase one and two data. It was shown that these models could not accurately classify or predict the new data, showing that the age of the sensor had an impact on the output of

the sensor. During phase four, the same analysis was conducted, but on data set three. This phase used the same techniques in phase three to prove that there were detection inconsistencies between different sets of sensors of the same types.

5.4 Relevance of the Research

This research can be applied to the Global War on Terrorism and homeland defense. The threat of chemical weapons attacks is a reality and the best way to combat it is through contamination avoidance. The technology discussed in this thesis directly contributes to avoidance through the detection and identification of a chemical vapor. Development of equipment using this technology could lead to faster and more accurate chemical detection in the field.

5.5 Recommendations for Future Research

Future research could include similar analysis conducted on much larger data sets.

Currently, the models are based on small data sets, which results in great sensitivity to any changes in sensor output. A larger data set one may account for these changes and lead to the correct classification of phase three and four data sets.

Another area of research would be to analyze data on sensors that have had collected residuals removed from the sensors before each detection. The method of residual removal could be anything, such as flash heat. The important factor would be that the sensor begins fresh at each detection cycle. This method could alleviate the differences in output from new and aged sensors.

More research should also be conducted to further examine the differences in different sets of sensors. This is important in determining the detection consistencies

between sensors. If the sensors have such diverse characteristics that they require different classification algorithms, this capability will be difficult to field.

The last area of research suggested is to examine the capability of the sensors to quantify the concentration of a chemical vapor. This is an important capability in the field and is one that most current USAF detectors do not have, but new generation detectors in development boast this capability. For this technology to be a viable option, it will also need to possess the ability to measure concentration.

Appendix A. Phases One and Two Raw Data

| | Cyclohexane-PI | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | -0.025 | 0.13643 | 0.11751 |
| 20 | -0.025 | -0.13643 | 0.11751 |
| 30 | 0 | -0.13643 | 0.11751 |
| 40 | 0 | -0.27285 | 0.11751 |
| 50 | -0.05 | 0 | 0.23502 |
| 60 | 0 | 0.13643 | 0.11751 |
| 70 | -0.025 | 0 | 0 |
| 80 | -0.025 | -0.13643 | 0.23502 |
| 90 | -0.05 | -0.27285 | 0.11751 |
| 100 | 0 | -0.13643 | 0.11751 |
| 110 | -0.025 | -0.13643 | 0 |
| 120 | 3.075 | 0 | 5.2879 |
| 130 | 10.1 | 4.7749 | 20.68155 |
| 140 | 15.75 | 6.95771 | 30.08226 |
| 150 | 20.675 | 7.63984 | 36.07521 |
| 160 | 25.325 | 8.45839 | 40.30552 |
| 170 | 29 | 8.86767 | 43.12573 |
| 180 | 32.05 | 9.82265 | 45.3584 |
| 190 | 35.375 | 10.23192 | 46.651 |
| 200 | 38.775 | 11.05048 | 47.9436 |
| 210 | 40.7 | 10.91405 | 48.29612 |
| 220 | 44.55 | 10.6412 | 49.00118 |
| 230 | 47.375 | 10.77763 | 49.58872 |
| 240 | 24.1 | 8.18554 | 39.48296 |
| 250 | 11.475 | 4.63847 | 27.61457 |
| 260 | 8.275 | 2.31924 | 22.56169 |
| 270 | 6.5 | 1.90996 | 20.56404 |
| 280 | 5.175 | 1.50068 | 19.62397 |
| 290 | 4.45 | 1.09141 | 18.56639 |
| 300 | 3.375 | 0.81855 | 17.2738 |
| 310 | 2.775 | 0.5457 | 15.39365 |
| 320 | 2.4 | 0.27285 | 14.57109 |
| 330 | 2.15 | 0.13643 | 14.10106 |
| 340 | 1.975 | -0.13643 | 13.74853 |
| 350 | 1.8 | -0.27285 | 13.2785 |
| 360 | 9.625 | -0.13643 | 26.79201 |

| | Cyclohexane-PI | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 370 | 22.35 | 4.63847 | 35.37015 |
| 380 | 28.8 | 7.77626 | 38.30787 |
| 390 | 33.25 | 8.18554 | 41.24559 |
| 400 | 37.8 | 9.27694 | 42.6557 |
| 410 | 40.2 | 9.41337 | 43.71328 |
| 420 | 43 | 9.82265 | 44.65335 |
| 430 | 47 | 9.95907 | 46.06345 |
| 440 | 48.45 | 9.68622 | 48.29612 |
| 450 | 51.275 | 10.0955 | 48.53114 |
| 460 | 55.075 | 9.95907 | 49.11868 |
| 470 | 56.425 | 10.0955 | 49.23619 |
| 480 | 30.575 | 7.77626 | 39.36545 |
| 490 | 9.425 | 4.7749 | 28.20212 |
| 500 | 7.075 | 3.54707 | 21.97415 |
| 510 | 6 | 1.36426 | 19.9765 |
| 520 | 5.35 | 0.95498 | 18.91892 |
| 530 | 4.925 | 0.40928 | 17.2738 |
| 540 | 4.35 | 0.13643 | 15.9812 |
| 550 | 3.825 | 0.13643 | 14.92362 |
| 560 | 3.625 | 0 | 13.98355 |
| 570 | 3.55 | -0.13643 | 13.74853 |
| 580 | 3.125 | -0.13643 | 13.396 |
| 590 | 2.95 | -0.27285 | 13.04348 |
| 600 | 5.175 | 0.13643 | 17.03878 |
| 610 | 21.975 | 4.36562 | 29.61222 |
| 620 | 32.85 | 6.82128 | 33.60752 |
| 630 | 35.15 | 7.77626 | 35.48766 |
| 640 | 40.425 | 8.04911 | 37.60282 |
| 650 | 43.1 | 8.86767 | 40.18801 |
| 660 | 46.575 | 9.27694 | 42.53819 |
| 670 | 48.95 | 9.5498 | 44.0658 |
| 680 | 50.675 | 9.5498 | 46.53349 |
| 690 | 53.45 | 9.82265 | 47.59107 |
| 700 | 55.25 | 10.0955 | 48.17861 |
| 710 | 57.125 | 10.50477 | 48.64865 |
| 720 | 30.85 | 8.45839 | 37.72033 |
| 730 | 11.525 | 4.2292 | 25.49941 |
| 740 | 8.55 | 3.54707 | 21.03408 |
| 750 | 7.05 | 2.04638 | 18.80141 |
| 760 | 5.425 | 1.36426 | 16.80376 |
| 770 | 4.6 | 0.81855 | 15.51116 |

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 780 | 4.25 | 0.27285 | 13.396 |
| 790 | 3.725 | 0.13643 | 12.69095 |
| 800 | 3.525 | 0 | 12.22092 |
| 810 | 3.4 | -0.13643 | 11.86839 |
| 820 | 3.475 | 0.13643 | 11.04583 |
| 830 | 3.225 | 0.27285 | 10.6933 |
| 840 | 5.425 | 0.40928 | 18.09636 |
| 850 | 24.375 | 5.72988 | 28.55464 |
| 860 | 30.95 | 6.54843 | 32.19741 |
| 870 | 36.1 | 7.23056 | 33.72503 |
| 880 | 39.45 | 7.63984 | 35.60517 |
| 890 | 42.225 | 8.32196 | 37.3678 |
| 900 | 44.1 | 8.59482 | 40.18801 |
| 910 | 46.55 | 9.14052 | 42.89072 |
| 920 | 48.275 | 9.5498 | 44.65335 |
| 930 | 50.6 | 9.27694 | 46.76851 |
| 940 | 52.075 | 9.41337 | 48.0611 |
| 950 | 54.85 | 9.68622 | 49.70623 |
| 960 | 29.275 | 7.63984 | 36.66275 |
| 970 | 12 | 5.45703 | 26.43948 |
| 980 | 8.05 | 3.13779 | 22.32667 |
| 990 | 6.625 | 1.90996 | 19.62397 |
| 1000 | 4.975 | 1.22783 | 17.3913 |
| 1010 | 4.75 | 0.5457 | 16.56874 |
| 1020 | 4.15 | 0.40928 | 13.74853 |
| 1030 | 3.45 | 0.13643 | 12.22092 |
| 1040 | 3.05 | 0.27285 | 11.51586 |
| 1050 | 2.825 | -0.13643 | 10.92832 |
| 1060 | 2.625 | -0.27285 | 10.6933 |
| 1070 | 2.45 | -0.40928 | 10.34078 |
| 1080 | 12.175 | -0.40928 | 13.63102 |
| 1090 | 27.15 | 4.09277 | 33.49001 |
| 1100 | 32.95 | 5.59345 | 36.07521 |
| 1110 | 35.375 | 6.13915 | 37.95535 |
| 1120 | 38.65 | 6.41201 | 41.71563 |
| 1130 | 40.35 | 6.82128 | 43.83079 |
| 1140 | 42.725 | 7.36698 | 46.29847 |
| 1150 | 47.8 | 8.04911 | 48.41363 |
| 1160 | 48.625 | 8.45839 | 49.23619 |
| 1170 | 50.925 | 9.27694 | 49.70623 |
| 1180 | 52.3 | 9.5498 | 50.52879 |

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1190 | 52.7 | 9.82265 | 50.99882 |
| 1200 | 26.275 | 7.09413 | 40.30552 |
| 1210 | 10.65 | 5.18417 | 29.84724 |
| 1220 | 7.85 | 4.63847 | 25.3819 |
| 1230 | 5.925 | 2.72851 | 21.2691 |
| 1240 | 5.125 | 1.77353 | 19.9765 |
| 1250 | 4.575 | 1.22783 | 18.6839 |
| 1260 | 3.45 | 0.68213 | 16.21622 |
| 1270 | 3.1 | 0.13643 | 14.45358 |
| 1280 | 2.875 | 0.27285 | 13.396 |
| 1290 | 3.15 | 0 | 12.57344 |
| 1300 | 2.9 | -0.40928 | 11.75088 |
| 1310 | 2.575 | -0.5457 | 11.28085 |
| 1320 | 12.45 | -0.5457 | 17.2738 |
| 1330 | 26.125 | 4.36562 | 33.3725 |
| 1340 | 34.725 | 5.3206 | 38.19036 |
| 1350 | 37.175 | 6.82128 | 42.53819 |
| 1360 | 39.25 | 7.50341 | 45.94595 |
| 1370 | 42.575 | 7.91269 | 47.59107 |
| 1380 | 45.375 | 8.18554 | 49.82374 |
| 1390 | 49.075 | 8.45839 | 50.88132 |
| 1400 | 52.275 | 8.73124 | 50.29377 |
| 1410 | 54.45 | 9.14052 | 50.99882 |
| 1420 | 55.25 | 9.27694 | 51.82139 |
| 1430 | 56.475 | 9.68622 | 51.70388 |
| 1440 | 29.675 | 7.09413 | 34.31257 |
| 1450 | 10.075 | 5.72988 | 30.31727 |
| 1460 | 6.525 | 4.7749 | 25.96945 |
| 1470 | 5.35 | 3.00136 | 22.56169 |
| 1480 | 4.525 | 2.18281 | 20.79906 |
| 1490 | 3.85 | 1.36426 | 19.50646 |
| 1500 | 3.55 | 0.95498 | 18.56639 |
| 1510 | 3.175 | 0.81855 | 16.92127 |
| 1520 | 2.875 | 0.40928 | 15.62867 |
| 1530 | 2.775 | 0.27285 | 14.92362 |
| 1540 | 2.55 | 0 | 13.98355 |
| 1550 | 2.425 | -0.40928 | 13.16099 |
| 1560 | 10.775 | -0.13643 | 16.80376 |
| 1570 | 24.55 | 4.09277 | 29.49471 |
| 1580 | 34.2 | 5.8663 | 37.83784 |
| 1590 | 36.475 | 7.09413 | 43.24324 |

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1600 | 39.15 | 7.63984 | 45.47591 |
| 1610 | 42.025 | 8.18554 | 47.00353 |
| 1620 | 44.575 | 8.73124 | 48.53114 |
| 1620 | 46.125 | 9.27694 | 49.47121 |
| 1640 | 48.925 | 9.68622 | 50.76381 |
| 1650 | 50.475 | 9.82265 | 51.23384 |
| 1660 | 54.95 | 9.5498 | 51.82139 |
| 1670 | 56.175 | 9.95907 | 52.40893 |
| 1680 | 28.85 | 6.54843 | 34.78261 |
| 1690 | 11 | 5.72988 | 26.08696 |
| 1700 | 6.8 | 4.36562 | 23.14924 |
| 1710 | 5.275 | 2.45566 | 19.85899 |
| 1720 | 4.175 | 1.90996 | 18.56639 |
| 1730 | 3.3 | 1.50068 | 17.74383 |
| 1740 | 2.875 | 1.22783 | 17.03878 |
| 1750 | 2.725 | 0.81855 | 15.9812 |
| 1760 | 2.525 | 0.27285 | 15.51116 |
| 1770 | 2.375 | 0.13643 | 15.15864 |
| 1780 | 2.25 | 0 | 14.6886 |
| 1790 | 2.125 | -0.27285 | 14.45358 |

| | Ethanol-PI | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|--------------------------------------|-----------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | -0.38023 | -0.19582 | -0.35211 |
| 20 | -1.14068 | 0.13055 | -0.23474 |
| 30 | 0 | 0.19582 | 0 |
| 40 | -0.76046 | 0.32637 | -0.11737 |
| 50 | -0.38023 | 0 | -0.46948 |
| 60 | -0.76046 | 0.06527 | -0.11737 |
| 70 | -1.14068 | -0.13055 | -0.23474 |
| 80 | -0.38023 | -0.06527 | -0.23474 |
| 90 | -1.14068 | 0.13055 | -0.23474 |
| 100 | -0.76046 | 0.06527 | -0.23474 |
| 110 | -0.76046 | 0 | -0.35211 |
| 120 | -1.14068 | 25.2611 | -0.23474 |
| 130 | 5.32319 | 47.78068 | 9.38967 |
| 140 | 7.98479 | 62.59791 | 20.65728 |
| 150 | 8.36502 | 68.60313 | 27.11268 |
| 160 | 7.22433 | 70.36554 | 31.4554 |
| 170 | 7.98479 | 71.86684 | 33.80282 |
| 180 | 9.88593 | 72.78068 | 36.26761 |
| 190 | 11.02662 | 73.49869 | 37.67606 |
| 200 | 12.54753 | 75.2611 | 39.31925 |
| 210 | 13.30798 | 76.50131 | 40.61033 |
| 220 | 13.68821 | 77.21932 | 42.01878 |
| 230 | 14.06844 | 78.85117 | 43.42723 |
| 240 | 4.56274 | 64.81723 | 31.80751 |
| 250 | 3.42205 | 53.5248 | 21.94836 |
| 260 | 1.90114 | 36.8799 | 16.43192 |
| 270 | 0.76046 | 28.39426 | 12.44131 |
| 280 | 0 | 26.10966 | 10.0939 |
| 290 | -1.14068 | 23.62924 | 8.21596 |
| 300 | -1.52091 | 21.27937 | 6.69014 |
| 310 | -0.76046 | 17.55875 | 5.6338 |
| 320 | -1.14068 | 15.79634 | 4.81221 |
| 330 | -1.90114 | 14.68668 | 4.34272 |
| 340 | -1.52091 | 12.85901 | 3.52113 |
| 350 | -0.76046 | 11.6188 | 2.93427 |
| 360 | -0.38023 | 12.46736 | 3.05164 |
| 370 | 6.08365 | 33.94256 | 16.43192 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 380 | 7.60456 | 47.7154 | 25.70423 |
| 390 | 9.88593 | 56.72324 | 29.57746 |
| 400 | 9.12548 | 57.63708 | 33.21596 |
| 410 | 7.22433 | 58.48564 | 34.38967 |
| 420 | 9.88593 | 60.18277 | 36.38498 |
| 430 | 9.88593 | 64.55614 | 37.9108 |
| 440 | 10.26616 | 66.12272 | 39.20188 |
| 450 | 11.02662 | 63.57702 | 40.25822 |
| 460 | 10.26616 | 68.14621 | 40.96244 |
| 470 | 11.78707 | 68.86423 | 42.25352 |
| 480 | 4.94297 | 57.04961 | 36.50235 |
| 490 | 3.42205 | 49.02089 | 29.69484 |
| 500 | 2.28137 | 39.81723 | 20.77465 |
| 510 | 1.52091 | 36.68407 | 14.78873 |
| 520 | 1.90114 | 32.3107 | 11.85446 |
| 530 | 0.76046 | 30.09138 | 9.2723 |
| 540 | 0.38023 | 26.95822 | 8.09859 |
| 550 | 0 | 24.08616 | 6.57277 |
| 560 | 0.38023 | 22.25849 | 5.75117 |
| 570 | 0 | 19.77807 | 4.81221 |
| 580 | -0.76046 | 17.23238 | 4.22535 |
| 590 | -0.38023 | 15.86162 | 3.28638 |
| 600 | 0 | 17.36292 | 3.40376 |
| 610 | 3.42205 | 47.58486 | 7.39437 |
| 620 | 4.94297 | 59.07311 | 20.65728 |
| 630 | 5.70342 | 65.20888 | 26.17371 |
| 640 | 7.22433 | 68.66841 | 29.81221 |
| 650 | 7.98479 | 72.7154 | 32.62911 |
| 660 | 7.22433 | 78.00261 | 34.74178 |
| 670 | 8.36502 | 74.21671 | 36.03286 |
| 680 | 9.12548 | 75.71802 | 37.32394 |
| 690 | 9.88593 | 76.30548 | 38.61502 |
| 700 | 11.40684 | 74.86945 | 39.31925 |
| 710 | 11.78707 | 74.80418 | 40.14085 |
| 720 | 2.6616 | 62.20627 | 36.26761 |
| 730 | 2.28137 | 38.57702 | 30.51643 |
| 740 | 1.90114 | 32.96345 | 18.30986 |
| 750 | 0.76046 | 30.8094 | 13.14554 |
| 760 | 0 | 28.26371 | 10.44601 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 770 | -0.76046 | 24.21671 | 8.92019 |
| 780 | -0.38023 | 20.43081 | 7.15962 |
| 790 | -1.90114 | 20.953 | 5.98592 |
| 800 | -1.52091 | 17.55875 | 5.16432 |
| 810 | -1.90114 | 16.97128 | 4.10798 |
| 820 | -1.14068 | 16.12272 | 3.28638 |
| 830 | -1.90114 | 14.62141 | 2.93427 |
| 840 | -1.14068 | 16.44909 | 2.93427 |
| 850 | 2.28137 | 44.58225 | 7.04225 |
| 860 | 3.42205 | 52.61097 | 23.70892 |
| 870 | 4.18251 | 63.6423 | 28.28638 |
| 880 | 4.56274 | 69.84334 | 31.10329 |
| 890 | 5.70342 | 72.06266 | 32.62911 |
| 900 | 6.84411 | 73.04178 | 34.85915 |
| 910 | 7.98479 | 74.93473 | 38.26291 |
| 920 | 8.74525 | 75.65274 | 40.96244 |
| 930 | 9.88593 | 77.08877 | 42.84038 |
| 940 | 10.64639 | 77.80679 | 44.48357 |
| 950 | 11.40684 | 78.72063 | 46.12676 |
| 960 | 3.04183 | 71.34465 | 41.19718 |
| 970 | 1.90114 | 57.5718 | 28.16901 |
| 980 | 0.76046 | 44.71279 | 22.30047 |
| 990 | 0 | 32.18016 | 20.07042 |
| 1000 | -0.76046 | 30.61358 | 17.84038 |
| 1010 | -0.38023 | 25.45692 | 15.84507 |
| 1020 | -1.14068 | 22.25849 | 13.96714 |
| 1030 | -1.52091 | 19.84334 | 12.55869 |
| 1040 | -1.14068 | 16.12272 | 11.26761 |
| 1050 | -1.90114 | 11.22715 | 9.85915 |
| 1060 | -2.6616 | 9.46475 | 7.98122 |
| 1070 | -3.42205 | 5.93995 | 5.98592 |
| 1080 | -2.28137 | 9.07311 | 6.10329 |
| 1090 | 1.90114 | 30.15666 | 9.50704 |
| 1100 | 3.80228 | 60.18277 | 18.66197 |
| 1110 | 5.32319 | 71.80157 | 24.1784 |
| 1120 | 6.08365 | 79.96084 | 27.46479 |
| 1130 | 6.84411 | 76.82768 | 30.98592 |
| 1140 | 7.60456 | 75.78329 | 33.33333 |
| 1150 | 9.12548 | 73.89034 | 36.38498 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1160 | 9.88593 | 73.2376 | 39.55399 |
| 1170 | 10.64639 | 68.47258 | 42.37089 |
| 1180 | 11.40684 | 66.44909 | 44.13146 |
| 1190 | 12.1673 | 64.42559 | 45.07042 |
| 1200 | 6.08365 | 65.99217 | 37.55869 |
| 1210 | 3.80228 | 52.87206 | 27.8169 |
| 1220 | 1.52091 | 42.10183 | 21.00939 |
| 1230 | 0.76046 | 36.42298 | 16.90141 |
| 1240 | 0.38023 | 31.52742 | 13.96714 |
| 1250 | -0.38023 | 24.34726 | 11.73709 |
| 1260 | -0.76046 | 23.62924 | 10.32864 |
| 1270 | -1.14068 | 22.19321 | 9.03756 |
| 1280 | -1.52091 | 14.42559 | 8.21596 |
| 1290 | -0.76046 | 10.11749 | 7.62911 |
| 1300 | -1.52091 | 7.5718 | 7.15962 |
| 1310 | -2.6616 | 6.39687 | 6.57277 |
| 1320 | -1.14068 | 10.11749 | 6.69014 |
| 1330 | 1.14068 | 43.53786 | 14.08451 |
| 1340 | 2.6616 | 57.50653 | 20.30516 |
| 1350 | 4.18251 | 62.27154 | 23.47418 |
| 1360 | 5.32319 | 63.90339 | 27.34742 |
| 1370 | 6.84411 | 65.53525 | 29.92958 |
| 1380 | 7.98479 | 67.29765 | 31.57277 |
| 1390 | 8.74525 | 68.73368 | 35.79812 |
| 1400 | 9.88593 | 69.97389 | 38.61502 |
| 1410 | 11.02662 | 70.49608 | 41.5493 |
| 1420 | 11.78707 | 72.32376 | 43.07512 |
| 1430 | 12.54753 | 74.34726 | 43.89671 |
| 1440 | 4.18251 | 53.91645 | 34.85915 |
| 1450 | 1.90114 | 43.21149 | 23.59155 |
| 1460 | 0.76046 | 31.39687 | 18.30986 |
| 1470 | -0.38023 | 27.67624 | 15.96244 |
| 1480 | 0 | 22.45431 | 13.84977 |
| 1490 | -1.14068 | 20.75718 | 11.50235 |
| 1500 | -1.90114 | 19.38642 | 9.50704 |
| 1510 | -0.76046 | 17.88512 | 6.80751 |
| 1520 | -1.90114 | 15.86162 | 3.87324 |
| 1530 | -2.6616 | 13.77285 | 3.05164 |
| 1540 | -1.90114 | 9.8564 | 2.11268 |
| 1550 | -2.6616 | 8.28982 | 1.87793 |
| 1560 | -0.76046 | 9.5953 | 1.99531 |

| | Ethanol-PI | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1570 | 1.90114 | 27.2846 | 15.37559 |
| 1580 | 4.56274 | 40.46997 | 22.53521 |
| 1590 | 6.08365 | 48.49869 | 26.52582 |
| 1600 | 7.60456 | 50.91384 | 28.28638 |
| 1610 | 8.36502 | 57.96345 | 31.22066 |
| 1620 | 9.12548 | 60.05222 | 33.21596 |
| 1620 | 9.88593 | 63.05483 | 34.97653 |
| 1640 | 10.26616 | 64.81723 | 36.03286 |
| 1650 | 11.02662 | 68.21149 | 37.44131 |
| 1660 | 11.40684 | 71.99739 | 39.08451 |
| 1670 | 12.54753 | 75.19582 | 41.78404 |
| 1680 | 5.32319 | 54.37337 | 23.59155 |
| 1690 | 2.6616 | 39.49086 | 19.60094 |
| 1700 | 1.52091 | 33.68146 | 17.723 |
| 1710 | 0.76046 | 25.13055 | 15.61033 |
| 1720 | -0.38023 | 23.89034 | 14.55399 |
| 1730 | -0.38023 | 22.84595 | 12.55869 |
| 1740 | -1.14068 | 22.51958 | 11.38498 |
| 1750 | -1.90114 | 17.62402 | 8.09859 |
| 1760 | -2.28137 | 15.4047 | 7.39437 |
| 1770 | -1.52091 | 10.70496 | 5.39906 |
| 1780 | -2.6616 | 4.69974 | 4.46009 |
| 1790 | -3.42205 | 7.8329 | 3.40376 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|-----------------------------------|-----------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | 0.00281 | 0 | -0.35211 |
| 20 | 0.0212 | 0.15083 | -0.23474 |
| 30 | 0.02238 | -0.15083 | 0 |
| 40 | 0.02115 | -0.15083 | -0.11737 |
| 50 | 0.01422 | -0.15083 | -0.46948 |
| 60 | -0.00805 | 0 | -0.11737 |
| 70 | -0.00823 | -0.15083 | -0.23474 |
| 80 | -1.87E-04 | 0 | -0.23474 |
| 90 | -0.00299 | -0.15083 | -0.23474 |
| 100 | 0.0015 | -0.15083 | -0.23474 |
| 110 | -0.01123 | -0.15083 | -0.35211 |
| 120 | 0.72179 | 0.75415 | -0.23474 |
| 130 | 4.65948 | 6.03318 | 9.38967 |
| 140 | 5.78495 | 9.65309 | 20.65728 |
| 150 | 5.77859 | 14.02715 | 27.11268 |
| 160 | 5.79936 | 22.02112 | 31.4554 |
| 170 | 5.77316 | 33.33333 | 33.80282 |
| 180 | 5.76699 | 46.00302 | 36.26761 |
| 190 | 5.80292 | 57.61689 | 37.67606 |
| 200 | 5.83286 | 74.05732 | 39.31925 |
| 210 | 5.89181 | 98.4917 | 40.61033 |
| 220 | 5.95562 | 113.12217 | 42.01878 |
| 230 | 6.08326 | 130.01508 | 43.42723 |
| 240 | 6.31251 | 84.01207 | 31.80751 |
| 250 | 5.65002 | 64.55505 | 21.94836 |
| 260 | 4.86047 | 55.80694 | 16.43192 |
| 270 | 4.54 | 52.33786 | 12.44131 |
| 280 | 4.37146 | 49.17044 | 10.0939 |
| 290 | 4.26105 | 45.24887 | 8.21596 |
| 300 | 4.2122 | 41.93062 | 6.69014 |
| 310 | 4.1555 | 41.3273 | 5.6338 |
| 320 | 4.10797 | 39.66817 | 4.81221 |
| 330 | 4.05931 | 38.15988 | 4.34272 |
| 340 | 4.01234 | 37.40573 | 3.52113 |
| 350 | 3.9779 | 35.89744 | 2.93427 |
| 360 | 3.97248 | 110.10558 | 3.05164 |
| 370 | 4.53353 | 156.71192 | 16.43192 |
| 380 | 6.24682 | 208.29563 | 25.70423 |
| 390 | 6.21706 | 228.50679 | 29.57746 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 400 | 6.16915 | 241.93062 | 33.21596 |
| 410 | 6.16635 | 266.36501 | 34.38967 |
| 420 | 6.2165 | 284.01207 | 36.38498 |
| 430 | 6.23971 | 289.44193 | 37.9108 |
| 440 | 6.2878 | 298.64253 | 39.20188 |
| 450 | 6.40159 | 288.98944 | 40.25822 |
| 460 | 6.48 | 284.91704 | 40.96244 |
| 470 | 6.51938 | 267.72247 | 42.25352 |
| 480 | 6.53652 | 200.45249 | 36.50235 |
| 490 | 5.80385 | 162.29261 | 29.69484 |
| 500 | 5.10094 | 132.73002 | 20.77465 |
| 510 | 4.9196 | 127.30015 | 14.78873 |
| 520 | 4.97575 | 113.42383 | 11.85446 |
| 530 | 4.93607 | 109.65309 | 9.2723 |
| 540 | 4.87862 | 105.42986 | 8.09859 |
| 550 | 4.81106 | 102.86576 | 6.57277 |
| 560 | 4.77925 | 101.20664 | 5.75117 |
| 570 | 4.76371 | 99.09502 | 4.81221 |
| 580 | 4.70476 | 96.98341 | 4.22535 |
| 590 | 4.61943 | 94.87179 | 3.28638 |
| 600 | 4.54083 | 105.58069 | 3.40376 |
| 610 | 4.54513 | 173.75566 | 7.39437 |
| 620 | 4.54363 | 206.33484 | 20.65728 |
| 630 | 5.25122 | 222.62443 | 26.17371 |
| 640 | 6.53128 | 230.31674 | 29.81221 |
| 650 | 6.66022 | 235.29412 | 32.62911 |
| 660 | 6.86155 | 249.62293 | 34.74178 |
| 670 | 7.03675 | 265.00754 | 36.03286 |
| 680 | 7.15446 | 274.81146 | 37.32394 |
| 690 | 7.27423 | 281.90045 | 38.61502 |
| 700 | 7.46287 | 289.74359 | 39.31925 |
| 710 | 7.66461 | 295.47511 | 40.14085 |
| 720 | 7.87365 | 190.49774 | 36.26761 |
| 730 | 7.13125 | 164.25339 | 30.51643 |
| 740 | 6.40963 | 136.80241 | 18.30986 |
| 750 | 6.15886 | 128.20513 | 13.14554 |
| 760 | 5.96386 | 115.98793 | 10.44601 |
| 770 | 5.85026 | 109.2006 | 8.92019 |
| 780 | 5.76025 | 106.03318 | 7.15962 |
| 790 | 5.67697 | 102.11161 | 5.98592 |
| 800 | 5.61802 | 100.60332 | 5.16432 |
| 810 | 5.62064 | 98.79336 | 4.10798 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|--------------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 820 | 5.58078 | 96.38009 | 3.28638 |
| 830 | 5.52688 | 94.11765 | 2.93427 |
| 840 | 5.48964 | 109.2006 | 2.93427 |
| 850 | 5.72581 | 156.56109 | 7.04225 |
| 860 | 7.07118 | 191.25189 | 23.70892 |
| 870 | 7.28958 | 208.59729 | 28.28638 |
| 880 | 7.53455 | 223.52941 | 31.10329 |
| 890 | 7.56636 | 231.97587 | 32.62911 |
| 900 | 7.62643 | 249.77376 | 34.85915 |
| 910 | 7.69942 | 262.7451 | 38.26291 |
| 920 930 | 7.81526 7.85849 | 274.20814 279.63801 | 40.96244 42.84038 |
| 930 | 7.05049 7.9442 | 287.48115 | 42.64036 |
| 950 | 7.78401 | 298.64253 | 46.12676 |
| 960 | 7.8948 | 191.40271 | 41.19718 |
| 970 | 7.30455 | 166.66667 | 28.16901 |
| 980 | 6.55523 | 138.91403 | 22.30047 |
| 990 | 6.23334 | 124.88688 | 20.07042 |
| 1000 | 5.87029 | 114.93213 | 17.84038 |
| 1010 | 5.74453 | 108.1448 | 15.84507 |
| 1020 | 5.65507 | 104.67572 | 13.96714 |
| 1030 | 5.5761 | 102.26244 | 12.55869 |
| 1040 | 5.46924 | 99.09502 | 11.26761 |
| 1050 | 5.4335 | 96.83258 | 9.85915 |
| 1060 | 5.35078 | 95.32428 | 7.98122 |
| 1070 | 5.27312 | 93.21267 | 5.98592 |
| 1080 | 5.23812 | 103.92157 | 6.10329 |
| 1090 | 6.19086 | 163.19759 | 9.50704 |
| 1100 | 7.29107 | 175.86727 | 18.66197 |
| 1110 1120 | 7.40561 7.44977 | 200.60332 | 24.1784 |
| 1130 | 7.50835 | 222.17195 239.51735 | 27.46479 30.98592 |
| 1140 | 7.61913 | 253.39367 | 33.33333 |
| 1150 | 7.71851 | 273.15234 | 36.38498 |
| 1160 | 7.85699 | 277.37557 | 39.55399 |
| 1170 | 7.9981 | 282.50377 | 42.37089 |
| 1180 | 8.12105 | 287.17949 | 44.13146 |
| 1190 | 8.17383 | 296.83258 | 45.07042 |
| 1200 | 8.30614 | 195.77677 | 37.55869 |
| 1210 | 7.77895 | 160.48265 | 27.8169 |
| 1220 | 6.85541 | 136.95324 | 21.00939 |
| 1230 | 6.45174 | 125.33937 | 16.90141 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|--------------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1240 | 6.27115 | 117.64706 | 13.96714 |
| 1250 | 6.19086 | 111.31222 | 11.73709 |
| 1260 | 6.13622 | 106.6365 | 10.32864 |
| 1270 | 6.02599 | 102.41327 | 9.03756 |
| 1280 | 6.13734 | 100 | 8.21596 |
| 1290 | 6.08619 | 95.77677 | 7.62911 |
| 1300 | 6.01757 | 93.96682 | 7.15962 |
| 1310 | 6.01813 | 92.76018 | 6.57277 |
| 1320 | 6.16204 | 98.19005 | 6.69014 |
| 1330 1340 | 6.57432 7.32532 | 161.99095 180.39216 | 14.08451 20.30516 |
| 1350 | 7.54783 | 198.79336 | 23.47418 |
| 1360 | 7.656 | 224.88688 | 27.34742 |
| 1370 | 7.72805 | 243.13725 | 29.92958 |
| 1380 | 7.76922 | 260.78431 | 31.57277 |
| 1390 | 7.85531 | 275.41478 | 35.79812 |
| 1400 | 7.94963 | 282.50377 | 38.61502 |
| 1410 | 8.06023 | 292.60935 | 41.5493 |
| 1420 | 8.03216 | 298.94419 | 43.07512 |
| 1430 | 8.09261 | 302.41327 | 43.89671 |
| 1440 | 8.19647 | 194.72097 | 34.85915 |
| 1450 | 8.16765 | 159.57768 | 23.59155 |
| 1460 | 7.06126 | 133.63499 | 18.30986 |
| 1470 | 6.74106 | 121.26697 | 15.96244 |
| 1480 | 6.63271 | 117.3454 | 13.84977 |
| 1490 | 6.59004 | 110.55807 | 11.50235 |
| 1500 | 6.47345 | 105.27903 | 9.50704 |
| 1510 | 6.42311 | 101.5083 | 6.80751 |
| 1520 | 6.35405 | 98.34087 | 3.87324 |
| 1530 | 6.30951 | 96.53092 | 3.05164 |
| 1540 | 6.285 | 94.11765 | 2.11268 |
| 1550 | 6.24476 | 92.00603 | 1.87793 |
| 1560 | 6.57844 7.2849 | 106.78733 | 1.99531 |
| 1570 1580 | 7.2849 7.49431 | 161.2368 183.55958 | 15.37559 |
| 1580 | 7.49431 7.61146 | 202.71493 | 22.53521 26.52582 |
| 1600 | 7.70335 | 229.41176 | 28.28638 |
| 1610 | 7.70333 | 252.63952 | 31.22066 |
| 1620 | 7.76473 | 256.1086 | 33.21596 |
| 1630 | 7.8525 | 269.98492 | 34.97653 |
| 1640 | 7.97995 | 279.93967 | 36.03286 |
| 1650 | 8.07483 | 290.04525 | 37.44131 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|-----------------------------------|-----------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1660 | 8.18767 | 294.26848 | 39.08451 |
| 1670 | 8.28312 | 297.73756 | 41.78404 |
| 1680 | 7.57366 | 195.62594 | 23.59155 |
| 1690 | 6.67968 | 162.59427 | 19.60094 |
| 1700 | 6.37146 | 138.61237 | 17.723 |
| 1710 | 6.21351 | 121.4178 | 15.61033 |
| 1720 | 6.18618 | 111.61388 | 14.55399 |
| 1730 | 6.12854 | 105.58069 | 12.55869 |
| 1740 | 6.22099 | 102.71493 | 11.38498 |
| 1750 | 6.11376 | 101.65913 | 8.09859 |
| 1760 | 6.12274 | 99.69834 | 7.39437 |
| 1770 | 6.09186 | 97.73756 | 5.39906 |
| 1780 | 6.0331 | 95.02262 | 4.46009 |
| 1790 | 5.94945 | 93.66516 | 3.40376 |

Appendix B. Phase Three Raw Data

| | Cyclobeyene DI | Cyclobovono DVA o | Cycloboxono DI/DVA o |
|----------|--------------------------------------|-----------------------------------|--------------------------------------|
| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | -0.27487 | 0.00348 | -0.14201 |
| 20 | -0.00598 | 0.00337 | -0.19112 |
| 30 | 0.86436 | 0.00532 | -0.19571 |
| 40 | 0.5856 | 0.00121 | -0.23577 |
| 50 | 0.2199 | -0.0011 | -0.27914 |
| 60 | 0.2112 | -3.91E-04 | -0.30082 |
| 70 | 0.30863 | 6.26E-04 | -0.33815 |
| 80 | -0.16433 | -0.00114 | -0.3304 |
| 90 | 0.81566 | -0.00153 | -0.3202 |
| 100 | 0.10547 | 0.04971 | -0.32049 |
| 110 | 0.1712 | 0.00407 | -0.39516 |
| 120 | 4.60114 | 0.15727 | 15.30917 |
| 130 | 27.01225 | 1.51934 | 25.75957 |
| 140 | 29.77592 | 2.6002 | 33.7144 |
| 150 | 32.18405 | 3.86527 | 38.80175 |
| 160 | 34.92979 | 4.27392 | 40.644 |
| 170 | 38.39558 | 5.35408 | 40.58513 |
| 180 | 43.28951 | 6.27392 | 40.97713 |
| 190 | 45.44368 | 6.67473 | 41.48112 |
| 200 | 47.32298 | 7.39416 | 40.756 |
| 210 | 49.40843 | 7.38946 | 41.46533 |
| 220 | 52.00777 | 7.64702 | 41.14943 |
| 230 | 54.55931 | 7.31783 | 41.28153 |
| 240 | 19.88647 | 6.14749 | 32.85861 |
| 250 | 10.84255 | 4.37788 | 24.47014 |
| 260 | 5.53331 | 3.27133 | 21.78072 |
| 270 | 3.58829 | 2.89596 | 19.24494 |
| 280 | 1.23693 | 2.60827 | 13.45687 |
| 290 | 0.34957 | 2.28887 | 4.86853 |
| 300 | -0.08157 | 2.45835 | 4.22209 |
| 310 | 0.98895 | 2.54916 | 3.35797 |
| 320 | -0.3914 | 2.4607 | 2.00895 |
| 330 | 0.22707 | 2.47166 | 1.82286 |
| 340 | -0.33762 | 2.6157 | 1.44853 |
| 350 | 0.00896 | 2.4564 | 1.25784 |
| 360 | 20.35853 | 3.34766 | 11.75965 |
| 370 | 35.64386 | 5.18342 | 19.90401 |

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|-----------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 380 | 41.51479 | 6.46963 | 22.79446 |
| 390 | 45.37496 | 6.62698 | 24.48019 |
| 400 | 46.08605 | 7.22663 | 25.34603 |
| 410 | 47.2931 | 8.51049 | 27.273 |
| 420 | 47.32596 | 9.41076 | 30.34293 |
| 430 | 46.93457 | 10.72201 | 38.14699 |
| 440 | 50.64535 | 11.02106 | 39.74944 |
| 450 | 54.2934 | 11.32911 | 40.08687 |
| 460 | 58.07888 | 11.01401 | 43.72111 |
| 470 | 58.59576 | 11.49311 | 47.65832 |
| 480 | 16.19958 | 9.50626 | 40.52626 |
| 490 | 8.87959 | 8.18757 | 26.23916 |
| 500 | 4.91485 | 7.12447 | 20.13663 |
| 510 | 2.85928 | 6.39291 | 9.74366 |
| 520 | 1.49089 | 5.81674 | 4.97995 |
| 530 | 0.25993 | 4.84523 | 3.1693 |
| 540 | 0.20317 | 4.6507 | 1.98813 |
| 550 | -0.12847 | 4.92469 | 1.64481 |
| 560 | 0.33463 | 4.6049 | 1.51257 |
| 570 | 0.14341 | 4.24636 | 1.4211 |
| 580 | 0.88437 | 4.05809 | 1.27507 |
| 590 | 0.10457 | 4.1532 | 1.29704 |
| 600 | 25.4885 | 5.89815 | 9.1133 |
| 610 | 31.08455 | 8.56842 | 14.01399 |
| 620 | 34.5862 | 9.0346 | 23.0802 |
| 630 | 38.93158 | 9.47338 | 29.53309 |
| 640 | 45.47356 | 9.87615 | 30.93882 |
| 650 | 54.61607 | 10.04251 | 30.99052 |
| 660 | 57.62773 | 10.44763 | 32.84568 |
| 670 | 56.42068 | 10.56466 | 34.54291 |
| 680 | 59.18733 | 10.2484 | 37.07151 |
| 690 | 61.54765 | 10.77955 | 40.91969 |
| 700 | 61.88527 | 10.23978 | 44.58982 |
| 710 | 61.25067 | 10.05425 | 47.49606 |
| 720 | 36.54019 | 6.82347 | 32.58292 |
| 730 | 13.01763 | 6.11359 | 18.60022 |
| 740 | 5.10607 | 5.969 | 8.1728 |
| 750 | 3.65103 | 5.40692 | 5.7605 |
| 760 | 1.98387 | 5.41514 | 3.78931 |

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|-----------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 770 | 0.65432 | 5.07147 | 3.38525 |
| 780 | -0.1213 | 4.76147 | 3.53071 |
| 790 | 0.61906 | 2.56756 | 3.39875 |
| 800 | -0.5853 | 1.28425 | 3.60537 |
| 810 | -0.87093 | 0.93886 | 3.37334 |
| 820 | 0.4389 | 1.49507 | 3.2945 |
| 830 | -0.196 | 1.98473 | 3.46523 |
| 840 | 25.81416 | 1.85243 | 13.12949 |
| 850 | 36.81506 | 2.11625 | 20.86031 |
| 860 | 45.57813 | 3.29756 | 36.09223 |
| 870 | 50.76188 | 5.66721 | 41.47682 |
| 880 | 53.3911 | 7.42234 | 42.7246 |
| 890 | 54.44876 | 8.51597 | 44.56111 |
| 900 | 54.26352 | 9.21661 | 43.67229 |
| 910 | 56.92262 | 10.31572 | 43.6048 |
| 920 | 59.12758 | 10.98152 | 43.67229 |
| 930 | 58.8769 | 10.93377 | 44.56111 |
| 940 | 59.13953 | 11.15062 | 44.40747 |
| 950 | 60.57783 | 11.27979 | 44.7534 |
| 960 | 25.40185 | 9.84562 | 27.96366 |
| 970 | 17.01225 | 7.75818 | 24.6166 |
| 980 | 10.36719 | 6.53264 | 21.52944 |
| 990 | 5.73648 | 5.98505 | 19.69294 |
| 1000 | 3.50164 | 4.4041 | 18.31018 |
| 1010 | 1.81655 | 2.87522 | 14.76927 |
| 1020 | 1.90917 | 2.21058 | 5.92276 |
| 1030 | -0.25695 | 1.56083 | 5.00235 |
| 1040 | 1.00388 | 1.92132 | 4.30997 |
| 1050 | -0.50194 | 1.44035 | 3.7784 |
| 1060 | 0.08664 | 1.26386 | 3.04121 |
| 1070 | 0.55244 | 1.31568 | 2.75346 |
| 1080 | 18.72722 | 4.31916 | 2.354 |
| 1090 | 24.87601 | 5.18812 | 7.1088 |
| 1100 | 30.69615 | 6.54556 | 16.18793 |
| 1110 | 33.13415 | 7.20784 | 27.76981 |
| 1120 | 35.88288 | 8.47135 | 38.09099 |
| 1130 | 38.50612 | 8.9571 | 45.40397 |
| 1140 | 42.3663 | 8.41271 | 51.87266 |
| 1150 | 46.99432 | 8.47957 | 57.8876 |

| | Cyclohexane-PI | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|-----------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1160 | 50.88886 | 8.59112 | 58.98749 |
| 1170 | 53.2686 | 8.58251 | 59.02338 |
| 1180 | 55.88497 | 8.74495 | 58.0398 |
| 1190 | 58.14759 | 8.65492 | 57.8876 |
| 1200 | 25.366 | 4.39745 | 50.76415 |
| 1210 | 12.17209 | 2.58361 | 39.14206 |
| 1220 | 6.8778 | 2.37459 | 33.66558 |
| 1230 | 4.42187 | 1.90332 | 21.33129 |
| 1240 | 2.68898 | 1.64929 | 15.45276 |
| 1250 | 1.83956 | 1.30977 | 11.23698 |
| 1260 | 0.39767 | 1.60788 | 6.85465 |
| 1270 | -0.6833 | 1.38508 | 6.53301 |
| 1280 | 0.20795 | 1.6316 | 5.95004 |
| 1290 | 0.99821 | 1.10897 | 4.34184 |
| 1300 | -0.3173 | 0.98505 | 3.81485 |
| 1310 | 0.30714 | 0.97002 | 3.40851 |
| 1320 | 13.80341 | 2.00219 | 10.74591 |
| 1330 | 22.01972 | 4.41232 | 23.07158 |
| 1340 | 30.23304 | 4.66792 | 31.65246 |
| 1350 | 35.07918 | 5.11688 | 39.07314 |
| 1360 | 38.91455 | 5.59167 | 42.87824 |
| 1370 | 43.75859 | 6.39878 | 46.73217 |
| 1380 | 47.67254 | 6.69274 | 49.61257 |
| 1390 | 49.84165 | 7.76444 | 53.64741 |
| 1400 | 53.87093 | 8.13042 | 55.16659 |
| 1410 | 59.93427 | 7.94411 | 57.66791 |
| 1420 | 58.63161 | 8.02669 | 57.62196 |
| 1430 | 62.20496 | 8.16213 | 58.63569 |
| 1440 | 25.35405 | 5.03468 | 52.53316 |
| 1450 | 19.92232 | 3.022 | 36.93653 |
| 1460 | 12.65611 | 1.81016 | 18.24987 |
| 1470 | 6.02928 | 1.50579 | 13.10938 |
| 1480 | 2.62324 | 1.2051 | 5.99312 |
| 1490 | 1.69704 | 1.08365 | 2.75949 |
| 1500 | 0.84255 | 1.21505 | 2.13115 |
| 1510 | 0.50792 | 1.38383 | 2.29398 |
| 1520 | 0.60353 | 1.0303 | 2.3583 |
| 1530 | 1.00388 | 1.06325 | 2.29225 |
| 1540 | -0.57365 | 1.10717 | 2.58747 |

| | Cyclohexane-PI | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|-----------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1550 | 0.02091 | 1.55817 | 2.12914 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|-----------------------------------|-----------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | 0 | -0.09963 | 0.04168 |
| 20 | -0.01852 | 0.16028 | 0.06252 |
| 30 | -0.01852 | -0.40286 | 0.06252 |
| 40 | 0 | 0.37687 | 0.08336 |
| 50 | -0.01852 | 0.08332 | 0.08336 |
| 60 | -0.03705 | 0.55014 | 0.04168 |
| 70 | 0 | 0.59346 | 0.06252 |
| 80 | -0.11114 | 0.55014 | 0.04168 |
| 90 | -0.05557 | 0.03355 | 0 |
| 100 | -0.0741 | 0.01696 | 0 |
| 110 | -0.03705 | 0.03032 | 0.02084 |
| 120 | 2.98237 | 5.40178 | 12.77462 |
| 130 | 7.00207 | 8.34741 | 20.13096 |
| 140 | 9.35522 | 11.11977 | 25.57008 |
| 150 | 11.8933 | 14.91423 | 28.07082 |
| 160 | 12.5243 | 17.17804 | 30.50904 |
| 170 | 13.52816 | 21.73273 | 33.0723 |
| 180 | 14.40776 | 26.90882 | 35.78144 |
| 190 | 14.01874 | 34.55491 | 38.42805 |
| 200 | 15.95392 | 38.71345 | 42.15803 |
| 210 | 15.99096 | 39.36322 | 43.92968 |
| 220 | 15.95392 | 39.96968 | 45.6805 |
| 230 | 16.00948 | 39.3199 | 20.10262 |
| 240 | 8.75852 | 24.72168 | 17.10173 |
| 250 | 7.60077 | 16.70782 | 15.20534 |
| 260 | 6.75793 | 13.93546 | 13.97581 |
| 270 | 6.21147 | 12.50596 | 12.82963 |
| 280 | 5.70206 | 11.76955 | 12.01689 |
| 290 | 5.34084 | 10.59996 | 11.32919 |
| 300 | 5.0352 | 9.34373 | 10.68317 |
| 310 | 4.74807 | 9.17046 | 10.1205 |
| 320 | 4.498 | 8.91055 | 9.74539 |
| 330 | 4.33128 | 8.21746 | 9.26608 |
| 340 | 4.11826 | 8.30409 | 8.93151 |
| 350 | 3.96956 | 8.04418 | 5.40963 |
| 360 | 4.50046 | 12.89582 | 12.84934 |
| 370 | 5.08396 | 19.65345 | 19.87225 |
| 380 | 6.14909 | 23.63873 | 21.42104 |
| 390 | 7.34389 | 27.58068 | 23.54667 |

| , | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|------------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 400 | 8.25157 | 30.9595 | 25.60978 |
| 410 | 9.52046 | 33.49144 | 29.96524 |
| 420 | 11.38213 | 36.22049 | 31.56988 |
| 430 | 14.16073 | 40.58631 | 35.32099 |
| 440 | 15.79024 | 42.98895 | 32.4243 |
| 450 | 14.7066 | 45.70804 | 31.56988 |
| 460 | 15.5581 | 49.43513 | 33.84139 |
| 470 | 14.03972 | 50.45267 | 32.50766 |
| 480 | 11.57663 | 31.9125 | 26.27665 |
| 490 | 9.5581 | 20.56314 | 17.29751 |
| 500 | 8.68777 | 15.40827 | 12.58911 |
| 510 | 8.06751 | 11.46632 | 9.15191 |
| 520 | 7.58589 | 10.34005 | 8.94351 |
| 530 | 7.14161 | 9.9935 | 9.86045 |
| 540 | 6.03973 | 8.95387 | 10.02717 |
| 550 | 5.5584 | 8.60732 | 9.03146 |
| 560 | 5.14161 | 7.69764 | 9.52702 |
| 570 | 5.08604 | 7.26446 | 9.88129 |
| 580 590 | 4.7584 4.39168 | 6.52805 6.27182 | 9.90213 10.04801 |
| 600 | 6.47564 | 11.63959 | 14.57018 |
| 610 | 8.55032 | 23.10158 | 21.73897 |
| 620 | 9.73586 | 31.436 | 24.03132 |
| 630 | 10.7269 | 38.45354 | 26.90717 |
| 640 | 11.579 | 40.966 | 29.7205 |
| 650 | 12.34775 | 44.20836 | 30.84584 |
| 660 | 12.92199 | 46.73554 | 31.47102 |
| 670 | 13.30173 | 49.27009 | 32.82559 |
| 680 | 13.72778 | 51.39268 | 33.68001 |
| 690 | 14.02417 | 52.09682 | 35.0971 |
| 700 | 14.4317 | 52.86918 | 35.36801 |
| 710 | 14.30203 | 52.40004 | 37.01433 |
| 720 | 12.00742 | 36.46091 | 26.49571 |
| 730 | 10.21059 | 27.58068 | 23.36979 |
| 740 | 9.39554 | 18.6175 | 20.34835 |
| 750 | 8.89539 | 14.54191 | 19.22302 |
| 760 | 8.65458 | 11.59627 | 18.27287 |
| 770 | 8.49712 | 9.90687 | 17.20189 |
| 780 | 8.34893 | 9.0405 | 16.39097 |
| 790 | 8.32115 | 8.30409 | 15.7851 |
| 800 | 8.46008 | 7.87091 | 14.47342 |
| 810 | 8.29336 | 7.77691 | 13.02677 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|--------------|--------------------------------------|--------------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 820 | 8.36746 | 7.40286 | 12.03517 |
| 830 | 8.33967 | 7.44813 | 11.76426 |
| 840 | 9.57152 | 13.37232 | 23.24475 |
| 850 | 10.65517 | 20.34655 | 30.20515 |
| 860 | 11.0627 | 32.82218 | 31.72643 |
| 870 | 11.39613 | 39.70977 | 33.14352 |
| 880 | 12.04447 | 43.95495 | 35.99853 |
| 890 | 12.60019 | 47.46372 | 35.74845 |
| 900 | 13.07255 | 50.66927 | 36.89463 |
| 910 | 13.42451 | 53.91813 | 37.22806 |
| 920 930 | 13.94318 14.00802 | 56.20663 58.20663 | 37.39811 37.64818 |
| 940 | 14.10064 | 60.67576 | 36.66873 |
| 950 | 14.14695 | 62.79835 | 38.12749 |
| 960 | 12.99994 | 35.20468 | 33.35525 |
| 970 | 12.29603 | 29.40004 | 29.24986 |
| 980 | 10.92555 | 23.42214 | 24.66606 |
| 990 | 10.74957 | 19.09032 | 20.83248 |
| 1000 | 10.56997 | 17.44423 | 17.43653 |
| 1010 | 10.35333 | 15.14836 | 15.70744 |
| 1020 | 10.16259 | 13.02577 | 14.895 |
| 1030 | 9.97186 | 11.59627 | 12.91584 |
| 1040 | 9.84219 | 9.90687 | 11.93668 |
| 1050 | 9.89776 | 8.82391 | 11.33263 |
| 1060 | 9.79588 | 8.39073 | 11.87416 |
| 1070 | 9.74957 | 8.79532 | 11.83248 |
| 1080 | 11.37968 | 14.67186 | 11.7911 |
| 1090 | 12.7406 | 23.50877 | 19.16947 |
| 1100 | 13.03788 | 31.16959 | 32.50379 |
| 1110 | 14.1299 | 38.23695 | 38.42073 |
| 1120 | 14.90791 | 43.50509 | 40.15011 |
| 1130 | 15.45437 | 47.85358 | 42.79614 |
| 1140 | 16.50098 | 49.93286 | 45.12957 |
| 1150 | 17.23267 | 51.57895 | 45.3588 |
| 1160 | 17.79766 | 53.09508 | 45.52552 |
| 1170 | 18.15887 | 53.44163 | 46.40078 |
| 1180 | 18.55714 | 54.39463 | 47.38023 |
| 1190 | 18.95541 | 55.30431 | 47.90122 |
| 1200 1210 | 16.26016 15.1302 | 33.47195 | 38.25253 34.04354 |
| 1210 | 14.55422 | 23.85532 15.14836 | |
| 1230 | 13.94496 | 12.33268 | 32.04295 |
| 1230 | 13.94490 | 12.33208 | 30.88449 |

| | Ethanol-PI | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1240 | 13.70415 | 10.45267 | 28.5431 |
| 1250 | 13.43758 | 8.60732 | 26.447 |
| 1260 | 13.04684 | 8.26078 | 23.60532 |
| 1270 | 12.95422 | 8.1815 | 22.33456 |
| 1280 | 12.92644 | 8.26446 | 21.2368 |
| 1290 | 12.98201 | 8.0875 | 20.85539 |
| 1300 | 12.9357 | 8.26078 | 18.9529 |
| 1310 | 13.00053 | 8.39073 | 17.14685 |
| 1320 | 14.02921 | 15.84146 | 27.56453 |
| 1330 | 14.94615 | 22.64241 | 34.12897 |
| 1340 | 15.53891 | 29.31341 | 36.62972 |
| 1350 | 16.30766 | 35.98441 | 38.13016 |
| 1360 | 16.99305 | 39.44986 | 40.21411 |
| 1370 | 17.92851 | 43.52177 | 41.97447 |
| 1380 | 18.02113 | 45.16786 | 42.70385 |
| 1390 | 18.19711 | 47.20381 | 43.45407 |
| 1400 | 18.39161 | 48.50336 | 44.05842 |
| 1410 | 18.42866 | 49.3264 | 44.53773 |
| 1420 | 18.53054 | 50.06281 | 44.93368 |
| 1430 | 18.46571 | 51.31904 | 45.37131 |
| 1440 | 17.14124 | 34.85813 | 39.88068 |
| 1450 | 15.74268 | 27.97054 | 33.42102 |
| 1460 | 14.82574 | 21.77605 | 29.35791 |
| 1470 | 14.22371 | 18.39723 | 26.00335 |
| 1480 | 13.91806 | 15.65086 | 24.31564 |
| 1490 | 13.61242 | 13.45896 | 22.62794 |
| 1500 | 13.39939 | 11.72623 | 21.14863 |
| 1510 | 13.13079 | 10.38337 | 19.8152 |
| 1520 | 13.07522 | 9.56032 | 18.35673 |
| 1530 | 12.95481 | 9.47368 | 17.14833 |
| 1540 | 12.86219 | 9.69028 | 16.93994 |
| 1550 | 12.7881 | 9.77691 | 16.44009 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|-----------------------------------|-----------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | 0.00926 | -0.09448 | 0.00578 |
| 20 | 0.01389 | -0.04973 | -0.14456 |
| 30 | 0.01389 | 0.17405 | 0.61871 |
| 40 | 0.01852 | -0.57684 | 0.11998 |
| 50 | 0.01852 | -0.04973 | 0.14167 |
| 60 | 0.00926 | 0.69121 | -0.00578 |
| 70 | 0.01389 | 0.11935 | -0.36284 |
| 80 | 0.00926 | 0.04475 | -0.31369 |
| 90 | 0 | -0.02486 | 0.0477 |
| 100 | 0 | 0.00497 | 0.17781 |
| 110 | 0.00463 | 98.93782 | -0.27611 |
| 120 | 2.8388 | 313.74667 | 55.4889 |
| 130 | 4.47355 | 370.58519 | 59.87481 |
| 140 | 5.68224 | 413.04849 | 61.75552 |
| 150 | 6.23796 | 473.51514 | 63.05944 |
| 160 | 6.77979 | 447.15957 | 65.29143 |
| 170 | 7.3494 | 428.81012 | 66.79484 |
| 180 | 7.95143 | 450.24267 | 69.58483 |
| 190 | 8.53957 | 425.72702 | 71.56528 |
| 200 | 9.14623 | 426.57238 | 73.06869 |
| 210 | 9.76215 | 418.91435 | 73.76258 |
| 220 | 10.37344 | 410.26177 | 75.45391 |
| 230 | 4.46725 | 418.61598 | 76.87059 |
| 240 | 3.80039 | 354.91507 | 59.04649 |
| 250 | 3.37896 | 325.92394 | 48.69753 |
| 260 | 3.10574 | 282.31293 | 29.20088 |
| 270 | 2.85103 | 280.8211 | 24.17168 |
| 280 | 2.67042 | 270.97506 | 20.60252 |
| 290 | 2.5176 | 258.64264 | 18.60038 |
| 300 | 2.37404 | 249.44305 | 17.40633 |
| 310 | 2.249 | 239.84565 | 16.81074 |
| 320 | 2.16564 | 230.79524 | 16.72256 |
| 330 | 2.05913 | 223.63448 | 16.44935 |
| 340 | 1.98478 | 222.29184 | 16.21082 |
| 350 | 1.20214 | 221.4962 | 16.07349 |
| 360 | 2.85541 | 227.29443 | 34.63051 |
| 370 | 4.41606 | 386.79039 | 72.53383 |
| 380 | 4.76023 | 418.6677 | 80.73031 |
| 390 | 5.23259 | 464.74599 | 82.81196 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|------------|-----------------------------------|--------------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 400 | 5.69106 | 483.55054 | 84.87915 |
| 410 | 6.65894 | 461.08326 | 86.83069 |
| 420 | 7.01553 | 446.01583 | 88.76778 |
| 430 | 7.84911 | 464.11664 | 92.38175 |
| 440 | 7.2054 | 446.46338 | 90.14109 |
| 450 | 7.01553 | 434.3796 | 90.82052 |
| 460 | 7.52031 | 446.06556 | 91.03735 |
| 470 | 7.22392 | 442.38573 | 90.86978 |
| 480 | 5.83926 | 362.62283 | 68.78975 |
| 490 | 3.84389 | 338.05745 | 34.38476 |
| 500 | 2.79758 | 331.99069 | 26.4427 |
| 510 | 2.03376 | 323.33811 | 21.98161 |
| 520 | 1.98745 | 316.12762 | 22.08136 |
| 530 | 2.19121 | 306.97776 | 20.10379 |
| 540 | 2.22826 | 302.40283 | 20.80924 |
| 550 | 2.00699 | 296.53499 | 19.83636 |
| 560 | 2.11712 | 296.08744 | 19.30149 |
| 570 | 2.19584 | 295.2918 | 19.12802 |
| 580 | 2.20047 | 295.24207 | 19.29282 |
| 590 | 2.23289 | 293.15352 | 18.92419 |
| 600 | 3.23782 | 443.28082 | 51.52943 |
| 610 | 4.83088 | 464.68473 | 85.09599 |
| 620 | 5.34029 | 486.17178 | 91.83243 |
| 630 | 5.97937 | 494.53555 | 94.30438 |
| 640 | 6.60456 | 490.72901 | 95.82225 |
| 650 | 6.85463 | 481.2583 | 97.06546 |
| 660 | 6.99356 | 488.91021 | 95.34521 |
| 670 | 7.29458 | 498.41429 | 96.53059 |
| 680 | 7.48445 | 486.76238 | 98.04846 |
| 690 700 | 7.79935 7.85956 | 468.19628 471.92585 | 99.45068 100.65051 |
| 710 | 8.22541 | 471.92565 | 104.81381 |
| 720 | 5.88794 | | 47.69429 |
| 730 | 5.19329 | 455.86188 398.22771 | 35.34174 |
| 740 | 4.74408 | 315.97844 | 28.22366 |
| 750 | 4.74406 | 285.84358 | 27.82034 |
| 760 | 4.38286 | 258.19509 | 24.07338 |
| 770 | 4.26709 | 245.61404 | 19.86816 |
| 780 | 4.20688 | 239.34837 | 19.81323 |
| 790 | 4.17447 | 236.46418 | 20.07054 |
| 800 | 4.17447 | 233.18216 | 19.67301 |
| 810 | 4.18373 | 227.71214 | 20.34087 |
| 010 | 4.10373 | 221.11214 | 20.34007 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|--------------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 820 | 4.23004 | 225.02685 | 18.62929 |
| 830 | 4.16983 | 223.08748 | 17.81254 |
| 840 | 5.1655 | 408.76994 | 37.221 |
| 850 | 6.71225 | 470.33258 | 82.19729 |
| 860 | 7.05032 | 430.30195 | 99.03146 |
| 870 | 7.36523 | 421.54991 | 104.94391 |
| 880 | 7.99967 | 414.4886 | 106.47623 |
| 890 | 7.9441 | 408.37212 | 108.09529 |
| 900 | 8.19881 | 408.17321 | 107.6327 |
| 910 | 8.2729 | 405.18956 | 107.90737 |
| 920 | 8.31069 | 398.52608 | 103.85972 |
| 930 | 8.36626 8.14861 | 402.60373 | 107.34551 |
| 940 950 | 8.47278 | 425.57783 399.86872 | 105.93848 102.5876 |
| 960 | 7.41228 | 283.95393 | 38.07101 |
| 970 | 6.49997 | 254.61471 | 27.1944 |
| 980 | 6.14801 | 239.14946 | 23.39829 |
| 990 | 5.96277 | 227.86132 | 22.16376 |
| 1000 | 5.87478 | 218.36337 | 22.7497 |
| 1010 | 5.93499 | 217.41357 | 20.85887 |
| 1020 | 5.97667 | 205.84199 | 19.64361 |
| 1030 | 5.9813 | 202.75888 | 17.98601 |
| 1040 | 5.98593 | 199.80507 | 17.1813 |
| 1050 | 6.07392 | 192.65425 | 17.90602 |
| 1060 | 5.97204 | 189.04404 | 16.93555 |
| 1070 | 5.96277 | 188.7407 | 16.21468 |
| 1080 | 6.1758 | 204.36508 | 90.45141 |
| 1090 | 8.70433 | 398.67526 | 97.52515 |
| 1100 | 9.44529 | 382.51382 | 99.07675 |
| 1110 | 9.64905 | 388.77949 | 100.57053 |
| 1120 | 9.81114 | 376.79516 | 102.57507 |
| 1130 | 9.9547 | 382.21546 | 105.69754 |
| 1140 | 10.02879 | 387.5363 | 105.89029 |
| 1150 | 10.07973 | 389.22704 | 105.20604 |
| 1160 | 10.11678 | 383.5581 | 104.27177 |
| 1170 1180 | 10.31128 10.52894 | 385.74611 | 105.52407 104.19413 |
| 1190 | 10.52694 | 387.18821 394.3987 | 105.20604 |
| 1200 | 9.56569 | 394.3967 | 35.22898 |
| 1210 | 8.50056 | 260.97983 | 26.6393 |
| 1210 | 8.00968 | 243.3763 | 22.38927 |
| | | | |
| 1230 | 7.85222 | 235.9669 | 19.41425 |

| • | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1240 | 7.67624 | 225.97168 | 19.00274 |
| 1250 | 7.5651 | 223.78367 | 19.37859 |
| 1260 | 6.86322 | 190.02367 | 18.82156 |
| 1270 | 6.51879 | 180.66993 | 18.4804 |
| 1280 | 5.87711 | 174.85181 | 18.17393 |
| 1290 | 5.52342 | 171.11787 | 17.60148 |
| 1300 | 5.46785 | 166.57716 | 16.53849 |
| 1310 | 5.36597 | 168.29773 | 16.82954 |
| 1320 | 6.12545 | 204.07169 | 25.05686 |
| 1330 | 7.58422 | 349.94232 | 95.87718 |
| 1340 | 8.13994 | 365.40757 | 96.59998 |
| 1350 | 8.47337 | 364.71138 | 95.38568 |
| 1360 | 8.93647 | 366.13578 | 101.55353 |
| 1370 | 9.32766 | 361.52882 | 104.3676 |
| 1380 | 9.48974 | 374.75634 | 104.64708 |
| 1390 | 9.65646 | 376.29789 | 104.20377 |
| 1400 | 9.79076 | 377.0438 | 107.26842 |
| 1410 | 9.89727 | 386.24339 | 110.80529 |
| 1420 | 9.98526 | 384.15483 | 110.05358 |
| 1430 | 10.08251 | 384.50292 | 113.43626 |
| 1440 | 8.86237 | 288.13104 | 41.90471 |
| 1450 | 7.87134 | 253.96825 | 27.94804 |
| 1460 | 7.41287 | 244.96758 | 23.38576 |
| 1470 | 7.11185 | 232.13788 | 20.62372 |
| 1480 | 6.95903 | 227.86132 | 17.63714 |
| 1490 | 6.80621 | 218.81092 | 17.00204 |
| 1500 | 6.6997 | 213.04253 | 17.53787 |
| 1510 | 6.6256 | 212.94307 | 17.25743 |
| 1520 | 6.52372 | 211.79934 | 16.25805 |
| 1530 | 6.47741 | 210.75506 | 15.82052 |
| 1540 | 6.4311 | 209.21351 | 16.53656 |
| 1550 | 6.54224 | 208.08967 | 15.92302 |

Appendix C. Phase Four Raw Data

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | -0.04979 | 0 | -0.07054 |
| 20 | -0.08299 | 0.01663 | -0.09959 |
| 30 | -0.07469 | 0.01996 | -0.08714 |
| 40 | -0.11618 | 0.00998 | -0.12864 |
| 50 | -0.21577 | 0.02662 | -0.23237 |
| 60 | -0.48133 | 0.0366 | -0.49795 |
| 70 | -0.62241 | 0.01331 | -0.63903 |
| 80 | -0.6556 | 0.02662 | -0.66393 |
| 90 | -0.6556 | 0.02662 | -0.67223 |
| 100 | -0.70539 | 0.02994 | -0.70957 |
| 110 | -0.72199 | 0.04658 | -0.37761 |
| 120 | 5.48548 | 0.32604 | 6.10814 |
| 130 | 5.54357 | 0.38592 | 7.80945 |
| 140 | 11.73444 | 1.01803 | 8.37379 |
| 150 | 14.55602 | 1.01138 | 8.60202 |
| 160 | 15.48548 | 1.19436 | 8.80534 |
| 170 | 16.29876 | 1.29084 | 8.95888 |
| 180 | 16.59751 | 1.3108 | 9.02112 |
| 190 | 16.96266 | 1.34407 | 8.94643 |
| 200 | 17.03734 | 1.36403 | 9.05017 |
| 210 | 17.27801 | 1.43057 | 9.11241 |
| 220 | 17.39419 | 1.42391 | 9.2037 |
| 230 | 17.45228 | 1.43057 | 7.75966 |
| 240 | 17.47718 | 1.43057 | 7.13308 |
| 250 | 17.53527 | 1.29084 | 6.77207 |
| 260 | 15.29461 | 1.19103 | 6.4899 |
| 270 | 14.6805 | 1.14113 | 6.28242 |
| 280 | 14.18257 | 1.11784 | 6.10814 |
| 290 | 13.91701 | 1.07459 | 5.9878 |
| 300 | 13.56846 | 1.02801 | 5.86746 |
| 310 | 13.361 | 0.94151 | 5.74298 |
| 320 | 13.24481 | 0.97811 | 5.60604 |
| 330 | 13.17012 | 0.94151 | 5.5687 |
| 340 | 12.97925 | 0.90159 | 5.36122 |
| 350 | 12.78008 | 0.89494 | 9.37383 |
| 360 | 12.6805 | 0.87498 | 13.34495 |
| 370 | 12.45643 | 1.03134 | 15.12926 |

| | Cyclohexane-PI | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 380 | 18.38174 | 1.04465 | 15.91352 |
| 390 | 19.74274 | 1.08457 | 16.50276 |
| 400 | 20.86307 | 1.1378 | 16.76418 |
| 410 | 21.56846 | 1.15111 | 17.00071 |
| 420 | 22.20747 | 1.15111 | 17.12934 |
| 430 | 22.99585 | 1.16442 | 17.30777 |
| 440 | 23.42739 | 1.20434 | 17.40736 |
| 450 | 23.9668 | 1.19768 | 17.49035 |
| 460 | 24.50622 | 1.27088 | 17.5277 |
| 470 | 24.77178 | 1.29749 | 16.1293 |
| 480 | 25.07884 | 0.94484 | 14.79314 |
| 490 | 24.41494 | 0.79846 | 14.39064 |
| 500 | 21.65145 | 0.73525 | 14.01303 |
| 510 | 20.84647 | 0.71861 | 13.72671 |
| 520 | 20.40664 | 0.75853 | 13.49019 |
| 530 | 19.9917 | 0.74523 | 13.29101 |
| 540 | 19.76763 | 0.76851 | 13.21632 |
| 550 | 19.56846 | 0.74523 | 13.09598 |
| 560 | 19.3112 | 0.76519 | 12.8719 |
| 570 | 19.17012 | 0.76519 | 12.71837 |
| 580 | 19.10373 | 0.77184 | 12.60218 |
| 590 | 19.07054 | 0.75188 | 16.28283 |
| 600 | 18.86307 | 0.97811 | 19.20412 |
| 610 | 18.71369 | 1.01138 | 20.32035 |
| 620 | 23.22822 | 1.09788 | 21.10461 |
| 630 | 24.08299 | 1.14445 | 21.84738 |
| 640 | 24.62241 | 1.15776 | 22.5611 |
| 650 | 25.07054 | 1.15111 | 23.20428 |
| 660 | 25.3029 | 1.21432 | 23.86406 |
| 670 | 25.49378 | 1.21099 | 24.23752 |
| 680 | 25.73444 | 1.24093 | 24.59023 |
| 690 | 25.92531 | 1.26422 | 24.94294 |
| 700 | 26.25726 | 1.2742 | 25.24586 |
| 710 | 26.30705 | 1.28418 | 22.38682 |
| 720 | 26.6888 | 0.90492 | 21.24569 |
| 730 | 25.12033 | 0.81176 | 20.63156 |
| 740 | 22.46473 | 0.71861 | 20.12117 |
| 750 | 21.88382 | 0.66871 | 19.8307 |
| 760 | 21.51867 | 0.67203 | 19.66887 |

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|--------------------------------------|-----------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 770 | 21.29461 | 0.6188 | 19.49044 |
| 780 | 21.00415 | 0.59884 | 19.25391 |
| 790 | 20.80498 | 0.58553 | 19.16262 |
| 800 | 20.6805 | 0.57555 | 19.06718 |
| 810 | 20.54772 | 0.57888 | 18.98004 |
| 820 | 20.43983 | 0.59219 | 18.79331 |
| 830 | 20.34855 | 0.57555 | 21.31209 |
| 840 | 20.18257 | 0.59884 | 23.63584 |
| 850 | 20.22407 | 0.73857 | 24.34541 |
| 860 | 24.24066 | 0.85834 | 24.81431 |
| 870 | 24.6556 | 0.89161 | 25.05083 |
| 880 | 24.95436 | 0.92821 | 25.28736 |
| 890 | 25.17012 | 0.97146 | 25.68156 |
| 900 | 25.40249 | 0.99807 | 25.87244 |
| 910 | 25.44398 | 1.01138 | 26.03842 |
| 920 | 25.80083 | 1.00805 | 26.20856 |
| 930 | 25.71784 | 1.00472 | 26.42848 |
| 940 | 25.84232 | 1.01138 | 26.60276 |
| 950 | 25.70954 | 1.00472 | 23.41591 |
| 960 | 25.76763 | 0.94484 | 22.10465 |
| 970 | 23.78423 | 0.93153 | 21.698 |
| 980 | 21.72614 | 0.81842 | 21.33698 |
| 990 | 20.89627 | 0.72526 | 21.15026 |
| 1000 | 20.53942 | 0.58553 | 20.93033 |
| 1010 | 20.32365 | 0.51234 | 20.74775 |
| 1020 | 20.12448 | 0.46577 | 20.59837 |
| 1030 | 19.91701 | 0.41254 | 20.47388 |
| 1040 | 19.69295 | 0.41919 | 20.37014 |
| 1050 | 19.63485 | 0.43915 | 20.29545 |
| 1060 | 19.64315 | 0.40588 | 20.15436 |
| 1070 | 19.46058 | 0.41254 | 23.9346 |
| 1080 | 19.3527 | 0.49904 | 24.59853 |
| 1090 | 20.45643 | 0.56557 | 24.80601 |
| 1100 | 23.50207 | 0.68534 | 25.08403 |
| 1110 | 24.16598 | 0.72526 | 25.37865 |
| 1120 | 24.47303 | 0.80511 | 25.46164 |
| 1130 | 24.53942 | 0.84503 | 25.75626 |
| 1140 | 24.63071 | 0.87165 | 25.66911 |
| 1150 | 24.6888 | 0.93819 | 25.7936 |

| | Cyclohexane-Pl | Cyclohexane-PVAc | Cyclohexane-PI/PVAc |
|----------|---|------------------|--------------------------------------|
| time (s) | (s) Change of Change of Relative Resistance (%) | | Change of Relative Resistance (%) |
| 1160 | 24.78838 | 0.93819 | 25.78945 |
| 1170 | 24.78838 | 1.01138 | 25.68571 |
| 1180 | 24.78008 | 1.02469 | 25.82265 |
| 1190 | 24.83817 | 1.05795 | 22.22499 |
| 1200 | 24.97925 | 1.0513 | 21.25814 |
| 1210 | 24.42324 | 0.75853 | 20.85149 |
| 1220 | 20.6722 | 0.69865 | 20.53612 |
| 1230 | 20 | 0.55559 | 20.30375 |
| 1240 | 19.49378 | 0.52565 | 20.06307 |
| 1250 | 19.27801 | 0.48573 | 19.8307 |
| 1260 | 19.11203 | 0.48573 | 19.69376 |
| 1270 | 19.07884 | 0.519 | 19.63152 |
| 1280 | 19.00415 | 0.47242 | 19.54853 |
| 1290 | 18.90456 | 0.46577 | 19.3784 |
| 1300 | 18.80498 | 0.43915 | 19.22486 |
| 1310 | 18.73029 | 0.39923 | 22.98436 |

| | Ethanol-PI Ethanol-PVAc | | Ethanol-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|-----------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 0 | 0 | 0 | 0 |
| 10 | 0.03165 | 0.03517 | 0 |
| 20 | 0.1864 | 0 | -0.01054 |
| 30 | 0.04572 | 0 | 0.05268 |
| 40 | 0.04572 | -0.03517 | 0.07901 |
| 50 | 0.03165 | -0.07033 | 0.14749 |
| 60 | 0.03869 | -0.07033 | 0.15276 |
| 70 | 0.02814 | -0.14067 | 0.13169 |
| 80 | 0.05276 | -0.14067 | 0.12642 |
| 90 | 0.0211 | -0.17583 | 0.04741 |
| 100 | 0.01055 | -0.07033 | 0.03687 |
| 110 | 0.00352 | -0.07033 | 0.02634 |
| 120 | 0.58735 | 5.486 | 0.33881 |
| 130 | 0.98477 | 9.84667 | 4.21934 |
| 140 | 1.10083 | 10.83134 | 10.59313 |
| 150 | 1.11138 | 11.14784 | 12.81079 |
| 160 | 1.19228 | 11.64017 | 14.17509 |
| 170 | 1.2169 | 12.09734 | 14.31732 |
| 180 | 1.25558 | 12.30834 | 14.49115 |
| 190 | 1.27669 | 12.73034 | 14.85988 |
| 200 | 1.31889 | 13.04684 | 15.27075 |
| 210 | 1.34703 | 13.39851 | 16.17151 |
| 220 | 1.45254 | 14.34801 | 16.0767 |
| 230 | 1.45605 | 14.69968 | 16.94058 |
| 240 | 0.9285 | 9.28401 | 16.48757 |
| 250 | 0.67879 | 6.752 | 9.22882 |
| 260 | 0.60141 | 5.908 | 6.32111 |
| 270 | 0.54162 | 5.41567 | 5.06216 |
| 280 | 0.49239 | 4.88817 | 4.06658 |
| 290 | 0.4537 | 4.5365 | 3.56089 |
| 300 | 0.39743 | 3.93867 | 3.03413 |
| 310 | 0.37632 | 3.72767 | 2.53371 |
| 320 | 0.33412 | 3.23534 | 2.20185 |
| 330 | 0.29895 | 2.88367 | 1.70143 |
| 340 | 0.28488 | 2.81334 | 1.64876 |
| 350 | 0.29191 | 2.60234 | 1.3327 |
| 360 | 0.83354 | 6.57617 | 1.10619 |
| 370 | 1.3013 | 12.51934 | 3.9981 |
| 380 | 1.41033 | 13.96118 | 10.09798 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 390 | 1.48419 | 14.73484 | 14.85461 |
| 400 | 1.51584 | 15.19201 | 17.04067 |
| 410 | 1.60377 | 15.82501 | 22.26085 |
| 420 | 1.64949 | 16.24701 | 23.12474 |
| 430 | 1.74797 | 16.70418 | 23.19848 |
| 440 | 1.81128 | 17.86468 | 24.26254 |
| 450 | 1.80424 | 17.97018 | 24.12558 |
| 460 | 1.88513 | 18.70868 | 23.32491 |
| 470 | 1.90272 | 18.84935 | 22.50316 |
| 480 | 1.30482 | 13.22268 | 23.43552 |
| 490 | 1.15359 | 11.53467 | 19.17931 |
| 500 | 1.03049 | 10.19834 | 15.64475 |
| 510 | 0.92146 | 9.00267 | 14.63864 |
| 520 | 0.88981 | 8.82684 | 14.09081 |
| 530 | 0.83354 | 8.44001 | 13.74842 |
| 540 | 0.84057 | 8.36967 | 12.92141 |
| 550 | 0.84057 | 8.26417 | 12.37885 |
| 560 | 0.79133 | 7.73667 | 12.05752 |
| 570 | 0.8265 | 8.15867 | 12.00485 |
| 580 | 0.84761 | 8.51034 | 11.80468 |
| 590 | 0.81947 | 8.08834 | 11.32533 |
| 600 | 1.39978 | 13.43368 | 11.24631 |
| 610 | 1.64597 | 16.14151 | 14.7914 |
| 620 | 1.74093 | 17.05584 | 17.10914 |
| 630 | 1.84293 | 18.21635 | 16.91424 |
| 640 | 1.88513 | 18.70868 | 17.67278 |
| 650 | 1.91679 | 19.09551 | 17.80973 |
| 660 | 1.99768 | 19.69335 | 17.94142 |
| 670 | 2.15595 | 21.45168 | 16.66667 |
| 680 | 2.21222 | 21.90885 | 16.11884 |
| 690 | 2.19815 | 21.94401 | 17.64117 |
| 700 | 2.25794 | 22.47151 | 18.63148 |
| 710 | 2.3318 | 23.13968 | 18.90013 |
| 720 | 1.66708 | 16.73934 | 18.85272 |
| 730 | 1.38571 | 13.89084 | 18.58407 |
| 740 | 1.31186 | 13.04684 | 15.13906 |
| 750 | 1.21338 | 12.09734 | 13.07944 |
| 760 | 1.17469 | 11.71051 | 12.61589 |
| 770 | 1.15711 | 11.42917 | 12.09966 |
| 780 | 1.07621 | 10.69067 | 11.29899 |
| 790 | 1.00236 | 10.05767 | 11.43595 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 800 | 1.00236 | 9.81151 | 11.04088 |
| 810 | 1.02346 | 10.19834 | 10.54572 |
| 820 | 1.01642 | 10.05767 | 10.32975 |
| 830 | 1.00939 | 9.88184 | 10.06637 |
| 840 | 1.27317 | 11.11267 | 9.20775 |
| 850 | 1.93437 | 18.99001 | 9.41846 |
| 860 | 1.97306 | 19.41201 | 14.9863 |
| 870 | 2.03637 | 20.25601 | 15.57627 |
| 880 | 2.19815 | 21.31101 | 16.57712 |
| 890 | 2.24035 | 22.15501 | 17.88348 |
| 900 | 2.25794 | 22.43635 | 16.12937 |
| 910 | 2.38104 | 23.28035 | 16.18732 |
| 920 | 2.32828 | 23.21002 | 15.75011 |
| 930 | 2.41269 | 23.91335 | 17.27771 |
| 940 | 2.45841 | 24.37052 | 17.78866 |
| 950 | 2.45138 | 24.30018 | 19.60598 |
| 960 | 1.89217 | 19.06035 | 20.15908 |
| 970 | 1.7339 | 17.30201 | 19.83776 |
| 980 | 1.55101 | 15.54368 | 16.1083 |
| 990 | 1.50881 | 14.98101 | 14.09608 |
| 1000 | 1.4455 | 14.38318 | 13.26907 |
| 1010 | 1.4033 | 13.99634 | 11.9469 |
| 1020 | 1.38923 | 13.75018 | 11.03561 |
| 1030 | 1.37516 | 13.75018 | 10.51938 |
| 1040 | 1.26965 | 12.51934 | 9.84513 |
| 1050 | 1.29075 | 12.73034 | 9.77665 |
| 1060 | 1.26965 | 12.66001 | 9.48694 |
| 1070 | 1.28372 | 12.83584 | 9.02339 |
| 1080 | 1.97306 | 18.91968 | 8.51243 |
| 1090 | 2.36697 | 23.52652 | 8.67046 |
| 1100 | 2.49358 | 24.68702 | 9.92941 |
| 1110 | 2.55689 | 25.32002 | 17.23557 |
| 1120 | 2.59206 | 25.81235 | 19.86936 |
| 1130 | 2.62723 | 26.09368 | 19.50063 |
| 1140 | 2.6835 | 26.65635 | 18.63148 |
| 1150 | 2.73977 | 27.21902 | 21.97113 |
| 1160 | 2.78198 | 27.85202 | 20.52255 |
| 1170 | 2.81012 | 28.02785 | 24.20459 |
| 1180 | 2.83825 | 28.16852 | 24.81563 |
| 1190 | 2.82418 | 28.13335 | 24.4469 |
| 1200 | 2.24035 | 22.57702 | 22.77708 |

| | Ethanol-Pl | Ethanol-PVAc | Ethanol-PI/PVAc |
|----------|--------------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1210 | 2.07154 | 20.67801 | 22.10282 |
| 1220 | 2.0012 | 20.00985 | 22.70333 |
| 1230 | 1.93085 | 19.30651 | 17.9941 |
| 1240 | 1.87458 | 18.53285 | 17.15655 |
| 1250 | 1.80424 | 17.97018 | 16.22419 |
| 1260 | 1.79017 | 17.79435 | 15.26022 |
| 1270 | 1.74797 | 17.58335 | 15.07585 |
| 1280 | 1.76204 | 17.54818 | 14.99157 |
| 1290 | 1.7339 | 17.19651 | 14.94943 |
| 1300 | 1.72687 | 17.02068 | 14.87042 |
| 1310 | 1.74797 | 17.16134 | 14.34893 |

| | THF-PI THF-PVAc T | | THF-PI/PVAc |
|----------|--------------------------------------|---|-------------|
| time (s) | Change of Relative Resistance (%) | Change of Change of Relative Resistance (%) | |
| 0 | 0 | 0 | 0 |
| 10 | -0.72324 | 0.046 | 0.04223 |
| 20 | -0.76143 | 0.092 | 0.03871 |
| 30 | -0.89895 | 0.393 | 0.02815 |
| 40 | -0.86839 | 0.532 | 0.02463 |
| 50 | -1.03392 | 0.601 | 0.02111 |
| 60 | -0.93206 | 0.671 | 0.02815 |
| 70 | -0.91678 | 0.74 | 0.02815 |
| 80 | -0.82765 | 0.532 | 0.0563 |
| 90 | -1.21982 | 0.671 | 0.00704 |
| 100 | -0.79963 | 0.763 | -0.02463 |
| 110 | -0.96007 | 0.555 | -0.0563 |
| 120 | -0.89131 | 1.619 | 24.7308 |
| 130 | 12.3663 | 1.318 | 30.6707 |
| 140 | 16.19894 | 1.504 | 33.46471 |
| 150 | 15.56229 | 3.54 | 34.66817 |
| 160 | 16.12509 | 13.999 | 35.51974 |
| 170 | 15.519 | 17.817 | 36.34316 |
| 180 | 15.64123 | 18.372 | 38.9014 |
| 190 | 15.67689 | 21.543 | 39.65093 |
| 200 | 16.1531 | 21.936 | 43.26131 |
| 210 | 15.91881 | 23.185 | 44.25012 |
| 220 | 16.06906 | 26.564 | 47.2623 |
| 230 | 15.56738 | 27.489 | 47.50158 |
| 240 | 16.03086 | 25.916 | 40.25969 |
| 250 | 12.35357 | 24.828 | 37.73665 |
| 260 | 11.02934 | 23.023 | 37.27919 |
| 270 | 10.04125 | 23.232 | 35.13266 |
| 280 | 9.68473 | 23.324 | 36.33261 |
| 290 | 9.55485 | 23.255 | 37.53607 |
| 300 | 9.00733 | 23.232 | 37.34253 |
| 310 | 7.89192 | 23.162 | 35.59012 |
| 320 | 7.93012 | 23.07 | 34.93209 |
| 330 | 8.06764 | 23 | 35.56197 |
| 340 | 7.49211 | 23.023 | 34.51334 |
| 350 | 7.72639 | 23.023 | 35.19248 |
| 360 | 7.40552 | 26.726 | 45.50285 |
| 370 | 14.66843 | 32.164 | 48.6593 |
| 380 | 20.57655 | 32.441 | 48.70153 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|--------------------------------------|---|-------------|
| time (s) | Change of Relative Resistance (%) | Change of Change of Relative Resistance (%) | |
| 390 | 21.75817 | 32.696 | 47.7831 |
| 400 | 22.16563 | 32.997 | 50.04223 |
| 410 | 22.77172 | 33.112 | 50.71082 |
| 420 | 23.25558 | 33.228 | 51.70315 |
| 430 | 23.41347 | 33.298 | 52.34007 |
| 440 | 24.19273 | 33.459 | 54.08896 |
| 450 | 23.48222 | 33.436 | 54.96164 |
| 460 | 24.34298 | 33.436 | 56.01379 |
| 470 | 25.61373 | 33.598 | 58.05475 |
| 480 | 26.2351 | 31.469 | 49.8135 |
| 490 | 20.75227 | 31.493 | 47.31508 |
| 500 | 17.75491 | 31.03 | 44.95038 |
| 510 | 16.60385 | 30.636 | 44.40847 |
| 520 | 15.2949 | 30.336 | 41.77986 |
| 530 | 15.08353 | 29.156 | 41.82208 |
| 540 | 14.08017 | 29.109 | 42.11767 |
| 550 | 13.58613 | 29.248 | 42.44845 |
| 560 | 13.43333 | 28.97 | 41.26258 |
| 570 | 13.6065 | 28.762 | 39.66148 |
| 580 | 13.29072 | 28.6 | 40.57288 |
| 590 | 12.75848 | 28.67 | 37.85981 |
| 600 | 11.85189 | 33.344 | 49.08861 |
| 610 | 19.62412 | 36.653 | 49.98241 |
| 620 | 26.57635 | 37.069 | 51.16124 |
| 630 | 31.27228 | 37.833 | 50.53135 |
| 640 | 30.51085 | 38.92 | 51.24569 |
| 650 | 30.65855 | 39.268 | 50.49265 |
| 660 | 30.61781 | 39.707 | 51.62221 |
| 670 | 31.22135 | 39.962 | 51.97762 |
| 680 | 31.97005 | 39.985 | 52.71659 |
| 690 | 32.68819 | 40.101 | 52.85734 |
| 700 | 32.3826 | 40.147 | 52.62862 |
| 710 | 33.15677 | 40.494 | 52.92068 |
| 720 | 33.2841 | 36.63 | 44.98557 |
| 730 | 28.04319 | 35.704 | 43.71173 |
| 740 | 24.09086 | 35.82 | 42.38863 |
| 750 | 22.42284 | 35.403 | 42.11063 |
| 760 | 22.4483 | 35.426 | 41.29073 |
| 770 | 22.18855 | 35.079 | 40.38989 |
| 780 | 21.6232 | 34.755 | 39.71075 |
| 790 | 21.10624 | 34.732 | 39.61222 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|--------------------------------------|---|-------------|
| time (s) | Change of Relative Resistance (%) | Change of Change of Relative Resistance (%) | |
| 800 | 19.23958 | 34.131 | 39.12661 |
| 810 | 19.13263 | 34.038 | 38.99993 |
| 820 | 19.33636 | 33.205 | 38.73601 |
| 830 | 19.02312 | 33.274 | 38.04631 |
| 840 | 17.98666 | 36.583 | 45.904 |
| 850 | 19.99847 | 39.43 | 45.8653 |
| 860 | 32.51502 | 39.615 | 45.93567 |
| 870 | 37.64388 | 39.661 | 46.85763 |
| 880 | 39.10818 | 40.077 | 47.05468 |
| 890 | 39.2839 | 40.887 | 47.48399 |
| 900 | 39.83396 | 41.049 | 47.21655 |
| 910 | 40.07334 | 41.327 | 47.52622 |
| 920 | 40.50117 | 41.466 | 48.0083 |
| 930 | 42.15392 | 41.258 | 48.37427 |
| 940 | 42.53336 | 41.35 | 48.25815 |
| 950 | 42.91535 | 41.466 | 49.07101 |
| 960 | 43.90853 | 40.934 | 40.94236 |
| 970 | 42.55883 | 41.096 | 39.1055 |
| 980 | 33.2077 | 42.114 | 38.30671 |
| 990 | 32.32148 | 38.897 | 36.50503 |
| 1000 | 31.36905 | 38.018 | 36.58245 |
| 1010 | 29.40308 | 37.671 | 36.12147 |
| 1020 | 28.5958 | 37.37 | 35.23119 |
| 1030 | 28.10686 | 36.722 | 34.93209 |
| 1040 | 27.12896 | 36.722 | 34.97783 |
| 1050 | 26.35989 | 36.56 | 34.75966 |
| 1060 | 26.41591 | 36.445 | 34.5802 |
| 1070 | 25.80218 | 36.329 | 33.9292 |
| 1080 | 25.7487 | 36.676 | 42.95869 |
| 1090 | 25.76398 | 38.388 | 44.64424 |
| 1100 | 42.44678 | 40.563 | 47.85347 |
| 1110 | 44.71071 | 40.864 | 49.06045 |
| 1120 | 45.24549 | 40.91 | 50.2041 |
| 1130 | 45.04176 | 41.049 | 50.61933 |
| 1140 | 44.94499 | 41.211 | 51.1542 |
| 1150 | 44.73108 | 41.327 | 52.2908 |
| 1160 | 45.14108 | 41.674 | 52.19931 |
| 1170 | 44.84568 | 41.744 | 52.72714 |
| 1180 | 45.06723 | 42.044 | 53.91653 |
| 1190 | 45.33462 | 42.715 | 54.27898 |
| 1200 | 45.76755 | 42.438 | 45.02076 |

| | THF-PI | THF-PVAc | THF-PI/PVAc |
|----------|-----------------------------------|--------------------------------------|--------------------------------------|
| time (s) | Change of Relative Resistance (%) | Change of Relative Resistance (%) | Change of Relative Resistance (%) |
| 1210 | 40.47061 | 38.851 | 43.13463 |
| 1220 | 36.19232 | 38.111 | 42.1036 |
| 1230 | 33.06764 | 37.763 | 41.28017 |
| 1240 | 31.36905 | 37.208 | 40.43212 |
| 1250 | 30.60507 | 37.278 | 40.10486 |
| 1260 | 29.82836 | 37.162 | 40.04152 |
| 1270 | 29.01599 | 37.162 | 39.77761 |
| 1280 | 28.75115 | 37.116 | 39.68611 |
| 1290 | 28.33096 | 37.023 | 38.88732 |
| 1300 | 28.04319 | 37.023 | 38.37005 |
| 1310 | 27.38617 | 36.954 | 38.07094 |

Appendix D. Lachenbruch's Holdout Confusion Matrices

One Feature:

Training:

| Actual Group | # of Cases | Predicted | | | |
|--------------|------------|-----------|----|------------|--|
| _ | | V1 | V2 | V 3 | |
| V1 | 6 | 5 | 0 | 1 | |
| V2 | 6 | 1 | 5 | 0 | |
| V3 | 6 | 0 | 0 | 6 | |

Test (Exposure 1):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 0 | 1 | 0 |
| V2 | 1 | 1 | 0 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 6 | 5 | 0 | 1 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 2):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 1 | 0 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 4 | 1 | 1 |
| V2 | 6 | 1 | 5 | 0 |
| V3 | 6 | 0 | 1 | 5 |

Test (Exposure 3):

| Actual | | | Duodiatad | |
|------------|------------|----|--------------|----|
| Group | # of Cases | V1 | Predicted V2 | V3 |
| V1 | 1 | 0 | 1 | 0 |
| V2 | 1 | 1 | 0 | 0 |
| V 3 | 1 | 1 | 0 | 0 |

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 5 | 0 | 1 |
| V2 | 6 | 1 | 5 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 4):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 0 | 1 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 1 | 5 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 5):

| Test (Exposure 5): | | | | |
|--------------------|------------|----|--------------|----|
| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
| V1 | 1 | 0 | 0 | 1 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 1 | 0 | 0 |

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 5 | 0 | 1 |
| V2 | 6 | 1 | 5 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 6):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V 3 | 1 | 0 | 0 | 1 |

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 4 | 1 | 1 |
| V2 | 6 | 1 | 5 | 0 |
| V3 | 6 | 1 | 0 | 5 |

Test (Exposure 7):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 1 | 0 | 1 | 0 |
| V2 | 1 | 1 | 0 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Two Features:

Training:

| Training. | | | | |
|-----------------|------------|----|--------------|----|
| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 1):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V 3 | 1 | 0 | 0 | 1 |

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 2):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 0 | 1 |
| V3 | 1 | 0 | 0 | 1 |

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|-----------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 3):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 0 | 0 | 1 |

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 4):

| Test (Exposure 1). | | | | |
|--------------------|------------|----|--------------|----|
| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
| V1 | 1 | 0 | 1 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Training:

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 6 | 6 | 0 | 0 |
| V2 | 6 | 0 | 6 | 0 |
| V3 | 6 | 0 | 0 | 6 |

Test (Exposure 5):

| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
|-----------------|------------|----|--------------|----|
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V 3 | 1 | 0 | 0 | 1 |

| Actual Group | # of Cases | Predicted V1 V2 V3 | | | |
|-----------------|------------|-----------------------|---|---|--|
| V1 | 6 | 6 | 0 | 0 | |
| V2 | 6 | 0 | 6 | 0 | |
| V3 | 6 | 0 | 0 | 6 | |

Test (Exposure 6):

| Test (Exposure o): | | | | |
|--------------------|------------|----|--------------|----|
| Actual Group | # of Cases | V1 | Predicted V2 | V3 |
| V1 | 1 | 1 | 0 | 0 |
| V2 | 1 | 0 | 1 | 0 |
| V3 | 1 | 0 | 0 | 1 |

Training:

| Actual Group | # of Cases | Predicted V1 V2 V3 | | | |
|-----------------|------------|-----------------------|---|---|--|
| V1 | 6 | 6 | 0 | 0 | |
| V2 | 6 | 0 | 6 | 0 | |
| V3 | 6 | 0 | 0 | 6 | |

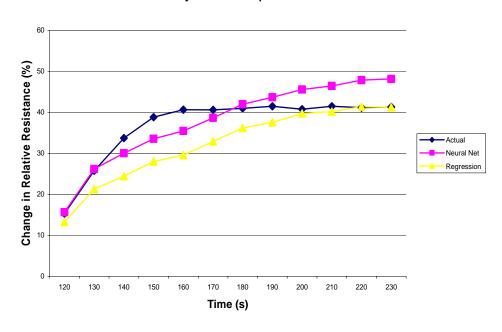
Test (Exposure 7):

| Actual Group | # of Cases | Predicted V1 V2 V3 | | | |
|-----------------|------------|-----------------------|---|---|--|
| V1 | 1 | 1 | 0 | 0 | |
| V2 | 1 | 0 | 1 | 0 | |
| V3 | 1 | 0 | 0 | 1 | |

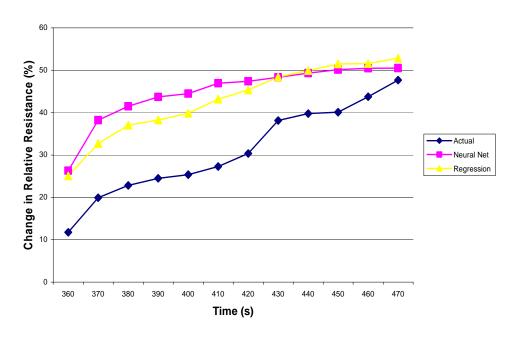
Appendix E. Predicted vs. Actual Sensor Three Values

Phase Three:

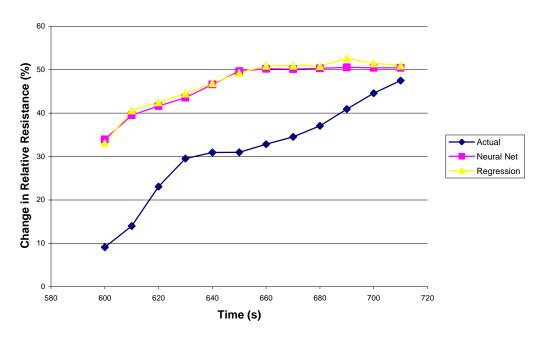
Cyclohexane Exposure One



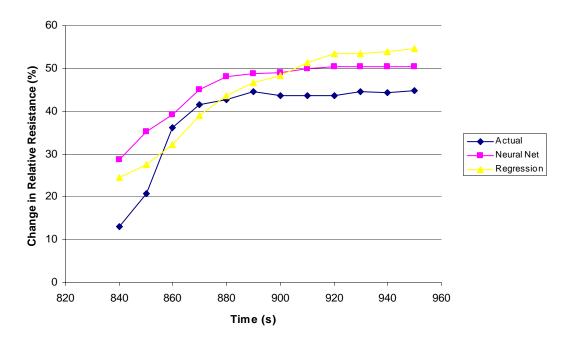
Cyclohexane Exposure Two



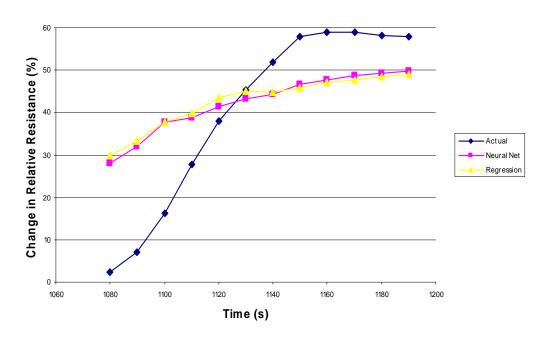
Cyclohexane Exposure Three



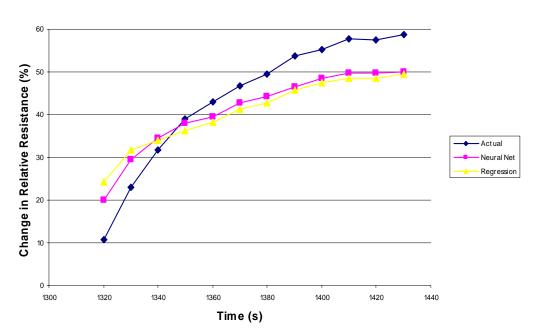
Cyclohexane Exposure Four



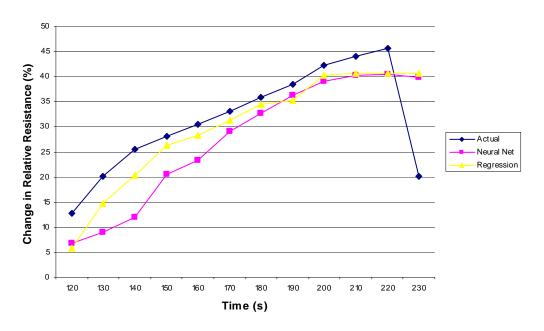
Cyclohexane Exposure Five



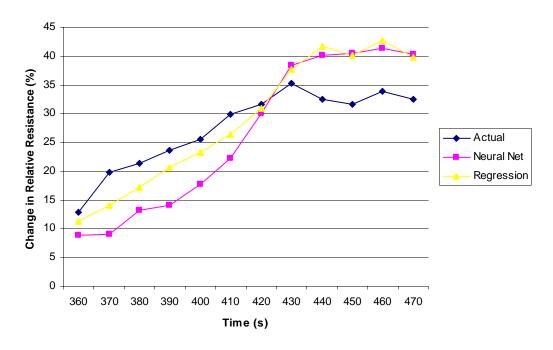
Cyclohexane Exposure Six



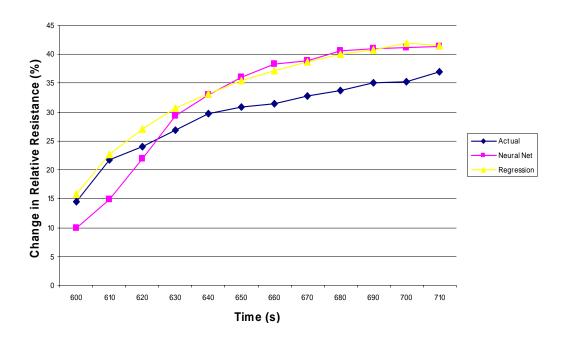
Ethanol Exposure One



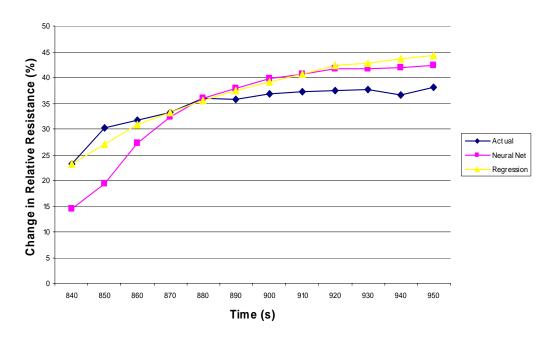
Ethanol Exposure Two



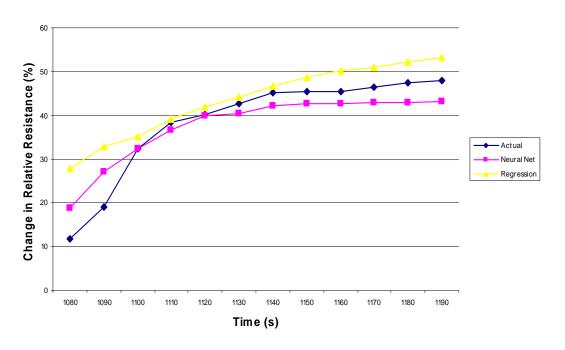
Ethanol Exposure Three



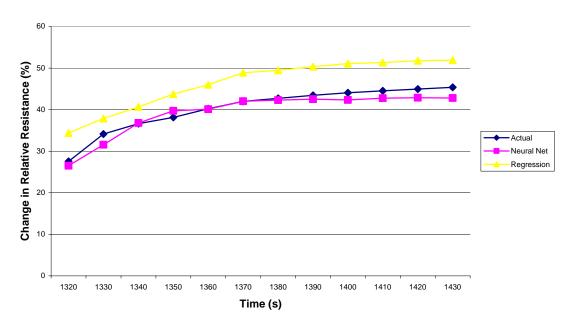
Ethanol Exposure Four



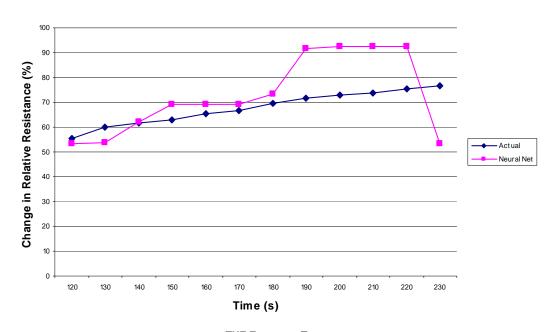
Ethanol Exposure Five



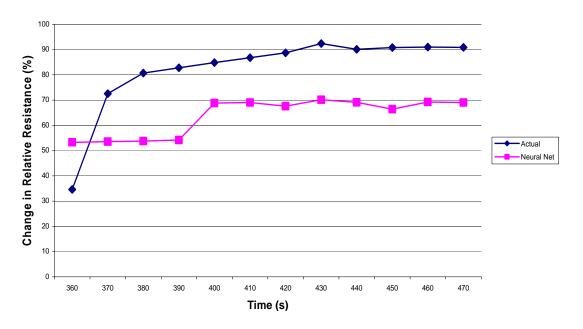
Ethanol Exposure Six



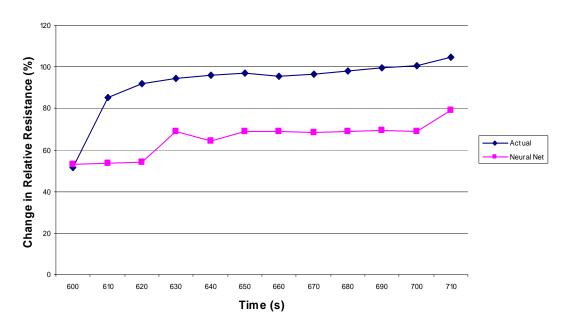
THF Exposure One



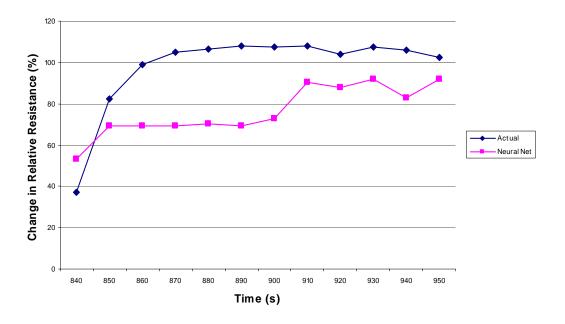
THF Exposure Two



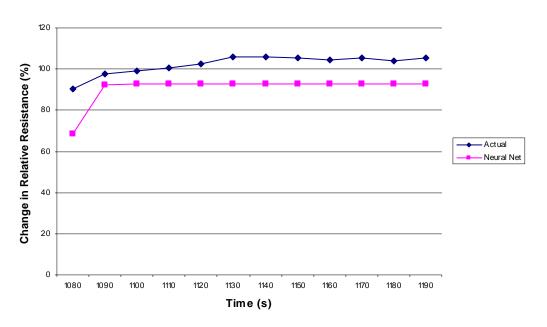
THF Exposure Three



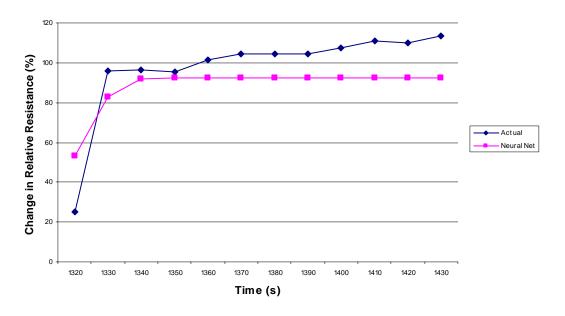
THF Exposure Four



THF Exposure Five

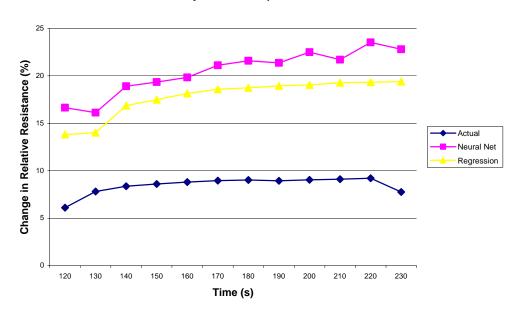


THF Exposure Six

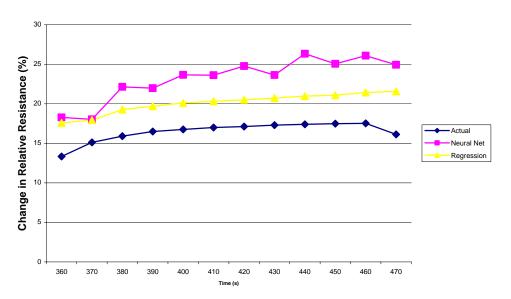


Phase Four:

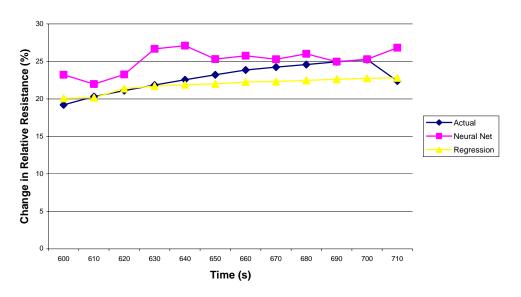
Cyclohexane Exposure One



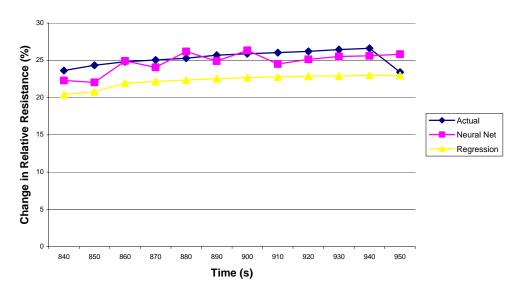
Cyclohexane Exposure Two



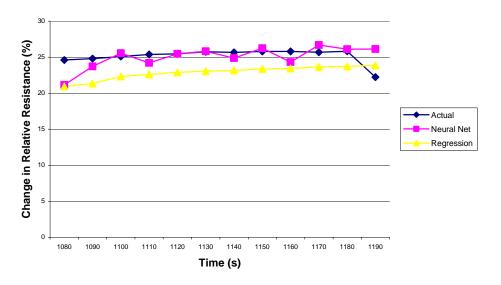
Cyclohexane Exposure Three



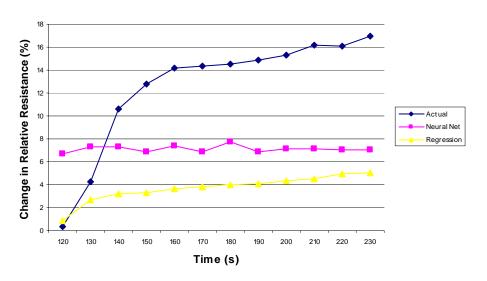
Cyclohexane Exposure Four



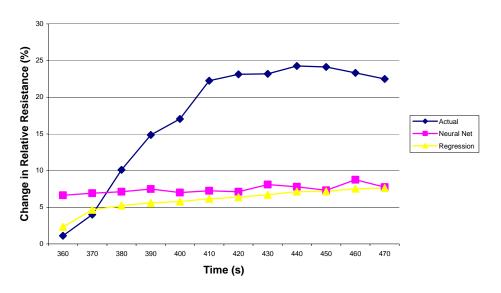
Cyclohexane Exposure Five



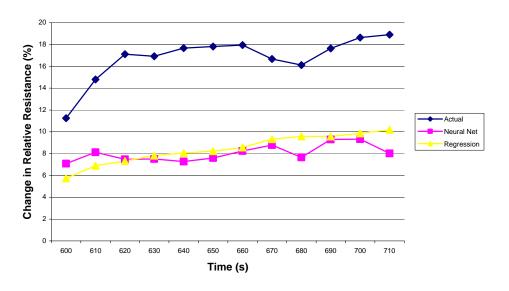
Ethanol Exposure One



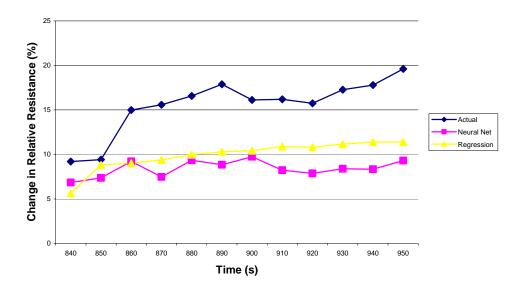
Ethanol Exposure Two



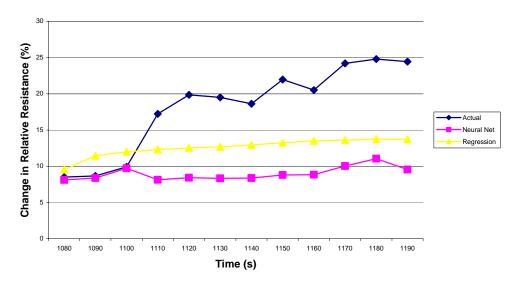
Ethanol Exposure Three



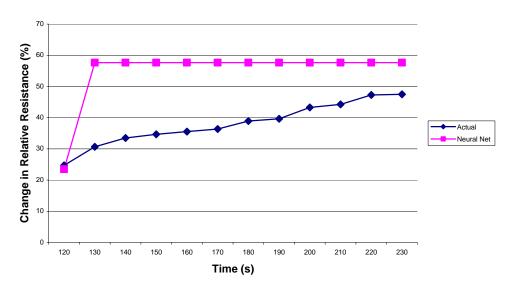
Ethanol Exposure Four



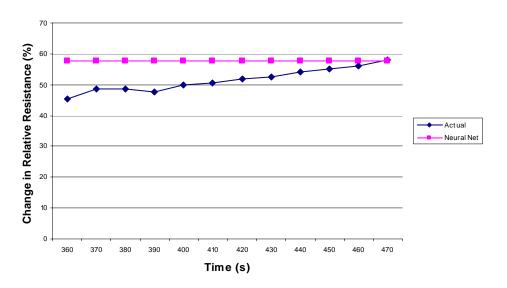
Ethanol Exposure Five



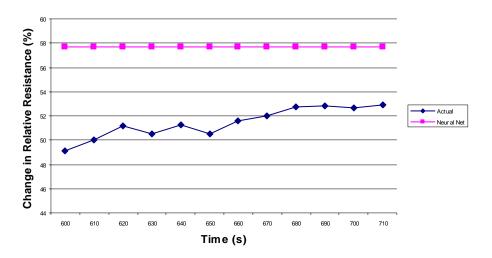
THF Exposure One



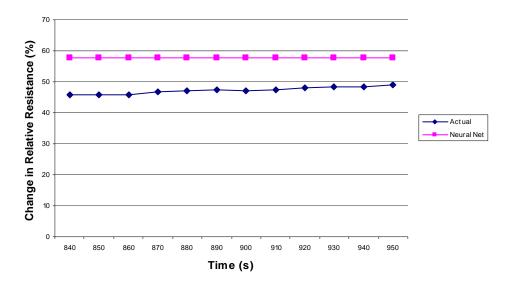
THF Exposure Two



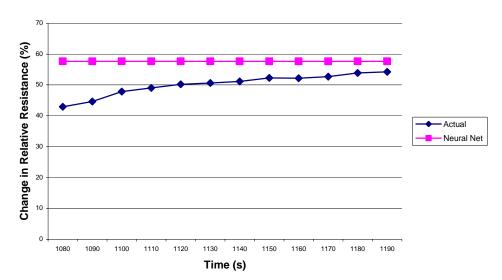
THF Exposure Three



THF Exposure Four







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