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18 *Abstract*

19

20 Cement has been widely used for low- to intermediate-level radioactive waste management;
21 however, the long-term modelling of multiple mineral transfer between the cement leachate and
22 the host rock of a geological disposal facility remains a challenge due to the strong physical-
23 chemical interactions within the chemically-disturbed zone. This paper presents a modelling study
24 for a 15-year experiment simulating the reaction of crystalline basement rock with evolved near-
25 field groundwater (pH = 10.8). A mixed kinetic equilibrium (MKE) modelling approach was
26 employed to study the dolomite-rich fracture-filling assemblage reacting with intermediate cement
27 leachate. The study found that the mineralogical and geochemical transformation of the system
28 was driven by the kinetically-controlled dissolution of the primary minerals (dolomite, calcite,
29 quartz, k-feldspar and muscovite). The initial high concentration of calcium ions appeared to be
30 the main driving force initiating the dedolomitization process, which played a significant role in
31 the precipitation of secondary talc, brucite and Mg-aluminosilicate minerals. The modelling study
32 also showed that most of the initially precipitated calcium silicon hydrate phases redissolved and
33 formed more stable calcium silicon aluminium hydrate phases. The findings highlight the
34 importance of a deep and insightful understanding of the geochemical transformations based on
35 the type and characteristics of the host rock, where the system is under out of equilibrium
36 conditions, and the rates of mineral reactions.

37

38 **Keywords:** Cement, Radioactive waste disposal, Mineral evolution, Modelling, Cement leachate,
39 Alkaline fluids, PHREEQC

40

41 ***1. Introduction***

42

43 Underground geological facilities are the most secure places to store/dispose of radioactive wastes
44 generated during the civil/military programmes, and also generated through scientific, engineering
45 and medical usage. One concept for low- and intermediate-level radioactive waste involves
46 constructing an underground facility in a host rock at a depth of several hundred metres, then
47 backfilling with a cementitious material. Such a facility is designed to achieve two main safety
48 objectives: 1) to isolate the radioactive waste from the biosphere, and 2) to provide multiple
49 barriers (including a high pH environment) to minimise radionuclide mobility over long
50 timescales.

51

52 The containment system involves multiple barriers in which the engineered barriers work
53 alongside natural ones (e.g. stable and low permeability host rock) to prevent the release of
54 radionuclides to the biosphere. The concept has been adopted by several countries, including the
55 UK, Sweden and South Korea (Authority 2010a; Francis et al. 1997; Kim et al. 2007; Skogsberg
56 and Ingvarsson 2006). The final design and performance assessment of the engineered barrier can
57 be influenced by the waste inventory, the surrounding conditions that can be expected during the
58 performance assessment timescale and the degree of reaction with the surrounding host geology.
59 Usually, the near field plays a crucial role in providing long-term control over radionuclide
60 migration, which limits their release to the surrounding environment. Over time, the chemical
61 properties (e.g., sorption capacity, reactive surface area) and physical properties (e.g., porosity,
62 permeability) of the host rock in the near field barrier evolve as a result of the interactions with
63 their surroundings and with other barriers. As this will happen long before any potential migration

64 of radionuclides, it is useful to understand and to be able to predict these changes, as they are likely
65 to influence potential radionuclide retardation.

66

67 One of the challenges in evaluating the effectiveness of an engineered barrier is understanding the
68 extent to which the evolving process of the near field host rock may occur. This will help in
69 assuring that the engineered barrier materials will fulfil their safety functions over performance
70 assessment timescales. The evolution of near field properties will strongly be linked to the
71 interaction of the host rock and high pH water leaching out of the cement (the ‘alkaline disturbed
72 zone’, ADZ).

73

74 Cement leachate is usually formed when the facility is closed and becomes saturated with
75 groundwater that then reacts and equilibrates with the cementitious engineered barrier. The
76 reaction process results in a high-pH plume that inhibits corrosion and limits some radionuclide
77 solubility. Eventually, some cement leachate will migrate into the surrounding rock and create a
78 chemically disturbed zone (CDZ) at the interface between the cement barrier and the host rock,
79 initiating a series of reactions (Chen et al. 2016; Chen and Thornton 2018; Chen et al. 2015). The
80 dissolution of primary minerals in the host rock is likely to be accompanied by precipitation of
81 new minerals with evolved chemical and physical properties that may contribute to decreased
82 radionuclide mobility through processes such as the reduction in permeability, increased sorption,
83 and coprecipitation.

84

85 For a cement-based geological disposal facility, several experimental studies and numerical
86 models have been performed to demonstrate the reaction of highly-alkaline cement leachate with

87 minerals in the host rock (Berner 1990; Harris et al. 2001a; Harris et al. 2001b; Schwyn et al.
88 2003). Previous research has considered three cement leachate evolution stages based on the
89 progression of pH values (Small et al. 2016), which can be summarised as: young cement leachate
90 (YCL), intermediate cement leachate (ICL) and old cement leachate (OCL). The reaction of ICL
91 with the near field host rock is the focus of this study, and this may result in the formation of a
92 changing series of mineral assemblages, changes to mineral surfaces, variations in pH, as well as
93 other changes (Moyce et al. 2014). These processes will eventually affect the sorption capability
94 of radionuclides at the mineral surface (Authority 2010b).

95
96 The paper models mineral evolution in a 15-year laboratory experiment, analysing interlinks
97 among multiple minerals known to occur in Borrowdale Volcanic Group (BVG) rocks in reaction
98 with ICL (the BVG is an important basement rock in north-west England, and which was
99 previously investigated by UK Nirex Limited (Francis et al. 1997). Importantly, the rock sample
100 comprised a hydraulically-conductive dolomite-rich fracture, and thought dolomite is only a minor
101 phase in the rock overall; it is a major phase in direct contact with current groundwater. The
102 modelling process implements the concept of a mixed kinetic equilibrium approach (MKE), which
103 combines the advantages of both equilibrium and kinetic formulations to enable the modelling of
104 complex geochemical reactions (Bethke 1994; Bethke 1996; Chen and Thornton 2018; Van der
105 Lee 1997; Van der Lee 1998; Westall 1986). This approach was initially developed to overcome
106 the shortage of kinetic data for minerals that dissolve and precipitate (Soetaert et al. 1996),
107 assuming a faster reaction by means of the equilibrium concept and a slower reaction controlled
108 by the kinetic process (Atkinson et al. 1988; Hoch et al. 2012). The model is used to develop a

109 deeper understanding of the pH evolution along with quantification of the amount of host rock
110 minerals dissolving or precipitating in the near field/alkaline disturbed zone.

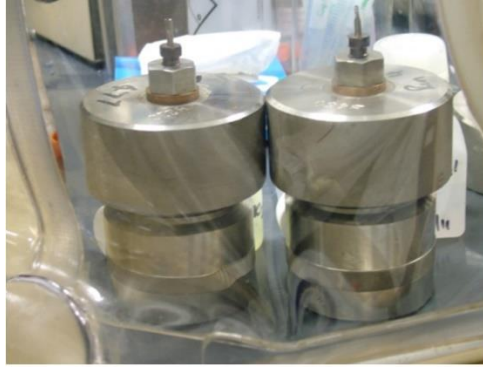
111

112 **2. *Experimental study***

113

114 The experiment was conducted by the British Geological Survey (Moyce et al. 2014; Rochelle et
115 al. 2016; Rochelle et al. 1997) over the course of 15 years, starting in 1995, and being part of a
116 larger series of experiments of different durations. The original intent of the experiment was to
117 study the reaction of a sample of Ordovician age Borrowdale Volcanic Group (BVG) rock with
118 both a pH 13 ‘young near-field porewater’ (YNFP) and a pH 12 ‘evolved near-field groundwater’
119 (ENFG) (rock type and fluid naming convention based on that used in the Nirex Safety Assessment
120 research programme [NSARP] at the time). These fluids represent, respectively, ‘young cement
121 leachate (YCL) and ‘intermediate cement leachate’ (ICL) (naming convention used in the
122 BIGRAD project) released from a representative cementitious barrier that could be used in a deep
123 geological disposal facility for intermediate-level radioactive waste. Although the experiments
124 significantly exceeded their originally planned durations and also that of the NSARP, it was useful
125 to continue them as the BVG contains many mineral phases typical of crystalline basement rocks
126 in general. In the experiment of relevance to the study presented here, a dolomite-rich fracture
127 assemblage in the BVG was reacted with YNFP, and the resultant solid and fluid products initially
128 examined after 15 months and also for up to 15 years. The focus of the current study was to better
129 understand the mineralogical evolution of this experimental system for the entire 15 years, in order
130 to investigate longer-term geochemical processes.

131



132

133 Figure 1: Stainless steel pressure vessels lined with Teflon® used to contain the BVG and synthetic CDZ-type fluid
134 experiments.

135

136 Two PTFE-lined stainless steel vessels, of 150 mL and 100 mL, were used for the ‘reacting’ and
137 blank experiments, respectively (Figure 1). The solid phase consisted of a piece of drill core
138 containing altered wall rock and a dolomite-rich fracture fill from a hydrogeological conductive
139 fracture zone in the BVG. The 2-kg rock sample was then disaggregated and sieved (Moyce et al.
140 2014; Rochelle et al. 1997). In the ‘reacting’ experiment, 35 g of disaggregated BVG was used
141 with 140 g of groundwater-cement leachate, and the stainless-steel vessel was kept in a 70°C oven.
142 The smaller blank experiment just contained the leachate. The ENFG leachate was presented by
143 slightly saline water (Na/CaCl) saturated with $\text{Ca}(\text{OH})_2$ (Table 1). All preparation processes were
144 performed under a nitrogen atmosphere to prevent reaction of the alkaline water with atmospheric
145 carbon dioxide. During the reaction, the rock underwent mineralogical changes that changed the
146 concentration of the dissolved ions in the ENFG leachate. Experiments were terminated and
147 sampled after the fourth, ninth and fifteenth months (Rochelle et al. 2016; Rochelle et al. 1997),
148 and importantly also at the end of the fifteenth year (Moyce et al. 2014). The solid experimental
149 residues were washed in propan-2-ol and then dried prior to storage and analysis. For X-ray
150 diffraction analysis, a subsample was milled and a 10% corundum (Al_2O_3) standard added. A
151 diffractometer instrument (PANalytical X’Pert Pro) with PANalytical X’Pert Highscore Plus

152 software was then used to carry out the final mineralogical analysis (Moyce et al. 2014; Rochelle
153 et al. 2016).

154

155 Table 1: Composition of the Evolved Near-Field Groundwater (ENFG) prepared by the British Geological Survey
156 (Rochelle et al. 2016; Rochelle et al. 1997).

Chemical component	Concentration (mg/L)
Al	4.17
B	0.335
Ba	0.017
Br	23.2
CO ₃	20
Ca	1930
Cl	15100
F	0.03
Fe	0.120
K	185
Li	0.153
Mg	0.117
Mn	0.010
Na	9160
SO ₄	1090
NO ₃	20
Si	2.07
Sr	166
pH (at 70°C)	10.84

157

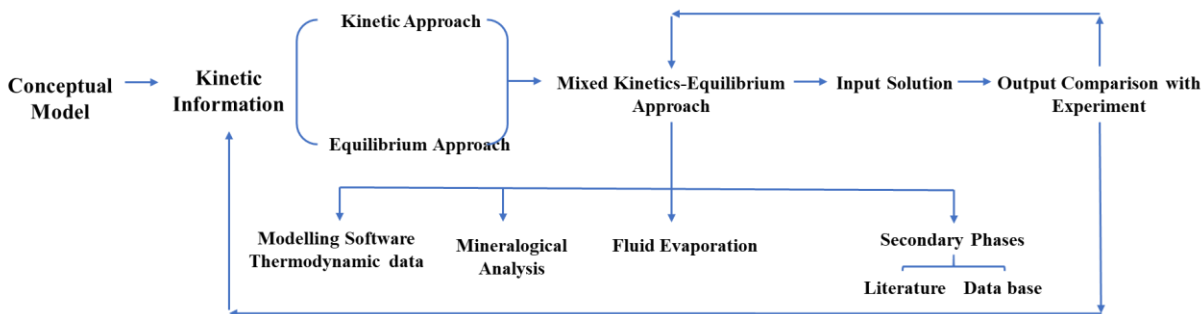
158 **3. Modelling methodology**

159

160 The conceptual model developed for this study is presented in Figure 2. The idea was developed
161 based on theoretical and experimental analysis. The MKE approach is based upon the timescale of
162 each mineral reaction rate (i.e., which reaction is faster and which slower). For each mineral, either
163 a kinetic or equilibrium approach, or a mix of both (if the difference between rates was more than
164 10^2), was used to provide the supporting information for the software. The concept of MKE has
165 been widely implemented in subsurface geochemical applications, as it allows both kinetic and

166 equilibrium reactions to model a multiphase and multi-component system (Brun and Engesgaard
167 2002; Lichtner 1996; Mayer et al. 2002; Prommer et al. 2003).

168



169

170

Figure 2: Conceptual Model for the Mixed Kinetic-Equilibrium approach.

171

172 **3.1. Conceptual model software and thermodynamic data**

173 The simulation carried out in this study was performed with the PHREEQC code (version 3.6.1).

174 The software can compute a wide range of chemical reactions in aqueous geochemical systems,

175 utilising both chemical thermodynamic and kinetic data. In recent years, several databases have

176 been developed by various authors to optimise the use of this geochemical code. For a cement

177 leachate–host rock reaction in an underground repository, the Lawrence Livermore National

178 Laboratory (LLNL), Thermoddem, Thermoddem DB and CEMDATA DB databases were applied

179 by previous researchers (Blanc et al. 2012; Lothenbach et al. 2019; Wolery 1992; Wolery and

180 Daveler 1992). In this work, LLNL database (Delany and Lundeen 1990) –was utilise though with

181 some modifications, namely; the addition of kinetic information for calcium silicon hydrate (CSH)

182 and calcium silicon aluminium hydrate phases (CASH). This database seemed to be the best option

183 available since it has kinetic information for a variety of minerals and aqueous species, especially

184 carbonate minerals that are required for the simulation of phases present in the BVG rock sample.

185 The data of thermodynamic reactions (equilibrium constants) for the major minerals are shown in

186 Table 2 (Chen and Thornton 2018). Note that the below values of $\log K_{eq}$ are valid for the
 187 experiment condition.

188

189 Table 2: Reactions and equilibrium constants for minerals used in the calculations.

<i>Mineral</i>	<i>Reaction</i>	<i>Log Keq</i>
<i>Calcite</i>	$CaCO_3 + H^+ = Ca^{++} + HCO_3^-$	1.8487
<i>Muscovite</i>	$KAl_3Si_3O_{10}(OH)_2 + 10H^+ = K^+ + 3Al^{+++} + 3SiO_2 + 6H_2O$	13.5858
<i>Kaolinite</i>	$Al_2Si_2O_5(OH)_4 + 6H^+ = +2Al^{+++} + 2SiO_2 + 5H_2O$	6.8101
<i>Quartz</i>	$SiO_2 = +1.0 SiO_2$	-3.9993
<i>Dolomite</i>	$CaMg(CO_3)_2 + 2H^+ = +1.0Ca^{++} + 1.0 Mg^{++} + 2 HCO_3^-$	2.5135
<i>K-feldspar</i>	$KAlSi_3O_8 + 4.0000 H^+ = + 1.0000 Al^{+++} + 1.0000 K^+ + 2.0000 H_2O + 3.0000 SiO_2$	-0.2753
<i>Brucite</i>	$Mg(OH)_2 + 2H^+ = + 1.0 Mg^{++} + 2H_2O$	16.2980
<i>Tobermorite-11A</i>	$Ca_5Si_6H_{11}O_{22.5} + 10H^+ = +5Ca^{++} + 6SiO_2 + 10.5H_2O$	65.6121
<i>Saponite-Mg</i>	$Mg_{3.165}Al_{.33}Si_{3.67}O_{10}(OH)_2 + 7.3200 H^+ = + 0.3300 Al^{+++} + 3.1650 Mg^{++} + 3.6700 SiO_2 + 4.6600 H_2O$	26.2523
<i>Nontronite-Mg</i>	$Mg_{.165}Fe_{2}Al_{.33}Si_{3.67}H_2O_{12} + 7.3200 H^+ = + 0.1650 Mg^{++} + 0.3300 Al^{+++} + 2.0000 Fe^{+++} + 3.6700 SiO_2 + 4.6600 H_2O$	-11.6200
<i>Talc</i>	$Mg_3Si_4O_{10}(OH)_2 + 6.0000 H^+ = + 3.0000 Mg^{++} + 4.0000 H_2O + 4.0000 SiO_2$	21.1383
<i>Mesolite (Zeolite)</i>	$Na_{.676}Ca_{.657}Al_{1.99}Si_{3.01}O_{10} \cdot 2.647H_2O + 7.9600 H^+ = + 0.6570 Ca^{++} + 0.6760 Na^+ + 1.9900 Al^{+++} + 3.0100 SiO_2 + 6.6270 H_2O$	13.6191
<i>Stilbite (Zeolite)</i>	$Ca_{1.019}Na_{.136}K_{.006}Al_{2.18}Si_{6.82}O_{18} \cdot 7.33H_2O + 8.7200 H^+ = + 0.0060 K^+ + 0.1360 Na^+ + 1.0190 Ca^{++} + 2.1800 Al^{+++} + 6.8200 SiO_2 + 11.6900 H_2O$	1.0545

190

191 3.2. Mineralogical analysis and kinetic information

192 The mineralogical composition of the BVG rock used in the experiment is shown in Table 3. The
 193 concept of MKE was applied to the minerals existing in the rock that react with the ENFG leachate.

194 The initial mass of each reactant was calculated based upon its abundance in the 35 g BVG sample
 195 (Rochelle et al. 2016; Rochelle et al. 1997). Note that the original rock sample showed some traces
 196 of other fracture filling phases such as clays, but these were not included in the model.

197

198

199

200 Table 3: BVG rock sample composition. Analysis conducted by the British Geological Survey (Rochelle et al. 2016;
201 Rochelle et al. 1997). The mass of each phase (m_0) is calculated based on a 35g rock sample.

Mineral	Weight %	m_0 (g)
Orthoclase	12	4.2
Quartz	41	14.35
Dolomite	29	10.15
Muscovite	13	4.55
Hematite	2	0.7
Calcite	3	1.05

202

203 When cement leachate encounters the surrounding host rock, they will be out of chemical
204 equilibrium, and local dissolution of existing ‘primary’ minerals will occur. The process releases
205 new solutes into the reaction system, resulting in the precipitation of new ‘secondary’ minerals.
206 Some secondary phases can have enhanced sorption and permeability-limiting properties relative
207 to the primary phases, and are thus beneficial in term of limiting radionuclide migration. Thus it
208 is important to be able to describe/model the temporal evolution of these phases.

209

210 Commonly, the rate of mineral dissolution is measured experimentally by measuring the rate of
211 change in solute concentration as a function of time under ‘far from equilibrium’ conditions. To
212 model the experimental values of dissolution and precipitation, a variety of factors must first be
213 addressed, which include: the reactive surface area of the mineral, initial and final amounts, the
214 specific dissolution rate constant, and slowing of reaction as equilibrium is approached. The
215 availability of these data is one of the challenges in the field of modelling mineral dissolution and
216 precipitation. The MKE approach is implemented to overcome that drawback with a proper
217 representation of the geochemical system. Equation 1 is a general form that is usually used to
218 calculate the overall dissolution rate of minerals (Appelo and Postma 2005; Parkhurst and Appelo
219 1999; Rimstidt and Barnes 1980).

220

221
$$R_k = r_k \frac{A_0}{V} \left(\frac{m_k}{m_{0k}} \right)^n \quad (1)$$

222 where

223
$$r_k = k_k \left(1 - \left(\frac{IAP}{K} \right)_k \right) \quad (2)$$

224

225 R is the overall dissolution rate into solution ($\text{mol L}^{-1} \text{s}^{-1}$), k_k is the specific dissolution rate
226 ($\text{mol/m}^2/\text{s}$), A_0 is the initial surface area (m^2), V is the solution volume (L), m is the moles at a
227 given time and m_0 is the initial moles. $(m_k/m_{0k})^n$ is an interpretation of the changes in the reactive
228 surface area as a result of changes in the size of the mineral during the dissolution process. The
229 value of $n = 2/3$ (Appelo and Postma 2005). (IAP/K) (i.e., ion activity divided by equilibrium
230 constant) is equal to the saturation ratio (SR) of the reactant.

231

232 It is worth noting that clay minerals were not the focus of the original experiment, and that the
233 exact mica/clay phase(s) present in the fracture of the BVG rock were not fully identified (Moyce
234 et al. 2014). However, muscovite was chosen to represent this phase(s) in the modelling process
235 to control aluminium concentration in solution. Table 4 shows the kinetic information (reaction
236 rate constant, reactive surface area, solution volume) obtained from the literature for the minerals
237 in BVG that were modelled by the MKE approach (k-feldspar, quartz, dolomite, calcite,
238 muscovite). Conversely, hematite was modelled by the equilibrium approach only, because of its
239 low percentage in the rock sample (2%) and its assumed minimal influence on the mineralogical
240 evolution process. In terms of the precipitation process, for most minerals the kinetics and specific
241 rates of precipitation are unknown. Therefore, the precipitation of secondary phases was modelled
242 assuming control by thermodynamic equilibrium.

Mineral	Modelling	Solution Volume (L)	Surface area (m ² /g)	Rate constant (mol m ⁻² s ⁻¹)
Orthoclase	MKE	0.14 (Rochelle et al. 2016)	0.02 (De Windt et al. 2008)	k (using equation 5) (Appelo and Postma 2005)
Quartz	MKE		0.02 (De Windt et al. 2008)	$k = 1 \times 10^{-12.2}$ (70°C) (Worley 1994)
Dolomite	MKE		0.02 (De Windt et al. 2008)	$k = 1.2 \times 10^{-12}$ (Appelo and Postma 2005) This value was lowered two orders of magnitude ($k = 1.2 \times 10^{-10}$)
Muscovite	MKE		1.1 (Knauss 1989)	$k = 10^{-18.1}$ (Knauss 1989)
Calcite	MKE		0.02 (De Windt et al. 2008)	$k_1 = 10^{(0.198 - 444.0 / (273.16 + T))}$ $k_2 = 10^{(2.84 - 2177.0 / (273.16 + T))}$ $k_3 = 10^{(-1.1 - 1737.0 / (273.16 + T))}$ in which T denotes temperature. (Appelo and Postma 2005; Plummer et al. 1978)
Hematite	Equilibrium	-	-	-

244

245 1) *Quartz (SiO₂)*

246 As per equation (1) and (2), the overall dissolution kinetic equation for quartz will be:

247
$$R_{Quartz} = k_{Quartz} \left(\frac{A_0}{V} \right) \left(\frac{m}{m_0} \right)^{0.67} \left(1 - \left(\frac{IAP}{K} \right)_{Quartz} \right) \quad (3)$$

248

249 2) *K-feldspar (KAlSi₃O₈)*

250

251 The overall dissolution rate proposed by (Appelo and Postma 2005; Parkhurst and Appelo 1999)

252 is used to simulate k-feldspar reaction at specific temperatures and pH value:

253
$$R_{K-feldspar} = k_{K-feldspar} \left(\frac{A_0}{V} \right) \left(\frac{m}{m_0} \right)^{0.67} \left(1 - \left(\frac{IAP}{K} \right)_{K-feldspar} \right) \quad (4)$$

254 where

255
$$k_{K-feldspar} = k_{H^+} \frac{[H^+]^n}{f_H} + k_{H_2O} \frac{1}{f_{H_2O}} + k_{OH^-} \frac{[OH^-]^o}{f_{OH}} + k_{CO_2} \frac{[P_{CO_2}]^{0.6}}{f_{CO_2}} \quad (5)$$

256

257 where $k_{K-feldspar}$ is the specific reaction rate ($\text{mol m}^{-2} \text{s}^{-1}$), k_i are the solute rate coefficients (mol
 258 $\text{m}^{-2} \text{s}^{-1}$), and f_i are inhibition factors.

259

260 3) Calcite (CaCO_3)

261

262 The specific dissolution rate for calcite was described by (Appelo and Postma 2005; Parkhurst and

263 Appelo 1999; Plummer et al. 1978):

264

$$265 \quad r_{\text{calcite}} = [k_1[\text{H}^+] + k_2[\text{H}_2\text{CO}_3] + k_3[\text{H}_2\text{O}]] * \left[1 - \left(\frac{\text{IAP}}{K} \right)_{\text{Calcite}}^{\frac{2}{3}} \right] \quad (6)$$

266

267 from equation (1), the overall dissolution rate of calcite will then be:

268

$$269 \quad R_{\text{calcite}} = r_{\text{calcite}} \left(\frac{A_0}{V} \right) \left(\frac{m}{m_0} \right)^{0.67} \quad (7)$$

270

271 The value of the coefficients k_1 , k_2 and k_3 in equations (6) are calculated by (Plummer et al. 1978)

272 by fitting them to the experimental data as a function of temperature.

273

274 4) Dolomite [$\text{CaMg}(\text{CO}_3)_2$]

275 The specific dissolution rate of dolomite is described below by (Appelo et al. 1984; Appelo and

276 Postma 2005; Parkhurst and Appelo 1999).

$$277 \quad r_{\text{Dolomite}} = -k_{\text{Dolomite}} \log \left(\frac{\text{IAP}}{K} \right)_{\text{Dolomite}} \quad (8)$$

278 then, the overall dissolution rate of dolomite will be:

279

$$280 \quad R_{\text{Dolomite}} = r_{\text{Dolomite}} \left(\frac{A_0}{V} \right) \left(\frac{m}{m_0} \right)^{0.67} \quad (9)$$

281

282 5) *Muscovite* [$KAl_2(AlSi_3O_{10})(OH)_2$]

283

284 The specific dissolution rate for muscovite was calculated from the below equation, which was
285 described by (Knauss 1989):

$$286 \quad r_{Muscovite} = 10^{-18.1}[a_{H^+}]^{+0.22} \quad (10)$$

287 then, as per equation (1), the overall dissolution rate of muscovite will be:

288

$$289 \quad R_{Muscovite} = r_{Muscovite} \left(\frac{A_0}{V}\right) \left(\frac{m}{m_0}\right)^{0.67} \quad (11)$$

290

291 *3.3.Fluid evaporation*

292 Over the 15-year experiment period, (Rochelle et al. 2016; Rochelle et al. 1997) note that some of
293 the reacting fluid was lost, most likely through diffusion around the threads in the steel vessel.

294 Measures were not taken to limit this process, because the experiments were only initially planned
295 to only run for <18 months. The extent of this process could be estimated based on measured

296 increases in the concentration of conservative (i.e. inactive) dissolved ions in the experiment. In
297 both ENFG experiments (blank and reactive), the chloride ion was set as the inactive and

298 conservative species over the entire experiment period. It was observed that the rate of change in
299 chloride ion concentration was the same in both solutions, and amounted to a 34% fluid loss

300 (Moyce et al. 2014). It is crucial that modelling includes this fluid loss since this loss affects the
301 concentration value (usually measured in mg/L) of all the ions released into the solution. In the

302 modelling procedure, the simulated result of the chloride ion concentration indicated only a 22%
303 fluid loss.

304

305

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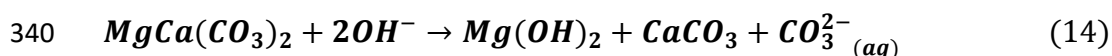
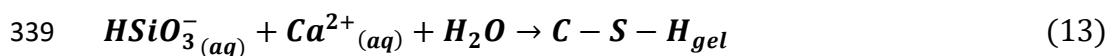
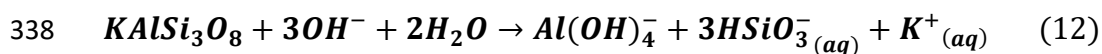
307 *3.4.Secondary phases*

308 During the reaction period of 15 years, the chemical characteristics of the system would
309 significantly evolve and result in multiple cycles of mineral dissolution and precipitation reactions.
310 The type of precipitated secondary mineral can vary over the entire experimental period. In this
311 study, two time periods were defined: from 0 to 15 months (short-term mineral evolution) and
312 from 15 months to 15 years (long-term mineral evolution). In numerical simulations, the
313 specification of each expected secondary mineral was defined to allow its precipitation after
314 saturation. In the modelling process, attention was paid to minerals that were actually observed in
315 the experiments, together with ones that might precipitate (i.e. with saturation index close to zero),
316 in order to achieve more accurate results. Moreover, the list of secondary minerals being tracked
317 during the modelling should reasonably embrace the range of chemical ions represented in the
318 experiment. Finally, the stability range of realistic secondary phases being modelled should be
319 coincident with the experimental conditions (e.g. especially temperature and pH).

320

321 Several previous experimental studies have shown that when high-pH calcium-bearing cement
322 leachate reacts with the host rock in the CDZ, the primary silicate dissolves, followed mostly by
323 the precipitation of secondary CSH phases with different calcium-to-silicon ratios (Bateman et al.
324 1999; Braney et al. 1993; Gaucher and Blanc 2006; Hodgkinson and Hughes 1999; Mäder et al.
325 2006; Savage and Rochelle 1993). Where the system also includes aluminosilicate minerals
326 (Equations 12 and 13) and potassium (from minerals or the cement leachate), then secondary
327 phases of aluminium- and potassium-bearing minerals (C-[Al]-[K]-S-H) also precipitate (Braney
328 et al. 1993; Savage et al. 1992). Carbonate minerals, especially dolomite, can also play a significant
329 role in the precipitation of other, secondary carbonates (e.g., calcite, Equation 14) when reacting

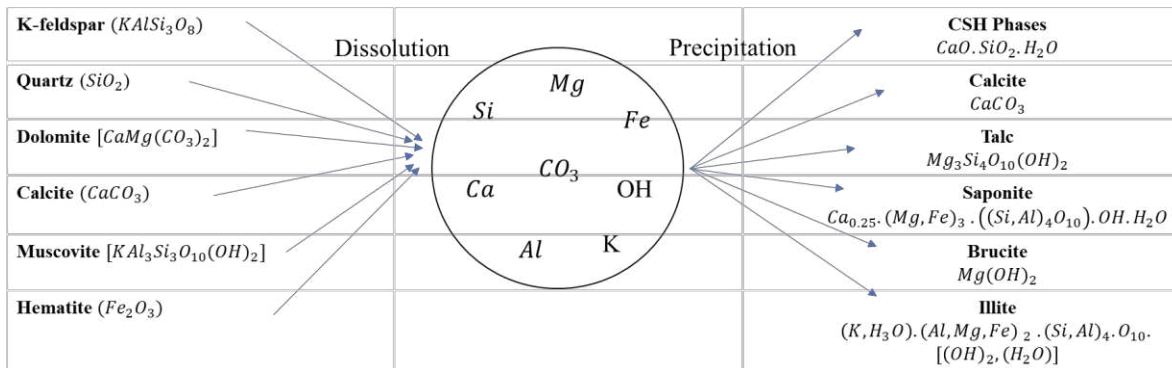
330 with cement porewater leachate (Braithwaite and Heath 2013; Poole and Sotiropoulos 1980). Their
 331 relatively fast dissolution reaction compared to silicate minerals can control fluid chemistry during
 332 the early stages of the reaction (Bérubé et al. 1990; Choquette et al. 1991). Modelling studies have
 333 also shown that the reaction time and the composition of the primary solution (e.g., pH) are the
 334 two dominant factors in controlling the precipitating phases. Those studies also indicate that over
 335 time, CSH gel will evolve into zeolite, feldspar and CSH minerals (Bateman et al. 1999; Braney
 336 et al. 1993; Fernández et al. 2010; Pfingsten et al. 2006; Savage et al. 1992; Savage and Rochelle
 337 1993; Soler and Mäder 2007).



341 As the BVG rock sample was rich in dolomite, it was assumed that the dedolomitization process
 342 would result in an enormous number of magnesium and carbonate ions. This indicates that aqueous
 343 calcium ions can also be a driving force for the dissolution process of dolomite, as well as the fluid
 344 pH level. At the beginning of the experiments (from 0 to 15 months), there was a low concentration
 345 of calcium ions in the YNFP, which led to undersaturation with respect to calcite and its
 346 dissolution. However, in the ENFG fluid, the system had a high concentration of calcium ions,
 347 which consumed all the aqueous ions of carbonate ($\mathbf{CO_3}^{2-}$) to form the secondary calcite. Since
 348 the rock sample also included quartz and feldspar, the released magnesium ions were expected to
 349 react with both aqueous calcium and silica to form a secondary (Ca)-Mg-(Al)-(K)-silicate and
 350 ettringite (In case sulphate ions were in the solution), as demonstrated in the literature (Derkowski
 351 et al. 2013; Galí et al. 2001; Garcia et al. 2020; Schwarzenbach et al. 2013; Techer et al. 2012;
 352 Tinseau et al. 2006; Xie et al. 2013). Studies have also confirmed the formation of talc, smectite

353 (Mg-saponite), illite and brucite as secondary Mg-rich phases during the dedolomitization process
 354 (Chen et al. 2018; Moyce et al. 2014; Rochelle et al. 2016). Figure 3 shows the conceptual model
 355 for mineral evolution during the dissolution and precipitation cycle of BVG rock reaction with
 356 ENFG fluid.

357



358

359 Figure 3: Conceptual model for minerals evolution during the dissolution and precipitation cycle of BVG reaction
 360 with ENFG.

361

362 4. Results and discussion

363 The reaction of BVG rock with ENFG was modelled over a simulated 15-year duration using the
 364 MKE approach. Changes in the concentration of Ca, Mg, Na, K, Al, Si, CO₃ and pH, as measured
 365 from the experiment, were analysed in the modelling simulations, and the comparison is shown in
 366 Figures 4–8. As an inactive ion, the chloride concentration (Figure 4, Plot A) increased in the
 367 solution as a result of the evaporation process, in line with the experimental data. Furthermore,
 368 since none of the primary minerals in the original rock sample included sodium and the potential
 369 secondary phases did not significantly consume sodium, the increase in sodium concentration (Plot
 370 A) also appears to be mainly a result of the evaporation process. This indicates that the sodium ion
 371 is also a conservative species in this geochemical system.

372

373 The dissolution process of quartz, which accounts for 41% of the BVG rock, released a significant
374 amount of silicon into the highly alkaline solution in the first few months (Plot B). The availability
375 of silicon ions along with the initial calcium concentration (plus calcium released from the
376 dissolution of dolomite) then promoted the precipitation of secondary CSH and CASH phases,
377 represented by a sharp drop in silicon concentration along with a decrease in calcium concentration
378 (Plot C). The increase in potassium concentration (Plot D) was mostly linked to the evaporation
379 plus the dissolution of k-feldspar and muscovite, which also released silicon and aluminium. This
380 can be seen in the numerical results of Plot E, which show a small increase in aluminium
381 concentration in the first few months. The concentration line then drops heavily and follows the
382 experimental behaviour as a result of forming secondary aluminosilicate phases. The saturation
383 index lines in Figure 5 show that k-feldspar and muscovite both start with a higher dissolution rate
384 than quartz, which defines the small peak in aluminium concentration in the beginning before it
385 drops down as secondary calcium silicates start to precipitate. The figure also shows that muscovite
386 was always undersaturated, and thus would have continued to dissolve, providing a source of
387 aluminium for secondary phases. Moreover, the precipitation rates for talc, CSH gel and
388 tobermorite (CSH) were all high in the first few months of the reaction (Figure 7). This high
389 precipitation was mirrored by a substantial drop in silicon, aluminium and calcium concentrations
390 at almost the same time. Note that in Figure 7, the positive value is for the dissolving process,
391 whereas, negative for the precipitation process. Both CSH gel and tobermorite precipitated initially
392 and redissolved after 18 months, with a similar kinetic rate. Talc started to precipitate from the
393 beginning of the experiment and reached a stable amount after around 18 months. The initial
394 concentration of magnesium in the leachate, plus that released during dedolomitization, drove
395 brucite precipitation in the high pH conditions and created a sink for Mg (Bérubé et al. 1990;

396 Cheng 1986), which also consumed hydroxyl ions and reduced the pH value. This rapid drop in
397 pH in the first few months (Figure 4, Plot H) is also reflected in Figure 6, which shows a higher
398 precipitation rate of brucite in the same period. Subsequently, the drop in the pH value
399 progressively continued, but at a slower rate. From Figure 4 (Plot F), it is also clear that the initial
400 magnesium ions were consumed in the first few months before the dedolomitization process took
401 control. The saturation index of dolomite (Figure 5) shows that it was undersaturated (dissolving)
402 in the geochemical system, but with a much slower rate as the pH value went below 9. This agrees
403 with literature information (Min and Mingshu 1993), which suggests that dedolomitization does
404 not occur below pH 11. Despite that, dedolomitization still occurred in the geochemical system,
405 but at a very slow rate. This is demonstrated by the high magnesium concentration (Evaporation
406 can also play a part in this increase as well) at the end of the 15 years (Figure 4, Plot F), which was
407 observed in the experiment as well (Moyce et al. 2014). The escalation of dedolomitization can be
408 caused by the high concentration of Ca^{2+} in the ENFG, which promotes this process even at lower
409 pH values. Dedolomitization provides calcium and aqueous CO_3^{2-} , which are removed effectively
410 (Figure 4, Plot G) from the system by the precipitation of calcite (Bérubé et al. 1990). This can be
411 seen in the saturation indices of calcite and brucite (Figure 6), which both precipitate in
412 concurrence with the consumption of CO_3^{2-} . The extra amount of CO_3^{2-} in Equation 14 plus the
413 amount released from the dissolution of calcite at later stages of the experiment is also reflected in
414 Figure 4 (Plot G) which shows a small increase in (CO_3^{2-}) concentration. Thus, to incorporate the
415 slow dedolomitization process in the modelling, the specific dissolution rate of dolomite was
416 lowered by two orders of magnitude. This compensates for the slower dolomitisation process
417 below pH 11 but at the same time allows the process to take place, driven by the high concentration
418 of calcium ions, especially at the early stage of the reaction. Another indication that supports the

419 dedolomitization process is the high precipitation rate of Mg-silicate (talc and saponite-Mg), which
420 was reflected by the higher dissolution rate of dolomite in the same period. Since brucite was close
421 to saturation after the first few months (Figure 6), most of the released magnesium from the
422 dedolomitization process was likely consumed during the formation of magnesium-silicate
423 minerals, which is also recognised in other literature (Eglinton 1998; Glasser 2001).

424

425 After the large drop in the pH value, tobermorite and CSH gel starts to dissolve; at that time, a
426 substitution between aluminium and silicon ions takes place to produce more stable calcium
427 aluminosilicate hydrate (Myers et al. 2015; Richardson 2014; Richardson et al. 1993). This
428 secondary CASH phase can then bind with the magnesium from the dedolomitization and create
429 Mg-aluminosilicate (Galí et al. 2001; Moyce et al. 2014). This phenomenon highlights the
430 importance of the modelling procedure for this kind of complex long-term geochemical reaction,
431 as it allows a better understanding of the potential chemical and physical reactions that occur in
432 the geosphere. It can also allow the extension of the timescale from relatively short-duration lab
433 tests to the long timescales of performance assessments. Additionally, it can reveal the type of
434 dissolved or precipitated secondary minerals that can contribute effectively to the retardation of
435 radionuclide migration. For example, zeolites would be useful secondary phases as they have a
436 high sorption capability to the radionuclide. Their considerable surface area and ion exchange
437 capacity could play a key role in retarding radionuclide migration. Unfortunately, no evidence of
438 zeolite precipitation was found in any of the NSARP experiments (Moyce et al. 2014; Rochelle et
439 al. 2016). A plausible explanation for this is the rapid removal of silicon and aluminium by CSH
440 and CASH phases that could suppress the formation of zeolites as they may have slower kinetic
441 precipitation. Even though the modelling results obtained from the geochemical analysis showed

442 potential for mesolite, stilbite and scolecite precipitation (based on the temperature of the
443 experiment), which all are part of the zeolite family (Figure 8; (Bucher and Stober 2010; Bucher
444 and Weisenberger 2013; Fridriksson et al. 1999; Weisenberger and Selbekk 2009)).

445
446 Even though those minerals did not precipitate in the experiment, this does not prove that the
447 situation will be the same in the actual geosphere. The experimental design tried to mimic the
448 actual environmental conditions as much as possible (rock type, temp, pH, etc.). However, there
449 are still some variances, which can lead to different results. For example, as reported by (Adler et
450 al. 1999), zeolite formation is preferred in the pore spaces in which leachate flux is minimal, and
451 in these experiments the leachate: rock ratio was very high. The composition and nature of the
452 rock type can also play a significant role, as it can affect the amount of CO₂ released into the
453 leachate (e.g., depending on dolomite percentage), which can buffer the formation of zeolites
454 (Mullis et al. 1994; Weisenberger and Bucher 2010). Taken together, the findings reveal the
455 potentially important role of dolomite in the geochemical system. Moreover, they provide valuable
456 insight into specific geochemical processes alongside the usefulness of iterating between
457 modelling and experimental results to achieve a better understanding of the system under study.

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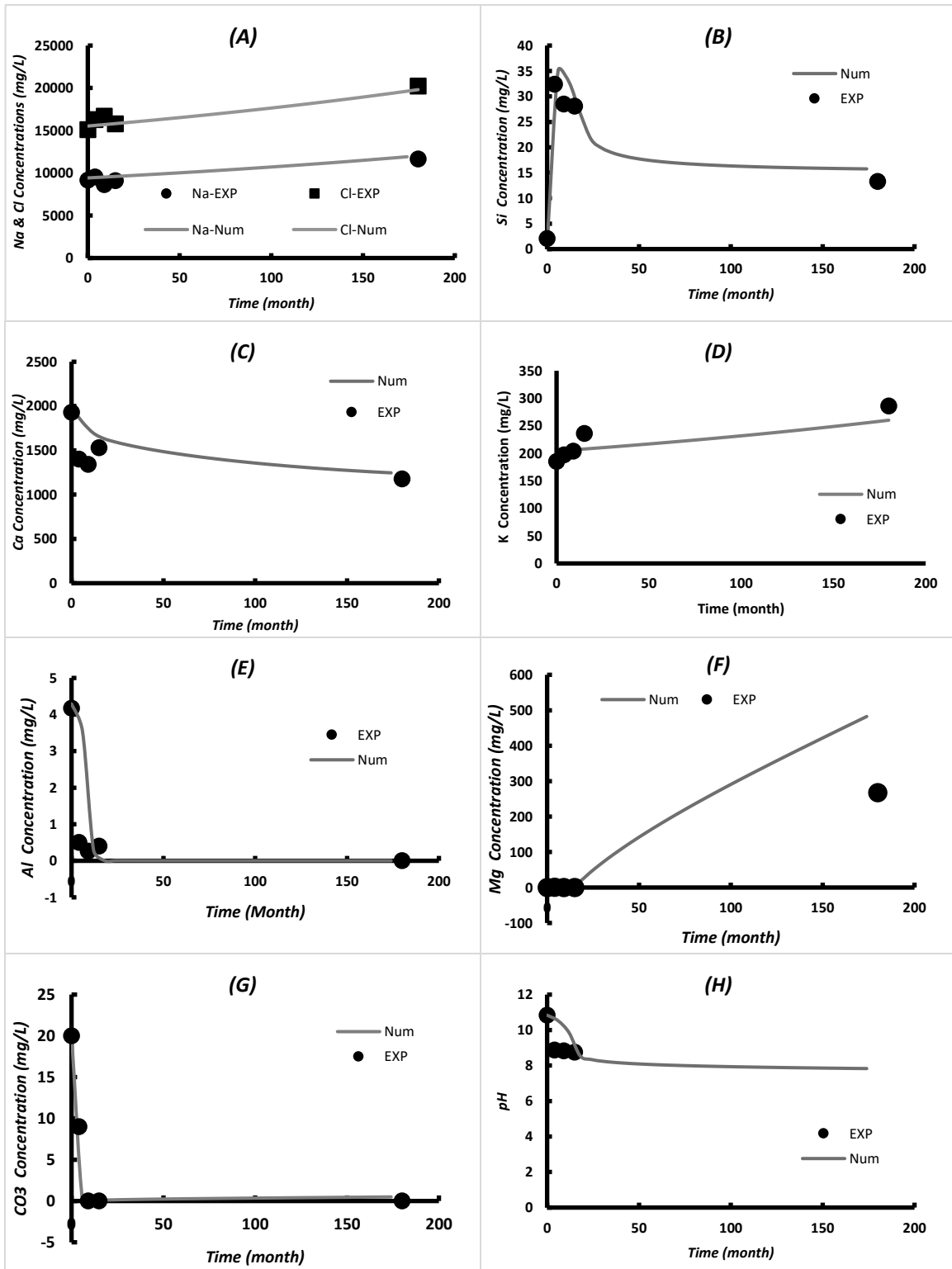
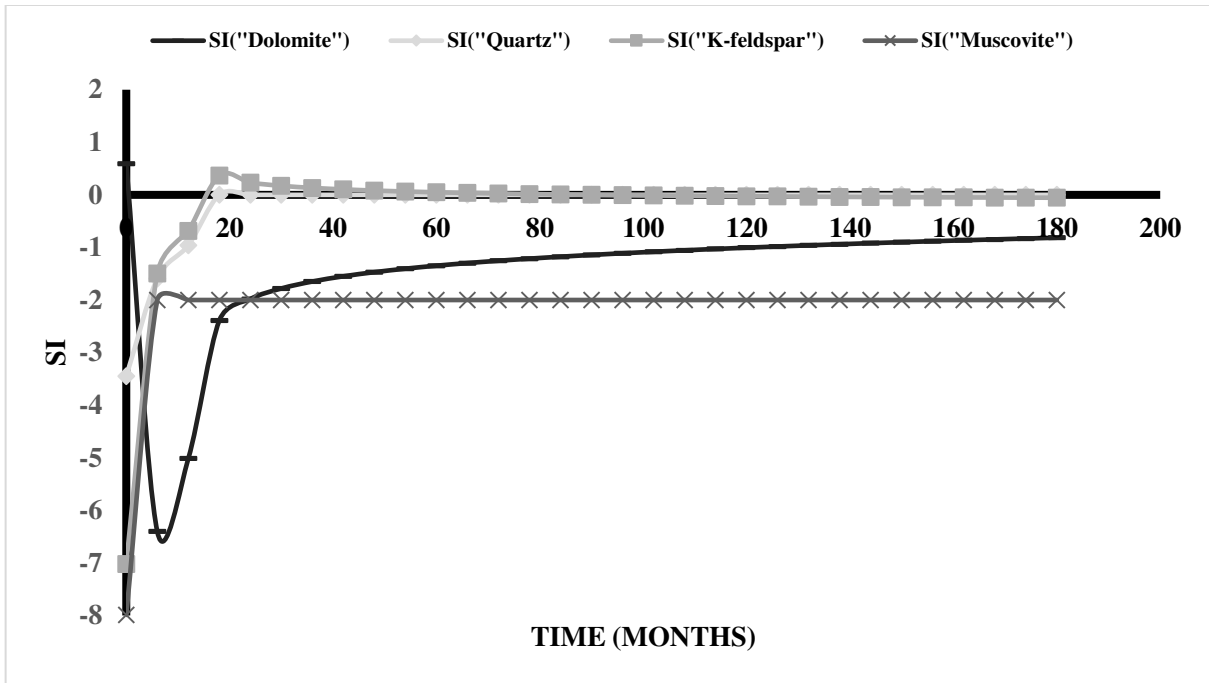


Figure 4: Modelled and experimental values for ions concentration and pH versus time.



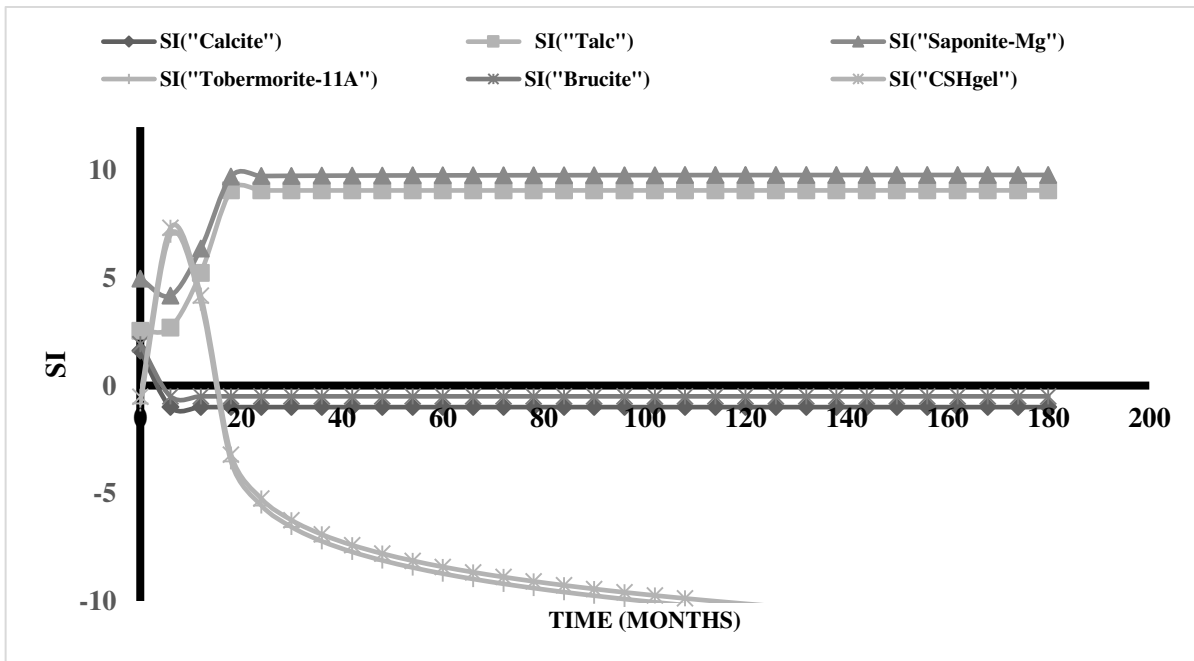
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Figure 5: Saturation indices of primary mineral versus time.

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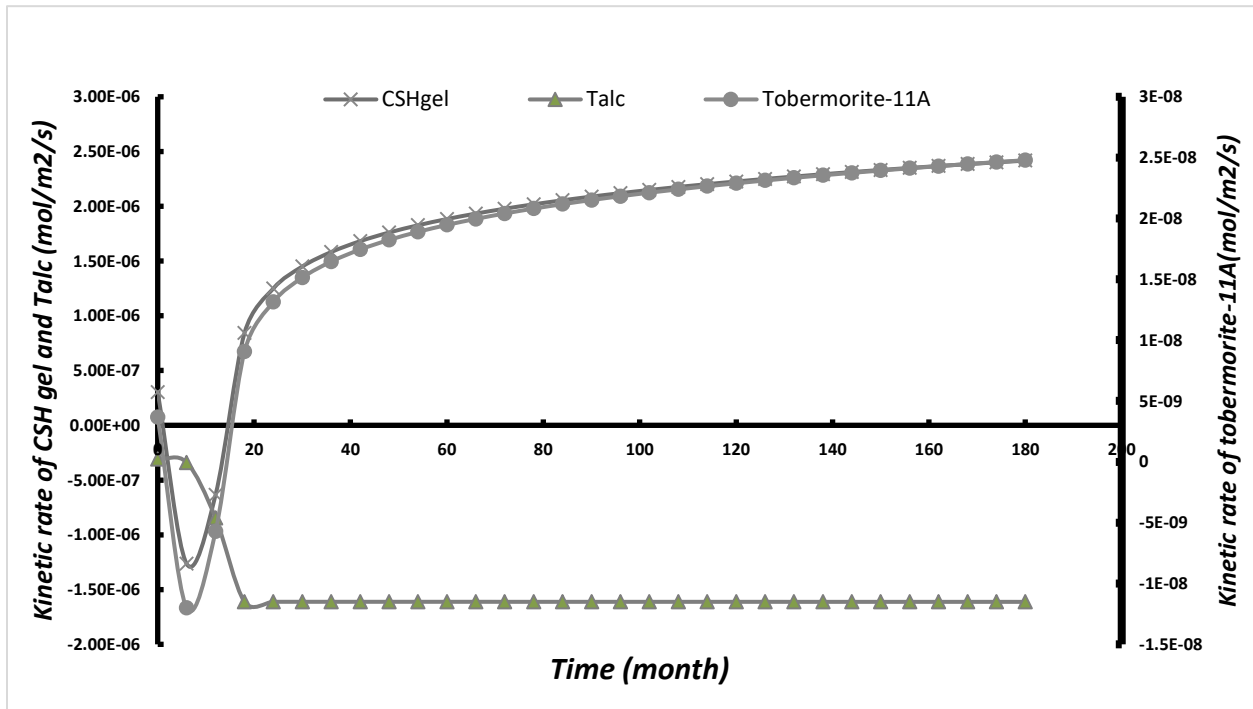
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Figure 6: Saturation indices of secondary phases versus time.

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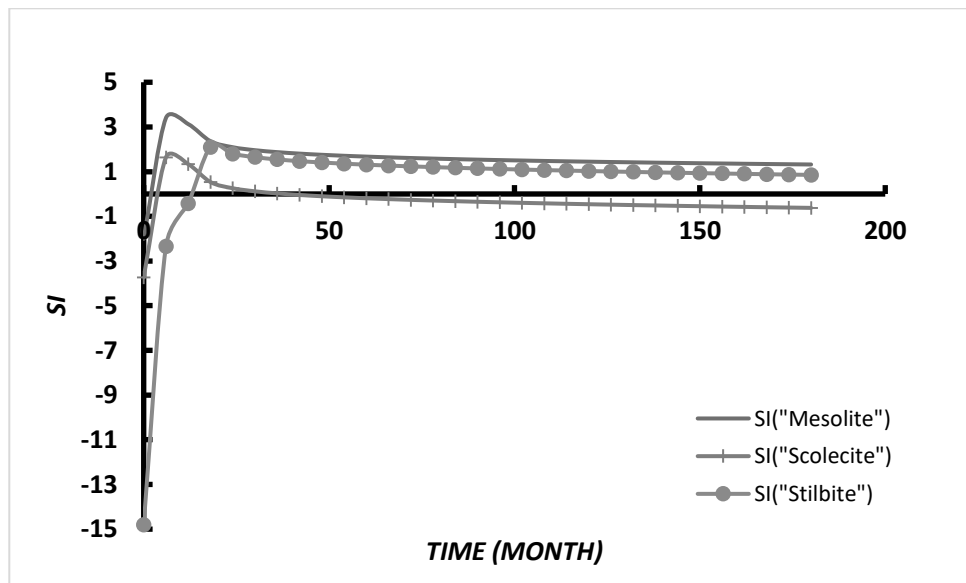
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Figure 7: Kinetic rates for CSH gel, talc and tobermorite-11A versus time.

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Figure 8: Zeolites minerals saturation indices versus time.

482

483 **5. Conclusion**

484

485 The construction of a cement-based, deep underground geological disposal facility for radioactive
486 waste will result in an alkaline plume when groundwater equilibrates with minerals in the cement
487 barrier. This will initiate a series of dissolution/precipitation reactions in the surrounding host rock,
488 and consequent changes in physical, hydraulic, chemical and sorption properties long before any
489 potential migration of radionuclides. It is useful to understand and to be able to predict these
490 changes, as they are likely to influence the potential retardation of future radionuclide migration.
491 This study modelled the mineralogical evolution and geochemical reactions of BVG rock in
492 contact with ENFG. Importantly, the rock sample comprised a hydraulically-conductive dolomite-
493 rich fracture, and though dolomite is only a minor phase in the rock overall, it is a major phase in
494 direct contact with current groundwater. Simulations were conducted using PHREEQC, and
495 predictions compared with data from experiments lasting up to fifteen years. The results showed
496 that: (1) secondary phases such as talc, brucite and Mg-aluminosilicate precipitated, driven by
497 dedolomitization; (2) solution pH initially dropped quickly as a result of brucite precipitation; (3)
498 although zeolites were predicted stable secondary phases, they were absent in the experiments,
499 possibly as a consequence of factors such as slow reaction kinetics, high leachate-to-rock ratios or
500 elevated CO₂ concentrations. Overall, the modelling results of these long-term experiments
501 indicate the important role of fluid-mineral reactions in controlling fluid chemistry and secondary
502 phases, and so sufficient attention should be focused on the mineralogical composition of flowing
503 features, as the minerals lining those can exert a critical influence on key geochemical reactions.

504

505

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511

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