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**EFFECT OF EXPANDED POLYSTYRENE CONTENT AND PRESS  
TEMPERATURE ON THE PROPERTIES OF LOW-DENSITY WOOD  
PARTICLEBOARD**

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**ABSTRACT**

In this study, three-layer low-density (about 400 kg/m<sup>3</sup>) particleboards consisting of a mixture of wood particles and expanded polystyrene (EPS) were manufactured. EPS bead was incorporated in the core layer as a light filler. The influence of EPS content (0 %, 2,5 %, 5 %, 7,5 %, 10 % and 12,5 %) and press temperature (110 °C and 140 °C) on the microstructure, density profile, bending properties, internal bond and thickness swelling of the panels was investigated. Results showed that incorporation of EPS beads filled in the voids between wood particles, improved the core layer integrity, and generated a more pronounced density profile. Consequently, the bending properties and internal bond of panels adding EPS were remarkably improved, and the thickness swelling was decreased. However, the variation of the amount of EPS from 2,5 % to 12,5 % had no significant effect on the bending properties and thickness swelling. Comparing the two press temperatures, although higher temperature (140 °C) was more favourable in control panels without EPS as filler, it had a negative effect on the properties of panels with addition of EPS filler, especially for high EPS contents (10 % and 12,5 %), attributing to the shrinkage of EPS bead under press temperature that is much higher than its glass transition temperature (104 °C).

**Keywords:** Density profile, expanded polystyrene (EPS), low-density particleboard, mechanical properties, microstructure, press temperature,

### 33 INTRODUCTION

34 Global wood-based panel industries have undergone a rapid growth in recent years.  
35 Inevitably, such increasing demand put strain on the wood supply. Nowadays, density  
36 reduction becomes a topical issue in wood-based panels industry due to limited supply  
37 and increased price of wood material (Benthien and Ohlmeyer 2016). As one of the most  
38 important types of wood-based panel, particleboard is increasingly used in furniture and  
39 interior decoration, especially in custom furniture sector in China. The mean density of  
40 conventional particleboards usually ranges between  $600 \text{ kg/m}^3$  and  $750 \text{ kg/m}^3$  (Thoemen  
41 *et al.* 2010). Development of lightweight particleboards (density below  $600 \text{ kg/m}^3$ ) bring  
42 many advantages such as more efficient utilization of wood, easier transportation and  
43 handling, lower transportation cost due to mass reduction (Barbu 2016; Monteiro *et al.*  
44 2018).

45 Simply using less amount of wood for panel manufacture leads to less compacted  
46 and density-reduced particleboard accompanied by deterioration of properties.  
47 Meanwhile, there will be a significant increase in the proportion of voids and empty  
48 spaces between wood particles (Bajzová *et al.* 2018). Incorporation of non-wood light  
49 filling materials (e.g. expanded polystyrene, foamed starch or even popcorn) in the core  
50 layer of particleboard is one strategy to achieve the light construction of panels (Monteiro  
51 *et al.* 2016; Monteiro *et al.* 2019). It is expected that the light fillers can fill up the voids  
52 and pores, making the structure of the panel more uniform and therefore counteracting

53 the decreased properties (Dziurka *et al.* 2015). Sundquist and Bajwa (2016) investigated  
54 the use of dried distillers grains with solubles (DDGS) as a functional filler in  
55 particleboards and manufactured the products with an average density of 580 kg/m<sup>3</sup> to  
56 640 kg/m<sup>3</sup>. The results show that concentration of 5 weight percent (wt%) DDGS  
57 produced superior properties compared to the control panel concerning water absorption  
58 and mechanical tests. Thus, light fillers play an important role in improving the  
59 performance of the low-density panels.

60 EPS bead is a very low-density material that contains 98 % air and only the rest is  
61 polystyrene (Fernando *et al.* 2017). EPS (including expandable and pre-expanded) has  
62 been investigated to use as foam core material in the sandwich panels (Shalbfafan *et al.*  
63 2015), mix with wood in the core layer of low-density panels (Jafarnezhad *et al.* 2018),  
64 and make lightweight wood plastic composites (Lyutyy *et al.* 2018). Dziurka *et al.* (2015)  
65 produced density-reduced particleboards (500 kg/m<sup>3</sup> to 650 kg/m<sup>3</sup>) with 7 % wood chips  
66 substituted with EPS beads in the core layer. This study found that wood chip-EPS boards  
67 with density of 600 kg/m<sup>3</sup> met the bending properties requirement for boards intended for  
68 interior fitments (including furniture) for use in dry conditions (P2 boards) according to  
69 EN 312: 2010. However, there are few studies about the influence of the EPS content on  
70 the properties of panel and the optimal content to be used.

71 Additionally, the glass transition temperature ( $T_g$ ) of EPS affects the processing  
72 conditions of the panel manufacture, such as press temperature. On the other hand, the

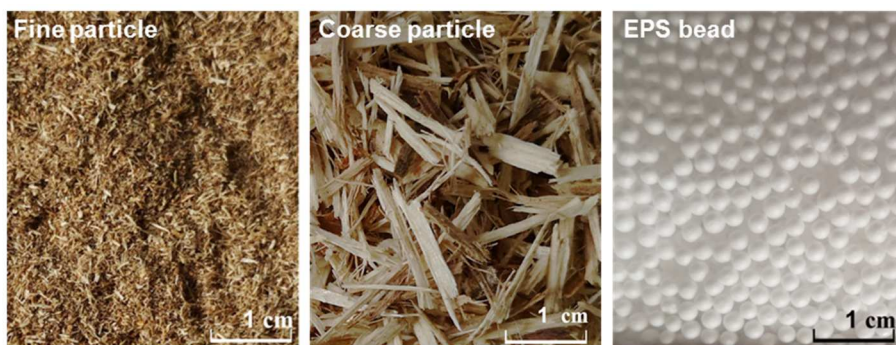
73 press temperature during hot press process is a key parameter because it is crucial to  
74 obtain a high enough temperature in the core to get the adhesive fully cured, and at the  
75 same time the temperature should not be too high to avoid thermal degradation (Monteiro  
76 *et al.* 2018) or severe EPS softening. Therefore, the selection of press temperature  
77 requires additional research.

78 In this study, three-layer low-density particleboards with a target density of 400  
79 kg/m<sup>3</sup> were manufactured. The panels consisted of a mixture of EPS beads with wood  
80 particle as the core layer. The aim of this study was to investigate how the amount of EPS  
81 and press temperature affected the properties of the studied panels.

## 82 **MATERIALS AND METHODS**

### 83 **Raw materials**

84 Poplar (*Populus* spp.) particles (air-dried moisture content of about 8 %) were  
85 provided by Ningfeng Wood-based Panels Corporation, China. The particles were sieved  
86 to obtain fine (< 1 mm) and coarse (1 mm to 4 mm) fractions for use, as shown in Figure  
87 1. EPS beads with a spherical shape (average diameter of 2,2 mm, density of 50 kg/m<sup>3</sup> to  
88 60 kg/m<sup>3</sup>) were used as light fillers. A polymethylene isocyanate (pMDI) resin  
89 (WANNATE<sup>®</sup> PM-200, viscosity of 150 ~ 200 mPa·s at 25 °C, NCO content of 30 ~ 32  
90 wt%), was obtained from the Wanhua Chemical Corporation, Beijing, China. Acetone  
91 was used as resin diluent for better adhesive distribution.



92

93 **Figure 1:** Fine and coarse wood particles and expanded polystyrene beads used for  
94 manufacture of low-density particleboard.

### 95 **Particle size analysis**

96 Particle size distribution of the fine and coarse particle samples was measured using  
97 the image analysis-based particle size measurement equipment (SCREENCAM 100  
98 Optical Lab Screen for Wood Chips, IMAL-PAL GROUP, Italy). The wood particles were  
99 separated by the system without altering their dimensional characteristics, imaged by a  
100 digital camera, and analysed by the software. The distribution of wood particles was given  
101 as a percentage over the total weight based on their dimensions. Approximately 100000  
102 particles were evaluated for each sample.

### 103 **Differential scanning calorimetry (DSC) analysis of EPS**

104 Glass transition temperature ( $T_g$ ) of the EPS bead was determined using a Q100 DSC  
105 (TA instruments) in flowing nitrogen (50 mL/min). An initial thermal program was  
106 performed using a heating rate of 10 °C/min to 140 °C and held isothermally for 3 min to  
107 erase any previous thermal history. Then the sample (about 5 mg) was cooled at a rate of  
108 20 °C/min to 50 °C and held isothermally for 3 min. After that, the same heating program  
109 as the initial one was repeated.

110 **Particleboards manufacturing**

111 Three layered particleboards with a target density of 400 kg/m<sup>3</sup> and thickness of 15  
112 mm were manufactured. The face layer was made of fine wood particles (16 % moisture  
113 content), while the core layer contained a mixture of air-dried coarse wood particles (8 %  
114 moisture content) and different amounts of EPS. To obtain a more pronounced density  
115 profile, the fine wood particles used in the face layer were sprayed with required amount  
116 of deionized water and conditioned to reach 16 % moisture content. The pMDI and  
117 acetone were weighed out at a mass ratio of 4:1 into a beaker and then mechanically  
118 stirred for 10 s to obtain a homogeneous mixture. The adhesive content was 7 % for core  
119 layer and 10 % for face layer (based on the oven-dry mass). The code number and  
120 composition of the low-density particleboards and their mean density is shown in Table  
121 1. The three-layer mat was made manually using a 340 mm × 360 mm forming box, and  
122 then pressed at 110 °C for 15 min or 140 °C for 9 min at an initial pressure of 2 MPa.  
123 Then the press was set to distance mode, applying a variable pressure to maintain the  
124 desired panel thickness using thickness gauges. Panels without EPS beads were also  
125 manufactured at the two press temperatures as the controls. For each panel variable,  
126 according to Table 1, two replicates were manufactured.

127

128

129

130 **Table 1:** Composition of low-density particleboards and their actual mean density.

Code	EPS bead content (%) <sup>1</sup>	Press temperature (°C)	Mean Density (kg/m <sup>3</sup> )
1	0,0	110	364
2	0,0	140	372
3	2,5	110	391
4	2,5	140	375
5	5,0	110	371
6	5,0	140	364
7	7,5	110	384
8	7,5	140	369
9	10,0	110	389
10	10,0	140	371
11	12,5	110	377
12	12,5	140	375

131 <sup>1</sup>The EPS content was based on the oven-dry mass of wood particles in core layer.

### 132 **Evaluation of particleboards**

133 The internal region in core layer was sputtered with gold and characterized using a  
134 scanning electron microscope (Hitachi S-3400N) at an acceleration voltage of 5 kV.

135 Vertical density profile was measured on a DENSE-LAB X densitometry (EWS,  
136 Germany), using X ray transmitted across the thickness of sample at a scanning speed of  
137 0,5 mm/s.

138 Mechanical properties were evaluated by determining internal bond (IB), bending  
139 strength (MOR) and modulus of elasticity in bending (MOE) according to Chinese standard

140 GB/T 17657-2013, using an Instron 5582 universal testing machine. Physical properties  
141 were characterized by measuring thickness swelling (TS) after 2 h of water immersion at  
142 20 °C (GB/T 4897-2015). Twelve replicates were tested for MOR and MOE, and eight  
143 replicates were tested for IB and TS, respectively.

#### 144 **Statistical analysis**

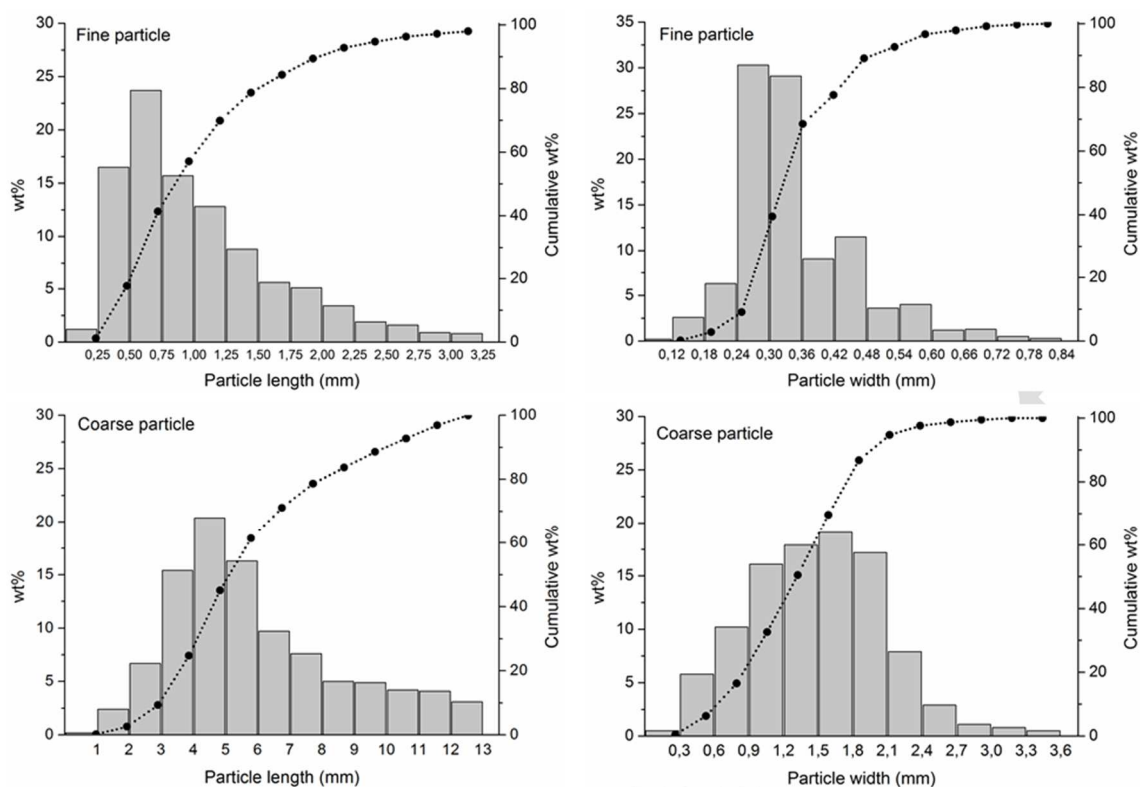
145 Data analysis was performed using the IBM® SPSS Statistics software (Version 19).  
146 The homogeneity of variances was checked using Leven test. Thereafter, comparison of  
147 mean values using one-way ANOVA test was conducted to determine whether the  
148 differences between the properties of the particleboards prepared at different conditions are  
149 statistically significant or not. Multiple comparisons using Scheffe test was performed to  
150 evaluate the statistical differences between variations, at a significance level of  $P < 0,05$ .

### 151 **RESULTS AND DISCUSSION**

#### 152 **Particle size characterization**

153 The particle size (length and width) distributions are displayed in Figure 2. Coarse  
154 particle sample had larger average length and width than fine particle. The length of  
155 coarse particle ranged from 1 mm to 13 mm and centered on 3 mm to 6 mm, while the  
156 width ranged from 0,3 mm to 3,6 mm and centered on 0,9 mm to 2,1 mm. In the case of  
157 fine particle, the length was less than 3,25 mm and centered on 0,25 mm to 1,25 mm,  
158 while the width was less than 0,84 mm and centered on 0,24 mm to 0,36 mm.





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**Figure 2:** Histogram of the distribution and cumulative distribution of the particle length and width.

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### 162 **T<sub>g</sub> of EPS bead**

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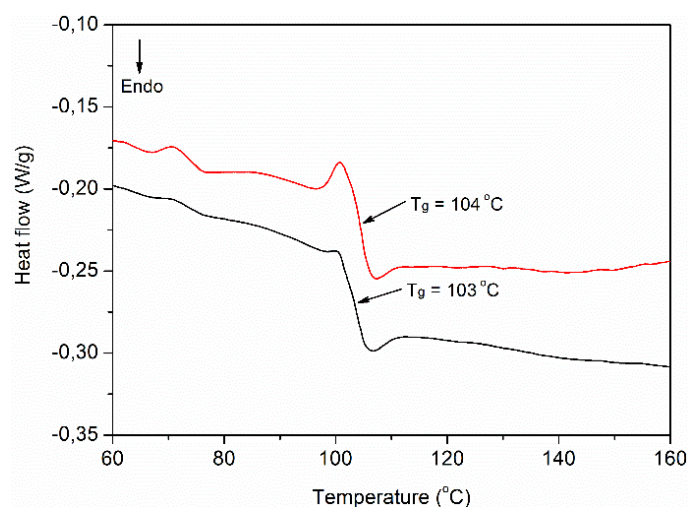
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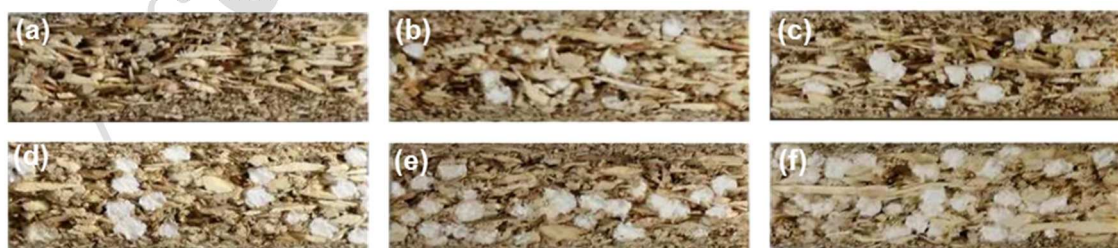
As the glass transition occurs over a temperature range, the midpoint temperature of the glass transition region (step change in specific heat capacity) in the second heating curve was selected to represent T<sub>g</sub>. DSC analysis of EPS bead revealed a T<sub>g</sub> of approximately 103 °C with a good reproducibility (Figure 3). This result was in agreement with previous research by Shalbafan *et al.* (2012) that reported T<sub>g</sub> of expandable polystyrene of 103 °C.



169 **Figure 3:** DSC second heating thermogram of EPS bead (two curves represent test on  
170 two duplicate samples)

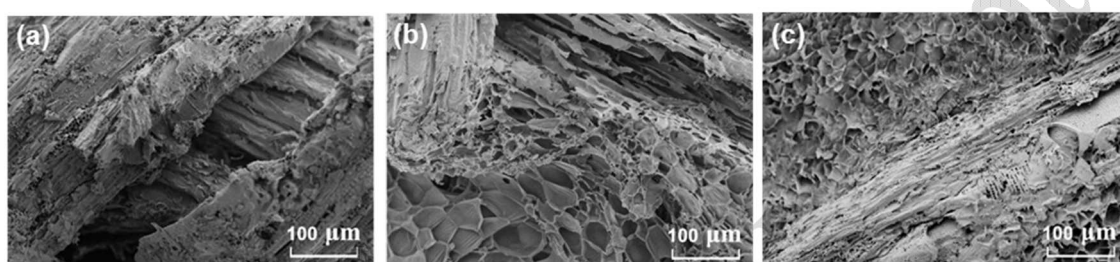
### 171 **Internal structure**

172 The internal section of the low-density particleboards is shown in Figure 4. In this  
173 study, the coarse particle was applied in the core layer, due to the large particles are  
174 expected to give better mechanical strength, while the fine particles were good for surface  
175 quality (Monteiro *et al.* 2018). It is clearly seen that with the increase of EPS bead content  
176 from 0 % to 12,5 % in the core layer, more and more wood particles were surrounded by  
177 EPS bead, and the empty spaces between particles were decreased.



178 **Figure 4:** Internal section of the 15 mm three-layer particleboards, containing fine  
179 particle in the face layers (3 mm) and a mixture of coarse particle with different contents  
180 of expanded EPS bead in the core layer (12 mm): (a) 0 % EPS; (b) 2,5 % EPS; (c) 5 %  
181 EPS; (d) 7,5 % EPS; (e) 10 % EPS; (f) 12,5 % EPS.

183 The microstructure of the panel core layer is shown in Figure 5. It can be clearly seen  
184 that in control panel there were empty spaces between wood particles in the core layer.  
185 EPS bead filled the voids between particles and improved the core layer integrity, making  
186 the core layer more uniform. The EPS bead consisted of numerous closed cells. With the  
187 increased press temperature from 110 °C to 140 °C, the size of foam cells became smaller.

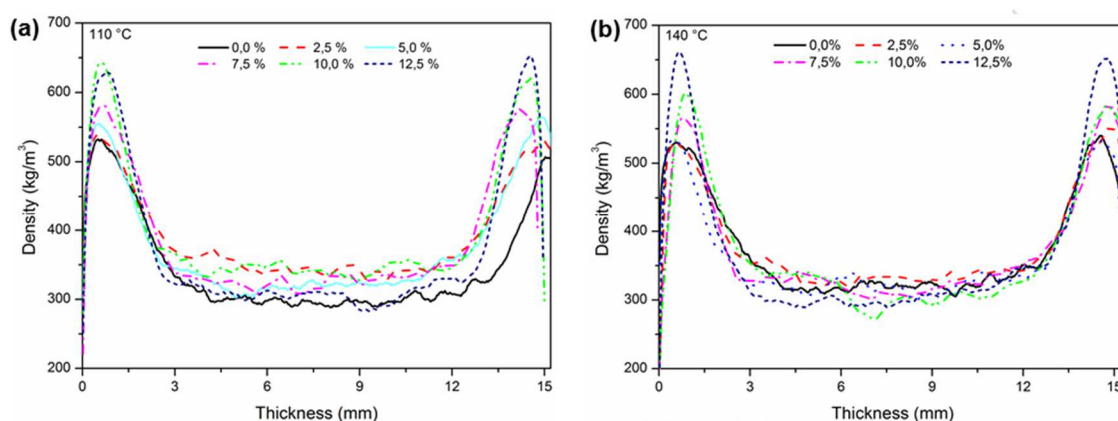


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189 **Figure 5:** Scanning electron micrographs of structure in the core layer of low-density  
190 particleboard: (a) control with 0,0% EPS; (b) addition of 12,5 % EPS and press  
191 temperature of 110 °C; (c) addition of 12,5 % EPS and press temperature of 140 °C.

### 192 **Density profile**

193 The mean density of all these particleboards is similar (Table 1). It is well-known  
194 that the density profile over the cross-section of the particleboard formed during hot  
195 pressing influences mechanical and physical properties of panels. Therefore, it is  
196 necessary to investigate the density gradient of the panels. The vertical density profile  
197 over the panel thickness generally resembles a U-shape, as shown in Figure 6. For both  
198 press temperature (110 °C and 140 °C), adding EPS bead to the core layer led to a more  
199 pronounced density gradient of the panel with higher face layer densities compared to the  
200 controls. The increase of EPS content in the core layer led to a higher face layer density.  
201 This effect was probably due to the higher volume of core particles, causing increased

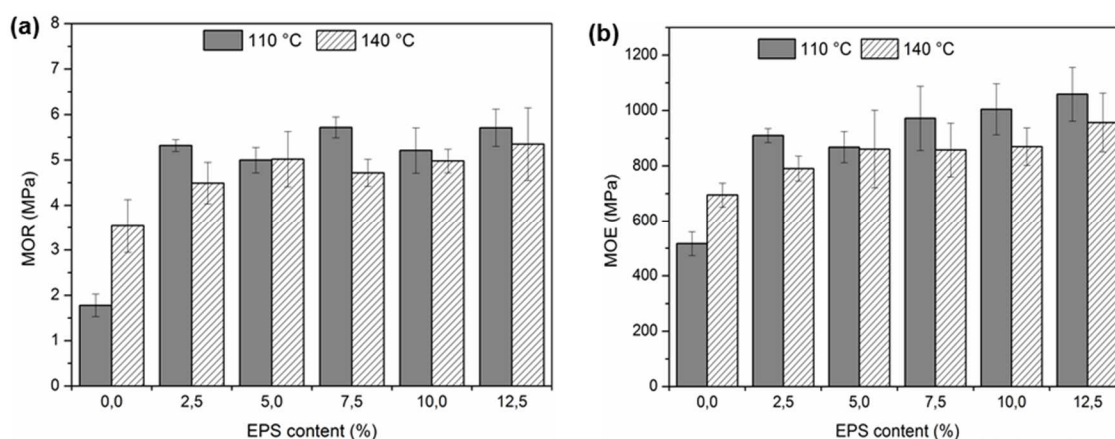
202 counterpressure during compression and thus more compacted face layer. The maximum  
203 face layer density (about  $650 \text{ kg/m}^3$ ) appeared in panels with 10 % and 12,5 % EPS  
204 content, while the minimum face layer density (about  $530 \text{ kg/m}^3$ ) appeared in control  
205 panel without EPS bead as filler.



206 **Figure 6:** Vertical density profiles of the low-density particleboards made with  
207 different contents of EPS bead in the core layer and (a) pressed at 110 °C or (b) 140  
208 °C.

### 209 **Bending properties**

210 The bending properties of the low-density particleboards are shown in Figure 7.  
211 Incorporation of EPS bead in the core layer had a positive effect on the bending properties,  
212 which was related with the improved density profile. The lowest MOR (1,8 MPa) and  
213 MOE (517 MPa) was observed for the control panel pressed at 110 °C. The highest MOR  
214 and MOE values were observed in the panel with addition of 12,5 % EPS bead as filler  
215 and pressed at 110 °C, with values of 5,7 MPa and 1059 MPa, respectively. Adding EPS  
216 bead significantly increased the MOR and MOE compared with the control, however, the  
217 variation of the amount of EPS from 2,5 % to 12,5 % had no significant effect on the  
218 MOR and MOE.



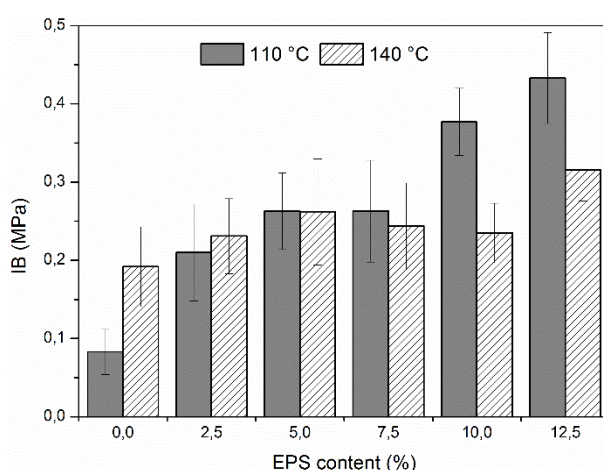
219 **Figure 7:** (a) Bending strength (MOR) and (b) modulus of elasticity (MOE) of the low-  
 220 density particleboards with addition of different contents of EPS bead in the core layer  
 221 and pressed at 110 °C or 140 °C.

222 Comparing the two press temperatures, higher temperature (140 °C) was more  
 223 favorable in reference panels without EPS as filler, because it is necessary to get a high  
 224 enough temperature in the core to make sure the adequate curing of the adhesive.  
 225 However, higher temperature had a negative effect on the bending properties of panels  
 226 with addition of EPS filler, resulted in lower MOR and MOE compared to that of panels  
 227 pressed at 110 °C. This is probably attributed to the shrinkage of EPS bead under press  
 228 temperature that is far beyond than its glass transition region (100 °C to 110 °C).

### 229 **Internal bond (IB)**

230 The values for IB of the low-density particleboards are shown in Figure 8.  
 231 Examinations of the tested samples revealed that the fractures were occurred in the core  
 232 layer. When pressed at 110 °C, adding EPS bead in the core layer as filler significantly  
 233 increased the IB of panels compared with that of control. The EPS bead filled the voids  
 234 between particles caused by the reduction of the amount of wood, allowing for improved

235 core layer integrity and cohesive strength, and accordingly enhanced IB strength. For the  
236 press temperature of 110 °C, it is noted that IB values of the panels with 10 % and 12,5 %  
237 EPS bead (0,38 MPa and 0,43 MPa) were significantly higher than that of panels with  
238 2,5 % to 7,5 % EPS and the control.

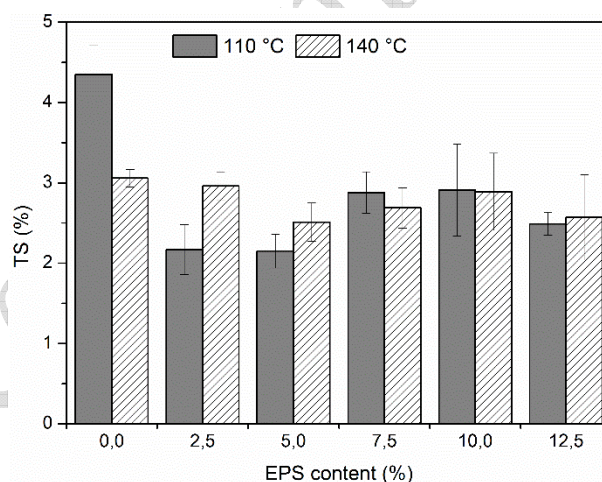


239 **Figure 8:** Internal bond (IB) values of the low-density particleboards with addition of  
240 different contents of EPS bead in the core layer and pressed at 110 °C or 140 °C.

241 Compared with the control panel (0 % EPS content) pressed at 110 °C, higher press  
242 temperature (140 °C) resulted in a significant increase in IB strength value from 0,08 MPa  
243 to 0,19 MPa. However, in the case of panels with addition of EPS bead, higher press  
244 temperature had a negative effect on the IB strength, especially in high EPS contents (10 %  
245 and 12,5%). This phenomenon is consistent with the previous study by Mir *et al.* (2016)  
246 who found that increasing press temperature had a negative effect on IB of lightweight  
247 particleboard using EPS as filler.

248 **Thickness swelling (TS)**

249 The thickness swelling after 2 h of water soaking (Figure 9) was measured to  
250 determine the thickness change of the low-density particleboards. The highest TS (4,4 %) was observed in panels pressed at 110 °C without adding EPS bead, due to the voids  
251 between wood particles. Adding 2,5 % content of EPS bead reduced the TS to 2,2 %,  
252 because EPS has the hydrophobic characteristic with a closed cell structure. Additionally,  
253 hydrophobic EPS bead filled in the empty spaces in the core layer, which reduced the  
254 water accessibility to the wood particles. However, there was no significant difference  
255 between TS of panels adding different contents of EPS from 2,5 % to 12,5 %. Compared  
256 with press temperature of 110 °C, pressing at 140 °C resulted in decreased TS (3,1 %) for  
257 panels without adding EPS bead, whereas TS was increased in panels adding EPS bead.  
258 panels without adding EPS bead, whereas TS was increased in panels adding EPS bead.



259 **Figure 9:** Thickness swelling (TS) of the particleboards with addition of different  
260 contents of EPS bead in the core layer and pressed at 110 °C or 140 °C.

## 261 Conclusions

262 EPS bead filled in the voids and empty spaces between wood particles caused by  
263 decreased density. As a result, adding EPS bead significantly improved the physical and

264 mechanical properties of the panel compared with the control, but the increase of the  
265 amount of EPS from 2,5 % to 12,5 % had no significant effect, except in the case of  
266 internal bond where high contents of EPS bead (10 % and 12,5 %) had a more remarkable  
267 effect than low contents. Comparing two press temperatures, 110 °C was preferable than  
268 140 °C to avoid softening and shrinkage of the EPS bead. The best formulation  
269 corresponded to the panel with density of 377 kg/m<sup>3</sup>, MOR of 5,7 MPa and MOE of 1059  
270 MPa, IB of 0,43 MPa and thickness swelling after 2 h water soaking of 2,5 %. These  
271 findings provide fundamental data for developing lightweight panels used in furniture and  
272 interior decoration.

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