

# The evolution of microstructure and electrical performance in doped Mn-Co and Cu-Mn oxide layers with the extended oxidation time

P.Y. Guo<sup>1</sup>, H. Sun<sup>1</sup>, Y. Shao<sup>1\*</sup>, J.T. Ding<sup>1</sup>, J.C. Li<sup>1</sup>, M.R. Huang<sup>1</sup>, S.Y. Mao<sup>1</sup>, Y.X. Wang<sup>1</sup>, J.F. Zhang<sup>2</sup>, R.C. Long<sup>3</sup>,  
X.H. Hou<sup>4</sup>

1 School of Materials Science and Engineering, Jiangsu University of Science and Technology, Jiangsu 212003, China

2 School of Electronics and Information Engineering, Suzhou Vocational University, Jiangsu 215104, China

3 School of Foreign Studies, Yanshan University, Hebei 066004, China

4 Faculty of Engineering, The University of Nottingham, Nottingham, NG7 2RD, UK

**Abstract:** Mn-Co and Cu-Mn based alloy coatings are deposited on 430 SS by high energy micro-arc alloying process, and then alloy coatings are oxidized at 750 °C in air to form the spinel oxides. Some composite oxides, such as  $\text{Co}_3\text{O}_4$ ,  $\text{Mn}_2\text{O}_3$  and  $(\text{Mn},\text{Co})_3\text{O}_4$ , are formed at the initial stage of oxidation. The single-phase spinel (pure  $\text{MnCo}_2\text{O}_4$ ) without impurity phases is only found on the surface of Co-33Mn-17Cu oxide layer with the extended oxidation time, its area-specific resistance values at 500 °C to 800 °C are low and close to that of Mn-35Cu oxide layer which mainly composed of  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  spinel.

**Keywords:** single-phase spinel; microcrystalline coating; high energy micro-arc alloying process; evolution

## 1. Introduction

Besides the excellent high-temperature oxidation resistance, Mn-Co based spinel has the high conductivity and the appropriate coefficient of thermal expansion (CTE) matching the metallic interconnects and other components of solid oxide fuel cell (SOFC)[1-4]. To improve the properties and sintering ability, some active elements and transition metals have been doped into Mn-Co based spinel, such as Ce, Ni, Fe or Cu, which can modify the CTE, enhance the densification and reduce the sintering temperature of  $\text{MnCo}_2\text{O}_4$  [2,3].

The incorporation of active elements into alloy coatings will generally cause different effects on the high temperature oxidation behavior of coatings, such as enhancing the selective oxidation, changing the transformation mechanism, decreasing the growth rate of  $\text{Cr}_2\text{O}_3$  at the substrate/coating interface, and improving the adhesion between oxide coating and substrate. When NiFe-CeO<sub>2</sub> alloy coatings are electrodeposited onto 430 SS [5], the addition of CeO<sub>2</sub> reduces the growth rate of  $\text{Cr}_2\text{O}_3$  and the number of pores near the oxide/substrate interface, with a higher coating electrical conductivity. In another report, Co-38Mn-2Dy alloy layer is prepared by high energy micro-arc alloying process [6], and the addition of Dy effectively improves the oxide scale adhesion and decreases the oxidation rate of coating. Lanthanum (La) is a basic element in the traditional perovskite cathodes and interconnects of SOFC, so Mn-Co based spinel coatings with Lanthanum will also be an important research content in this work.

Cu-Mn metallic coatings [7] are deposited on SUS 430 via magnetron sputtering process. The results show that the converted  $(\text{Mn,Cu})_3\text{O}_4/\text{CuO}$  oxide layers suppresses Cr outward diffusion and improves the electrical performance of metallic interconnects. Cu-Mn spinel coatings[8] are also deposited by electrophoretic deposition process, followed by a thermo-mechanical treatment, and the coatings after oxidation have a dense layer near the oxide/substrate interface, a porous outer layer and a CuO layer on the coating surface. Owing to its high conductivity and the matched CTE with metallic interconnects, Cu-Mn based spinel coatings are garnering the increasing attention compared to traditional Mn-Co based spinels [9,10].

The expanded application of spinel coatings is now subjected to its poor adhesion, homogenization and densification. In recent attempts, the high-energy micro-arc alloying (HEMAA) process has been used to produce the metallurgically bonded alloy coatings which are then converted *in-situ* into spinel coatings by the thermal growth process [11-15]. Some reports have studied the oxidation behavior and electrical property of  $\text{LaCrO}_3$ -based coatings, Mn-Co and Cr-La alloying layers deposited by the HEMAA process [16,17], confirming that the coating prepared by this process offers the excellent adhesion to the substrate and keeps low electrical contact resistance for the

interconnects.

The single-phase Mn-Co or Cu-Mn based spinel without impurity phases is generally hard to form, even they are the calcined body synthesized by solid-state reaction, because some impurity oxide phases would be formed by the decomposition in the solid solution of cubic spinel [18,19]. Therefore, it becomes more difficult to prepare the pure single-phase spinel coatings, due to the phase diagram, restricted reaction temperature, pressure and other reaction conditions for metallic interconnects. In this experiment, Cu-Mn, Mn-Co and La/Cu doped Mn-Co alloy coatings are deposited on 430 SS substrate by the HEMAA process. The microstructure and electrical performance of the alloy coatings with the extended oxidation time are discussed in details. This work aims to investigate the formation process of the pure single-phase spinel coatings, and elucidate the underlying mechanisms in such process.

## **2. Experiments**

### **2.1 Preparation of alloys and coatings**

Type 430 stainless steel is used as the substrate (cathodes for HEMAA process) and its nominal composition is 16-18 Cr, 1 Mn, 0.12 C, 0.75 Si, 0.03 S, 0.06 Ni, 0.04 P, and balance Fe (wt. %). Alloy ingots of Co-33Mn-17Cu (Cu doped Mn-Co), Mn-35Cu, Co-38Mn-2La (La doped Mn-Co) and Co-35Mn (at.%) is pre-prepared by argon arc melting of high purity metals (99.99 wt.%). The molar ratios of element Cu/Mn and Mn/Co in the alloys are designed to be between 1.0:2.0 and 1.5:2.0. The alloy ingots are cut into the specific rods as anodes for HEMAA process. The details for deposition process of alloy layers have been described in previously published articles [20-22].

### **2.2 Oxidation experiment and area-specific resistance testing**

The thermal oxidation experiments are conducted at 750°C in air in a horizontal tube furnace (Hengli-CHLZG, Luoyang, China). The coated substrates are suspended ahead in the constant temperature zone of the furnace, and then the temperature gradually rises to 750°C. After oxidation for 20h, 100h, 300h, and 500h, samples are respectively taken out from the furnace and directly cooled to room temperature (RT). The mass gain of samples is weighed at room temperature after cooling using an electronic balance with an accuracy of 0.01 mg.

The area-specific resistance (ASR) measurement of oxide layers is based on the four-probe DC method with the applied voltage 5 V and contact area 10 mm<sup>2</sup> by Pt plate. Every setting temperature (per 100 °C from 500 °C-800 °C) keeps stable for at least one hour for the accuracy of resistance reading [20-22].

### 2.3 Microstructure analysis

The phase structures of oxide scale on the surface are identified with X-ray diffraction (XRD) (D/MAX-3B, Rigaku Co., Tokyo, Japan). The oxidized samples are embedded into a cold-setting epoxy resin for the cross-section morphology analysis by scanning electron microscopy (SEM) (JSM-5800, JEOL, Tokyo, Japan). The surface morphology and elemental homogeneity in oxide layers are examined by SEM with energy dispersive X-ray spectroscopy (EDS).

## 3. Results and Discussion

### 3.1 Evolution of oxide particle sizes

Figure 1 shows the average particle size, minimum particle size and maximum particle size of spinel oxide for four alloy layers oxidized at 750°C in air for the different time. In the previous study[21, 22], Cu-Mn spinel size is larger than that of Mn-Co spinel, and Mn-Co spinel size is larger than that of Mn oxides and Co oxides after alloy layers oxidized at 750°C for 100h, which is also shown in Fig.1. Fig.1a discloses that the average particle size of Mn-35Cu oxides is the largest among the oxide layers, and average particle size increases firstly then turns to decrease with the extended oxidation time. Cu doped Mn-Co spinel is the second largest, and there is a slight increase in size after oxidation between 100h and 500h. The average particle size of Co-35Mn oxide layer is small and close to that of La doped Mn-Co spinel which is the smallest in size. The results indicate that the doping of element La reduces the particle size of Mn-Co-base spinel, while the doping of element Cu increases the size. Fig.1b shows that the minimum particle size of Cu doped Mn-Co spinel is the largest among the oxide layers and that of Mn-35Cu oxides is the smallest. Fig.1c discloses that the maximum grain sizes of Mn-Co-based oxides are slightly different, and that of Mn-35Cu oxides is much larger than the other three oxides when coatings oxidized for 100 h and 300 h, which is mainly due to the formation and growth of Cu-Mn spinel instead of Mn-Co spinel in Mn-Co-based oxides. There appears the significant fluctuation of particle size for Mn-35Cu oxides and the small fluctuation for Cu doped Mn-Co oxides during the oxidation period of 500 h.

### 3.2 Evolution of oxidation products for Cu-Mn layer and Cu doped Mn-Co layer

Figures 2 (a) and 2 (b) show the XRD spectra of Mn-35Cu alloy layer oxidized at 750°C for 20 h, 100 h, 300 h and 500 h. The surface oxides of Mn-35Cu layer are mainly  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  spinel and  $\text{Mn}_2\text{O}_3$  with a small amount of  $\text{Fe}_2\text{O}_3$ . The partial XRD analysis discloses that at the initial stage of oxidation (20 h) the characteristic diffraction peak intensity is weak for both  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  and  $\text{Mn}_2\text{O}_3$  and peak appears broad. When the oxidation time is extended to

100 h, the intensity of  $\text{Mn}_2\text{O}_3$  diffraction peak ( $32.9^\circ$ ,  $38.2^\circ$  and  $55.1^\circ$ ) increases substantially with a sharp shape, and the  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  peak intensity also enhanced. The discussion of oxide products for 20 h and 100 h were shown in details in reference 22. At the oxidation time of 300 h and 500 h, the intensity of the  $\text{Mn}_2\text{O}_3$  diffraction peak is weaker compared to 100 h, while the  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  peak intensity obviously increases such as the peaks of  $30.2^\circ$ ,  $35.7^\circ$ ,  $57.4^\circ$  and  $63.1^\circ$ . This indicates that a mass of stable  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  spinel phase is formed and  $\text{Mn}_2\text{O}_3$  oxides reduce. The surface oxide phases become more uniform with the oxidation time increasing to 500 h.

The XRD analysis of Co-33Mn-17Cu layer oxidized at different times is presented in Figs. 2 (c) and 2 (d). The oxide products oxidized for 20 h and 100 h are mainly the mixed oxides of  $\text{MnCo}_2\text{O}_4$  spinel and  $\text{Mn}_2\text{O}_3$ . The magnification of the diffraction peak at  $29^\circ$ - $38^\circ$  shows that the characteristic peak of  $\text{MnCo}_2\text{O}_4$  spinel is weak and relatively smooth (such as the peaks of  $30.2^\circ$  and  $35.9^\circ$ ) in the early stage of oxidation (before 100 h), indicating that spinel gradually begins to form. Meanwhile,  $\text{Mn}_2\text{O}_3$  diffraction peak is noticeable at the beginning (the peak of  $32.9^\circ$  for 20 h). The discussion of oxide products for 20 h and 100 h were shown in details in reference 21.

When the oxidation time is extended to 300 h, the surface oxides of Co-33Mn-17Cu layer tend to be a single-phase spinel structure. The peak intensity of  $\text{MnCo}_2\text{O}_4$  spinel with a small quantity of  $\text{CuMn}_2\text{O}_4$  is obviously enhanced in the range of  $29^\circ$ - $38^\circ$  in Fig.2(d). Meanwhile, the characteristic peak of  $\text{Mn}_2\text{O}_3$  is greatly weakened. When the oxidation time reaches 500 h, the characteristic peaks of non-spinel oxides disappear and there is only pure  $\text{MnCo}_2\text{O}_4(\text{CuMn}_2\text{O}_4)$  spinel phase, which suggests that the extended oxidation time promotes the spinel growth in Cu doped Mn-Co layer. In addition, the characteristic peak at 500h shifts slightly to the left, mainly because the atomic ratios of Mn/Co in spinel phases slightly change.

### **3.3 Oxidation products for four coatings and 430 SS**

The oxide XRD peaks of Mn-35Cu, Co-33Mn-17Cu, Co-38Mn-2La and Co-35Mn layers after oxidation at  $750^\circ\text{C}$  for 500 h are the significantly different, as shown in Fig. 3(a) and 3(b). The main products of La doped Mn-Co layer and Co-35Mn layer oxidized for 500 h are  $\text{Mn}_2\text{O}_3$  with some  $(\text{Mn},\text{Co})_3\text{O}_4$  spinel which is an intermediate tetragonal spinel structure between  $\text{MnCo}_2\text{O}_4$  (cubic) and  $\text{Mn}_3\text{O}_4$  (tetragonal) [21]. The spinel diffraction peaks are not sharp and mainly exhibit non-spinel phase. Cu doped Mn-Co layer only shows the sharp spinel oxide peaks. Meanwhile, Mn-35Cu layer shows the strong spinel peaks and strong  $\text{Mn}_2\text{O}_3$  peaks, indicating the mixed oxides at room temperature. Fig. 3(c) shows XRD patterns of 430 SS substrate oxidized at  $750^\circ\text{C}$  for 300 h and 500 h, respectively. It can be seen that the surface oxides of 430 SS are mainly Mn-Cr spinel and  $\text{Cr}_2\text{O}_3$ .

### 3.4 Oxidation kinetic and morphology characteristics

Oxidation kinetic curves of Mn-35Cu layer, Co-33Mn-17Cu layer and 430 SS oxidized at 750 °C for 500h are shown in Fig. 4. The previous published articles [21] propose that, after oxidation for 100 h, the mass gains of the three oxide layers (Mn-Co and La or Cu doped Mn-Co layers) change and follow the same tendency, so these data of Co-35Mn and Co-38Mn-2La layer is not shown in Fig. 4. The mass gain of 430 SS is the smallest during the oxidation process and that of Mn-35Cu layers is the largest in the initial stage of 100 h. The mass gains of Mn-35Cu and Co-33Mn-17Cu layers between 100 h and 500 h lightly change.

Surface morphology is presented for the coated 430 SS after oxidation at 750 °C for 500 h in Fig.5. According to the reference [22], after oxidation for 100 h,  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  spinel on the surface of Mn-35Cu oxide layer reveals large granules, while  $\text{Mn}_2\text{O}_3$  is much smaller than the spinel. This is in accordance with maximum particle sizes and minimum particle sizes for 100 h in Fig.1. With the increasing oxidation time to 500 h, the particle sizes gradually become uniform and large granules decrease. Fig.5a<sub>1</sub> shows the typical oxide morphology on the surface of Mn-35Cu layer and only the small amount of tiny particles are found (area 1). Element concentration analysis by EDS discloses that the different areas have approximately the similar composition for element Cu and Mn shown in Table 1. Combined with XRD in Fig.2, The oxides are mainly composed of  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  spinel and some Fe is also detected on the surface of Mn-35Cu oxide layer.

The typical surface morphology of Co-33Mn-17Cu layer oxidized for 500 h is shown in Fig. 5b<sub>1</sub>. The particle sizes relatively keep uniform during the oxidation process and  $\text{MnCo}_2\text{O}_4$  spinel (cubic-shaped) gradually is formed in the initial stage of 20 h [21]. Morphology characteristics of  $\text{MnCo}_2\text{O}_4$  spinel are similar to that of  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  on Cu-35Mn oxide layer, but  $\text{MnCo}_2\text{O}_4$  has the more uniform particle size. Element concentration in Table 1 discloses that Fe content on surface of Co-33Mn-17Cu oxide layer is a little lower than that on Cu-35Mn oxide layer.

Surface morphology of Co-38Mn-2La and Co-35Mn oxide layer in Fig.5c<sub>1</sub> and Fig.5d<sub>1</sub> shows their particle sizes are relatively small. The previous study [21] shows their spinel oxides are mainly an intermediate tetragonal spinel after oxidation for 100 h. With the increasing oxidation time to 500 h, the oxides keep the mixed phase structure and spinel diffraction peaks are not significantly enhanced (Fig. 3a and Table 1). In addition, though the small particles on the surface after 100 h are rich in element Mn, analysed by EDS, small particles as revealed in area 3 and area 4 after 500 h are nearly the same composition with large particles.

Cross section of Mn-35Cu oxide layer after oxidation for 500 h (Fig.5a<sub>2</sub>) shows some isolated pores distributing on

the outer part of oxide layer, and these pores are also detected in the external oxides of Co-33Mn-17Cu layer (Fig.5b<sub>2</sub>). The reason is speculated that the formation of vast coarse Cu-Mn grains leads to numerous pores formed at the grain boundaries, such as some micro-pores between grains on the surface in Fig.5a<sub>1</sub>. The doping of Cu in Mn-Co oxides makes the spinel particles enlarge, so that the number of micro-pores in Co-33Mn-17Cu oxide layer is much more than that in Co-38Mn-2La and Co-35Mn oxide layer (Fig.5c<sub>2</sub> and Fig.5d<sub>2</sub>). Both Cu-Mn and Mn-Co spinel favor to form in areas of high oxygen partial pressure, which explains some micro-pores mainly distribute on the outer oxide layer. In addition, the rapid diffusion of element Cu might also produce porous oxides[23].

The average thickness of four oxide layers is slightly different in Figs.5a<sub>2</sub>-d<sub>2</sub>. We should note the thickness can be adjusted by the deposition parameters of HEMAA process [20]. Line scanning of EDS shows that the distribution of element Co, Mn and Cu throughout the oxide layers is approximately uniform after 500 h. Cr content is relatively low in the whole oxide layers and the Cr<sub>2</sub>O<sub>3</sub> interface layers between the oxides and substrate are thin after oxidation for 500 h. Some Fe from 430 SS substrate diffuses into the oxide layer, and the line scanning in Fig.5a<sub>3</sub>-d<sub>3</sub> shows that Fe content gradually decreases from oxide/substrate interface to the top surface, except for La doped Mn-Co layer. The single CuMn<sub>2</sub>O<sub>4</sub>/MnCo<sub>2</sub>O<sub>4</sub> spinel phase in Co-33Mn-17Cu oxide layer is more effective to blocks the outward diffusion of Fe than the mixed oxides of Co-38Mn-2La and Co-35Mn oxide layers, such as Fe content in Fig.5b<sub>3</sub>.

### 3.5 Evolution of ASR for Cu-Mn based and Mn-Co based oxide layers

Figure 6(a) is the curves of ASR versus temperature in the range of 500 °C to 800 °C for the Mn-35Cu layer after oxidation at 750°C for the different time. It can be seen that all the ASR values at the four oxidation periods decrease with the increasing temperature in the range of 500 °C to 800 °C. After the oxidation for 20 h, ASR is remarkably higher than that of the other three oxidation periods, especially at 500 °C and 600 °C. It might be because a large amount of mixed oxides which has the low electrical conductivity is formed at the early oxidation stage, such as Mn<sub>2</sub>O<sub>3</sub>, Mn<sub>3</sub>O<sub>4</sub> and CuO, resulting in a high ASR of the oxide film. With the prolongation of oxidation time, Cu ions have enough time to diffuse and react with Mn oxides to form Cu-Mn spinel. In the meantime, the content of Mn<sub>2</sub>O<sub>3</sub> oxides reduces, which improves the electrical conductivity of the whole oxide layer and leads to an obvious decline of ASR. After oxidation for 500h, ASR values of Mn-35Cu oxide layer is 33.8 mΩ·cm<sup>2</sup> for 500 °C, 18.8 mΩ·cm<sup>2</sup> for 600 °C, 8.1 mΩ·cm<sup>2</sup> for 700 °C, and 74.1 mΩ·cm<sup>2</sup> for 800 °C, respectively. Fig. 6(b) shows the Arrhenius plots of ASR/T versus 10<sup>3</sup>/T for Mn-33Cu layer after oxidation. It is an accurate linear relationship between Log(ASR/T) and 10<sup>3</sup>/T, indicating the semiconductor characteristic of oxides formed on the substrate and the slopes of the lines decrease after oxidation for 100 h. The ASR value is directly related to the high temperature behavior of thermally

grown oxide layer, thus the oxides of Mn-35Cu coating after 500 h exhibits superior electrical conductivity between 500°C and 800°C.

Figure 6(c) shows ASR values vs. temperature for Cu doped Mn-Co layer oxidized at 750°C with the extended oxidation time. The relationship between ASR and oxidation time for Cu doped Mn-Co layer shows the different evolution rules from that of Mn-35Cu layer. The highest resistance in the range of 500 °C to 800 °C is the value after oxidation for 100h, and the resistance rapidly decreases after 100 h. The ASR values oxidized for 300 h and 500 h are almost the same, indicating that the characteristics of oxide layers in the two oxidation periods, such as the average thickness, oxide composition and the thickness of interface Cr<sub>2</sub>O<sub>3</sub> layer, are almost the similar. The results of ASR are consistent with XRD and EDS analysis. According to cross-section analysis in Fig.5, Mn-35Cu layer oxidized for 500 h are porous and Fe content is relatively high in it, but the ASR values in Fig. 6(a) are still lower than that of Cu doped Mn-Co layer in Fig. 6(c), especially at 500 °C and 600 °C.

ASR values at 800 °C of four oxide layers and bared 430SS are shown in Fig. 7. The resistance of bared 430 SS in 500 h of oxidation time is high and more than 100 mΩ·cm<sup>2</sup> in Fig. 7(a), except for 100 h. The ASR values of four oxide layers shown in Fig. 7(b) all have a rapid increase in the initial stage of oxidation. The ASR at 800 °C of Co-35Mn layer and La doped Mn-Co layer continues to increase after 100 h shown in Fig. 7b and the dopant of La obviously decreases the electrical resistance in the beginning. With the oxidation time increasing, the effect of La gradually reduces and the electrical resistance of the two oxide layers is close. The ASR at 800 °C of Cu doped Mn-Co layer and Cu-35Mn layer increases first, and then decreases. The peak value of Cu-35Mn oxides is about 18 mΩ·cm<sup>2</sup> at 20h, after which the values decrease slowly with the oxidation time. The peak value of Co-33Mn-17Cu oxides is about 41 mΩ·cm<sup>2</sup> at 100 h, which is a bit higher than that of Cu-35Mn oxides. The electrical resistance sharply decreases after 100h, and then gently slows between 300h and 500h. It is worth mentioning that Cu doped Mn-Co oxide layer exhibits the better electrical conductivity than Co-35Mn and Co-38Mn-2La oxide layers, and its value is close to that of Cu-Mn spinel (electrical conductivity at 800 °C [24], MnCo<sub>2</sub>O<sub>4</sub> ~60 S·cm<sup>-1</sup> and Cu<sub>1.2</sub>Mn<sub>1.8</sub>O<sub>4</sub> ~225 S·cm<sup>-1</sup>). The ASR values at 800 °C are 4.2 mΩ·cm<sup>2</sup> for Mn-35Cu oxides and 7.7 mΩ·cm<sup>2</sup> for Co-33Mn-17Cu oxides after the oxidation for 500 h.

#### 4. Discussions

Schematic diagrams of formation process for the homogeneous oxides prepared by HEMAA are shown in Fig. 8. There are four important steps described in the process of formation, and mass transport and microstructural



evolution of alloy layers after oxidation are also discussed.

(1) Step 1, melting: The selected high purity metal pieces are melted and uniformly mixed to form an alloy of a given composition, which may be a solid solution (MnCo) or a two-phase or multi-phase structure[21,22].

(2) Step 2, HEMAA process: The alloys with some certain composition are deposited on the 430 SS substrate by HEMAA, which is a pulsed micro-welding technique with the instantaneous release of high current, resulting in a high cooling rate ( $\sim 10^6$  Ks<sup>-1</sup>). The microcrystalline or even nanocrystalline alloy layers are obtained and metallurgically bonded to the 430 SS substrate [6,12,14,17,21,22].

(3) Step 3 oxidation (0-100 h): The uniform microcrystalline coatings are oxidized at the SOFC operating temperature. The oxide products in the initial stage exhibit some multi-layer structures, and the element concentrations are uneven in each oxide layer [21,22].

(4) Step 4, oxidation (more than 300 h): After the sufficient reaction time, oxide products are converted into the homogeneous oxide layers. The element concentrations in the oxide layer are gradually uniform, and the oxide products may be homogeneous, accompanied by the formation of the pure single-phase spinel (MnCo<sub>2</sub>O<sub>4</sub>/CuMn<sub>2</sub>O<sub>4</sub>).

#### 4.1 Concentration control and composition uniformity

The given concentrations and uniform composition of Mn-Co and Cu-Mn alloy layers are obtained by step 1 and step 2 in Fig.8. The sintered bodies consisting of the single-phase spinel structure are usually synthesized by solid-state reaction method after the oxide powders were ball milled which is to achieve uniform crystallite size and better chemical homogeneity [25,26]. The temperature of solid-state reaction is generally above 1000 °C. The temperature higher for the formation of pure spinel-type oxides [27,19]. Furthermore, multiple oxides may be generated after calcination instead of the single-phase spinel, if the powder concentration is not precisely controlled. Mn-Co-O phase diagram in air [28] shows a single-phase MnCo<sub>2</sub>O<sub>4</sub> spinel would be formed between 600 °C and 900 °C (the operating temperatures of SOFC). When Mn concentration is more than 40%, lots of Mn-rich oxides are formed, and when Mn concentration is less than 20%, oxides are mainly Co<sub>3</sub>O<sub>4</sub>, which has been found in previous published articles [16,20]. Cu-Mn-O phase diagram[28] shows that Cu<sub>x</sub>Mn<sub>3-x</sub>O<sub>4</sub> spinel may not be the pure phase at the operating temperatures of SOFC, because the atomic ratios of Mn/Co need be precisely controlled with the temperature. According to Reference 31, pure Cu-Mn spinel phase is formed at 850°C, but Mn<sub>3</sub>O<sub>4</sub> peaks appears when samples cooled down to room temperature. XRD in Fig.2 shows that the Mn-35Cu coating oxidized for 300 h and 500 h is mainly Cu<sub>1.2</sub>Mn<sub>1.8</sub>O<sub>4</sub> spinel with some Mn<sub>2</sub>O<sub>3</sub>, so it may be pure Cu<sub>1.2</sub>Mn<sub>1.8</sub>O<sub>4</sub> spinel at high

temperature, which will be discussed in the future. The concentration control and composition uniformity of Mn-Co and Cu-Mn alloy coatings are critical to the subsequent formation of single-phase spinel. Some other methods of coating preparation, such as electrochemical deposition, plasma spraying and physical vapor deposition, are normally difficult to ensure both concentration accuracy and uniformity of element distribution in the coating, especially when the coatings contain high Mn content[29,30] and multiple elements [31-34].

#### **4.2 Grain refinement and metallurgical bonding**

The grain sizes of Mn-Co and Cu-Mn alloy layers are much smaller than that of the corresponding cast alloys, which is owed to the rapid solidification of primary deposited particles during high energy micro-arc alloy process [20,35,36]. The effects of grain sizes on the high-temperature oxidation behavior have been extensively investigated, and it is generally believed that fine-grained alloys had much better high temperature performance than the coarse-grained alloys [37-39], such as oxide spallation reduced and thinner oxide layer formed on the fine-grained alloy. The common role of grain refinement in the oxidation of alloys is to enhance the diffusion of elements and accelerate phase transformation (the rapid formation of some oxides), because that the fine-grained structure may provide abundant grain boundaries, which has been found during the oxidation process of Co-33Mn-17Cu and Mn-35Cu alloy layers. The inward diffusion of oxygen in air is mainly along the grain boundary, and the microcrystalline structure of coatings promotes oxygen diffusion and increases the partial pressure of oxygen inside the coating. Metallurgical bonding between the alloy layer and 430SS substrate enhances interfacial bonding and restrains the growth of interfacial transition layer ( $\text{Cr}_2\text{O}_3$ ). Some other methods of coating preparation are normally difficult to make the coatings compact and metallurgical [2,40-42].

#### **4.3 Element doping and spinel types**

Some doped or substituted elements may suppress the decomposition of oxides and result in a more stable spinel structure for the oxides [26,43,44]. The crystal structure of the as-sintered Mn-Ni-Co oxides is a cubic spinel with a small amount of Ni-rich oxide phase, but no Ni-rich phase is detected in the Cr-substituted samples which is a single-phase of cubic spinel structure. The oxidation products of Cu doped Mn-Co layer after 300h is the pure single-phase spinel but not for the other Mn-Co based layers. Structure and electrical properties of oxidation products are also greatly affected by spinel types. The grain size of Cu-Mn spinel is generally large and some micro-pores is formed between the grain boundaries which is shown on the surface morphology and cross section (Fig.5 and Fig.8), especially for the initial oxidation stage [21,22]. The grain size of Mn-Co spinel is relatively small and uniform, and so there are few micro-pores in the oxides. The grain size of Cu doped Mn-Co spinel is between the two kinds of

oxides mentioned above and the micro-pores are a little smaller than Cu-Mn spinel. Cu-Mn spinel has better conductivity than Mn-Co spinel and the high Mn content will decrease the electrical conductivity Mn-Co spinel, such as  $\text{MnCo}_2\text{O}_4$   $60 \text{ S}\cdot\text{cm}^{-1}$ ,  $\text{CoMn}_2\text{O}_4$   $6.4 \text{ S}\cdot\text{cm}^{-1}$  and  $\text{Mn}_3\text{O}_4$   $0.1 \text{ S}\cdot\text{cm}^{-1}$ . The doping of Cu in Mn-Co spinel accelerates the formation of Mn-Co spinel and promotes electrical conductivity. Additionally, when a small amount of Fe is doped in Cu-Mn oxides, the porosity of oxides may reduce. Such as the micro-pores are mostly present in the outer part of oxides in Fig.5(a<sub>2</sub>,b<sub>2</sub>) and Fig.8 where Fe content is lower than in the inner part of oxides.

#### 4.4 Control of the factors affecting thermal growth

Besides the phase diagram, the oxygen activity, temperature, oxidation time and element concentrations all affect the thermal growth of spinel. According to previous research [6,16,45], the ambient oxygen partial pressure at SOFC operating temperature  $600^\circ\text{C}$ - $900^\circ\text{C}$  will favor the formation of  $\text{Co}_3\text{O}_4$ ,  $\text{CuO}$ ,  $\text{Mn}_3\text{O}_4$  and  $\text{Fe}_3\text{O}_4$ , but the partial pressure of oxygen gradually decreases from air/oxide interface to oxide/substrate interface. The calculated values of oxygen partial pressure at equilibrium are  $4.26\times 10^{-3}$  atm for  $\text{Co}_3\text{O}_4$ ,  $2.70\times 10^{-6}$  atm for  $\text{CuO}$ ,  $4.69\times 10^{-18}$  atm for  $\text{Fe}_3\text{O}_4$  and  $1.28\times 10^{-25}$  atm for  $\text{Mn}_3\text{O}_4$ , and a higher value for the formation of Cu-Mn and Mn-Co spinels. In the beginning of oxidation, Mn and Cu in the coating rapidly diffuse outward to the surface, and Co diffuses outward and also inward into the substrate [45, 33].  $\text{Cr}_2\text{O}_3$  is formed at oxide/substrate interface, some mixed oxides, such as  $\text{MnO}$ ,  $\text{Mn}_3\text{O}_4$ ,  $\text{Fe}_3\text{O}_4$  and  $\text{CoO}$ , are also formed at the initial stage of oxidation. Mn-Co spinel oxides first dispersedly precipitate along grain boundaries of mixed oxides and then evolve into a continuous spinel oxide layer. Therefore, a continuous Mn-Co or Cu-Mn spinel oxide layer may be formed in the outer part of oxide layer because of the relatively high oxygen activity and the extended oxidation time. In step 3, when the four alloy layers are oxidized for 100h,  $(\text{Co,Mn})_3\text{O}_4$  spinel, Co-rich oxides and Mn-rich oxides are found in the oxide layer, respectively. These data is discussed in detail in previous studies (reference 21 and 22). In step 4, a homogeneous oxide layer is found after 500 h. There is no element aggregation in the whole oxide layers, and Co-rich oxides and Mn-rich oxides are not found, yet. The single-phase  $\text{MnCo}_2\text{O}_4$  is formed on the surface of Co-33Mn-17Cu coating and  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  is the main oxide products on the surface of Cu-35Mn coating.

#### 5. Conclusions

Co-33Mn-17Cu, Mn-35Cu, Co-38Mn-2La and Co-35Mn alloy layers have been prepared by HEMAA process. The evolution of oxide particle sizes on the surface shows that Mn-35Cu oxides have both the largest and smallest particles among the four oxide layers and particles tend to be uniform in size after 500h. Particle sizes of

Co-33Mn-17Cu oxide layer slightly increase during the oxidation period of 500 h. The evolution of oxidation products after 500 h shows that Mn-35Cu oxides correlate to  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  spinel with  $\text{Mn}_2\text{O}_3$  and Co-33Mn-17Cu oxides are only  $\text{MnCo}_2\text{O}_4$  spinel, while Co-38Mn-2La and Co-35Mn oxides correlate to  $\text{Mn}_2\text{O}_3$  and  $(\text{Mn},\text{Co})_3\text{O}_4$  spinel. The evolution of ASR values shows that the resistance of Co-33Mn-17Cu and Mn-35Cu oxides increases first and then decreases, but the resistance of Co-38Mn-2La and Co-35Mn oxides continues to increase after 100 h. The ASR values at 800°C are  $4.2 \text{ m}\Omega\cdot\text{cm}^2$  for Mn-35Cu oxides and  $7.7 \text{ m}\Omega\cdot\text{cm}^2$  for Co-33Mn-17Cu oxides after oxidation for 500 h. The formation process of the homogeneous oxide layers (pure single-phase  $\text{MnCo}_2\text{O}_4$  spinel) is affected by many factors, such as the given concentrations and uniform composition of alloy layers, grain refinement and metallurgical bonding to the substrate, element doping and the types of spinel oxidized, the oxidation temperature and time, *etc.*. The pure single-phase spinel without impurity phases is only found on Co-33Mn-17Cu oxide layer after oxidation at 750 °C for 500 h.

#### **Acknowledgments:**

This work was financially supported by China Scholarship Fund (2017), National Natural Science Foundation of China (51801077, 51201073), Research Fund of Jiangsu University of Science and Technology (1624821607-5)

#### **Reference**

- [1] M. Bednarz, S. Molin, M. Bobruk, M. Stygar, E. Długoń, M. Sitarz, T. Brylewski. High-temperature oxidation of the Crofer 22H ferritic steel with  $\text{Mn}_{1.45}\text{Co}_{1.45}\text{Fe}_{0.1}\text{O}_4$  and  $\text{Mn}_{1.5}\text{Co}_{1.5}\text{O}_4$  spinel coatings under thermal cycling conditions and its properties. *Mater. Chem. Phys.* 225 (2019) 227–238
- [2] B. Talic, S.Molin, K. Wiik, P.V. Hendriksen, H.L. Lein. Comparison of iron and copper doped manganese cobalt spinel oxides as protective coatings for solid oxide fuel cell interconnects. *J. Power Sources* 372 (2017) 145–156
- [3] S. Molin, P. Jasinski, L. Mikkelsen, W. Zhang, M. Chen, P.V. Hendriksen. Low temperature processed  $\text{MnCo}_2\text{O}_4$  and  $\text{MnCo}_{1.8}\text{Fe}_{0.2}\text{O}_4$  as effective protective coatings for solid oxide fuel cell interconnects at 750°C. *J. Power Sources* 336 (2016) 408-418
- [4] Y.M. Liao, B. Zhang, M.H. Chen, M. Feng, J.I. Wang, S.L. Zhu, F.H. Wang, Self-healing metal-enamel composite coating and its protection for TiAl alloy against oxidation under thermal shock in NaCl solution. *Corros. Sci.* 167 (2020) 10852
- [5] P.F. You, X. Zhang, H.L. Zhan, H.J. Liu, C.L. Zeng. Effect of  $\text{CeO}_2$  on oxidation and electrical behaviors of

- ferritic stainless steel interconnects with Ni-Fe coatings. *Int. J. Hydrogen Energ.* 43(2018)7492-7500
- [6] Y.B. Lai, P.Y. Guo, Y. Shao, Y. Zhang, N. Liu. The role of Dy doping on oxidation behavior of Co-40Mn/Co coating for solid oxide fuel cell metal interconnects. *J. Alloy. Compd.* 694 (2017) 383-393
- [7] S.J. Geng, Q.Q. Zhao, Y.H. Li, J.J. Mu, G. Chen, F.H. Wang, S.L. Zhu. Sputtered MnCu metallic coating on ferritic stainless steel for solid oxide fuel cell interconnects application. *Int. J. Hydrogen Energ.* 42(2017)10298-10307.
- [8] Z.H. Sun, S. Gopalan, U.B. Pal, S.N. Basu.  $\text{Cu}_{1.3}\text{Mn}_{1.7}\text{O}_4$  spinel coatings deposited by electrophoretic deposition on Crofer 22 APU substrates for solid oxide fuel cell applications. *Surf. Coat. Tech.* 323 (2017) 49-57
- [9] S.Y. Zhen, W. Sun, P.Q. Li, G.Z. Tang, D. Rooney, K.N. Sun, X.X. Ma, High performance cobalt-free  $\text{Cu}_{1.4}\text{Mn}_{1.6}\text{O}_4$  spinel oxide as an intermediate temperature solid oxide fuel cell cathode. *J. of Power Sources* 315 (2016) 140-144
- [10] S. Joshi, A. Petric. Nickel substituted  $\text{CuMn}_2\text{O}_4$  spinel coatings for solid oxide fuel cell interconnects. *Int. J. Hydrogen Energ.* 42 (2017) 5584-5589
- [11] Ph.V. K. Korneev, A.N. Sheveyko, N.V. Shvindina, E.A. Levashov, D.V. Shtansky. Comparative study of Ti-C-Ni-Al, Ti-C-Ni-Fe, and Ti-C-Ni-Al/Ti-C-Ni-Fe coatings produced by magnetron sputtering, electro-spark deposition, and a combined two-step process. *Ceram. Int.* 44 (2018) 7637–7646
- [12] P.Y. Guo, C.L. Zeng, N. Wang, Y. Shao. FeAl-based coatings deposited by high-energy micro-arc alloying process for wet-seal areas of molten carbonate fuel cell. *J. Power Sources*, 217 (2012) 485-490
- [13] X. Wei, Z.G. Chen, J. Zhong, L. Wang, Z.W. Hou, Y. Zhang, F.L. Tan. Facile preparation of nanocrystalline Fe<sub>2</sub>B coating by direct electrospark deposition of coarse-grained Fe<sub>2</sub>B electrode material. *J. Alloy. Compd.* 717 (2017) 31-40
- [14] P.Y. Guo, Y. Shao, C.L. Zeng, M.F. Wu, W.L. Li. Oxidation characterization of FeAl coated 316 stainless steel interconnects by high-energy micro-arc alloying technique for SOFC. *Mater Lett.* 65 (2011) 3180–3183
- [15] L.L. Yang, M.H. Chen, J.L. Wang, Y.X. Qiao, P.Y. Guo, S.L. Zhu, F.H. Wang, Microstructure and composition evolution of a single-crystal superalloy caused by elements interdiffusion with an overlay NiCrAlY coating on oxidation, *J. Mater. Sci. Technol.* 45(2020) 49-58,

- [16] Y.B. Lai, P.Y. Guo, Y. Shao, P.J. Tang, Y. Zhang, J.F. Zhang. Formation and performances of spinel reaction layers on Co-40Mn coatings under an oxygen pressure of  $10^5$  Pa for solid oxide fuel cell interconnect application. *Vacuum*.130 (2016) 14-24
- [17] Z.J. Feng, C.L. Zeng. Oxidation behavior and electrical property of ferritic stainless steel interconnects with a Cr-La alloying layer by high-energy micro-arc alloying process. *J. Power Sources*, 195(2010) 7370-7374
- [18] K. Park, I.H. Han. Effect of  $\text{Cr}_2\text{O}_3$  addition on the microstructure and electrical properties of Mn-Ni-Co oxides NTC thermistors. *J. Electroceram.* (2006) 17:1069–1073
- [19] T. Yokoyama, A. Yamazaki, T. Meguro, D. Ito, Y. Koshiba, S. Okazaki. Preparation and electrical properties of sintered bodies composed of  $\text{Mn}_{(2.25-X)}\text{Fe}_X\text{Ni}_{0.75}\text{O}_4$  ( $0 \leq X \leq 2.25$ ) with cubic spinel structure. *J. Electroceram.* (2016) 37:151-157
- [20] Y. Zhang, P.Y. Guo, Y. Shao, Y.B. Lai, J.Q. Zhang. Preparation and high-temperature performance of Co-10Mn and Co-40Mn alloy coatings for solid oxide fuel cell metal interconnects. *J. Alloy. Compd.* 680 (2016) 685-693
- [21] P.Y. Guo, Y.B. Lai, Y. Shao, Y. Zhang, H.Sun, Y.X. Wang. Oxidation characteristics and electrical properties of doped Mn-Co spinel reaction layer for solid oxide fuel cell metal interconnects. *Coatings*, 8(2018) 42-53
- [22] P.Y. Guo, Y.B. Lai, Y. Shao, Y. Zhang, Y.X. Wang. Thermal growth of  $\text{Cu}_{1.2}\text{Mn}_{1.8}\text{O}_4$  spinel coatings on metal interconnects for solid oxide fuel cell applications. *Metals*, 7(2017)522-532
- [23] Q.X. Fu, F. Tietz, D. Sebold, E. Wessel, H.P. Buchkremer, Magnetron-sputtered cobalt-based protective coatings on ferritic steels for solid oxide fuel cell interconnect applications. *Corros. Sci.* 2012, 54, 68–76.
- [24] N. Shaigan, W. Qu, D.G. Ivey, W.X. Chen. A review of recent progress in coatings, surface modifications and alloy developments for solid oxide fuel cell ferritic stainless steel interconnects. *J. Power Sources*, 195(2010)1529-1542
- [25] J.M. Varghese, A. Seema, K.R. Dayas. Ni–Mn–Fe–Cr–O negative temperature coefficient thermistor compositions: Correlation between processing conditions and electrical characteristics. *J. Electroceram.* (2009) 22:436–441
- [26] Q. Wang, W. Kong, J.C. Yao, A.M. Chang. Fabrication and electrical properties of the fast response  $\text{Mn}_{1.2}\text{Co}_{1.5}\text{Ni}_{0.3}\text{O}_4$  miniature NTC chip thermistors. *Ceram. Int.* 45 (2019) 378–383

- [27] P.P. Deepak, M.Parokkaran, K.R. Ranjith, M.N. Muralidharan, S. Ansari. Optimization studies on nanocrystalline NTC thermistor compositions by a self-propagated high temperature synthesis route. *Ceram. Int.* 44 (2018) 4360-4366
- [28] M.R. Bateni, P. Wei, X.H. Deng, A. Petric. Spinel coatings for UNS 430 stainless steel interconnects. *Surface & Coatings Technology* 201 (2007) 4677–4684
- [29] S. Apelt, Y. Zhang, J.H. Zhu, C. Leyens. Electrodeposition of Co-Mn<sub>3</sub>O<sub>4</sub> composite coatings. *Surf. Coat. Tech.* 280 (2015) 208-215
- [30] J. Puranen a, M. Pihlatie, J. Lagerbom, G. Bolelli, J. Laakso, L. Hyvarinen, M. Kylmalahti, O. Himanen, J. Kiviahho, L.Lusvarghi, P. Vuoristo. Post-mortem evaluation of oxidized atmospheric plasma sprayed Mn-Co-Fe oxide spinel coatings on SOFC interconnectors. *Int. J. Hydrogen Energ.* 39(2014)17284-17294
- [31] Z.H. Sun, R.F. Wang, A.Y. Nikiforov, S. Gopalana, U.B. Pala. Soumendra N. Basua CuMn<sub>1.8</sub>O<sub>4</sub> protective coatings on metallic interconnects for prevention of Cr-poisoning in solid oxide fuel cells. *J. Power Sources* 378 (2018) 125-133
- [32] S.I. Castañeda, F.J. Pérez. Al-Mn CVD-FBR coating on P92 steel as protection against steam oxidation at 650°C: TGA-MS study. *J. Nucl. Mater.* 499 (2018) 419-430
- [33] Y. Shao, P.Y. Guo, H.Sun, T.C. Zhou, J.T. Ding, K.X. Xu, Y.X. Wang, Y.X. Guo, D.P. Wang, X.H. Hou. Structure and properties of composite Ni–Co–Mn coatings on metal interconnects by electrodeposition. *J. Alloy. Compd.* 811 (2019) 152006
- [34] Y.Z. Hu, S.W. Yao, C.X. Li, C.J. Li, S.L. Zhang. Influence of pre-reduction on microstructure homogeneity and electrical properties of APS Mn<sub>1.5</sub>Co<sub>1.5</sub>O<sub>4</sub> coatings for SOFC interconnects. *Int. J. Hydrogen Energ.* 42(2017)27241-27253
- [35] D.W. Heard, M. Brochu. Development of a nanostructure microstructure in the Al-Ni system using the electrospark deposition process. *Journal of Materials Processing Technology*, 210(2010)892–898
- [36] W.F. Wang, M.C.Wang, F.J. Sun, Y.G. Zheng, J.M. Jiao. Microstructure and cavitation erosion characteristics of Al–Si alloy coating prepared by electrospark deposition. *Surf. Coat. Tech.* 2008, 202:5116 -5121
- [37] X. Wang, J.A. Szpunar. Effects of grain sizes on the oxidation behavior of Ni-based alloy 230 and N. *J. Alloy.*

Compd. 752 (2018) 40-52

- [38] W. Peng, J Wang, H.W. Zhang, X.Y. Hong, Z.Y. Wu, Y.L. Xu, J. Lia, X.S. Xiao. Insights into the role of grain refinement on high-temperature initial oxidation phase transformation and oxides evolution in high aluminium Fe-Mn-Al-C duplex lightweight steel. *Corros. Sci.* 126 (2017) 197–207
- [39] X. Peng, J. Yan, Y. Zhou, F. Wang. Effect of grain refinement on the resistance of 304 stainless steel to breakaway oxidation in wet air. *Acta. Mater.* 53(2005) 5079-5088
- [40] J. Li, C.Y. Xiong, J. Li, D. Yan, J. Pu, B. Chi, L. Jian. Investigation of  $\text{MnCu}_{0.5}\text{Co}_{1.5}\text{O}_4$  spinel coated SUS430 interconnect alloy for preventing chromium vaporization in intermediate temperature solid oxide fuel cell. *Int. J. Hydrogen Energ.* 42(2017) 16752-16759
- [41] Y.X. Wang, D. Cao, W.D. Gao, Y.X. Qiao, Y.X. Jin, G. Cheng, W. Gao, Microstructure and properties of sol-enhanced Co-P-TiO<sub>2</sub> nano-composite coatings, *J. Alloy. Compd.*, 792(2019)617-625.
- [42] Q.Q. Zhao, S.J. Geng, G. Chen, F.H. Wang. Application of sputtered NiFe<sub>2</sub> alloy coating for SOFC interconnect steel. *J. Alloy. Compd.* 769 (2018) 120-129
- [43] K. Park, I.H. Han. Effect of Cr<sub>2</sub>O<sub>3</sub> addition on the microstructure and electrical properties of Mn-Ni-Co oxides NTC thermistors. *J. Electroceram.* 17 (2006) 1069–1073
- [44] H.M.T. Farid, I. Ahmad, I.Ali, S.M. Ramay, A. Mahmood. Study of spinel ferrites with addition of small amount of metallic elements. *J. Electroceram.* 42 (2019) 57–66
- [45] F. Gesmundo, P. Nanni, D.P. Whittle. High temperature oxidation of Mn-Co alloys, *Corros. Sci.* 19(1979)675-691
- [46] H. Zhang, J.W. Wu, X.B. Liu, A. Baker. Studies on elements diffusion of Mn/Co coated ferritic stainless steel for solid oxide fuel cell interconnects application. *Int. J. Hydrogen Energ.* 38(2013)5075-5083



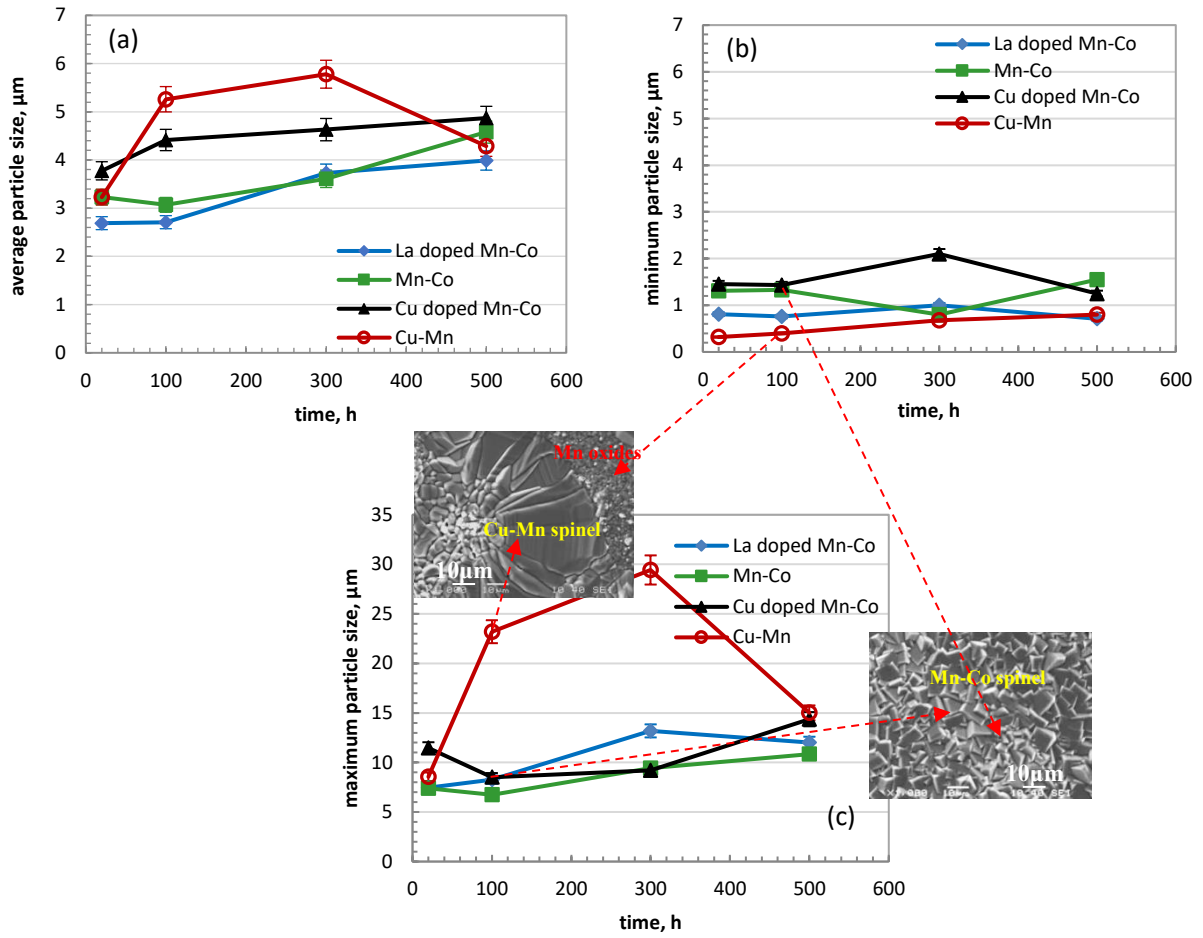


Fig.1 Particle sizes of spinel oxides on the surface for four alloy layers oxidized at 750°C in air.  
 (a) average particle size (b) minimum particle size (c) maximum particle size

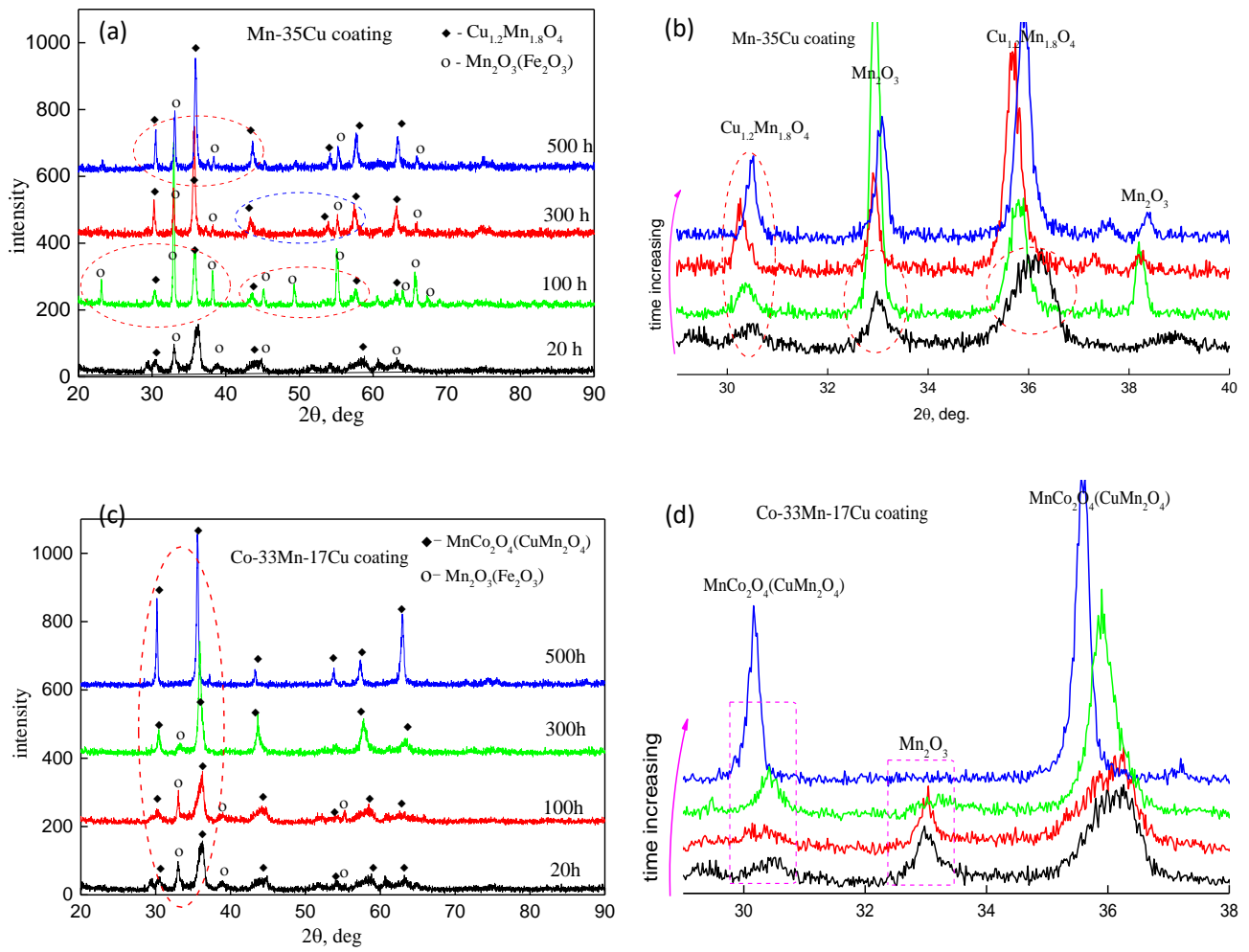


Fig.2 XRD patterns and partial XRD of (a) (b) Mn-35Cu and (c) (d) Cu doped Mn-Co alloy layers oxidized in air at 750 °C with the extended oxidation time

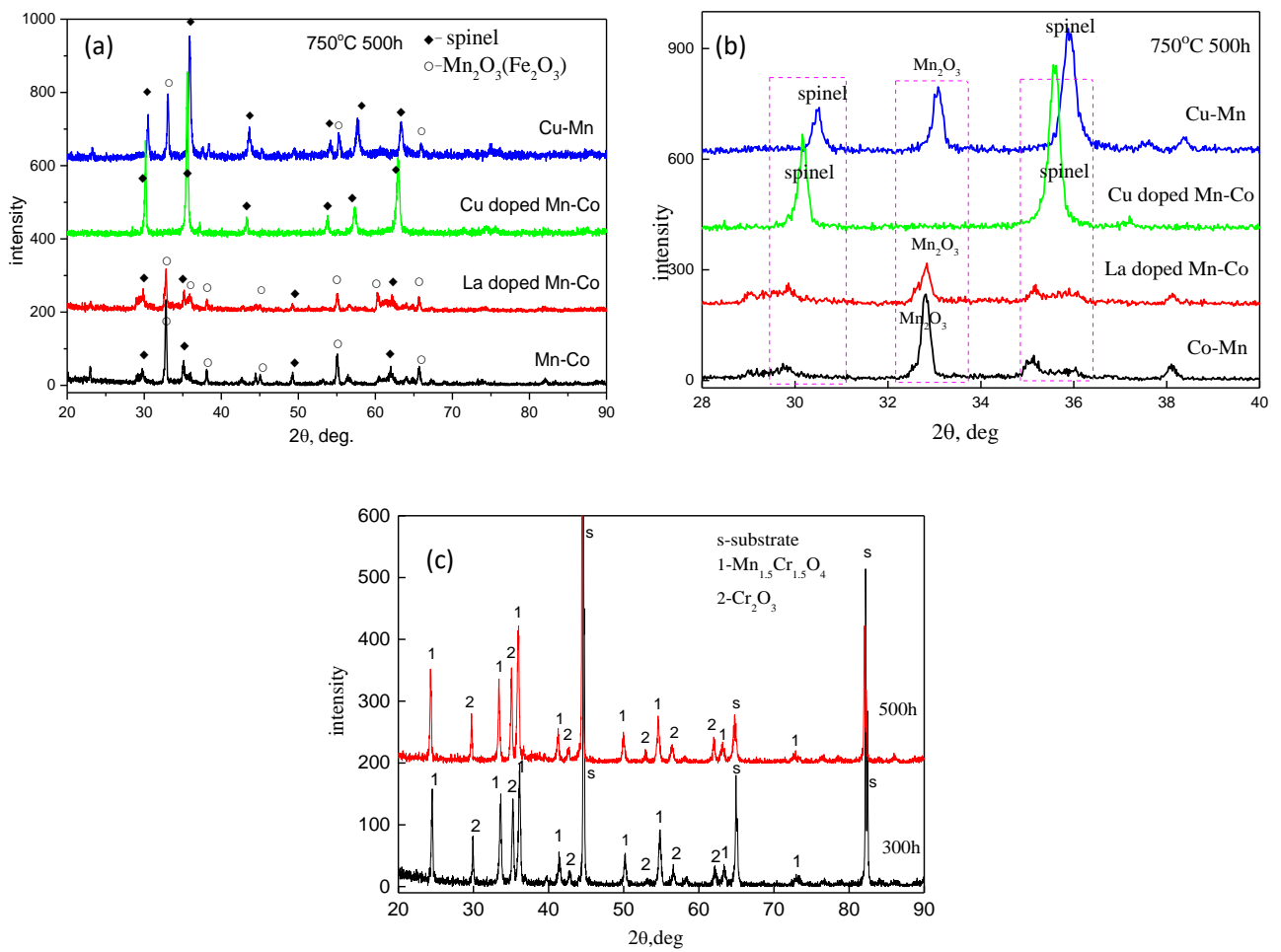


Fig.3 (a) (b) XRD patterns and partial XRD ( $28^\circ$ – $40^\circ$ ) of four alloy layers after oxidation in air at 750°C for 500 h  
(c) XRD patterns of 430SS oxidized in air at 750 °C for 300h and 500h

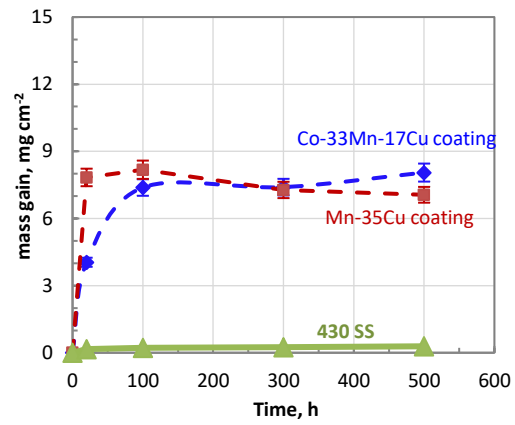


Fig.4 Oxidation kinetic curves of Mn-35Cu layer, Co-33Mn-17Cu layer and 430SS oxidized at 750 °C for 500h in air

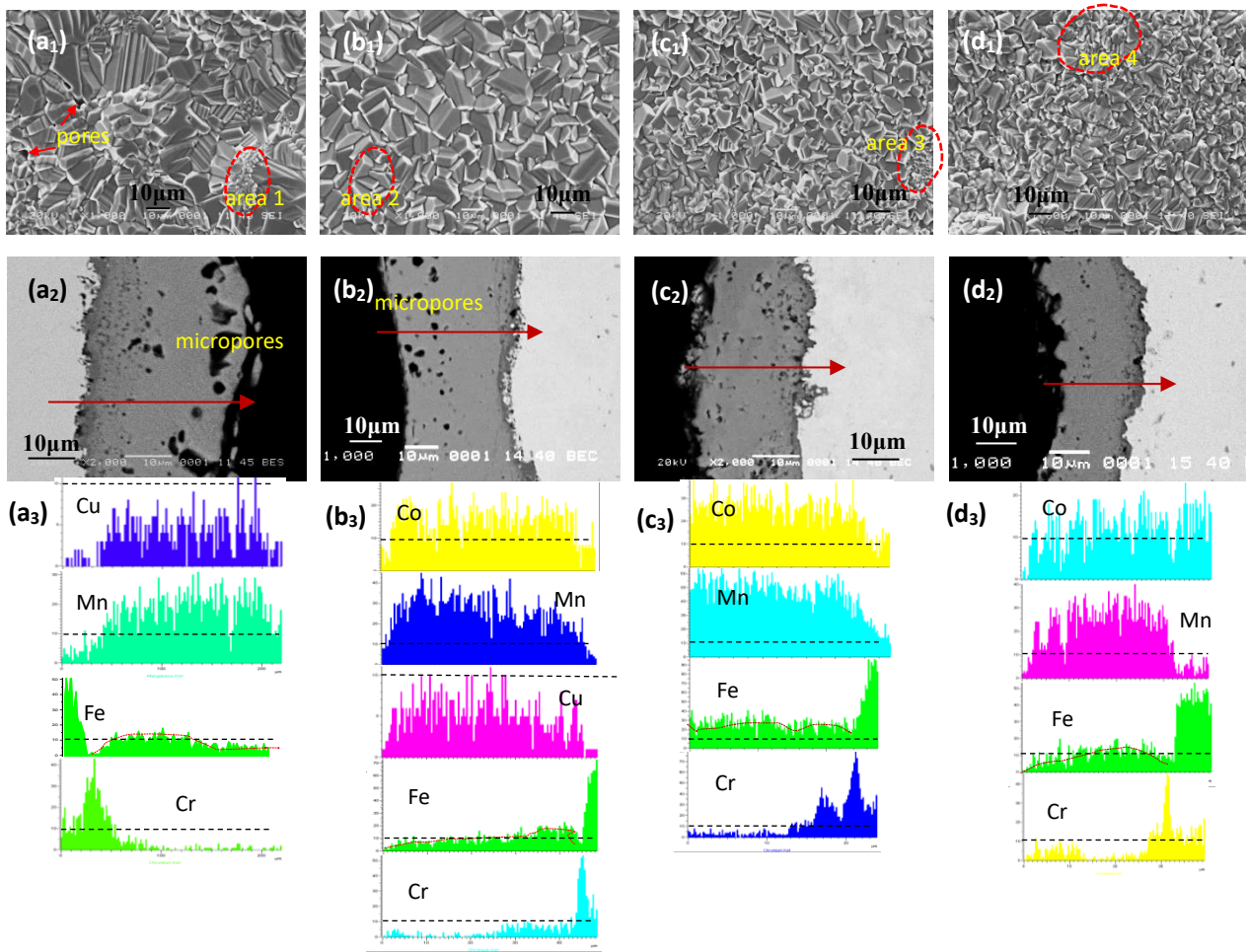


Fig.5 Surface and cross-sectional morphology of oxide layers on 430 SS after oxidation at 750°C for 500 h  
 (a<sub>1</sub>) (a<sub>2</sub>) (a<sub>3</sub>) Mn-35Cu layer, (b<sub>1</sub>) (b<sub>2</sub>) (b<sub>3</sub>) Cu doped Mn-Co layer, (c<sub>1</sub>) (c<sub>2</sub>) (c<sub>3</sub>) La doped Mn-Co layer, (d<sub>1</sub>) (d<sub>2</sub>) (d<sub>3</sub>)  
 Co-35Mn layer, (a<sub>3</sub>) (b<sub>3</sub>) (c<sub>3</sub>) (d<sub>3</sub>) EDS line scanning of elements

Table 1 Element concentration (at.%) on the surface of samples after oxidation at 750°C for 500 h

Alloy layers	Co	Mn	Cu	Fe	Cr	O
<b>Mn-35Cu</b>	-	22.6	12.2	6.8	-	58.4
<b>Cu doped Mn-Co</b>	11.8	20.9	7.0	3.8	-	56.5
<b>La doped Mn-Co</b>	15.6	19.2	-	5.4	-	59.8
<b>Co-35Mn</b>	14.2	24.3	-	6.5	-	55.0

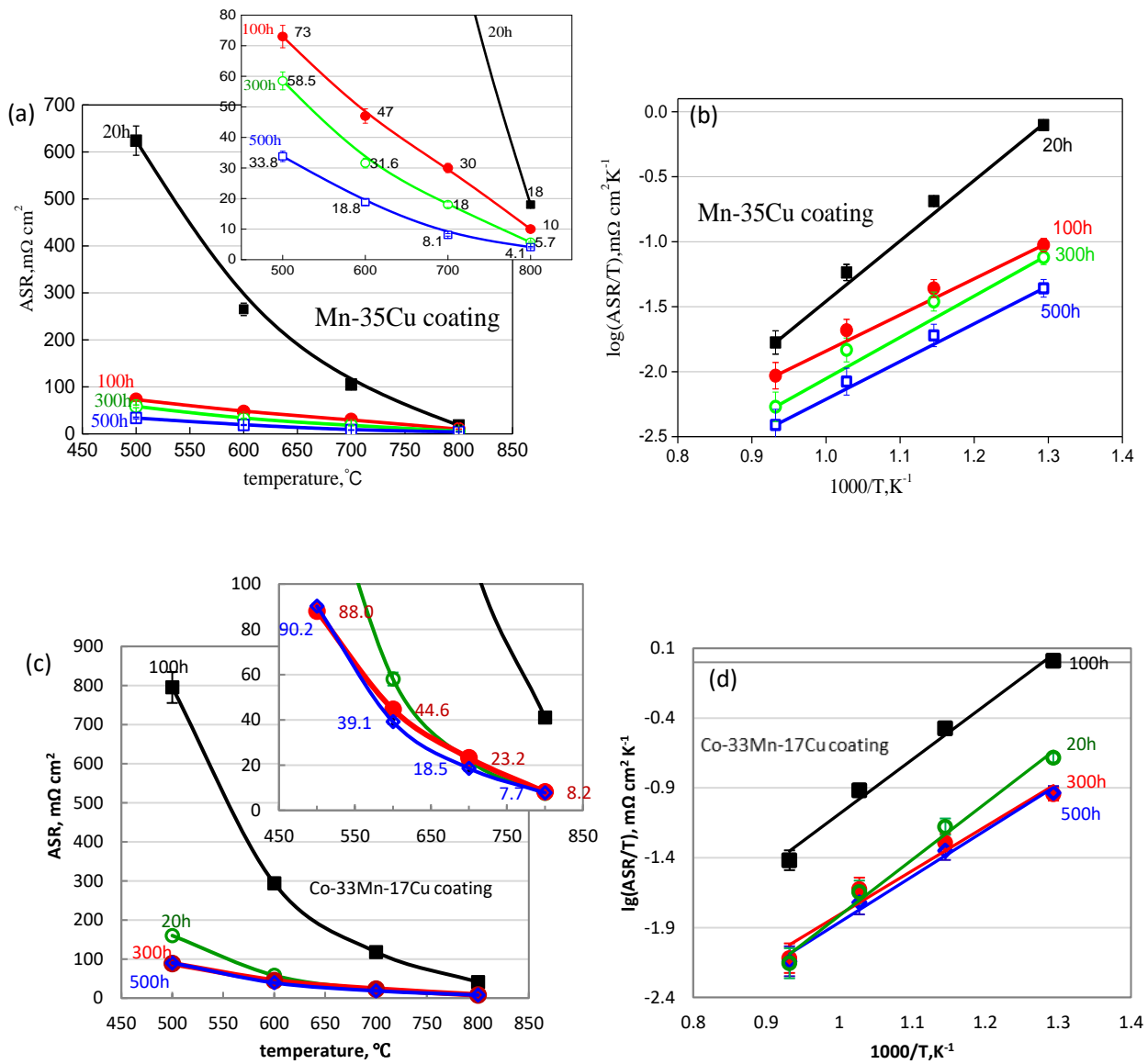


Fig.6 ASR values vs. temperature (a) (c) and Arrhenius plots of  $ASR/T$  vs.  $10^3/T$  (b) (d) for Mn-35Cu and Cu doped Mn-Co layers oxidized in air at 750°C with the extended oxidation time

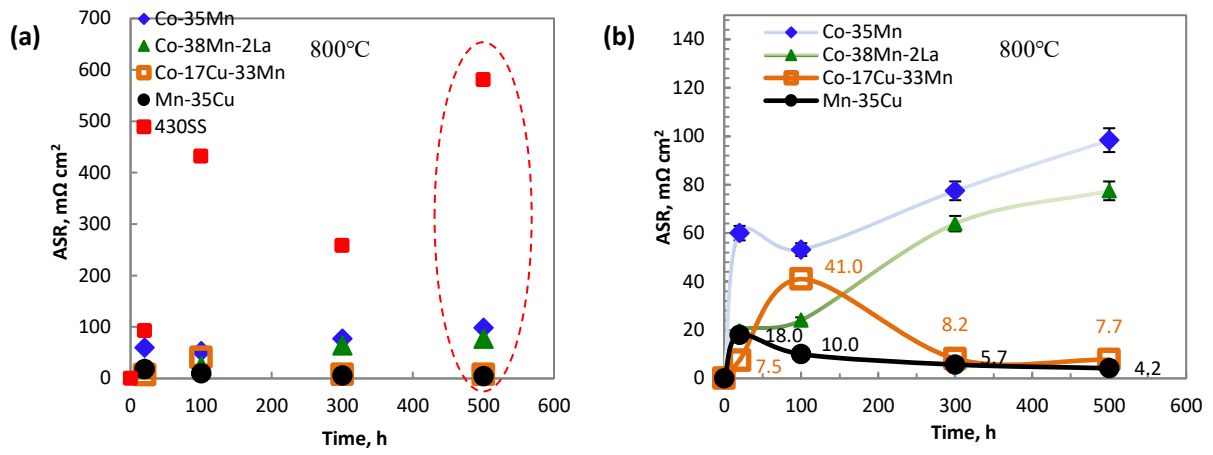


Fig.7 ASR values at 800°C vs. oxidation time for four oxide layers and bared 430 SS after oxidation at 750°C

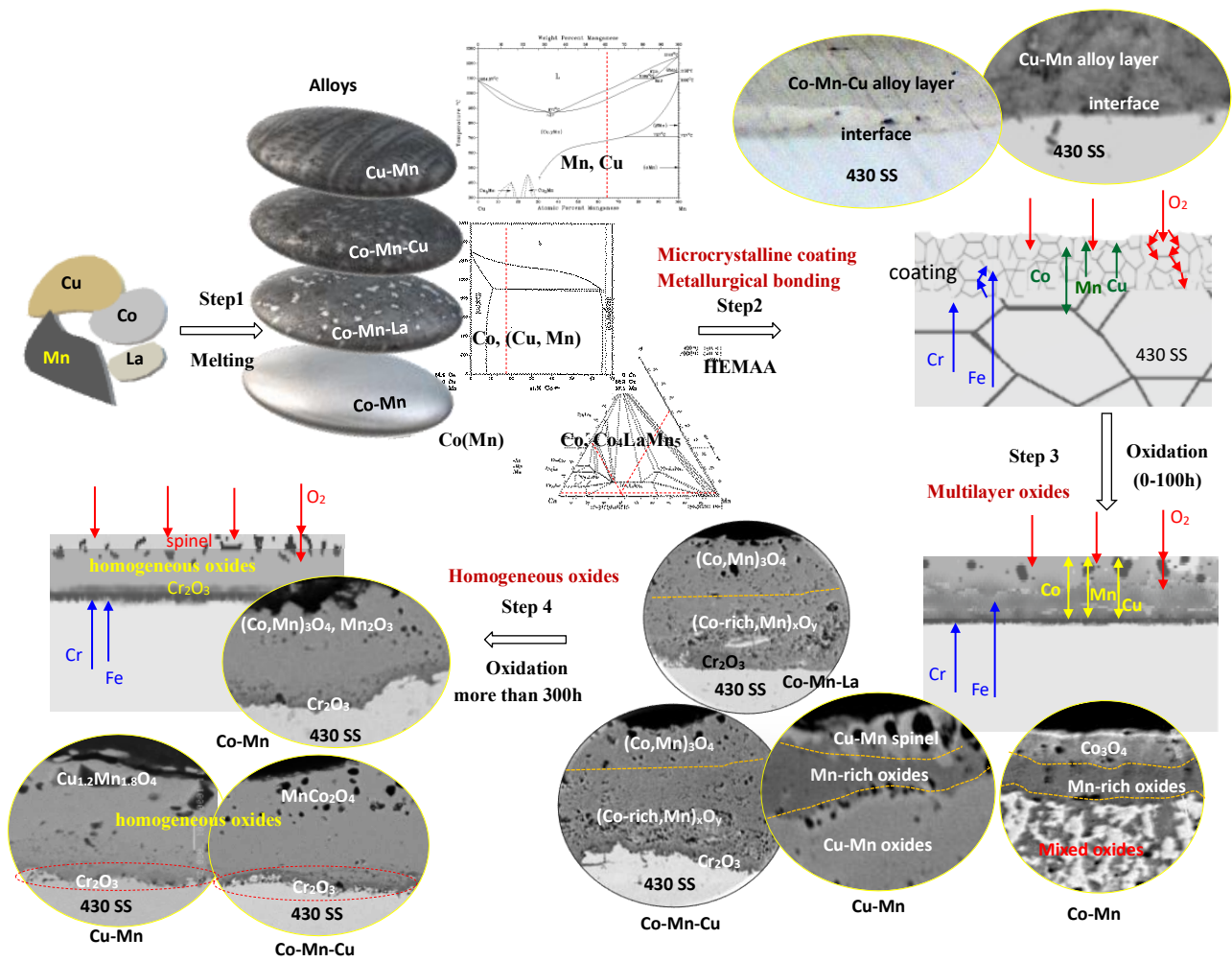


Fig.8 Schematic diagrams of formation process for the homogeneous oxides prepared by high-energy micro-arc alloying process[6, 21,22]