

NANOFIBRILLATED CELLULOSE, THE SMALL PROMISING FIBER: CHARACTERISTICS AND POTENTIALITIES

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Resumo

Celulose nanofibrilada, a pequena fibra promissora: características e potencialidades. Celulose, um material vegetal, abundante, biodegradável, renovável e disponível no mundo todo, a partir da qual se extrai a celulose nanofibrilada, uma suspensão homogênea de fibras com diâmetros nanométricos. É possível que a celulose nanofibrilada substitua no todo ou parcialmente outros materiais, uma vez que suas propriedades físicas possibilitam tal aplicação. O conhecimento de suas características e propriedades são importantes na compreensão de seu comportamento em diversas aplicações. Com isso, os objetivos deste trabalho foram extrair a nanocelulose a partir de polpa branqueada de eucalipto, via processamento mecânico por moagem, e caracterizar a celulose nanofibrilada obtida, comparando-as. A celulose nanofibrilada apresentou aparência bem distinta em relação à polpa celulósica de partida, quando em mesma concentração, demonstrando maior poder de absorção de água e entrelaçamento fibrilar. O material nanofibrilado apresentou respostas diferentes em relação ao material de partida quanto às dimensões, estabilidade térmica, cristalinidade, viscosidade e grau de polimerização. A celulose nanofibrilada possui a mesma composição química por infravermelho, diâmetros menores, da ordem de 21,7 nm em relação aos 11,4 µm da celulose. A celulose nanofibrilada apresenta, também, menor resistência térmica, cuja temperatura de degradação foi cerca de 20 °C menor que a da polpa celulósica de partida e, teve seu índice de cristalinidade diminuído. Quanto à viscosidade e grau de polimerização, houve queda de 25% em comparação ao material de partida. Os resultados aqui apresentados indicam que a celulose nanofibrilada mostra-se diferenciada em relação à polpa celulósica de partida o que sugere sua aplicação como alternativa a materiais já existentes.

Palavras-chave: nanocelulose; desfibrilação mecânica; caracterização.

Abstract

Cellulose: an abundant, biodegradable and renewable plant material that is available all around the globe, from which nanofibrillated cellulose (a homogeneous suspension of fibers with nanometer-scale diameters) can be extracted. The nanofibrillated cellulose, in what concerns its range of application, may completely or partially replace other materials due to its particular physical properties. Knowing its characteristics and properties is important in understanding its behavior in various applications. In light of this remarks, the objective of this research was to extract the nanocellulose from bleached eucalyptus pulp through mechanical milling to characterize the resulting nanofibrillated cellulose and compare both. The nanofibrillated cellulose presented a very distinct appearance in relation to the original cellulose pulp when they were analysed in the same concentrations, demonstrating greater water absorption and fibrillar interweaving. The nanofibrillated material showed different responses in comparison to the original in terms of dimensions, thermal stability, crystallinity, viscosity, and degree of polymerization. The nanofibrillated cellulose displays the same chemical composition through infrared analysis and has diameters of around 21.7 nm, smaller than the cellulose diameter of 11.4 µm. The nanofibrillated cellulose also exhibits lower thermal resistance: its decomposition temperature was about 20 °C lower than that of the original cellulose pulp, and its crystallinity index has decreased. As for viscosity and degree of polymerization, there was reduction of 25% compared to the original material. The results presented hereby indicate that the nanofibrillated cellulose has unique features in relation to the original cellulose pulp, which supports its application as an alternative to existing materials.

Keywords: Nanocellulose, mechanical defibrillation, characterization.

INTRODUCTION

Nanofibrillated cellulose (NFC) exhibits attractive properties such as large surface area, high aspect ratio, low thermal expansion, non-abrasive nature and non-toxic character. It also has the ability to act as a significant reinforcement even at low loading levels, being used as a reinforcing agent in polymer nanocomposites. Nanocellulose-based materials are by nature environmentally friendly, carbon neutral, non-toxic, sustainable and recyclable. Thus, they have potential to be classified as green nanocomposite materials, with many favorable and unexplored characteristics.

In addition, NFC has great potential application in various industrial segments, such as textiles, regenerative medicine, tissue engineering, catalysis, surface coatings, drug delivery, food packaging and nanocomposite materials (CORREIA *et al.*, 2016; DEEPA *et al.*, 2015; KHALIL *et al.*, 2014; SACUI *et al.*, 2014; LAVOINE *et al.*, 2014). It can impact different fields not only due to its peculiarities, but also because it is very light, resistant, cheap, renewable, biodegradable and environmentally friendly (SOUZA *et al.*, 2016; SOUZA *et al.*, 2010). Apart from being manufactured from the cellulose pulp, this material may also be prepared from branches or even wood processing residues, which are transformed in materials of higher added value (DEEPA *et al.*, 2015). Nanofibrillated cellulose may even substitute in great measure most of the plastic (SABA *et al.*, 2014), since its physical properties enable its application in composite materials. Composite materials with natural fibers are used in the automotive industry, for example, due to an overall weight reduction, which increases efficiency and consequently reduces engine emissions (MOON *et al.*, 2016).

The mechanical treatment – through which NFC can be obtained – may be classified as mechanical defibrillation with high shear forces, microfluidization, and ultrasonication, resulting in a material composed of micro and nanofibrils. During the mechanical defibrillation process, the structure of the fiber, composed of multiple layers of nanofibrils bound by hydrogen bonding, is defibrillated by high shear forces generated by friction inside the equipment (CORREIA *et al.*, 2016; LAVOINE *et al.*, 2014; VILLANOVA *et al.*, 2011, KALIA *et al.*, 2014). Micro and nanofibrils of cellulose have many industrial applications, such as pharmaceuticals (VILLANOVA *et al.*, 2011), diet foods (OKIYAMA *et al.*, 1993), packaging and films (SYVERUD *et al.*, 2011), and special papers (SEHAQUI *et al.*, 2011), in addition to being used especially as a reinforcing agent in polymer matrices (KALIA *et al.*, 2014).

The interaction and compatibility between the polymer and cellulose raw materials are essential for industrial applications as well as for the processing and quality of the final products (TONOLI *et al.*, 2012). The morphological properties of nanocellulose structures, such as shape, length and diameter, depend mainly on the extraction process used and on the origin of the cellulose raw material (KALIA *et al.* 2014).

The present research aims at the production and at the comparative characterization of both the nanofibrillated cellulose produced through mechanical defibrillation with high shear forces and the original cellulose pulp, in order to understand the differences between both.

MATERIAL AND METHODS

In this study, we used bleached cellulose kraft pulp of *Eucalyptus* sp. (*Kappa* 2.0) from commercial sources.

Preparation of nanofibrillated cellulose via mechanical defibrillation

The pulp was initially hydrated in water and went through a degradation treatment by using a mixer. Then, it went through a mechanical defibrillation treatment in the Supermasscolloider Masuko Sangyo (MKCA6-3-Masuko Sangyo Co., Ltd.) grinder. The samples of cellulose material were suspended in distilled water at concentration of 1.5% on a dry basis. Grinder settings were 1500 RPM, distance between discs of 0.1 mm and total number of 10 passes, based on the literature (KALIA *et al.*, 2014). The resulting material was then designated Nanofibrillated Cellulose (NFC). During the sample processing, portions that had undergone 1, 3, 5, 8 and 10 passes through the grinder were separated, in order to evaluate viscosity, degree of polymerization (DP) and crystallinity of the cellulose during the process.

Morphological characterization

Scanning Electron Microscopy (SEM)

The images for the visualization of the structures and dimensions of the original fibers were obtained in a Tabletop Hitachi TM-1000 Scanning Electron Microscope. Measurements of 25 fiber dimensions were made, adapted from Muñiz and Coradim (1992). The images were processed with the Gwyddion 2.48 (Czech Metrology Institute) Open Source software.

Atomic Force Microscopy (AFM)

The topographic image of the NFC was obtained through Atomic Force Microscopy, non-contact mode, in an Agilent 5500 Scanning Probe Microscope equipment and PicoView imaging software. The characteristics of the tip are: monolithic silicon AFM probe - Model: TAP190AL-G (Budgetsensors), with Force Constant of 48 N/m; Resonant Frequency of 190 kHz; Length of 225 μm ; Width of 38 μm and Thickness of 7 μm . The sample was diluted in water to an approximate concentration of 0.03 mg/mL. Three drops of this solution were deposited on a surface made of Mica and air dried before proceeding for analysis. The images were processed with the Gwyddion 2.48 (Czech Metrology Institute) Open Source software.

Transmission Electron Microscopy (TEM)

The evaluation of the structure and dimensions of the NFC was done using a Transmission Electron Microscope JEOL – JEM 1200EX-II - with resolution of 0.5 nm, magnification range of up to 600 kx and voltage of up to 120kV, equipped with a CCD Gatan (Orius SC1000B) high resolution camera.

The NFC sample was prepared by dilution in water to an approximate concentration of 0.03 mg/mL. A drop of this solution was deposited on the sample holder, which consists of a nitrocellulose film-coated grill with grid size of 200 mesh. This sample holder was dried in a vacuum desiccator with silica as the desiccant at room temperature. After drying, the holder with the sample was taken to the imaging equipment. The images were processed with the Gwyddion 2.48 (Czech Metrology Institute) Open Source software.

Chemical and Thermal Characterization

Fourier transform infrared spectroscopy (FTIR)

Mid-infrared spectra were obtained in a Bruker model Tensor 37 spectrometer using films (produced by solution casting method) directly on the support. Measurements were performed between 4000 and 400 cm^{-1} in transmission mode with an accumulation of 64 scans and nominal resolution of 4 cm^{-1} .

Thermogravimetric analysis (TGA)

The equipment used was the Setaram Setsys Evolution TGA-DTA/DSC 1500. The test was carried out using an Alumina crucible. The conditions of analysis were: Argon purge rate of 20 mL/min, constant temperature at 30 $^{\circ}\text{C}$ for 10 min (stabilization), heating from 30 $^{\circ}\text{C}$ to 650 $^{\circ}\text{C}$ at a rate of 10 $^{\circ}\text{C}/\text{min}$ (thermal analysis) and cooling from 650 $^{\circ}\text{C}$ to 30 $^{\circ}\text{C}$ at a rate of 30 $^{\circ}\text{C}/\text{min}$ (finalization). Data on mass loss (thermogram) were acquired in the thermoanalysis stage. The bleached pulp samples were grouped in fiber bundles and the NFC samples were prepared over films obtained from solution casting and cut into small pieces of approximately 1 mm^2 .

Rheological Characterization and Crystallinity

Viscosity and Degree of Polymerization (DP)

Viscosity establishes a relationship between the DP of the chains and the level of cellulose degradation due to the mechanical defibrillation process. The determination of the viscosity and DP of both the cellulose pulp and the NFC suspensions followed the ASTM D4243 Active Standard (ASTM INTERNATIONAL, 2009). A 1% cupric ethylenediamine (EDC) solution was used as solvent and a capillary viscometer was used for measurements, according to the same Standard. Two samples from each cellulose treatment step (0, 1, 3, 5, 8 and 10 grinder passes) were used to evaluate the effect of the mechanical treatment on the viscosity and on the DP of the sample.

The specific viscosity (η_s) was transformed into intrinsic viscosity by using Martin equation. After that, the Mark–Houwink–Sakurada equation was used to transform the intrinsic viscosity data into the viscometric degree of polymerization.

$$\eta_s = [\eta] \cdot c \cdot 10^{k[\eta]c}$$

In which: η_s : specific viscosity; $[\eta]$: intrinsic viscosity, c : cellulose concentration (dry basis) in the sample; and k : a constant whose value is 0.14.

$$[\eta] = k(\text{GP}v)^\alpha$$

In which: $[\eta]$: intrinsic viscosity; k and α : constants that depend on the solvent/polymer system. The ASTM D-4243 (ASTM INTERNATIONAL, 2009) Active Standard recommends the use of $\alpha = 1$ and $k = 7.5 \times 10^{-3}$ for the Kraft cellulose system in cupric ethylenediamine.

Crystallinity Index

The crystallinity index is an empirical method that uses focusing and transmission techniques, measuring the intensity of the interference in the 002 crystalline plane ($2\theta = 22^\circ$) and the amorphous scatter at $2\theta = 18^\circ$. To determine the crystalline structure, the Shimadzu X-ray Diffractometer model XRD-7000 was used, along with the XRD-6100/7000 v5.0 software. A scanning speed of $2^\circ/\text{min}$ varying from 5° to 40° was adopted, using Cu-K α radiation with a 1.5418 \AA wavelength and a voltage of 40 kV with current of 20 mA. This method – adopted for the determination of the crystallinity indexes – is suggested by Segal *et al.* (1959). In this method, the crystalline cellulose percentage (I_{Cr}) is determined by the relationship between the intensity of the crystalline peak and the intensity of the amorphous portion:

$$I_{Cr} = \left(\frac{I_{002} - I_{am}}{I_{002}} \right) * 100$$

In which: I_{Cr} : crystallinity index, I_{am} : diffraction intensity of the amorphous portion; and I_{002} : peak diffraction intensity of the crystalline portion of plane 002.

RESULTS

Morphological characterization

Figure 1A shows the Scanning Electron Microscopy image of the original cellulose pulp sample, and Figure 1B illustrates the appearance of this material prior to the mechanical defibrillation process. The cellulose fibers analyzed presented width of $11.4 \mu\text{m}$ with deviation of $\pm 0.61 \mu\text{m}$ and a homogeneous distribution. After mechanical treatment, the nanofibrillated cellulose samples showed a visible change in their physical appearance (Figure 1C). The homogeneity of the material increased in proportion to the number of passes through the grinder.

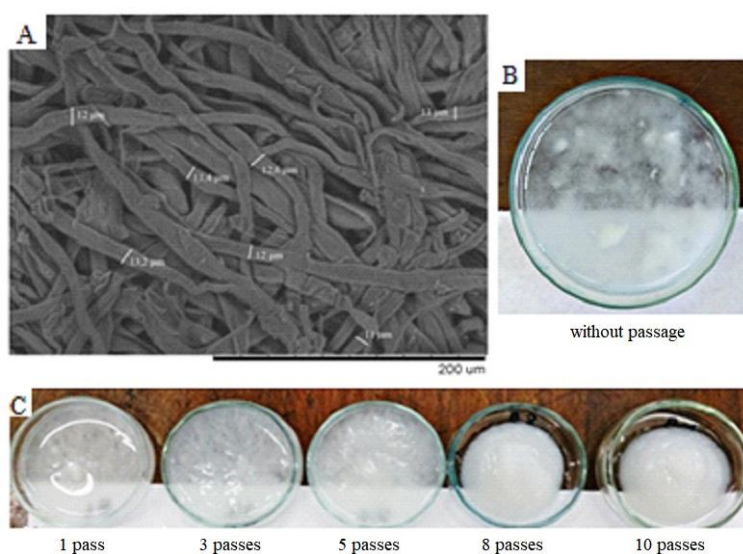


Figura 1. Imagens da polpa celulósica original (A e B) e CNF após o processamento mecânico nas diferentes passagens (C).

Figure 1. Images of the original cellulose pulp (A and B) and of the NFC after the respective passes through mechanical treatment (C).

A larger detail of nanostructures was verified by using the Atomic Force Microscopy (Figure 2A) and Transmission Electron Microscopy (Figures 2B-E) methods. The thickness of the nanofibrils was measured with mean of 19.5 nm and deviation of $\pm 12.11 \text{ nm}$ (Figures 2C, D and E).

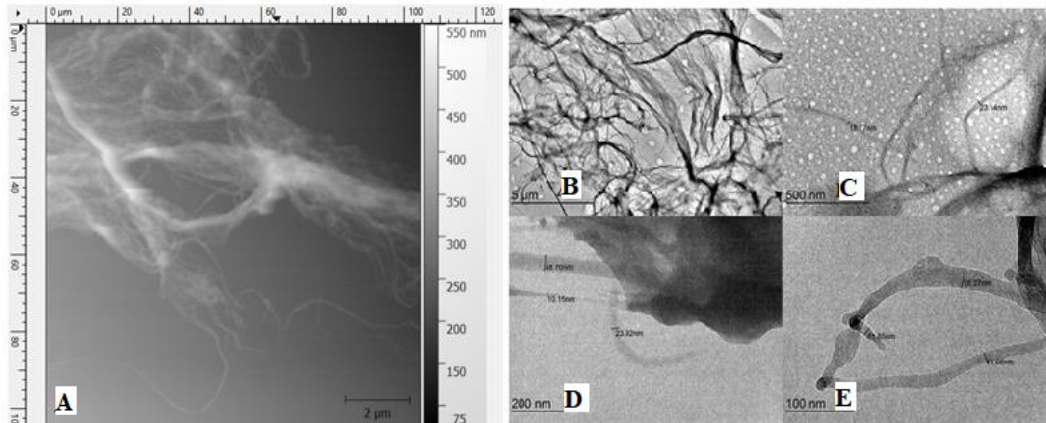


Figura 2. Imagens para CNF da análise por AFM aumento 2000x (A), e obtidas por MET: Vista geral da amostra com aumento de 1500x (B); detalhes em 3000x (C), 30000x (D) e 60000x (E).

Figure 2. NFC images of AFM analysis at 2000 times magnification (A), obtained by TEM: sample overview at 1500 times magnification (B); details at 3000 times (C), at 30000 times (D) and at 60000 times (E).

Chemical and Thermal Characterization

Analysis by Fourier transform infrared (FTIR) spectroscopy

FTIR spectra of the original cellulose and of NFC are shown in Figure 3.

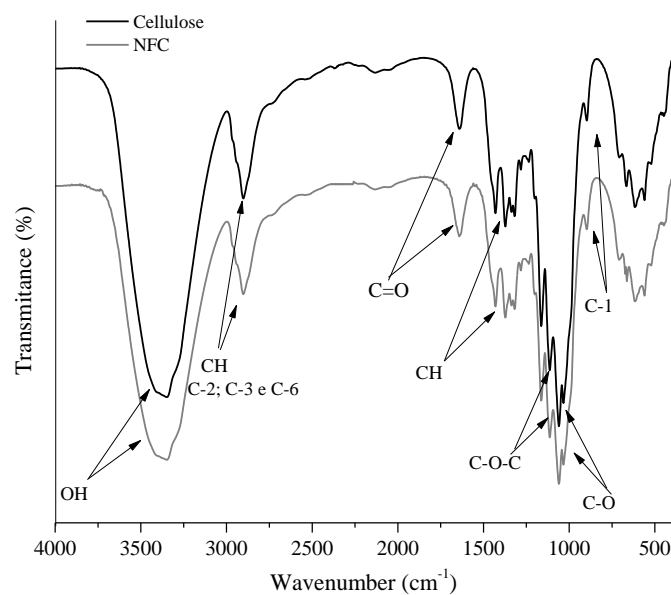


Figura 3. Espectro de FTIR das fibras de celulose antes (A) e CNF após o processamento mecânico (B).

Figure 3. FTIR spectrum of the cellulose fibers before (A) and NFC after mechanical treatment (B).

Thermogravimetric Analysis (TGA)

Figure 4 shows the results of the thermogravimetric analysis of the cellulose fibers before and after the mechanical treatment. In both samples, two events of mass loss were observed.

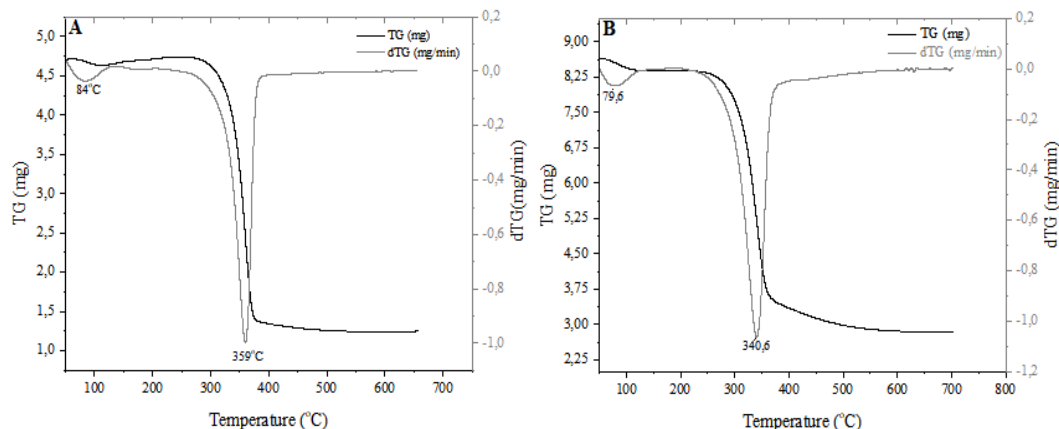


Figure 4. Termogramas obtidos para as amostras de celulose (A) e celulose nanofibrilada (B).
Figure 4. Thermograms obtained for the cellulose (A) and for the nanofibrillated cellulose (B) samples.

Rheological Characterization and Crystallinity

Viscosity and Degree of Polymerization

The mechanical fibrillation was responsible for the viscosity and DP variation in the sample, when compared to the original material (Table 1).

Tabela 1. Resultados de viscosidade e GP do material original e após cada passagem no moinho.

Table 1. Viscosity and DP of the original material and after each pass through the grinder.

Pass	Specific viscosity (mPa.s)	Viscosity for c^*	Intrinsic viscosity	Degree of polymerization
0	7.29f	2.88f	5.71e	2410e
1	3.69a	1.96a	3.90a	1643a
3	3.82b	2.00b	4.56d	1923d
5	4.69c	2.26c	4.37c	1844c
8	5.06d	2.37d	4.25b	1793b
10	5.34e	2.43e	4.37c	1842c

*According to c values in (ASTM INTERNATIONAL, 2009). Letters next to the numbers indicate that these values are statistically different from each other in the Tukey test (95% of confidence).

X-ray diffraction (XRD)

By using X-ray diffraction, as indicated by Segal *et al.* (1959), it was possible to calculate the crystallinity index of the cellulose before and after the mechanical treatment. This index varied with the number of passes through the grinder. The results are shown in Figure 5.

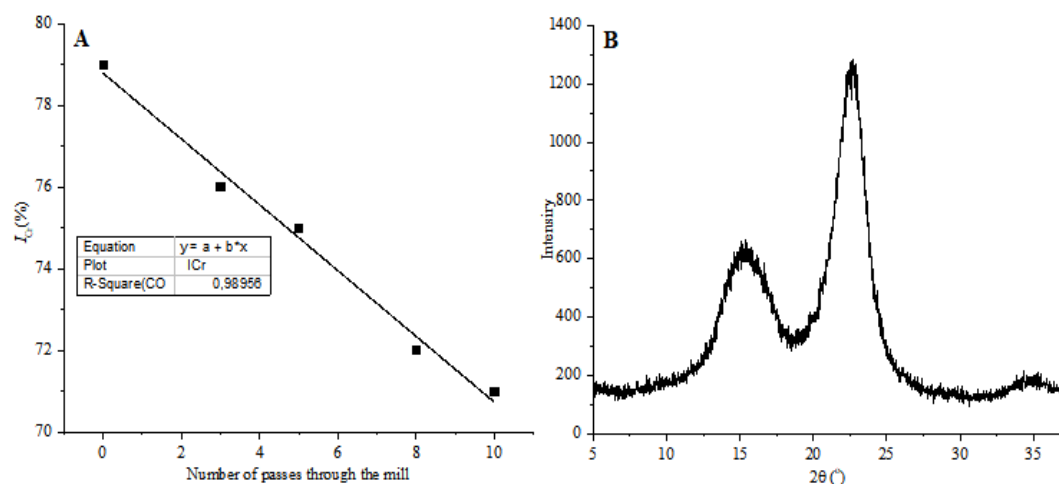


Figura 5. Variação no índice de cristalinidade para a celulose de acordo com o processamento mecânico (A) e Perfil do difratograma de Raios X para as amostras analisadas (B).

Figure 5. Variation in the crystallinity index of the cellulose according to the mechanical treatment (A) and X-ray diffraction profile for the analyzed samples (B).

DISCUSSION

Morphological characterization

The width of the cellulose fibers measured a mean of 11.4 μm ($\pm 0.61 \mu\text{m}$), which is consistent with the mean typically found in literature (SILVA *et al.*, 2007). After mechanical defibrillation, a visual change in the appearance of the material was observed, as well as a greater fibril/water and fiber/fiber interaction capacity through hydrogen bonds.

The AFM technique provides information on the exact topography of the nanostructures. As sample scanning occurs, valleys and peaks are defined as a function of the shape and organization of the nanofibrillated cellulose. The images obtained help in the evaluation of the material by showing properties of the NFC, such as nano-scale diameters and varied lengths. They also depict a formation of a nanostructure network, which differentiates the fibers from the original ones. Figure 2A and 2B show that the mechanical treatment on the cellulose pulp causes a fibrillation effect on the cell wall of the fibers, reducing their diameter and generating NFC, whose length is in micrometer scale and diameter in nano-scale, as studied by Coutts (2005).

Since cellulose is considered nanofibrillated when one of its dimensions is below 100 nm, it is concluded that the mechanical defibrillation treatment enabled the production of nano-scale material, as also observed by other authors (SEHAQUI *et al.*, 2011; SYVERUD *et al.*, 2011).

When occurring in the outer layers of the cell wall, defibrillation exposes the inner layers, reduces one of the cell wall dimensions and increases its contact area and its potential for bonds, thus forming a nanostructured network. In this sense, the three hydroxyl groups bonded to carbons 2, 3 and 6 of the glucose units in cellulose are responsible for the intermolecular interactions in the cellulose chain, allowing for new structures to be formed (HABIBI *et al.*, 2007).

Chemical and Thermal Characterization

For the mid-infrared spectrometry analyses (Figure 3), the characteristics of cellulose were attributed for both samples: the intense and broad band in the region from 3500 to 3400 cm^{-1} corresponds to the absorption of OH groups; the signal near 2900 cm^{-1} represents the symmetrical stretching of C-H bonds originating from H-C-OH (C-2 and C-3 carbon) and CH_2OH (C-6 carbon) groups of the cellulose; the band in the region 1640 cm^{-1} can be attributed to the presence of conjugated carbonyls, which probably derived from the oxidation of carbohydrates during the bleaching process (FAN *et al.*, 2012).

The bands around 1430 and 1370 cm^{-1} refer to the angular deformation of C-H in the carbonic chain; absorption bands in 1330 and 1320 cm^{-1} correspond to the OH angular vibrations of primary and secondary alcohols; bands in 1165 and 1110 cm^{-1} are in this regions due to asymmetric axial deformations of C-O-C; bands from 1050 to 1030 cm^{-1} correspond to the axial deformations of C-O in primary and secondary alcohols; and finally the deformation in 896 cm^{-1} is attributed to the anomeric carbon C-1 of the anhydroglucose. Because it is a bleached pulp with low *kappa* number, no characteristic bands of lignin were observed in the cellulose spectrum in general, which justifies the qualitative character of the FTIR analysis (ASHORI *et al.*, 2014).

As observed in both spectra, the samples behave in the same way. This evidence suggests that nanofibrillation of cellulose does not promote change in its carbon chain, which remains with the same supramolecular structure.

The thermograms of the cellulose pulp (Figure 4A) and nanofibrillated cellulose (Figure 4B) samples can be divided into three events, considering that the initial mass of the cellulose pulp was 4.5 mg. In the first event, from 45 $^{\circ}\text{C}$ to 130 $^{\circ}\text{C}$, the thermogram presented a small mass loss (3%), which is attributed to desorption of water present in the fibers. In the second event, from 280 $^{\circ}\text{C}$ to 375 $^{\circ}\text{C}$, with degradation peak at 359.6 $^{\circ}\text{C}$ and mass loss of 70%, the crystalline region began to be destroyed. The decomposition of the sample was likewise noted, resulting in the increase of the amorphous portion and a decrease in the degree of polymerization. The third event occurs from 375 $^{\circ}\text{C}$ up to the end of the analysis: it is when the crystalline region was completely destroyed and decomposed into D-glucopyranose monomer. This monomer, in turn, is decomposed into free radicals at higher temperatures (above 600 $^{\circ}\text{C}$). The complete process generated a mass loss of about 73%, leaving a mass residual of approximately 1.24 mg.

For the nanofibrillated cellulose, the decomposition process is the same, but with different temperatures for the thermal events. The initial sample mass was 8.56 mg. The first event is also related to the evaporation of the water present in the fibers, since it occurred from 79.6 °C to 130 °C and had a mass loss of 3%. The second event occurs from 235 °C to 392 °C, with degradation peak at 340.6 °C and mass loss of approximately 59% at this temperature. The total process generated a mass loss of approximately 62%, and a residual mass of 2.84 mg.

The thermal degradation events are attributed to two main mechanisms: i) dehydration of the cellulose caused by an endothermic event; and ii) thermal depolymerization of the cellulose (NETO *et al.*, 2013). From 392 °C onwards, the thermal decomposition of the cellulose in D-glucopyranose monomers starts, as well as its decomposition into free radicals (ASHORI *et al.*, 2014).

The thermogravimetric curves are very similar, since NFC and cellulose have basically the same chemical composition. The initial temperature of the cellulose degradation (280 °C) was higher than the NFC's (235 °C). The decrease in the thermal stability of the natural fiber due to mechanical treatment has been described in literature and generally is related to the cellulose degradation resulted from the shear forces involved in the mechanical treatment (MTIBE *et al.*, 2015; QING *et al.*, 2013).

Rheological Characterization and Crystallinity

The results found for both viscosity and degree of polymerization (Table 1) after the mechanical treatment demonstrate the negative influence of this procedure on the integrity of the cellulose fiber. According to some studies, mechanical defibrillation treatment causes irreversible changes in the fibers, for example, reduction in crystallinity and viscosity resulted from internal and external fibrillation. Defibrillation exposes the inner layers, reducing the size of the fibers, which facilitates the formation of inter and intra fibrillary interactions, forming a nanostructured network (COUTTS, 2005; WANG *et al.*, 2012; KHALIL, 2014).

Thus, a decrease in the viscosity and in the DP of the cellulose was observed in relation to the initial sample (which did not pass through the grinder). When comparing the viscosity and DP results of the samples treated mechanically, a variation in both properties was observed (Table 1), which demonstrates the influence of mechanical treatment on the integrity of the material.

During the first passes (1 and 3) through the grinder, there was a sharp decrease in the rheological properties of the samples. As the number of passes through the grinder increased, as well as the formation of fibrils, the inter- and intra- fibrillary attraction forces were capable of exerting an effect that minimizes the mechanical degradation observed in the initial stages of the process. This effect may be due to the increase in the aspect ratio, in the contact area between the fibrils surface, and in the iterations and interweaving of the nanofibrils, generating a kind of resistant nanofibrillar net that enables these interactions and maintains the characteristics of viscosity and DP very similar in the treated samples (5, 8 and 10). This observation indicates that the formation of nanofibrils influences the pulp properties, which becomes a material of peculiar and desirable characteristics for the development of new products.

Because of the mechanical action, the material defibrillates, as observed in the micrographs shown in Figures 1 and 2. This behavior is probably responsible for the decrease in the DP and in the viscosity of the cellulose in relation to the initial material, since it generates cellulose chains of varying sizes. The reduction in the cellulose viscosity after mechanical defibrillation treatment was also observed by some authors (WANG *et al.*, 2012).

When the number of passes through the grinder increases, the crystallinity index or the beginning of the degradation of the crystalline portion decreases, as a function of the shear forces involved in the process. The internal and external defibrillation of the fiber is the cause of the reduction in the dimensions of the fibers, in addition to affecting its crystallinity. The X-ray diffractogram of the cellulose shows a peak in the region 2θ of 15 °C (little intense) and a more intense one in the region 2θ of 22 °C (Figure 5B), which represent the crystal planes for both cellulose fibers and nanofibrillated cellulose. The reduced crystallinity of the cellulose after treatment may be the property responsible for the decrease in the thermal stability of the viscosity and DP of this material, since this is the portion of the cellulose fiber that suffers the mechanical action of the grinder, as observed by other authors (KALIA *et al.*, 2014; WANG *et al.*, 2012; COUTTS, 2005).

Therefore, the values found for the cellulose crystallinity in this study are similar to those expected and suggested by previous studies. Regarding nanofibrillated cellulose, there is practically no variation in the crystallinity indexes. However, there is a tendency of reduction in relation to the initial value, which has been also observed in the literature (KALIA *et al.*, 2014).

CONCLUSION

- The mechanical defibrillation treatment of the cellulose was sufficient to generate fibrils of nanometric dimensions in thickness.
- The nanofibrillated cellulose suspension is much more homogeneous than the initial fiber suspension, because the surface area of the nanofibrils is much larger. This property provides much more stability through the possible hydrogen bonds.
- The nanofibrillated material showed different responses in relation to the initial material. In addition to the dimensions, the thermal stability, crystallinity, viscosity and DP presented lower values than the original material.
- The reduced crystallinity of the cellulose after treatment may be the property responsible for the decrease in the thermal stability of the viscosity and DP of this material, since this is the portion of the cellulose fiber that suffers the mechanical action of the grinder.
- As surface area increases, the number of reactive points on the surface increases, which can be used in derivatization reactions or in the basis of other compounds of interest, thus, providing a range of options for the production of new materials.

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