

# The University of Wisconsin Space Science and Engineering Center Absolute Radiance Interferometer (ARI): Instrument Overview and Radiometric Performance

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Logan, UT, USA



**SSEC Engineering Research and Development**

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# Summary

- The University of Wisconsin-Madison Space Science and Engineering Center (UW-SSEC) and Harvard University (HU) submitted a successful joint proposal entitled “[A New Class of Advanced Accuracy Satellite Instrumentation \(AASI\) for the CLARREO Mission](#)” to the NASA Instrument Incubator Program (IIP). The UW-SSEC / HU team has a long history with the scientific and measurement concepts that have formed the foundation for climate benchmark measurements from space
- The objective of this effort is to advance the technological development of advanced accuracy instrumentation for the measurement of [absolute spectrally resolved infrared radiances \(5 – 50  \$\mu\text{m}\$ \) with high accuracy \(< 0.1 K, k = 3, brightness temperature at scene temperature\)](#) for climate benchmark measurements from space
- The UW-SSEC, developed a [demonstration test bed](#) which includes an FTS instrument and calibration and validation system to demonstrate the feasibility of the far and mid infrared instrumentation for a Climate Benchmark Mission.

# Topics

1. Introduction
2. The UW-SSEC Absolute Radiance Interferometer (ARI)
3. Radiometric Performance
4. Conclusion

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# Climate Benchmark Measurements

- Satellite Instrument Calibration for Measuring Global Climate Change (NIST Publication NISTIR 7047, 2003)
- ASIC<sup>3</sup> Report: Achieving Satellite Instrument Calibration for Climate Change (2007)
- US NRC Decadal Survey (NRCDS, 2007): *Earth science and applications from space: national imperatives for the next decade and beyond*
  - Climate Absolute Radiance and Refractivity Observatory (CLARREO): Tier 1 (highest priority) mission
- NASA Implementation of CLARREO
  - Selected for development/implementation by NASA (lead: NASA LaRC)
  - Successful MCR (November 2010)
  - Guidance received in the President's FY 2012 budget removed \$1.24B from the \$2.08B FY'11 proposed Climate Initiative ... directed cuts include CLARREO
- **Zeus**

# Capability of Current Systems

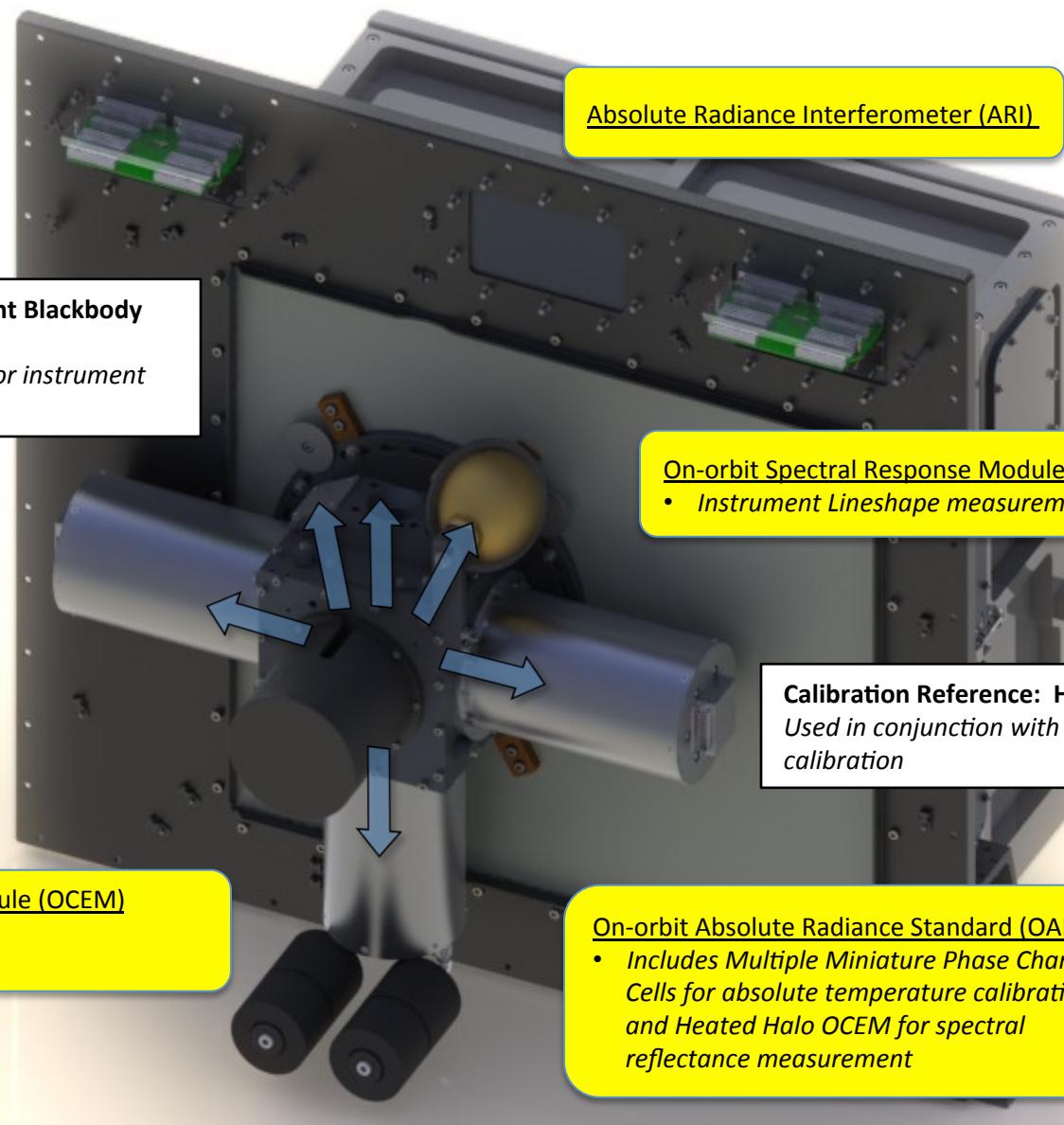
- Current generation of high resolution IR sounders: AIRS, IASI, CrIS...
  - Tremendous advance in information content & accuracy
  - Huge advance for climate process studies
- Provide a solid foundation for IR Climate Benchmark Measurement feasibility
- But, not optimized for unequivocal decadal trending of climate change, and for the most part, are not designed to provide:
  - The radiometric accuracy and sampling required to detect the small trends associated with global climate change
  - On-orbit calibration traceability to absolute standards
  - Far infrared (FIR) coverage beyond the normal IR sounding region (typically some part or all of the 3-15  $\mu\text{m}$  region)

# Requirements for IR Climate Benchmark Measurements

- **Absolute Accuracy:**  $< 0.1 \text{ K}$ ,  $k = 2$ , brightness temperature for combined measurement and sampling uncertainty for annual averages of  $15^\circ$  zones to approach goal of resolving a climate change signal in the decadal time frame
  - Measurement uncertainty:  $< 0.1 \text{ K}$ ,  $k = 3$
  - Sampling uncertainty:  $< 0.1 \text{ K}$ ,  $k = 3$
- **On-orbit Verification and Test:** Provide an **On-orbit Absolute Radiance/Brightness Temperature Standard** with an accuracy of  $< 0.1 \text{ K}$ ,  $k = 3$ , to provide SI traceability of on-orbit measurements
- **Spectral Coverage and Resolution:**  $200 - 2000$  (goal:  $3000$ )  $\text{cm}^{-1}$ ;  $\sim 0.5 \text{ cm}^{-1}$  ( $\pm 1$  cm MOPD)
- **Spatial Footprint & Angular Sampling:** Order 100 km **or less**, nadir only
- **Coverage:** Contiguous coverage **not** required

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# Technology Developments Under NASA IIP



Fred Best: ["On-Orbit Absolute Radiance Standard for the Next Generation of IR Remote Sensing Instruments"](#) (Monday, 13:35 – 13:55)  
Jon Gero: ["The Heated Halo for Space-Based Blackbody Emissivity Measurement"](#) (Tuesday, 16:30 – 16:50)

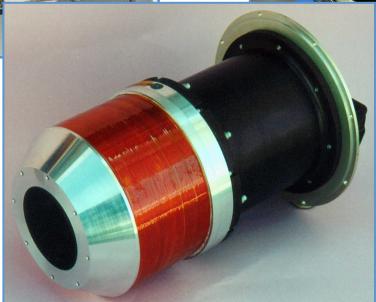
# UW-SSEC Spectrometer, Blackbody Heritage & Ties to NIST

Ground-based



AERI

NIST  
Water-bath  
Blackbody



High-altitude Aircraft

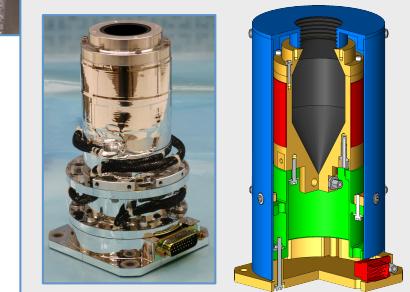


S-HIS

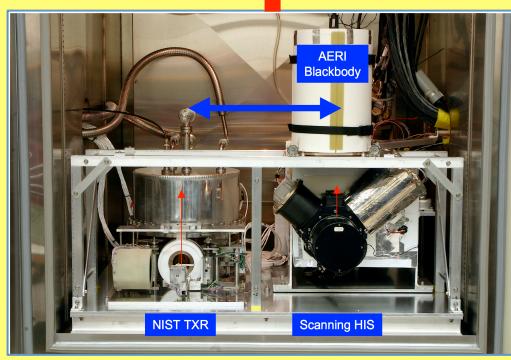
NIST  
TXR



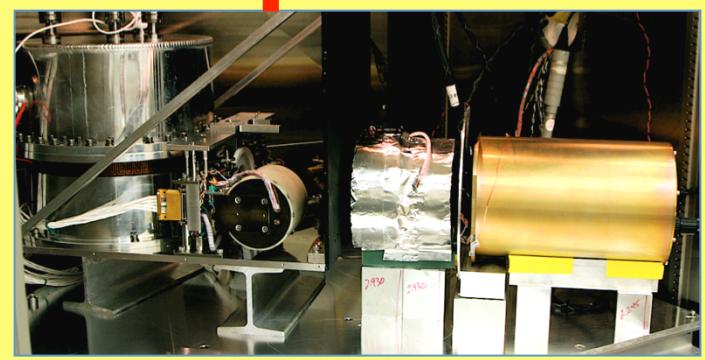
GIFTS



< 0.065 K error (293 to 333 K)



< 0.06 K error (220 to 333 K)



$\epsilon > 0.9994$  (within estimated uncertainty)

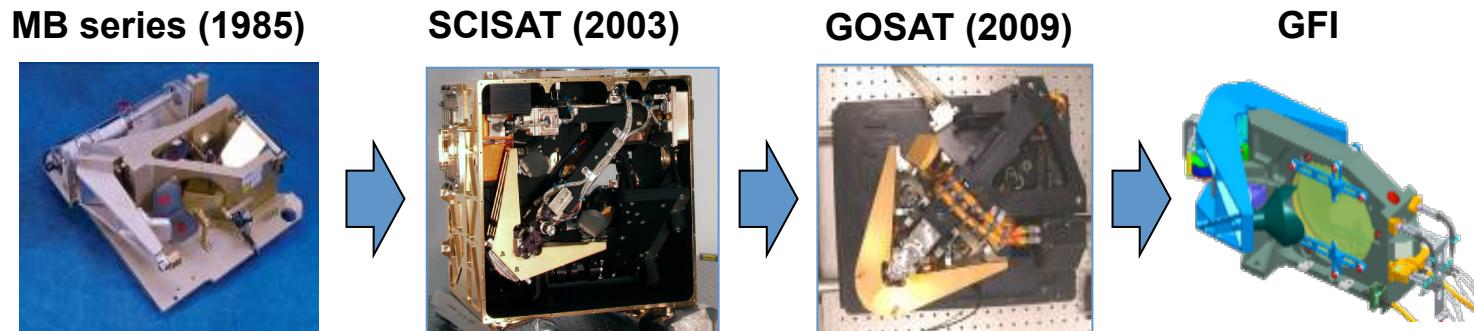
# UW-SSEC Absolute Radiance Interferometer

- The UW-SSEC Absolute Radiance Interferometer includes:
  - A scene selection mirror assembly;
  - Fore optics designed specifically for high radiometric accuracy;
  - A 4-port cube corner, rocking arm interferometer with a diode laser based metrology system;
  - Two aft optics assemblies, 1 at each output port of the interferometer;
  - A 77 K multiple semi-conductor detector ( $400 - 3000 \text{ cm}^{-1}$ ) and dewar assembly, and associated mechanical cooler;
  - A DTGS pyroelectric detector ( $200 - 1800 \text{ cm}^{-1}$ ) assembly.

Each chosen for their strong spaceflight heritage such that detailed performance testing can be conducted on a system with a clear path to space. *For compatibility with an IIP budgets, the electronics are not flight designs*

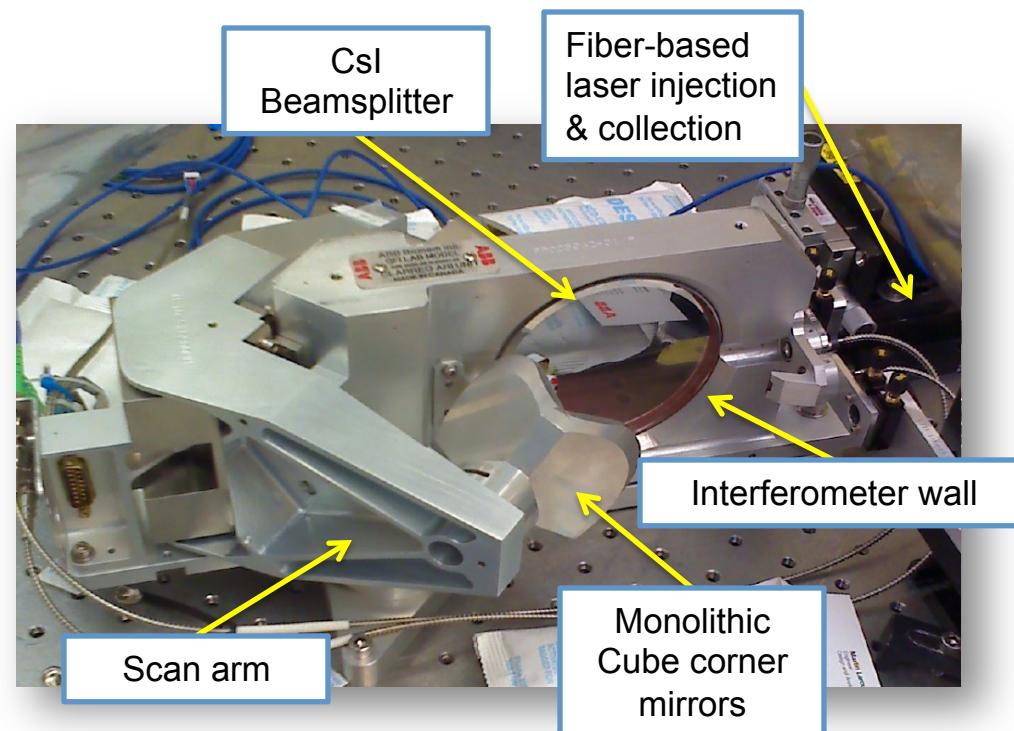
# The Generic Flight Interferometer (GFI)

- The UW ARI is based on ABB's Generic Flight Interferometer (GFI) architecture: a flex blade-based frictionless double pendulum scanning mechanism with 25 years of heritage and a direct evolution of 2 successful spaceborne interferometers:
  - **SCISAT / ACE-FTS (2003)**: Initial design life of 2 years and still operating in compliance with performance requirements after 9 years
  - **GOSAT / TANSO-FTS (2009)**: Currently meets all performance requirements in flight
- Additionally, the GFI baseline includes:
  - Fiber-linked metrology for reduced heat load on interferometer and simplified alignment / redundancy management
  - Monolithic cube corner mirror for increased robustness to launch vibration



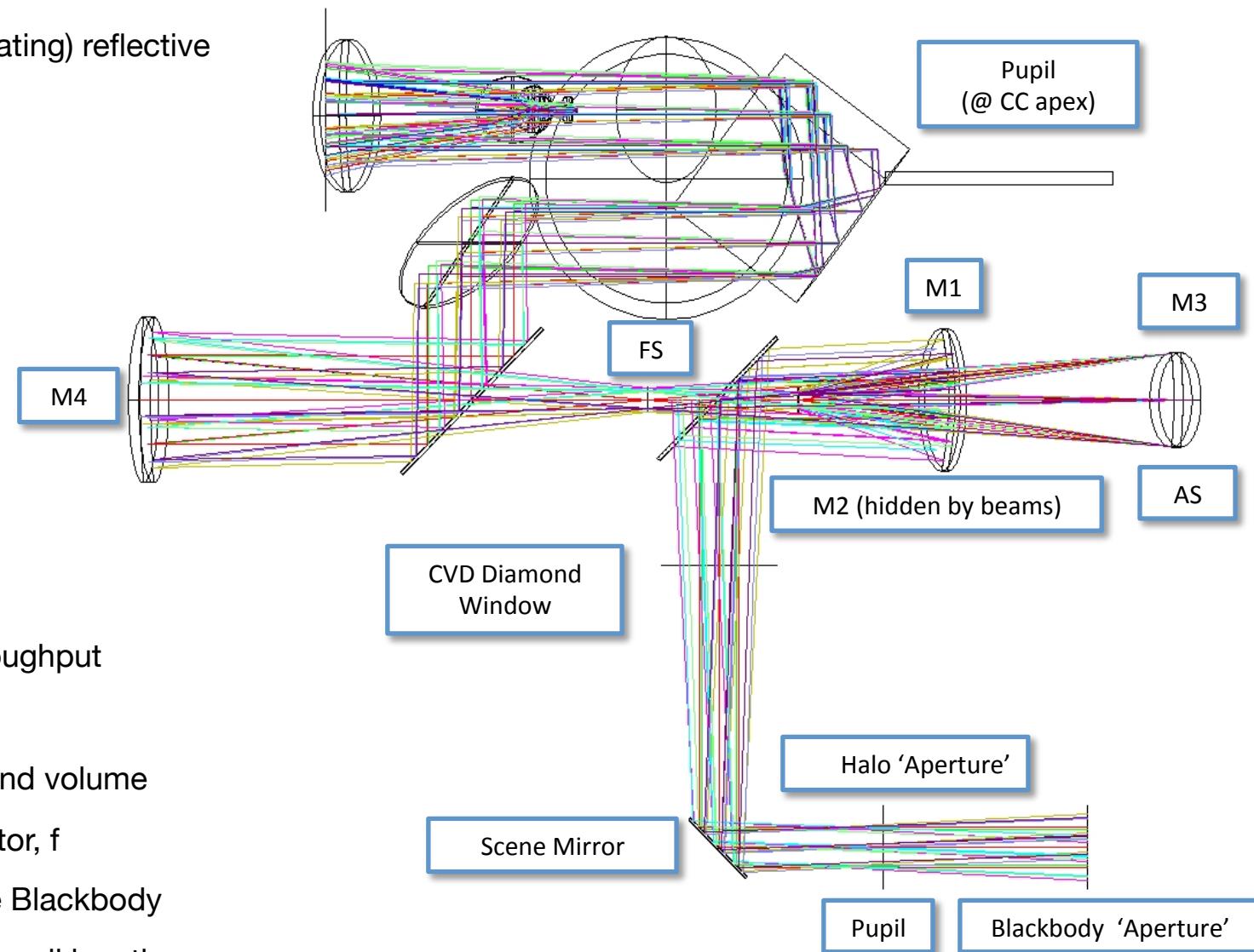
# The Generic Interferometer for Climate Studies (GICS)

- 4 port
- Different met laser path
- **CsI beamsplitter** to cover spectral range
- Mounting adapted for CsI
- **Self compensated beamsplitter** instead of substrate and compensator
- **Replicated monolithic cube corner**
- Vacuum compatible Interferometer
- Modified COTS electronics and software used for IIP
- Mass: < 7 kg (GICS, Aluminum)
- Power: Avg 18 W / Pk 23 W (flight design)



# Optical Design

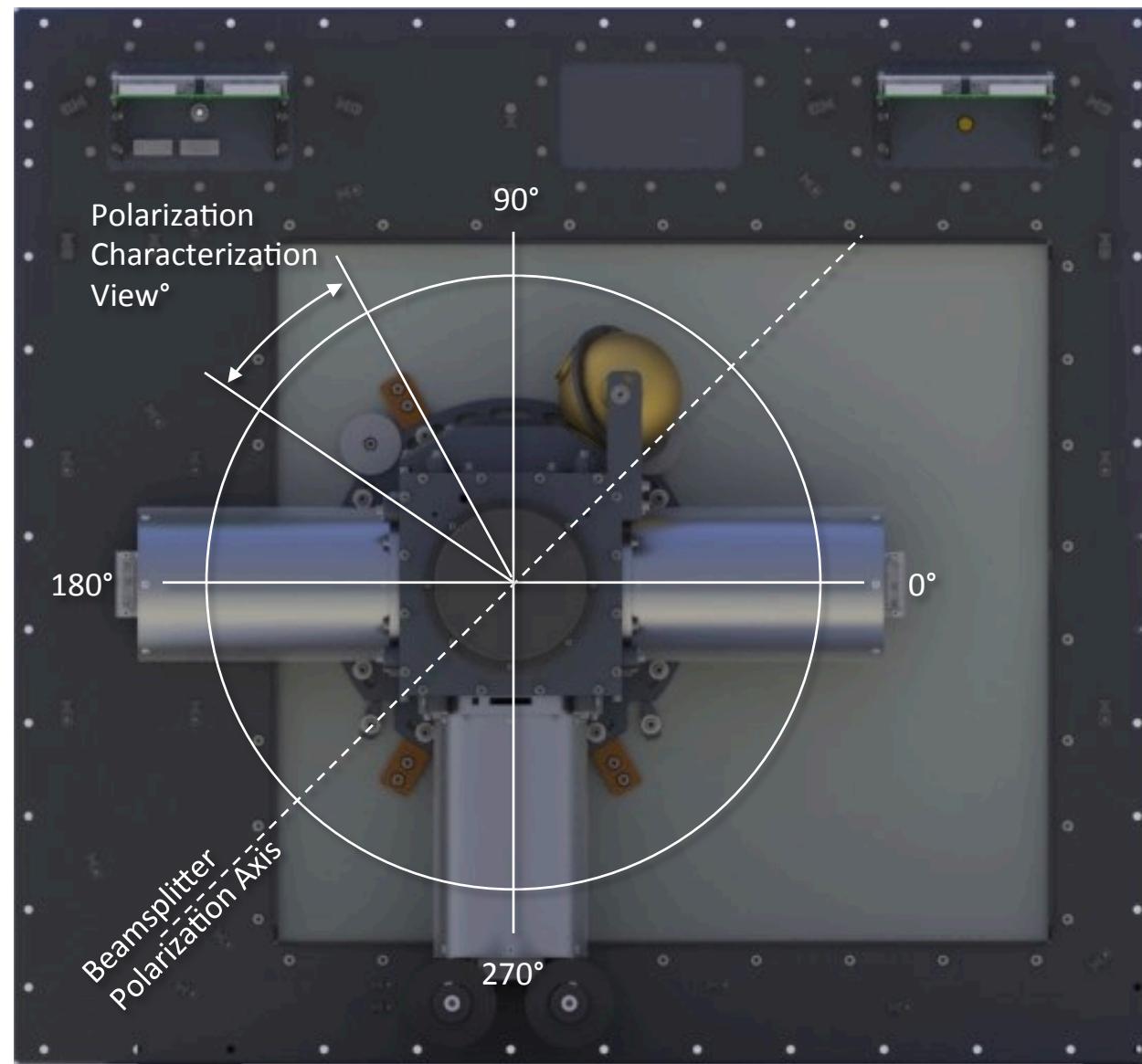
Gold coated Aluminum (no AR coating) reflective components



Design goals included:

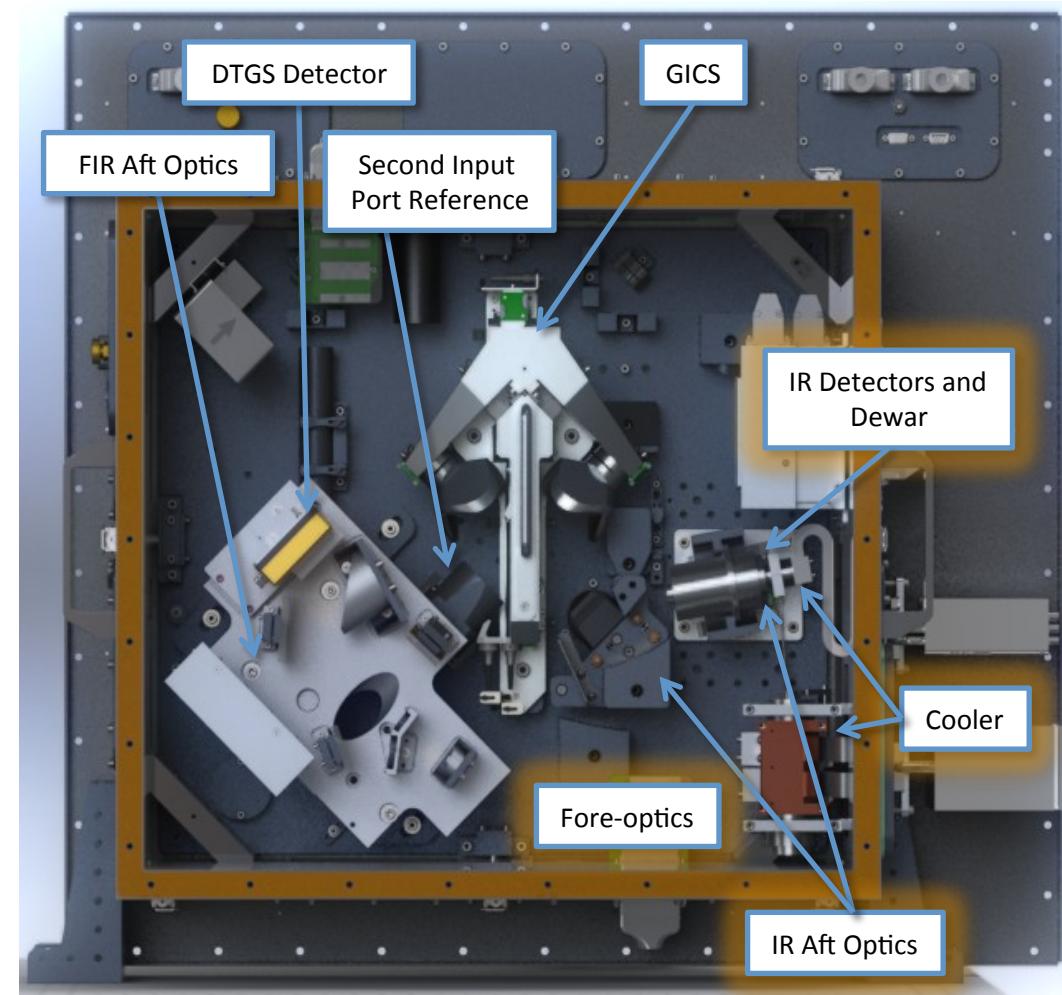
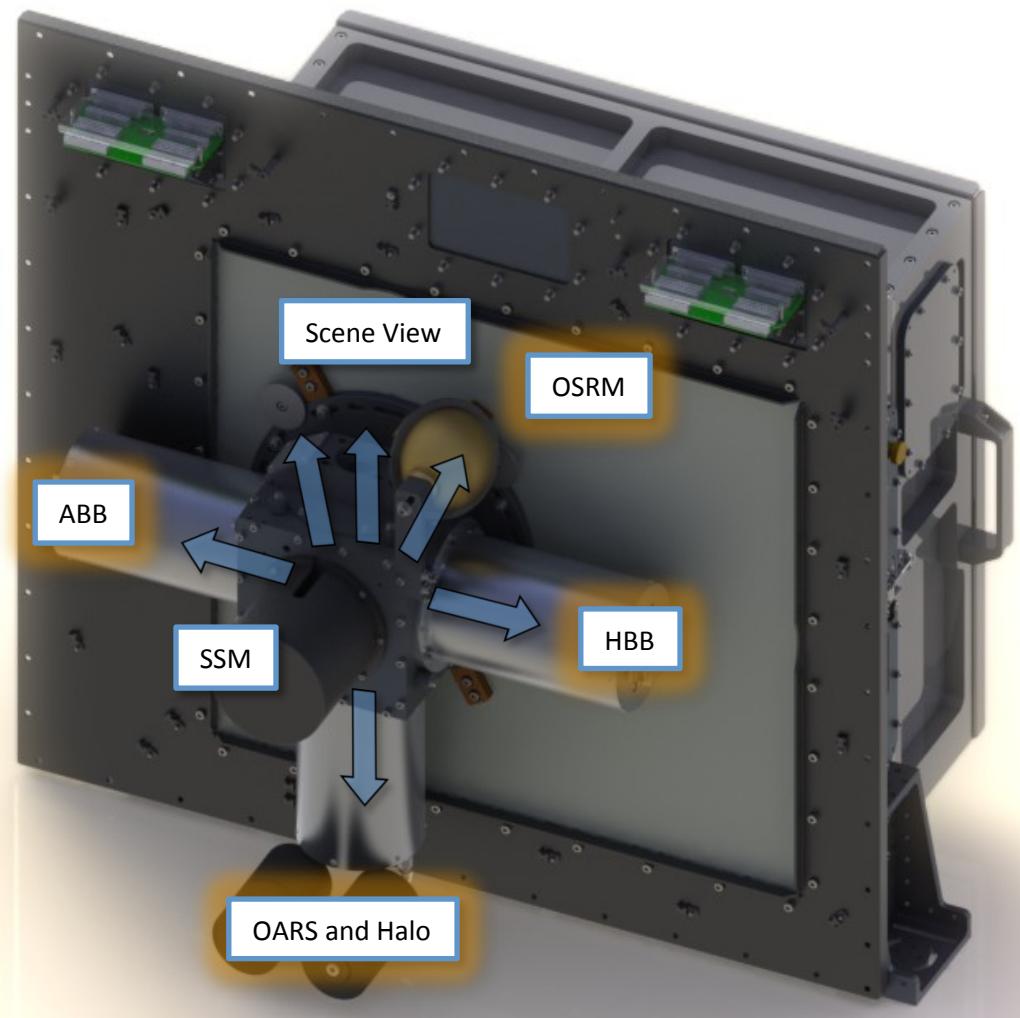
- Optimize interferometer throughput
- Maximize Stray light control
- Minimize instrument mass and volume
- Optimize heated halo fill factor,  $f$
- Compatible with 1" aperture Blackbody
- Allow 'tuning' of polarization null locations

# Absolute Radiance Interferometer



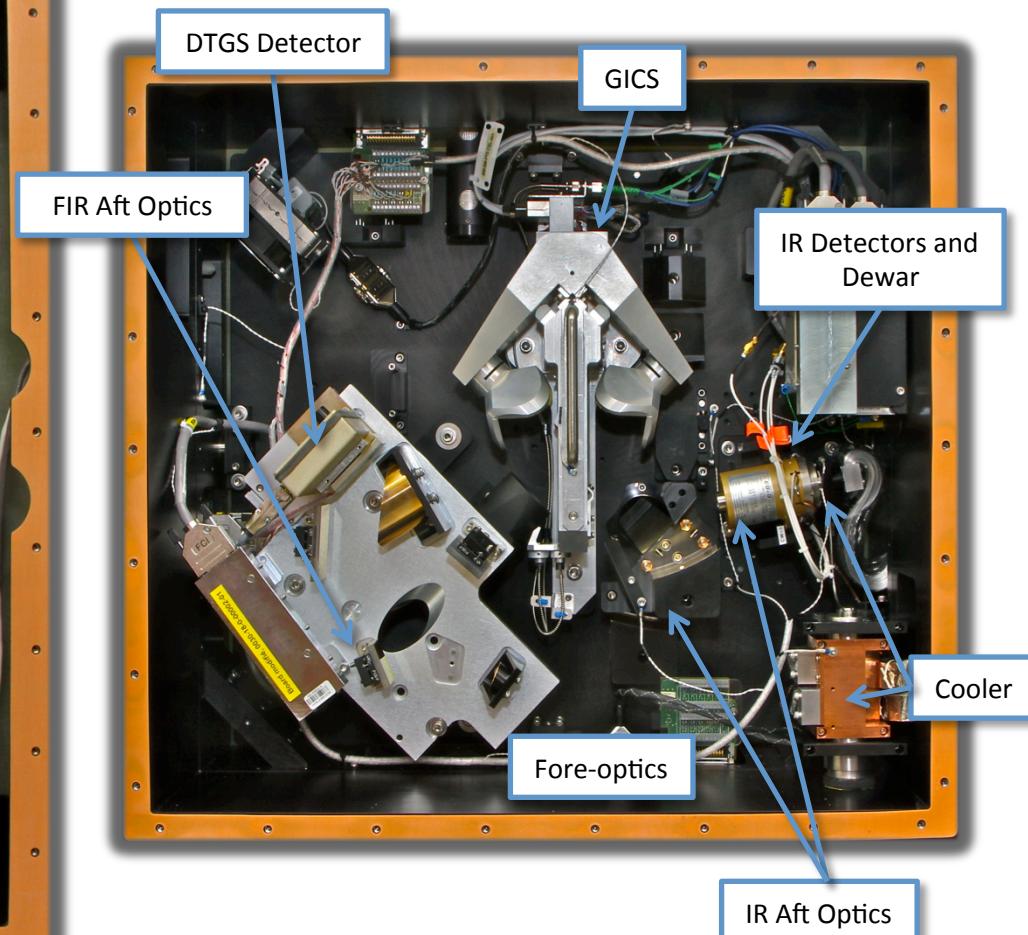
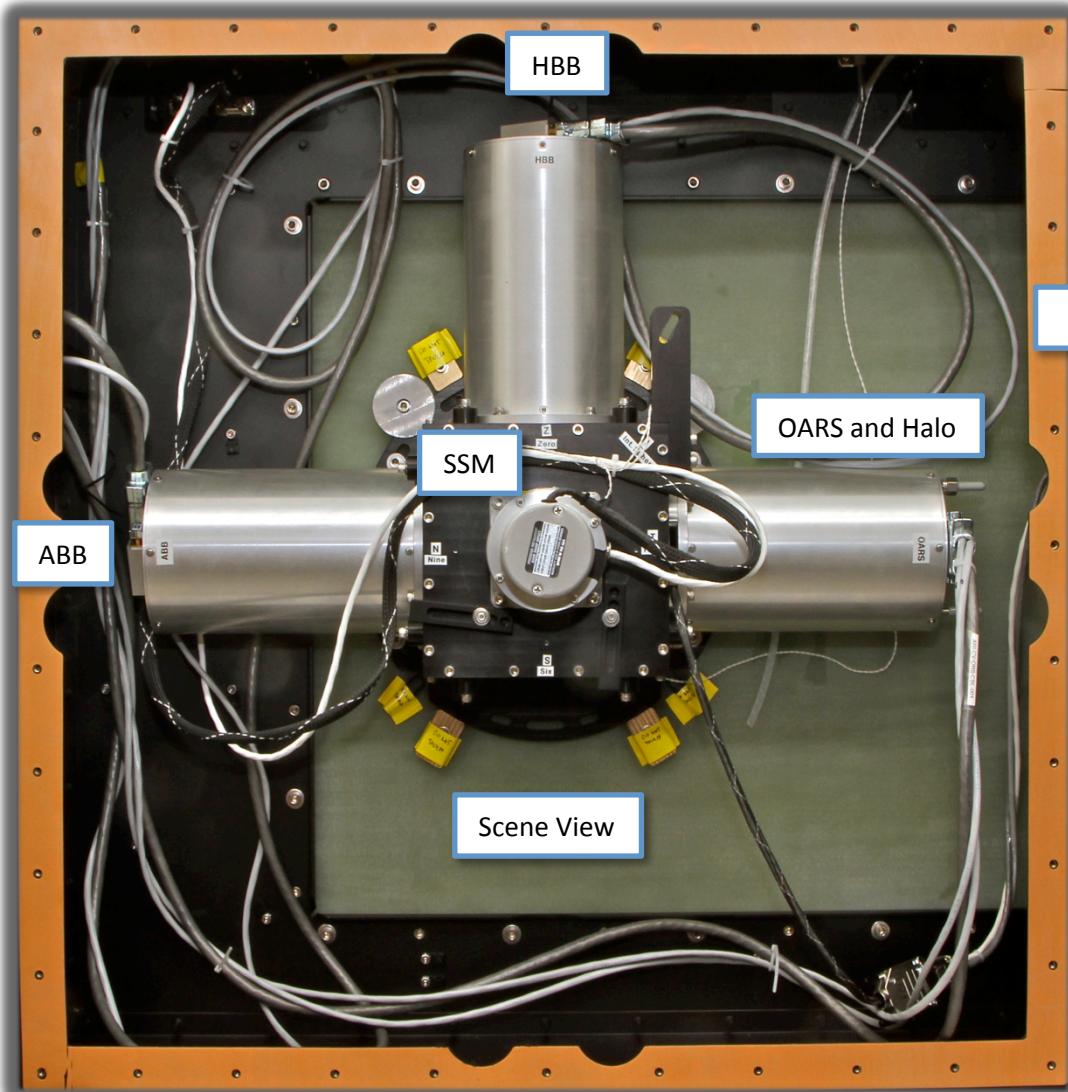
Viewing configuration providing immunity to polarization effects.

# Absolute Radiance Interferometer



Solid Model (Solidworks)

# Absolute Radiance Interferometer



Completed Prototype

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# Instrument Testing

- Near Field Response Mapping
- Detector Performance Testing and Demonstrations
- Interferometric Noise Testing and Analysis
- Spectral Calibration Verification
- Nonlinearity Characterization and Analysis
- Radiometric Calibration Verification: OARS
- Radiometric Calibration Verification: Ice Bath Blackbody
- OCEM Heated Halo

# Radiometric Uncertainty

- Recall the basic calibration expression for the complex calibration method:

$$N = (L_H - L_C) \operatorname{Re} \left\{ \frac{C_S - C_C}{C_H - C_C} \right\} + L_C,$$

$$L = eB(T) + (1-e)B(T_R)$$

- Radiometric uncertainty estimate: Differential error analysis (and/or perturbation analysis) of the calibration equation
- The uncertainty in the verification of the calibrated radiance includes a contribution from the uncertainty in the determination of the predicted radiance in addition to the uncertainty in the measured radiance

# Radiometric Uncertainty (Predicted On-orbit)

- **On-orbit:**
  - Space view for cold calibration reference
  - Onboard ambient calibration blackbody for “hot” calibration reference
  - These values satisfy the Zeus/CLARREO accuracy requirements

Temperatures			Associated Uncertainty (3- $\sigma$ )	
Cold Cal Ref (Space Target)	$T_C$	4 K	$u(T_C)$	0 K
Hot Cal Ref (Internal Cal Target)	$T_H$	295 K	$u(T_H)$	0.045 K
Verification Target (OARS)	$T_{OARS}$	220 – 320 K	$u(T_{OARS})$	0.045 K
Reflected Radiance, Cold Cal Ref	$T_{R,C}$	290 K	$u(T_{R,C})$	0 K
Reflected Radiance, Hot Cal Ref	$T_{R,H}$	290 K	$u(T_{R,H})$	4 K
Reflected Radiance, Verification Target	$T_{R,OARS}$	290 K	$u(T_{R,OARS})$	4 K
Emissivities				
Cold Cal Ref (Space Target)	$e_C$	1	$u(e_C)$	0.0006
Hot Cal Ref (Internal Cal Target)	$e_H$	0.999	$u(e_H)$	0.0006
Verification Target (OARS)	$e_{OARS}$	0.999	$u(e_{OARS})$	0.0006*

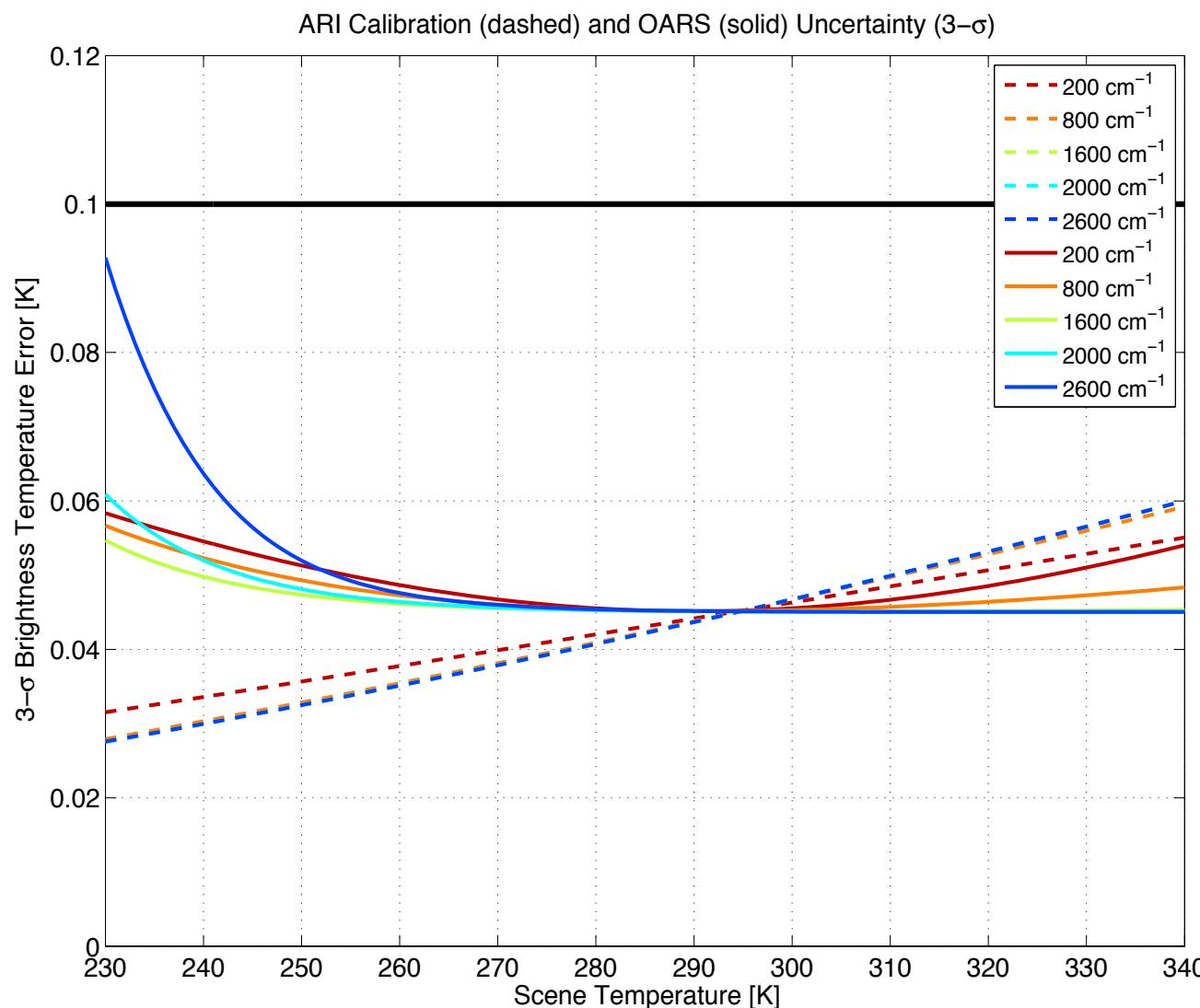
Cal BB / OARS  
Uncertainty Analysis

Halo Uncertainty  
Analysis

- \* **For the On-orbit uncertainty analysis**, it has been assumed that the OARS emissivity and associated uncertainty is determined from prelaunch TVAC testing with a very high emissivity source

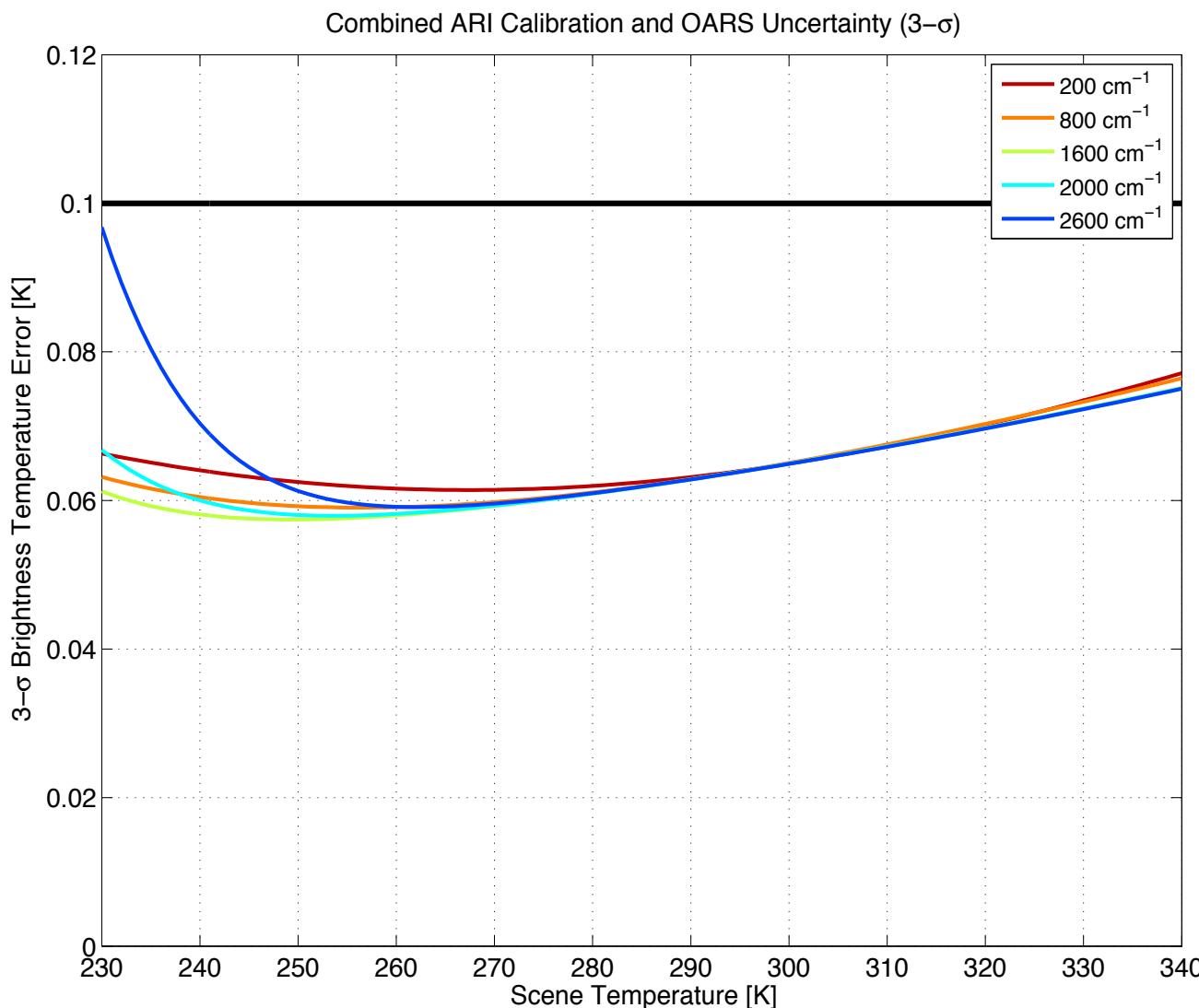
- $e_{OARS} = 0.9990 \pm 0.0006$  (200 cm<sup>-1</sup>)
- $e_{OARS} = 0.9990 \pm 0.0004$  (800 cm<sup>-1</sup>)
- $e_{OARS} = 0.9990 \pm 0.0002$  (1400 cm<sup>-1</sup>)
- $e_{OARS} = 0.9990 \pm 0.0001$  (2000 cm<sup>-1</sup>)
- $e_{OARS} = 0.9990 \pm 0.00075$  (2600 cm<sup>-1</sup>)

# Radiometric Uncertainty (Predicted On-orbit)



\* Uncertainty due to residual nonlinearity not shown

# Radiometric Uncertainty (Predicted On-orbit) Combined UW – ARI Calibration and OARS Uncertainty ( $k = 3$ )



\* Uncertainty due to residual nonlinearity not shown

# Radiometric Uncertainty (Laboratory Environment)

- IIP Demonstration (Laboratory Environment):
  - Onboard ambient calibration blackbody for “cold” calibration reference
  - Onboard hot calibration blackbody for “hot” calibration reference

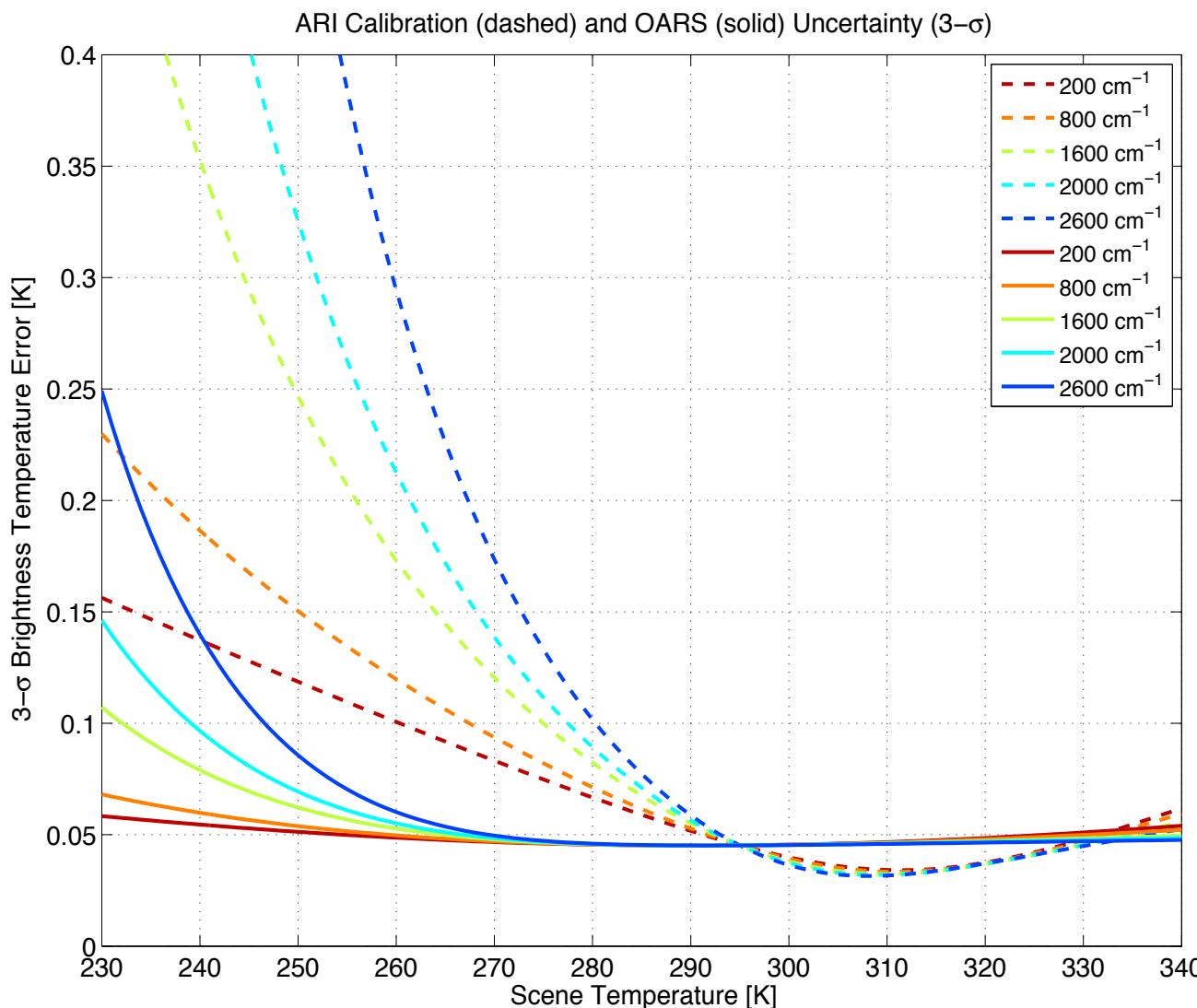
Temperatures			Associated Uncertainty (3- $\sigma$ )	
Cold Cal Ref (Ambient Blackbody)	$T_c$	293 K	$u(T_c)$	0.045 K
Hot Cal Ref (Hot Blackbody)	$T_h$	333 K	$u(T_h)$	0.045 K
Verification Target (OARS)	$T_{OARS}$	213 – 333 K	$u(T_{OARS})$	0.045 K
Reflected Radiance, Cold Cal Ref	$T_{R,C}$	290 K	$u(T_{R,C})$	4 K
Reflected Radiance, Hot Cal Ref	$T_{R,H}$	290 K	$u(T_{R,H})$	4 K
Reflected Radiance, Verification Target	$T_{R,OARS}$	290 K	$u(T_{R,OARS})$	4 K
Emissivities				
Cold Cal Ref (Ambient Blackbody)	$e_c$	0.999	$u(e_c)$	0.0006
Hot Cal Ref (Hot Blackbody)	$e_h$	0.999	$u(e_h)$	0.0006
Verification Target (OARS)	$e_{OARS}$	0.999	$u(e_{OARS})$	0.0006

Cal BB / OARS Uncertainty Analysis

Halo Uncertainty Analysis

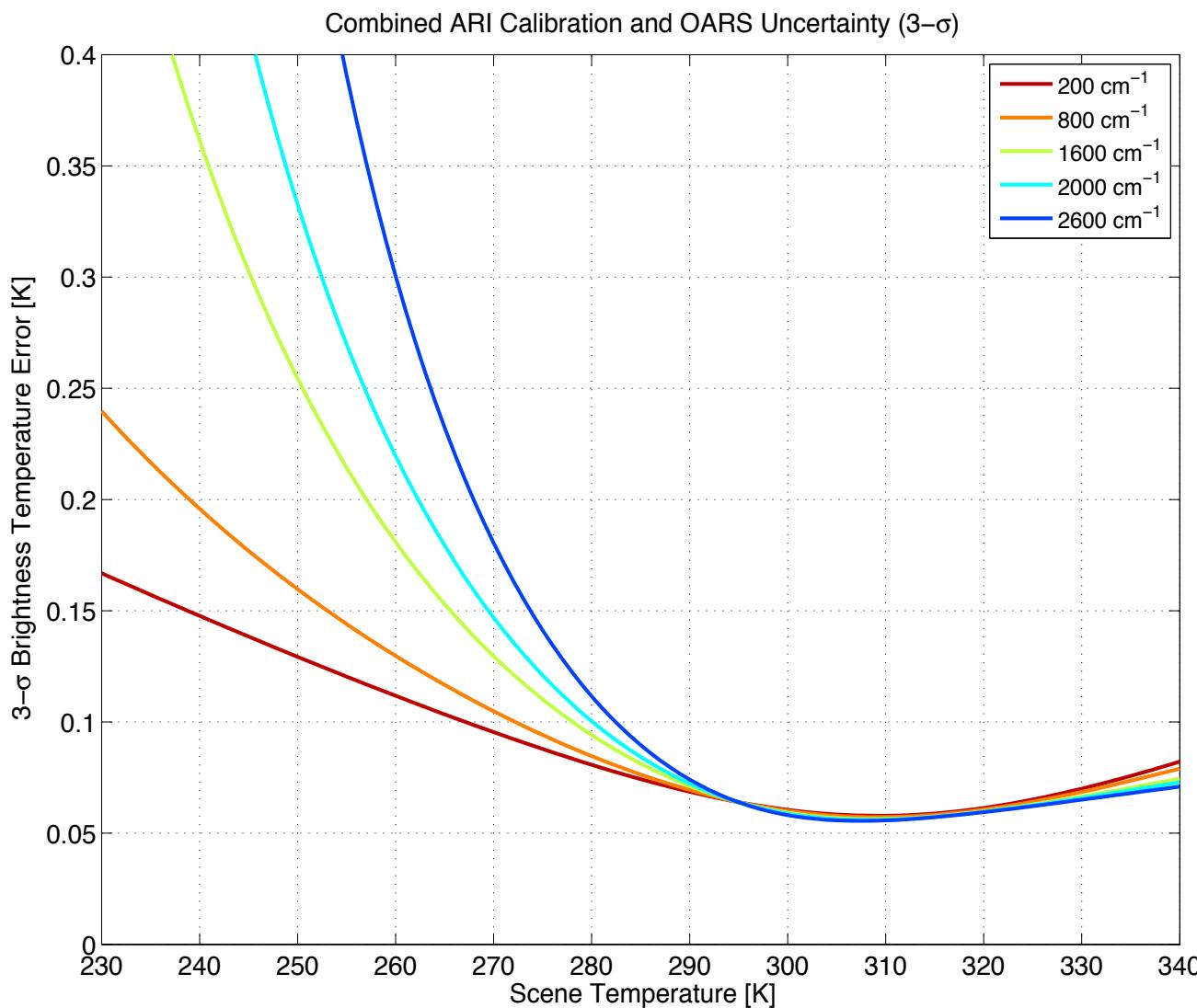
# Radiometric Uncertainty (Laboratory Environment)

## UW – ARI Calibration and OARS Uncertainty ( $k = 3$ )



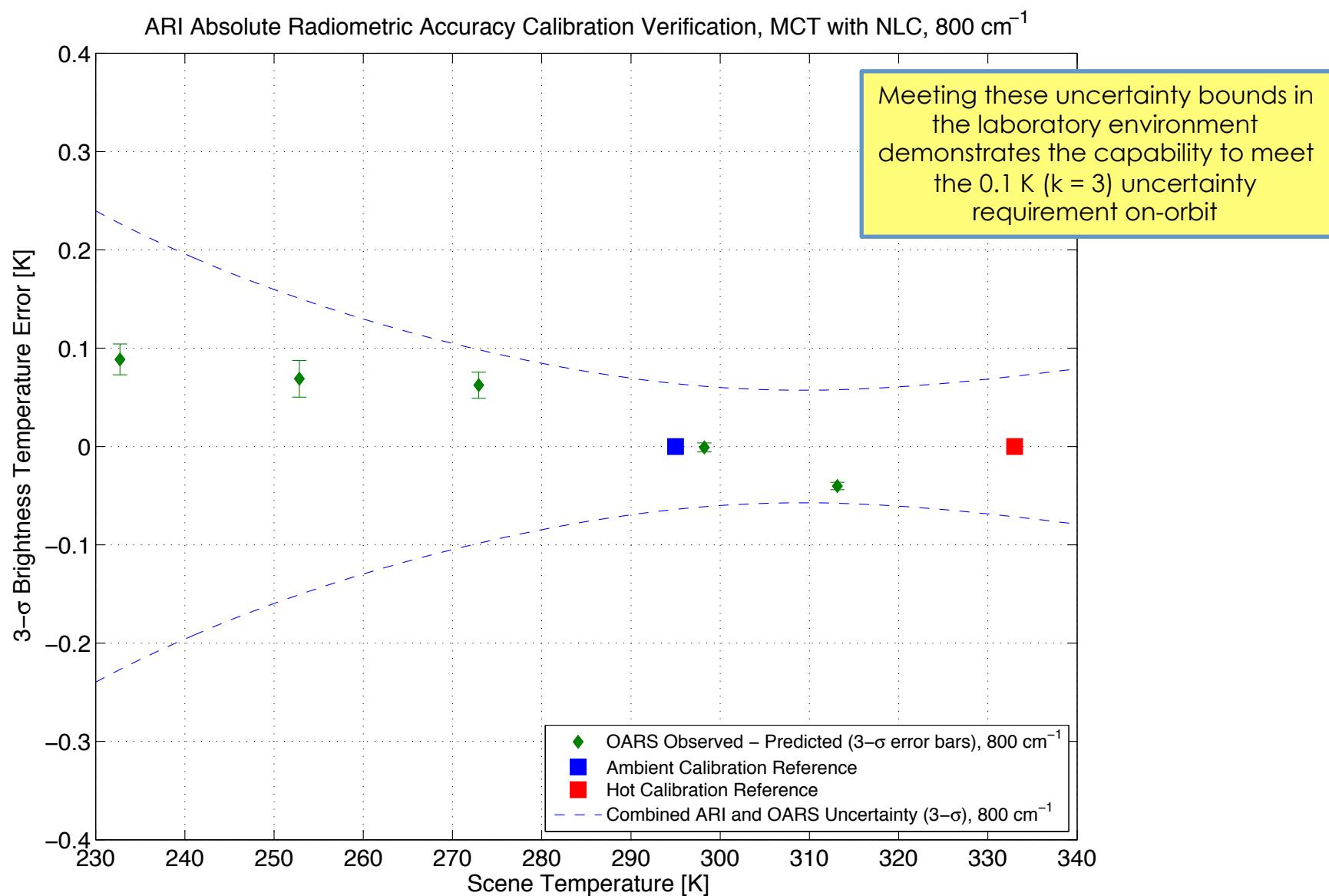
# Radiometric Uncertainty (Laboratory Environment)

## Combined UW – ARI Calibration and OARS Uncertainty ( $k = 3$ )

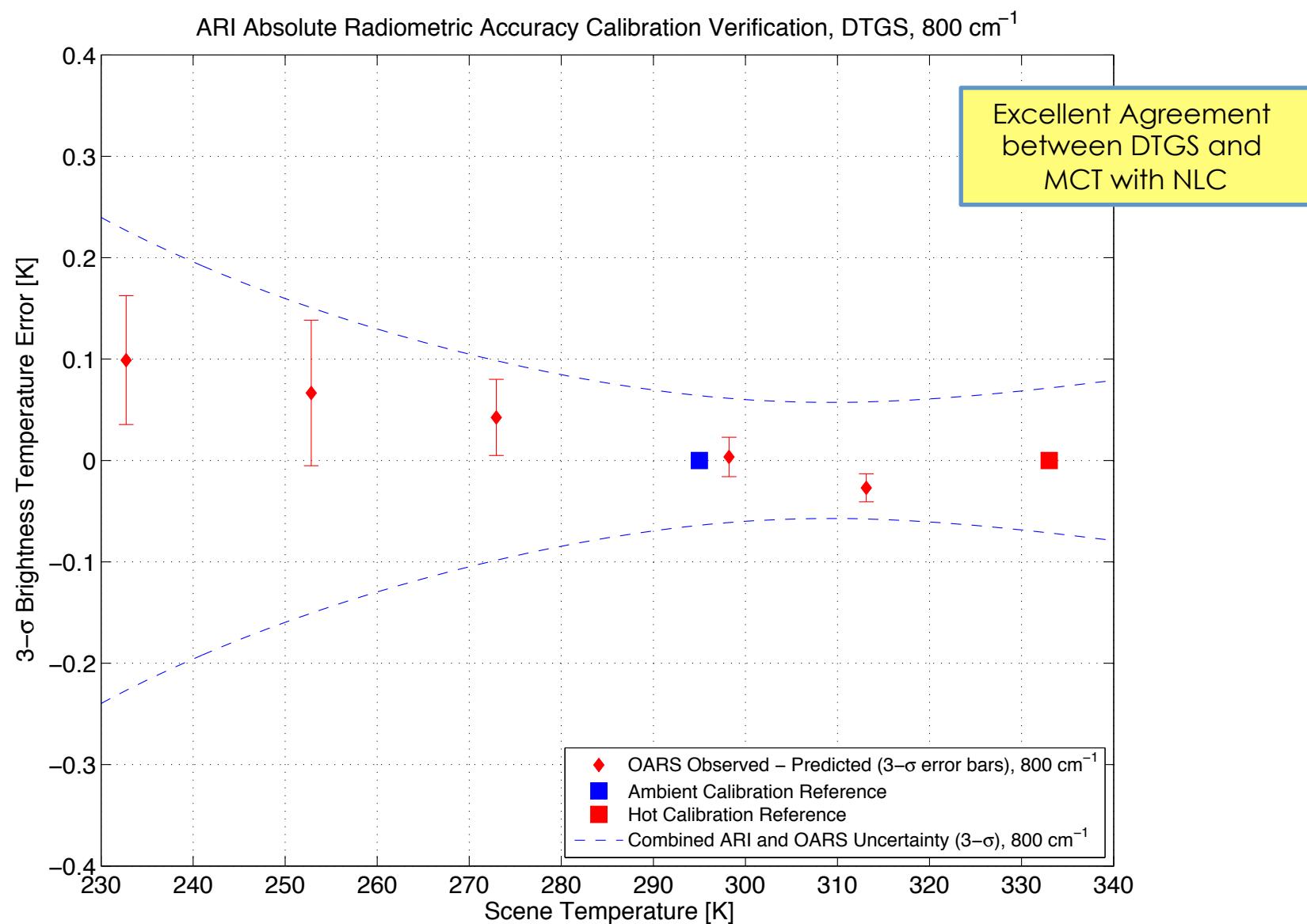


Meeting these uncertainties in the laboratory environment demonstrates the capability to meet the 0.1 K ( $k = 3$ ) uncertainty requirement on-orbit

# Radiometric Calibration Verification – MCT with NLC



# Radiometric Calibration Verification – DTGS ( $800\text{ cm}^{-1}$ )



# Conclusion

- An excellent, low cost, climate benchmark mission has been defined
- The proposed IR measurement requirements are supported by good technical readiness
- The UW-SSEC ARI (and OTM)
  - Facilitates the demonstration of the technology necessary to measure IR spectrally resolved radiances ( $5 - 50 \mu\text{m}$ ) with ultra high accuracy ( $< 0.1 \text{ K}$ ,  $k = 3$ , brightness temperature at scene temperature) for a benchmark climate mission.
  - Subsystems have been selected and developed to provide a system with a clear path to space.
  - Initial end to end system tests have been completed – meets radiometric uncertainty goals
  - Vacuum testing preparation underway
- This technology can form the basis of a future climate benchmark mission, such as CLARREO or Zeus.

# THANK YOU