# The Radiative and Conductive Heat Exchange of a Cold Desert 

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THE RADIATIVE AND CONDUCTIVE HEAT EXCHANGE

OF A COLD DESERT
by
Luis R. Martinez

A thesis submitted in partial fulfillment of the requirements for the degree
of

MASTER OF SCIENCE
in
Soil Science and Biometeorology
in

Biometeorology

Approved:

UTAH STATE UNIVERSITY Logan, Utah

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Luis R. Martinez

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## LIST OF SYMBOLS AND DEFINITION OF TERMS

```
R
R
R
    cm. - min. - )
    \alpha = albedo (dimensionless)
R
    ( cal. cm. - min-1 )
R
    (cai. cm. -2 min-1 )
R 
RA}-\mp@subsup{R}{E}{}=\mathrm{ long wave net radiation (long wave radiation) (cal. cm. -2
        min}\mp@subsup{0}{}{-1}\mathrm{ )
\varepsilon = emissivity (dimensionless)
\sigma = Stefan-Boltzmann constant ( }8.13\times1\mp@subsup{0}{}{-11}1\textrm{y}.\mp@subsup{\textrm{min}}{}{-1}\mp@subsup{\textrm{K}}{}{-4}\mathrm{ )
T = absolute temperature at the surface (degrees Kelvin)
K = coefficient of thermal conductivity of soil (cal. cm. - . }\mp@subsup{}{0}{0}\mp@subsup{\textrm{C}}{}{\mathbf{-1}}\mp@subsup{\textrm{min}}{}{-1}\mathrm{ )
\lambda coefficient of thermal diffusivity of soil ( cm. min. }\mp@subsup{}{}{-1}\mathrm{ )
c = specific heat of soil (cal. }\mp@subsup{}{}{\circ}\mp@subsup{\textrm{C}}{}{-1}\textrm{g}\mp@subsup{.}{}{-1}
\rho
C
t = time (min.)
\partialT/\partialt = change in temperature at a given point with time ( }\mp@subsup{}{}{\circ}\textrm{C}.\operatorname{min}\mp@subsup{.}{}{-1}
\partial}\mp@subsup{}{}{2}\textrm{T}/\partial\mp@subsup{\textrm{Z}}{}{2}=\mathrm{ rate of change of temperature gradient ( }\mp@subsup{}{}{\circ}\mp@subsup{\textrm{C}}{}{2}.\mp@subsup{\textrm{cm}}{}{-2}
```


## LIST OF SYMBOLS AND DEFINITION OF TERMS (Continued)

```
Z = depth (cm.)
\Delta finite increment
i = subscript denoting the "ith" depth increment at i.z depth
j = subscript denoting the "jht" time increment at a time j.T
a = empirical constant ( 0.820)
b = empirical constant ( 0.250)
c = empirical constant (0.094)
e = vapor pressure (mb.)
D = amplitude or phase equation ( }\mp@subsup{\textrm{cm}}{0}{2}.\mp@subsup{\textrm{sec}}{}{-1}
A}\mp@subsup{A}{1}{}=\mathrm{ amplitude at Z }\mp@subsup{|}{1}{}(\mp@subsup{}{}{\circ}\textrm{C}
A}\mp@subsup{\mp@code{2}}{}{=}\mathrm{ amplitude at }\mp@subsup{\textrm{Z}}{2}{}(\mp@subsup{}{}{\circ}\textrm{C}
\deltat = time interval between occurrence of maximum soil temperature at
    depths }\mp@subsup{Z}{1}{}\mathrm{ and }\mp@subsup{Z}{2}{}
w = radial frequency
\DeltaHC = change in heat content
```

ABSTRACT

The Radiative and Conductive Heat Exchange of a Cold Desert by

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Utah State University, 1975
Major Professor: Dr. I. Dirmhirn
Department: Soil Science

The heat exchange during dry conditions in Curlew Valley for selected clear days is determined from recordings in 10 minute intervals. The two heat budget components, radiative exchange and heat flow in the soil, are studied in detail.

Maximum surface temperature due to radiative exchange above, assuming no heat loss by other components, is determined.

Reduction of surface temperature by heat conduction into the ground was calculated as a second step to solve the heat budget equation.

Substantial heat flow throughout a day is restricted to the upper 10 cm of the soil.

Diffusivity of the soil was determined from soil temperature using phase and amplitude equations, of which the first gave better results.

## Introduction

This study is concerned with the determination of radiative and conductive heat exchange of a cold desert. Curlew Valley was selected, since the sagebrush desert type is one of the most extensive vegetation types in the United States and the study of this type has a high priority in the Desert Biome Program.

Important in analysis of the sagebrush ecosystem is the movement of heat within the system, since the soil plant interface forms a particular environment where climatic phenomena and processes occur and, under normal circumstances, a considerable exchange of heat occurs across it.

The thermal phenomena occuring in the air layer near the ground depend on the algebraic sum of all heat balance components: (1) influx and loss of heat by radiation at the surface $\left(\mathrm{R}_{\mathrm{N}}\right)$, (2) heat exchange between the surface and deeper layers of the soil (Q), (3) heat exchange between soil and air (H), and (4) heat lost by evaporation of water from the surface or heat gained by condensation and sublimation of water vapor (LE).

In accordance with the law of conservation of energy at any given moment the inflow and outflow of heat in the active surface should be equal. To express this condition mathmatically, the algebraic sum of all inflow and outflow on the active surface is equal to zero:

$$
\begin{equation*}
R_{N}+Q+H+L E=0 \tag{1}
\end{equation*}
$$

Of all the above mentioned heat balance components, only $R_{N}$ and Q will be considered in this thesis, while $H$ and LE will be part of our other forthcoming study. From the existing data, days under "dry" condition were selected, such that LE could be considered zero. The equation then reduces to the first three components and a balance can be written considering $H$ as a residual component while $R_{N}$ and $Q$ are studied in detail using the recorded data.

## Objectives

1. To determine the radiative and conductive heat exchange of a cold desert.
a) To evaluate existing models to describe radiative and conductive heat exchange.
b) To determine the conductive and radiative properties of a cold desert.

## Net radiation

The radiation balance or net radiation can be expressed by the equation

$$
\begin{equation*}
R_{N}=\left(R_{S}+R_{D}\right)(1-a)-R_{E}+R_{A} \tag{2}
\end{equation*}
$$

The radiant energy from the sun ( $0.3-4 \mathrm{u}$ ) is dissipated and distributed by components of the earth's atmosphere as it passes downward toward the earth. A portion is reflected by clouds into outer space; some is absorbed by the molecules of carbon dioxide, oxygen, ozone and water vapor. Part is scattered and diffused by the molecules and small particles in the air. A portion of this diffused radiation is returned
to outer space. The remainder is transmitted to the earth's surface as sky radiation $\left(R_{D}\right)$. That fraction of the solar radiation that is not affected by the earth's atmosphere reaches the surface as a direct beam ( $R_{S}$ ).

The global radiation reaching the earth's surface is partitioned into reflected radiation $a\left(R_{S}+R_{D}\right)$ and absorbed energy, which is utilized in heating the soil and the air above the soil, or in latent heat of evaporation, or in long wave net radiation ( $R_{A}-R_{E}$ ). Long wave radiation ( 4 to 100 u ) is emitted by the earth's surface to the sky. It is referred to as "terrestrial" or "outgoing" radiation ( $\mathrm{R}_{\mathrm{E}}$ ) and is equal to $\varepsilon \sigma T^{4}$. $R_{E}$ takes place both day and night. Approximately $90 \%$ of this radiation is absorbed by the earth's atmosphere, primarily by water vapor. There is considerable reradiation of this absorbed radiation back to the surface. This is known as atmospheric radiation $\left(R_{A}\right)$ which plays the major role in preventing excessive cooling at the earth's surface at night.

The difference between the outgoing terrestrial radiation and the atmospheric radiation is referred to as net long-wave radiation $\left(R_{A}-R_{E}\right)$. At night $R_{S}, R_{D}$ and $a\left(R_{S}+R_{D}\right)$ are zero, then

$$
\begin{equation*}
R_{N}=R_{A}-R_{E} \tag{3}
\end{equation*}
$$

Heat flux between the surface
The heat flux into the soil and the daily, seasonal and yearly heat accumulations are determined by the thermal properties of the soil and boundary conditions of the soil. These thermal properties or parameters are: $K, \lambda$, and $C_{V}$. The following relationship exists between
these three quantities:

$$
\lambda=\frac{\mathrm{K}}{\mathrm{C}_{\mathrm{v}}}
$$

[4]

The flow of heat in the soil can be described by the following equation:

$$
\begin{equation*}
\frac{\partial T}{\partial t}=\lambda \frac{\partial^{2} T}{\partial Z^{2}}=\frac{K}{C_{V}} \frac{\partial^{2} T}{\partial Z^{2}} \tag{5}
\end{equation*}
$$

The thermal diffusivity of the soil is of great importance as it governs the soil temperature distribution at different depths. In soils with a low thermal diffusivity the daily and annual temperature amplitudes are smaller than in soils with higher thermal diffusivity.

## REVIEW OF LITERATURE

In the last 40 years numerous workers have studied the seasonal and diurnal variation of radiative properties on vegetative surfaces as part of field studies of environmental aspects of land use. Many relationships between air temperature and solar radiation with soil temperature have been reported and several techniques have been used to study these relationships. A series of case studies showing the temperature response of the soil in several typical weather situations have been prepared and analyzed to show quantitatively the temperature change in the soil as a result of a given change of the external meteorological conditions.

Wexler (1936), pointed out that the net outgoing radiation decreases as the ground cools and reaches zero at a certain critical difference between air and ground temperature. Groen (1947), showed that the soil surface temperature approaches its minimum value asymptotically as the net radiation decreases to a minimum. The boundary condition used by Groen requires that, as the minimum ground surface temperature is approached, the net outgoing radiation and the heat flux through the ground surface approach zero. This requires that the vertical temperature gradient at the ground surface also approaches zero; it follows, that the temperature can remain constant for only a shallow depth and a short period of time.

Fleagle (1949), shows that the lowest temperature a radiating surface may reach depends upon the thickness of the ground surface
layer which undergoes temperature change, the conductivity of the layer, and the presence of obstructions above the plane of the horizon.

Robinson (1950), found that the emission from short turf was close Lo black-body radiation at the minimum turf temperature. Roach's (1955), showed a seasonal variation in the difference between the mean surface temperature of turf and mean air temperature. Houghton (1958), inferred from radiometer measurements in aircraft that the effective radiative temperature of open country at night lay between the temperature of grass minimum and screen air temperature. Analysis of solar and net radiation records on clear days at Rothamsted showed that the diurnal variation of net long-wave exchange was closely related to changes in surface temperature, and that surface heating was proportional to net radiation (Montheith and Szeicz, 1961).

Monteith (1958), studied the diurnal variations of soil heat flux under grass, potatoes, and wheat. He reported that approximately $20 \%$ of the net incoming radiation was stored in the soil between 6 A.M. and 6 P.M. in the summer season under English conditions. The net radiation day was longer than the heat flux day. Meck (1969), reported that total solar radiation and resulting soil temperature had little correlation during a 5 day period in Canada.

Hanks, Austin and Ondrechen (1971), developed a computer model to predict the temperature fluctuation in the subsoil from the temperature variation at the soil surface, taking into account changes in the apparent thermal conductivity with depth below the soil surface and soil temperature. The suggested to solve the equation [5] with a numerical approximation as follows:
$\frac{T_{i, j}-T_{i, j-1}}{\Delta t}=\frac{\left(T_{i-1, j}-T_{i j}\right) \lambda_{i-\frac{1}{2}, j}-\left(T_{i, j}-T_{i+1, j}\right) \lambda_{i+\frac{1}{2}, j}}{\Delta z^{2}}$

They reported that computed and measured soil temperatures agreed within $1.0{ }^{\circ} \mathrm{C}$ when soil thermal diffusivity was assumed constant at $0.20 \mathrm{~cm}^{2} \mathrm{~min}^{-1}$ They also reported that where the thermal diffusivity was assumed uniform at . $45 \mathrm{~cm}^{2} \min ^{-1}$, temperature errors grew from $1.0-1.7^{\circ} \mathrm{C}$ after 3 days to $1.7-3.1{ }^{\circ} \mathrm{C}$ after 6 days.

Hanks and Jacobs (1971), indicated that in comparison of soil heat flow as estimated by the calorimetric, flux meter, and a combination of the two methods, the best method for measuring daily soil heat flow is the calorimetric method, in which soil temperature measurements are made to 64 cm for daily flux. They reported that the calorimetric method has the advantage of less critical assumptions than the flux meter for daily measurements with no accumulation of errors when integrated values over 1 day, or part of 1 day, are desired, and the combination method had the disadvantages of both methods.

Hanks, Bowers and Bark (1961), with the purpose to clarify the relationship of net radiation, soil temperature, and soil surface conditions on evaporation, reported that there was no direct relationship under the conditions of the experiment between net radiation or soil temperature and evaporation. This was probably due to the great limiting influence of soil moisture within the soil after the soil surface dries. Taylor (1928), working in Egypt, reported that no relationship between air and soil temperature could be traced. Many investigators, Antonova (1929), Hursh (1940), Brown (1943), and Reeder (1920), have reported the density of vegetative cover to have a significant effect on soil temperature. They have also found that the temperature of bare soil
in summer was higher than those of a grass cover. Hide (1942), reported that the surface soil has a much higher variability than either air or deep soil temperatures. Austin (1972), reported about $15{ }^{\circ} \mathrm{C}$ maxima difference between exposed and shaded points in the cold desert of Curlew Valley (U.S.A.). He found a strong correlation between hourly air temperature and soil temperature at 2 cm depth and between global radiation and soil temperature.

A computer model for the radiative heat exchange developed by Dirmhirn (unpublished) was written in a fortran program (appendix) and was used to determine the heat applied by radiation to the soil surface. In this model a thin soil layer was used as reference layer and as mass for the energy provided by the net radiation on clear days during the summer season. This method shows the heating of a surface layer by radiative processes when no other heat dissipation (exchange with the air or soil and evaporative processes) takes place.

## general description of experimental area

Curlew Valley is a drainage basin astride the Utah-Idaho border encompassing some 3,471 square kilometer. It is bordered by mountains ranging up to 2,743 meter above sea level on the east, north and west, and terminates at its southern end on the salt flats of Great Salt Lake and the lake itself.

The valley floor is a lacustrine basin sloping from about 1,280 meter altitude at the lake level to 1,585 meter in the north in a series of step-like levels. This altitudinal gradient correlates with rainfall, soil, and biotic gradients. Total, annual precipitation ranges from 15 cm to 20 cm at the southern end of the valley to $36-41 \mathrm{~cm}$ at the northern end. From south to north, soil salinity declines from the very high levels of the lake fringe while soil organic matter increases progressively. The correlated vegetation gradient is formed by pickleweed (Allenrolfia occidentalis) which occupies a virtual monotype on the salt flats; greasewood (Sarcobatus vermiculatus) at elevation still close to the water table; shadscale (Atriplex confertifolia) on soil of still substantial salinity; and big sage (Artemisia tridentata).

A study area was selected in the valley with a vegetation of natural stand of sagebrush and a micrometeorological station was set up on this site. In general, the climate of the big sagebrush zone can be classified as "cold desert" with an average annual rainfall from 20 to 41 cm with about three-fourths of this occurring between October and May. Big sage
is the principal primary producer species involved in the area under consideration. Big sage exhibits a season of observable growth between late March and early July varying between years with the available moisture and with the prevailing temperature regime. The dominant texture of the soil appears to be silt loam.

## INSTRUMENTATION AND PROCEDURE

## Instrumentation

Net radiation was measured with a net radiometer (Kahlisco) which was mounted on a stand about 1 meter in height above ground. Careful consideration was taken to ensure that the surface below the radiation balance meter was representative of a wide area of the surroundings. Incoming solar and scattered radiation were measured with a star pyranometer placed over a rigid stand of 1 meter height with a horizontal top surface. The site for the star pyranometer was free from any obstructions above the plane of the sensing element. Copper-constantan thermocouples, as described by Dike (1954), were constructed to measure air temperature, surface temperature and soil temperature. Measurements of air temperature were made in the air immediately above the surface by means of unshielded thermocouples, which were installed on a triangular television tower of about 8 meter height. The thermocouples for the temperature measurements in the air were built from thin, 0.005 cm diameter copper and constantan wire. The heat dissipation from these thermocouples under natural environment is large enough that no over-heating by radiative processes can occur. Thermocouples were placed on a triangular television tower at 5, 20, $50,100,200,400$, and 800 cm above the ground to measure air temperature. One more thermocouple was placed at 5 cm in the shade of a plant.

The surface temperature was measured by placing a surface thermojunction on the ground covered by a minute layer of dust. This surface junction was built from $0.1 \mathrm{~mm} \mathrm{cu} . / \mathrm{o} .12 \mathrm{~mm}$ constantan wire. A reference junction was placed at 125 cm depth.

Measurements of soil temperature were made at depths of $2,10,25$, 50 , and 125 cm . The thermocouple junctions were of 1 mm diameter gauge thermo wire. The thermocouple junctions were coated with an insulating paint to protect and insulate the junctions.

A Metrodata Magnetic Tape Recorder was employed as a recording system. This digital recorder is designed for receiving data in time intervals from 1 second to 1 hour. Intervals of 10 minutes were used throughout this study.

## Procedure

Short-wave solar and scattered radiation flux ( $R_{S}+R_{D}$ ), net radiation flux ( $\mathrm{R}_{\mathrm{N}}$ ), surface temperature, subsoil and air temperature data as observed in the field were analyzed for several clear days during the summer season. Short-wave reflected radiation data were determined from incoming solar and scattered by considering albedo to be 0.16 as reported by Dirmhirn (1972). The diurnal variation in the net longwave term ( $R_{A}-R_{E}$ ) was calculated by difference (residual method) from formula [2]. To determine the atmospheric radiation, the expression developed by Angstrom (Sellers, 1972) was used:

$$
\begin{equation*}
\mathrm{R}_{\mathrm{A}}=\varepsilon \sigma \mathrm{T}^{4}\left(\mathrm{a}-\mathrm{b} \cdot 10^{-\mathrm{ce}}\right) \tag{7}
\end{equation*}
$$

The values for the empirical constants ( $a, b$, and $c$ ) were taken from Geiger (Sellers, 1972). The surface emissivity was assumed to be 0.9. (Sellers, 1972). To obtain (e) the vapor pressure of air, published
data from Salt Lake City (National Weather Service FCST DFC, 1973) were used, referred to: air temperature, wet bulb temperature and atmospheric pressure, together with psychrometric data from Smithsonian Meteorological Tables (1968).

Surface temperature, atmospheric radiation and emitted radiation from the surface of the soil were predicted with the model for the radiative heat exchange, to determine the heat applied by radiation to the soil surface. In this model data of incoming solar radiation of several days during the months of June, July and August in Logan, Utah were used.

A simulated profile subsoil temperature was predicted using the computer model developed by Hanks, Austin and Ondrechen (1971). Predicted soil temperatures were compared with soil temperature observed in the field at $2,10,25$, and 50 cm depths below the surface of the soil.

The initial temperature as a function of the depth and the surface temperature as a function of time used in the model were obtained from the soil temperature record in the field. The apparent thermal diffusivity values [4] were obtained, also, from the soil temperature record in the field using phase and amplitude relations, Wierenga, Nielsen and Hogan (1969). The equations used to estimate the apparent thermal diffusivity from observed temperature variations at several soil depths were the amplitude equation:

$$
\begin{equation*}
\mathrm{D}=\frac{\mathrm{w}}{2} \frac{\left(\mathrm{Z}_{2}-\mathrm{Z}_{1}\right.}{\ln )_{1} / \mathrm{A}_{2}} \tag{8}
\end{equation*}
$$

and phase equation:

$$
\begin{equation*}
D=\frac{1}{2 w}\left(\frac{z_{2}-z_{1}}{\delta t}\right)^{2} \tag{9}
\end{equation*}
$$

Different thermal diffusivity values approximately to the calculated values were assumed and used in the model to compare with the calculated values. The diffusivity at low depths was assumed constant and equal to that of the layer $35-40 \mathrm{~cm}$ depth. Table 1 shows the thermal diffusivity values as calculated from [8] and [9] used for determining the simulated subsoil temperature; bulk densities in this area as reported by Austin (1972) ranged from 1.1 to 1.5 with the mode at $1.2 \mathrm{~g} / \mathrm{cm}^{3}$. The value of (c) was arrived at from data in literature cited by Hanks and Jacobs (1971). They listed the value of (c) for most mineral soil to be from 0.18 to $0.22 \mathrm{Cal} \mathrm{g}{ }^{-1}{ }^{\circ} \mathrm{C}^{-1}$. Thus, we chose 1.2 and 0.2 as bulk density and specific heat respectively as a good average to the complete profile. The thermal conductivity was calculated from the above values.

The change in heat content (heat flux when divided by the time interval) was calculated from:

$$
\Delta H C=\sum_{i=1}^{n} \quad\left(c \rho_{b_{i}}+\theta_{i}\right) \Delta T_{i} \cdot \Delta z_{i}
$$

assuming the volumetric heat capacity of soil $\left(C_{v}=c \rho_{b_{i}}+\theta_{i}\right)$ is known. Furthermore, a profile subsoil temperature of actual data and of simulated data from models was used. Both results were then compared.

Table 2 shows the values of atmospheric radiation for several clear days as calculated by Angstrom's equation, that were used in the radiation model. Table 3, shows the hourly global radiation as observed on some clear days used, also, in the radiation model.

Table 1. Thermal parameters used for determining the simulated subsoil temperature.

| Depth | $\begin{aligned} & \text { bulk } \\ & \text { density } \end{aligned}$ | specific heat | thermal diffusivity | thermal conductivity |
| :---: | :---: | :---: | :---: | :---: |
| 2 | $\rho \mathrm{b}$ | c | $\lambda$ | K |
| cm | $\mathrm{g} / \mathrm{cm}^{3}$ | cal/g ${ }^{\circ} \mathrm{C}$ | $\mathrm{cm}^{2} / \mathrm{min}$ | $\mathrm{cal} / \mathrm{cm} \min { }^{\circ} \mathrm{C}$ |
| 0-5 | 1.2 | 0.2 | 0.13 | 0.032 |
| 5-10 | 1.2 | 0.2 | 0.23 | 0.056 |
| 10-15 | 1.2 | 0.2 | 0.31 | 0.073 |
| 15-20 | 1.2 | 0.2 | 0.35 | 0.085 |
| 20-25 | 1.2 | 0.2 | 0.36 | 0.086 |
| 2.5-30 | 1.2 | 0.2 | 0.37 | 0.088 |
| 30-35 | 1.2 | 0.2 | 0.39 | 0.093 |
| 35-40 | 1.2 | 0.2 | 0.40 | 0.095 |
| 40-45 | 1.2 | 0.2 | 0.40 | 0.095 |
| 45-50 | 1.2 | 0.2 | 0.40 | 0.095 |

Table 2. Calculated atmospheric radiation (incoming radiation from the atmosphere in $1 \mathrm{y} / \mathrm{min}$.) from 12 clear days during summer season, 1973.

| Hours | Jun 5 | Jun 9 | Jun12 | Jun20 | Jun25 | Ju1 1 | Jul 5 | Ju125 | Aug 1 | Aug10 | Aug15 | Aug30 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | 0.40 | 0.46 | 0.47 | 0.39 | 0.47 | 0.51 | 0.50 | 0.48 | 0.50 | 0.51 | 0.46 | 0.45 |  |
| 2 | 0.39 | 0.46 | 0.46 | 0.38 | 0.46 | 0.49 | 0.47 | 0.46 | 0.48 | 0.50 | 0.46 | 0.43 |  |
| 3. | 0.38 | 0.46 | 0.46 | 0.37 | 0.45 | 0.47 | 0.45 | 0.44 | 0.46 | 0.50 | 0.45 | 0.43 |  |
| 4 | 0.38 | 0.46 | 0.45 | 0.36 | 0.45 | 0.45 | 0.44 | 0.44 | 0.45 | 0.50 | 0.45 | 0.42 |  |
| 5 | 0.38 | 0.47 | 0.46 | 0.37 | 0.45 | 0.44 | 0.45 | 0.44 | 0.45 | 0.50 | 0.45 | 0.43 |  |
| 6 | 0.40 | 0.49 | 0.47 | 0.39 | 0.47 | 0.45 | 0.47 | 0.46 | 0.47 | 0.51 | 0.47 | 0.45 |  |
| 7 | 0.42 | 0.50 | 0.48 | 0.41 | 0.49 | 0.46 | 0.49 | 0.47 | 0.49 | 0.52 | 0.49 | 0.47 |  |
| 8 | 0.44 | 0.52 | 0.49 | 0.42 | 0.50 | 0.47 | 0.51 | 0.49 | 0.51 | 0.53 | 0.50 | 0.49 |  |
| 9 | 0.44 | 0.53 | 0.51 | 0.44 | 0.52 | 0.47 | 0.53 | 0.50 | 0.52 | 0.55 | 0.51 | 0.49 |  |
| 10 | 0.44 | 0.54 | 0.52 | 0.46 | 0.53 | 0.48 | 0.55 | 0.52 | 0.54 | 0.56 | 0.52 | 0.50 |  |
| 11 | 0.44 | 0.55 | 0.52 | 0.48 | 0.54 | 0.48 | 0.56 | 0.53 | 0.55 | 0.57 | 0.53 | 0.51 |  |
| 12 | 0.46 | 0.56 | 0.52 | 0.49 | 0.55 | 0.48 | 0.57 | 0.54 | 0.56 | 0.57 | 0.55 | 0.53 |  |
| 13 | 0.47 | 0.61 | 0.52 | 0.50 | 0.55 | 0.49 | 0.57 | 0.54 | 0.56 | 0.57 | 0.56 | 0.55 |  |
| 14 | 0.48 | 0.61 | 0.52 | 0.51 | 0.55 | 0.49 | 0.57 | 0.55 | 0.57 | 0.58 | 0.57 | 0.55 |  |
| 15 | 0.48 | 0.55 | 0.52 | 0.51 | 0.56 | 0.48 | 0.59 | 0.55 | 0.56 | 0.58 | 0.56 | 0.54 |  |
| 16 | 0.48 | 0.55 | 0.51 | 0.51 | 0.56 | 0.48 | 0.59 | 0.55 | 0.56 | 0.57 | 0.56 | 0.52 |  |
| 17 | 0.48 | 0.55 | 0.51 | 0.51 | 0.55 | 0.48 | 0.59 | 0.55 | 0.55 | 0.56 | 0.55 | 0.50 |  |
| 18 | 0.48 | 0.55 | 0.50 | 0.50 | 0.55 | 0.49 | 0.57 | 0.55 | 0.53 | 0.55 | 0.55 | 0.50 |  |
| 19 | 0.46 | 0.54 | 0.50 | 0.49 | 0.54 | 0.49 | 0.55 | 0.52 | 0.52 | 0.54 | 0.55 | 0.49 |  |
| 20 | 0.46 | 0.53 | 0.49 | 0.48 | 0.53 | 0.48 | 0.53 | 0.50 | 0.50 | 0.52 | 0.54 | 0.48 |  |
| 21 | 0.45 | 0.52 | 0.48 | 0.48 | 0.52 | 0.48 | 0.52 | 0.49 | 0.49 | 0.51 | 0.53 | 0.48 |  |
| 22 | 0.44 | 0.51 | 0.48 | 0.47 | 0.51 | 0.47 | 0.51 | 0.49 | 0.48 | 0.51 | 0.51 | 0.47 |  |
| 23 | 0.44 | 0.50 | 0.48 | 0.47 | 0.50 | 0.46 | 0.50 | 0.48 | 0.47 | 0.50 | 0.50 | 0.47 |  |
| 24 | 0.43 | 0.49 | 0.47 | 0.46 | 0.49 | 0.45 | 0.50 | 0.48 | 0.47 | 0.50 | 0.48 | 0.46 |  |

Table 3. Observed global radiation (incoming solar and scattered radiation in $1 y / m i n$.) from 12 clear days during summer season, 1973.

| Hours | Jun 5 | Jun 9 | Jun12 | Jun20 | Jun25 | Jul 1 | Jul 5 | Ju125 | Aug 1 | Aug10 | Aug15 | Aug 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 0.10 | 0.00 | 0.10 | 0.10 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6 | 0.20 | 0.10 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | 0.10 | 0.10 | 0.10 | 0.10 | 0.00 |
| 7 | 0.50 | 0.30 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 | 0.40 | 0.40 | 0.30 | 0.30 | 0.20 |
| 8 | 0.80 | 0.60 | 0.80 | 0.80 | 0.80 | 0.70 | 0.70 | 0.70 | 0.70 | 0.60 | 0.60 | 0.50 |
| 9 | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.90 | 0.90 | 0.90 | 0.90 | 0.80 |
| 10 | 1.20 | 1.10 | 1.20 | 1.20 | 1.20 | 1.20 | 1.20 | 1.10 | 1.10 | 1.10 | 1.10 | 1.00 |
| 11 | 1.40 1.40 | 1.30 | 1.40 | 1.40 | 1.30 | 1.40 | 1. 30 | 1.30 | 1.30 | 1.20 | 1.20 | 1.20 |
| 13 | 1.40 1.40 | 1.40 1.40 | 1.40 1.40 | 1.40 | 1.40 | 1.40 | 1.40 | 1. 30 | 1.30 | 1.30 | 1.30 | 1.30 |
| 14 | 1.40 1.30 | 1.40 1.40 | 1.40 1.30 | 1.40 1.30 | 1.40 | 1.40 | 1.40 | 1.30 | 1. 30 | 1.20 | 1.30 | 1.30 |
| 15 | 1.20 | 1.40 1.20 | 1.30 1.20 | 1.30 1.20 | 1.30 | 1.40 | 1.30 | 1.30 | 1.30 | 1.10 | 1.20 | 1.20 |
| 16 | 1.00 | 1.00 | 1.20 1.00 | 1.20 1.00 | 1.10 0.90 | 1.20 1.00 | 1.20 1.00 | 1.10 0.90 | 1.10 | 0.80 | 1.00 | 1.00 |
| 17 | 0.70 | 0.80 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.60 | 0.30 | 0.60 | 0.60 |
| 18 | 0.40 | 0.60 | 0.40 | 0.50 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.10 | 0.30 | 0.30 |
| 19 | 0.20 | 0.30 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | 0.10 | 0.00 | 0.10 | 0.10 |
| 20 | 0.00 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 21 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

## RESULTS AND DISCUSSION

The radiation balance (actual data)
The diurnal variation in radiation components on three clear days is shown in Figures 1, 2, and 3 where short-wave solar and scattered radiation flux ( $R_{S}+R_{D}$ ), net radiation flux $\left(R_{N}\right)$ and albedo are all measured quantities in the field.

These three figures show that for each situation there was a noteworthy daily cycle. Net radiation was greater in the period of midday and morning than in the afternoon. These results agree with those of Monteith and Szeicz (1961), where net radiation was always smailer in the afternoon than in the morning. They attributed the difference to higher afternoon surface temperature, along with an almost constant long-wave emission from the atmosphere.

In the figures is noted that in the early morning and late afternoon, net radiation was usually slightly negative; this was because the emitted radiation from the surface is greater than the atmospheric radiation.

At midday and early afternoon, the heat loss by long-wave exchange ( $R_{A}-R_{E}$ ) was (on July 9 and August 1) three times its nocturnal value, and twice the loss by short-wave reflection. A similar variation of the net long wave term was reported by Monteith and Szeicz (1961).

The mean long-wave loss on clear days increased from $0.10 \mathrm{cal} . \mathrm{cm}^{-2}$ $\min ^{-1}$ before dawn to $0.29 \mathrm{cal} . \mathrm{cm}^{-2} \min ^{-1}$ at midday when maximum solar radiation was $1.39 \mathrm{cal} . \mathrm{cm}^{-2} \min ^{-1}$ (on July 7 and July 9) and 1.34 cal. $\mathrm{cm}^{-2} \min ^{-1}$ (on August 1).

Table 4, shows the diurnal variation in long-wave radiation $\left(R_{E}\right.$ and $\left.R_{A}\right)$ as calculated from observed data. The emitted radiation, ( $R_{E}$ ), varied from $0.46 \mathrm{cal} . \mathrm{cm}^{-2} \min ^{-1}$ before sunrise to $1.03 \mathrm{cal} . \mathrm{cm}^{-2} \mathrm{~min}^{-1}$ at midday (on July 7 and 9) and from 0.45 cal. $\mathrm{cm}^{-2} \min ^{-1}$ to 0.92 cal. $\mathrm{cm}^{-2} \mathrm{~min}^{-1}$ (on August 1).

In those days shown, the maximum atmospheric radiation ( $R_{A}$ ) reached $0.75 \mathrm{cal}_{\mathrm{cal}} \mathrm{cm}^{-2} \min ^{-1}$ in early afternoon and the minimum was 0.33 cal . $\mathrm{cm}^{-2} \min ^{-1}$ before dawn when the emitted radiation was approximately $0.46 \mathrm{cal} . \mathrm{cm}^{-2} \min ^{-1}$ and $1.02 \mathrm{cal} . \mathrm{cm}^{-2} \min ^{-1}$ respectively.

Table 4. Emitted and atmospheric radiation (in 1y/min) on July 7 and 9, calculated from observed data.

| Hours | July 7 |  | July 9 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{R}_{\mathrm{E}}$ | $\mathrm{R}_{\text {A }}$ | $\mathrm{R}_{\mathrm{E}}$ | $\mathrm{R}_{\mathrm{A}}$ |
| 1 | 0.500 | 0.366 | 0.469 | 0.372 |
| 2 | 0.483 | 0.362 | 0.465 | 0.371 |
| 3 | 0.481 | 0.362 | 0.461 | 0.369 |
| 4 | 0.466 | 0.339 | 0.460 | 0.372 |
| 5 | 0.458 | 0.329 | 0.478 | 0.383 |
| 6 | 0.466 | 0.329 | 0.549 | 0.453 |
| 7 | 0.527 | 0.407 | 0.659 | 0.529 |
| 8 | 0.627 | 0.447 | 0.778 | 0.608 |
| 9 | 0.730 | 0.510 | 0.853 | 0.653 |
| 10 | 0.820 | 0.570 | 0.925 | 0.692 |
| 11 | 0.925 | 0.660 | 1.005 | 0.720 |
| 12 | 1.008 | 0.728 | 1.025 | 0.713 |
| 13 | 1.002 | 0.732 | 1.008 | 0.715 |
| 14 | 0.976 | 0.746 | 0.939 | 0.687 |
| 15 | 0.942 | 0.732 | 0.868 | 0.658 |
| 16 | 0.858 | 0.678 | 0.775 | 0.615 |
| 17 | 0.789 | 0.639 | 0.672 | 0.552 |
| 18 | 0.683 | 0.563 | 0.609 | 0.519 |
| 19 | 0.615 | 0.485 | 0.544 | 0.468 |
| 20 | 0.562 | 0.442 | 0.525 | 0.411 |
| 21 | 0.534 | 0.414 | 0.516 | 0.413 |
| 22 | 0.518 | 0.408 |  |  |

Compared with the calculated values presented in Table 2 , these data derived from observations, are slightly higher ( $0.121 \mathrm{y} / \mathrm{min}$ at maximum). This inconsistency seems to be due to a change in calabration of the net radiometer in the long-wave range, particularly since the maximum of the $R_{A}$ is also shifted somewhat to the earlier hours. Further observations are underway with this particular instrument.

Soil temperature profile (actual data)
The soil temperature as a function of time is presented in Figures 4, 5 and 6 (these data are in Tables 19,20 and 21 in Appendix C). The maximum soil temperatures at the surface were found to occur at 1300 , 1400 and 1500 hours in each of the cited days. The maximum soil temperatures at 2 cm depth were reached 1500,1700 and 1600 hours respectively; thus the time 1 ag at 2 cm depth was $2 \frac{1}{2}$ hours on July 7 and 1 hour on July 9 and August 1.

The amplitude of the diurnal wave at 2 cm depth was approximately $58 \%$ of that of the surface. At 10 cm depth it was $18 \%$ on July 7 and July 9 and $25 \%$ on August 1. At 25 cm depth the wave amplitude was $4 \%$ that of the surface on July 7 and July 9.

The maximum temperatures reached at the surface were $69.5{ }^{\circ} \mathrm{C}$, $71{ }^{\circ} \mathrm{C}$ and $62.5{ }^{\circ} \mathrm{C}$ on July 7, July 9 and August 1 respectively. At 2 cm depth the maximum temperatures were $49.25{ }^{\circ} \mathrm{C}, 51{ }^{\circ} \mathrm{C}$ and $44.75{ }^{\circ} \mathrm{C}$ in the same order of days as above. At 10 cm depth the maximum temperatures were $31{ }^{\circ} \mathrm{C}$ and $32.25{ }^{\circ} \mathrm{C}$. Soil temperature at this depth approached air temperature between 2 meter and 8 meter. At 2 cm depth the temperature of the soil was warmer than the air.


Figure 1. Observed variation of global radiation $\left(R_{S}+R_{D}\right)$, net radiation $\left(R_{N}\right)$, albedo $\left(R_{S}+R_{D}\right) \alpha$
and net long-wave radiation $\left(R_{A}-R_{E}\right)$ on July 7.


Figure 2. Observed variation of global radiation $\left(R_{S}+R_{D}\right)$, net radiation $\left(R_{N}\right)$, albedo $\left(R_{S}+R_{D}\right) \alpha$
and net long-wave radiation $\left(R_{A}-R_{E}\right)$ on July 9 .


Figure 3. Observed variation of global radiation ( $R_{S}+R_{D}$ ), net radiation ( $R_{N}$ ), albedo ( $\mathrm{R}_{\mathrm{S}}+\mathrm{R}_{\mathrm{D}}$ ) $\alpha$ and net long wave radiation $\left(R_{A}-R_{E}\right)$ on August 1 .

The data of Figures 4,5 and 6 show that before dawn the variations of temperature were small (about $1{ }^{\circ} \mathrm{C}$ or $2^{\circ} \mathrm{C}$ ) and the minimum temperature was reached before the sunrise. With the beginning of solar radiation, surface temperature began to rise very slowly at first and more rapidly after 0700 A.M. The temperature gradually increased as time advanced until solar noon when the surface temperature began to decrease. Between 1300 and 1500 hours, soil surface temperature changed and thereafter dropped off rapidly in late afternoon.

After solar noon, the rate of temperature decrease was low (about $3{ }^{\circ} \mathrm{C} \mathrm{hr}{ }^{-1}$ ) and increases gradually to about $6^{\circ} \mathrm{C} /$ hour. A maximum of about $11{ }^{\circ} \mathrm{C} /$ hour was reached between 1800 and 1900 hours. After this period, the rate was again low as temperatures began to decline more slowly.

It was also found that soil temperature at 25 cm depth had daily variations of $2{ }^{\circ} \mathrm{C}$ to $3{ }^{\circ} \mathrm{C}$. At 50 cm depth, almost no variations occured. At 125 cm depth, the temperature was constant throughout the day.

## Simulated subsoil temperature

To simulate the conditions of subsoil temperature, the apparent thermal diffusivity of soil was determined using the soil temperature records and plotting the diurnal cycle of each. Using the phase and amplitude relations, it was possible to get estimates of the variations of thermal diffusivity with depth. Diffusivity values obtained with the phase equation gave better results than those calculated with the amplitude equation. In simulated situation, it was assumed that the diffusivity values calculated at various depth did not vary with time.


Figure 4. Observed soil temperature variation at $0,2,10,25$, and 50 cm depth on July 7 .


Figure 5. Observed soil temperature variation at $0,2,10,25$, and 50 cm depth on July 9 .


Figure 6. Observed soil temperature variation at $0,2,10$, and 50 cm depth on August 1 .


Figure 7. Observed and simulated soil temperature variation. The solid lines are the observed soil temperatures. The dots represent the computed soil temperatures on July 7.


Figure 8. Observed and simulated soil temperature variation, on July 9. The solid lines are the observed soil temperatures. The dots represent the computed soil temperatures.

Figures 7 and 8 show a comparison of two days (July 7 and July 9)
between temperatures recorded in the field and temperatures simulated by the computer model. A close agreement was found between the measured values and computed values.

Since the soil temperature recorded in the field were as 0,2 , $10,25,50$, and 150 cm depth and the predicted temperatures were taken at layers of 5 cm each $(5,10,15,20,25,30,35,40,45$, and 50 cm depth), it was only possible to campare exactly the temperatures at 10,25 , and 50 cm depth. At 10 cm depth, soil temperature observed and predicted were in close agreement. This agreement was even better at 25 cm depth and particularly at 50 cm since nothing changed there. Calculated long-wave radiation $\left(R_{F}\right)$ (with radiation model). Table 5 shows a comparison between several clear days of emitted radiation from the surface of soil as obtained by the radiation model. The calculated radiation varied from $0.441 \mathrm{y} / \mathrm{min}$ (average value) at early hours in the morning to $1.66 \mathrm{ly} / \mathrm{min}$ (average value) at midday. In the morning there is no notable difference between calculated from observed data in the field and calculated with the radiation model, but at midday the differences were $0.631 \mathrm{y} / \mathrm{min}$. This is due to the suppression of all other heat change components except radiative transfer. The infinitesimal soil surface layer theoretically then heats up by far more than under natural conditions until radiative equilibrium is reached, thus resulting in these high values of $R_{E}$. Calculated surface temperature (with radiation model). Table 6 shows the hourly simulated temperature of the surface on several clear days as determined by the radiation model. The high temperature obtained at the surface of the soil represent the temperature of the

Table 5. Calculated long-wave radiation, $\mathrm{R}_{\mathrm{E}}$ by radiation model (emitted radiation from the surface in $1 \mathrm{y} / \mathrm{min}$. ) from 12 clear days during the summer season, 1973.

| Hours | Jun 5 | Jun 9 | Junl2 | Jun20 | Jun2.5 | Jul 1 | Jul 5 | Ju125 | Aug 1 | Aug10 | Aug15 | Aug 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.40 | 0.46 | 0.47 | 0.39 | 0.47 | 0.51 | 0.50 | 0.48 | 0.50 | 0.51 | 0.46 | 0.45 |
| 2 | 0.39 | 0.46 | 0.46 | 0.48 | 0.46 | 0.49 | 0.47 | 0.46 | 0.48 | 0.50 | 0.46 | 0.43 |
| 3 | 0.38 | 0.46 | 0.46 | 0.37 | 0.45 | 0.47 | 0.45 | 0.44 | 0.46 | 0.50 | 0.45 | 0.43 |
| 4 | 0.42 | 0.47 | 0.50 | 0.41 | 0.49 | 0.48 | 0.47 | 0.44 | 0.46 | 0.50 | 0.45 | 0.42 |
| 5 | 0.58 | 0.53 | 0.65 | 0.57 | 0.64 | 0.61 | 0.61 | 0.56 | 0.56 | 0.58 | 0.53 | 0.47 |
| 6 | 0.83 | 0.74 | 0.88 | 0.82 | 0.88 | 0.84 | 0.86 | 0.80 | 0.80 | 0.79 | 0.75 | 0.64 |
| 7 | 1.08 | 1.02 | 1.12 | 1.06 | 1.12 | 1.08 | 1.11 | 1.05 | 1.05 | 1.03 | 1.00 | 0.90 |
| 8 | 1.30 | 1.26 | 1.34 | 1.28 | 1.34 | 1.30 | 1.34 | 1.20 | 1.27 | 1.25 | 1.24 | 1.14 |
| 9 | 1.47 | 1.45 | 1.52 | 1.47 | 1.51 | 1.50 | 1.53 | 1.46 | 1.46 | 1.45 | 1.43 | 1.34 |
| 10 | 1.59 | 1.60 | 1.65 | 1.60 | 1.64 | 1.63 | 1.66 | 1.59 | 1.59 | 1.58 | 1.56 | 1.48 |
| 11 | 1.64 | 1.71 | 1.71 | 1.67 | 1.70 | 1.68 | 1.72 | 1.66 | 1.66 | 1.65 | 1.63 | 1.56 |
| 12 | 1.65 | 1.74 | 1.71 | 1.69 | 1.70 | 1.68 | 1.72 | 1.66 | 1.67 | 1.58 | 1.63 | 1.60 |
| 13 | 1.59 | 1.70 | 1.64 | 1.63 | 1.64 | 1.62 | 1.67 | 1.60 | 1.62 | 1.46 | 1.56 | 1.55 |
| 14 | 1.46 | 1.60 | 1.51 | 1.50 | 1.52 | 1.49 | 1.56 | 1.48 | 1.59 | 1.28 | 1.44 | 1.42 |
| 15 | 1.28 | 1.43 | 1.33 | 1.33 | 1.34 | 1.30 | 1.39 | 1.31 | 1.32 | 1.06 | 1.26 | 1.22 |
| 16 | 1.07 | 1.23 | 1.11 | 1.12 | 1.14 | 1.09 | 1.19 | 1.10 | 1.09 | 0.83 | 1.04 | 0.98 |
| 17 | 0.83 | 1.02 | 0.88 | 0.89 | 0.92 | 0.86 | 0.95 | 0.87 | 0.84 | 0.63 | 0.80 | 0.74 |
| 18 | 0.61 | 0.79 | 0.65 | 0.66 | 0.70 | 0.64 | 0.72 | 0.65 | 0.62 | 0.55 | 0.61 | 0.55 |
| 19 | 0.48 | 0.60 | 0.52 | 0.52 | 0.56 | 0.51 | 0.57 | 0.64 | 0.56 | 0.54 | 0.55 | 0.49 |
| 20 | 0.46 | 0.53 | 0.49 | 0.48 | 0.53 | 0.48 | 0.53 | 0.50 | 0.50 | 0.52 | 0.54 | 0.48 |
| 21 | 0.45 | 0.52 | 0.48 | 0.48 | 0.52 | 0.48 | 0.52 | 0.49 | 0.49 | 0.51 | 0.53 | 0.48 |
| 22 | 0.44 | 0.51 | 0.48 | 0.47 | 0.51 | 0.47 | 0.51 | 0.49 | 0.48 | 0.51 | 0.51 | 0.47 |
| 23 | 0.44 | 0.50 | 0.48 | 0.47 | 0.50 | 0.46 | 0.50 | 0.48 | 0.47 | 0.50 | 0.50 | 0.47 |
| 24 | 0.43 | 0.49 | 0.47 | 0.46 | 0.49 | 0.45 | 0.50 | 0.48 | 0.47 | 0.50 | 0.48 | 0.46 |

Table 6. Calculated surface temperature $\left(i n^{\circ} \mathrm{C}\right)$ obtained from radiation model for 12 clear days in summer season, 1973.

| Hours | Jun5 | Jun 9 | Jun 12 | Jun20 | Jun25 | Ju1 1 | Ju1 5 | Jul25 | Aug 1 | Aug10 | Aug15 | Aug 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | -0.61 | 10.67 | 8.13 | -2.38 | 9.98 | 16.52 | 14.67 | 11.00 | 14.67 | 16.02 | 9.21 | 6.70 |
| 2 | -3.46 | 8.92 | 7.92 | -5.40 | 7.91 | 12.63 | 10.28 | 8.00 | 10.79 | 14.80 | 7.74 | 4.44 |
| 3 | -5.08 | 7.85 | 8.20 | -7.16 | 6.74 | 9.48 | 7.43 | 5.00 | 8.22 | 14.10 | 6.78 | 3.13 |
| 4 | 1.70 | 13.76 | 10.25 | -0.29 | 12.81 | 11.62 | 10.60 | 6.00 | 8.06 | 13.93 | 6.57 | 2.87 |
| 5 | 24.92 | 33.77 | 18.71 | 23.87 | 33.23 | 28.65 | 29.54 | 22.00 | 22.71 | 25.14 | 18.93 | 9.61 |
| 6 | 53.38 | 58.50 | 44.54 | 52.18 | 58.46 | 54.53 | 56.51 | 50.00 | 50.30 | 48.74 | 44.92 | 33.01 |
| 7 | 75.22 | 78.94 | 71.32 | 74.22 | 78.90 | 75.66 | 78.03 | 72.00 | 72.74 | 70.98 | 69.09 | 59.71 |
| 8 | 91.84 | 94.86 | 89.04 | 90.67 | 94.51 | 92.27 | 94.66 | 90.00 | 90.16 | 88.48 | 87.68 | 80.21 |
| 9 | 103.53 | 106.39 | 102.27 | 103.34 | 106.04 | 105.48 | 106.96 | 102.00 | 102.59 | 102.02 | 100.67 | 94.53 |
| 10 | 110.66 | 114.34 | 111.62 | 111.72 | 113.74 | 113.20 | 114.80 | 111.00 | 110.86 | 110.47 | 109.04 | 104.08 |
| 11 | 113.88 | 118.11 | 117.59 | 115.84 | 117.52 | 116.35 | 118.47 | 114.00 | 115.23 | 114.30 | 112.95 | 109.09 |
| 12 | 114.63 | 117.69 | 119.52 | 116.49 | 117.39 | 116.22 | 118.32 | 115.00 | 115.85 | 110.25 | 113.15 | 111.16 |
| 13 | 111.12 | 113.78 | 117.35 | 112.94 | 113.74 | 112.60 | 115.61 | 111.00 | 112.53 | 102.51 | 109.25 | 108.25 |
| 14 | 103.00 | 105.78 | 111.27 | 105.39 | 106.26 | 104.36 | 108.80 | 104.00 | 105.48 | 90.33 | 101.42 | 100.33 |
| 15 | 90.75 | 93.97 | 100.85 | 93.76 | 94.90 | 92.18 | 98.47 | 92.00 | 93.71 | 74.06 | 89.16 | 85.92 |
| 16 | 74.49 | 78.16 | 87.14 | 78.47 | 80.23 | 76.05 | 83.92 | 77.00 | 76.42 | 52.96 | 72.30 | 67.24 |
| 17 | 53.67 | 57.91 | 70.34 | 58.85 | 61.29 | 55.79 | 64.79 | 57.00 | 54.53 | 32.07 | 50.38 | 46.51 |
| 18 | 28.59 | 34.46 | 49.27 | 34.57 | 39.37 | 32.89 | 41.50 | 33.00 | 30.77 | 21.27 | 29.54 | 21.59 |
| 19 | 11.52 | 17.57 | 28.29 | 16.89 | 23.12 | 16.01 | 24.08 | 33.00 | 22.40 | 19.44 | 20.74 | 12.95 |
| 20 | 7.92 | 13.07 | 18.00 | 12.09 | 18.54 | 11.92 | 18.46 | 14.00 | 14.74 | 17.80 | 19.66 | 11.81 |
| 21 | 6.98 | 12.19 | 16.85 | 11.00 | 17.23 | 11.07 | 16.65 | 13.00 | 13.05 | 16.44 | 18.23 | 10.82 |
| 22 | 6.11 | 11.41 | 15.41 | 10.06 | 15.83 | 9.86 | 15.39 | 12.00 | 11.58 | 15.41 | 16.44 | 10.06 |
| 23 | 5.25 | 10.77 | 14.03 | 9.30 | 14.33 | 8.29 | 14.72 | 11.00 | 10.33 | 14.74 | 14.80 | 9.43 |
| 24 | 4.34 | 10.28 | 12.34 | 8.69 | 12.75 | 6.36 | 14.66 | 11.00 | 9.27 | 14.44 | 11.81 | 8.71 |

soil if no dissipation of heat occurs horizontal and vertical in the layers adjacent to the thin layer of the surface.

A comparison of the minimum temperatures of the surface as observed in the field on July 7 and July 9 with these calculated by the radiation model on July 5, shows good agreement. However, the maximum calculated values obtained at midday and early in afternoon are approximately $48{ }^{\circ} \mathrm{C}$ higher than the measured values.

Simulated subsoil temperature using calculated surface temperature
obtained with radiation model. A simulated profile of soil temperature was determined with the radiation model. From Tables 7, 8, and 9 it can be seen that high differences of temperature result between these calculated values and the actual temperatures that occur in the top layers. These differences gradually decrease with depth and at 50 cm depth no difference is found. Thus, the heat formed at the surface does not reach that depth ( 50 cm ) and probably did not even reach levels some centimeters above this depth.

At 25 cm depth, the difference in the maximum temperature between observed and calculated for simulation was $5.5{ }^{\circ} \mathrm{C}$ (on July 7), $5.7{ }^{\circ} \mathrm{C}$ (on July 9), and $3.5{ }^{\circ} \mathrm{C}$ (on August 1) and occurred in the evening. The difference of minimum values were $1.0{ }^{\circ} \mathrm{C}$ (on July 7), $1.7{ }^{\circ} \mathrm{C}$ (on July 9), and $0.7^{\circ} \mathrm{C}$ (on August 1) and occurred in the morning.

At 10 cm depth, the difference of maximum values was $13.2{ }^{\circ} \mathrm{C}$ (on July 7), $13.5{ }^{\circ} \mathrm{C}$ (on July 9), and $12.0^{\circ} \mathrm{C}$ (on August 1). The difference of minimum values was $2.7{ }^{\circ} \mathrm{C}, 3.8{ }^{\circ} \mathrm{C}$, and $3.5^{\circ} \mathrm{C}$ respectively.

At the surface, the differences of the maximum temperature were $49.0{ }^{\circ} \mathrm{C}$ (on July 7), $51.3{ }^{\circ} \mathrm{C}$ (on July 9), and $53.3{ }^{\circ} \mathrm{C}$ (on August 1). The minimum difference was $0.9{ }^{\circ} \mathrm{C}, 1.1{ }^{\circ} \mathrm{C}$, and $0.9{ }^{\circ} \mathrm{C}$ respectively.

Table 7. Hourly subsoil profile temperature determined from hourly surface temperature (from radiation model) on July 7.

| Hours | surface | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 cm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 14.7 | 24.4 | 25.8 | 25.8 | 25.2 | 24.3 | 23.3 | 22.2 | 21.1 | 20.1 | 19.0 |
| 2 | 10.3 | 23.2 | 25.1 | 25.3 | 24.9 | 24.1 | 23.2 | 22.2 | 21.1 | 20.1 | 19.0 |
| 3 | 7.4 | 21.9 | 24.3 | 24.8 | 24.6 | 23.9 | 23.1 | 22.1 | 21.1 | 20.1 | 19.0 |
| 4 | 10.6 | 21.4 | 23.6 | 24.3 | 24.2 | 23.7 | 22.9 | 22.0 | 21.1 | 20.0 | 19.0 |
| 5 | 29.5 | 23.1 | 23.4 | 23.9 | 23.9 | 23.5 | 22.8 | 21.9 | 21.0 | 20.0 | 19.0 |
| 6 | 56.1 | 27.1 | 24.1 | 23.7 | 23.6 | 23.2 | 22.6 | 21.8 | 20.9 | 20.0 | 19.0 |
| 7 | 78.0 | 32.2 | 25.7 | 24.1 | 23.5 | 23.0 | 22.4 | 21.7 | 20.9 | 20.0 | 19.0 |
| 8 | 94.6 | 37.5 | 28.0 | 24.9 | 23.7 | 23.0 | 22.3 | 21.6 | 20.8 | 19.9 | 19.0 |
| 9 | 106.9 | 42.5 | 30.7 | 26.1 | 24.2 | 23.1 | 22.3 | 21.5 | 20.7 | 19.9 | 19.0 |
| 10 | 114.8 | 47.0 | 33.4 | 27.6 | 25.0 | 23.4 | 22.4 | 21.5 | 20.7 | 19.9 | 19.0 |
| 11 | 118.5 | 50.8 | 36.1 | 29.2 | 25.9 | 23.9 | 22.6 | 21.6 | 20.7 | 19.8 | 19.0 |
| 12 | 118.3 | 53.7 | 38.6 | 30.9 | 27.0 | 24.5 | 22.9 | 21.7 | 20.7 | 19.9 | 19.0 |
| 13 | 115.6 | 55.7 | 40.7 | 32.5 | 28.1 | 25.2 | 23.3 | 21.9 | 20.8 | 19.9 | 19.0 |
| 14 | 108.8 | 56.7 | 42.4 | 34.0 | 29.3 | 26.0 | 23.8 | 22.2 | 21.0 | 20.0 | 19.0 |
| 15 | 98.5 | 56.5 | 43.6 | 35.3 | 30.4 | 26.9 | 24.3 | 22.5 | 21.2 | 20.0 | 19.0 |
| 16 | 83.9 | 55.1 | 44.2 | 36.3 | 31.4 | 27.7 | 24.9 | 22.9 | 21.4 | 20.1 | 19.0 |
| 17 | 64.8 | 52.2 | 44.0 | 37.0 | 32,2 | 28.4 | 25.5 | 23.3 | 21.6 | 20.3 | 19.0 |
| 18 | 41.5 | 47.8 | 43.0 | 37.2 | 32.8 | 29.1 | 26.0 | 23.7 | 21.9 | 20.4 | 19.0 |
| 19 | 24.1 | 43.0 | 41.3 | 37.0 | 33.2 | 29.6 | 26.5 | 24.1 | 22.2 | 20.5 | 19.0 |
| 20 | 18.5 | 39.2 | 39.4 | 36.4 | 33.2 | 29.9 | 26.9 | 24.5 | 22.4 | 20.6 | 19.0 |
| 21 | 16.7 | 36.3 | 37.5 | 35.5 | 32.9 | 30.0 | 27.2 | 24.7 | 22.6 | 20.8 | 19.0 |
| 22 | 15.4 | 34.0 | 35.8 | 34.6 | 32.5 | 30.0 | 27.4 | 25.0 | 22.8 | 20.9 | 19.0 |
| 23 | 14.7 | 32.2 | 34.3 | 33.6 | 32.0 | 29.8 | 27.4 | 25.1 | 23.0 | 20.9 | 19.0 |
| 24 | 14.6 | 30.7 | 32.9 | 32.7 | 31.5 | 29.6 | 27.3 | 25.2 | 23.0 | 21.0 | 19.0 |

Table 8. Hourly subsoil profile temperature determined from hourly surface temperature (from radiation model) on July 9.

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Hours | surface | 5 cm | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 cm |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | 14.7 | 25.6 | 26.8 | 26.4 | 25.5 | 24.5 | 23.5 | 22.5 | 21.5 | 20.4 | 19.3 |
| 2 | 10.3 | 24.1 | 25.9 | 25.9 | 25.3 | 24.5 | 23.5 | 22.4 | 21.4 | 20.4 | 19.3 |
| 3 | 7.4 | 22.7 | 25.0 | 25.4 | 25.0 | 24.3 | 23.4 | 22.4 | 21.4 | 20.4 | 19.3 |
| 4 | 10.6 | 22.0 | 24.3 | 24.9 | 24.7 | 24.1 | 23.3 | 22.3 | 21.4 | 20.3 | 19.3 |
| 5 | 29.5 | 23.6 | 24.0 | 24.4 | 24.3 | 23.9 | 23.1 | 22.3 | 21.3 | 20.3 | 19.3 |
| 6 | 56.1 | 27.6 | 24.6 | 24.3 | 24.1 | 23.6 | 23.0 | 22.2 | 21.3 | 20.3 | 19.3 |
| 7 | 78.0 | 32.7 | 26.3 | 24.6 | 24.0 | 23.5 | 22.8 | 22.0 | 21.2 | 20.3 | 19.3 |
| 8 | 94.6 | 37.9 | 28.5 | 25.4 | 24.2 | 23.4 | 22.7 | 22.0 | 21.1 | 20.2 | 19.3 |
| 9 | 106.9 | 42.9 | 31.1 | 26.6 | 24.7 | 23.6 | 22.7 | 21.9 | 21.1 | 20.2 | 19.3 |
| 10 | 114.8 | 47.4 | 33.9 | 28.0 | 25.4 | 23.8 | 22.8 | 21.9 | 21.0 | 20.2 | 19.3 |
| 11 | 118.5 | 51.2 | 36.5 | 29.6 | 26.3 | 24.3 | 23.0 | 21.9 | 21.0 | 20.2 | 19.3 |
| 12 | 118.3 | 54.0 | 39.0 | 31.3 | 27.4 | 24.9 | 23.3 | 22.1 | 21.1 | 20.2 | 19.3 |
| 13 | 115.6 | 56.0 | 41.1 | 32.9 | 28.6 | 25.6 | 23.7 | 22.3 | 21.2 | 20.2 | 19.3 |
| 14 | 108.8 | 57.0 | 42.8 | 34.4 | 29.7 | 26.4 | 24.1 | 22.5 | 21.3 | 20.3 | 19.3 |
| 15 | 98.5 | 56.8 | 44.0 | 35.7 | 30.8 | 27.3 | 24.7 | 22.9 | 21.5 | 20.4 | 19.3 |
| 16 | 83.9 | 55.4 | 44.5 | 36.7 | 31.8 | 28.1 | 25.3 | 23.3 | 21.7 | 20.5 | 19.3 |
| 17 | 64.8 | 52.5 | 44.3 | 37.4 | 32.6 | 28.8 | 25.8 | 23.7 | 22.0 | 20.6 | 19.3 |
| 18 | 41.5 | 48.1 | 43.3 | 37.6 | 33.2 | 29.4 | 26.4 | 24.1 | 22.2 | 20.7 | 19.3 |
| 19 | 24.1 | 43.3 | 41.7 | 37.4 | 33.5 | 29.9 | 26.9 | 24.5 | 22.5 | 20.8 | 19.3 |
| 20 | 18.5 | 39.5 | 39.7 | 36.7 | 33.5 | 30.2 | 27.3 | 24.8 | 22.8 | 21.0 | 19.3 |
| 21 | 16.7 | 36.6 | 37.8 | 35.9 | 33.3 | 30.4 | 27.5 | 25.1 | 23.0 | 21.1 | 19.3 |
| 22 | 15.4 | 34.2 | 36.1 | 34.9 | 32.9 | 30.3 | 27.7 | 25.3 | 23.2 | 21.2 | 19.3 |
| 23 | 14.7 | 32.4 | 34.5 | 33.9 | 32.4 | 30.2 | 27.7 | 25.4 | 23.3 | 21.3 | 19.3 |
| 24 | 14.6 | 30.9 | 33.2 | 33.0 | 31.8 | 29.9 | 27.7 | 25.5 | 23.4 | 21.3 | 19.3 |

Table 9. Hourly subsoil profile temperature determined from hourly surface temperature (from radiation model) on August 1.

| Hours | surface | 5 cm | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 cm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 14.7 | 21.7 | 23.9 | 24.4 | 24.0 | 23.3 | 22.4 | 21.5 | 20.5 | 19.6 | 18.7 |
| 2 | 10.8 | 21.1 | 23.2 | 23.8 | 23.7 | 23.1 | 22.3 | 21.4 | 20.5 | 19.6 | 18.7 |
| 3 | 8.2 | 20.3 | 22.6 | 23.3 | 23.3 | 22.9 | 22.2 | 21.4 | 20.5 | 19.6 | 18.7 |
| 4 | 8.1 | 19.6 | 22.0 | 22.9 | 23.0 | 22.6 | 22.0 | 21.3 | 20.5 | 19.6 | 18.7 |
| 5 | 22.7 | 20.8 | 21.7 | 22.5 | 22.6 | 22.4 | 21.9 | 21.2 | 20.4 | 19.6 | 18.7 |
| 6 | 50.3 | 24.6 | 22.3 | 22.3 | 22.3 | 22.1 | 21.7 | 21.1 | 20.3 | 19.5 | 18.7 |
| 7 | 72.7 | 29.6 | 23.8 | 22.6 | 22.3 | 22.0 | 21.5 | 20.9 | 20.3 | 19.5 | 18.7 |
| 8 | 90.2 | 34.9 | 26.1 | 23.3 | 22.4 | 21.9 | 21.4 | 20.8 | 20.2 | 19.5 | 18.7 |
| 9 | 102.6 | 40.0 | 28.7 | 24.5 | 22.9 | 22.0 | 21.4 | 20.8 | 20.1 | 19.4 | 18.7 |
| 10 | 110.9 | 44.6 | 31.4 | 25.9 | 23.6 | 22.3 | 21.4 | 20.7 | 20.1 | 19.4 | 18.7 |
| 11 | 115.2 | 48.4 | 34.2 | 27.6 | 24.5 | 22.8 | 21.6 | 20.8 | 20.1 | 19.4 | 18.7 |
| 12 | 115.8 | 51.5 | 36.7 | 29.2 | 25.6 | 23.4 | 21.9 | 20.9 | 20.1 | 19.4 | 18.7 |
| 13 | 112.5 | 53.5 | 38.8 | 30.9 | 26.7 | 24.1 | 22.3 | 21.1 | 20.2 | 19.4 | 18.7 |
| 14 | 105.5 | 54.5 | 40.5 | 32.4 | 27.9 | 24.9 | 22.8 | 21.4 | 20.4 | 19.5 | 18.7 |
| 15 | 93.7 | 54.1 | 41.7 | 33.7 | 29.0 | 25.7 | 23.3 | 21.7 | 20.5 | 19.6 | 18.7 |
| 16 | 76.4 | 52.3 | 42.2 | 34.7 | 30.0 | 26.5 | 23.9 | 22.1 | 20.8 | 19.7 | 18.7 |
| 17 | 54.5 | 48.8 | 41.8 | 35.3 | 30.8 | 27.2 | 24.5 | 22.5 | 21.0 | 19.8 | 18.7 |
| 18 | 30.7 | 43.9 | 40.6 | 35.4 | 31.4 | 27.8 | 25.0 | 22.9 | 21.3 | 19.9 | 18.7 |
| 19 | 22.4 | 39.9 | 38.8 | 35.1 | 31.6 | 28.3 | 25.5 | 23.3 | 21.5 | 20.0 | 18.7 |
| 20 | 14.7 | 36.2 | 36.9 | 34.4 | 31.6 | 28.6 | 25.9 | 23.6 | 21.8 | 20.2 | 18.7 |
| 21 | 13.1 | 33.5 | 35.1 | 33.6 | 31.3 | 28.7 | 26.1 | 23.9 | 22.0 | 20.3 | 18.7 |
| 22 | 11.6 | 31.2 | 33.4 | 32.6 | 30.9 | 28.6 | 26.2 | 24.1 | 22.2 | 20.4 | 18.7 |
| 23 | 10.3 | 29.3 | 31.9 | 31.7 | 30.4 | 28.4 | 26.3 | 24.2 | 22.3 | 20.5 | 18.7 |
| 24 | 9.3 | 27.7 | 30.6 | 30.8 | 29.8 | 28.2 | 26.2 | 24.2 | 22.4 | 20.5 | 18.7 |

These values indicate the possible losses of heat by conduction in the several layers of the soil. The higher loss is found at the top of the soil.

## Heat flow in the soil

The change in heat content in the soil was calculated by equation [10] using data of subsoil profile temperature observed in the field and assuming the volumetric heat capacity of soil ( $\mathrm{C}_{\mathrm{v}}$ ) is known.

If we consider the volumetric heat capacity of soil to be constant $\left(C_{v}\right)$ all over the profile, the variation of heat flux through the several layers below the soil surface between 5 A.M. and 2 P.M. on typical clear days is shown in Tables 10, 11, and 12. The flow in the first layer ( $0-2 \mathrm{~cm}$ depth) represent $37 \%$ (on July 7 ), $33 \%$ (on July 9), and $30 \%$ (on August 1) of the overall profile. In the second layer ( $2-10 \mathrm{~cm}$ depth) the heat flow was 60\% (on July 7) and 59\% (on July 9 and August 1). Thus, the heat flow was concentrated in these first two layers.

With varying volumetric heat capacity as reported in Table 10, 11 and 12, we found the following percentages: the the first layer $35 \%$ (on July 7), $31 \%$ (on July 9), and $28 \%$ (on August 1). In the second layer (2-10 cm depth) 66\% (on July 7), $75 \%$ (on July 9) and $72 \%$ ( on August 1).

The daily net heat gain was relatively small indicating that most of the $\triangle \mathrm{HC}$ gained during the day was lost during the night.

Calculated heat flow in the soil using data of simulated profile of subsoil temperature. Data of simulated subsoil profile temperature were used to calculate heat flow with formula [10]. Also, here the maximum flow of heat was concentrated in the first 10 cm depth. Tables

13,14 , and 15 show the following percentages: July 7, $97 \%$; $93.4 \%$ on July 9 ; and $92 \%$ on August 1. These high percentages were calculated for ( $0-10 \mathrm{~cm}$ depth) observing $C_{v}$ to be constant throughout the profile. With estimated values of the volumetric heat capacity, we found $99 \%$ on July 7, $94.5 \%$ on July 9 and $93 \%$ on August 1 for the first two layers. These values indicate a good agreement if compared with the calculated values using the observed data of temperature in the field. Furthermore, very little downward flux occurs in layers below 10 cm depth.

Tables 16, 17, and 18 show the calculated heat flow using the temperature profiles of Tables 7, 8, and 9 respectively. In the two first layers ( $0-10 \mathrm{~cm}$ depth) we found the following percentages: on July 7, $74 \%$; on July 9, $74 \%$; and on August 1, $75 \%$ for constant $C_{v}$ throughout the profile. For varying $C_{v}$ a percentage of $70 \%$ on July 7 , $69 \%$ on July 9, and $71 \%$ on August 1 was found.

Table 10. Heat flow calculated of observed values of soil temperature in the field on July 7.

| DEPTH <br> (cm) | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 5 \mathrm{~A} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} \mathrm{T} & \left({ }^{\circ} \mathrm{C}\right) \\ \text { at } & 2 \mathrm{P} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \Delta Z \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \cdot \Delta \mathrm{Z} \\ & { }^{\circ} \mathrm{C} . \mathrm{cm} \end{aligned}$ | $\stackrel{\Delta \mathrm{HC}}{\mathrm{cal} . \mathrm{cm}^{-2}}$ | \% | Cv | $\begin{gathered} \Delta \mathrm{HC} \\ \text { cal. } \mathrm{cm}^{-2} \end{gathered}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0-2$ | 11.63 | 58.00 | 46.37 | 2 | 92.74 | 92.74 Cv | 36.8 | 0.39 | 36.16 | 35.3 |
| $2-10$ | 18.75 | 38.50 | 19.75 | 8 | 158.00 | 158.00 Cv | 62.7 | 0.43 | 67.94 | 66.4 |
| 10-25 | 23.13 | 24.88 | 1.75 | 15 | 26.25 | 26.25 Cv | 10.4 | 0.49 | 12.86 | 12.6 |
| $25-50$ | 21.50 | 20.50 | $-1.00$ | 25 | -25.00 | -25.00 Cv | -9.9 | 0.59 | -14.75 | -14.4 |
| TOTAL |  |  |  |  |  | 251.99 CV |  |  | 102.21 |  |

Table 11. Heat flow calculated of observed values of soil temperature in the field on July 9.

| $\begin{aligned} & \text { DEPTH } \\ & (\mathrm{cm}) \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 5 \mathrm{~A} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 2 \mathrm{P} . \mathrm{M}_{.} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \Delta Z \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \cdot \Delta \mathrm{Z} \\ & { }^{\circ} \mathrm{C} \cdot \mathrm{~cm} \end{aligned}$ | $\begin{gathered} \Delta H C \\ \mathrm{cal} . \mathrm{cm}^{-2} \end{gathered}$ | \% | Cv | $\begin{aligned} & \Delta \mathrm{HC} \\ & \text { cal. } \mathrm{cm}^{-2} \end{aligned}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-2 | 11.25 | 60.25 | 49.00 | 2 | 98.00 | 98.00 Cv | 33.0 | 0.39 | 38.22 | 30.9 |
| 2-10 | 17.75 | 39.62 | 21.87 | 8 | 174.96 | 174.96 Cv | 58.9 | 0.43 | 75.23 | 60.8 |
| 10-25 | 22.50 | 25.13 | 2.63 | 15 | 39.45 | 39.45 Cv | 13.3 | 0.49 | 19.33 | 15.6 |
| 25-50 | 21.25 | 20.63 | -0.62 | 25 | -15.50 | -15.50 Cv | -5.2 | 0.59 | -9.14 | -7.4 |
| TOTAL |  |  |  |  |  | 296.91 Cv |  |  | 123.64 |  |

Table 12. Heat flow calculated of observed values of soil temperature in the field on August 1.

| $\begin{aligned} & \text { DEPTH } \\ & (\mathrm{cm}) \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 5 \mathrm{~A} \cdot \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \mathrm{T} \quad\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 2 \mathrm{P} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{Z} \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \cdot \Delta \mathrm{Z} \\ & { }^{\circ} \mathrm{C} \cdot \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \triangle H C \\ & \mathrm{cal} . \mathrm{cm}^{-2} \end{aligned}$ | \% | Cv | $\begin{aligned} & \Delta H C \\ & \mathrm{cal} . \mathrm{cm}^{-2} \end{aligned}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-2 | 10.38 | 52.50 | 42.12 | 2 | 84.24 | 84.24 Cv | 29.8 | 0.39 | 32.85 | 28.3 |
| $2-10$ | 16.25 | 37.25 | 21.00 | 8 | 168.00 | 168.00 Cv | 59.4 | 0.43 | 72.24 | 62.2 |
| 10-25 | 21.13 | 25.88 | 4.75 | 15 | 71.25 | 71.25 Cv | 25.1 | 0.49 | 34.91 | 30.1 |
| 25-50 | 20.63 | 22.25 | -1.62 | 25 | -40.50 | $-40.50 \mathrm{Cv}$ | -14.3 | 0.59 | -23.89 | -20.6 |
| TOTAL |  |  |  |  |  | 282.99 CV |  |  | 116.11 |  |

Table 13. Heat flow calculated from simulated values of subsoil profile temperature on July 7.

| DEPTH <br> (cm) | $\begin{aligned} \mathrm{T} & \left({ }^{\circ} \mathrm{C}\right) \\ \text { at } & 5 \mathrm{~A} . \mathrm{M} \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 2 \mathrm{P} . \mathrm{M} \end{aligned}$ | $\begin{aligned} & \Delta T \\ & \mathrm{PC} \end{aligned}$ | $\begin{aligned} & \Delta Z \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta T \cdot \Delta Z \\ & { }^{\circ} \mathrm{C} \cdot \mathrm{~cm} \end{aligned}$ | $\stackrel{\Delta H C}{\mathrm{cal} . \mathrm{cm}_{-}^{-2}}$ | \% | Cv | $\begin{aligned} & \Delta \mathrm{HC} \\ & \mathrm{cal.} . \mathrm{cm}^{-2} \end{aligned}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-5 | 14.25 | 51.50 | 37.25 | 5 | 186.25 | 186.25 Cv | 74.6 | 0.39 | 72.64 | 75.9 |
| 5-10 | 21.50 | 32.70 | 11.20 | 5 | 56.00 | 56.00 Cv | 22.4 | 0.40 | 22.40 | 23.4 |
| 10-15 | 23.10 | 27.25 | 4.15 | 5 | 20.75 | 20.75 Cv | 8.3 | 0.43 | 8.92 | 9.3 |
| 15-20 | 23.55 | 24.50 | 0.95 | 5 | 4.75 | 4.75 Cv | 1.9 | 0.54 | 2.57 | 2.6 |
| 20-25 | 23.40 | 23.00 | -0.40 | 5 | -2.00 | -2.00 Cv | -0.8 | 0.54 | -1.08 | -1.1 |
| 25-30 | 22.90 | 22.00 | -0.90 | 5 | -4.50 | $-4.50 \mathrm{Cv}$ | -1.8 | 0.54 | -2.43 | -2.53 |
| 30-35 | 22.20 | 21.25 | -0.95 | 5 | -4.75 | $-4.75 \mathrm{Cv}$ | -1.9 | 0.67 | -3.18 | -3.32 |
| 35-40 | 21.35 | 20.60 | -0.75 | 5 | -3.75 | -3.75 Cv | -1.5 | 0.67 | -2.51 | -2.6 |
| 40-45 | 20.45 | 20.00 | -0.45 | 5 | -2.25 | $-2.25 \mathrm{Cv}$ | -0.9 | 0.54 | -1.22 | -1.3 |
| 45-50 | 19.50 | 19.35 | -0.15 | 5 | -0.75 | $-0.75 \mathrm{Cv}$ | -0.3 | 0.54 | -0.40 | -0.4 |
| TOTAL |  |  |  |  |  | 249.75 Cv |  |  | 95.71 |  |

Table 14. Heat flow calculated from simulated values of subsoil profile temperature on July 9.

| $\begin{aligned} & \text { DEPTH } \\ & (\mathrm{cm}) \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 5 \mathrm{~A} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 2 \mathrm{P} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{array}{r} \mathrm{Z} \\ \mathrm{~cm} \end{array}$ | T. Z <br> ${ }^{\circ} \mathrm{C}$. cm | $\underset{\text { cal. } \mathrm{cm}_{.}^{-2}}{\text { HC }}$ | \% | Cv | $\stackrel{\mathrm{HC}}{\mathrm{al.cm}} \mathrm{c}^{-2}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0-5$ | 14.10 | 53.25 | 39.15 | 5 | 195.75 | 195.75 Cv | 71.1 | 0.39 | 76.34 | 71.5 |
| $5-10$ | 20.90 | 33.20 | 12.30 | 5 | 61.50 | 61.50 Cv | 22.3 | 0.40 | 24.60 | 23.0 |
| 10-15 | 22.60 | 27.50 | 4.90 | 5 | 24.50 | 24.50 Cv | 8.9 | 0.43 | 10.53 | 9.9 |
| 15-20 | 23.20 | 24.65 | 1.45 | 5 | 7.25 | 7.25 Cv | 2.6 | 0.54 | 3.91 | 3.7 |
| 20-25 | 23.20 | 23.10 | -0.10 | 5 | -0.50 | -0.50 Cv | -0.2 | -. 54 | -0.27 | -0.3 |
| 25-30 | 22.55 | 22.10 | -0.45 | 5 | -2.25 | -2.25 Cv | -0.8 | 0.54 | -1.21 | -1.1 |
| 30-35 | 22.25 | 21.35 | -0.90 | 5 | -4.50 | -4.50 Cv | -1.6 | 0.67 | -3.01 | -2.8 |
| 35-40 | 21.50 | 20.75 | -0.75 | 5 | -3.75 | -3.75 Cv | -1.3 | 0.67 | -2.51 | -2.3 |
| 40-45 | 20.65 | 20.20 | -0.45 | 5 | -2.25 | -2.25 Cv | -0.8 | 0.54 | -1.21 | -1.1 |
| 45-50 | 19.75 | 19.60 | -0.15 | 5 | -0.75 | -0.75 Cv | -0.2 | 0.54 | -0.40 | -0.4 |
| TOTAL |  |  |  |  |  | 275.50 Cv |  |  | 106.77 |  |

Table 15. Heat flow calculated from simulated values of subsoil profile temperature on August 1.

| DEPTH <br> (cm) | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 5 \mathrm{~A} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} \mathrm{T} & \left({ }^{\circ} \mathrm{C}\right) \\ \text { at } & 2 \mathrm{P} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \Delta Z \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \cdot \Delta \mathrm{Z} \\ & { }^{\circ} \mathrm{C} \cdot \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta H C \\ & \mathrm{cal} . \mathrm{cm}^{-2} \end{aligned}$ | \% | Cv | $\begin{aligned} & \triangle \mathrm{HC} \\ & \mathrm{cal} . \mathrm{cm}^{-2} \end{aligned}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-5 | 13.05 | 47.10 | 34.05 | 5 | 170.25 | 170.25 Cv | 69.0 | 0.39 | 66.39 | 69.1 |
| $5-10$ | 19.30 | 30.70 | 11.40 | 5 | 57.00 | 57.00 Cv | 23.1 | 0.40 | 22.80 | 23.7 |
| 10-15 | 21.00 | 25.85 | 4.85 | 5 | 24.25 | 24.25 Cv | 9.8 | 0.43 | 10.42 | 10.8 |
| 15-20 | 21.70 | 23.35 | 1.65 | 5 | 8.25 | 8.25 Cv | 3.3 | 0.54 | 4.45 | 4.6 |
| 20-25 | 21.85 | 21.95 | 0.10 | 5 | 0.50 | 0.50 Cv | 0.2 | 0.54 | 0.27 | 0.3 |
| 25-30 | 21.65 | 21.05 | -0.60 | 5 | -3.00 | $-3.00 \mathrm{Cv}$ | -1.2 | 0.54 | -1.62 | -1.7 |
| 30-35 | 21.20 | 20.40 | -0.80 | 5 | -4.00 | -4.00 Cv | -1.6 | 0.67 | -2.68 | -2.8 |
| 35-40 | 20.60 | 19.90 | -0.70 | 5 | -3.50 | $-3.50 \mathrm{Cv}$ | -1.4 | 0.67 | -2.34 | -2.4 |
| 40-45 | 19.90 | 19.45 | -0.45 | 5 | -2.25 | -2.25 Cv | -0.9 | 0.54 | -1.21 | -1.3 |
| 45-50 | 19.10 | 18.95 | -0.15 | 5 | -0.75 | $-0.75 \mathrm{Cv}$ | -0.3 | 0.54 | -0.40 | -0.4 |
| TOTAL |  |  |  |  |  | 246.75 Cv |  |  | 96.08 |  |

Table 16. Heat flow calculated from data of profile temperature from Table 7.

| $\begin{aligned} & \text { DEPTH } \\ & (\mathrm{cm}) \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 5 \mathrm{~A} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 2 \mathrm{P} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \Delta Z \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \cdot \Delta \mathrm{Z} \\ & { }^{\circ} \mathrm{C} . \mathrm{cm} \\ & \hline \end{aligned}$ | $\begin{gathered} \Delta \mathrm{HC} \\ \mathrm{cal} . \mathrm{cm}^{-2} \end{gathered}$ | \% | Cv | $\begin{aligned} & \triangle \mathrm{HC} \\ & \mathrm{cal} . \mathrm{cm}^{-2} \end{aligned}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-5 | 26.30 | 82.75 | 56.54 | 5 | 282.25 | 282.25 CV | 50.6 | 0.39 | 110.07 | 47.3 |
| 5 -10 | 23.25 | 49.55 | 26.30 | 5 | 131.50 | 131.50 Cv | 23.6 | 0.40 | 52.60 | 22.6 |
| 10-15 | 23.65 | 38.20 | 14.55 | 5 | 72.75 | 72.75 Cv | 13.0 | 0.43 | 31.28 | 13.4 |
| 15-20 | 23.90 | 31.65 | 7.75 | 5 | 38.75 | 38.75 Cv | 6.9 | 0.54 | 20.92 | 9.0 |
| 20-25 | 23.70 | 27.65 | 3.95 | 5 | 19.75 | 19.75 Cv | 3.5 | 0.54 | 10.66 | 4.6 |
| 25-30 | 23.15 | 24.90 | 1.75 | 5 | 8.75 | 8.75 Cv | 1.6 | 0.54 | 4.72 | 2.0 |
| 30-35 | 22.35 | 23.00 | 0.65 | 5 | 3.25 | 3.25 Cv | 0.6 | 0.67 | 2.17 | 0.9 |
| 35-40 | 21.45 | 21.60 | 0.15 | 5 | 0.75 | 0.75 Cv | 0.1 | 0.67 | 0.50 | 0.2 |
| 40-45 | 20.50 | 20.50 | 0.00 | 5 | 0.00 | 0.00 Cv | 0.0 | 0.54 | 0.00 | 0.0 |
| 45-50 | 19.50 | 19.50 | 0.00 | 5 | 0.00 | 0.00 Cv | 0.0 | 0.54 | 0.00 | 0.0 |
| TOTAL |  |  |  |  |  | 557.75 Cv |  |  | 232.92 |  |

Table 17. Heat flow calculated from data of profile temperature from Table 8.

| DEPTH (cm) | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 5 \mathrm{~A} . \mathrm{M} . \end{aligned}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 2 \mathrm{P} . \mathrm{M}^{2} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \Delta Z \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \cdot \Delta \mathrm{Z} \\ & { }^{\circ} \mathrm{C} \cdot \mathrm{~cm} \end{aligned}$ | $\begin{gathered} \triangle \mathrm{HC} \\ \mathrm{cal} . \mathrm{cm}^{-2} \\ \hline \end{gathered}$ | \% | Cv | $\begin{gathered} \Delta \mathrm{HC} \\ \mathrm{cal} . \mathrm{cm}^{-2} \end{gathered}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-5 | 26.55 | 82.90 | 56.35 | 5 | 281.75 | 281.75 Cv | 50.8 | 0.39 | 109.88 | 47.5 |
| $5-10$ | 23.80 | 49.90 | 26.10 | 5 | 130.50 | 130.50 Cv | 23.5 | 0.40 | 52.20 | 22.5 |
| 10-15 | 24.20 | 38.60 | 14.40 | 5 | 72.00 | 72.00 Cv | 13.0 | 0.43 | 30.96 | 13.4 |
| 15-20 | 24.35 | 32.05 | 7.70 | 5 | 38.50 | 38.50 Cv | 6.9 | 0.54 | 20.79 | 9.0 |
| 20-25 | 24.10 | 28.05 | 3.95 | 5 | 19.75 | 19.75 Cv | 3.6 | 0.54 | 10.66 | 4.6 |
| 25-30 | 23.50 | 25.25 | 1.75 | 5 | 8.75 | 8.75 Cv | 1.6 | 0.54 | 4.72 | 2.0 |
| 30-35 | 22.70 | 23.30 | 0.60 | 5 | 3.00 | 3.00 Cv | 0.5 | 0.67 | 2.01 | 0.9 |
| 35-40 | 21.80 | 21.90 | 0.10 | 5 | 0.50 | 0.50 Cv | 0.1 | 0.67 | 0.33 | 0.1 |
| 40-45 | 20.80 | 20.80 | 0.00 | 5 | 0.00 | 0.00 Cv | 0.0 | 0.54 | 0.00 | 0.0 |
| 45-50 | 19.80 | 19.80 | 0.00 | 5 | 0.00 | 0.00 Cv | 0.0 | 0.54 | 0.00 | 0.0 |
| TOTAL |  |  |  |  |  | 554.75 Cv |  |  | 231.55 |  |

Table 18. Heat flow calculated from data of subsoil profile temperature from Table 9.

| $\begin{aligned} & \text { DEPTH } \\ & (\mathrm{cm}) \end{aligned}$ | $\begin{gathered} \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ \text { at } 5 \mathrm{~A} \cdot \mathrm{M} . \end{gathered}$ | $\begin{aligned} & \mathrm{T}\left({ }^{\circ} \mathrm{C}\right) \\ & \text { at } 2 \text { P.M. } \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{Z} \\ & \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & \Delta \mathrm{T} . \Delta \mathrm{Z} \\ & { }^{\circ} \mathrm{C} . \mathrm{cm} \end{aligned}$ | $\stackrel{\Delta \mathrm{HC}}{\text { cal. } \mathrm{cm}^{-2}}$ | \% | Cv | $\begin{gathered} \Delta H C \\ \text { cal. } \mathrm{cm}^{-2} \end{gathered}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0-5$ | 21.75 | 80.00 | 58.25 | 5 | 291.25 | 291.25 Cv | 51.73 | 0.39 | 113.58 | 48.43 |
| $5-10$ | 21.25 | 47.50 | 26.25 | 5 | 131.25 | 131.25 Cv | 23.31 | 0.40 | 52.50 | 22.38 |
| 10-15 | 22.10 | 36.45 | 14.35 | 5 | 71.75 | 71.75 Cv | 12.74 | 0.43 | 30.85 | 13.15 |
| 15-20 | 22.55 | 30.15 | 7.60 | 5 | 38.00 | 38.00 Cv | 6.75 | 0.54 | 20.52 | 8.75 |
| 20-25 | 22.50 | 26.40 | 3.90 | 5 | 19.50 | 19.50 Cv | 3.46 | 0.54 | 10.53 | 4.49 |
| 25-30 | 22.15 | 23.85 | 1.70 | 5 | 8.50 | 8.50 Cv | 1.51 | 0.54 | 4.59 | 1.95 |
| 30-35 | 21.55 | 22.10 | 0.55 | 5 | 2.75 | 2.75 Cv | 0.49 | 0.67 | 1.84 | 0.78 |
| 35-40 | 20.80 | 20.90 | 0.10 | 5 | 0.50 | 0.50 Cv | 0.09 | 0.67 | 0.34 | 0.14 |
| 40-45 | 20.00 | 19.95 | -0.95 | 5 | -0.25 | -0.25 Cv | -0.04 | 0.54 | -0.13 | -0.05 |
| 45-50 | 19.15 | 19.10 | -0.05 | 5 | -0.25 | -0.25 Cv | -0.04 | 0.54 | -0.13 | -0.05 |
| TOTAL |  |  |  |  |  | 563.00 Cv |  |  | 234.49 |  |

For equal short-wave radiation intensities, the net radiation was always smaller in the afternoon than in the morning because of higher afternoon surface temperature.

The diurnal changes were much greater in the outgoing than in the incoming component of long-wave radiation.

At midday and early afternoon, the heat loss by long-wave exchange was approximately three times its nocturnal value.

At midday the atmospheric radiation calculated from observed data was about $70 \%$ of the emitted long-wave radiation from the surface.

At midday the value of the long-wave radiation $\left(R_{E}\right)$ derived from the radiation model (average value of 12 days) was $1.661 \mathrm{y} / \mathrm{min}$. which was about $0.631 y / m i n$. higher than calculated from observed measurements of radiation.

During early morning hours there were no marked differences between the emitted radiation $\left(R_{E}\right)$ derived from the radiation model and observed data.

High values of surface temperature (about $115.5{ }^{\circ} \mathrm{C}$, average value for 12 days) were calculated with the radiation model. This indicates a surface temperature without dissipation effects. When compared with the observed temperature in the field, the difference represents the heat lost from the surface to the soil below and the air above.

In the past, many investigators had determined the thermal diffusivity of the soil from soil temperature records using phase and amplitude
equations. Those investigators who determined thermal diffusivities from the annual soil temperature records reported more realistic and consistent values than those using the daily cycle. In the present study, better values were obtained by using the phase equation than using the amplitude equation.

The equated measurements of the soil profile were under dry conditions. For wet conditions or those where soil water content changes considerably with depth as well as for more periodic surface temperature change, the phase and amplitude equation cannot be used to determine thermal diffusivity since the thermal properties of soil depend mainly on the mineral composition, the porosity and the soil water content.

The maximum soil temperature at the surface was found to occur between 1300 and 1500 hours. The maximum value of temperature reached at the surface was $71{ }^{\circ} \mathrm{C}$.

At 2 cm depth, the temperature of the soil always was warmer than the air. But the variation of temperature at 10 cm depth approached the air temperature between 2 meter and 8 meter.

The minimum temperatures were reached before sunrise. $7.2^{\circ} \mathrm{C}$ was the minimum value observed in the field.

The variations of temperature at 25 cm depth were found to be of $2^{\circ}$ to $3{ }^{\circ} \mathrm{C}$ throughout the day and at 50 cm depth no notable variations occurred.

In the present study a computer model was used to predict the temperature of the subsoil from the temperature variation at the soil surface with values of the apparent thermal diffusivity which is dependent upon depth below soil surface and soil temperature. From soil profile temperature data in Figure 3, it is obvious that with the computer model
a good estimate can be made of the hourly values of the soil profile. We could note, also, that a better agreement in the profile could be recorded if 5 layers rather than 10 cm layers were used.

The maximum transfer of heat occurred in the first two layers of the profile (surface -10 cm depth). $33 \%$ of total heat in the profile was concentrated in the two first centimeters of depth, if calculated from daily soil temperature records in the field, and assuming a constant volumetric heat capacity throughout the profile. For estimated values of volumetric heat capacity as reported in Tables 10,11 and $12,31 \%$ of total value of heat was found in the first layer ( $0-2$ centimeters of depth) and almost all the rest of the heat was concentrated in the second layer ( $2-10 \mathrm{~cm}$ depth).

Also, for the computed soil temperature, the major heat flow occurred in the first two layers (surface - 10 cm depth), particularly in the first 5 cm (75\%). The further decrease occurred gradually with depth.

High values of heat flow were found using temperatures calculated with the radiation model. The difference between these values and the values of heat flow calculated with records of temperature observed in the field indicate the possible loss of heat by conduction and convection.

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## Appendix A

## Computer Program of Radiation Mode1

COMMON FF (24), ALPHA, BETA, GAMMA, DELTA, EPSLN, TX, TAIR, RA, TSOIL, EZ
COMMON X,DELEP
READ (5, 6)ALPHA, BETA, GAMMA, DELTA, EPSLN
6 FORMAT(3F10.4,E10.4, F10.4)
5 WRITE (6, 7)ALPHA, BETA, GAMMA, DELTA, EPSLN
7 FORMAT(1H1,10X,'PARAMETER VALUES FOR THIS RUN ARE:'/
11H0,5x, 'ALPHA' , 6X'BETA' , 5x, 'GAMMA' ,5x, 'DELTA' , 3x, 'EPSILON'/
21X,3F10.4E10.4,F10.4///' DATE HR RS+RD TAIR(F) TAIR(K)'
3' E ZERO RA RE T SOIL')
DELEP=DELTA*EPSLN
$\operatorname{READ}(5,8) \operatorname{DATE},(\mathrm{FF}(\mathrm{I}), \mathrm{I}=1,24)$
8 FORMAT(A6,11F4.1/6X,13F4.1)
DO $9 \mathrm{I}=1,24$
$9 \quad \mathrm{FF}(\mathrm{I})=\mathrm{FF}(\mathrm{I}) / 60.0$
$10 \operatorname{READ}(5,11) \mathrm{X} 1, \mathrm{Y} 1, \mathrm{Z} 1, \mathrm{X} 2, \mathrm{Y} 2, \mathrm{Z} 2, \mathrm{X} 3, \mathrm{Y} 3, \mathrm{Z} 3$
11 FORMAT(3X,F3.0,F4.0,F8.4/3X,F3.0,F4.0,F8.4/3X,F3.0, F4.0,F8.4)
DIFFY=Y2-Y1
DIFFX $=\mathrm{X} 2-\mathrm{X} 1$
DiffZ=Z2-Z1
SUMX $=\mathrm{X} 1+\mathrm{X} 2$
$\mathrm{C}=[(\mathrm{Y} 3-\mathrm{Y} 2) * \mathrm{DIFFX}-\mathrm{DIFFY} *(\mathrm{X} 3-\mathrm{X} 3)] /[(\mathrm{X} 3-\mathrm{X} 2) * \mathrm{DIFFX} *(\mathrm{X} 3-\mathrm{X} 1)]$
B=DIFFY/DIFFX-C*SUMX

```
A=Y1=(B+C*X1)*X1
CE=[(Z3-Z2)*DIFFX-DIFFZ*(X3-X2) ]/[(X3-X2)*DIFFX*(X3-X1)]
BE=DIFFZ/DIFFX-CE*SUMX
AE=Z1-(BE+CE*X1)*X1
X=X1-1.0
TX=A+(B+C*X)*X
EZ=AE+(BE+CE*X)*X
```

CALL COMPT
WRITE $(6,13)$ DATE, $\mathrm{X}, \mathrm{FF}(\mathrm{X})$, TX, TAIR, EZ, RA, RE, TSOIL
13 FORMAT(1H, A6, I4 , F6.1,2F10.4,F8.3,2F7.2,F8.2)
$\mathrm{X}=\mathrm{x} 1$
$T X=Y 1$
$E Z=Z 1$
CALL COMPT
WRITE $(6,13)$ DATE $, X, F F(X), T X, T A I R, E Z, R A, R E, T S O I L$
$14 \mathrm{X}=\mathrm{Xl}+1$
$T X=A+(B+C * X) * X$
$\mathrm{EZ}=\mathrm{AE}+(\mathrm{BE}+\mathrm{CE} * \mathrm{X}) * \mathrm{X}$
CALL COMPT
WRITE $(6,13)$ DATE, $\mathrm{X}, \mathrm{FF}(\mathrm{X}), \mathrm{TX}$, TAIR, EZ, RA, RE, TSOIL
$\mathrm{X}=\mathrm{x} 1+2$
$T X=A+(B+C * X) * X$
$\mathrm{EZ}=\mathrm{AE}+\mathrm{BE}+\mathrm{CE} * \mathrm{X}) * \mathrm{X}$
CALL COMPT
WRITE $(6,13)$ DATE $, \mathrm{X}, \mathrm{FF}(\mathrm{X}), \mathrm{TX}, \mathrm{TAIR}, \mathrm{EZ}, \mathrm{RA}, \mathrm{RE}, \mathrm{TSOIL}$
$x=x 2$
$\mathrm{TX}=\mathrm{Y} 2$
$\mathrm{EZ}=\mathrm{Z} 2$
CALL COMPT
WRITE $(6,13)$ DATE $, \mathrm{X}, \mathrm{FF}(\mathrm{X}), \mathrm{TX}, \mathrm{TAIR}, \mathrm{EZ}, \mathrm{RA}, \mathrm{RE}, \mathrm{TSOIL}$
IF (X3.CE.24.0) GO TO 25
$\mathrm{X} 1=\mathrm{X} 2$
$\mathrm{Y} 1=\mathrm{Y} 2$
$\mathrm{Zl}=\mathrm{Z} 2$
$\mathrm{X} 2=\mathrm{X} 3$
$\mathrm{Y} 2=\mathrm{Y} 3$
$\mathrm{Z} 2=\mathrm{Z} 3$
$\operatorname{READ}(5,19) \mathrm{X} 3, \mathrm{Y} 3, \mathrm{Z} 3$
19 FORMAT (3X,F3.0,F4.0,FB. 4
DIFFY $=Y \mathrm{Y}-\mathrm{YI}$
DIFFX $=\mathrm{X} 2-\mathrm{X} 1$
DIFFZ $=$ Z2-Z1
SUMX $=\mathrm{X} 1+\mathrm{X} 2$
$\mathrm{C}=[(\mathrm{Y} 3-\mathrm{Yx})$ *DIFFX-DIFFY* $(\mathrm{X} 3-\mathrm{X} 2)] /[(\mathrm{X} 3-\mathrm{X} 2) * \mathrm{DIFFX} *(\mathrm{X} 3-\mathrm{X} 1)]$
$\mathrm{B}=\mathrm{DIFFY} /$ DIFFX - C*SUMX
$\mathrm{CE}=[(\mathrm{Z} 3-\mathrm{Z2}) * \mathrm{DIFFX}-\mathrm{DIFFZ} *(\mathrm{X} 3-\mathrm{X} 2)] /[(\mathrm{X} 3-\mathrm{X} 2) * \operatorname{DIFFX} *(\mathrm{X} 3-\mathrm{X} 1)]$
BE=DIFFZ/DIFFX-CE*SUMX
$\mathrm{AE}=\mathrm{Z1}-(\mathrm{BE}+\mathrm{CE} * \mathrm{Xl}) * \mathrm{X} 1$
GO TO 14
$25 \quad \mathrm{X}=21$
DO $30 \mathrm{I}=1,3$
$T X=A+(B+C * X) * X$
$\mathrm{EZ}=\mathrm{AE}+(\mathrm{BE}+\mathrm{CE} * \mathrm{X}) * \mathrm{X}$
CALL COMPT

WRITE $(6,13)$ DATE, $\mathrm{X}, \mathrm{FF}(\mathrm{X}), \mathrm{TX}, \mathrm{TAIR}, \mathrm{EZ}, \mathrm{RA}, \mathrm{RE}, \mathrm{TSOIL}$
$\mathrm{X}=\mathrm{x}+1$
30 CONTINUE
$\mathrm{X}=\mathrm{X} 3$
$\mathrm{TX}=\mathrm{Y} 3$
EZ=Z3
CALL COMPT
WRITE $(6,13)$ DATE, $X, F F(X), T X, T A I R, E Z, R A, R E, T S O I L$
GO TO 5
99 STOP
END

SUBROUTINE COMPT
COMMON FF (24), ALPHA, BETA, GAMMA, DELTA, EPSLN, TX, TAIR, RA, RE, TSOIL, EZ
COMMON X, DELEP
TAIR $=(T X-32.0) * 5.0 / 9.0+273.0$
RA=DELTA*TAIR**4*[ALPHA-BETA/10.0** (GAMMA*EZ)]
$\mathrm{RE}=\mathrm{FF}(\mathrm{X}) * 0.84+\mathrm{RA}$
TSOIL=(RE/DELEP)**0.25
RETURN
END

## Appendix B

Computer Program of Temperature Model

```
DIMENSION B(25),G(25),H(25),E(25),F(25),V(24)
K=16
KK=K+1
READ (5,1) (G(I),I=1,KK
READ(5,1) (B (I), I=1,KK
WRITE (6,5)
WRITE (6,4)(B(I),I=1,KK)
WRITE (6,7)
WRITE (6,4) (G(I), I=1,KKO
WRITE (6,9)
READ(5,1) V
H(1)=V(1)
H(KK)=G(KK)
DELX=10
DELT=1
N}=
AL=0.5
BT=1.0-AL
POT=DELT/ (DELX*DELX)
C--COMPUTATION OF TRIDIAGONAL MATRIX
38 DO 46 I=2,K
```

```
BB=BT*POT*[B(I)+B(I-1)]+1.0
DD=POT*AL*(B(I-1)*(G(I-1)_G(I))-B(I)*(G(I)-G(I+1)))+G(I)
IF(1.GT.2) GO TO 44
DD=DD+BT* }\textrm{B}(\textrm{I}-1)*POT*G(I-1
F(I)=DD/BB
E(I)=B(I)*BT*POT/BB
GO TO 46
4 4 ~ I F ( I . G E . K ) ~ G O ~ T O ~ 4 7 ~
E(I)=BT*B(I)*POT/[SB-BT*B (I-1)*POT*E(I-1)]
F(I)=[DD+BT*B(I-1_*POT*F(I-1)]/[BB-ST*B(I-1)*POT*E(I-1)]
4 6 ~ C O N T I N U E ~
4 7 \mathrm { DD } = \mathrm { DD } + \mathrm { G } ( \mathrm { L } + 1 ) * B T * B ( I ) * P O T
H(I)}=[DD+BT**B(I-1)*POT*F(IO1)]/[BB-BT*B(I-1)*POT*E(IP1)] [
4 8 ~ I = I - 1
H(I)=E(I)*H(I+1)+F(I)
IF(I.GT.2) GO TO 48
CTIME=CTIME+DELT
WRITE (6, 2) CTIME, (H(I) , I=1,KK)
IF(CTIME.GE.24.0) GO TO 6
H(I)=V(N)
N}=\textrm{N}+
DO 3 I=1,K
3 G(I)=H(I)
GO TO 38
1 FORMAT(14F5.1)
2 FORMAT(25F5.1)
4 FORMAT(5X,25F5.1)
```

5 FORMAT (45X,1H, 'DIFFUSIVITY VALUES')
7 FORMAT (40X,1H, 'INITIAL PROFILE TEMPERATURES')
9 FORMAT ( $48 \mathrm{X}, 1 \mathrm{H},{ }^{\prime}$ COMPUTED DATA')
6 STOP

END

## Appendix C

Table 19. Data of observed surface and subsoil temperature (in ${ }^{\circ} \mathrm{C}$ ) at Curlew Valley (experimental site) on July 7, 1973.

| Hours | Depth (in cm) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 2 | 10 | 25 | 50 | 150 |
| 0 | 17.00 | 23.50 | 27.00 | 24.50 | 19.00 | 12.50 |
| 1 | 15.25 | 22.00 | 26.25 | 24.50 | 19.00 | 12.50 |
| 2 | 14.50 | 20.75 | 25.50 | 24.50 | 19.00 | 12.50 |
| 3 | 12.00 | 19.00 | 24.75 | 24.50 | 19.25 | 12.50 |
| 4 | 11.75 | 17.75 | 24.00 | 24.25 | 19.25 | 12.50 |
| 5 | 9.50 | 16.50 | 23.00 | 24.00 | 19.25 | 12.50 |
| 6 | 8.25 | 15.00 | 22.50 | 24.75 | 19.25 | 12.50 |
| 7 | 9.50 | 14.25 | 21.75 | 23.50 | 19.25 | 12.50 |
| 8 | 18.25 | 15.50 | 21.00 | 23.25 | 19.25 | 12.50 |
| 9 | 31.25 | 21.75 | 20.75 | 23.00 | 19.25 | 12.50 |
| 10 | 43.00 | 28.25 | 21.00 | 22.75 | 19.25 | 12.50 |
| 11 | 53.75 | 34.25 | 21.75 | 22.50 | 19.25 | 12.25 |
| 12 | 62.25 | 40.00 | 22.75 | 22.00 | 19.00 | 12.25 |
| 13 | 69.50 | 45.00 | 24.50 | 22.00 | 19.00 | 12.25 |
| 14 | 69.00 | 48.50 | 26.75 | 22.00 | 19.00 | 12.50 |
| 15 | 66.75 | 49.25 | 27.25 | 22.00 | 19.00 | 12.25 |
| 16 | 63.75 | 49.25 | 29.25 | 22.50 | 19.25 | 12.50 |
| 17 | 58.00 | 48.00 | 30.25 | 23.00 | 19.25 | 12.50 |
| 18 | 49.25 | 45.75 | 31.00 | 23.35 | 19.25 | 12.50 |
| 19 | 37.75 | 40.75 | 31.00 | 23.75 | 19.25 | 12.50 |
| 20 | 29.75 | 35.50 | 30.75 | 24.00 | 19.25 | 12.50 |
| 21 | 23.00 | 31.25 | 30.00 | 24.25 | 19.00 | 12.50 |
| 22 | 19.25 | 27.25 | 29.25 | 24.50 | 19.25 | 12.50 |
| 23 | 17.00 | 25.00 | 28.25 | 24.50 | 19.25 | 12.50 |
| 24 | 15.25 | 23.00 | 27.25 | 24.50 | 19.00 | 12.50 |

## Appendix C

Table 20. Data of observed surface and subsoil temperature (in ${ }^{\circ} \mathrm{C}$ ) at Curlew Valley (experimental site) on July 9, 1973.

| Hours | Depth (in cm) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 2 | 10 | 25 | 50 | 150 |
| 0 | 16.75 | 25.25 | 28.00 | 24.50 | 19.25 | 12.50 |
| 1 | 14.75 | 22.75 | 27.50 | 24.75 | 19.50 | 12.75 |
| 2 | 12.75 | 20.75 | 26.50 | 24.75 | 19.50 | 12.75 |
| 3 | 12.25 | 19.00 | 25.50 | 24.75 | 19.50 | 12.75 |
| 4 | 10.75 | 17.75 | 24.50 | 24.50 | 19.00 | 12.75 |
| 5 | 10.00 | 16.50 | 23.75 | 24.50 | 19.00 | 12.75 |
| 6 | 9.25 | 15.50 | 23.00 | 24.25 | 19.00 | 12.75 |
| 7 | 8.75 | 14.50 | 22.25 | 24.00 | 19.00 | 12.75 |
| 8 | 8.50 | 14.00 | 21.50 | 23.50 | 19.00 | 12.75 |
| 9 | 11.25 | 14.00 | 21.00 | 23.50 | 19.00 | 12.75 |
| 10 | 21.25 | 16.25 | 20.50 | 23.00 | 19.00 | 12.75 |
| 11 | 35.00 | 23.00 | 20.25 | 22.75 | 19.00 | 12.75 |
| 12 | 48.00 | 30.50 | 20.75 | 22.50 | 19.00 | 12.75 |
| 13 | 55.50 | 36.50 | 21.50 | 22.00 | 19.25 | 12.50 |
| 14 | 62.25 | 42.00 | 23.00 | 22.00 | 19.25 | 12.50 |
| 15 | 69.25 | 46.50 | 24.75 | 21.75 | 19.25 | 12.50 |
| 16 | 71.00 | 49.75 | 26.50 | 21.75 | 19.25 | 12.50 |
| 17 | 69.50 | 51.00 | 28.25 | 22.00 | 19.25 | 12.50 |
| 18 | 63.50 | 50.25 | 29.50 | 22.25 | 19.25 | 12.50 |
| 19 | 57.00 | 49.00 | 30.50 | 22.50 | 19.25 | 12.50 |
| 20 | 47.75 | 45.50 | 31.00 | 23.00 | 19.25 | 12.50 |
| 21 | 36.50 | 40.75 | 31.00 | 23.25 | 19.00 | 12.50 |
| 22 | 29.00 | 35.50 | 30.75 | 23.75 | 19.00 | 12.50 |
| 23 | 22.00 | 31.25 | 30.25 | 24.00 | 19.25 | 12.75 |
| 24 | 18.00 | 27.75 | 29.50 | 24.50 | 19.25 | 12.75 |

## Appendix C

Table 21. Data of observed surface and subsoil temperature (in ${ }^{\circ} \mathrm{C}$ ) at Curlew Valley (experimental site) on August 1, 1973.

| Hours | Depth (in cm ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 2 | 10 | 25 | 50 | 150 |
| 0 | 12.25 | 19.25 | 25.50 | 23.50 | 18.75 | 13.50 |
| 1 | 10.50 | 18.00 | 24.75 | 23.50 | 18.50 | 13.50 |
| 2 | 10.00 | 16.75 | 24.25 | 24.00 | 19.00 | 14.00 |
| 3 | 8.50 | 15.75 | 23.50 | 24.00 | 19.25 | 14.25 |
| 4 | 8.50 | 14.50 | 22.50 | 23.75 | 19.00 | 14.25 |
| 5 | 8.25 | 14.25 | 21.25 | 23.25 | 18.75 | 14.25 |
| 6 | 7.25 | 13.50 | 20.25 | 23.00 | 19.00 | 14.25 |
| 7 | 8.00 | 12.75 | 19.75 | 22.50 | 18.75 | 14.25 |
| 8 | 13.25 | 13.25 | 18.25 | 21.25 | 17.25 | 13.25 |
| 9 | 25.75 | 18.50 | 19.25 | 22.25 | 19.20 | 14.50 |
| 10 | 37.75 | 24.50 | 19.50 | 22.00 | 19.75 | 14.50 |
| 11 | 48.00 | 30.50 | 20.75 | 21.75 | 20.00 | 14.50 |
| 12 | 53.25 | 35.50 | 22.50 | 21.50 | 20.50 | 14.50 |
| 13 | 56.50 | 38.75 | 24.25 | 21.25 | 20.75 | 14.25 |
| 14 | 61.50 | 42.00 | 26.50 | 21.25 | 21.00 | 14.25 |
| 15 | 62.50 | 43.75 | 28.25 | 21.50 | 22.00 | 14.25 |
| 16 | 60.25 | 44.75 | 29.75 | 22.00 | 22.50 | 14.25 |
| 17 | 55.75 | 44.50 | 31.00 | 22.50 | 23.00 | 14.25 |
| 18 | 46.25 | 42.00 | 32.25 | 23.25 | 23.75 | 14.50 |
| 19 | 36.00 | 38.25 | 32.25 | 24.00 | 23.75 | 14.50 |
| 20 | 28.75 | 33.25 | 32.00 | 24.25 | 23.25 | 14.50 |
| 21 | 22.25 | 30.25 | 31.25 | 24.75 | 22.50 | 14.50 |
| 22 | 18.50 | 26.00 | 30.00 | 25.00 | 22.00 | 14.50 |
| 23 | 16.50 | 23.50 | 28.75 | 25.25 | 22.00 | 14.50 |
| 24 | 15.00 | 21.75 | 27.75 | 25.25 | 21.75 | 14.00 |

## Appendix D

Table 22. Data of observed global radiation $\left(R_{S}+R_{D}\right)$, net radiation $\left(R_{N}\right)$, and albedo $\left(R_{S}+R_{D}\right) \alpha$, and calculated net long-wave radiation ( $R_{A}-R_{E}$ ), in ly/min, at Curlew Valley (experimental site) on July 7, 1973.

|  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Hours | $R_{S}+R_{D}$ | $R_{N}$ | $\left(R_{S}+R_{\mathcal{D}}\right) \alpha$ | $R_{A}-R_{E}$ |
|  |  |  |  |  |
| 1 |  | -0.1340 |  | -0.1340 |
| 2 |  | -0.2305 |  | -0.1205 |
| 3 |  | -0.1195 |  | -0.1195 |
| 4 | 0.0648 | -0.1270 |  | -0.1270 |
| 5 | 0.3015 | 0.1150 | 0.0104 | -0.1294 |
| 6 | 0.5703 | 0.3290 | 0.0480 | -0.1200 |
| 7 | 1.0185 | 0.5090 | 0.0912 | -0.1800 |
| 8 | 1.2446 | 0.6714 | 0.1699 | -0.2200 |
| 9 | 1.3513 | 0.7955 | 0.1991 | -0.2500 |
| 10 | 1.3874 | 0.8700 | 0.2162 | -0.2651 |
| 11 | 1.2426 | 0.8800 | 0.2219 | -0.2800 |
| 12 | 1.0591 | 0.8650 | 0.2168 | -0.2700 |
| 13 | 0.8249 | 0.8150 | 0.1988 | -0.2300 |
| 14 | 0.5575 | 0.7116 | 0.1694 | -0.2100 |
| 15 | 0.2902 | 0.5130 | 0.1319 | -0.1800 |
| 16 | 0.0600 | 0.3180 | 0.0892 | -0.1500 |
| 17 |  | 0.1238 | 0.0464 | -0.1200 |
| 18 | -0.0790 | 0.0006 | -0.1300 |  |
| 19 |  | -0.1200 |  | -0.1200 |
| 20 |  | -0.1200 |  | -0.1200 |
| 21 |  |  |  | -0.1160 |

## Appendix D

Table 23. Data of observed global radiation $\left(R_{S}+R_{D}\right)$, net radiation $\left(R_{N}\right)$, and albedo $\left(R_{S}+R_{D}\right) \alpha$, and calculated net long-wave radiation $\left(R_{A}-R_{E}\right)$, in $1 y / m i n$, at Curlew Valley (experimental site) on July 9, 1973.

| Hours | $R_{S}+R_{D}$ | $R_{N}$ | $\left(R_{S}+R_{D}\right) \alpha$ | $R_{A}-R_{E}$ |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |
| 1 |  | -0.0970 |  | -0.0970 |
| 2 |  | -0.0935 |  | -0.0935 |
| 3 |  | -0.0925 |  | -0.0925 |
| 4 | 0.0844 | -0.0880 |  | -0.0880 |
| 5 | 0.2965 | 0.1530 | 0.0135 | -0.0949 |
| 6 | 0.5689 | 0.3479 | 0.0470 | -0.0961 |
| 7 | 0.8344 | 0.5309 | 0.0910 | -0.1300 |
| 8 | 1.0655 | 0.6950 | 0.1705 | -0.1700 |
| 9 | 1.3382 | 0.8073 | 0.1981 | -0.2000 |
| 10 | 1.3861 | 0.8480 | 0.2157 | -0.2328 |
| 11 | 1.3379 | 0.8532 | 0.2217 | -0.3112 |
| 12 | 1.0242 | 0.8314 | 0.2140 | -0.2925 |
| 13 | 0.7900 | 0.7664 | 0.1939 | -0.2520 |
| 14 | 0.5100 | 0.6504 | 0.1638 | -0.2100 |
| 15 | 0.2700 | 0.5036 | 0.1264 | -0.1600 |
| 16 | 0.0350 | 0.3084 | 0.0816 | -0.1200 |
| 17 |  | 0.1370 | 0.0430 | -0.0900 |
| 18 | -0.0566 | 0.0056 | -0.0860 |  |
| 19 |  | -0.1131 |  | -0.1131 |
| 20 |  | -0.1033 |  | -0.1033 |

## Appendix D

Table 24. Data of observed global radiation ( $R_{S}+R_{D}$ ), net radiation ( $R_{N}$ ), and albedo $\left(R_{S}+R_{D}\right) \alpha$, and calculated net long-wave radiation $\left(R_{A}-R_{E}\right)$, in $1 y / m i n$, at Curlew Valley (experimental site) on August 1, 1973.

| Hours | $R_{S}+R_{D}$ | $R_{N}$ | $\left(R_{S}+R_{D}\right) \alpha$ | $R_{A}-R_{E}$ |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |
|  |  | -0.0980 |  | -0.0980 |
| 1 |  | -0.0900 |  | -0.0900 |
| 2 |  | -0.0954 |  | -0.0954 |
| 3 |  | -0.0954 |  | -0.0954 |
| 4 | 0.0627 | 0.0588 | 0.0100 | -0.1115 |
| 5 | 0.2533 | 0.0899 | 0.0405 | -0.1229 |
| 6 | 0.5400 | 0.3430 | 0.0864 | -0.1133 |
| 7 | 0.7927 | 0.5159 | 0.1268 | -0.1500 |
| 8 | 1.0276 | 0.6727 | 0.1644 | -0.1900 |
| 9 | 1.2054 | 0.7934 | 0.1928 | -0.2192 |
| 10 | 1.3087 | 0.8700 | 0.2093 | -0.2294 |
| 11 | 1.3106 | 0.87245 | 0.2147 | -0.25475 |
| 12 | 1.2036 | 0.8314 | 0.2096 | -0.2696 |
| 13 | 1.0246 | 0.74255 | 0.1925 | -0.26605 |
| 14 | 0.7976 | 0.63375 | 0.1639 | -0.2269 |
| 15 | 0.5399 | 0.4908 | 0.2376 | -0.1792 |
| 16 | 0.2700 | 0.2999 | 0.0860 | -0.1540 |
| 17 | 0.0500 | 0.0722 | 0.0432 | -0.1546 |
| 18 |  | -0.0986 | 0.0080 | -0.1406 |
| 19 |  | -0.1298 |  | -0.1298 |
| 20 |  | -0.1127 |  | -0.1127 |
| 21 |  | -0.1099 |  | -0.1099 |

## Appendix E

Table 25. Data of observed air temperature (in ${ }^{\circ} \mathrm{C}$ ) at Curlew Valley (experimental site) on July 7, 1973.

| Hours | Height (in cm) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 800 | 400 | 200 | 100 | 50 | 20 | 5 | 5 (shade) |
| 1 | 19.25 | 19.00 | 18.25 | 8.00 | -1.25 | 17.50 | 17.75 | 17.00 |
| 2 | 19.00 | 18.00 | 16.50 | 6.50 | -3.25 | 14.75 | 14.25 | 14.50 |
| 3 | 16.25 | 15.75 | 14.25 | 5.50 | -4.50 | 14.00 | 11.00 | 11.75 |
| 4 | 14.75 | 14.50 | 14.00 | 5.00 | -3.50 | 12.75 | 12.50 | 12.75 |
| 5 | 13.25 | 12.00 | 10.75 | 2.00 | -6.00 | 9.00 | 8.75 | 8.50 |
| 6 | 12.50 | 10.25 | 10.00 | 0.50 | -6.25 | 8.50 | 8.25 | 7.50 |
| 7 | 11.25 | 11.00 | 10.00 | 1.75 | $-3.50$ | 11.50 | 11.00 | 10.75 |
| 8 | 17.50 | 17.50 | 17.50 | 8.00 | -0.25 | 18.75 | 18.50 | 18.75 |
| 9 | 21.25 | 21.00 | 21.50 | 10.75 | 1.75 | 23.50 | 23.00 | 24.00 |
| 10 | 23.50 | 24.50 | 26.00 | 26.75 | 1.75 | 28.00 | 29.50 | 28.75 |
| 11 | 25.00 | 25.00 | 25.25 | 27.50 | 5.25 | 32.25 | 33.50 | 34.00 |
| 12 | 27.25 | 27.00 | 27.00 | 16.00 | 5.50 | 30.00 | 36.50 | 32.00 |
| 13 | 30.00 | 30.25 | 30.00 | 18.00 | 5.75 | 30.75 | 39.75 | 34.50 |
| 14 | 30.50 | 30.75 | 30.50 | 17.00 | 6.50 | 32.75 | 39.00 | 39.00 |
| 15 | 30.75 | 33.00 | 34.00 | 21.75 | 7.75 | 36.50 | 37.75 | 38.25 |
| 16 | 31.00 | 34.00 | 34.75 | 20.50 | 6.50 | 38.25 | 39.25 | 39.50 |
| 17 | 32.00 | 32.50 | 33.50 | 20.50 | 6.75 | 37.25 | 36.75 | 38.25 |
| 18 | 33.50 | 33.25 | 32.75 | 20.00 | 6.25 | 36.50 | 33.75 | 37.25 |
| 19 | 32.25 | 32.25 | 32.50 | 19.75 | 5.75 | 34.00 | 34.50 | 34.75 |
| 20 | 31.50 | 32.00 | 32.00 | 19.00 | 5.25 | 33.00 | 31.25 | 31.75 |
| 21 | 28.75 | 28.00 | 27.25 | 13.75 | 1.75 | 20.50 | 19.75 | 20.25 |
| 22 | 21.75 | 20.75 | 20.00 | 9.00 | -1.25 | 19.00 | 18.50 | 21.75 |
| 23 | 21.50 | 21.00 | 19.50 | 8.50 | -2.75 | 15.25 | 14.25 | 14.25 |
| 24 | 19.75 | 17.25 | 16.00 | 8.75 | -0.50 | 14.75 | 14.75 | 14.25 |

