

Attributing the Electrical Conductivity into Asphalt Composite Using Kaoline-Dominant Mixture Clays

Ameer J. Al-Shammari ^a

Qais. A.J. N. Al Rashid ^b

Department of Civil Engineering, University of Babylon, Babylon - Iraq,

ameeralshammari@gmail.com

kezalr63@gmail.com

Submission date:- 8/10/2019

Acceptance date:- 22/12/2020

Publication date:- 18/2/2020

Abstract

Asphalt mixtures have great potentials as electrical connectors for many functions in the field of self-sensing, hospitalization and energy collection. Electrical conductivity (EC) controls the pouring of asphalt concrete to a priority stage for such presentations, taking into account some additives that minimize damage to basic materials over time. Previously fibre conductivity tests are used in the conductivity of the asphalt mixture. There is now a need for mitigation due to the sudden change in the ER electrical curve of the filtration conditions of the down mixtures, considering the sudden transition from the electrical resistivity (ER) values to the conduction phase (EC). Efficient clay mixtures to relieve defects of sudden changes are considered eco-friendly. Therefore, this study looks for an output where encapsulation efficiency used by directing the electrical conductivity (EC) of asphalt concrete only by adding a specific content of bentonite content in the kaolin-dominant mixture between (KB0.1) to (KB0.4). Therefore, eight different types of clay mixture KB0.1 to KB0.4 and Kaolinite 0.9-Sand 0.1 to KS0.4 have different geophysical properties and different geotechnical parameters. EC values. ER values are evaluated by asphalt-mixed samples containing different contents of the dominant K-clay mixture.

Keywords: Asphalt mixtures, Electrical resistivity (ER), K-dominant clay mixtures, Asphalt mastic, Asphalt concrete, Electrical conductivity (EC).

Introduction

This study focuses on the possible applications of EC for asphalt, which some former investigators have tried using hard wool, hard fibre, and carbon fibre. In this paper, some of the contents K-Bentonite clay mixtures, which are additives to advanced electrode conductivity, have been added and the effect of different types of K-Bentonite contents on EC in composite materials for asphalt have been emphasized. Previous investigations have shown that the contents of the K-Bentonite. Prominent results have been obtained for specific control conductivity by controlling the gradual decrease of ER with increased Kaoline-Bentonite content. In this regard, the procedures for the mastic are developed by [1] who improved asphalt concrete by adding conductive materials. The concept of asphalt concrete conductivity implemented by [2], where many efforts have been greatly encouraged in detecting the potential benefits of using electrical properties as one of the geotechnical parameters of asphalt mixtures. For example, applications of electrical heating of ice and snow platforms [3]. While asphalt concrete is used as a multifunctional material by monitoring conductivity (EC) and with the use of asphalt concrete which is a composite non-conductive material, using additives with EC, can develop conductivity. The structure of asphalt composition can be designed through the use of electrical properties. Therefore, other specific functions of compounds that have properties which can be used as intelligent structures affect the performance of the lining of the dominant structure, regarding the safety and positive efficiency [4]. There are several ways to correlate measurements of conductivity values in asphalt concrete. Therefore, the researchers have previously attempted to establish conductivity to the asphalt concrete by adding fillings with conductivity. Most of the previous selective primary conductors are alternative additives consisting of powder types to obtain better fibre quantity and quality to improve conductivity [5].

1. Materials and Methodology

1.1. Materials

Mastic asphalt samples are arranged using the asphalt binder according to [6] with a mixture of different fillings with various EC, the binder with a standard dry unit weight of 1.032 g/cm^3 . Mastic asphalt samples are made from asphalt bonding materials in balanced proportions for the total mastic of both asphalt fillers and gaskets, which remained constant throughout the test. Portland cement (Type II) used as a conventional non-conductive additive. A portion of the cement filler is replaced with K-Bentonite stuffing materials, which range between 10% and 50% of the mastic weight for example; K-Bentonite with the installation content as materials such as; wood, viscous materials, and others are 20% and 30% cement content to maintain standard packing in mastic.

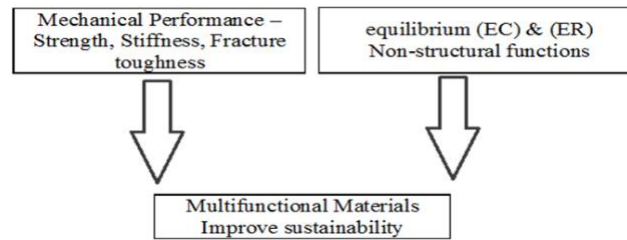


Figure1. Multifunctional materials with mechanical and (ER) measurement

The samples are arranged in the form of a thin layer where dry pine wood is added to these samples, to strengthen the binder, filler and wood at 105°C for nearly 1 hour in the oven before mixing. Binder and filler a mixture of cement and K-Bentonite contents mixed at different rates. Epoxy-coated wooden blocks are then reinforced again at 120°C with one hour of hydration. The thickness of the mastic determined and the weight of the wood mass determined before and after the distribution to apply the relationship with the weight of the dry unit weights and to gain uniform thickness. The priority in the test of the mastic samples is at room temperature for adaptation before the basic test. The 50 mm copper rods are proven to be electrodes. The silver paste is tied to copper-plate strips using three-point sensors. Previous analyses of the K-bentonite clay mixture have shown promising results for EC control in the gradual reduction of ER measurement relative to the increase of bentonite contents in kaolin-dominant. Asphalt material has been used extensively for the construction of loads (driveways and bicycle driveways).

2.1.1 Evolution in clay studies

The use of bentonite or sand with dominant Caroline as a mixture of minerals from kaolinite, elite, feldspar, mica, quartz, and montmorillonite Clay [7] used as fillers or additives to improve the durability of asphalt concrete, including carbon, clay, asphalt concrete, and therefore its use aims to increase the service life of asphalt concrete in paving systems and make it sustainable according to [8]. It can be noted that the vital benefit of using clay is to modify pavement material to meet growing the commercial interest, in [9], unlike other studies on how clay and montmorillonite change in the behaviour of polymeric matter, there is an interest in knowing the components of clay and its mineral properties. Ironically, large quantities of kaolin are made up of dust during the manufacture of Portland cement. Bentonite is used as a dietary supplement in the [10]. These mixtures may experience various industrial achievements, such as membranes [11]. Also, the mineral property of clay, such as bentonite, is exposed to properties in which particle properties change. These properties can change in clay minerals which depend on the content of the water solution and the cations around the particles and are transportable in the interstitial void. In [12], the development of many other mineral products such as bentonite containing the montmorillonite property has the dominant bentonite property. So kaolin with this mineral mixture will not be exposed to harmful effects, there are treatments in the industrial structures, both for those health risks with attention to the priority of safety in the workplace, and attention to the consumption of clay as a filler or as additives in multiple application [13]. Bentonite could be used in the contents of the clay mixture and can be used as hydraulic containment in the following categories [14] additive to compacted soil barriers in landfill and cover systems. Bentonite is used in vertical slicing as in walls, which have been filled with a mixture of bentonite with another dominant mineral clay or bentonite cement, and in these experiments, as shown in the K-bentonite mixture used, as flakes filled with a mixture of mastic asphalt and K-bentonite as selective content.

1.2. Test Methodology

1.2.1. Preparation of samples

2.2.1.A. Samples of Kaolin, bentonite, and sand

Samples of kaolin-dominant are prepared to obtain from two Australian companies. A large pilot program is implemented in these samples to achieve the objectives of this study. Samples collected under the Unified Soil Classification System (USCS) are analyzed using sieve analysis, liquid limits, plastic limits, and plasticity index test results obtained. In the study of [15], eight kaolinite-dominant clay mixtures are tested for comparison and selection to achieve the objectives of this study, as shown in Fig 2. In this study, the effect of coarse soil (sand) and swelling clay (bentonite) on the value (ER) of the clay mixture in kaolin-dominant is detected through the use of geophysical properties and geotechnical parameters. The KB and KS membranes are hand-made, with water solution contents 5%, to 23% are developed by (NaCl) ion, followed by 180 rpm for 40 hours, so the gel is obtained homogeneously.

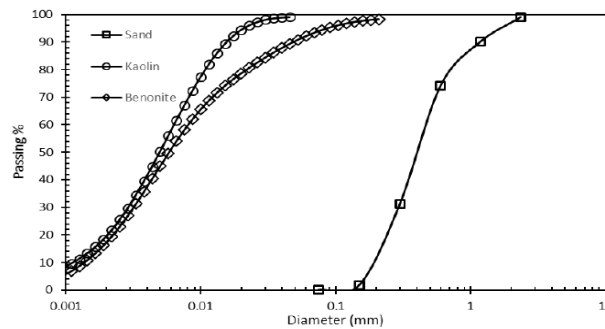


Fig 2. Particle size distributions of sand, kaolin, and bentonite [15].

2.2.1.B. The asphalt concrete samples

The asphalt concrete samples are prepared using the asphalt binder, by selecting type paving grade asphalt (PG70-22), with a density of (1.032 g/cm³), then, the samples are prepared according to the Superpave mixture design method. The optimal binder content is determined by the weight of the total mixture using the Superpave method. The gravel consists of limestone powder (coarse aggregate) 35%, 5% filler, and 60% sand (fine aggregate). The specific gravity for coarse aggregate [16], the fine gravel and fillings also are measured. The ratio of coarse aggregates and fine is measured to meet the requirements of mixtures specified in [17]. Finally, the results of the sieve analysis selected from fine and coarse aggregates, and the mixture design determined in the form of a stable mixture of samples containing clay mixtures of varied as a conductor. 5% of the filler content in the mixture maintained to be constant by adjusting the variable for the cement packing quantity as non- conductive. After sampling, the volumetric analysis has been carried out according to the Superpave standard specification for volumetric mixture design to comply with [17], and [18]. The samples of aggregates and fillers are displayed together in the oven at 105°C for more than 1 hour to remove the moisture. The binder heated for an hour at the same temperature before mixing. After mixing the filler with the aggregates, the bleach is added with the filler and aggregate, which are displayed together on the mechanical mixer until the material is well coated. The mixture samples adapted in the air conditioning before being placed in the oven at a compacted temperature (105°C) [19], Six cylindrical samples are brought to each stage, as shown in Figures (3,4 and 5): three of them administrated to measure non-direct tensile strength, but the rest is administrated to measure EC, where clay mixtures of 10% replace a small fraction of cement filler in mastic samples.

1.2.2. Fibre Fineness

Previous tests have used conductive fibres added to asphalt mixtures, so clay mixture such as K-Bentonite 0.4 is required, which has a minimum electrical ER of 20% to 30%. To complete the curve of the distribution of aggregate, it must determine the maximum moist dry unit weight in the total part of the mixture by the following equation:

$$P = 100 \left(\frac{d}{D} \right)^{0.5} \dots\dots\dots 1$$

Where P is the total volume relative to the total sieve, D is the maximum aggregate volume in the mixture. These summaries are derived from [20]. In this investigation, the compacted density of Portland cement associated with the classification of aggregates are used in manufacturing [6;21; 22]. As a layer of fibre (or titter T) can be more accurately defined as the mass per unit length., since it depends on diameter d of the fibres and its moist dry unit weight ρ. Fibre fineness unit is TEX (grams per 1,000 m). The following equation is performed to estimate the fineness of fibre diameter [23]:

$$D = \sqrt{4 * \frac{T}{(\pi * \rho)}} \dots\dots\dots 2$$

It is possible to measure accuracy by using two options, either the first option is full sloughing and the second option is to measure individual threads. As for the voids, a pulley is used to prepare fixed-length fibres (usually 100 meters) or by determining the fineness of individual threads by analyzing the resonance frequency f at the specified length l and by determining the pre-tensioning with force F. The following equation shall be compatible with the corresponding precision calculation [24]:

$$T = \frac{F}{4 * F^2 * l^2} \dots\dots\dots 3$$

However, the following restrictions observed in the use of conductive fibres: The filtration threshold is the required point in the sudden change from the insulation state to the conduction stage which is made to control the fibre distribution, and to ensure the uniform distribution of all the mixture contents, which hold the property as a good conductor [6]. Therefore, mixing the fibres with asphalt concrete has shown a challenge to physical dimensions in the fibres, which may lead to heterogeneous ER in samples through difficult tests. The clay mixtures are one of the conductive additives being a powder used as a supplement to this paper. While the above difficulties are dominant with conductive type fibre additives, the use of clay mixture as a powder confirms the ease of mixing and is relatively uniform.

2.2.3. Strain and sensor damage

The strain and damage are detected by the self-sensing mechanism through the attached smart structures [25]. This type of detection is preferred due to the integration of the sensors because of their low cost, high durability and high volume, according to the technical procedures of fixed processing, in the repetition of its quality control procedures which are reliable to apply standard ER measurements, in [26], it is necessary to contact ER to materials filled with asphalt mixtures or common clay mixtures. When an external load provided, the particles will approach each other in the filling of the mixture contents, because there are two contradictory sets of ER values and conductivity values, where ER values have decreased. [23].

2.2.4. Mechanical tests

2.2.4.1. Indirect tensile force test (IDT)

The tensile force properties of K-bentonite and K-Sand mineral clay prepared under extension, as a single-axle using universal testing machines. The films are cut into 5 mm wide and 25 mm longitudinal strips, the films which are formed between the upper and lower panels to test the strength of the tensile, and which are performed on a 2 mm/min strain, where the tensile strength, r, and elongation factors renewed. Three compacted samples have been tested at room temperature (25 °C) before mechanical and hydraulic tests [6;21;22]. And for measurements of ER values in samples in IDT cases by (Instron 5583), where the load has used (monotonous compressive) on each sample through the IDT test at a constant displacement rate of 40.8 mm/min (1.58 inch /min) until it has broken, where stress and strain have been loaded. IDT’s strength calculated as follows:

$$ST = \frac{2p}{\pi * l * D} \dots\dots\dots 4$$

Calculation of Volumetric Properties

The test conducted following [22], where the specific gravity is Gsb and the aggregates (coarse+ fine+ filler) in the mix. Most samples contain an air-void (AV) c about 4% according to [19]. Gsb decreases with the increase in the content of the clay mixture due to the added weight of the dry density of the dominant material mixture less than the weight of the dry cement unit compared to the increase in the weight of those units. Where Gmm and Gmb, are the theoretical gravity and the other is the specific gravity of the mineral clay mix, respectively according to Australian standards [16] and [21]. To specify the volumetric properties (VTM, VMA, VMA, F / A) of the mixture, the specific gravity of the mixture (Gmb), the maximum gravity (Gmm), the total degree of asphalt content is determined. In addition, the determination of the effective gravitational attractiveness of the aggregate and the total gravity of aggregates are calculated, where VMA defines the voids in the mineral aggregate (VMA) by using the following formula:

$$VMA = 100 - (Gmb \times ps)Gsb \dots\dots\dots 4$$

VMA is the air voids that exist between the total particles in a compacted mixture, which includes asphalt-packed voids.

$$VTM = 100 \times 1 - Gmb \dots\dots\dots 5$$

Where Gmb = bulk specific gravity of mixture. ps = per cent stone ($100 - P_b$ Ignition Method)

Gsb = bulk specific gravity of aggregate,

Determine the voids filled with asphalt (VFA) using the following formula:

$$VFA = (VMA - VTM) \times 100 \dots\dots\dots 6$$

The properties of VFA are necessary as a measure of relative robustness with an excellent relation to the density. Also, the samples are organized and assessed to provide the volumetric characteristics of the mean values.

2. Result of materials (Clay mixtures) and mastic asphalt

3.1 Result of materials (Clay mixtures)

There is an urgent need to mitigate sudden changes in ER values by activating the contents of asphalt mixtures, as well as by stimulating the enormous potential of asphalt mixtures and multifunction protection. There is an urgent need to mitigate sudden differences in the ER curve by tempering the practical widths of asphalt mixtures, while simultaneously exposing the enormous potential of asphalt mixtures and multifunctional displays. It has been observed that the sudden displacement of ER values to the conduction control phase to the phase that is considered a priority for the higher asphalt material compared to the rest of the mixture, as shown in Fig. 3.

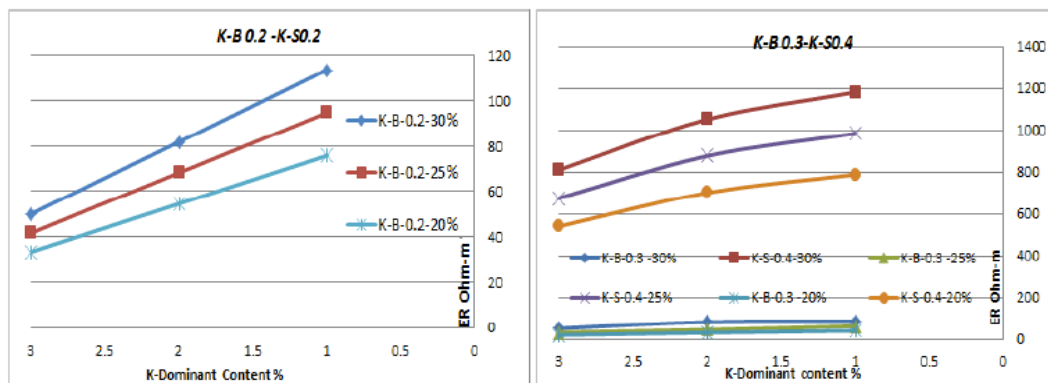


Figure3. Comparison (ER) of 30% K-dominant mixture contents

3.2. Result of mastic asphalt

Results show that ER values in mastic asphalt vary greatly with the variation of Kaoline-dominant clay mixtures. The mastics, which contain natural slices of clay mixtures, show a gradual decrease in the values of ER, which is proportional to the increase in the content of the clay mixtures, where low ER values can be obtained adequately with flakes scattered to the natural clay mixture. On the other hand, the non-controlled kaolin-dominant clay mixtures reduce ER in such, Kaolin-sand with high surface area properties that are difficult to mix.

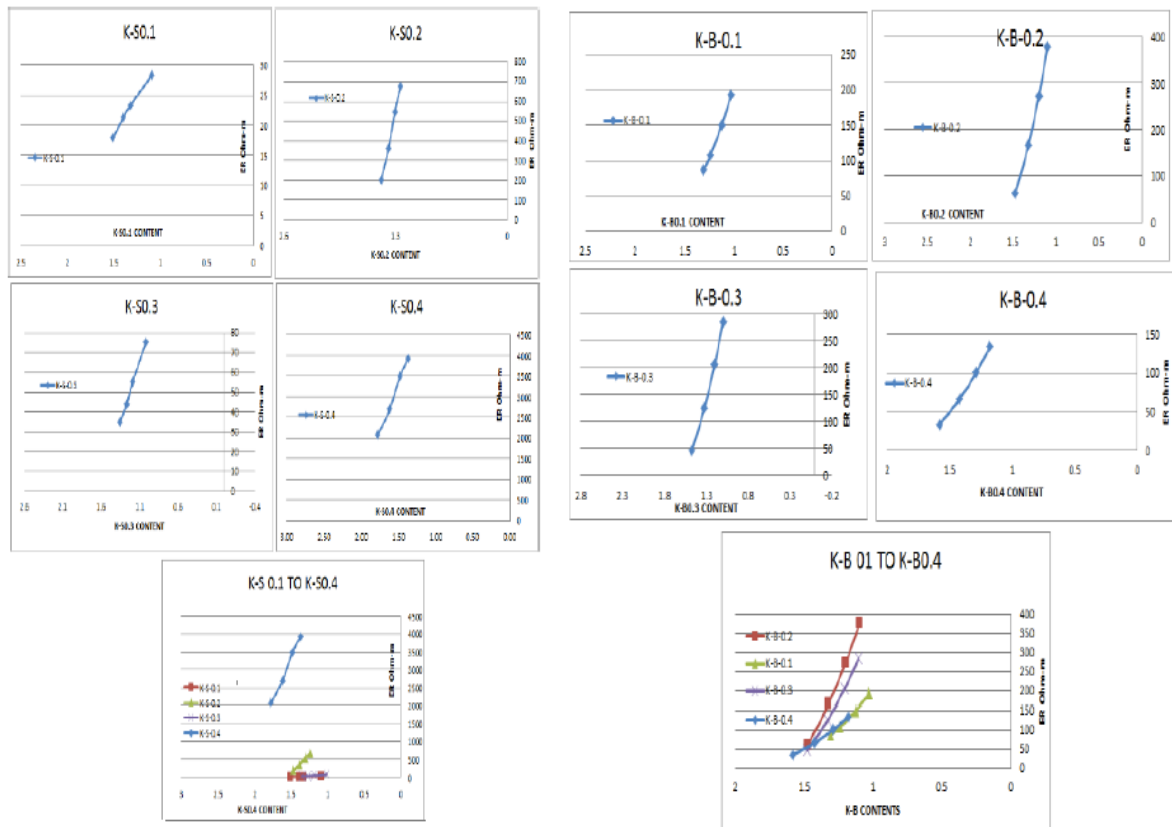


Fig4. Laboratory comparisons between values for measurements ER for different contents for clay mixtures K-dominant and separate from contents of mixtures in concrete asphalt.

Four highly efficient clay mixtures are selected; KS-0.3 to KS-0.4 KB-0.3 to KB-0.4 Out of eight different types; KS-0.1 to KS-0.4 KB-0.1 to KB-0.4, to complete it in their choice of asphalt concrete, as shown in Figure 4, where the impact of aggregates on the ER is tested. Clay mixtures with mineral property were also found to provide consistency of the EC value together to improve the mechanical performance of asphalt concrete.

3.3. Result of materials (Clay mixtures) *On the IDT strength*

The reduction of ER values in KS-0.1 to KS-0.4 is twice the reduction of ER values in slurry mixtures samples from KB-0.1 to KB-0.4 without asphalt contents in phases 1 and 2, affecting the IDT values. The IDT trace values are shown in ER measurements in clay mixtures, as shown in Figure 5.

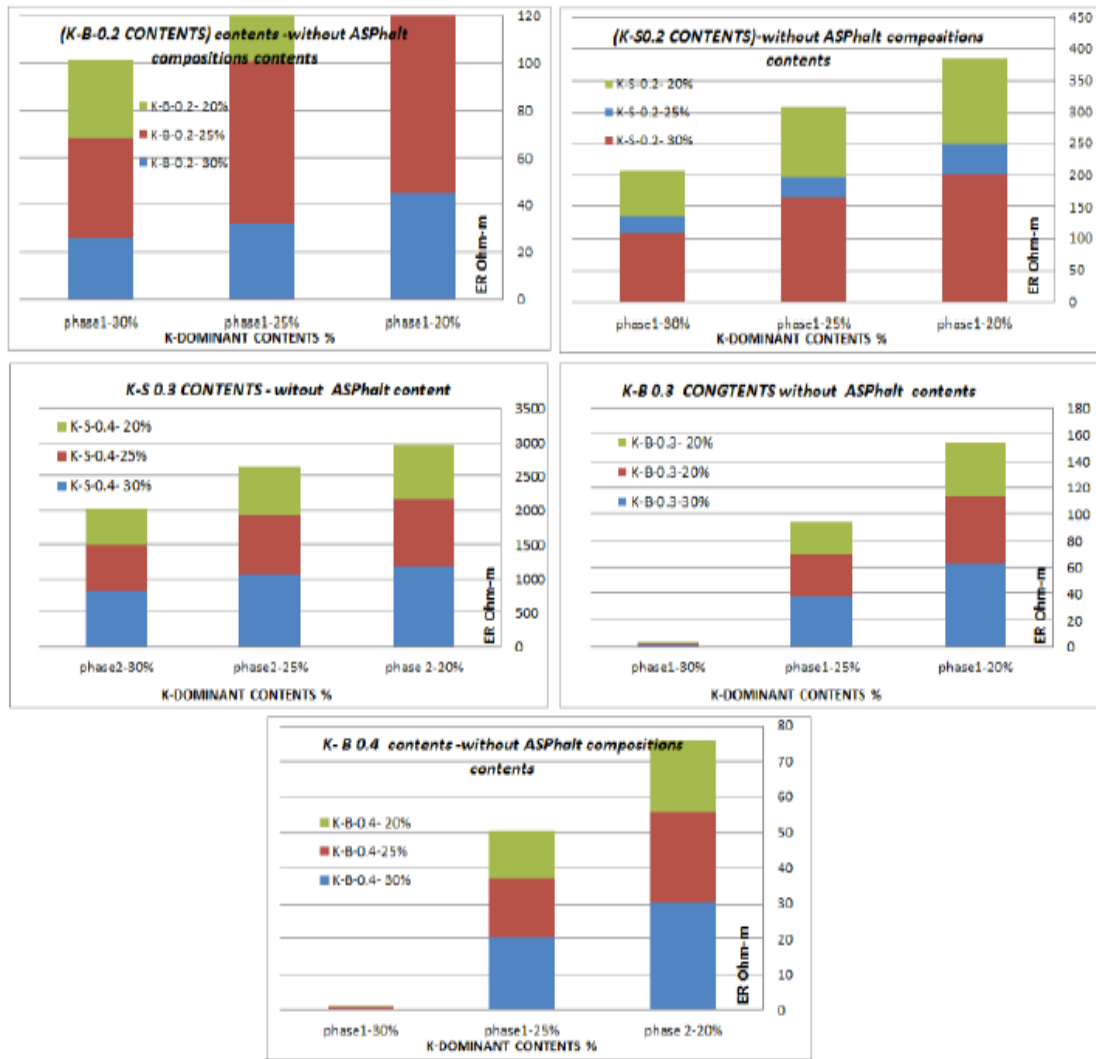


Fig 5. Effect of clay mixtures K-dominants without the contents of asphalt in phase 1&2. On the IDT strength of K-dominants

3.4. Result of Mixing asphalt concrete with clay mixtures *On the IDT strength*

The ease of mixing following the increase in the content ratio to 0.4KB compared to the preparation of samples consisting of a clay mixture of is up to 30%. At the same time, the mixing used in samples of KB 0.4 –ASP 0.25 and KB 0.4 –ASP 0.30 is more accessible compared to the mixing process in samples KS 0.4 –ASP 0.25 and KS 0.4 –ASP 0.30, and samples that are with 30%, 25% and 20% for clay mixtures, as shown in Figures 5 and 6. The mastic becomes thicker and viscous at the limits of certain concentrations, which results from the use of clay mixtures with contents (Kaolin 0.60-Bentonite 0.4) within the content of 20% of the mud mixture relative to the mastic. Which confirm that the IDT values for mechanical testing are in ER values for slurry mixtures, as shown in Figure 5 and 6.

3.5. Results and discussion

Study and control of conductivity effect are greater in samples KB0.2, KB0.3, KB0.4, Kaolin-sand 0.2 (KS 0.2), and Kaolin-sand 0.4 (KS 0.4) for contents of 30, 25 and 20% relative to the mastic of phase 1 & phase 2, as shown in Figure 6. The probability of viscous property is greater with increasing concentration of contents, but this probability is less likely to find an obstacle in mixing observed during high concentration load, where the synthetic pattern KB0.3, KB0.4 is produced as an aqueous mixture that is easier to diffuse than KS0. 1, KS0. 2, Kaolin-bentonite 0.1 (KB 0.1), Kaolin-bentonite 0.2 (KB 0.2) as different contents. By contrast, it is difficult to mix all kinds of ingredients with the clay mixture mentioned above the proportion of 30%. Consider the determination of the layer quality of the thin-clay mineral-liner mixture that exemplifies the non-impacting density of that lining, which causes some damage to the concrete asphalt with the length of time through geophysical tests and the cumulative mechanical properties of both the asphalt concrete and the selected clay

mix. Therefore, the different types of clay mixture have been selected to investigate their effect on conductivity control.

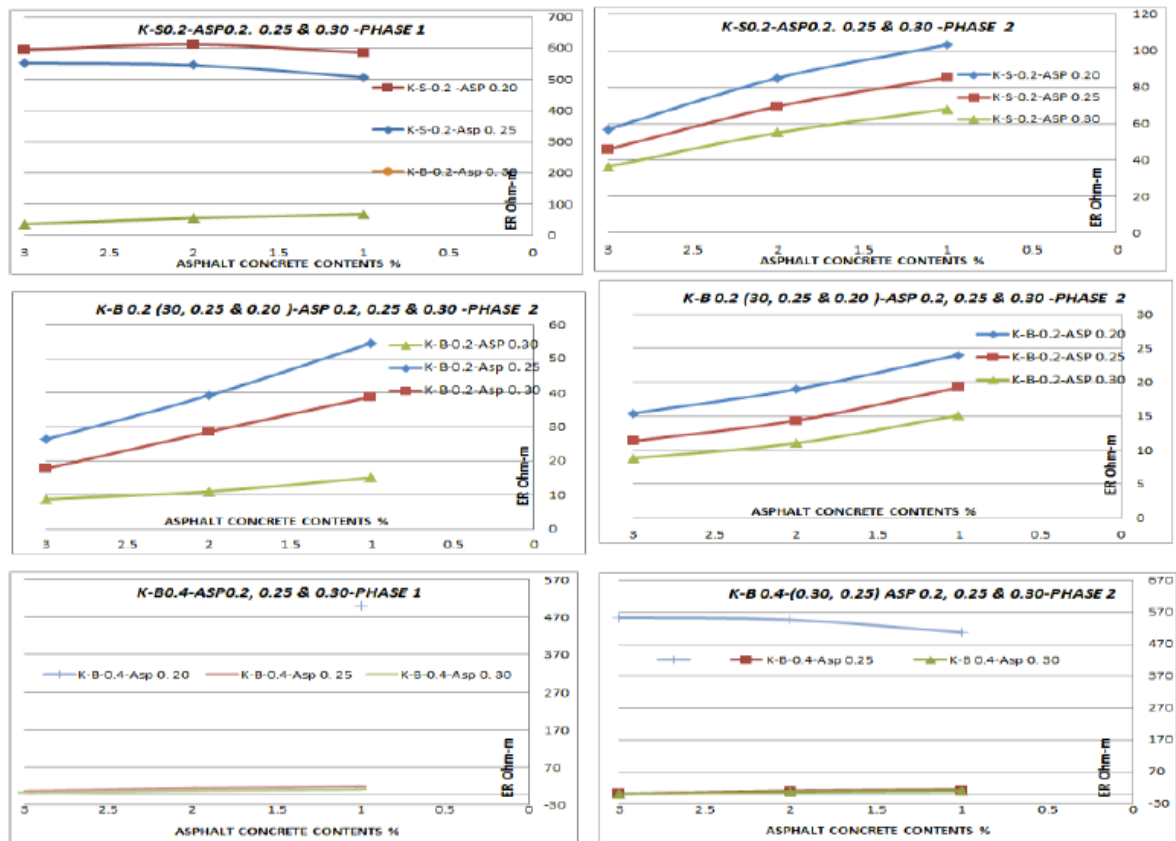


Figure 6. Effect of K-dominants (Asphalt 0.2) on the strength of IDT of asphalt concrete on ER.

Conclusion

The purpose of this study is to minimize damage resulting from defects in asphalt concrete with high ER values, taking into account the variable densities that result from the mixing of these different materials can be avoided by providing a specific technology to reduce moisture. Its increase causes negative damage to the mixture, using balanced additions of the dominant kaolin mixture with the asphalt and cumulative binder.

In this work, kaolin-Sand and kaolin-bentonite particles are incorporated into the natural matrix, where the films are made from a mixture of clay with it to simulate environmental conditions. The effect of Kaolin 0.6-B 0.4(K 0.60-b 0.4) from phase1 and phase 2 on the determination of EC in asphalt concrete is studied in this study. The ER value of the asphalt mastics significantly differs with the clay mixture types and contents; Major conclusions of the study are listed as follows:

The presence of types of clay mixed with mineral clay in such as 0.4 KB in the form of chips prepared to improve conductivity in asphalt mixtures avoids damage to a longer extent;

- Difficulties are observed in mixing the types and contents of a high-volume clay mixture from a surface with the large particles size (K 0.90 to 0.60 -S 0.1 to 0.4).

Mix sheets with a content (K0.60-B0.4) of 20% to 30% preferred over asphalt concrete mixtures ranging from 80% to 70%, together to improve the strength of IDT, so the conductivity improves over time. And the proper EC value profiles are shown with the mechanical performance of the clay mixture (K 0.60-b 0.4) in the second phase. With the best gradual reduction and access to the delivery point, it can be used to extend the life and environmental sustainability, as well as for specific construction purposes, and multi-functional applications.

- The use of clay mixtures K 0.60-b 0.4 (20% and 30%) conforms to the standards for the design of the selected asphalt concrete, or Portland 7 mixtures identified by their particles and distributed with the maximum weight of the moist unit in the moisture part of the mixture. It is necessary to use the curve for ER values continuously, which is the key to gradual softening, from which the strength of the fibres are known, whether

to obtain sustainable and intermediate compounds with the Wilhelm Steinmann et al. (2016). Any future defects intended for use in special biking trails, or parking with concrete asphalt that deals with geophysical mineral materials derived from nature, can be avoided.

Conflicts of Interest

The author declares that they have no conflicts of interest.

References

- [1] Wu, S., Mo, L., and Shui, Z., "Piezoresistivity of graphite modified asphalt-based composites." *Key Engineering Materials*, 249, 391-396, 2003.
- [2] Minsk LD, Electrically conductive asphalt for control of snow and ice accumulation. *Highway Research Record*, 1968.
- [3] Xiangyang, W. and Yuxing, G., "Research on the preparation of conductive asphalt concrete for deicing and snow melting." *Proceedings of 3rd International Conference on Advanced Computer Theory and Engineering*, 381-384, 2010.
- [4] Aishwarya Baranikumar, imparting EC into asphalt composite using graphite, Texas A&M University. August 2016.
- [5] Huang BS, Cao JY, Chen XW, et al., Laboratory investigation into electrically conductive HMA mixtures. *Journal of the Association of Asphalt Paving Technologists* 75:1235–1253, 2006.
- [6] ASTM., "Standard specification for performance graded asphalt binder." ASTM D6373-07, West Conshohocken, PA, 2007a.
- [7] EHC 231, Home Page: www.inchem.org, accessed July 9, 2007, pp. 12 and 15, 2005.
- [8] Park, P., "Characteristics and Application of High-Performance Fiber, 2012.
- [9] L.M. Sherman.: Nanocomposites, *Plastic Technology*, Online Article, Home Page: www.ptonline.com/articles/05fa.html, pp. 1–2, 2007.
- [10] US FDA, Code of Federal Regulations. Title 1. Food and Drugs. Part 84. Direct food substances affirmed as generally recognized as safe (GRAS). Washington, DC, US Department of Health and Human Services, Food and Drug Administration, 2004.
- [11] Alexandr V. Agafonov, Andrew V. Noskov, Effect of the bentonite filler on structure and properties of composites based on hydroxyethyl cellulose, July 2015.
- [12] Montmorillonite, Home Page: www.en.wikipedia.org, accessed, Olga V. Alekseeva, Anna N. Rodionova, Nadezhda A. Bagrovskaya, July 9, 2007.
- [13] Faheem Uddin, Clays, Nanoclays and Montmorillonite Minerals Article in *Metallurgical and Materials Transactions A* · Balochistan University of Information Technology, Engineering and Management Sciences, 2008.
- [14] Gleason, M. H., Daniel, D. E., and Eykholt, G. R., "Calcium and sodium bentonite for hydraulic containment applications." *J. Geotech. Geoenviron. Eng.* 1997.
- [15] Q.A.N. Al Rashid, Abo El-Naga, H., Leong, C., Lu, Y. & Al Abadi, H.; Experimental-artificial intelligence approach for characterizing electrical ER of partially saturated clay liners. *Applied Clay Science*. Latrobe university, 2018.
- [16] ASTM., "Standard test method for theoretical maximum specific gravity and density of bituminous paving mixtures." ASTM D2041-03, West Conshohocken, PA, 2003.
- [17] ASTM., "Standard Specification for hot-mixed, hot-laid bituminous paving mixtures." ASTM D3515-01, West Conshohocken, PA, 2001.
- [18] AASHTO., "Standard specification for Superpave Volumetric Mix Design." AASHTO Designation: M 323-12, 2001.
- [19] ASTM., "Standard test method for percent air voids in compacted dense and open bituminous paving mixtures." ASTM D3203-05, West Conshohocken, PA, 2005.

- [20] Fuller, W. B., & Thompson, S. E., The laws of proportioning concrete. *Journal of Transportation Engineering-ASCE*, 59, 67–143, 1907.
- [21] ASTM., “Standard test method for bulk specific gravity and density of compacted bituminous mixtures using coated samples.” ASTM D1188-07, West Conshohocken, PA, 2007b.
- [22] ASTM., “Standard test method for indirect tensile (IDT) strength of bituminous mixtures.” ASTM D6931-07, West Conshohocken, PA, 2007c.
- [23] Wulfhorst B, Gries T, Veit D, *Textile technology*. Hanser, Munich, 2006.
- [24] DIN EN ISO Textilien—Fasern—Bestimmung der Feinheit- Gravimetrisches Verfahren und Schwingungsverfahren, 1973: 1995–12.
- [25] Chung, D.D.L. and Wang, S., “Self-Sensing of Damage and Strain in Carbon Fiber Polymer-Matrix Structural Composites by Electrical Resistance Measurement,” *Polym. & Polym. Compos*, 2003.
- [26] Wen, S. and Chung, D. D. L., “Electrical resistance-based damage self-sensing in carbon fiber-reinforced cement.” *Carbon*, 45(4), 710-716, 2007.

إدخال التوصيلية الكهربائية في مركب الأسفلت باستخدام طين الخلطة المهيمنة بالكاولين

امير جاسم الشمري قيس عبد الجبار ناجي الراشد

قسم الهندسة المدنية، جامعة بابل، بابل، العراق

kezalr63@gmail.com

ameeralshammari@gmail.com

الخلاصة

تمتلك مخاليط الإسفلت إمكانات كبيرة كموصلات كهربائية للعديد من الوظائف في مجال الاستشعار الذاتي والاستشفاء وجمع الطاقة. تتحكم التوصيلية الكهربائية (EC) في صب الخرسانة الإسفلتية إلى مرحلة ذات أولوية لمثل هذه العروض المقدمة، مع مراعاة بعض الإضافات التي تقلل من تلف المواد الأساسية مع مرور الوقت. تستخدم اختبارات الموصلية الليفية سابقاً في توصيل خليط الإسفلت. هناك الآن حاجة للتخفيف بسبب التغيير المفاجئ في منحنى ER المقاومة الكهربائية لظروف الترشيح للمخاليط الإسفلتية، مع مراعاة الانتقال المفاجئ من قيم المقاومة الكهربائية (ER) إلى مرحلة التوصيل الكهربائي (EC). يعتبر وجود الخلائط الطينية الفعالة لتخفيف عيوب التغيرات المفاجئة صديقة للبيئة. لذلك، تبحث هذه الدراسة عن ناتج حيث كفاءة التغليف المستخدمة عن طريق توجيه التوصيل الكهربائي (EC) من الخرسانة الإسفلتية فقط عن طريق إضافة محتوى معين من محتوى البنتونيت في خليط الكاولين المهيمن بين الكولين-البنتونايت 0.4 إلى الكولين-البنتونايت 0.1 (KB0.1) إلى و 0.4 إلى (الكولين-البنتونايت) الكولين-البنتونايت 0.1 التي تتميز بخصائص جيوفيزيائية مختلفة ومعلمة 0.4 إلى (الكولين-البنتونايت) الكولين-البنتونايت 0.1) لذلك، فإن ثمانية أنواع المختبرة والمختلفة من خليط الطين جيوتقنية مختلفة. يتم تقييم قيم ER بواسطة عينات مختلطة من الأسفلت التي تحتوي على محتويات مختلفة من خليط الطين المهيمن..

الكلمات الدالة: مخاليط الأسفلت، المقاومة الكهربائية، مخاليط الطين المهيمنة (للكاولين)، الأسفلت الصمغي، الأسفلت الكونكريتي، التوصيل الكهربائي، الموصلية الكهربائية.