

1	A preliminary investigation of anaerobically digested municipal sludge cake and
2	contaminated soil for recycling by pyrolysis.
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10	Abstract
11	This work has investigated the potential of pyrolysis as a recycling solution for two largely
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uncharacterised waste streams, anaerobically digested (AD) municipal sludge cake and 12 13 brownfield soil (contaminated with oily sludge). Characterisation of emitted organic 14 compounds from pyrolysis were captured in a solvent (acetone) scrubber and analysed by 15 GC-MS. Both AD sludge cake and brownfield soil showed considerable promise for 'green-er' 16 fuels, as a source of syngas (with CO supplementation) and volatile aromatics essential for 17 fuel quality. However, these waste streams also generated significant amounts of additional highly toxic pollutants of varying chemistries, further emphasising the importance of using a 18 trapping approach applicable to a broader range of chemicals. Pleasingly the acetone trap 19 20 showed very good efficacy in capturing this breadth of chemistries, supporting its use as an alternative capture and preparative method, for monitoring volatile and semi-volatile organic 21 22 tars 23

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29	Keywords
30	Scrubber
31	Pyrolysis/gasification contaminants
32	Tar analysis
33	Gas chromatography-thermal conductivity detection (GC-TCD)
34	Gas chromatography-mass spectrometry (GC-MS)
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#### 57 **1. Introduction**

58 Thermal conversion techniques, such as pyrolysis and gasification, can be used to generate value-added products from organic waste. During pyrolysis carbon-rich feedstocks are heated 59 in anoxic environments between 400-700 °C, causing the organic material to decompose and 60 61 generate products of a higher heating value (e.g. flammable syngas, bio-oils and bio-chars (Brownsort, 2009; Mohan et al., 2006; Ok, 2015)). Meanwhile, gasification involves higher 62 temperatures above >700°C with the addition of controlled mounts of oxidant commonly, 63 64 oxygen or steam. This causes partial combustion of the solid and volatile material, thereby 65 increasing the yield of syngas Syngas is composed of carbon monoxide (CO), hydrogen  $(H_2)$ and methane (CH<sub>4</sub>), and can be used to generate energy by forming liquid fuels using Fischer-66 Tropsch (FT) catalysts (Davis, 2001; Jahangiri et al., 2014; Krylova, 2014). However, syngas 67 can also contain organic pollutants or 'tars' that consist of linear chain hydrocarbons and 68 69 volatile organic compounds (VOCs) such as aromatic, phenolic, and polyaromatic hydrocarbon (PAH) species (Carpenter et al., 2007; Palma, 2013; Ponzio et al., 2006). Despite 70 their importance to the calorific value of syngas for energy generation (Hossain and Davies, 71 2013; Sharma et al., 2012) small VOCs such as benzene, ethylene, and acetylene are 72 73 particularly important to monitor as they can cause chemical contamination and catalyst deactivation at significant monetary cost (Bosmans et al., 2013; Rabou and Drift, 2011). 74 Similarly, the components of bio-oils can provide economic value as an additional feedstock 75 for fuels (Unyaphan et al., 2017; Zhang et al., 2019) however, they can also cause mechanical 76 fouling of equipment if poorly captured. Thus, there remains a need to both capture the 77 resulting pollution by-products and molecularly characterise the recycling approach, using fit-78 for-purpose trapping and measurement processes, prior to the re-use or disposal of 'new' 79 organic waste. Unfortunately, this can come at significant cost, with VOCs often requiring 80 specific sampling methods, using sorbents and modified instrumentation, when gas 81 chromatography-mass spectrometry (GC-MS) analyses are required (Agilent, 2014). 82 Therefore, a cheap(er) pollutant capture method, such as a solvent trap or 'scrubber' using 83 84 methanol, water or isopropanol (Phuphuakrat et al., 2010; Prando et al., 2016), is important

85 for process viability; however, these are often selected specifically to target pollutant classes common to well-characterised feedstocks such as biomass (pine wood), and are mainly 86 87 untested on alternative wastes. Given the drive to recycle more sources of organic waste, 88 current work has shown an increasing need to capture and monitor for a broader range of 89 organic pollutants, from an expanding list of largely uninvestigated feedstocks (e.g. municipal 90 sludge cake and contaminated brownfield soil). Although previous thermal studies on 91 suitability sewage sludge as a feedstock exist (Gomez-Rico et al., 2008; Mohan et al., 2006; 92 Oleszczuk et al., 2014; Rosa et al., 2018; Rulkens, 2008), the literature is lacking particularly 93 with the treatment of AD sludge cake and the analysis of the volatiles organic compounds 94 emitted in the process. AD sludge cake is the remaining solid material from sewage sludge treatment. Sewage sludge is treated firstly, by dewatering and centrifugation to form a solid 95 96 material (19% dry mass) before it is thermally hydrolysed and anaerobically digested (Gavala 97 et al., 2003). The undigested solids from this process is further dewatered to produce anaerobically digested (AD) municipal sludge (Gavala et al., 2003). A recent thermal 98 99 gravimetric study on pine wood and anaerobically digested (AD) municipal sludge cake 100 indicated significant differences in the evolved chemicals of these feedstocks during 101 thermochemical conversion, with primary losses of sample occurring at 200-400 °C for pine wood (63.8 %), and 200-500 °C for AD municipal sludge cake (36.5 %) ((Sullivan et al., 2019)). 102 Although studies on the suitability of sewage sludge as a thermochemical feedstock exist 103 (Gomez-Rico et al., 2008; Mohan et al., 2006; Oleszczuk et al., 2014; Rosa et al., 2018; 104 Rulkens, 2008), there is little published literature concerning AD sludge cake and the 105 pollutants emitted during thermochemical conversion. Similarly, whilst research on brownfield 106 soil contaminated with coal tar has shown harmful persistent organic pollutants following 107 pyrolysis (e.g. volatile aromatics, furans and polyaromatic hydrocarbons) (Lara-gonzalo et al., 108 109 2015); (Abdel-Shafy and Mansour, 2016) there is again limited work in characterising oil-110 contaminated brownfield soil for land remediation. Therefore, to investigate the breadth of 111 pollutants anticipated from the thermochemical recycling of these more complex waste 112 materials, acetone was tested as a low cost scrubber, that offers compatibility with a standard

GC-MS set-up (Maštovská and Lehotay, 2004), and a wider dissolution range for alternative pollutants. For pollutant capture, the scrubber was initially tested using relevant volatile and semi-volatile standards, followed by application to the thermochemical recycling of these waste materials; to understand the limitations and benefits of the thermochemical processing of these feedstocks, further characterisation in terms of nitrogen content and calorific value was also carried out.

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### 120 2. Materials and methods

### 121 2.1. Standard reference materials

Acetone, methanol, 70% nitric acid (all ACS grade), pentane (GC grade), and 122 triphenylethylene (internal standard, IS) were purchased from Sigma Aldrich (Suffolk, UK). 123 The standard solutions for creating the calibration graph (QTM PAH mixture 1 and EPA 8040a 124 phenol calibration mixture) were obtained from Supelco (Suffolk, UK), while those used for 125 quality control (QC) samples (aromatic mixture 1 (PAHs), phenol mixture 1 and 2 8040a, 126 volatile aromatic mixture (CLP Volatile mega mix<sup>™</sup>) and naphthalene-d<sub>8</sub> (IS) were sourced 127 128 from Restek (Wycombe, UK). For GC-MS and gas chromatography-thermal conductivity 129 detection (GC-TCD), ultra-pure helium and argon gases were purchased from Air Products (Swansea, UK), while high purity nitrogen for pyrolysis was acquired from BOC (Port Talbot, 130 UK). To test the scrubbers with complex samples, pine wood (purchased from Waters and 131 132 Morris in Ammanford, UK), AD municipal sludge cake (sourced from wastewater treatment plants in South Wales, UK and Accra, Ghana), and soil (10 % contamination with 133 petrochemical waste from a field site in Rumney, UK) were pyrolysed for syngas production. 134

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### 136 2.2. <u>Standard (stock) solutions</u>

A 10 mg/L VOC and equivalent QC stock solution (for quantitation) were prepared by spiking
the volatile aromatic mixture and a separate batch of CLP Volatile mega mix<sup>™</sup>, respectively
in acetone. Similarly, 10 mg/L calibration stock solution for SVOCs were prepared using the

QTM PAH mixture 1 or EPA 8040a phenol solution along with an appropriate 10 mg/L QC
stock solution for quantitation (see standard reference materials section). The IS solutions
were also prepared in acetone as a 100 mg/L mixture of triphenylethylene and naphthalened<sub>8</sub>.

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#### 145 2.3. Instrumentation

Analyses of volatile single-ring aromatics, phenols and polyaromatic hydrocarbons (PAH) 146 147 were undertaken using a Trace 1300 and ISQ GC-MS system, operating with Tracefinder Xcalibur™ software and a TG-5MS column (30 m x 0.25 mm, 0.25 µm) (Thermo Scientific, 148 Hemel Hempstead, UK). Due to poor column retention and difficulties in differentiating from 149 low mass fragment ions, simple combustion gases, such as CO,  $H_2$  and CH<sub>4</sub>, were measured 150 using a Varian micro GC-TCD (Palo Alto, USA). This was operated with two columns using 151 an argon carrier gas; an 8 m 100 % dimethyl-polysiloxane (CP-SIL 5CB) column (channel 1) 152 to separate small organics (C3-C6) and a 10 m aluminosilicate molecular sieve column 153 (Molsieve MSA BF, Varian, Palo Alto, USA) (channel 2) for simple gases (e.g. CO, H<sub>2</sub>, CH<sub>4</sub>). 154 To generate the syngas, a pyrolysis rig (based on a commercial design) were fabricated in-155 house; the latter consisted of a stainless steel (SS) tube (4.7 cm<sup>2</sup> x 70 cm) with a sample 156 stage, a removable end cap to introduce the feedstock, an inlet valve for nitrogen, and an exit 157 158 port for syngas that was connected to (1) an in-line scrubber system (containing acetone) and, 159 (2) the GC-TCD system for real-time simple gas monitoring. The sample stage was located at 160 the hottest part of the rig, with operating temperatures monitored here and at the end cap using two thermocouples. The rig was also fitted with a pressure sensor and a gas safety 161 dump valve in case of emergencies. The scrubber system comprised of three glass impingers 162 163 (max capacity of 250 mL), connected by a short length (~7-10 cm) of inert high temperature PTFE tubing; this was maintained at 20 °C by air recirculation to minimise evaporation of the 164 scrubber solvent, with the PTFE exit-line of the rig to the first impinger fitted at a longer length 165

166 (~50 cm) to ensure gas cooling (please see the graphical abstract for a simplified schematic167 of the rig).

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#### 169 2.4. <u>Analysis of volatile and semi-volatile organic pollutants</u>

170 Two GC-MS methods were used based on analyte volatility, with each optimised for the relevant compound suites using a 2.5 µL split-less injection, operating at an inlet temperature 171 of 300 °C. For VOCs, an oven temperature programme of 40-150 °C at 15 °C/minute (held for 172 173 one minute), and 150-300 °C at 25 °C/minute was used, with the transfer line and ion source temperature set at 300 °C and 250 °C, respectively. Whilst for SVOCs alternative conditions 174 to accommodate changes in volatility were applied; an oven temperature programme of 40-175 250 °C at 20 °C/minute, held for five minutes, 250-300 °C at 20 °C/minute, and, the transfer 176 line and ion source temperatures of 300 °C and 310 °C, respectively. Data was acquired under 177 full scan and single ion monitoring (SIM) conditions for the relevant analytes, with the latter 178 operated as a segmented approach (see Supplementary for details). Compounds within the 179 scrubbers were identified using the NIST 2.0 database, with reverse and forward match scores 180 181 >800 (Vladimir and Sparkman, 2008), and quantified using the nearest eluting IS.

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#### 183 2.5. Validation of GC-MS Method for VOCs and SVOCs.

184 Prior to application, the method was validated for limit of detection (LOD), accuracy, precision, 185 lower level of quantitation (LLOQ) and upper limit of quantitation (ULOQ), using two batches of samples run over separate days. To create and assess the calibration curve each batch 186 187 contained a set of calibration standards (250-2000 µg/L and 50-1500 µg/L for SVOC and VOCs, respectively), five blanks, and five analytical quality controls (AQCs) spiked at 500 µg/L 188 for VOCs and 1500 µg/L for SVOCs. The LOD for the GC-MS methods was initially calculated 189 using 3x the standard deviation of the blank signal; however, this can often be misleading with 190 191 discrepancies from the manual integration of the signal. Therefore, to confirm the LOD, the lowest standard with a signal to noise ratio (S/N) >3 was also used. To determine the LLOQ 192

and ULOQ, additional AQCs were analysed at low (50  $\mu$ g/L for VOCs and 250  $\mu$ g/L SVOCs) and high concentrations (1000  $\mu$ g/L for VOCs and 1500  $\mu$ g/L for SVOCs), respectively, whereby the LLOQ was confirmed as the concentration below or near the lowest standard with acceptable accuracy and precision (see Equations 1 and 2). The acceptance criteria used for method validation was based on a UKAS approved standard operating procedure (ISO, 2006), which required an accuracy and precision of ≤20 % for the AQCs at the specified concentration.

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 $Accuracy (\%) = \frac{(Mean \ determined \ QC \ concentration - true \ QC \ concentration)}{true \ QC \ concentration} \ X100$ 

Equation 1

203Precision (%) =  $\frac{standard \ deviation \ of \ determined \ QC \ concentration}{Mean \ determined \ QC \ concentration} X \ 100$ 205Equation 2

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## 207 2.6. Pyrolysis of organic feedstock

Pine wood, AD municipal sludge cake (both 10 g), and contaminated soil (20 g to ensure 208 sufficient amounts of VOC and SVOCs) were sieved to <2 mm and heated to >700 °C at 20 209 °C/minute under nitrogen, in the laboratory-scale test system to mimic slow pyrolysis. Given 210 the greater anticipated variability of tar content from the raw feedstocks, the scrubber system 211 212 comprised of a series of three impingers and each contained a 150 mL of solvent (chosen 213 from the scrubber evaluation). To assess the usefulness of the target feedstock, the calorific value (CV) of the material and the producer gas was also determined using a bomb calorimeter 214 (ISO 1928, "Solid mineral fuels - Determination of gross calorific value by the bomb 215 216 calorimetric method; and calculation of net calorific value," 2009) and by the molar fraction results from the GC-TCD analysis, respectively. 217

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## 220 3. Results and discussion

#### 3.1. <u>Method validation</u>

222 All of the analytes within the VOC methods showed acceptable signal at 1  $\mu$ g/L for the LOD and, acceptable precision and accuracy for quantifying over the tested concentration range 223 224 (including ULOQ), with 4.08-18.36 % relative standard deviation (%RSD) and -18.6-5.53 %accuracy (see Table 1). As expected, higher LOD values were observed for the less volatile 225 226 SVOCs (phenol and PAH standards) but this method also showed acceptable precision and 227 accuracy for the tested calibration range, with values between 3.24-15.93 %RSD and -9.27-228 19.81 % accuracy, respectively (Table 1). Given both protocols met the acceptance criteria for 229 validation these were then applied for characterising and quantifying compounds observed in 230 the scrubbers following pyrolysis of the waste samples.

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## 232 3.2. Characterisation of AD sludge cake and brownfield soil during pyrolytic waste recycling.

Prior to application, the scrubbers and feedstocks were subjected to a programme of 233 234 preliminary tests to understand limitations in their performance and suitability for recycling. 235 Firstly, the capacity of the acetone scrubber to capture organic pollution was determined by measuring the 'bleed' of organic compounds between the series of scrubbers; this showed 236 that a typical saturation range for acetone at 20 °C was equivalent to 125-200 g/L of pyrolysed 237 238 feedstock, and a series of 3x150 mL scrubbers would be sufficient to capture detectable 239 organic pollution generated from 10-20 g of feedstock. However, during this work it was noted 240 that scrubber performance was volume dependent, with a potential loss of performance due to scrubber evaporation by the syngas. This was therefore tested repeatedly over a 30-40 241 minute process time to mimic the operation of the rig; pleasingly, despite some evaporative 242 243 loss of the scrubber adjacent to the syngas line, this did not exceed 10 %, indicating a sufficient level of syngas cooling prior to the scrubber system. The largely un-investigated AD municipal 244 sludge cake and contaminated soil samples were also characterised to understand their 245 usability for recycling; measurements of inorganic composition, syngas production, CV and tar 246

247 content were taken as these are thought to differ with feedstock chemistry (and production method) (Chang et al., 2000; Palma, 2013; Tian et al., 2014; Werner et al., 2014). Interestingly, 248 despite the common manufacturing method, the pre-pyrolysed Ghanaian AD sludge cake 249 contained a greater amount of nitrogen (3.5 mg/Kg) and SVOCs (3500 mg/Kg) than that from 250 251 the UK (2.5 mg/Kg and 230 mg/Kg, respectively), with the former generating more than double the amount of harmful nitrogen-containing aromatics following pyrolysis (e.g. to 188.2 mg/L, 252 253 see Table 2). To the best of the authors' knowledge, this disparity of AD sludge cake 254 composition between common production processes has been largely underreported in the 255 literature and highlights the importance of feedstock (and tar) characterisation. Similarly, this 256 finding also supports the use of a syngas clean-up that covers a broader range of pollutants, to minimise the exposure to harmful emissions prior to release/use. To understand the 257 usefulness of recycling the (waste) feedstocks as an energy source, the syngas composition 258 259 and CV were also established; the results again were significant, as they highlighted differences in syngas production, a variation in organic waste composition and the importance 260 261 of material characterisation. Unlike brownfield soil, the syngas generated from AD sludge cake showed significant potential for thermochemical recycling, with competitive gas ratios to pine 262 263 wood; therefore, with CO supplementation, this remains a promising route for 'green' fuel production due to the significant CV (~25-33%) and lower levels of greenhouse gas (CH<sub>4</sub>) 264 produced. 265

To provide data indicative of the final process, pine wood (as a well characterised 266 sample), AD sludge cake and brownfield soil were therefore pyrolysed using the SS rig at 267 >700 °C and an acetone scrubber. Despite the higher operating temperature of the process 268 (and lower boiling point of acetone) minimal latent heating and evaporation of the scrubber 269 was observed, indicating the continued capture of pollutants by solvation. As expected, the 270 271 pyrolysis of pine wood showed significant amounts of typical breakdown products and minor 272 constituents of biomass such as furan derivatives and phenols (Brebu and Vasile, 2010; Kibet et al., 2012), and terpenoid compounds, respectively. However, the use of acetone also 273 274 proved very beneficial in terms of monitoring the volatile emission during the recycling of AD

275 sludge cake as it showed significant capture of highly toxic nitrogen-containing heterocyclic aromatics (see Table 3). In addition to these pollutants, acetone also captured significant 276 levels of volatile aromatics desired for fuel production; pleasingly, sludge cake showed 277 significant promise in generating these 'BTEX' compounds (e.g. benzene, toluene, ethyl 278 279 benzene and xylene), with similar levels of observed to pine wood, further supporting the use of pyrolysis as a viable and valuable recycling solution. Similarly, pyrolysis of oil contaminated 280 brownfield soil showed significant amounts of single ring aromatic and polyaromatic 281 hydrocarbons (indicative of the oil content) with very high amounts of benzene and 282 283 naphthalene captured in the initial scrubber (see Table 4). Interestingly, the compound profile 284 observed in the scrubbers post-pyrolysis appear to be the same observed in a prior 285 characterisation study of the pre-pyrolysed material (raw feedstock). This data is important as 286 it shows a potential for soil remediation following contamination. Analysis of the post-pyrolysed 287 soil (vial solvent extractions) showed a decrease of 80.5% of oily sludge contaminant in the remaining sample. This data is important as it shows potential for contaminated soil 288 289 remediation and for recycling this feedstock to generate a source of fuel given the high calorific 290 value (>30 MJ/kg) of these compounds.

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## 3.3. The recycling of contaminated acetone scrubbers

293 In the interest of meeting the needs of a Circular Economy the remediation of contaminated 294 acetone for less volatile species was also explored; this was achieved by comparing levels of 295 VOCs and SVOCs before and after evaporating (and re-condensing) using a distillation apparatus, at a temperature representing heat that may be sequestered from pyrolysis through 296 297 simple heat exchange (e.g. 60 °C). However, given this temperature was significantly lower 298 than that of pyrolysis (700 °C), it was anticipated that the remediation of the more volatile BTEX components may be limited due to condensation within the acetone extract. Pleasingly 299 a colourless liquid was generated following 'scrubber recycling' and most promisingly, SVOCs 300 were undetectable within the scrubber, with some less volatile BTEX compounds 301

(ethylbenzene, p-xylene and styrene) showing a significant reduction in levels of 67 %, 65.4
%, 82.4 %, respectively (see Supplementary for details). This pilot data therefore, highlights
the potential of acetone as a 'recyclable' capture method for pollution generated via
thermochemical conversion of different feedstocks, aligned with the principles of a Circular
Economy.

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### 308 4. Conclusion

309 Analyte capture using an acetone scrubber and analysis via direct injection GC-MS provides a simple and effective approach for monitoring and facilitating the recycling of organic waste. 310 The greater solubility range of acetone has enabled the measurement of a wider breadth of 311 organic pollutants, essential for de-risking the recycling of 'newer' organic feedstocks such as 312 oil-contaminated brownfield soil and AD municipal sludge cake. This work has also shown 313 differences in pollutants generated from materials that have been produced using the same 314 treatment processes, highlighting the importance of material characterisation prior to 315 316 release/re-use of the resulting thermochemical products.

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#### 321 **Declarations of interest**

322 None.

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#### 324 **References**

- Abdel-Shafy, H.I., Mansour, M.S.M., 2016. A review on polycyclic aromatic hydrocarbons:
- 326 Source, environmental impact, effect on human health and remediation. Egypt. J. Pet.
- 327 25, 107–123. https://doi.org/10.1016/j.ejpe.2015.03.011
- Agilent, 2014. Fundamentals. Agil. Present. 42, 2555–2568.

- 329 https://doi.org/10.1515/9783110289169
- Bosmans, A., Wasan, S., Helsen, L., 2013. Waste-to-clean syngas: avoiding tar problems.
  Status Accept. 1–21. https://doi.org/10.5772/54528
- Brebu, M., Vasile, C., 2010. Thermal degradation of lignin—a review. Cellul. Chem. Technol.
  44, 353–363.
- Brownsort, P.A., 2009. Biomass Pyrolysis Processes: Review of Scope, Control and
- 335 Variability. Biomass 38. https://doi.org/10.1017/CBO9781107415324.004
- 336 Carpenter, D.L., Deutch, S.P., French, R.J., 2007. Quantitative measurement of biomass
- 337 gasifier tars using a molecular-beam mass spectrometer: Comparison with traditional
- impinger sampling. Energy and Fuels 21, 3036–3043.
- 339 https://doi.org/10.1021/ef070193c
- Chang, C.Y., Shie, J.L., Lin, J.P., Wu, C.H., Lee, D.J., Chang, C.F., 2000. Major Products
- 341 Obtained from the Pyrolysis of Oil Sludge. Energy and Fuels 14, 1176–1183.
- 342 https://doi.org/10.1021/ef0000532
- 343 Davis, B.H., 2001. Fischer-Tropsch synthesis: Current mechanism and futuristic needs. Fuel
- 344 Process. Technol. 71, 157–166. https://doi.org/10.1016/S0378-3820(01)00144-8
- Gavala, H.N., Yenal, U., Skiadas, I. V., Westermann, P., Ahring, B.K., 2003. Mesophilic and
- 346 thermophilic anaerobic digestion of primary and secondary sludge. Effect of pre-
- treatment at elevated temperature. Water Res. 37, 4561–4572.
- 348 https://doi.org/10.1016/S0043-1354(03)00401-9
- 349 Gomez-Rico, M.F., Fullana, A., Font, R., 2008. Volatile organic compounds released from
- thermal drying of sewage sludge. WIT Trans. Ecol. Environ. 111, 425–433.
- 351 https://doi.org/10.2495/WP080411
- Hossain, A.K., Davies, P.A., 2013. Pyrolysis liquids and gases as alternative fuels in internal
- combustion engines A review. Renew. Sustain. Energy Rev. 21, 165–189.
- 354 https://doi.org/10.1016/j.rser.2012.12.031
- ISO, 2006. ISO 17025. General requirements for the competence of testing and calibration
- laboratories. Technical corrigendum 1 1–55.

- 357 ISO 1928, "Solid mineral fuels Determination of gross calorific value by the bomb
- 358 calorimetric method; and calculation of net calorific value," 2009.
- Jahangiri, H., Bennett, J., Mahjoubi, P., Wilson, K., Gu, S., 2014. A review of advanced
- 360 catalyst development for Fischer–Tropsch synthesis of hydrocarbons from biomass
- derived syn-gas. Catal. Sci. Technol. 4, 2210–2229.
- 362 https://doi.org/10.1039/C4CY00327F
- 363 Kibet, J., Khachatryan, L., Dellinger, B., 2012. Molecular products and radicals from
- 364 pyrolysis of lignin. Environ. Sci. Technol. 46, 12994–13001.
- 365 https://doi.org/10.1021/es302942c
- 366 Krylova, A.Y., 2014. Products of the Fischer-Tropsch synthesis (A Review). Solid Fuel
- 367 Chem. 48, 22–35. https://doi.org/10.3103/S0361521914010030
- Lara-gonzalo, A., Kruge, M.A., Lores, I., Gutiérrez, B., Gallego, J.R., 2015. Organic
- 369 Geochemistry Pyrolysis GC MS for the rapid environmental forensic screening of
- 370 contaminated brownfield soil. Org. Geochem. 87, 9–20.
- 371 https://doi.org/10.1016/j.orggeochem.2015.06.012
- 372 Maštovská, K., Lehotay, S.J., 2004. Evaluation of common organic solvents for gas
- 373 chromatographic analysis and stability of multiclass pesticide residues. J. Chromatogr.
- A 1040, 259–272. https://doi.org/10.1016/j.chroma.2004.04.017
- Mohan, D., Pittman, C.U., Steele, P.H., 2006. Pyrolysis of wood/biomass for bio-oil: A critical
- 376 review. Energy and Fuels 20, 848–889. https://doi.org/10.1021/ef0502397
- 377 Ok, Y., 2015. Biochar: production, characterisation and application. CRC press.
- 378 Oleszczuk, P., Zielińska, A., Cornelissen, G., 2014. Stabilization of sewage sludge by
- 379 different biochars towards reducing freely dissolved polycyclic aromatic hydrocarbons
- 380 (PAHs) content. Bioresour. Technol. 156, 139–145.
- 381 https://doi.org/10.1016/j.biortech.2014.01.003
- Palma, C.F., 2013. Model for biomass gasification including tar formation and evolution.
- 383 Energy and Fuels 27, 2693–2702. https://doi.org/10.1021/ef4004297
- Phuphuakrat, T., Namioka, T., Yoshikawa, K., 2010. Tar removal from biomass pyrolysis gas

in two-step function of decomposition and adsorption. Appl. Energy 87, 2203–2211.

386 https://doi.org/10.1016/j.apenergy.2009.12.002

- Ponzio, A., Kalisz, S., Blasiak, W., 2006. Effect of operating conditions on tar and gas
- 388 composition in high temperature air/steam gasification (HTAG) of plastic containing
- waste. Fuel Process. Technol. 87, 223–233.
- 390 https://doi.org/10.1016/j.fuproc.2005.08.002
- 391 Prando, D., Shivananda Ail, S., Chiaramonti, D., Baratieri, M., Dasappa, S., 2016.
- 392 Characterisation of the producer gas from an open top gasifier: Assessment of different
- tar analysis approaches. Fuel 181, 566–572. https://doi.org/10.1016/j.fuel.2016.04.104
- Rabou, L.P.L.M., Drift, A. Van Der, 2011. Benzene and ethylene in Bio-SNG production :
- nuisance, fuel or valuable products? Proc. Int. Conf. Polygeneration Strateg. 11 11,
  157–162.
- 397 Rosa, A.P., Chernicharo, C.A.L., Lobato, L.C.S., Silva, R. V., Padilha, R.F., Borges, J.M.,
- 2018. Assessing the potential of renewable energy sources (biogas and sludge) in a
- full-scale UASB-based treatment plant. Renew. Energy 124, 21–26.
- 400 https://doi.org/10.1016/j.renene.2017.09.025
- 401 Rulkens, W., 2008. Sewage sludge as a biomass resource for the production of energy:
- 402 Overview and assessment of the various options. Energy and Fuels 22, 9–15.
- 403 https://doi.org/10.1021/ef700267m
- 404 Sharma, P.K., Kuinkel, H., Shrestha, P., Poudel, S., 2012. Use of Acetylene as an
- 405 Alternative Fuel in IC Engine. Mech. Confab 1, 19–22.
- 406 Sullivan, G.L., Prigmore, R.M., Knight, P., Godfrey, A.R., 2019. Activated carbon biochar
- 407 from municipal waste as a sorptive agent for the removal of polyaromatic hydrocarbons
- 408 (PAHs), phenols and petroleum based compounds in contaminated liquids. J. Environ.
- 409 Manage. 251, 109551. https://doi.org/10.1016/j.jenvman.2019.109551
- 410 Thomas, S., 2008. Enhanced oil recovery-an overview. Oil Gas Sci. Technol. ... 63, 9–19.
- 411 https://doi.org/10.2516/ogst
- Tian, K., Liu, W.J., Qian, T.T., Jiang, H., Yu, H.Q., 2014. Investigation on the evolution of N-

413	containing	organic com	pounds duri	ing pyrolys	is of sewage	e sludge.	Environ. Sci.
	J	J			J	J J	

- 414 Technol. 48, 10888–10896. https://doi.org/10.1021/es5022137
- Unyaphan, S., Tarnpradab, T., Takahashi, F., Yoshikawa, K., 2017. An Investigation of Low
- 416 Cost and Effective Tar Removal Techniques by Venturi Scrubber Producing Syngas
- 417 Microbubbles and Absorbent Regeneration for Biomass Gasification. Energy Procedia
- 418 105, 406–412. https://doi.org/10.1016/j.egypro.2017.03.333
- Vladimir, Z., Sparkman, J., 2008. NIST 2008 User Guide. Natl. Inst. Stand. Technol. NIST 1–
  420 49.
- 421 Werner, K., Pommer, L., Broström, M., 2014. Thermal decomposition of hemicelluloses. J.
- 422 Anal. Appl. Pyrolysis 110, 130–137. https://doi.org/10.1016/j.jaap.2014.08.013
- Zhang, S., Yang, X., Zhang, H., Chu, C., Zheng, K., Ju, M., Liu, L., 2019. Liquefaction of
- 424 biomass and upgrading of bio-oil: A review. Molecules 24, 1–30.
- 425 https://doi.org/10.3390/molecules24122250
- 426
- 427
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## 441 Tables

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Table 1: Summary validation data for VOCs and SVOCs showing linearity (coefficient of determination, R<sup>2</sup>), and precision (%Prec) and accuracy (%Acc) of the LLOQ, AQC and ULOQ. For the LLOQ, AQC and ULOQ, concentrations were spiked at 50 µg/L, 500 µg/L and 1000 µg/L VOC protocol and 250 µg/L, 1500 µg/L and 2000 µg/L for the SVOC method, respectively. All analytes showed acceptable linearity (R<sup>2</sup> ≥0.99), precision and accuracy at each concentration level (<20%).

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Compound	Linearity	LLOQ		AQC		ULOQ	
Compound	R <sup>2</sup>	%Acc	%Prec	%Acc	%Prec	%Acc	%Prec
VOC method							
Benzene	0.9965	3.72	7.61	2.24	12.39	3.18	18.36
Toluene	0.9973	-6.58	16.27	5.53	10.02	1.07	6.01
Ethylbenzene	0.9978	-18.60	4.25	2.89	6.52	3.03	8.43
1,3-dimethylbenzene	0.9984	-18.25	4.08	1.71	6.11	3.54	8.76
P-xylene	0.9983	-15.18	4.52	2.33	6.12	4.09	9.11
Styrene	0.9989	-17.38	4.11	-0.36	7.30	0.47	10.74
1-methy-2-	0 0000	17 70	6 20	2.24	6 75	2 77	7 60
ethylbenzene	0.9969	-17.79	0.30	2.34	0.75	2.11	7.00
1,3-dichlorobenzene	0.9998	-12.66	7.67	0.73	5.90	3.55	8.71
1, 4-dichlorobenzene	0.9998	-11.65	6.95	0.44	5.40	3.70	8.75
1,2-dichlorobenzene	0.9998	-10.61	10.03	1.18	5.89	4.12	8.45
SVOC method							
Napthalene	0.9992	18.00	5.42	-4.70	6.91	0.14	7.78
Acenaphthylene	0.9994	15.03	9.93	-3.26	6.65	0.28	6.38
Acenaphthene	0.9983	12.64	7.58	-3.13	5.66	1.27	6.95
Fluorene	0 9992	14 16	8 52	-3.83	4 50	-0.25	6 71
Phenanthrene	0.9994	15.25	7.46	-3.10	4.35	0.32	5.38
Anthracene	0 9981	19.81	5 58	-5.98	4 94	-2.05	7 69
Fluoranthene	0 9997	8.91	9.81	-3.21	4 59	-1 29	7.06
Pyrene	0 9963	10 11	6 64	-3 48	4 60	-0.74	6.36
Benza(a)anthracene	0.9990	10.98	15.93	-2.15	5.67	-0.73	4.01
Chrvsene	0.9963	16.12	9.09	-1.45	5.17	-0.71	3.95
Benza(b)fluoranthene	0.9913	3.18	14.30	-2.64	6.00	-0.22	4.40
Benzo(a)pyrene	0.9932	16.47	10.19	-2.00	6.35	-0.19	3.93
Indeno(123-cd)pyrene	0.9904	15.65	9.98	-2.63	6.87	-0.24	5.11
Dibenza(ah)anthracene	0.9920	14.25	9.53	-1.87	7.32	0.37	3.98
Benzo (ghi) pervlene	0.9981	11.15	10.42	-2.18	6.46	-1.02	5.27
Phenol	0.9967	12.33	4.62	-1.74	10.32	3.09	10.93
2-chlorophenol	0.9975	11.76	4.97	-3.71	9.12	0.44	9.45
2-methyl phenol	0.9950	15.77	3.24	-1.51	8.31	0.81	9.24
4-methyl phenol	0.9969	12.70	6.45	-2.58	7.73	0.97	9.31
2-nitro phenol	0.9949	7.29	5.40	-2.75	10.86	-0.94	6.85
2,3-dimethyl phenol	0.9982	6.33	6.44	-1.32	8.84	-2.00	6.76
2.5-dichlorophenol	0.9973	13.82	6.08	-2.01	7.66	-0.46	8.23
2,6-dichlorophenol	0.9997	8.21	6.84	-1.62	7.72	0.07	8.39
4-chloro-3-	0.9930	14.44	3.38	-0.77	7.67	1.28	9.71
methylphenol							
2,3,6-trichloro phenol	0.9977	8.60	7.67	-4.18	7.16	-1.70	6.34
2,3,5-trichlorophenol	0.9993	5.01	7.76	4.70	10.17	5.48	9.91
4-nitrophenol	1.000	-9.27	14.74	-2.80	8.58	-2.42	7.20
Pentachlorophenol	0.9871	4.96	14.35	0.75	8.33	1.74	8.27

Table 2: Table listing the compounds identified within the scrubbers from the pyrolysis of anaerobically digested sludge cake from a wastewater treatment plant in Ghana at 700 °C. Some of the compounds have been quantified by targeted analysis while those untargeted species have been elucidated by their mass spectrum and semi-quantified in 1 mL aliquot of scrubber (150 mL acetone) by comparing the peak area to an IS. Atargeted compounds, #non-targeted compounds, ND – none detected.

Anaerobically digested sludge cake (Ghana)	Compound name	conce	Scrubber concentration (mg/L)			
		1	2	3		
Volatile aromatic compounds^	Benzene	8.00	19.47	ND		
	Toluene	22.10	44.18	ND		
	Ethylbenzene	4.91	2.13	ND		
	p-xylene	2.75	0.87	ND		
	Styrene	4.49	0.80	ND		
	1,3-dimethylbenzene	2.95	0.60	ND		
Phenolic compounds^	Phenol	5.20	ND	ND		
	4-methylphenol	2.27	ND	ND		
	2-methylphenol	22.49	ND	ND		
	2,3-dimethylphenol	3.13	ND	ND		
Nitrogen containing compounds	N-isopropyl cyclohexamine					
(LOD <0.1 mg/L) <sup>#</sup>	2-ethylamino methyl cyclohexanone	5.47	2.07	ND		
	2.2.6.6-tetramethyl-4-	37.61	19.19	ND		
	piperidinone	26.91	30.49	ND		
	n-cyclohexylacrylamide	1.53	1.47	ND		
	n-cyclohexyl-propanamide	13.62	13.73	ND		
	1-butyl-2,5 dimethyl-1H-pyrrol	6.33	2.33	ND		
	1,2,2,5-tetramethyl-3-	7.47	4.73	ND		
	piperidinone	4.80	ND	ND		
	Indole	4.87	ND	ND		
	7-methyl indolizine	5.53	ND	ND		
	Glutamic acid dibutyl ester					
Estimated total tar content (mg/L)		192.4 3	142.0 6	<0.10 0		
Mass of tar (mg)		28.86	21.31	<0.01 5		

Table 3: Table listing the compounds identified within the scrubbers from the pyrolysis of UK anaerobically digested (AD) sludge cake at 700 °C. Some of the compounds have been quantified by targeted analysis while those untargeted species have been elucidated by their mass spectrum and semi-quantified in 1 mL aliquot of scrubber (150 mL acetone) by comparing the peak area to an IS. ^targeted compounds, <sup>#</sup>non-targeted compounds, ND – none detected.

Anaerobically		Scrubber concentration			
digested sludge	Compound name	(mg/L)			
cake (UK)		1	2	3	
Volatile aromatic	Benzene	6.50	0.38	ND	
compounds^	Toluene	32.40	0.75	ND	
	Ethylbenzene	6.50	0.22	ND	
	o-xylene	15.31	0.13	ND	
	p-xylene	2.00	ND	ND	
	styrene	11.40	0.15	ND	
	1,3-dimethylbenzene	1.72	ND	ND	
	1-methyl-2-ethylbenzene	0.66	ND	ND	
Polycyclic aromatic	Naphthalene	5.00	0.36	ND	
compounds^	Acenaphthylene	0.74	0.15	ND	
	Phenanthrene	1.30	0.24	ND	
	Anthracene	0.30	ND	ND	
	Fluoranthene	0.21	0.01	ND	
	Pyrene	0.30	ND	ND	
	Benzo (b) fluoranthene	0.11	ND	ND	
	Benzo (a) anthracene	0.11	ND	ND	
Phenolic	Phenol	4.60	0.89	ND	
compounds^	4-methylphenol	2.40	0.43	ND	
	2-methylphenol	6.50	0.83	ND	
	2,3-dimethylphenol	6.50	0.60	ND	
Nitrogen containing	N-isopropyl cyclohexamine	3 03			
compounds	2-ethylaminomethyl cyclohexanone	22.50	2.26		
(LOD <0.1 mg/L)#	N-cyclohexylpropanamide	18 31	2.20		
	n-cyclohexylacrylamide	3.88			
	2,2,6,6-tetramethy-4-piperidinone	19.00	0.54		
	1,2,2,5-tetramethyl-3-piperidinone	7 52	2.05		
	3-hydroxy-1-isopropyl-2-methyl-4(1H)-	1 29			
	pyridinone	0.83	ND		
	5-pentyl-1-H-1,2,4-triazol amine	1 13	ND	ND	
	5-hexyl-1-H-1,2,4-triazol amine				
Estimated total tar		183.06	11.72	<0.100	
content (mg/L)					
Mass of tar (mg)		27.46	1.76	<0.015	

Table 4: Table listing the compounds identified within the scrubbers from the pyrolysis of oilcontaminated brownfield soil at 700 °C. Some of the compounds have been quantified by targeted analysis while untargeted species have been elucidated by their mass spectrum and semi-quantified in 1 mL aliquot of scrubber (150 mL acetone) by comparing the peak area to an IS. ^targeted compounds, #non-targeted compounds, ND – none detected.

Oil contaminated	Compound nome	Scrubber concentration			
brown field soil	Compound name	1	(mg/L)	3	
Volatile aromatic	Benzene	184 00	1 80		
compounds^	Toluene	73 28	0.36		
compoundo	Ethylbenzene	5 16	0.08	ND	
	Styrene	24.92	0.03	ND	
	p-Xvlene	8 52	0.19	ND	
	m-Xvlene	5.92	0.09	ND	
Phenolic compounds^	Phenol	2.50	ND	ND	
		2.00			
Targeted* and non-	Naphthalene*	169.61	4.13	ND	
targeted	2-methylnapthalene	2.12	0.74	ND	
polyaromatic	1-methylnapthalene	11.71	0.42	ND	
compounds	Biphenyl	8.40	0.33	ND	
	1, 6-dimethylnaphthalene	5.79	0.22	ND	
	1, 7-dimethylnaphthalene	9.36	0.37	ND	
	2-ethenylnapthalene	4.24	0.02	ND	
	Acenaphthylene*	27.6	1.02	ND	
	Acenaphthylene derivatives	5.46	0.21	ND	
	Phenalene	4.43	ND	ND	
	Fluorene*	14.22	0.04	ND	
	Dibenzothiophene	4.15	0.55	ND	
	Phenanthrene*	67.60	0.23	ND	
	2-methylanthracene	11.20	2.39	ND	
	8,9-dihydro-4-cyclopenta (def) -	9.14	0.40	ND	
	phenanthrene				
	Anthracene*	16.23	0.43	ND	
	2-phenylnapthalene	4.92	0.64	ND	
	Fluoranthene*	20.41	0.22	ND	
	Pyrene*	27.62	0.73	ND	
	Benz(a)anthracene*	8.00	0.94	ND	
	Chrysene*	8.20	0.33	ND	
	Benzo (a) pyrene*	3.54	0.32	ND	
	Benz (b) fluoranthene*	5.47	0.32	ND	
	Indeno (123-cd) pyrene*	1.20	0.26	ND	
	Dibenza (ah) anthracene*	0.36	0.04	ND	
	Benzo (ghi) perylene*	1.52	ND	ND	
Estimated total tar		756.80	17.85	<0.10	
content (mg/L)					
Mass of tar (mg)		113.52	2.68	0.015	

# **Supplementary**

Table S1: Table detailing the mass scan parameters used for quantitation of volatile and semi-volatile compounds.

Compound	Full mass scan ( <i>m/z</i> )	Retention time (minutes)	SIM scan ( <i>m/z</i> )
Volatile Benzene and Toluene Ethyl benzene Xylene and Styrene Benzene (1-methyl 2-ethyl) Dichlorobenzene D8-Napthalene, Trichlorobenzene	50-350	2.00-3.80 3.80-4.55 4.55-4.80 4.80-5.70 5.70-6.50 6.50-16.33	78, 91 91 91, 104 105 146 136, 179
<b>Semi-volatile</b> Chrysene and Benzo (a) anthracene Indeno (1,2,3 cd)-pyrene, Dibenzo (ab) anthracene, Benzo (ghi) perylene	50-450	14.00-20.00 20.00-24.00	228 276, 278

Table S2: Table detailing the typical chemical composition and energy content of the pyrolysis feedstocks and products generated. The lipid and semi-volatile composition of feedstocks were determined by pentane extraction and GC-MS full scan using spiked internal standards for semi-quantification. The nitrogen content for solid material was determined by standard Kjeldahl method. The total energy content of feedstocks was determined by bomb calorimetry and the syngas derived from pyrolysis of the feedstocks was calculated by from the GC-TCD analysis of the permanent gases calculated based on molar percentage.

Sample	Lipid/semi-volatile composition in feedstock		Mass of nitrogen	Calorific value		Syngas composition Mol %			
	Source	Mass (mg/Kg)	(mg/Kg)	Feedstock (MJ/Kg)	Syngas (MJ/m <sup>3</sup> )	H <sub>2</sub>	со	CO <sub>2</sub>	CH₄
Pine wood	Terpenoids	195.84	N/A	18.67	6.34	45. 3	1.9 8	<0.1	2.71
UK AD sludge cake	Lipids and dietary fats	230.13	2.5	12.15	3.04	22. 6	1.1	<0.1	<0.1
Ghana AD sludge cake	Sterols	3500	3.5	18.00	6.41	45. 5	7.5 8	3.35	<0.1
Brown field soil	10% mass contaminated with PAHs	equiv. 2500	N/A (Kjeldahl)	7.02	0.725	3.3	<0. 1	<0.1	<0.1

Table S3: Table listing the compounds identified within the scrubbers from the pyrolysis of pine wood at 700 °C. Targeted compounds have been quantified while untargeted species have been elucidated by their mass spectrum and semi-quantified in 1 mL aliquot of scrubber (150 mL acetone) by comparing the peak area to an IS. ^targeted compounds, <sup>#</sup>non-targeted compounds, ND – none detected.

		Scrubber	conce	ntration
Pine wood	Compounds identified	(mg/L)		
		1	2	3
Volatile aromatic	Benzene	31.71	ND	ND
compounds^	Toluene	25.60	0.16	ND
	Ethylbenzene	9.03	0.18	ND
	1,3-dimethylbenzene	5.50	ND	ND
	Styrene	3.00	ND	ND
	P-xylene	2.74	ND	ND
Polycyclic aromatic	Naphthalene	2.70	0.70	ND
compounds^	Acenaphthylene	0.46	0.13	ND
	Phenanthrene	0.41	ND	ND
	Anthracene	0.18	ND	ND
	Fluorene	0.21	0.15	ND
Phenolic	Phenol	10.98	1.90	ND
compounds^	4-methylphenol	5.79	1.52	ND
	2-methylphenol	6.84	1.01	ND
	2,3-dimethylphenol	7.40	1.00	ND
	4-chloro-3-methylphenol	3.02	0.52	ND
Non-Targeted	2-Furancarboxylic acid	5.70	2.05	ND
Other (LOD 0.05	2-Furanmethanol	7.30	2.79	ND
mg/L) <sup>#</sup>	2-Furanone	6.28	1.99	ND
<b>U</b> ,	2-Cyclopenten-1-one	7.11	2.76	ND
	Carbanicacic-phenyl ester	9.23	4.11	ND
	3-methylcyclopentane	10.06	3.43	ND
	Benzyl alcohol	4.47	1.98	ND
	2-methoxyphenol	20.86	10.35	ND
	Cresol	31.06	27.57	ND
	6-methyl-4-pyrimidinol	21.75	ND	ND
	4-ethyl-2-hydroxy-cyclopentene-1-one	5.21	5.29	ND
	Salicyl alcohol	6.32	3.65	ND
	p-ethylguaicol	16.20	3.21	ND
	4-ethenyl-2-methoxyphenol	16.20	5.06	ND
	Isoeugenol	32.00	11.91	ND
	Anhydro-D-mannosan	150.12	5.74	ND
	Conifyl aldehyde	10.78	2.15	ND
	Arabinose	6.35	0.67	ND
	Dehvdroabietic acid	0.10	ND	ND
	Methyldehydroabietate	0.060	ND	ND
	Retene	0.067	ND	ND
Estimated total tar		400.00	404.00	10 100
content (mg/L)		482.80	101.98	<0.100
Total mass of tar		72 42	15 30	<0.015
(mg)		12.72	10.00	-0.013

		Scrubber conc	entration (mg/L)
	Compounds identified	Pre-recycling	Recycled
	Benzene	10.84	9.17
VOC	Toluene	9.86	8.19
VUC	Ethylbenzene	1.37	0.46
Targeled	P-xylene	0.78	0.27
	Styrene	2.56	0.45
	Total	25.41	18.54
	Phenol	3.89	ND
	2-methylphenol	2.0	ND
SVOC	4-methylphenol	2.62	ND
SVUC Targeted	2,3-dimethylphenol	2.23	ND
Targeleu	Naphthalene	0.60	ND
	4-chlorophenol	0.70	ND
	Phenanthrene	0.35	ND
	Total	12.39	<0.01
	2-propyl-1-pentanol methyl ether	1.09	ND
	N-cyclohexyl propanamide	6.21	ND
Non	2,2,6,6 Tetramethy-4-piperidinone	2.41	ND
targeted	Cresol	8.69	ND
largeleu	2, 5-dimethoxytoluene	1.19	ND
	Isoegenol	1.37	ND
	Andro D-mannosan	3.00	ND
	Total	23.96	<0.100

Table S4: Table describing the compounds identified in the acetone pooled scrubber before and after acetone remediation.



Figure S1: Shows the total ion chromatogram of scrubber 1 showing volatile and semivolatile organic compounds captured during the thermal treatment (pyrolysis) of pine wood (1.), brown field soil contaminated with oily sludge (2.) and UK AD sludge cake (3.). The main components of each spectra were identified from NIST 2.0 library search.