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Study of the $^{240}Pu(n,f)$ reaction at n_TOF/EAR2 facility in the 9 meV - 6 MeV range

2	A. Stamatopoulos. ^{1,*} A. Tsinganis. ^{1,2} N. Colonna. ³ M. Kokkoris. ¹ R. Vlastou. ¹ M. Diakaki. ^{4,1} P. Žugec. ⁵
3	P. Schillebeecky. ⁶ F. Gunsing. ^{4,2} M. Sabaté-Gilarte. ^{2,7} M. Barbagallo. ³ O. Aberle. ² J. Andrzejewski. ⁸
4	L Audouin ⁹ V Bécares ¹⁰ M Bacak ¹¹ J Balibrea ¹⁰ S Barros ¹² F Bečvář ¹³ C Beinrucker ¹⁴
5	F. Belloni. ⁴ E. Berthoumieux. ⁴ J. Billowes. ¹⁵ D. Bosnar. ⁵ M. Brugger. ² M. Caamaño. ¹⁶ S. Lo Meo. ^{17,18}
6	F. Calviño ¹⁹ M. Calviani ² D. Cano-Ott ¹⁰ F. Cerutti ² F. Chiaveri ² G. Cortés ¹⁹ M. A. Cortés-Giraldo ⁷
7	L Cosentino ²⁰ L A Damone ^{3,21} K Deo ²² C Domingo-Pardo ²³ B Dressler ²⁴ E Dupont ⁴ I Durán ¹⁶
, ,	B. Fernández-Domínguez ¹⁶ A. Ferrari ² P. Ferreira ¹² P. Finocchiaro ²⁰ R. I. W. Frost ¹⁵ V. Furman ²⁵ K. Göbel ¹⁴
8	A B Caraía ¹⁰ I Cheorgho ²⁶ T Clodariut ²⁶ I E Congelves ¹² E Cangélez Bomere ¹⁰ A Coverdevelei ²⁷
9	F. Chicamaran ¹¹ C. Chicamara ⁷ H. Hanada ²⁸ T. Hoffmich ¹⁴ S. Hoinitz ²⁴ A. Hannondoz Drieto ^{2,19} I. Hanada ⁶
10	D. C. Jonling ²⁹ E. Jonicho ¹¹ E. Käppeler ³⁰ V. Kedi ² T. Ketabuchi ³¹ D. Kermigin ¹¹ V. Ketlerer ²⁷
11	D. G. Jenkins, E. Jencha, F. Kappeler, T. Kadi, T. Katabuchi, F. Kavinghi, V. Ketlelov,
12	V. Knryachkov, ¹⁷ A. Kimura, ¹⁰ N. Kivel, ¹¹ I. Knapova, ¹⁰ N. Krticka, ¹⁰ E. Leal-Oldoncha, ¹⁰ C. Lederer, ¹⁰
13	C. Magainai 18,33 D. Magtinu 34 M. Magtanapana 3 E. Mattauagi 35,36 E. Mandara 10 A. Mangani 17 D. M. Milaga 35
14	E. Mingmong ¹⁸ M. Mingg ²⁶ C. Montagong ² A. Mugumanna ^{20,37} D. Nalta ³⁸ E. D. Dalama Dinta ⁷ C. Davadala ¹⁶
15	r. Mingrone, M. Mirea, S. Montesano, A. Musumarra, M. R. Noite, F. R. Palomo-Pinto, C. Paradeia, N. Detronic ³⁹ A. Devlik ⁴⁰ I. Devleveli ⁸ A. Diemen ⁶ I. I. Devreg ² ⁴¹ I. Dreene ⁷ I. M. Ouegada ⁷
16	N. Patronis, A. Pavink, J. Perkowski, A. Piompen, J. I. Porras, J. J. Praena, J. M. Quesada, T. Davishar 42, 43 D. Daifarth 14 A. Diana Davis 19 M. Dahlar 16 C. Dahlar 2, J. A. Davis 15 A. Carrang 22
17	1. Rauscher, ¹² , ¹⁶ R. Reifarth, ¹⁷ A. Riego-Perez, ¹⁶ M. Robles, ¹⁶ C. Rubbia, ² J. A. Ryan, ¹⁶ A. Saxena, ²² G. T. P. 24 D. G. L. L. 25 A. G. G. V. 15 G. M. G. 22 G. T. P. 3
18	S. Schmidt, ¹⁴ D. Schumann, ²⁴ P. Sedyshev, ²⁵ A. G. Smith, ¹⁶ S. V. Suryanarayana, ²² G. Tagliente, ⁵
19	J. L. Tain, ²⁵ A. Tarifeno-Saldivia, ²⁵ L. Tassan-Got, ⁵ S. Valenta, ¹⁵ G. Vannini, ^{16,35} V. Variale, ⁵ P. Vaz, ¹²
20	A. Ventura, ¹⁶ V. Vlachoudis, ² A. Wallner, ⁴⁴ S. Warren, ¹⁵ M. Weigand, ¹⁴ C. Weiss, ^{2,11} and T. Wright ¹⁵
21	(The n_TOF Collaboration (www.cern.ch/ntof))
22	¹ National Technical University of Athens, Greece
23	² European Organization for Nuclear Research (CERN), Switzerland
24	^a Istituto Nazionale di Fisica Nucleare, Sezione di Bari, Italy ⁴ CFA Infu, Université Paris Saclay, F 01101 Cif sur Vyette, France
25	⁵ Department of Physics Faculty of Science University of Zaareb Zaareb Croatia
27	⁶ European Commission, Joint Research Centre, Geel, Retieseweg 111, B-2440 Geel, Belgium
28	⁷ Universidad de Sevilla, Spain
29	⁸ University of Lodz, Poland
30	⁹ Institut de Physique Nucléaire, CNRS-IN2P3, Univ. Paris-Sud,
31	Université Paris-Saclay, F-91406 Orsay Cedex, France
32	Centro de Investigaciones Energeticas Medioambientales y Techologicas (CIEMAI), Spain ¹¹ Technische Universität Wien Austria
34	¹² Instituto Superior Técnico. Lisbon. Portugal
35	¹³ Charles University, Praque, Czech Republic
36	¹⁴ Goethe University Frankfurt, Germany
37	15 University of Manchester, United Kingdom
38	¹⁶ University of Santiago de Compostela, Spain
39	¹ Agenzia nazionale per le nuove tecnologie (ENEA), Bologna, Italy ¹⁸ letitute Newionale di Ficio Nucleane Coriene di Bologna, Italy
40	¹⁹ Universitat Politècnica de Catalunya Spain
41	²⁰ INFN Laboratori Nazionali del Sud. Catania. Italu
43	²¹ Dipartimento di Fisica, Università degli Studi di Bari, Italy
44	²² Bhabha Atomic Research Centre (BARC), India
45	²³ Instituto de Física Corpuscular, CSIC - Universidad de Valencia, Spain
46	²⁴ Paul Scherrer Institut (PSI), Villingen, Switzerland
47	²⁶ Joint Institute for Nuclear Research (JINR), Dubna, Russia ²⁶ Honio Halubei National Institute of Dhusics and Nuclear Engineering. Remanic
48	²⁷ Institute of Physics and Power Engineering (IPPE) Obninsk Bussia
49 50	²⁸ Japan Atomic Energy Agency (JAEA). Tokai-mura, Japan
51	²⁹ University of York, United Kingdom
52	³⁰ Karlsruhe Institute of Technology, Campus North, IKP, 76021 Karlsruhe, Germany
53	³¹ Tokyo Institute of Technology, Japan
54	³² School of Physics and Astronomy, University of Edinburgh, United Kingdom
55 56	³⁴ Istituto Nazionale di Fisica Nucleare, Sezione di Leanaro, Italy
эо 57	³⁵ Istituto Nazionale di Fisica Nucleare, Sezione di Trieste Italu
58	³⁶ Dipartimento di Astronomia, Università di Trieste, Italy

³⁷Dipartimento di Fisica e Astronomia, Università di Catania, Italy

³⁸ Physikalisch-Technische Bundesanstalt (PTB), Bundesallee 100, 38116 Braunschweig, Germany

³⁹University of Ioannina, Greece

⁴⁰ University of Vienna, Faculty of Physics, Vienna, Austria ⁴¹ University of Granada, Spain

⁴²Centre for Astrophysics Research, University of Hertfordshire, United Kingdom

⁴³Department of Physics, University of Basel, Switzerland

⁴⁴Australian National University, Canberra, Australia

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Background: Nuclear waste management is considered amongst the major challenges in the field of nuclear energy. A possible means of addressing this issue, is waste transmutation in advanced nuclear systems, whose operation requires a fast neutron spectrum. In this regard, the accurate knowledge of neutron-induced reaction cross sections of several (minor) actinide isotopes is essential for design optimisation and improvement of safety margins of such systems. One such case is ²⁴⁰Pu, due to its accumulation in spent nuclear fuel of thermal reactors and its usage in fast reactor fuel. The measurement of the 240 Pu(n,f) cross section was previously attempted at the CERN n_TOF facility EAR1 measuring station using the time-of-flight technique. Due to the low amount of available material and the given flux at EAR1 the measurement had to last several months to achieve a sufficient statistical accuracy. This long duration led to detector deterioration due to the prolonged exposure to the high α -activity of the fission foils, therefore the measurement could not be successfully completed.

Purpose: Determine whether it is feasible to study neutron-induced fission at n_TOF/EAR2 and provide data on the 240 Pu(n,f) reaction in energy regions requested for applications.

Methods: The study of the ²⁴⁰Pu(n,f) reaction was made at a new experimental area (EAR2) with a shorter flight-path which delivered on average 30 times higher flux at fast neutron energies. This enabled the measurement to be performed much faster thus limiting the exposure of the detectors to the intrinsic activity of the fission foils. The experimental setup was based on microbulk Micromegas detectors and the time-of-flight data were analysed with an optimised pulse-shape analysis algorithm. Special attention was dedicated to the estimation of the non-negligible counting loss corrections with the development of a new methodology and other corrections were estimated via Monte Carlo simulations of the experimental setup.

Results: This new measurement of the 240 Pu(n,f) cross section yielded data from 9 meV up to 6 MeV incident neutron energy and fission resonance kernels were extracted up to 10 keV.

Conclusions: Neutron-induced fission of high activity samples can be successfully studied at the n_TOF/EAR2 facility at CERN covering a wide range of neutron energies, from thermal to a few MeV.

Keywords: Fission, Cross section, Plutonium 240, Time of flight, n_TOF, Micromegas, Resonance analysis

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I.

Α. Motivation

INTRODUCTION

A significant fraction of electricity production (25% in ⁹¹ 71 Europe [1]) is based on nuclear sources, however, this re- ⁹² 72 sults in the accumulation of long-lived radioactive waste. 93 73 A possible means of disposing this waste is through its ⁹⁴ 74 transmutation in advanced nuclear systems, such as Gen-⁹⁵ 75 IV reactors [2, 3] and Accelerator Driven Systems [4, 5], ⁹⁶ 76 which will be operated with a fast neutron spectrum. 97 77 The consumption of known uranium resources by 2050 [6] 98 78 should also be considered in the design of future power ⁹⁹ 79 plants since it constrains the nuclear fuel possibilities.100 80 The accurate knowledge of neutron-induced reactions is101 81 therefore essential for feasibility studies and optimum op-102 82 eration of such systems. At the same time, the improve-103 83 ment of safety margins of thermal reactors which are104 84 currently in operation is considered equally important,105 85 therefore the accurate knowledge of cross sections on fer-106 86

tile isotopes is also required. In this respect, the Nuclear Energy Agency (NEA) [7] has introduced the High Priority Request List (HPRL) [8] in which data on a plethora of reactions and derived quantities are requested.

The 240 Pu(n,f) is among these reactions since 2008 [9] and up to present the requested accuracies [10] have not been met. ²⁴⁰Pu is a long-lived fertile plutonium isotope and is produced in conventional reactors from neutron capture on ²³⁹Pu, therefore it plays an important role in the U/Pu cycle affecting the breeding process. In addition, about ~ 60 kg of 240 Pu are annually discharged per reactor unit [11], which is a significant quantity to be used as fuel in future fast reactors.

Finally, the intermediate structures that can be observed in the (n,f) cross section in the resolved resonance region can provide constraints on phenomenological fission models through the characterisation of resonance properties. At the same time, resonance structures appear in the cross section in the hundreds of keV region near the threshold fission, as an effect of vibrational states in the second well of the double-humped fission barrier, which require a combination of high flux and resolution to be observed and can contribute to the understanding of the fission mechanism.

^{*} athanasios.stamatopoulos@cern.ch

B. Previous measurements

Due to the importance of the 240 Pu(n,f) reaction many₁₆₇ 112 data-sets exist in the EXFOR database [12] covering in-113 cident neutron energies from 25.3 meV up to 200 MeV. 114 More specifically, the cross section was measured at the_{170} 115 thermal point by Pratt et al. $(\sigma_{\rm th} = 3700(8000) \text{ mb}, [13])_{171}$ 116 and Eastwood et al. ($\sigma_{\rm th} = 30(45)$ mb, [14]) and both re-₁₇₂ 117 sults were uncertain and discrepant by more than two or-173 118 ders of magnitude. In addition, spectrum and maxwellian $_{174}$ 119 average cross section at the thermal point were reported₁₇₅ 120 by Bigham [15] and Hulet et al. [16], respectively. 121 176

The first resonance in the ²⁴⁰Pu + n system is observed 1.05 eV above the neutron separation energy. For¹⁷⁷ neutron-induced fission, only a single data-set exists in¹⁷⁸ this region reported by Leonard Jr. et al. [17] which was¹⁷⁹ obtained with poor neutron energy resolution. ¹⁸⁰

¹²⁷ Up to 5 keV several measurements have been per-¹⁸¹ formed, however only the data by Weston et al. [18] have¹⁸² the level of resolution and statistics required to perform¹⁸³ resonance analyses, according to the extensive argumen-¹⁸⁴ tation of Bouland et al. [19].¹⁸⁵

¹³² Between 5 and 50 keV, the data reported by Weston ¹³³ [18] and by Budtz-Jorgensen and Knitter [20] show over-¹³⁴ lapping class-II resonance structures which are quite dis-¹³⁵ crepant. For instance the structures seen at $E_n \sim 13.5$ ¹³⁶ keV (fig. 19) and 20 keV are discrepant by 40% and 30%¹⁸⁶ ¹³⁷, respectively.

Above 50 keV up to the vicinity of the fission threshold, 138 a plethora of measurements has been performed. The $^{\rm 187}$ 139 three latest ones were reported by Salvador-Castineira et 140 [21], Tovesson et al. [22] and Laptev et al. $[23]_{188}$ al. 141 and discrepancies that reach up to 15% were observed. 142 In addition, the latest time-of-flight data by Tovesson et_{190} 143 al. [22] are of insufficient resolution to observe structures₁₉₁ 144 attributed to vibrational phenomena. 145 192

Finally, in the first chance fission plateau up to 6 $MeV_{,_{193}}$ 146 several measurements have been performed as well. Con- $_{\scriptscriptstyle 194}$ 147 cerning the three latest ones, the data by Tovesson et al.,105 148 [22] are systematically higher by about 6% compared to 149 the corresponding ones by Salvador-Castineira et al. $[21]^{196}$ 150 and Laptev et al. [23] which justifies the need for addi-197 151 198 tional measurements in this region as well. 152 199

C. The need for a second experimental area at n_TOF

The ²⁴⁰Pu(n,f) reaction was attempted to be studied₂₀₄ 155 at n_TOF in 2010 at the horizontal 185m-long flight path,205 156 commonly referred to as EAR1, using the time-of-flight²⁰⁶ 157 technique to determine the incident neutron energy $[24]_{207}$ 158 and Micromegas fission fragment detectors. The moder-208 159 ate neutron flux delivered at EAR1, inevitably led to a²⁰⁹ 160 lengthy measurement to achieve sufficient statistical ac-210 161 curacy in the MeV region. The detectors were therefore₂₁₁ 162 exposed for several months to the high intrinsic α -activity₂₁₂ 163 of the samples, which caused them to deteriorate and₂₁₃ 164

eventually rendered the study incomplete.

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To further expand the measuring capabilities of n_TOF and to perform studies of important reactions where samples with either high activity, low mass or small cross section are needed, a second experimental beam line (EAR2) was commissioned in 2014 [25]. The present measurement [26, 27], where high activity samples were used, along with the ⁷Be(n, α) one [28], in which the short halflife of ⁷Be ($t_{1/2} = 53.2$ d) limits the study of its low cross section, exemplify the capabilities of EAR2 which are a result of the high instantaneous flux and good resolution (see section II A).

Taking advantage of these characteristics a new study of the 240 Pu(n,f) reaction was successfully performed in EAR2. This experimental campaign was the first performed in EAR2 and the derived cross section spanned across 9 orders of magnitude in incident neutron energy, ranging from 9 meV up to 6 MeV. The results that will be presented illustrate the potential of EAR2 in completing challenging fission studies which was also demonstrated by succeeding measurements [29–31].

II. EXPERIMENTAL DETAILS

A. Neutron source

Neutrons at n_TOF are produced by spallation with a 20 GeV/c pulsed proton beam that impinges on a lead block. The spallation target assembly consisted of a cylindrical lead block, 40 cm in length and 60 cm in diameter, which was surrounded by a thin layer of water for cooling and moderation purposes, thus the neutron spectrum delivered in EAR2 covered a broad energy range from thermal energies up to 100 MeV [32].

The proton beam is delivered by CERN's Proton Synchrotron (PS) at a low frequency which does not exceed 0.8 Hz and has a spread of 7 ns RMS. The beam intensity was 6.6×10^{12} protons/bunch on average and was constant within 2%.

The experimental area rests at the end of a 18.4 m long beam-line from the centre of the spallation target, which is kept under a 10^{-2} mbar vacuum. The beam was shaped by means of a 3 m long neutron collimator with an aperture of 2.2 cm, which consisted of 2 m Fe and 1 m polyethylene enriched with boron. The proximity of EAR2 to the target yielded a 30 times higher flux than the one of EAR1 while neutrons needed an approximately 10 times shorter time of flight to reach the experimental area. These attributes resulted in a considerably improved background suppression, as shown in fig. 1, and mitigated the effects of the strong α -activity which occurred in EAR1.

TABLE I. List of the main characteristics of the fission foils used in the experiment along with the estimated uncertainties, provided by JRC-Geel which were determined on May 2011 for the 240 Pu samples, on January 1981 for 235 U and on February 2012 for 238 U.

Sample	Lot	Reference Number	$\begin{array}{c} {\rm Mass} \\ {\rm (mg)} \end{array}$	Areal density (mg/cm^2)	$\begin{array}{c} \text{Atomic} \\ \text{abundances} \\ (\%) \end{array}$
²⁴⁰ Pu	BC01269B	TP2010-011-01 TP2010-011-03 TP2010-011-04	$egin{array}{c} 0.7163(28) \ 0.809(3) \ 0.763(3) \end{array}$	$\begin{array}{c} 0.1017(4) \\ 0.1148(5) \\ 0.1083(5) \end{array}$	$\begin{array}{r} {}^{238}{\rm Pu:} \ 0.0733(29) \\ {}^{239}{\rm Pu:} \ 0.0144(18) \\ {}^{240}{\rm Pu:} \ 99.8915(18) \\ {}^{241}{\rm Pu:} \ 0.00041(31) \\ {}^{242}{\rm Pu:} \ 0.02027(41) \\ {}^{244}{\rm Pu:} \ 0.000046(88) \end{array}$
Total			2.2883	0.3248	
²³⁵ U	SP 3576	SP 3576-1	0.563(11)	0.0912(17)	${}^{234}\text{U: } 0.1698 \\ {}^{235}\text{U: } 99.475 \\ {}^{236}\text{U: } 0.0273 \\ {}^{238}\text{U: } 0.3277 \\ \end{array}$
²³⁸ U	2677	TP2011-008-03	0.745(15)	0.1070(22)	238 U> 99.9
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FIG. 1. Amplitude spectra recorded in EAR1 and EAR2²³⁹ for a ²⁴⁰Pu sample. The α -particle background in EAR2 is appreciably suppressed while the fission rate is significantly²⁴¹ higher.²⁴³

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B. Fission foils

Three high purity ²⁴⁰Pu samples in the form of₂₄₈ 215 ²⁴⁰PuO₂, with a total activity of 19.22 MBq, were origi-₂₄₉ 216 nally prepared at EC-JRC-Geel [33] for the measurement₂₅₀ 217 in EAR1 but were also used in the EAR2 experimen-251 218 tal campaign. The plutonium material was deposited₂₅₂ 219 through molecular plating on 0.25 mm thick and 5 cm_{253} 220 in diameter aluminium backings, whereas the deposits₂₅₄ 221 themselves had a diameter of 3 cm. It needs to be noted₂₅₅ 222 that the small difference in the diameters did not $affect_{256}$ 223 the analysis and the results, as shown in Ref. [34]. 224 257

Two additional samples were used as reference foils: $_{258}$ (a) a 235 U sample with a 40.5 Bq activity and (b) a 238 U₂₅₉ sample with 9.4 Bq activity. The 235 U deposit had a₂₆₀

diameter of 2.9 cm and was in the chemical form of UF₄. The 238 U sample had a diameter of 3 cm and was made of U(OH)₆ material. Both samples were manufactured by means of molecular plating and had aluminium backings similar to the plutonium ones.

The main characteristics of the fission foils used in the measurement can be seen in Table I.

C. Detectors

To detect the fission fragments a setup based on the compact and neutron-transparent microbulk Micromegas detector was used [35]. The gas volume of the detector was divided in two regions by a thin (5 μ m) copper micromesh: (a) The drift region (6 mm), between the cathode and the micromesh and (b) the narrow amplification gap (50 μ m) between the micromesh and the 5 μ m thick copper anode. In this configuration, the fission foil was positioned so that the deposit faced the drift region and its backing served as the cathode.

An electric field of the order of 50 kV/cm was applied in the amplification gap, which is sufficient to cause avalanche multiplication resulting in a high detector gain. What is remarkable in this detector is the fact that its gain is intrinsic and depends only on the applied electric field, hence enhancing the signal to electronic background ratio. This is important in cases where the electronic noise is high and the signal must be individually amplified.

All detector-sample sets were stacked in a cylindrical aluminium chamber which was equipped with 50 μ m thick kapton windows. The spacing between the detector-sample sets was 2 cm. The chamber was filled with a circulating gas mixture of Ar:CF₄:iC₄H₁₀ at 88 : 10 : 2 volume fraction, at atmospheric pressure and



FIG. 2. Schematic view of the fission foil stack, with respect to the neutron beam direction. Apart from the fission samples, an empty cathode was placed to monitor possible proton and α -recoils from the detector itself.

The low amount of material present in the Micromegas, 262 minimised the production of charged particles from neu-263 tron interactions with the detector itself which was con-264 firmed by an empty cathode-detector set, placed behind 265 the 238 U sample, as schematically shown in fig. 2. 266

In addition to the fission detectors, a set-up based on 267 Silicon detectors was used to monitor the neutron beam. 268 based on the detection of α -particles and tritons pro-269 duced from the ${}^{6}Li(n,t)$ reaction. Details on the monitor 270 set-up, which is referred to as "SiMon2" can be found in 271 [36].272

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Data acquisition D.

Data were digitised through the use of 8-bit flash ADCs 274 that were operated at a 500 MHz sampling rate. The ac- $^{\rm 310}$ 275 quisition window was 16 ms wide and allowed to reach³¹¹ 276 down to thermal and cold neutron energies. Finally, an³¹² 277 online zero-suppression algorithm was applied to min-imise the amount of data recorded during the acquisition³¹⁴ 278 279 [37].280

III. 281

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Signal processing Α.

DATA REDUCTION AND ANALYSIS

The digitised waveforms were processed offline by a 283 pulse shape analysis framework developed at n_TOF [38]. 284 The signal recognition was based on a single-stage differ-285 entiation filter whereas the reconstruction of the wave-286 forms was based on pulse shape fitting procedures. 287

Signal processing was performed in two procedures re-288 garding: (a) the so-called γ -flash, which is a burst of 289 photons and relativistic particles that are produced dur-290 ing spallation and arrive promptly at the experimental 291 hall [39] and (b) regular fission and α -particle signals. 292

a. γ -flash In the present case, the baseline follow-293 ing the γ -flash had an oscillatory behaviour that remained consistent from pulse to pulse. Since fission signals were sitting on the trailing edge of the γ -flash as well as on top of the oscillations, the subtraction of an average γ -flash shape was applied to each individual waveform, 298 as described in detail in ref. [38].

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The calculation of the average shape was achieved from recorded waveforms which were stacked, as shown in fig. 3. In the calculation, fission signals were not taken into account since they would have distorted the average shape. Such a procedure is important since it can extend to the highest reachable neutron energy and it allowed to better discriminate low-amplitude fission signals that sit on the crest of the oscillations.



FIG. 3. Stacked recorded waveforms in the γ -flash region for a ²⁴⁰Pu sample. The solid line corresponds to the calculated average. The signals shown correspond to 1% of the statistics. A few indicative neutron energies are also shown.

This procedure was followed by the calculation of the residuals between the average γ -flash shape and each individual waveform as a means of cross-checking that the subtraction was properly applied and estimating the highest reachable energy. The individual residuals were then stacked and projected along the amplitude axis, as shown in the inset of fig. 4.



FIG. 4. Stacked residuals between the average γ -flash and the recorded waveforms in the $\gamma\text{-flash}$ region for a $^{240}\mathrm{Pu}$ sample. The inset contains the projection of the residuals to the y-axis, up to 10 MeV neutron energy. The signals shown correspond to 1% of the statistics.

A gaussian fit on the projected residuals indicated₃₅₈ 315 a mean value of 0, which verified that the subtraction₃₅₉ 316 was properly applied within an uncertainty of ~ 5 chan-₃₆₀ 317 nels (2% of the full range), up to the time-of-flight that₃₆₁ 318 corresponds to 10 MeV incident neutron energy. For₃₆₂ 319 smaller times the projection of the residuals significantly₃₆₃ 320 widened, therefore 10 MeV was considered to be the max-364 321 imum highest reachable energy as far as the signal pro-365 322 cessing is concerned. 323 366

b. Fission signals: A similar approach was followed 324 concerning the fission signals. Isolated detector signals $_{368}$ 325 were stacked and average pulse shapes were extracted for 326 each individual detector. These were then fed into the re-327 construction routines and pulse shape fitting was applied 328 to determine signal attributes such as the arrival time, 329 the amplitude etc. This information was then stored in³⁶⁹ 330 the so-called list mode, in order to perform the offline 331 analysis and reconstruct the reaction yield as a function $_{370}$ 332 of the time-of-flight. 333

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B. Cross section calculation

The cross section was deduced with reference to The cross section was deduced with r

$$\sigma = \frac{C}{C^{(\text{ref})}} \frac{f_{\text{amp}}}{f_{\text{amp}}^{(\text{ref})}} \frac{f_{\text{imp}}}{f_{\text{imp}}^{(\text{ref})}} \frac{f_{\text{DT}}}{f_{\text{DT}}^{(\text{ref})}}$$
$$\frac{f_{\text{abs}}}{f_{\text{abs}}^{(\text{ref})}} \frac{f_{\text{shield}}}{f_{\text{shield}}^{(\text{ref})}} \frac{f_{\text{SF}}}{f_{\text{SF}}^{(\text{ref})}} \frac{f_{\gamma f}}{f_{\gamma f}^{(\text{ref})}}$$
$$\frac{m^{(\text{ref})}}{m} \frac{\Phi^{(\text{ref})}}{\Phi} \sigma^{(\text{ref})}$$
(1a)

$$\sigma = \frac{Cf_{\text{amp}} f_{\text{imp}} f_{\text{DT}} f_{\text{abs}} f_{\text{shield}} f_{\text{SF}} f_{\text{CD}} f_{\gamma f}}{m \Phi} \qquad (1b)$$

- 340 where:
- 1. C refers to the fission counts
- ³⁴² 2. f_{amp} is the correction factor of the rejected fission ³⁴³ signals below the amplitude threshold which was ³⁴⁴ applied to reject α -particles and noise (see section ³⁴⁵ III B 2).
- 346 3. $f_{\rm imp}$ corrects for the parasitic counts that contributed to the recorded yield and were attributed to fission reactions from contaminants or impurities in the fission foils
- 4. $f_{\rm DT}$ is a correction factor applied for counting losses₃₈₁ due to dead-time, pile-up and insufficient signal re-₃₈₂ construction effects 383
- 5. f_{abs} takes into account the self-absorption of fission₃₈₄ fragments within the fission foils

- 7. $f_{\rm SF}$ accounts for the contribution of spontaneous fission events
- 8. $f_{\gamma f}$ is the correction factor due to parasitic counts that contributed to the recorded fission yield from photo-fission reactions
- 9. *m* is the mass term and corresponds to the areal density of the fission foil (table I).
- 10. Φ is the neutron fluence incident at the corresponding foil.

The terms that include the superscript "(ref)" refer to the reference sample.

1. Fission counts

The number of fission events as a function of the timeof-flight was determined from the signal processing described in section III A. A typical distribution of the reconstructed time-of-flight vs amplitude can be seen in fig. 5, for a ²⁴⁰Pu sample. The reconstructed signals were then thoroughly checked in order to reject noise (i.e. saturated signals from sparks in the gas, falsely reconstructed signals etc) and to apply the proper thresholds to reject non-fission events (i.e. α -particles). In the latter case the appropriate correction factors were applied to the fission yield, as will be described later in the text.



FIG. 5. Typical 2D distribution of the reconstructed timeof-flight and amplitude signals for a 240 Pu sample. Residuals from the γ -flash subtraction and signals from the α -activity are illustrated in the bottom left and right part of the figure, respectively. Resonances are also visible. A few indicative neutron energies are shown.

The statistical uncertainties after the application of the correction factors, were of the order of 10% in the thermal region and vary between 6 - 60% and 5 - 30%in the resolved and unresolved resonance region, respectively. These high statistical uncertainties were observed in the valleys between resonances where the reaction rate was quite low. At higher neutron energies the statistical uncertainties did not exceed 8% as shown in fig. 6.



FIG. 6. Statistical uncertainties, after applying the corrections, in the 100 keV - 6 MeV high-energy region concerning the lightest 240 Pu sample. Up to 1 MeV an isolethargic binning of 100 bins per decade was used whereas in the MeV region a custom binning that is shown in Appendix B was adopted.

2. Amplitude threshold

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A typical fission amplitude spectrum, such as the one 390 reconstructed in the present case and shown in fig. 7. 391 consists mainly of two parts: (a) the fission fragments 392 and (b) the α -particles from the intrinsic radioactivity 393 of the fission foil. To reject the α -counts, an amplitude 394 threshold was introduced in the analysis based on beam-395 off runs to locate the high amplitude tail of the α -particle 396 spectrum. However, a fraction of fission counts was in-397 evitably rejected as well, whose estimation was based on 398 Monte Carlo simulations by coupling the GEF [40] and 399 FLUKA [41] codes. 436 400

Fission fragment (FF) distributions were generated in437 401 GEF and were then used as a source term in FLUKA. Fis-438 402 sion fragments were produced within the sample and₄₃₉ 403 propagated towards the gas in order to estimate the de-440 404 posited energy. The simulated energy deposition was₄₄₁ 405 convoluted with an appropriate response function of the₄₄₂ 406 detection/read-out system and was finally calibrated in443 407 order to be compared to the experimental amplitude444 408 spectrum. 445 409

The α -particles were not simulated since only a small⁴⁴⁶ 410 part of the tailing edge was recorded, however, in or-447 411 der to benchmark the simulations, beam-off spectra, that⁴⁴⁸ 412 practically consisted only of α -counts, were used. More⁴⁴⁹ 413 specifically, the simulated spectra which contained only 414 FF, were summed with beam-off amplitude distributions 415 and were then compared to experimental beam-on spec-450 416 tra, which consisted of both FF and α -counts. As char-417 acteristically shown for a ²⁴⁰Pu sample in fig. 7, a quite₄₅₁ 418 satisfactory agreement was achieved. 452 419 The $f_{\rm amp}$ correction factor can then be estimated from 453 420 the simulations as the fraction of the integral beneath the454 421

422 corresponding amplitude threshold (shaded area, fig. 7).455
423 The aforementioned procedure was performed individu-456
424 ally for the ²⁴⁰Pu, ²³⁵U and ²³⁸U samples and correction457
425 factors in the 2-11.5% range were determined, as shown458

in table II.

To estimate the uncertainty of the simulations, the uranium samples were used. The low activity of these samples (a few tens of Bq) and the narrow acquisition window (16 ms) made the detection of α -particles highly improbable. In this respect, the simulated and experimental fraction of the rejected FF was compared and an agreement within 3% was achieved, which was considered to be the an upper bound of systematic uncertainty of this correction factor.



FIG. 7. Comparison between the experimental and simulated amplitude spectra from a 240 Pu sample. For the low amplitude region, a beam-off spectrum was added to the simulated one. The reproduction of the experimental points is quite satisfactory. The shaded area represents the fraction of the rejected FF for an amplitude threshold equal to 30 channels.

In the simulations, apart from the energy deposition in the gas, several other effects on the correction factor were studied such as: (a) the chemical composition of the samples, which might deviate from the nominal one due to the preparation method [42] and/or environmental conditions (i.e. moisture) and (b) the FF angular distribution which might be important above 1 MeV. In the former case the chemical composition was varied (e.g. in the ²³⁸U sample from U(OH)₆ to U(OH)₁₀) while in the latter one FF were propagated unidirectionally towards the gas from 0° to 89° with respect to the neutron beam. In both studies the effect on $f_{\rm amp}$ was less than 3% and 1%, respectively. More information can be found in ref. [34].

3. Impurities

It was previously mentioned that in the ²⁴⁰Pu samples impurities with a total abundance of 0.1% were present (table I). Despite this small fraction, their contribution to the fission yield was high in the thermal and resolved resonance regions, attributed mainly to the fissile ²³⁹Pu. The estimation of the $f_{\rm imp}$ correction factor, was based on "weighting" the ENDF/B-VIII.0 evaluated (n,f) crosssection $\sigma^{(i)}$ of each isotope found in the samples with its ⁴⁵⁹ reported atomic abundance $f_{abun}^{(i)}$, as seen in eq. (2).

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$$\sigma_w^{(i)} = f_{\text{abun}}^{(i)} \cdot \sigma^{(i)}$$
 (2)486 (2)486

⁴⁶¹ Then $f_{\rm imp}$ was calculated, point-wise with respect to⁴⁸⁸ ⁴⁶² the neutron energy, from the ratio of eq. (3) where the⁴⁸⁹ ⁴⁶³ sum in the denominator includes the isotopes reported⁴⁹⁰ ⁴⁶⁴ in table I as well as the ²³⁶U daughter nucleus¹ from the⁴⁹¹ ⁴⁶⁵ α -decay of ²⁴⁰Pu. ⁴⁹²

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$$f_{\rm imp} = \frac{\sigma_w^{240} P u}{\sum_i \sigma_w^{(i)}}$$
 (3)⁴⁹⁵₄₉₆



FIG. 8. The f_{imp} correction factor (top panel) applied to₅₁₃ 240 Pu with respect to the neutron energy. The bottom panel shows the total estimated uncertainty which was obtained ⁵¹⁵ from the diagonal elements of the covariance matrix.

The uncertainty in the correction was determined by 518 467 means of the covariance matrix provided by EC-JRC-519 468 Geel. As far as the ENDF/B-VIII.0 cross sections were 520 469 concerned, the main contribution to the uncertainty was₅₂₁ 470 the 239 Pu(n,f) cross section, since it was the contami-471 nant that mainly contributed to the fission yield. The 472 ENDF/B-VIII.0²³⁹Pu(n,f) cross section was evaluated 473 with an 1.4% uncertainty above 2.5 keV, therefore it was 474 considered negligible compared to the uncertainties of the 475 atomic abundances. Below 2.5 keV, the ENDF/B-VIII.0 476 library reports uncertainties of the order of a few per-477 cent (< 4% at a 2 bins/decade binning) which although 478 non-negligible, was not included in the covariance matrix 479 because its component relies on evaluations which can 480 change in the future, therefore only experimental com-481 ponents were propagated. 482

⁴⁸³ In the case of the uranium samples, the corresponding ⁴⁸⁴ correction was negligible.

4. Counting losses

Below the fission threshold, up to about 1 MeV, the recorded fission rate did not exceed 1 MHz concerning the plutonium and uranium samples. The analytical correction formulae proposed by Coates [43] and Moore [44] were applied to the recorded fission counts which practically yielded identical corrections. Correction factors less than 0.5% and 25% were estimated in the 9 meV - 300 keV and 300 keV - 1 MeV regions respectively, concerning ²⁴⁰Pu. For ²³⁵U, a 0.6% correction was estimated at 56 meV, where the fission rate peaked in the thermal region. An average 1% correction was applied up to 20 keV while up to 1 MeV, the estimated counting losses progressively reached 16%. The corresponding correction for ²³⁸U was practically negligible.

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Above 1 MeV, the expected instantaneous counting rate reached several MHz and resulted in significant pileup that was observed in the reconstructed counting spectra. Indeed, between 850 keV and 10 MeV (fig. 3 and 5) signals with systematically higher amplitudes were reconstructed, which is attributed to pile-up effects. The analytical methods used below 1 MeV were not able to provide realistic corrections, therefore a new methodology was developed [45] to treat such cases based on two approaches: (a) exponential decay fits in experimental waiting time distributions as shown in fig. 9 and (b) correction functions predicted from detector emulation devices. It has to be mentioned that this methodology can also account for an insufficient signal reconstruction which can occur at high counting rates. It was demonstrated that both approaches provide compatible corrections for counting rates up to 2 MHz, however the uncertainty of method (a) is higher. In the present measurement, the fission rate in ²⁴⁰Pu was higher than 2 MHz, therefore $f_{\rm DT}$ was estimated by means of fitting waiting time distributions, yielding a correction factor that varied from 1.44 up to 2.26 with 10% uncertainty.



FIG. 9. Exponential fits in waiting time distributions are a useful experimental tool in estimating counting losses by calculating the integral below the extrapolated fitting function [46].

For the uranium samples the correction function de-

¹ About 0.04% of the initial ²⁴⁰Pu has decayed to ²³⁶U after 3.5 y from the sample characterisation when the measurement took place. 522

scribed in ref. [45] was used. The correction factors that 557 523 were calculated with a 3% uncertainty, did not exceed⁵⁵⁸ 524 1.62 and 1.31 for the 235 U and 238 U, respectively. Fi-559 525 nally, in fig. 10 the correction factors that were applied 526 to the recorded fission yield, are shown. 560 527

It has to be noted that above 6 MeV, the waiting time₅₆₁ 528 distributions lacked sufficient statistical accuracy which 562 529 was a limiting factor for the highest reachable neutron₅₆₃ 530 energy. In addition, concerning the 01 and 03 targets, the564 531 signal reconstruction above 4 MeV was not possible since₅₆₅ 532 the γ -flash subtraction could not be applied at higher 566 533 energies. In addition, above 3 MeV the trends in the₅₆₇ 534 correction factors shown in fig. 10 are attributed to₅₆₈ 535 counting losses not only due to pile-up effects, but to 536 inefficient signal reconstruction. 537



FIG. 10. Estimated correction factors for counting losses. Below 1 MeV the methodology proposed by Coates [43]/Moore [44] was applied while above, the correction was based on ref. [45]. Average correction factors are shown per 0.5 MeV, above 1 MeV.

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2.4

2.2

²⁴⁰Pu-04 ²⁴⁰Pu-03

²⁴⁰Pu-01

Miscellaneous corrections 5.

The remaining correction factors were either estimated 539 to be negligible or did not require a complicated analysis, 540 however a brief discussion will follow on their calculation. 541 a. Self-absorption of fission fragments: Emitted fis-542 sion fragments deposit an amount of their kinetic energy 543 in the sample. A fraction of those might then produce 544 a signal below the detection threshold, thus the fission 545 yield is underestimated. To estimate the amount of these 546 fission fragments, the Monte Carlo simulations described 547 in $\rm III\,B\,2$ were used. A fraction that did not exceed 0.1%548 was estimated with an uncertainty that is defined by the 549 uncertainty of the reported masses and has negligible574 550 contribution to the final cross section uncertainty. Nev-575 551 ertheless, at high neutron energies the fission fragment⁵⁷⁶ 552 angular distribution (FFAD) might have an effect on the₅₇₇ 553 self-absorption and thus on the detection efficiency, as⁵⁷⁸ 554 demonstrated in refs. [47–49]. In the present case, thesa 555 Monte Carlo simulations described in III B 2 were used₅₈₀ 556

and the fission fragments were propagated towards the gas at angles ranging from $0^{\circ} - 90^{\circ}$. The simulations showed that the effect on the correction can be neglected.

b. Neutron beam attenuation: The neutron beam attenuation in the detector stack layers (fig. 11), was taken into account using Beer-Lambert's attenuation law and ENDF/B-VIII.0 (n,tot) cross sections (σ_{tot}). According to the configuration shown in fig. 11, the beam with an I_0 intensity, that exits ²³⁵U, suffered successive losses when crossing a layer with $n \text{ atoms/cm}^2$, described by the ratio seen in eq. (4), where *i* denotes each layer from the exit of ²³⁵U up to the corresponding fission foil.

$$\frac{f_{\text{shield}}}{f_{\text{shield}}^{(\text{ref})}} = \exp\left\{\sum_{i} n_i \cdot \sigma_{tot,i}\right\}$$
(4)

The neutron transport in the gas was neglected due to its negligible mass, therefore it is not visible in fig. 11, and Kapton was assumed to be pure 12 C, which accounts for 70% of Kapton [50].



FIG. 11. The neutron self-shielding correction was based on the Beer-Lambert law and ENDF/B-VIII.0 (n,tot) cross sections for the materials seen in the figure.

The estimated correction factors can be seen in fig. 12. It has to be noted that the correction in 238 U was not applied below 1 MeV due to the absence of statistics. In addition, the uncertainty of this correction, depends mainly on the uncertainty of the evaluated cross sections and was estimated to be less than 2%, since the number of atoms was known with an accuracy better than 1%.



FIG. 12. Correction factors for neutron beam attenuation 611 that were applied to 240 Pu and 238 U. 612

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c. Spontaneous fission: To estimate the contribu-616 581 tion of spontaneous fission and cluster decay, the beam-617 582 off spectra were used. It was experimentally shown that⁶¹⁸ 583 per proton bunch (fig. 13) less than 0.4% of the recorded⁶¹⁹ 584 counts were attributed to spontaneous fission and clus-620 585 ter decay events. The uncertainty in this case was esti-621 586 mated to be 5% based on the statistical uncertainty of the622 587 recorded spontaneous fission events in the longest beam-623 588 off run, which corresponded to 50000 proton bunches.624 589 It has to be mentioned that the branching ratio of clus-590 ter decay is appreciably smaller than spontaneous fission, 591 therefore it was neglected in the correction. 592



FIG. 13. Comparison between beam-on and -off spectra recorded from the most massive ²⁴⁰Pu sample. The contribution of spontaneous fission was considered negligible. Spectra are normalised to the number of triggers for a direct comparison.

⁵⁹³ *d. Photo-fission:* To estimate the contribution of ⁶²⁹ ⁵⁹⁴ photo-fission events, Monte Carlo simulations were used. ⁶³⁰ ⁵⁹⁵ More specifically, the simulated photon fluence from the ⁶³¹ ⁵⁹⁶ spallation process was used, along with the ENDF/B-⁶³² ⁵⁹⁷ VIII.0 (γ , f) cross sections in order to calculate the ex-⁶³³ ⁵⁹⁸ pected reaction rate. Photo-fission events were estimated ⁶³⁴ ⁵⁹⁹ to contribute less than 0.2% in the worst case. ⁶³⁵

6. Neutron flux

In the resolved resonance region, the 240 Pu(n,f) cross section was calculated using the EAR2 evaluated flux [32]. The flux of the vertical neutron beam is given at the floor level of the bunker, therefore a normalisation factor was applied to estimate the flux at the sample position, which was determined by the neutron flux obtained from 235 U.

The neutron flux was calculated using 235 U from 9 meV up to 6 MeV, excluding the 1 eV - 2 keV resonance region. Then, the neutron flux from 238 U was also calculated in order to benchmark the flux calculated from 235 U. As shown in fig. 14, the agreement was quite satisfactory in the MeV region, indicating that the absolute flux value was properly calculated.

Moreover, the flux was also calculated using the data obtained from SiMon2 and was normalised to 235 U at the thermal peak (56 meV). As shown in fig. 14, the agreement in the overlapping energy region between SiMon2 and 235 U was quite satisfactory, indicating a proper reconstruction of the shape of the neutron spectrum.

The next step was to normalise the evaluated flux at the thermal peak and to examine the agreement concerning the shape of the neutron flux. As illustrated in fig. 14, an overall agreement was observed.



FIG. 14. The neutron flux calculated from 235 U, 238 U and Si-Mon2 was found in satisfactory agreement with the evaluated and the simulated ones.

Finally, to benchmark the normalisation, the n_TOF simulation pool was used. Neutrons that were scored at the exit of the spallation target, were propagated towards EAR2 using an optical transport, to the position of 235 U. As shown in fig. 14, the simulated flux was in agreement at the thermal peak with the 235 U , the evaluated and the SiMon2 flux, indicating the consistency obtained by the redundant determination of the neutron flux.

As a result, the normalised evaluated flux was used to calculate the 240 Pu(n,f) cross section in the resolved resonance region.

In addition, the simulations were used to estimate the decrease of the neutron flux during its propagation. The flux on each fission foil was calculated and an average drop of 0.24% per cm was estimated and taken into account in the analysis of the flux ratio. Finally, table II summarises the correction factors and their corresponding uncertainties.

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C. Analysis benchmark

Prior to reporting the final results, a benchmarking procedure was adopted. First of all, the data from the reference foils were used to reproduce the 238 U(n,f) neutron standard. As shown in fig. 15, the 238 U(n,f) cross section was calculated with reference to 235 U(n,f) and a satisfactory agreement with the ENDF/B-VIII.0 evaluation within less than 3% was achieved.



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FIG. 15. The 238 U(n,f) cross section that was calculated with 680 reference to the 235 U(n,f) one was in a satisfactory agreement 681 with the ENDF/B-VIII.0 evaluation. 682

Finally, an overall agreement within uncertainties was₆₈₅ observed between the corrected counting spectra for each sample, therefore the reported cross section was the weighted average of the individual ones.

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IV. RESULTS AND DISCUSSION

The 240 Pu(n,f) cross section was obtained in a broad 656 energy range that spanned from 9 meV up to 6 MeV (fig. 657 16), covering almost 9 orders of magnitude in neutron 658 energy, illustrating the impressive capabilities of EAR2 659 for fission measurements. It has to be noted that the con-660 version from time-of-flight to the incident neutron energy 661 was made by using an effective flight path L, that was es-662 timated with the methodology described in ref. [51]. The 663 effective flight path was found to be 19.5 m for ^{235}U and 664 0.017 m were added for each successive fission foil, which 665 corresponds to the geometric spacing which was accu-666 rately known within 0.1%. The uncertainties shown in 667 fig. 16 correspond to the statistical uncertainties, after 668 the application of the correction factors. 669



FIG. 16. The 240 Pu(n,f) cross section that was derived in the present work spanned across a wide range in neutron energy, from 9 meV up to 6 MeV.

A. Thermal region

In the thermal region, only two measurements were reported in EXFOR, which were discrepant and with a high uncertainty as described in IB. The derived cross section between 9 – 100 meV is shown in fig. 17 and corresponds to the only available time-of-flight data set in literature. The present data set is in a better agreement with the data point by Eastwood compared to the corresponding one by Pratt. In addition, a fair agreement within uncertainties was observed between CENDL-3.1 [52] and JEFF-3.3 [53] while ENDF/B-VIII.0 [54] was systematically lower by about 15%. Finally, JENDL-4.0 [53] was underestimating the cross section by about a factor of 2. The present data-set is expected to provide additional material for future evaluations, thus reducing the discrepancies among the libraries.



FIG. 17. The ²⁴⁰Pu(n,f) cross section between 9 - 100 meV in comparison with the experimental data Eastwood et al. [14] and the evaluation by Bouland et. al [19] as well as the most common evaluation libraries [52–55].

TABLE II. List of the correction factors that were applied to the fission yields along with the corresponding uncertainties (when estimated). In cases of energy dependent correction factors, a reference to a figure is given. When a single correction factor is given, it corresponds to all fission foils, unless a hyphen is used in the corresponding row.

Sample				Correction	1 factor			
_	$f_{ m amp}$	$f_{ m imp}$	$f_{\rm DT}$	$f_{ m abs}\ (\%)$	$f_{ m shield}$	$f_{ m SF}, f_{ m CD}$ (%)	$f_{\gamma f} \ (\%)$	Φ ratio
²³⁵ U ²⁴⁰ Pu-04 ²⁴⁰ Pu-01 ²⁴⁰ Pu-03 ²³⁸ U	$\begin{array}{c} 1.040(2) \\ 1.070(4) \\ 1.115(10) \\ 1.090(9) \\ 1.020(3) \end{array}$	- Fig. 8 -	Fig. 10	< 0.100(1)	- Fig. 12	< 0.40(2)	< 0.2	$\begin{array}{c} 1.000 \\ 0.996 \\ 0.992 \\ 0.988 \\ 0.984 \end{array}$

В. Resonance at 1.05 eV

ported by Tovesson et al. [22].

1.0

Cross section (b) 9.0 70 8.0 8.0

0.5

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Although a comparison in the resolved resonance re-687 gion is only possible through resonance parameters, a 688 brief discussion will follow regarding the first resonance 689 in the ²⁴⁰Pu(n,f) cross section at ~ 1 eV. The only avail-690 able data set was reported in 1956 by Leonard Jr. et 691 al. [17] with poor resolution. The efficient α -background 692 suppression and high instantaneous flux allowed to de-693 rive a high resolution cross section, as shown in fig. 18, 694 demonstrating the impressive capabilities of EAR2 as a 695 spectrometer in low energy fission studies. Concerning 696 the cross section in the resolved resonance region, a dis-697 cussion will follow in section V. 698



The high resolution 240 Pu(n,f) cross section at₇₁₄ FIG. 18. the 1.05 eV region, demonstrates the impressive capabilities $_{715}$ of EAR2 in low energy fission measurements. 716

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С. Unresolved resonance region

In the unresolved resonance region, between a few keV_{721} 700 and a few tens of keV, clusters of overlapping resonances722 701 were resolved that correspond to coupling between class-I₇₂₃ 702 and class-II states. A typical example is shown between₇₂₄ 703 10 and 30 keV (fig. 19). The present data is in agree-725 704 ment with high resolution data that exist in literature₇₂₆ 705 [18, 20], however, evaluated cross sections do not present₇₂₇ 706 any structures. The only exception is ENDF/B-VIII.0,728 707 which was clearly based on the lower resolution data re-729 708

1981, Budtz-Jorgenser Present work CENDL-3.1 2009. Tovesson JENDL-4.0 1984, Weston ENDF/B-VIII.0 JEFF-3.3



gion. It is evident that despite the availability of high resolution data, the observed structures are only considered in the ENDF/B-VIII.0 evaluation [54].

Fission threshold D.

At sub-barrier neutron energies, structures that could be attributed to vibrational bumps were observed (e.g. around 100, 140, 280, 350, 650, 785 keV), as shown in fig. 20. An overall agreement with the latest reported data by Salvador-Castineira et al. [21] was observed. In addition, an overall agreement within uncertainties was observed with the data by Laptev et al. [23], Meadows [56] and Nesterov et al. [57] while the data-set reported by Tovesson et al. [22] was systematically higher by 10 -15%, depending on the energy range.

The evaluations are in overall agreement with each other and provide cross sections that lie between the experimental data. The present data-set, is expected to provide useful additional material to correct the future evaluations. In addition to the previous comparison, the evaluated cross sections did not predict the subthreshold structures that were observed in the present data. The only exception is JEFF-3.3 which shows some structures, however, they seem unrealistically pronounced.



FIG. 20. The cross section in the 100 keV - 1 MeV region. An overall agreement with reported data-sets was observed apart from the one reported by Tovesson et al. [22].



FIG. 21. Comparison of the cross section in the 1 - 6 MeV region with the respective statistical uncertainties.

E. First chance fission

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In the energy region between 1 and 6 MeV, the derived⁷⁶⁶ 731 cross section is in agreement within uncertainties with the⁷⁶⁷ 732 data reported by Salvador-Castineira et al. [21], Laptev⁷⁶⁸ 733 et al. [23] and Meadows [56], as shown in fig. 21. Up⁷⁶⁹ 734 to 2.7 MeV, the systematic discrepancy concerning the⁷⁷⁰ 735 data by Tovesson et al. [22] was still present, while above771 736 4 MeV, the uncertainty in the present data-set did not⁷⁷² 737 allow to draw any conclusions. The same remarks were⁷⁷³ 738 also valid regarding the data-set by Kari et al. [58–60],774 739 since it is in agreement with the one by Tovesson et al.775 740 [22].776 741

An interesting dip around 2.5 MeV was observed not
only in the present work, but also in the data of Laptev778
et al. [23], Cance et al. [61] and Kazarinova et al. [62].779
Its origin has not yet been understood, therefore further780
investigation would be justified. 781

Finally, concerning the evaluations, an overall agree-747 ment with JENDL-4.0 was observed across the first 748 chance fission plateau. A slightly worse agreement be-749 tween the present data and CENDL-3.1 was observed, 750 due to the underestimated evaluated cross section be-751 tween 2.3 - 3.6 MeV. JEFF-3.3 overestimated the fission 752 cross section and exhibited an overall smoother behaviour 753 than the one observed in the present work and previous 754 experimental data. Finally, ENDF/B-VIII.0 lies between 755 the reported data, following the trend of the data by 756 Tovesson et al. [22]. 757

It has to be noted that the larger statistical uncertainties in the 4 – 6 MeV energy region are attributed to the fact that the cross section was calculated using only one ²⁴⁰Pu sample, since in all the others the γ -flash subtraction and counting loss correction could only be applied up to 4 MeV.

F. Covariance propagation

The cross section calculation was accompanied by the estimation of the uncertainties and correlations. In this respect only non-negligible components were taken into account such as the fission counts, $f_{\rm amp}$, $f_{\rm imp}$, the mass m, the neutron flux in the 800 meV - 2 keV region and $f_{\rm DT}$ above 1 MeV. The fission counts and the neutron flux were considered to have a fully uncorrelated contribution to the covariance matrix while $f_{\rm amp}$ and m have correlated components. Regarding $f_{\rm imp}$, its covariance matrix was calculated separately assuming that the biggest contribution were the atomic abundances, neglecting therefore the uncertainty of the known 239 Pu(n,f) cross section.

The covariance matrix was used to estimate the total uncertainty, which is reported in Appendix B and the correlations in the cross section. The estimated correlations are illustrated in fig. 22.



FIG. 22. The correlations of the 240 Pu(n,f) cross section, which were calculated by means of covariance propagation.

V. RESONANCE ANALYSIS

Between 1 eV and 10 keV a total of 25 fission reso-⁸³⁶
nances were resolved with sufficient statistical accuracy.
Due to the nature of the double humped fission barrier,
fission resonances are grouped resulting in a significant⁸³⁷

⁷⁸⁷ fluctuation of fission widths which justifies the analysis

788 of only strong resonances.

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A. Details of the resonance analysis

The resolved resonances were analysed by means of $^{\rm 840}$ 790 the SAMMY code [63] implementing the R-Matrix for- $^{\rm 841}$ 791 malism. The present analysis was performed under the⁸⁴² 792 following assumptions: (a) the Reich-Moore approxima-⁸⁴³ 793 tion was selected, (b) Doppler broadening was taken into⁸⁴⁴ 794 account using the free gas model (T=300 K), (c) multiple $^{\rm 845}$ 795 scattering effects were neglected due to the small thick-796 ness of the samples compared to the mean neutron path, 797 (d) broadening due to the time resolution of the spec-798 trometer was used taking into account both the proton⁸⁴⁹ 799 burst width (7 ns RMS) and the neutron transport within $^{\rm 850}$ 800 the target-moderator assembly which was obtained from⁸⁵¹ 801 Monte Carlo simulations [64]. 802

As far as the calculation is concerned, resonances were⁸⁵³ 803 considered to be s-waves (l = 0). In addition, since fis-804 sion widths (Γ_f) in a non-fissile nucleus are appreciably⁸⁵⁵ 805 smaller than the neutron (Γ_n) and capture (Γ_{γ}) widths, 806 the present data could not provide Γ_n and Γ_{γ} . Therefore, 807 up to 5.7 keV, Γ_n and Γ_γ were fixed to the values pro-808 posed by Bouland et al. [19], which are the ones adopted 809 by ENDF/B-VIII.0 and JEFF-3.3, while the neutron en-⁸⁵⁷ 810 ergy E_n and Γ_f were fitted. 811

Above 5.7 keV, in the absence of resonance parame-⁸⁵⁹ 812 ters in literature, a constant radiation width of 31.8 meV 813 was adopted from ENDF/B-VIII.0. Despite the existence 814 of transmission data by Gwin [65], neutron widths were 815 also absent in literature. In this respect, a constant re-816 duced neutron width was used, which was calculated con-817 sidering a mean level spacing $\langle D \rangle = 12.06(60)$ eV and 818 the strength function $S_0 = 1.032(71)10^{-4}$ proposed by 819 Bouland et al. [19], using eq. (5). 820

$$g_J \Gamma_n^0 = S_0 \langle D \rangle \sqrt{E_n} \tag{5}$$

where g_J is the spin factor and in the present work had a value of 1 since only s-waves were considered.

The neutron energy was fitted using a fudge factor of 824 0.01 = 1% and an overall agreement with the evaluation 825 of Bouland et al. [19] was observed. On the contrary, 826 fission widths were left practically free to vary using a 827 fudge factor of 10. The uncertainty in the varying param-828 eters was provided by SAMMY as the uncertainty of the⁸⁶⁰ 829 Propagated Uncertainty Parameters (PUP in SAMMY 830 831 notation).

It has to be noted that the broadening induced by the⁸⁶² neutron moderation did not allow the determination of⁸⁶³

 Γ_f unless it was much greater than Γ_n and Γ_γ , therefore the fission kernels F_K will be reported, which were calculated using eq. (6).

$$F_K = g_J \frac{\Gamma_f \Gamma_n}{\Gamma_f + \Gamma_n + \Gamma_\gamma} \tag{6}$$

B. Results and discussion

The discussion that follows concerns resolved resonances with sufficient statistical accuracy and fission kernels with an uncertainty less than 30%. Other, perhaps doubtful, resonances were accepted in the analysis and their parameters, which were calculated with an uncertainty higher than 30% can be retrieved in Appendix A where the parametrisation of the present cross section is provided.

In the following figures, a comparison is presented (top panels) between the experimental data, the fits obtained by SAMMY and the evaluated cross section by Bouland et al. [19] which was broadened using the response function of EAR2. In the bottom panels, the residuals between the SAMMY fits and the experimental data are given. In table V the fission kernels are reported, while a full parametrisation of the cross section is given in Appendix A.

1. Resonance at $1.05 \ eV$

The extracted Γ_f at the first resonance at 1.05 eV was 0.0077(4) meV, which is roughly 6% smaller than the 0.0081(15) meV reported by Bouland et al. [19].



FIG. 23. Resonance at 1.05 eV where a fission width with a 5% uncertainty was derived.

2. Energy region between 19 - 400 eV

In this energy region, five typical examples of fission resonances are presented in fig. 24. The analysis of the second isolated resonance at 20.4 eV (fig. 24a), provided

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a fission width $\Gamma_f = 0.29$ meV, that is higher by 30%, 864 compared with the 0.20 meV proposed by Bouland et 865 al. The uncertainty in Γ_f , mainly attributed to statis-866 tics, cannot justify this discrepancy. In addition, in this 867 energy region, the corrections were quite small, there-868 fore the present fission width is considered to be accu-869 rate. The same was observed for an isolated resonance 870 at 38.4 eV, where the extracted fission width is 0.017 meV 871 and the evaluated one 0.0095 meV. The 45% discrepancy 872 clearly exceeds the 20% statistical uncertainty. 873

A resonance at 152 eV was also resolved, with a fission width of 0.38 meV, 5% higher than the corresponding value of Bouland et al. who reported Γ_f equal to 0.36 meV. The statistical uncertainty in the Γ_f calculation of the present work was of the order of 6%, therefore both values were in agreement within uncertainties, as illustrated in fig. 24b.

Two isolated resonances were also resolved at 260.5 881 and 286.9 eV, as shown in fig. 24c. The resonance anal-882 vsis yielded fission widths of 0.12 and 0.37 meV respec-883 tively while the corresponding ones from Bouland et al. 884 were 0.09 and 0.38 meV, respectively. In the former res-885 onance, a 25% discrepancy was observed which could be 886 attributed to the 30% statistical accuracy while in the 887 latter the present data confirm Bouland's et al. evalua-888 tion. 889

Finally, an 8% discrepancy was observed for the 405890 eV resonance for which Bouland et al. proposed $\Gamma_f =$ 891 0.47 meV compared to the 0.43 meV extracted from the 892 present work. In this case the statistical uncertainty was 893 of the order of 25%, therefore both fission kernels were 894 compatible within uncertainties, as illustrated in fig. 24d. 895 All in all, fair agreement within uncertainties was ob-896 served compared to the evaluation by Bouland et al. 897 The limitation of statistical accuracy cannot provide a 898 clear confirmation of the resonance parameters reported 899 by Bouland et al., however, the discrepancy observed at 900 the 20.4 eV resonance indicates an underestimation of 901 the fission cross section, therefore further investigation is 902 recommended. 903

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3. Resonances with large fission widths

⁹⁰⁵ In fission resonances where the fission width is no-⁹⁰⁶ tably higher than Γ_n and Γ_γ , eq. (6) is reduced to eq. ⁹⁰⁷ (7), which implies that the resonance area is sensitive to ⁹⁰⁸ the neutron width. In addition the determination of the ⁹⁰⁹ fission width can be achieved by transmission measure-⁹¹⁰ ments, since in this case the total width Γ is practically ⁹¹¹ equal to Γ_f .



$$F_K \approx g_J \Gamma_n \tag{7}$$

Among such resonances two of them were resolved at 782
and 1402 eV. Apart from Bouland et al. [19], Guerrero
et al. [66] provided resonance parameters, analysing capture data from n_TOF [67] and transmission data from
Kolar and Böckhoff [68].



FIG. 24. A few resonances that were resolved in the 19 - 400 eV region. An overall agreement within uncertainties was observed with the evaluation by Bouland et al. [19], except for the resonance at 20.4 eV. See text for further details.

In these resonances, the radiation widths proposed by Bouland et al. and Guerrero were adopted along with the common fission widths they used. The neutron widths were left free to vary.

a. Resonance at 783 eV: Concerning the 783 eV 922 resonance, which can be seen in fig. 25a, Bouland et 923 al. [19] proposed a neutron width which was equal to 924 3.83 meV and a 31.2 meV radiation width. Guerrero 925 et al. [66] proposed a radiation width of 36.6 meV and 926 the analysis of the transmission data of Kolar and and 927 Böckhoff, vielded a width of 6.26 meV. Both reported a 928 fission width $\Gamma_f = 1858$ meV which was adopted in this 929 930 work. The present analysis yielded a 3.3 meV fission kernel using Γ_{γ} and Γ_{f} from Bouland et al., which was 931 14% smaller than the evaluated value. The Γ_n that was 932 derived using Guerrero's Γ_{γ} was 3.88 meV, which practi-⁹⁵¹ 933 cally confirms the neutron width by Bouland et al. The 934 Γ_n extracted from the analysis of the transmission data⁹⁵² 935

 P_{355} I $_n$ extracted from the analysis of the transmission data⁹⁵² was 53% larger than the one derived from the present⁹⁵³ analysis. ⁹⁵⁴

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The neighbouring resonances were analysed using the procedure described in the beginning of section VA, therefore the Γ_f were fitted. The results are reported in table V.

b. Resonance at 1402 eV: The neutron widths pro-942 posed by Bouland et al. [19] and Guerrero et al. [66] were 943 9.83 and 10.02 meV, respectively while Γ_{γ} was practically 944 the same (31.8 and 31.0 meV, respectively). Both used 945 a fission width of 2085.5 meV which was adopted in the 946 present work. The fission kernel that was estimated from 947 the present work was 9.4 meV and in agreement with the 948 values derived by Guerrero et al. [66] and Bouland et al. 949 [19], as illustrated in fig. 25b. 950



(a) The cross section close to the 782 eV resonance



FIG. 25. Cross section in regions where resonances with high fission widths were observed.

4. Resonances beyond evaluations

Bouland et al. extracted resonance parameters up to 5.7 keV, however in the present data prominent resonance structures were resolved at higher energies, even up to 20 keV. An example is shown in fig. 26 in the 6.2 - 10.2 keV energy region. The corresponding parametrisation of the cross section is given in Appendix A by means of Reich-Moore resonance parameters. It has to be noted that in this overlapping region, resonances are Ericson type fluctuations and the fission kernels reflect some fission mixtures of the coherent mixing of a set of overlapping compound states.



FIG. 26. Prominent resonance structures that were observed between 6.2 and 10.2 keV. A parametrisation of the cross section is provided in Appendix A using Reich-Moore resonance parameters.

C. Remarks on the resonance analysis

The resonance analysis that was presented demonstrated the capability of measurements in EAR2 in resolving fission resonances. Although the experiment was not originally designed to achieve the required statistical accuracy for resonance analyses, the parameters from the present data were in overall agreement with the evaluation by Bouland et al. [19], including fission and neutron

TABLE III. List of the fission kernels with a statistical uncertainty of less than 30%. Negative differences correspond to a smaller fission kernel compared to the corresponding one by 992 Bouland et al. [19].

Fission kernel 995					
		(meV)			996
E_n	Present	Relative	Bouland	Differen	ce
	work	uncertainty	et al. [19]		000
(eV)		(%)		(%)	990
1.06	0.00059(8) 14	0.00063	-6	-990
20.4	0.027(6)	20	0.019	35	1000
38.4	0.0078(7) 9	0.0043	59	1001
66.6	0.021(1)	5	0.016	25	1002
72.8	0.044(2)	5	0.041	8	1003
152.0	0.099(2)	2	0.094	6	1004
260.5	0.048(2)	4	0.038	26	1005
287.0	0.30(5)	17	0.30	-2	1006
405.0	0.33(6)	18	0.36	-8	1007
743.1	0.017(3)	18	0.040	-81	1007
750.3	8.2(2)	2	6.9	17	1000
778.1	0.020(1)	5	0.019	5	1009
783.1	3.3(6)	18	3.8	-14	1010
790.5	5.5(2)	4	5.7	-4	1011
1402	9.4(1)	1	9.6	-2	1012
1842	8.2(3)	4	7.7	6	1013
1902	3.2(2)	6	2.8	12	1014
1917	20(2)	10	21	-4	1015
1948	7.5(2)	3	6.0	22	1016
1955	17.8(4)	2	20	-13	1017
2033	10.3(25)	24	6.6	43	1010
2698 ^a	82(8)	10	77	6	1010
6551	12.5(3)	2	—	-	1019
7508	64.5(5)	1	—	_	1020
8098	111(9)	8	—	_	1021

^a Resonance energy was found higher by 4 eV

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widths. On top of that, new and/or more accurate res₁₀₂₆ 971 onance parameters could be proposed. The resulting fis₁₀₂₇ 972 sion kernels which were extracted with a statistical $\operatorname{accu}_{1028}$ 973 racy better than 30% are listed in table V, in comparison₁₀₂₉ 974 to the ones proposed by Bouland et al. 975 1030

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VI. CONCLUSION

The second experimental area (EAR2, 19m ${\rm flight}^{1033}$ 977 path) was commissioned in 2014 [25] in order to expand 978 the measuring capabilities of CERN's n_TOF facility in1034 979 studying reactions where high activity and/or low mass⁰³⁵ 980 samples are involved. In this respect, the first experiment⁰³⁶ 981 that was performed was the study of the 240 Pu(n,f) cross 982 section, which could not be completed in a previous mea-983 surement in the existing experimental area (EAR1, 185m¹⁰³⁷ 984 flight path) due to the detector deterioration induced by 985 the long exposure to the activity of the fission foils $[24]_{.1038}$ 986 The present measurement was successfully completed₀₃₉ 988

and yielded a cross section in a broad energy range from₀₄₀ 9 meV up to 6 MeV incident neutron energy, covering al-1041 989

most 9 orders of magnitude. This experimental campaign demonstrated the capabilities of EAR2 for measurements especially at neutron energies below the fission threshold where the limited amount of fission material makes the study of resonances and thermal cross sections challenging. The high instantaneous neutron flux which was delivered in a short time interval, compensated for this experimental limitation, thus appreciably reducing the intrinsic background from the α -activity and providing a sufficient fission rate to observe resonance structures.

These structures were analysed by means of SAMMY fits [63], incorporating the R-Matrix formalism. A total of 25 resonance kernels are reported although the experiment was not initially designed for sub-barrier fission. The majority of fission kernels is in agreement with evaluations [19], while three new values could be determined and recommended.

In the near-threshold region, resonance structures were also observed which correspond to overlapping class-II states but could not be analysed using the available statistical model codes.

Above the fission threshold, the high instantaneous fission rate resulted in appreciably large counting losses, which were estimated by means of a dedicated methodology that was applied to the fission counts [45]. The derived cross section is in agreement with the latest data-set by Salvador-Castineira et al. [21] and the time-of-flight data by Laptev et al. [23] but systematically smaller than the latest time-of-flight measurement by Tovesson et al. [22] and the ENDF/B-VIII.0 and JEFF-3.3 evaluations. An overall agreement was observed with the CENDL-3.1 and JENDL-4.0 evaluation libraries.

The present measurement is expected to provide additional material for the evaluated libraries while emphasizing the need for an additional study in the resolved resonance region. The further upgrade of the n_TOF spallation target is expected to offer an increased neutron flux and a significantly better resolution.

Finally, due to the substantially higher instantaneous flux especially near thermal energies, EAR2 is expected to facilitate the measurement of new fission cross section data concerning actinides which are important both in nuclear energy applications and fundamental research.

ACKNOWLEDGMENTS

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Appendix A: Reich-Moore resonance parameters

The resonance parameters that reproduce the reported cross section are given below. Each file line corresponds to the parameters of one resonance. From left to right the columns contain the energy, radiation, neutron and

fission widths of each resonance. The first five fictitious
resonances were adopted from Bouland et al. [19] and
were used to simulate the contributions of external resonances. The sign in the fission widths is used to indicate

the definite amplitude of fission.

TABLE IV: Resonance parameters that were used to parametrise the 240 Pu(n,f) cross section. The resonances were considered s-waves, therefore the resonance spins are J = 1/2.

Energy	Г	Г	Гс
(eV)	(meV)	(meV)	(meV)
$\frac{(0.1)^{-4}}{-4.070 \times 10^{3}}$	$\frac{(110,1)}{3,18\times10^1}$	$\frac{(110.7)^{4}}{3.55 \times 10^{4}}$	$\frac{(110.7)^{-3}}{3.37 \times 10^{-3}}$
-1.300×10^{3}	3.18×10^{1}	3.52×10^3	-4.31×10^{-2}
-3.050×10^{2}	3.18×10^{1}	2.14×10^2	4.00×10^{-2}
-7.010×10^{1}	3.18×10^{1}	3.09×10^2	-4.00×10^{-2}
-3.000×10^{0}	3.10×10^{1} 3.01×10^{1}	1.31×10^{0}	1.00×10^{-3}
1.058×10^{0}	2.91×10^{1}	2.45×10^{0}	7.65×10^{-3}
2.043×10^{1}	2.51×10^{10} 2 70 × 10 ¹	2.45×10^{-2} 2.75 × 10 ⁰	-2.90×10^{-1}
3.835×10^{1}	2.10×10^{10} 2.40×10^{10}	1.96×10^{1}	1.74×10^{-2}
4.175×10^{1}	2.10×10^{1} 2.55×10^{1}	1.00×10^{1} 1.74×10^{1}	7.11×10^{-3}
6.664×10^{1}	3.30×10^{1}	5.55×10^{1}	3.27×10^{-2}
7.277×10^{1}	2.64×10^{1}	2.17×10^{1}	9.21×10^{-2} 9.78×10^{-2}
9.078×10^{1}	3.08×10^{1}	1.33×10^{1}	-1.01×10^{-2}
9.249×10^{1}	2.83×10^{1}	3.00×10^{0}	-6.32×10^{-2}
1.050×10^2	2.85×10^{1}	4.62×10^{1}	-5.10×10^{-3}
1.217×10^2	3.36×10^{1}	1.49×10^{1}	8.70×10^{-2}
1.257×10^2	3.18×10^{1}	1.20×10^{-1}	-2.00×10^{-2}
1.308×10^2	3.09×10^{1}	1.79×10^{-1}	2.41×10^{-1}
1.351×10^{2}	3.29×10^{1}	1.83×10^{1}	4.83×10^{-2}
1.520×10^{2}	3.75×10^{1}	1.35×10^{1}	3.77×10^{-1}
1.627×10^2	2.91×10^1	8.48×10^{0}	1.58×10^{0}
1.698×10^{2}	3.10×10^1	1.32×10^{1}	-1.37×10^{-1}
1.858×10^2	3.10×10^1	1.58×10^1	8.95×10^{-3}
1.920×10^2	3.06×10^1	2.85×10^{-1}	-1.28×10^{-1}
1.956×10^2	3.18×10^1	1.60×10^{-1}	1.20×10^{-1}
1.974×10^2	3.18×10^1	1.60×10^{-1}	-1.20×10^{-1}
1.997×10^2	2.86×10^{1}	9.70×10^{-1}	1.37×10^{-1}
2.389×10^2	2.87×10^1	1.19×10^1	1.35×10^{-1}
2.605×10^2	3.28×10^1	2.23×10^1	-1.19×10^{-1}
2.869×10^2	3.20×10^1	1.35×10^2	-3.69×10^{-1}
3.049×10^2	3.39×10^1	7.37×10^0	2.12×10^{-1}
3.136×10^{2}	3.18×10^1	1.20×10^{-1}	-2.50×10^{-1}
3.181×10^{2}	3.22×10^1	5.23×10^{0}	3.21×10^{-1}
3.207×10^2	3.49×10^{1}	1.89×10^1	-3.26×10^{-2}
3.327×10^2	3.18×10^1	1.30×10^{-1}	2.49×10^{-2}
3.383×10^{2}	3.14×10^{1}	5.94×10^{0}	-4.57×10^{-3}
3.459×10^{2}	3.39×10^{1}	1.59×10^{1}	3.52×10^{-1}
3.635×10^{2}	3.88×10^{1}	3.16×10^{1}	1.37×10^{-1}
3.719×10^{2}	3.04×10^{1}	1.33×10^{1}	-1.35×10^{-1}
3.930×10^{2}	3.18×10^{1}	1.50×10^{-1}	-1.70×10^{-2}
4.050×10^{2}	3.24×10^{1}	1.03×10^{2}	-4.31×10^{-1}
4.189×10^{2}	3.09×10^{1}	$5.77 \times 10^{\circ}$	2.87×10^{-1}
4.457×10^{2}	3.14×10^{1}	1.84×10^{0}	-5.84×10^{-1}
4.498×10^{2}	3.22×10^{1}	1.61×10^{1}	1.47×10^{-1}
4.666×10^{2}	3.29×10^{1}	$2.65 \times 10^{\circ}$	$1.03 \times 10^{\circ}$
4.733×10^{2}	3.07×10^{1}	$4.11 \times 10^{\circ}$	1.00×10^{0}
4.938×10^{2}	3.15×10^{11}	5.35×10^{6}	-5.30×10^{-1}

TABLE IV – Continued from previous column

Energy	Γ_{γ}	Γ_n	Γ_f
(eV)	(meV)	(meV)	(meV)
4.989×10^{2}	3.63×10^{1}	1.85×10^{1}	2.08×10^{-1}
5.100×10^{2}	3.18×10^1	4.14×10^{-1}	6.40×10^{-2}
5.125×10^{2}	3.18×10^1	5.17×10^{-1}	-4.47×10^{-2}
5.145×10^2	3.36×10^1	2.09×10^1	-2.06×10^{-1}
5.263×10^2	3.18×10^1	9.61×10^{-1}	$1.00 imes 10^0$
5.308×10^{2}	3.18×10^1	6.77×10^{-1}	2.92×10^0
5.463×10^{2}	3.99×10^1	3.11×10^1	-9.97×10^{-2}
5.534×10^{2}	3.48×10^{1}	1.79×10^{1}	3.95×10^{-1}
5.665×10^{2}	3.38×10^{1}	3.14×10^{1}	-2.79×10^{-1}
5.844×10^{2}	3.18×10^{1}	1.15×10^{0}	3.61×10^{0}
5.966×10^{2}	3.72×10^{1}	5.42×10^{1}	1.22×10^{-1}
6.080×10^2	2.91×10^{1}	2.22×10^{1}	-9.02×10^{-2}
6.322×10^2	3.24×10^{1}	1.35×10^{1}	-4.07×10^{-1}
6.376×10^2	3.06×10^{1}	1.00×10^{1} 1.19×10^{1}	-1.16×10^{-1}
6.498×10^2	3.18×10^{1}	1.20×10^{0}	2.20×10^{0}
6.657×10^2	2.74×10^{1}	2.03×10^2	-3.59×10^{-1}
6.789×10^2	3.20×10^{1}	2.00×10^{1} 2.54×10^{1}	-1.31×10^{0}
0.103×10^{2} 7.121×10^{2}	3.20×10^{1} 3.18×10^{1}	1.33×10^{0}	3.26×10^{-1}
7.121×10 7.433×10^2	3.18×10^{1} 3.18×10^{1}	$1.03 \times 10^{-1.00}$	5.20×10^{-1} 5.60 × 10 ⁻¹
7.433×10 7.503×10^2	3.16×10^{-10}	1.01×10 6.05 × 10 ¹	1.36×10^{1}
7.503×10 7.580×10^2	3.20×10^{1}	$0.93 \times 10^{-5.82} \times 10^{0}$	-1.30×10^{-1}
7.389×10 7.782×10^2	3.20×10^{-10}	1.12×10^{0}	1.03×10 5.85 × 10 ⁻¹
7.763×10 7.820×10^2	3.10×10^{10}	1.12×10 2.22 $\times 10^{0}$	1.60×10^{3}
7.829×10 7.005×10^2	3.12×10^{-1}	3.33×10^{-1}	$-1.80 \times 10^{-1.80}$
7.903×10^{2} 8.102×10^{2}	$2.32 \times 10^{-2.32} \times 10^{1-1}$	2.32×10 2.20×10^2	-1.54×10^{1}
8.103×10^{2}	3.73×10^{-10}	2.20×10 1.11 × 10 ²	1.00×10^{-1}
8.200×10^{2}	2.98×10^{-2}	1.11×10 1.02×10^{0}	0.40×10 2 50 × 10 ⁰
8.333×10	3.18×10^{-1}	1.02×10^{-10}	-3.50×10^{-1}
8.430×10	3.30×10 2.47 × 10 ¹	9.48×10	1.24×10
8.330×10^{2}	3.47×10^{-101}	4.71×10 1.02×10^{0}	-3.33×10
8.080×10 8.764×10^{2}	3.18×10^{-1}	1.02×10^{1}	1.42×10^{-1}
8.704×10 8.017×10^2	3.29×10^{-1}	1.45×10	$(.08 \times 10)$
8.917×10^{-1}	3.23×10^{-1}	9.47×10^{-1}	-9.35×10^{-1}
9.000×10	3.18×10^{10}	1.00×10^{1}	-1.20×10 7.20 × 10 ⁻¹
9.040×10	3.48×10^{-1}	2.21×10	-7.32×10
9.089×10^{-10}	3.22×10^{-1}	7.79×10^{-1}	3.24×10^{-1}
9.152×10^{-2}	3.48×10^{-1}	3.59×10^{2}	-3.40×10^{-1}
9.435×10^{2}	3.27×10^{1}	1.23×10^{2}	-2.98×10^{-1}
9.584×10^{-2}	3.10×10^{1}	7.39×10^{12}	7.04×10^{-2}
9.700×10^{-2}	3.18×10^{12}	$1.00 \times 10^{\circ}$	$5.00 \times 10^{\circ}$
9.713×10^{2}	2.99×10^{10}	7.98×10^{4}	6.00×10^{-2}
9.792×10^{2}	3.18×10^{10}	$7.20 \times 10^{\circ}$	-4.37×10^{-1}
9.830×10^{2}	3.18×10^{1}	$1.00 \times 10^{\circ}$	4.80×10^{4}
9.919×10^{2}	3.18×10^{-1}	3.00×10^{-1}	2.67×10^{4}
1.002×10^{3}	2.98×10^{1}	9.73×10^{1}	$-1.56 \times 10^{\circ}$
1.012×10^{3}	3.18×10^{1}	2.00×10^{6}	$8.11 \times 10^{\circ}$
1.024×10^{3}	3.18×10^{1}	$5.23 \times 10^{\circ}$	8.05×10^{-1}
1.029×10^{3}	3.18×10^{1}	$2.00 \times 10^{\circ}$	$4.53 \times 10^{\circ}$
1.037×10^{3}	3.18×10^{1}	$2.00 \times 10^{\circ}$	$-2.17 \times 10^{\circ}$
1.042×10^{3}	2.97×10^{1}	1.21×10^{1}	-1.70×10^{-1}
1.046×10^{3}	3.18×10^{1}	$3.94 \times 10^{\circ}$	$2.47 \times 10^{\circ}$
1.051×10^{3}	3.18×10^{1}	$2.00 \times 10^{\circ}$	$7.49 \times 10^{\circ}$
1.072×10^{3}	2.91×10^{1}	1.09×10^{2}	-2.72×10^{-1}
1.077×10^{3}	3.18×10^{1}	$1.70 \times 10^{\circ}$	$-1.85 \times 10^{\circ}$
1.086×10^{3}	3.18×10^{1}	2.00×10^{0}	2.21×10^{6}
		Continued or	n next column

Continued on next column

TABLE IV – Continued from previous column

Energy	Γ_{γ}	Γ_n	Γ_f
(\mathbf{eV})	(meV)	(meV)	(meV)
1.100×10^{3}	3.41×10^{1}	8.00×10^{1}	-3.04×10^{-1}
1.116×10^{3}	3.18×10^1	2.57×10^0	-5.47×10^{-1}
1.129×10^{3}	3.09×10^{1}	4.98×10^{1}	6.72×10^{-1}
1.134×10^{3}	3.18×10^{1}	6.97×10^{0}	3.62×10^{-1}
1.101×10^{3} $1.1/3 \times 10^{3}$	3.10×10^{1}	4.22×10^{1}	-4.22×10^{-1}
1.140×10^{3}	3.10×10^{1}	1.22×10^{1}	6.87×10^{-1}
1.100×10 1.176×10^{3}	3.23×10^{-10}	2.50×10^{-1}	$-0.87 \times 10^{-0.00}$
1.170×10 1.100×10^3	3.10×10^{-10}	1.50×10^{2}	4.12×10^{-1}
1.180×10 1.101 10 ³	3.21×10	1.39×10 1.14 $\times 10^{2}$	1.11×10
1.191×10^{-1}	3.18×10	1.14×10	-1.40×10
$1.201 \times 10^{\circ}$	3.18×10^{11}	$2.00 \times 10^{\circ}$	$1.40 \times 10^{\circ}$
1.209×10^{3}	3.17×10^{1}	6.25×10^{1}	-3.50×10^{-1}
1.228×10^{3}	3.18×10^{1}	1.04×10^{1}	9.40×10^{-1}
1.237×10^{3}	3.18×10^{1}	1.12×10^{1}	7.82×10^{-1}
1.256×10^{3}	3.12×10^{1}	7.99×10^{1}	-4.52×10^{0}
1.281×10^{3}	3.18×10^1	4.20×10^0	-1.01×10^{0}
1.301×10^{3}	3.06×10^{1}	2.49×10^2	-2.67×10^{-1}
1.328×10^3	3.27×10^1	3.68×10^2	5.07×10^{-1}
1.345×10^{3}	3.18×10^{1}	2.49×10^{1}	1.09×10^{-1}
1.351×10^{3}	3.18×10^{1}	7.74×10^{0}	-2.72×10^{-2}
1.363×10^{3}	3.18×10^{1}	7.31×10^{0}	2.78×10^{-1}
1.377×10^3	3.12×10^{1}	6.61×10^{1}	-1.13×10^{-1}
1.377×10^{-1} 1.380×10^{-3}	3.12×10^{1} 3.18×10^{1}	1.47×10^{1}	6.30×10^{0}
1.369×10^{3}	3.10×10^{1}	1.47×10^{0}	0.30×10^{3}
1.402×10 1.400 × 10 ³	3.10×10^{10}	$9.38 \times 10^{-0.01}$	-2.09×10^{-10}
1.408×10^{3}	3.18×10^{-10}	9.91×10^{1}	-8.52×10
1.426×10^{3}	2.99×10^{12}	3.91×10^{1}	$5.49 \times 10^{\circ}$
1.429×10^{3}	3.18×10^{1}	1.57×10^{10}	$-1.02 \times 10^{\circ}$
1.442×10^{3}	3.18×10^{1}	$2.00 \times 10^{\circ}$	$6.74 \times 10^{\circ}$
1.450×10^{3}	3.18×10^{1}	2.69×10^{1}	$-1.49 \times 10^{\circ}$
1.451×10^{3}	3.15×10^{1}	2.74×10^{1}	-2.74×10^{0}
1.463×10^{3}	3.18×10^{1}	2.18×10^{1}	3.72×10^{-1}
1.466×10^{3}	3.18×10^1	$2.00 imes 10^0$	-2.73×10^{0}
1.475×10^{3}	3.18×10^1	2.00×10^0	-4.67×10^{0}
1.481×10^{3}	3.18×10^{1}	9.76×10^{0}	2.01×10^{0}
1.498×10^{3}	3.18×10^1	2.00×10^{0}	4.27×10^{0}
1.503×10^{3}	3.18×10^{1}	4.00×10^{0}	-1.11×10^{-1}
1.529×10^{3}	3.18×10^{1}	5.00×10^{0}	3.25×10^{0}
1.520×10^{3}	3.23×10^{1}	1.02×10^2	-1.60×10^{-1}
1.540×10^{3}	3.23×10^{-1} 3.17×10^{1}	1.02×10^{2} 1.62×10^{2}	4.11×10^{-1}
1.545×10^{3}	3.17×10^{-10} 3.18×10^{-10}	1.02×10^{-10}	3.61×10^{0}
1.555×10^{3}	3.10×10^{-10}	2.50×10^{-1}	-5.04×10^{-1}
1.304×10 $1.575 \dots 10^3$	3.04×10^{-10}	1.10×10 1.00×10^{2}	-1.20×10
1.575×10^{-1}	3.10×10	1.20×10	-5.10×10^{-1}
$1.582 \times 10^{\circ}$	3.18×10^{12}	$3.00 \times 10^{\circ}$	1.10×10^{-1}
1.600×10^{3}	3.18×10^{1}	2.00×10^{6}	-1.01×10^{-1}
1.610×10^{3}	3.18×10^{1}	3.60×10^{1}	7.25×10^{-1}
1.621×10^{3}	3.18×10^{1}	2.80×10^{1}	-3.70×10^{-1}
1.629×10^{3}	3.18×10^{1}	5.00×10^{0}	8.37×10^{-1}
1.643×10^{3}	3.17×10^1	1.11×10^2	9.52×10^{-1}
1.663×10^{3}	3.22×10^1	$6.91 imes 10^1$	-7.91×10^{-1}
1.667×10^3	3.18×10^1	6.00×10^0	1.12×10^{-1}
1.688×10^3	3.18×10^1	3.53×10^1	-1.89×10^{0}
1.707×10^{3}	3.18×10^{1}	4.50×10^{0}	1.43×10^{0}
1.724×10^{3}	3.14×10^{1}	8.44×10^{1}	1.79×10^{0}
1.749×10^{3}	3.18×10^{1}	3.00×10^{0}	-9.90×10^{-2}
1.742×10^3	3.18×10^{1}	2.48×10^{1}	7.81×10^{-1}
1., 12 / 10	3.10 / 10	2.10 / 10	
		Continued o	n next column

TABLE IV – Continued from previous column

Energy	Γ_{γ}	Γ_n	Γ_f
(eV)	(meV)	(meV)	(meV)
1.764×10^{3}	3.18×10^{1}	5.55×10^{1}	-2.68×10^{-1}
1.772×10^{3}	3.18×10^{1}	$9.73 \times 10^{\circ}$	9.92×10^{-2}
1.779×10^{3}	3.07×10^{1}	4.87×10^{2}	-4.53×10^{-2}
1.789×10^{3}	3.18×10^{1}	5.00×10^{0}	8.02×10^{-1}
1.811×10^{3}	3.18×10^{1}	5.00×10^{0}	7.41×10^{-1}
1.842×10^{3}	3.31×10^{1}	1.28×10^2	-1.10×10^{1}
1.853×10^{3}	3.18×10^1	3.39×10^{1}	-1.26×10^{0}
1.862×10^{3}	3.18×10^{1}	4.00×10^{0}	-1.01×10^{-1}
1.873×10^{3}	3.07×10^1	$8.07 imes 10^1$	4.14×10^{0}
1.886×10^{3}	3.18×10^1	5.00×10^0	-2.28×10^{0}
1.902×10^{3}	3.18×10^1	2.18×10^2	3.71×10^0
1.917×10^3	3.06×10^1	3.52×10^1	$8.70 imes 10^1$
1.939×10^{3}	3.10×10^{1}	1.31×10^{0}	-1.81×10^{3}
1.943×10^{3}	3.18×10^1	$7.93 imes 10^0$	1.74×10^1
1.948×10^3	3.18×10^1	8.58×10^1	1.12×10^1
1.955×10^3	3.08×10^1	2.76×10^2	-2.12×10^{1}
1.974×10^3	3.18×10^1	7.16×10^1	1.76×10^{0}
1.991×10^{3}	3.07×10^1	1.18×10^2	-4.79×10^{-2}
1.999×10^{3}	3.18×10^1	5.40×10^0	4.76×10^{-2}
2.017×10^3	3.15×10^1	5.50×10^1	-3.98×10^{-1}
2.023×10^{3}	2.87×10^{1}	6.02×10^{1}	1.83×10^{0}
2.033×10^{3}	3.23×10^{1}	1.11×10^2	1.46×10^{1}
2.038×10^{3}	3.18×10^{1}	5.00×10^{0}	1.16×10^{-1}
2.054×10^{3}	2.84×10^{1}	7.25×10^{1}	-5.76×10^{0}
2.061×10^{3}	3.10×10^{1}	5.00×10^{0}	8.57×10^{-2}
2.001×10^{3} 2.083 × 10 ³	3.09×10^{1}	9.91×10^{1}	-1.53×10^{-1}
2.000×10^{3} 2.097×10^{3}	3.18×10^{1}	1.00×10^{1}	6.94×10^{-1}
2.001×10^{3} 2 111 × 10 ³	3.18×10^{1}	1.00×10^{1} 1.39×10^{1}	-2.40×10^{0}
2.111×10^{3} 2.127×10^{3}	3.18×10^{1}	6.00×10^{0}	-7.72×10^{-1}
2.127×10^{3} 2 142 × 10 ³	3.18×10^{1}	8.00×10^{0}	-8.85×10^{-1}
2.142×10^{3} 2.155×10^{3}	3.18×10^{1}	1.41×10^{1}	1.36×10^{0}
2.100×10^{-2} 2.177×10^{-3}	3.10×10^{1} 3.18×10^{1}	1.41×10^{-1} 1.00×10^{1}	2.64×10^{0}
2.177×10 2.182×10^3	3.10×10^{1} 3.01×10^{1}	1.00×10^{-10} 8.06 × 10 ¹	1.20×10^{-1}
2.102×10^{3} 2.108×10^{3}	3.01×10^{1} 3.07×10^{1}	1.40×10^2	-5.09×10^{-1}
2.130×10 2.223×10^3	3.07×10^{1} 3.18×10^{1}	1.40×10^{-1} 1.20×10^{1}	-1.40×10^{-1}
2.223×10^{3}	3.18×10^{1}	$1.20 \times 10^{-0.00}$	-1.40×10 1.17×10^{-1}
$2.230 \times 10^{-2.230} \times 10^{-3}$	3.18×10^{1}	9.00×10^{-10}	0.16×10^{-1}
2.241×10 2.257×10^3	3.16×10^{10}	3.41×10 1.27×10^2	-9.10×10^{-1}
$2.237 \times 10^{-2.237} \times 10^{-3}$	3.10×10 2.18 × 10 ¹	1.37×10 1.00×10^{1}	4.21×10 1.17×10^{-1}
2.203×10	3.10×10^{-10}	1.00×10^{-100}	-1.17×10^{-1}
2.200×10	3.16×10^{-10}	8.00×10^{2}	1.04×10 4.02×10^{-1}
2.278×10^{3}	3.10×10^{-10}	3.98×10^{-10}	4.02×10 7 CA + 10 ⁻¹
$2.283 \times 10^{\circ}$	3.10×10^{-1}	2.79×10^{-2}	$(.64 \times 10^{-1})$
$2.291 \times 10^{\circ}$	3.09×10^{-1}	2.18×10^{-1}	-2.36×10^{-1}
2.303×10^{3}	3.18×10^{-1}	1.70×10^{1}	-1.00×10^{-1}
2.318×10^{3}	3.18×10^{12}	1.00×10^{1}	$-4.83 \times 10^{\circ}$
2.334×10^{3}	3.18×10^{1}	3.78×10^{1}	5.53×10^{-1}
2.351×10^{3}	3.18×10^{1}	3.85×10^{1}	1.29×10^{-1}
2.360×10^{3}	3.18×10^{1}	1.20×10^{1}	-1.27×10^{-1}
2.366×10^{3}	3.05×10^{1}	2.43×10^{2}	3.84×10^{-1}
2.373×10^{3}	3.18×10^{1}	$9.65 \times 10^{\circ}$	-1.03×10^{-1}
2.386×10^{3}	3.18×10^{1}	1.83×10^{1}	$1.34 \times 10^{\circ}$
2.405×10^{3}	3.18×10^{1}	2.50×10^{1}	-6.17×10^{-2}
2.416×10^{3}	3.18×10^{1}	6.84×10^{1}	5.86×10^{-1}
2.425×10^{3}	3.18×10^{1}	5.00×10^{0}	1.04×10^{-1}
		Continued o	n next column

TABLE IV – Continued from previous column

Energy	Γ_{γ}	Γ_n	Γ_f
(eV)	(meV)	(meV)	(meV)
2.434×10^{3}	3.04×10^{1}	2.15×10^2	3.00×10^{-1}
2.459×10^{3}	3.18×10^1	2.63×10^{1}	-4.30×10^{-1}
2.470×10^{3}	3.18×10^{1}	4.89×10^{1}	-2.10×10^{-1}
2.477×10^{3}	3.18×10^1	1.00×10^{1}	-5.15×10^{0}
2.484×10^{3}	3.18×10^{1}	2.14×10^{1}	3.39×10^{-1}
2.512×10^3	3.18×10^{1}	1.00×10^{1}	-1.13×10^{-1}
2.512×10^{3} 2.521×10^{3}	3.38×10^{1}	1.00×10^{2} 1.14×10^{2}	3.50×10^{-1}
2.521×10^{3}	3.30×10^{1} 3.18×10^{1}	1.14×10^{1} 1.50×10^{1}	1.04×10^{-1}
2.531×10 2.538×10^3	3.10×10^{-10}	1.50×10^{2} 2.87×10^{2}	-1.04×10^{-1} 2.10 × 10 ⁻¹
2.336×10 2.542×10^3	3.23×10^{-10}	2.67×10^{-1}	2.10×10^{-2}
2.345×10	3.16×10^{-10}	7.00×10^{-10}	9.00×10^{-1}
$2.549 \times 10^{\circ}$	3.26×10^{-1}	8.56×10^{-1}	-0.55×10^{-1}
2.563×10^{3}	3.18×10^{11}	7.00×10^{-1}	-1.00×10^{-1}
2.575×10^{3}	3.64×10^{1}	4.68×10^{1}	-4.84×10^{-1}
2.578×10^{3}	3.18×10^{1}	1.00×10^{1}	9.50×10^{-2}
2.595×10^{3}	3.18×10^{1}	1.00×10^{1}	-1.12×10^{0}
2.602×10^{3}	3.18×10^{1}	1.00×10^{1}	6.67×10^{0}
2.627×10^3	3.18×10^{1}	1.50×10^{1}	-8.15×10^{-2}
2.633×10^{3}	3.18×10^{1}	1.00×10^{1}	9.23×10^{-2}
2.645×10^{3}	3.16×10^1	4.30×10^{2}	-4.59×10^{0}
2.652×10^3	3.18×10^1	3.83×10^1	1.36×10^1
2.670×10^{3}	3.18×10^{1}	1.00×10^{1}	-1.02×10^{1}
2.698×10^{3}	3.18×10^{1}	3.26×10^{2}	1.20×10^{2}
2.700×10^{3}	3.18×10^{1}	1.50×10^{1}	7.56×10^{1}
2.706×10^{3}	3.18×10^{1}	1.00×10^{1}	-1.97×10^{1}
2.718×10^{3}	3.18×10^{1}	4.04×10^{1}	1.97×10^{0}
2.729×10^{3}	3.18×10^{1}	1.00×10^{1}	-1.02×10^{-1}
2.739×10^{3}	3.18×10^{1}	1.82×10^2	6.71×10^{-1}
2.754×10^{3}	2.91×10^{1}	1.10×10^{2}	8.33×10^{0}
2.764×10^{3}	3.18×10^{1}	1.00×10^{1}	9.80×10^{-2}
2.817×10^{3}	3.18×10^{1}	4.43×10^{1}	-1.60×10^{0}
2.844×10^{3}	3.18×10^{1}	1.72×10^2	-1.28×10^{-1}
2.858×10^{3}	3.18×10^{1}	2.87×10^{1}	1.20×10^{-1} 1.52×10^{0}
2.882×10^{3}	3.18×10^{1}	3.20×10^{1}	-3.50×10^{-1}
2.002×10^{3} 2.896 × 10 ³	3.18×10^{1}	6.39×10^{1}	1.60×10^{-1}
2.000×10^{3} 2.905 × 10 ³	3.18×10^{1}	1.23×10^2	6.10×10^{-1}
$2.900 \times 10^{-2.900}$	3.18×10^{1}	1.20×10^{1} 1.80×10^{1}	-1.00×10^{-1}
2.921×10^{3} 2.938 × 10 ³	3.18×10^{1}	1.00×10^{2} 1.53×10^{2}	-4.00×10^{-1}
$2.550 \times 10^{-2.000} \times 10^{-3}$	3.18×10^{1}	0.87×10^{1}	-3.60×10^{-1}
2.500×10^{3} 2.980 × 10 ³	3.18×10^{1}	1.12×10^2	5.00×10^{-2}
2.300×10 2.087×10^{3}	3.18×10^{1} 3.18×10^{1}	1.12×10^{-1} 1.00×10^{1}	-9.60×10^{-1}
2.987×10^{3}	3.18×10^{-10}	1.09×10^{-10}	-9.00×10 2.25 × 10 ⁻¹
2.994×10 2.004 $\times 10^3$	3.18×10^{-10}	0.12×10^{10}	5.25×10^{-1}
3.004×10	3.10×10^{-10}	0.39×10^{-1}	1.02×10^{-1}
3.010×10^{-2}	3.18×10^{-2}	1.27×10 2.01×10^{1}	-1.95×10 2.17 × 10 ⁰
3.029×10^{-3}	3.18×10^{-10}	2.01×10 1.00 × 10 ¹	2.17×10 2.22×10^{-1}
3.040×10^{3}	3.18×10^{1}	1.00×10^{1}	-2.52×10^{-1}
3.048×10^{3}	3.18×10	1.00×10	3.71×10
3.055×10^{3}	3.18×10^{-1}	4.90×10^{-1}	$-5.81 \times 10^{\circ}$
$3.070 \times 10^{\circ}$	3.18×10^{1}	1.37×10^{2}	2.10×10^{-100}
$3.078 \times 10^{\circ}$	3.18×10^{1}	1.33×10^{2}	$3.82 \times 10^{\circ}$
3.088×10^{3}	3.18×10^{1}	3.35×10^{-1}	-1.94×10^{-11}
3.092×10^{3}	3.18×10^{10}	1.00×10^{1}	$-2.59 \times 10^{\circ}$
3.106×10^{3}	3.18×10^{1}	0.00×10^{6}	-1.27×10^{1}
3.113×10^{3}	3.18×10^{1}	3.97×10^{1}	8.34×10^{-1}
3.140×10^{3}	3.18×10^{11}	4.00×10^{6}	-4.21×10^{6}
		Continued or	n nert column

TABLE IV – Continued from previous column

Energy $(\mathbf{o}\mathbf{V})$	Γ_{γ}	Γ_n	Γ_f
$\frac{(ev)}{2.172 \times 10^3}$	$\frac{(110)}{218 \times 10^{1}}$	$\frac{(110 \text{ v})}{2.20 \times 10^2}$	$\frac{(110 \text{ v})}{1.56 \times 10^0}$
3.173×10 3.107×10^3	3.10×10^{10}	$2.39 \times 10^{\circ}$	1.50×10^{-1}
3.185×10^{-103}	3.18×10	$8.00 \times 10^{-10^2}$	-3.07×10
3.192×10^{-103}	3.18×10	3.60×10	4.41×10
$3.209 \times 10^{\circ}$	3.18×10^{11}	1.50×10^{11}	3.18×10^{-1}
3.238×10^{3}	3.18×10^{1}	7.40×10^{1}	-7.59×10^{-1}
3.258×10^{3}	3.18×10^{1}	6.00×10^{0}	-3.11×10^{-1}
3.266×10^{3}	3.18×10^{1}	2.60×10^{1}	1.24×10^{-1}
3.269×10^{3}	3.18×10^{1}	1.09×10^{2}	1.72×10^{-1}
3.291×10^{3}	3.18×10^1	1.00×10^{1}	-1.81×10^{0}
3.305×10^{3}	3.18×10^1	1.20×10^1	-1.01×10^{0}
3.317×10^3	3.18×10^1	1.50×10^{1}	2.99×10^{-1}
3.332×10^{3}	3.18×10^1	1.48×10^{1}	-1.65×10^{0}
3.340×10^{3}	3.18×10^{1}	1.40×10^{1}	2.86×10^{0}
3.346×10^{3}	3.18×10^{1}	5.00×10^{0}	6.25×10^{0}
3.360×10^3	3.18×10^{1}	1.30×10^{1}	-7.34×10^{0}
3.382×10^3	3.18×10^{1}	1.50×10^{1} 1.50×10^{1}	-3.09×10^{-1}
3.302×10^{3}	3.10×10^{1} 3.18×10^{1}	1.60×10^{1}	9.03×10^{3}
3.362×10^{3}	3.10×10^{1}	1.00×10^{-1}	2.74×10^{-1}
3.369×10	3.18×10^{10}	1.30×10 2.51 $\times 10^{1}$	3.00×10^{0}
3.423×10^{3}	3.18×10	3.51×10^{-1}	0.00×10^{-1}
3.440×10^{3}	3.18×10^{12}	1.00×10^{1}	-3.39×10^{-1}
3.458×10^{3}	3.18×10^{11}	7.12×10^{12}	-5.48×10^{-1}
3.466×10^{3}	3.18×10^{1}	3.65×10^{2}	$-1.60 \times 10^{\circ}$
3.487×10^{3}	3.18×10^{1}	2.50×10^{1}	3.47×10^{-1}
3.494×10^{3}	3.18×10^{1}	6.59×10^{1}	-1.22×10^{0}
3.500×10^{3}	3.18×10^{1}	1.00×10^{1}	6.03×10^{-1}
3.514×10^{3}	3.18×10^1	1.00×10^1	-5.00×10^{-1}
3.539×10^{3}	3.18×10^1	1.00×10^1	5.00×10^{-1}
3.555×10^{3}	$3.18 imes 10^1$	9.06×10^{1}	0.00×10^0
3.567×10^3	3.18×10^1	1.79×10^2	-2.56×10^{-1}
3.581×10^{3}	3.18×10^1	1.50×10^{1}	0.00×10^0
3.595×10^{3}	3.18×10^1	4.22×10^{1}	-3.00×10^{-1}
3.610×10^{3}	3.18×10^{1}	7.57×10^{1}	3.02×10^{-1}
3.614×10^3	3.18×10^{1}	3.80×10^{1}	3.65×10^{-1}
3.648×10^3	3.18×10^{1}	1.00×10^{1}	2.80×10^{-1}
3.657×10^3	3.18×10^{1} 3.18×10^{1}	1.00×10^{2} 2.74×10^{2}	-7.08×10^{-2}
3.057×10^{3}	3.16×10^{-10}	2.74×10^{10}	-7.90×10^{-1}
3.000×10^{3}	3.10×10^{10}	3.41×10^{-1}	2.63×10^{-1}
3.082×10^{3}	3.18×10^{10}	1.00×10 5.07 · · · 10 ¹	-9.01×10^{-1}
$3.702 \times 10^{\circ}$	3.18×10^{-1}	5.37×10^{-1}	9.13×10^{-1}
$3.711 \times 10^{\circ}$	3.18×10^{-1}	2.50×10^{-1}	-5.00×10^{-1}
$3.723 \times 10^{\circ}$	3.18×10^{11}	5.58×10^{-1}	9.40×10^{-1}
3.743×10^{3}	3.18×10^{1}	$8.00 \times 10^{\circ}$	5.00×10^{-1}
3.765×10^{3}	3.18×10^{1}	$5.00 \times 10^{\circ}$	-5.00×10^{-1}
3.777×10^{3}	3.18×10^{1}	$5.00 \times 10^{\circ}$	$-3.25 \times 10^{\circ}$
3.800×10^{3}	3.18×10^{1}	1.08×10^{2}	1.14×10^{0}
3.823×10^{3}	3.18×10^1	$8.00 imes 10^0$	-4.76×10^{-1}
3.833×10^{3}	3.18×10^1	4.00×10^0	-4.84×10^{-1}
3.844×10^3	3.18×10^1	8.03×10^1	-9.97×10^{-2}
$3.853 imes 10^3$	3.18×10^1	1.03×10^2	3.95×10^{-1}
3.859×10^3	3.18×10^1	1.00×10^1	2.70×10^{0}
3.872×10^3	3.18×10^1	4.51×10^1	1.34×10^0
3.886×10^{3}	3.18×10^{1}	1.00×10^{1}	-5.00×10^{-1}
3.901×10^3	3.18×10^{1}	2.30×10^2	1.10×10^{-1}
3.916×10^3	3.18×10^{1}	1.83×10^2	-2.85×10^{-1}
3.030×10^{3}	3.18×10^{1}	1.00×10^{1}	9.34×10^{-1}
0.000 × 10	3.10 × 10	1.00 \ 10	0.01 X 10
		Continued o	n next column

TABLE IV – Continued from previous column

Energy	Γ_{γ}	Γ_n	Γ_f
(eV)	(meV)	(meV)	(meV)
3.954×10^{3}	3.18×10^{1}	1.09×10^{2}	-9.12×10^{0}
3.960×10^{3}	3.18×10^{1}	1.00×10^{1}	$1.00 imes 10^0$
3.975×10^{3}	3.18×10^{1}	1.19×10^{2}	-1.36×10^{0}
3.990×10^3	3.18×10^{1}	2.90×10^{1}	9.02×10^{-2}
4.002×10^3	3.10×10^{1}	2.50×10^{1} 2.50×10^{1}	$0.02 \times 10^{-0.00}$
4.002×10^{3}	3.10×10^{10}	2.50×10^{2}	-9.90×10
4.022×10^{-103}	3.18×10	3.33×10	1.11×10^{-1}
$4.031 \times 10^{\circ}$	3.18×10^{-1}	1.13×10^{-1}	-4.00×10^{-1}
$4.055 \times 10^{\circ}$	3.18×10^{-1}	2.90×10^{-1}	3.00×10^{-1}
4.073×10^{3}	3.18×10^{1}	$7.50 \times 10^{\circ}$	3.00×10^{-1}
4.084×10^{3}	3.18×10^{1}	1.35×10^{2}	-3.10×10^{-1}
4.100×10^{3}	3.18×10^{1}	2.90×10^2	4.69×10^{-1}
4.110×10^{3}	3.18×10^{1}	$9.00 imes 10^0$	3.00×10^{-1}
4.122×10^{3}	3.18×10^{1}	5.42×10^{2}	1.57×10^{-1}
4.135×10^{3}	3.18×10^1	6.79×10^{1}	-3.13×10^{-1}
4.143×10^{3}	3.18×10^{1}	$5.00 imes 10^0$	-3.00×10^{-1}
4.149×10^{3}	3.18×10^{1}	2.91×10^{2}	-2.25×10^{-1}
4.160×10^3	3.18×10^{1}	9.03×10^{1}	1.40×10^{-1}
4.100×10^{3}	3.10×10^{1} 3.18×10^{1}	2.00×10^{1}	3.00×10^{-1}
4.170×10 4.902×10^3	3.10×10^{1}	2.40×10 4.61×10^2	3.00×10 2.21×10^{-1}
4.203×10	3.10×10	4.01×10	-3.31×10^{-1}
4.221×10^{3}	3.18×10^{-1}	6.89×10^{-100}	5.84×10^{-2}
$4.241 \times 10^{\circ}$	3.18×10^{11}	$6.00 \times 10^{\circ}$	$-5.80 \times 10^{\circ}$
4.260×10^{3}	3.18×10^{1}	$8.00 \times 10^{\circ}$	$7.84 \times 10^{\circ}$
4.271×10^{3}	3.18×10^{1}	1.59×10^{2}	1.93×10^{-1}
4.280×10^{3}	3.18×10^{1}	3.10×10^{1}	-3.00×10^{-1}
4.288×10^{3}	3.18×10^{1}	3.23×10^2	1.52×10^{-1}
4.315×10^{3}	3.18×10^1	3.50×10^1	-2.98×10^{-1}
4.329×10^{3}	3.18×10^1	3.19×10^2	-3.96×10^{-2}
4.338×10^{3}	3.18×10^{1}	$7.50 imes 10^0$	3.00×10^{-1}
4.363×10^{3}	3.18×10^{1}	2.00×10^{1}	5.86×10^{-1}
4.376×10^{3}	3.18×10^{1}	8.20×10^{1}	0.00×10^{0}
4.386×10^{3}	3.18×10^{1}	3.20×10^{1}	-6.36×10^{-1}
4.308×10^3	3.18×10^{1}	7.80×10^{1}	-1.04×10^{0}
4.396×10^{3}	3.16×10^{-10}	7.30×10^{1}	-1.04×10 1.20 × 10 ¹
4.410×10 4.400×10^3	3.18×10^{1}	3.00×10^{-10}	1.30×10^{-1}
4.422×10^{-103}	3.18×10	0.10×10	$3.07 \times 10^{-0.01}$
4.433×10^{3}	3.18×10^{-1}	4.70×10^{11}	$3.05 \times 10^{\circ}$
4.447×10^{3}	3.18×10^{1}	1.80×10^{4}	-3.60×10^{-1}
4.459×10^{3}	3.18×10^{1}	1.03×10^{2}	6.74×10^{-1}
4.473×10^{3}	3.18×10^{1}	2.50×10^{1}	-3.00×10^{-1}
4.491×10^{3}	3.18×10^{1}	2.00×10^{1}	-3.00×10^{-1}
4.502×10^{3}	3.18×10^1	2.00×10^1	3.00×10^{-1}
4.517×10^{3}	3.18×10^1	1.00×10^1	-1.88×10^{0}
4.538×10^{3}	3.18×10^1	2.60×10^{1}	3.00×10^{-1}
4.560×10^{3}	3.18×10^{1}	2.00×10^{1}	3.00×10^{-1}
4570×10^{3}	3.18×10^{1}	2.35×10^2	-3.60×10^{-1}
4.588×10^3	3.18×10^{1}	5.50×10^2	-3.09×10^{-1}
4.500×10^{3}	3.10×10^{1} 3.18×10^{1}	7.54×10^{1}	5.03×10^{-1} 5.61 × 10 ⁻¹
4.099×10	3.16×10^{-10}	7.54×10^{2}	-5.01×10^{-100}
4.010×10^{-103}	3.10×10^{1}	$2.00 \times 10^{-1.02}$	$-4.00 \times 10^{\circ}$
$4.040 \times 10^{\circ}$	3.18×10^{-1}	1.52×10^{-1}	2.24×10^{-1}
4.004×10^{3}	3.18×10^{12}	8.00×10^{6}	-3.00×10^{-1}
4.687×10^{3}	3.18×10^{1}	2.00×10^{1}	$3.40 \times 10^{\circ}$
4.713×10^{3}	3.18×10^{1}	5.60×10^{1}	4.71×10^{-1}
4.721×10^{3}	3.18×10^{1}	5.10×10^{2}	-9.75×10^{-2}
4.745×10^{3}	3.18×10^{1}	2.53×10^2	3.01×10^{-1}
4.755×10^{3}	3.18×10^{1}	5.47×10^{1}	-1.66×10^{0}
		Continued o	n next column

TABLE IV – Continued from previous column

Energy	Γ_{γ}	Γ_n	Γ_{f}
(eV)	(meV)	(meV)	(meV)
4.769×10^{3}	3.18×10^{1}	3.73×10^{1}	1.33×10^{0}
4.778×10^{3}	3.18×10^1	3.42×10^1	6.78×10^{-1}
4.791×10^{3}	3.18×10^{1}	1.37×10^2	9.32×10^{-1}
4.800×10^{3}	3.18×10^1	2.00×10^1	-4.11×10^{-1}
4.812×10^3	3.18×10^1	1.81×10^2	2.83×10^{-1}
4.822×10^{3}	3.18×10^1	6.34×10^1	5.58×10^{0}
4.843×10^{3}	3.18×10^{1}	1.80×10^{1}	7.76×10^{-1}
4.868×10^{3}	3.18×10^{1}	1.30×10^{1}	-1.40×10^{0}
4.894×10^{3}	3.18×10^{1}	6.28×10^{1}	-9.19×10^{-1}
4.912×10^{3}	3.18×10^{1}	1.50×10^{1}	-3.79×10^{1}
4.933×10^{3}	3.18×10^{1}	2.00×10^{1}	1.90×10^{1}
4.900×10^{-10}	3.18×10^{1}	5.17×10^{1}	-8.26×10^{0}
4.058×10^{3}	3.10×10^{1} 3.18×10^{1}	3.20×10^2	4.45×10^{0}
4.958×10^{3}	3.18×10^{1}	5.20×10^{-1}	4.40×10^{-10} 5.02 × 10 ⁰
4.900×10 4.074×10^{3}	3.18×10^{1} 3.18×10^{1}	1.54×10^{-1} 7.50×10^{1}	3.52×10^{-1}
4.974×10^{3}	3.10×10^{1}	7.50×10^{-10}	$-3.07 \times 10^{-1.01}$
4.994×10	3.10×10^{1}	9.50×10^{1}	-1.21×10
$5.035 \times 10^{\circ}$	3.18×10^{-1}	1.50×10^{-1}	$1.47 \times 10^{\circ}$
$5.047 \times 10^{\circ}$	3.18×10^{-1}	$1.00 \times 10^{-10^2}$	$-1.51 \times 10^{\circ}$
5.072×10^{3}	3.18×10^{-1}	5.66×10^{2}	$-7.53 \times 10^{\circ}$
5.097×10^{3}	3.18×10^{11}	3.60×10^{1}	2.34×10^{6}
5.111×10^{3}	3.18×10^{1}	8.61×10^{1}	1.59×10^{1}
5.120×10^{3}	3.18×10^{1}	1.95×10^{1}	-4.45×10^{-1}
5.131×10^{3}	3.18×10^{1}	4.36×10^{1}	-4.91×10^{1}
5.148×10^{3}	3.18×10^{1}	5.00×10^{1}	0.00×10^{0}
5.161×10^{3}	3.18×10^{1}	4.00×10^{1}	1.34×10^{0}
5.176×10^{3}	3.18×10^1	$8.00 imes 10^0$	-2.02×10^{0}
5.194×10^{3}	3.18×10^1	3.46×10^2	5.56×10^{-1}
5.216×10^{3}	3.18×10^{1}	1.62×10^{2}	-7.15×10^{-1}
5.235×10^3	3.18×10^1	2.40×10^1	$6.37 imes 10^0$
5.250×10^3	3.18×10^1	5.23×10^2	-5.94×10^{0}
5.272×10^{3}	3.18×10^1	1.44×10^2	2.21×10^1
5.286×10^{3}	3.18×10^1	5.30×10^1	3.98×10^{-1}
5.301×10^{3}	3.18×10^1	2.83×10^{2}	3.46×10^{0}
5.327×10^{3}	3.18×10^1	1.78×10^2	-1.28×10^{1}
5.353×10^{3}	3.18×10^{1}	1.50×10^{2}	2.38×10^{0}
5.357×10^{3}	3.18×10^{1}	3.60×10^{1}	-4.46×10^{-1}
5.367×10^3	3.18×10^{1}	6.97×10^{1}	-8.59×10^{0}
5.380×10^3	3.18×10^{1}	8.00×10^{0}	5.99×10^{-1}
5.393×10^3	3.18×10^{1}	8.46×10^{1}	1.06×10^{0}
5.000×10^{3} 5.417×10^{3}	3.18×10^{1}	2.64×10^2	3.21×10^{-1}
5.417×10^{3} 5.440×10^{3}	3.10×10^{1} 3.18×10^{1}	1.20×10^{1}	-3.75×10^{0}
5.440×10^{3} 5.456×10^{3}	3.18×10^{1}	1.20×10^{-10}	-5.75×10^{-1}
5.450×10^{3}	3.18×10^{1}	3.00×10^{-10}	-4.09×10^{-100}
5.403×10^{3}	3.16×10^{-10}	4.97×10^{1}	0.49×10^{-1}
5.465×10^{3}	3.10×10^{-10}	0.07×10^{1}	-9.14×10^{-1}
5.498×10	3.10×10^{1}	9.92×10^{2}	3.23×10^{-1}
$5.511 \times 10^{\circ}$	3.18×10^{-1}	3.58×10^{-1}	-4.83×10^{-1}
5.523×10^{3}	3.18×10^{1}	1.75×10^{2}	4.94×10^{5}
5.531×10^{3}	3.18×10^{1}	1.60×10^{10}	-5.52×10^{-1}
5.545×10^{3}	3.18×10^{1}	5.51×10^{2}	-3.50×10^{-1}
5.551×10^{3}	3.18×10^{1}	1.21×10^{2}	-7.06×10^{-1}
5.564×10^{3}	3.18×10^{1}	1.50×10^{1}	7.60×10^{-1}
5.574×10^{3}	3.18×10^{1}	7.90×10^{2}	2.26×10^{-1}
5.592×10^{3}	3.18×10^{1}	1.96×10^{2}	7.61×10^{-1}
5.600×10^{3}	3.18×10^{1}	1.41×10^{2}	-3.32×10^{-1}
		Continued o	n next column

TABLE IV - Continued from previous column

TABLE V: List of the fission kernels that were extracted with a statistical uncertainty less than 30%.

Energy	Γ_{γ}	Γ_n	Γ_f
(eV)	(meV)	(meV)	(meV)
5.615×10^{3}	3.18×10^{1}	6.20×10^{1}	3.55×10^{0}
5.629×10^3	3.18×10^1	2.00×10^1	-6.24×10^{-1}
5.644×10^{3}	3.18×10^1	5.50×10^{1}	1.26×10^{0}
5.667×10^3	3.18×10^1	4.50×10^1	-7.49×10^{-1}
5.682×10^3	3.18×10^1	1.05×10^2	-7.03×10^{0}
5.692×10^{3}	3.18×10^1	9.10×10^1	$1.00 imes 10^0$
5.995×10^3	3.18×10^1	9.64×10^1	-2.74×10^2
5.924×10^{3}	3.18×10^1	9.58×10^1	-8.72×10^{4}
5.981×10^3	3.18×10^1	9.62×10^1	-7.39×10^{-2}
5.990×10^3	3.18×10^1	9.63×10^1	1.70×10^{-2}
6.299×10^{3}	3.18×10^1	9.88×10^1	-2.38×10^{0}
6.427×10^{3}	3.18×10^1	9.98×10^1	8.49×10^{-3}
6.446×10^{3}	3.18×10^{1}	9.99×10^{1}	3.22×10^{-1}
6.513×10^{3}	3.18×10^1	1.00×10^2	2.58×10^{0}
6.535×10^{3}	3.18×10^1	1.01×10^2	$7.01 imes 10^0$
6.551×10^{3}	3.18×10^{1}	1.01×10^{2}	1.87×10^1
6.568×10^{3}	3.18×10^{1}	1.01×10^{2}	2.85×10^{2}
7.508×10^{3}	3.18×10^{1}	1.08×10^{2}	2.08×10^{2}
8.021×10^{3}	3.18×10^{1}	1.11×10^{2}	2.98×10^{0}
8.064×10^{3}	3.18×10^{1}	1.12×10^{2}	3.13×10^0
8.098×10^{3}	3.18×10^{1}	1.12×10^{2}	1.92×10^{4}
8.361×10^{3}	3.18×10^{1}	1.14×10^{2}	7.80×10^{0}
8.472×10^{3}	3.18×10^{1}	1.77×10^{2}	1.60×10^{1}
8.708×10^{3}	3.18×10^{1}	1.16×10^{2}	1.02×10^{2}
8.975×10^{3}	3.18×10^{1}	1.18×10^{2}	5.59×10^{4}
1.002×10^{4}	3.18×10^{1}	1.25×10^{2}	8.64×10^{0}
1.008×10^{4}	3.18×10^{1}	1.25×10^{2}	2.69×10^{2}
1.015×10^{4}	3.18×10^{1}	1.25×10^{2}	1.16×10^{2}
1.096×10^{4}	3.18×10^{1}	1.30×10^{2}	6.89×10^{1}
1.118×10^{4}	3.18×10^{1}	1.32×10^{2}	3.61×10^{2}
1.150×10^{4}	3.18×10^{1}	1.33×10^{2}	1.15×10^{3}
1.166×10^{4}	3.18×10^{1}	1.34×10^{2}	-4.64×10^{3}
1.215×10^{4}	3.18×10^{1}	1.37×10^{2}	3.87×10^{2}
1.250×10^{4}	3.18×10^{1}	1.39×10^{2}	-8.21×10^{1}
1.311×10^{4}	3.18×10^{1}	1.42×10^{2}	-4.84×10^{2}
1.317×10^{4}	3.18×10^{1}	1.43×10^{2}	-4.90×10^{4}
1.356×10^4	3.18×10^{1}	1.45×10^{2}	1.76×10^{3}
1.405×10^4	3.18×10^{1}	1.48×10^{2}	8.55×10^{1}
1.450×10^4	3.18×10^{1}	1.50×10^2	2.39×10^2
1.447×10^4	3.18×10^{1}	1.50×10^{2}	3.38×10^{2}
1.605×10^4	3.18×10^{1}	1.58×10^2	6.44×10^3
1.643×10^4	3.18×10^{1}	1.60×10^2	-5.70×10^{2}
1.748×10^4	3.18×10^{1}	1.65×10^2	3.87×10^{3}
1.822×10^4	3.18×10^{1}	1.68×10^2	-2.32×10^{3}
1.845×10^4	3.18×10^{1}	1.69×10^2	6.22×10^2
1.921×10^4	3.18×10^{1}	1.73×10^2	-1.44×10^{3}
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1047	Appendix B: Cross section in the 100 keV - 6 MeV
1048	region

¹⁰⁴⁹ The derived ²⁴⁰Pu(n,f) cross section (σ) along with its ¹⁰⁵⁰ corresponding uncertainty ($\delta\sigma$) is reported below, in the ¹⁰⁵¹ energy region between 100 keV and 6 MeV.

Energy	σ	δσ	δσ
(eV)	(b)	(b)	(%)
1.01×10^5	$\frac{(5)}{4.90 \times 10^{-2}}$	$\frac{(5)}{5 \times 10^{-3}}$	10
1.01×10^{-5}	4.90×10^{-2}	5×10^{-3}	0
1.04×10^{5}	4.03×10^{-2} 5.80 × 10 ⁻²	3×10 4×10^{-3}	8
1.00×10 1.08×10^5	5.80×10^{-2}	4×10 5×10^{-3}	8
1.00×10 1.11 × 10 ⁵	0.30×10^{-2}	5×10^{-3}	1
1.11×10 1.14×10^5	0.00×10	5×10^{-3}	1
1.14×10^{5}	0.91×10	5×10^{-3}	
$1.16 \times 10^{\circ}$	6.97×10^{-2}	5×10^{-3}	(
1.19×10^{-1}	4.70×10	4×10^{-3}	9
$1.22 \times 10^{\circ}$	5.29×10^{-2}	4×10^{-3}	8
1.24×10^{5}	6.19×10^{-2}	4×10^{-3}	7
1.27×10^{5}	6.95×10^{-2}	4×10^{-3}	6
1.30×10^{5}	7.70×10^{-2}	4×10^{-3}	6
1.33×10^{3}	8.47×10^{-2}	5×10^{-3}	6
1.36×10^{5}	9.09×10^{-2}	6×10^{-3}	7
1.40×10^{5}	8.74×10^{-2}	7×10^{-3}	8
1.43×10^{5}	6.74×10^{-2}	7×10^{-3}	10
1.46×10^{5}	7.08×10^{-2}	7×10^{-3}	10
1.50×10^{5}	6.19×10^{-2}	6×10^{-3}	10
1.53×10^{5}	5.54×10^{-2}	5×10^{-3}	10
1.57×10^{5}	6.04×10^{-2}	6×10^{-3}	10
1.60×10^{5}	6.87×10^{-2}	6×10^{-3}	8
1.64×10^{5}	5.71×10^{-2}	5×10^{-3}	8
1.68×10^{5}	7.80×10^{-2}	5×10^{-3}	6
1.72×10^{5}	6.48×10^{-2}	4×10^{-3}	7
1.76×10^{5}	6.58×10^{-2}	4×10^{-3}	7
1.80×10^{5}	6.43×10^{-2}	4×10^{-3}	7
1.84×10^{5}	6.42×10^{-2}	4×10^{-3}	7
1.88×10^{5}	8.12×10^{-2}	5×10^{-3}	6
1.93×10^{5}	8.12×10^{-2}	5×10^{-3}	7
1.97×10^5	9.02×10^{-2}	6×10^{-3}	7
2.02×10^5	8.81×10^{-2}	6×10^{-3}	7
2.07×10^5	7.75×10^{-2}	5×10^{-3}	7
2.11×10^{5}	8.00×10^{-2}	5×10^{-3}	7
2.16×10^{5}	7.92×10^{-2}	5×10^{-3}	6
2.21×10^5	9.67×10^{-2}	5×10^{-3}	5
2.26×10^5	8.64×10^{-2}	5×10^{-3}	6
2.32×10^5	9.47×10^{-2}	5×10^{-3}	5
2.37×10^5	8.84×10^{-2}	5×10^{-3}	5
2.43×10^5	8.99×10^{-2}	5×10^{-3}	5
2.48×10^5	8.44×10^{-2}	4×10^{-3}	5
2.54×10^5	8.31×10^{-2}	4×10^{-3}	5
2.60×10^5	6.46×10^{-2}	4×10^{-3}	6
2.66×10^5	7.65×10^{-2}	4×10^{-3}	5
2.72×10^5	1.01×10^{-1}	5×10^{-3}	5
2.79×10^5	1.31×10^{-1}	6×10^{-3}	5
2.85×10^5	1.11×10^{-1}	6×10^{-3}	5
2.92×10^5	9.86×10^{-2}	5×10^{-3}	5
2.99×10^5	$7.95 imes 10^{-2}$	4×10^{-3}	5
3.06×10^5	7.47×10^{-2}	4×10^{-3}	5
3.13×10^5	6.80×10^{-2}	4×10^{-3}	6
3.20×10^5	8.64×10^{-2}	4×10^{-3}	5
3.27×10^5	8.93×10^{-2}	4×10^{-3}	5
3.35×10^5	1.33×10^{-1}	6×10^{-3}	4

Continued on next column

TABLE V – Continued from previous column

Energy	σ	$\delta\sigma$	$\delta\sigma$
(eV)	(b)	(b)	%
3.43×10^{5}	1.46×10^{-1}	6×10^{-3}	4
3.51×10^5	1.68×10^{-1}	7×10^{-3}	4
3.59×10^5	1.59×10^{-1}	6×10^{-3}	4
3.67×10^5	1.37×10^{-1}	5×10^{-3}	4
3.76×10^5	1.01×10^{-1}	5×10^{-3}	4
3.85×10^5	1.10×10^{-1} 1.70×10^{-1}	5×10^{-3}	3
3.94×10^5	1.77×10^{-1}	6×10^{-3}	3
4.03×10^5	2.14×10^{-1}	7×10^{-3}	3
4.12×10^5	2.15×10^{-1}	7×10^{-3}	3
4.22×10^{5}	2.37×10^{-1}	8×10^{-3}	3
4.32×10^{5}	2.52×10^{-1}	8×10^{-3}	3
4.42×10^{5}	3.12×10^{-1}	9×10^{-3}	3
4.52×10^{5}	3.11×10^{-1}	8×10^{-3}	3
4.62×10^{5}	3.15×10^{-1}	8×10^{-3}	2
4.73×10^{5}	2.97×10^{-1}	7×10^{-3}	2
4.84×10^5	3.44×10^{-1}	8×10^{-3}	2
4.95×10^5	3.31×10^{-1}	7×10^{-3}	2
5.07×10^5	3.62×10^{-1}	7×10^{-3}	2
5.19×10^5	4.17×10^{-1}	8×10^{-3}	2
5.31×10^{5}	4.68×10^{-1}	9×10^{-3}	2
5.43×10^5	4.97×10^{-1}	1×10^{-2}	2
5.56×10^5	5.45×10^{-1}	1×10^{-2}	2
5.69×10^5	5.67×10^{-1}	1×10^{-2}	2
5.82×10^5	6.49×10^{-1}	1×10^{-2}	2
5.96×10^{5}	6.78×10^{-1}	1×10^{-2}	2
6.10×10^{5}	7.41×10^{-1}	1×10^{-2}	2
6.24×10^{5}	7.32×10^{-1}	1×10^{-2}	2
6.38×10^{5}	7.75×10^{-1}	1×10^{-2}	2
6.53×10^{5}	8.35×10^{-1}	1×10^{-2}	2
6.68×10^{5}	7.94×10^{-1}	1×10^{-2}	2
6.84×10^{3}	8.31×10^{-1}	1×10^{-2}	2
7.00×10^{3}	8.62×10^{-1}	1×10^{-2}	2
7.16×10^{3}	8.97×10^{-1}	2×10^{-2}	2
7.33×10^{5}	9.23×10^{-1}	2×10^{-2}	2
$7.50 \times 10^{\circ}$	9.74×10^{-1}	2×10^{-2}	2
$7.67 \times 10^{\circ}$	$1.05 \times 10^{\circ}$	2×10^{-2}	2
$7.85 \times 10^{\circ}$	$1.04 \times 10^{\circ}$	2×10^{-2}	2
8.04×10^{5}	$1.03 \times 10^{\circ}$	2×10	2
8.22×10^{5}	1.11×10^{-1}	2×10 2×10^{-2}	2
8.41×10^{-8}	1.17×10 1.20×10^{0}	2×10 2×10^{-2}	2
8.01×10^{5}	1.20×10 1.22×10^{0}	2×10 2×10^{-2}	2
0.01×10^{5}	1.22×10 1.28×10^{0}	2×10 2×10^{-2}	1
9.02×10^{-10}	1.23×10^{-1} 1.32×10^{0}	2×10 2×10^{-2}	1
9.23×10^{-5}	1.32×10^{-1} 1.38×10^{0}	2×10^{-2} 2×10^{-2}	1
9.44×10^{-9}	1.33×10^{-1} 1.43×10^{0}	2×10^{-2} 2×10^{-2}	1
9.80×10^{5}	1.10×10^{-1} 1.47×10^{0}	2×10^{-2} 2×10^{-2}	1
1.05×10^{6}	1.41×10^{-10} 1.48×10^{-0}	$\frac{2}{1} \times 10^{-2}$	1
1.15×10^{6}	1.51×10^{0}	1×10^{-2}	1
1.25×10^{6}	1.49×10^{0}	1×10^{-2}	1
1.35×10^{6}	$1.49 \times 10^{\circ}$	1×10^{-2}	1
1.45×10^{6}	1.57×10^{0}	2×10^{-2}	1
1.55×10^{6}	1.56×10^{0}	2×10^{-2}	1
1.65×10^{6}	1.58×10^{0}	2×10^{-2}	- 1
			-

 $Continued \ on \ next \ column$

TABLE V – Continued from previous column

Energy	σ	$\delta\sigma$	$\delta\sigma$
(eV)	(b)	(b)	%
1.75×10^{6}	1.60×10^{0}	2×10^{-2}	1
1.85×10^6	1.66×10^0	2×10^{-2}	1
1.95×10^6	$1.65 imes 10^0$	2×10^{-2}	1
2.10×10^6	1.71×10^0	2×10^{-2}	1
2.30×10^{6}	$1.70 imes 10^0$	2×10^{-2}	1
2.50×10^6	$1.60 imes 10^0$	3×10^{-2}	2
2.70×10^6	1.72×10^0	3×10^{-2}	2
2.90×10^6	$1.73 imes 10^0$	3×10^{-2}	2
3.12×10^6	1.71×10^0	4×10^{-2}	2
3.38×10^{6}	1.71×10^0	4×10^{-2}	2
3.62×10^6	1.61×10^0	4×10^{-2}	2
3.88×10^6	1.64×10^0	8×10^{-2}	5
4.25×10^6	1.52×10^0	8×10^{-2}	5
4.75×10^6	1.55×10^0	8×10^{-2}	5
5.25×10^{6}	1.52×10^{0}	8×10^{-2}	5
5.75×10^6	1.63×10^0	1×10^{-1}	8

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