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26 **Abstract**

27 Pressure retarded osmosis (PRO) process is hindered by severe fouling  
28 occurred within porous support of the FO membranes. We designed a novel  
29 double-skinned FO membrane containing a polyamide salt-rejecting layer and  
30 a zwitterionic brushes-decorated, multi-walled carbon nanotube  
31 (MWCNT/PSBMA) foulant-resisting layer on the back side. Our results  
32 demonstrated that the coating of MWCNT/PSBMA layer on the porous  
33 polyketone (PK) support imparted enhanced hydrophilicity and smaller  
34 membrane pore size, thereby providing excellent resistance toward both  
35 protein adhesion and bacterial adsorption. We also further evaluated this  
36 resultant double-skinned membrane (i.e., TFC-MWCNT/PSBMA) in dynamic  
37 PRO fouling experiments, using protein and alginate as model organic foulants.  
38 Comparing to the pristine TFC-PK and hydrophobic TFC-MWCNT membranes,  
39 the TFC-MWCNT/PSBMA membrane exhibited not only the lowest water flux  
40 decline but also the highest water flux recovery after simple physical flushing.  
41 These results shed light on fabrication of antifouling PRO membranes for water  
42 purification purposes.

43 **Keywords:** Forward osmosis; Double-skinned composite membrane; Anti-  
44 fouling; zwitterionic brushes; MWCNT

45

## 46 **Introduction**

47 With growing global water scarcity, forward osmosis (FO), as a new kind  
48 of membrane-based process, has been widely applied in many areas, such as  
49 industrial wastewater treatment, seawater desalination, and power generation<sup>1-  
50 6</sup>. In an FO process, water permeation is osmotic pressure-driven rather than  
51 hydraulic pressure. Therefore, FO process has the advantages of higher water  
52 recovery and higher fouling reversibility compared to other pressure-driven  
53 membrane processes (e.g. NF or RO)<sup>7-9</sup>.

54 Thin-film composite (TFC) membranes containing a thick porous support  
55 and a thin polyamide (PA) selective layer, are the predominant membrane  
56 materials of the FO process up to date<sup>10</sup>. Generally, the FO membrane water  
57 flux in pressure retarded osmosis (PRO) mode (polyamide layer facing to draw  
58 solution) is much higher than the water flux in FO mode (polyamide layer facing  
59 to feed solution) because of the suppressed internal concentration polarization  
60 (ICP)<sup>11</sup>. However, TFC FO membranes suffer from severer membrane fouling  
61 in PRO mode due to the blockage of foulants within the porous support and  
62 difficulty in membrane cleaning<sup>12-13</sup>. Therefore, FO process is chosen  
63 preferentially to be manipulated under the FO mode for avoiding the membrane  
64 fouling, even though the ICP significantly lowers the water flux<sup>12</sup>. Recent  
65 studies highlighted the significance of redesigning support structures to  
66 maximize the water flux in FO process<sup>14-18</sup>; as such, it is of paramount  
67 importance to the development of FO membranes with superior antifouling

68 properties in PRO mode.

69 In order to prevent the entry of foulants to the support, constructing an  
70 antifouling “barrier” layer on the TFC membrane back side is considered as the  
71 most effective approach to alleviate membrane fouling in PRO mode<sup>19-21</sup>.  
72 However, technical obstacles to fabricate such a dense layer on the back side  
73 are posed by the typical preparation methods of TFC membranes, such as  
74 phase separation or interfacial polymerization. So far, extensive studies have  
75 attempted to graft soft polymer brushes (e.g. zwitterionic polymer) on the back  
76 side to control the fouling in PRO mode<sup>22,23</sup>. These polymer brushes possess  
77 strong hydrophilicity and excellent resistance towards foulants caused by their  
78 electrostatically induced hydration capacity<sup>24</sup>. However, the large pores with  
79 sizes ranging from hundreds of nanometers to a few micrometers on the TFC  
80 membrane back side cannot be fully covered with soft polymer brushes with  
81 current surface modification approaches. As a result, there is an imperative  
82 need to design novel surface modification techniques to specifically block the  
83 accumulation of foulants inside the porous support.

84 Carbon nanotubes (CNTs) have a stable physical and chemical properties,  
85 an appropriate mechanical strength and larger length-to-diameter ratio, which  
86 have been used in the preparation of the self-supported CNTs filtration  
87 membrane<sup>25-28</sup>, and CNTs incorporated thin film nanocomposite membranes<sup>29-  
88 32</sup>. Better water permeability as well as enhanced anti-fouling capability was  
89 usually achieved for these fabricated membranes. Inspired by these studies,

90 we hypothesize that CNTs can be assembled on the back side of a TFC  
91 membrane to alleviate the PRO fouling. The aim of this work is to develop a  
92 novel anti-fouling, double-skinned FO membrane containing a polyamide salt-  
93 rejecting layer and a zwitterionic brushes-decorated, multi-walled carbon  
94 nanotube (MWCNT) foulant-resisting layer. Fouling resistance of the fabricated  
95 double-skinned membranes were assessed by static adsorption tests of BSA  
96 and *E.coli*. Dynamic fouling experiments further confirmed the effective  
97 membrane fouling control in PRO mode by coating a zwitterionic brushes-  
98 decorated MWCNT layer on the TFC membrane back side.

99

## 100 **Materials and Methods**

101 **Materials and Chemicals.** Polyketone (PK,  $M_w=400,000 \text{ g mol}^{-1}$ ) was  
102 obtained from Asahi Kasei Corporation (Japan). Acetone, resorcinol, hexane,  
103 and methanol were provided from Wako Pure Chemical Co. (Japan) to fabricate  
104 the PK support. 1,3,5-Benzenetricarbonyl trichloride (TMC), 1,3-  
105 Phenylenediamine (MPD), Triethylamine (TEA), Sodium dodecyl sulfate (SDS),  
106 Hexamethylphosphoric triamide (HMPA), and 10-camphorsulfonic acid (CSA)  
107 were ordered from Tokyo Kasei Co. (Japan) to fabricate the polyamide layer.  
108 Sodium dodecyl benzene sulfonate (SDBS), bovine serum albumin (BSA),  
109 multi-walled carbon nanotube (MWCNT) and alginate were obtained from  
110 Sigma-Aldrich Co. (USA). Dopamine hydrochloride (DA), [2-  
111 (Methacryloyloxy)ethyl]dimethyl-(3-sulfopropyl)ammonium hydroxide (SBMA),

112 2-Bromo-2-methylpropionyl bromide (BiBB), N,N-dimethylformamide (DMF), L-  
113 ascorbic acid, Tris(2-pyridylmethyl)amine (TPMA), Copper(II) chloride and  
114 Tris(hydroxymethyl)aminomethane (Tris) were purchased from J&K Scientific  
115 Ltd. (China).

116 In the protein adsorption test, NaH<sub>2</sub>PO<sub>4</sub> and Na<sub>2</sub>HPO<sub>4</sub> was used to prepare  
117 the phosphate buffer solution (PBS, 0.2 mol/L, pH=7) (Wako, Japan). Albumin-  
118 fluorescein isothiocyanate conjugate BSA (FITC-BSA) and Escherichia coli  
119 (*E.coli*) (Sigma-Aldrich, USA) were chosen as model protein and bacteria,  
120 respectively. Tryptic soy broth (TSB; Becton, Dickinson and Co., USA) was  
121 employed as culture medium. SYTO9 (Life Technologies, USA) was chosen to  
122 stain the bacteria.

123

#### 124 **Zwitterionic brushes-decorated MWCNT dispersion preparation.**

125 Zwitterionic brushes-decorated MWCNT was prepared by grafting PSBMA  
126 brushes on the MWCNT via atom-transfer radical-polymerization (ATRP)  
127 methods as shown in **Figure 1**<sup>33</sup>. The grafting yield (GY) was 21%, which was  
128 calculated according to the following equation:

$$129 \text{ GY} = \frac{W_b - W_a}{W_a} \times 100\%$$

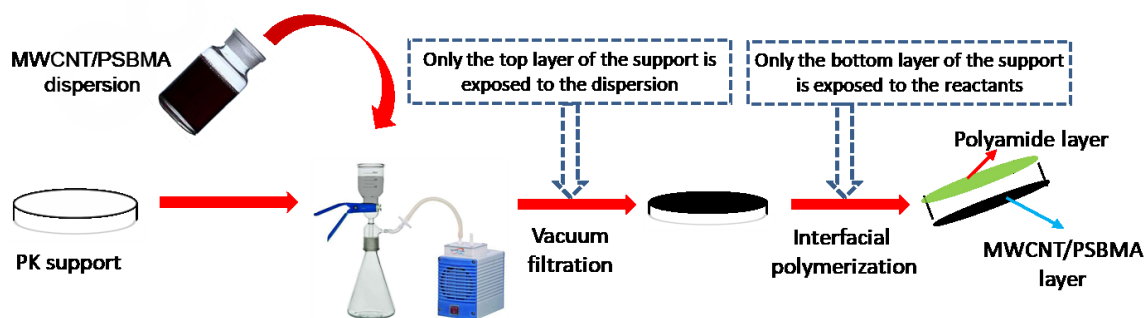
130 where  $W_a$  is the dried MWCNT weight and  $W_b$  is the dried PSBMA modified  
131 MWCNT weight. The detailed modification procedures are shown in the  
132 Supporting Information. The PSBMA brushes grafted MWCNT is designated as  
133 MWCNT/PSBMA and their FT-IR spectra are presented in **Figure S1**. The





155 homogeneous. After degassed at 50 °C overnight, this homogenous solution  
156 was casted in a height of 300 μm on the neat glass plate and then the whole  
157 composite was soaked in a methanol/water (3.5/6.5, w/w) bath for 20 min. The  
158 resultant porous PK membrane was sequentially soaked in acetone for 20 min  
159 and in hexane for another 20 min, and finally taken out for drying. The  
160 illustration of the PK support fabrication step is shown in **Figure S2** (Supporting  
161 Information).

162 **Figure 2** illustrated the schematic procedure for the preparation of double-  
163 skinned FO membrane. Firstly, coating the MWCNT/PSBMA layer on the PK  
164 support top side was performed by vacuum-filtered MWCNT/PSBMA  
165 dispersion (5 mL) through the PK support<sup>35</sup>. Subsequently, the polyamide layer  
166 was interfacial polymerized via the reaction of MPD and TMC on the other side  
167 (bottom side) of the PK support according to our previous study<sup>34</sup>. Briefly, the  
168 bottom layer of PK support was first exposed to the aqueous MPD solution (1.1  
169 wt% TEA, 2.0 wt% MPD, 0.15 wt% SDS, 3.0 wt% HMPA, and 2.3 wt% CSA in  
170 water) for 5 min and then followed by wiping the solution from the membrane  
171 surface. After that, 0.15 wt% TMC in hexane solution was covered over the  
172 bottom layer of PK support for 2 min. The resultant polyamide layer was further  
173 deep crosslinked at 90 °C for 10 min and then stored in DI water for future usage.  
174 These double-skinned membranes based on different second skin layer (e.g.  
175 PK layer, MWCNT layer and MWCNT/PSBMA layer) are designated as TFC-  
176 PK, TFC-MWCNT and TFC-MWCNT/PSBMA membranes, respectively.



177

178 **Figure 2.** Lab scale fabrication steps for the double-skinned FO membrane.

179

180 **Membrane Characterizations.** Membrane surface morphologies were  
 181 determined by an atomic force microscopy (AFM, SPA-400, Japan) and a field-  
 182 emission scanning electron microscope (FE-SEM, JSF-7500, Japan). The  
 183 membrane surface elemental content was quantified by X-ray photo electron  
 184 spectroscopy (XPS, JPS-9010MC, JEOL). The surface zeta potential was  
 185 determined by a SurPASS<sup>TM</sup> 3 electrokinetic analyzer (Anton Paar, Austria) in  
 186 a background electrolyte solution (75 mg/L KCl solution). The membrane  
 187 surface hydrophilicity was characterized by a contact angle meter (DM-300,  
 188 Japan).

189 A cross-flow RO setup was employed to evaluate the water permeability  
 190 ( $A$ ,  $L \cdot m^{-2} \cdot h^{-1} \cdot bar^{-1}$ ), salt permeability ( $B$ ,  $L \cdot m^{-2} \cdot h^{-1}$ ) and salt rejection rate ( $R_s$ , %)  
 191 of the FO membranes<sup>36</sup>. Structural parameter ( $S$ ,  $\mu m$ ) can be calculated by  
 192 fitting the  $A$  and  $B$  values with the FO water flux ( $J_v$ ,  $L \cdot m^{-2} \cdot h^{-1}$ )<sup>36</sup>. Detailed  
 193 information on filtration experiments is described in the Supporting Information.

194

195 **Static Adhesion Tests.** Anti-fouling abilities of the fabricated membranes

196 were assessed by the static adhesion tests of BSA and *E. coli*<sup>37</sup>. FITC-BSA  
197 solution (20 mg/L, pH=7.4) was prepared in a 0.2 mol/L PBS buffer. Membrane  
198 samples (0.5 cm x 2 cm) were first soaked into the 2 mL FITC-BSA solution and  
199 then shaken at 100 rpm in the dark place for 12 hours. After that, these  
200 membrane samples were taken out and then washed twice with fresh PBS  
201 buffer. Confocal laser scanning microscopy (CLSM; FV1000D, Japan) was  
202 employed to take the fluorescence images.

203 Membrane adhesion property for bacteria was also evaluated by the static  
204 *E.coli* adhesion test as described in reference<sup>37</sup>. First, *E.coli* were precultured  
205 in 20 mL of 30 g/L TBS medium overnight at 30 °C. And then, 30 g/L TSB  
206 medium was used to dilute the *E.coli* suspension 50 times. Next, this *E.coli*  
207 suspension was cultivated for another 4 h until its optical density at 450 nm  
208 reached to 0.05. Membrane samples (0.5 cm × 2.0 cm) were soaked in the  
209 above-prepared *E.coli* suspension (2 mL, pH=7) and shaken at 30 °C for 24 h.  
210 After that, these membrane samples were washed twice by 0.85 wt% NaCl  
211 solution and followed by sequentially soaked in the salty SYTO9 solution (0.85  
212 wt% NaCl) for 20 min, and 2.5 wt% glutaraldehyde solution for 3 min to dye and  
213 fix the bacteria, respectively. The resultant membranes were washed and  
214 stored in 0.85 wt% NaCl solution until the characterization by using CLSM. The  
215 Image J software (National Institutes of Health, MD, USA) was employed to  
216 calculate the bacteria coverage.

217

218 **Membrane Fouling Protocol in PRO mode.** A cross-flow FO setup was  
219 employed to perform the dynamic fouling experiments in PRO mode (polyamide  
220 layer facing to the draw solution) at ambient pressure<sup>19</sup>. In this work, the feed  
221 solution at ambient pressure could reflect the PRO operating environment,  
222 where no hydraulic pressure is applied in the feed side and the draw side is  
223 pressured<sup>38</sup>. All experiments were started with 30 mg/L foulants (BSA or  
224 alginate), 0.5 mmol/L CaCl<sub>2</sub> and 50 mmol/L NaCl in the feed solution, and an  
225 initial water flux of  $\sim 30 \text{ L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$ , which was accomplished by controlling the  
226 NaCl concentration of draw solution side. The temperature and crossflow  
227 velocity of both feed and draw solutions were set at  $25 \pm 2 \text{ }^\circ\text{C}$  and 8.5 cm/s,  
228 respectively. The fouling experiments were conducted for 10 to 20 hours  
229 depending on membranes, until 200 mL of the cumulative permeate volume  
230 was attained. Once the fouling run finished, the resultant fouled membrane was  
231 physically flushed with fresh water through the both sides of the FO membrane  
232 for 30 min at an elevated crossflow velocity of 21 cm/s. To determine the flux  
233 recovery, the water flux was obtained again after the cleaning tests using the  
234 same but foulant-free feed and draw solutions as in the fouling experiment. To  
235 account for the flux drop due to dilution effects, we also carried out the baseline  
236 experiments under the same experimental conditions without foulants. The flux  
237 decline obtained from fouling experiments has been corrected using the  
238 baseline flux profile to account for the dilution effects.

239

240 **Molecular Dynamic Simulation.** To understand the hydrophilicity of  
241 different three types of given materials (e.g. CNT, PK, and SBMA), three  
242 simulation models contenting these given materials and water molecules were  
243 constructed through the Amorphous Cell module with similar atomic numbers,  
244 in which the density values were set at 1 g/cm<sup>3</sup> at the outset<sup>39-41</sup>. Detailed  
245 information is described in the Supporting Information.

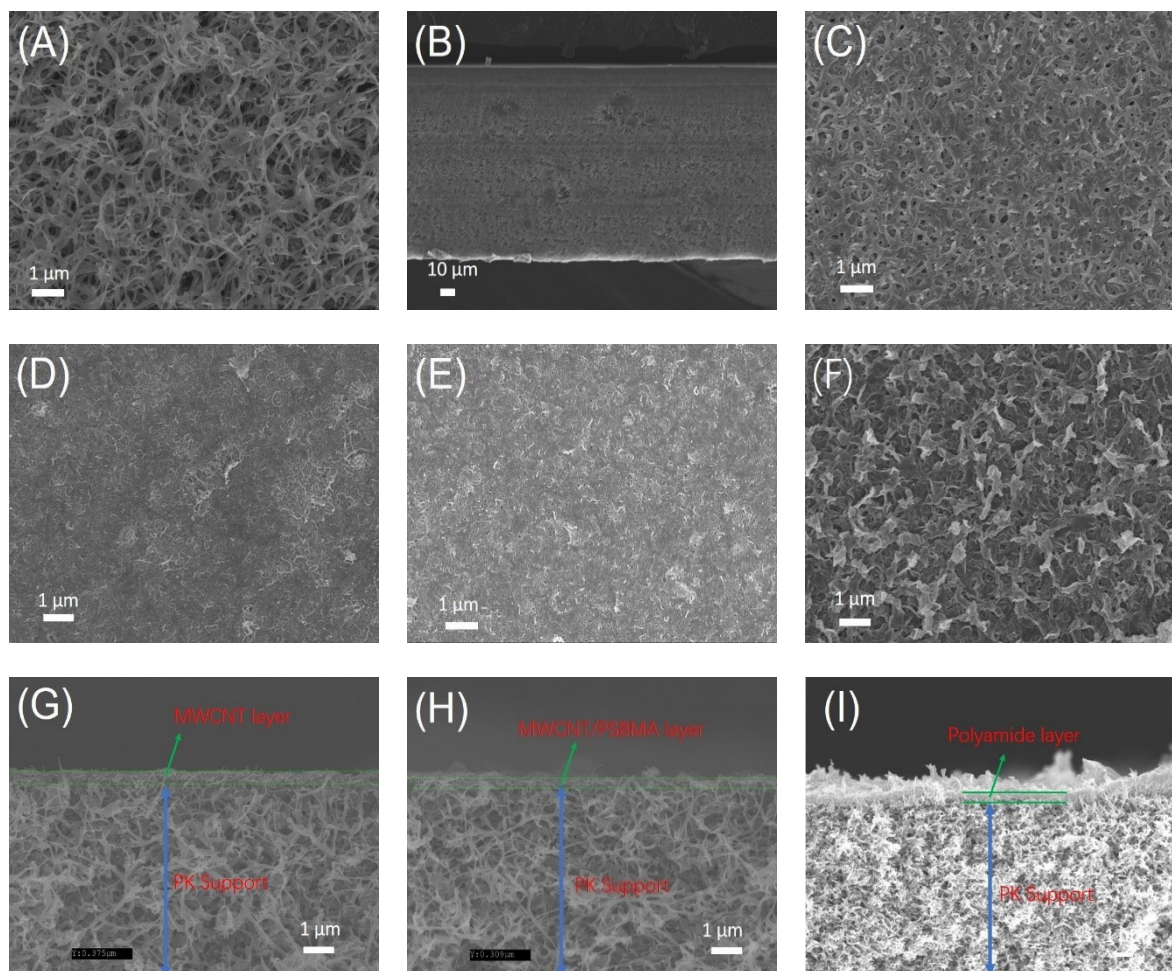
246

## 247 **Results and Discussion**

248 **Characterizations of the fabricated membranes.** The PK support  
249 possesses a fully sponge-like structure (**Figure 3**), which can promote the mass  
250 transport and provide better mechanical stability during long-term operations.  
251 Although visible pores cover on the bottom layer of the PK support (**Figure 3C**),  
252 a dense selective polyamide layer consisting of larger “leaf-like” curls is  
253 successfully interfacial polymerized on the bottom surface (**Figure 3F**). This  
254 may be driven by the special interactions between the MPD solution and the  
255 PK matrix<sup>34</sup>. In order to operate the FO membranes in the PRO mode, the top  
256 porous surface of the PK support is coated with different second skin layers  
257 (e.g. MWCNT and MWCNT/PSBMA layers) via vacuum filtration method. As  
258 illustrated in **Figures 3(G and F)** and **Table S2**, the fabricated MWCNT layer  
259 has a thickness of 375 nm and a loading density of 322 mg/m<sup>2</sup>; for the  
260 MWCNT/PSBMA layer, the thickness and loading density are 309 nm and 288  
261 mg/m<sup>2</sup>, respectively. As imaged in **Figures 3D and 3E**, compared with the

262 pristine porous top layer structure (**Figure 3A**), relatively dense and continuous  
263 second skin layers are appeared on the top surface of the PK support,  
264 evidencing for the successful fabrication. Noting that it is difficult to achieve  
265 such a dense coverage of the porous support by using conventional membrane  
266 surface modification techniques with soft polymers<sup>42</sup>. The roughness data of  
267 these three membranes are shown in **Figure S3**, Supporting Information.  
268 MWCNT layer and MWCNT/PSBMA layer are smoother than the PK support  
269 surface.

270



271 **Figure 3.** SEM micrographs of the (A) top surface, (B) cross-section and (c) bottom surface  
272 of the PK support surface; Morphologies of the (D) MWCNT surface and (E)

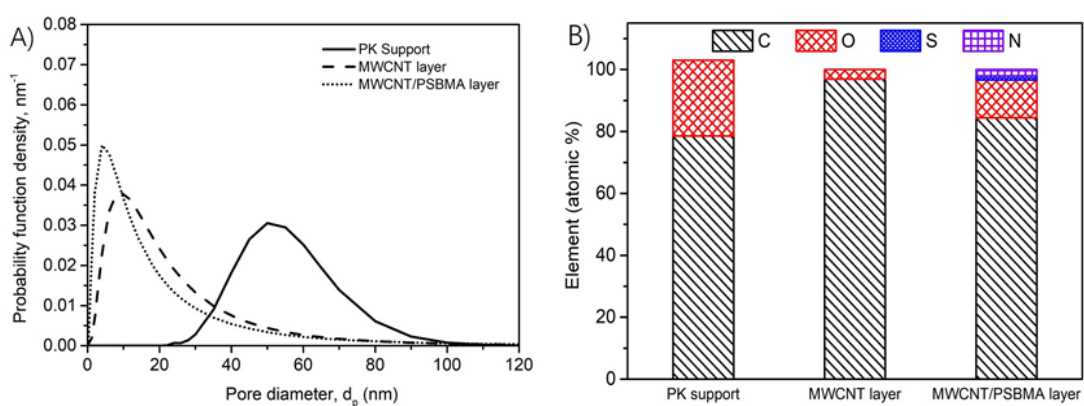
273 MWCNT/PSBMA surface after vacuum suction of carbon nanotube dispersion onto the top  
274 of PK support; Morphology of the (F) polyamide layer after interfacial polymerization on the  
275 bottom of PK support. Cross-sections of the (G) MWCNT layer, (H) MWCNT/PSBMA layer  
276 and (I) polyamide layer.  
277

278 At the same time, the mean pore sizes of the three different supports are  
279 estimated based on the PEO rejection coefficient and the corresponding pore  
280 size distributions are plotted as the probability density function<sup>17</sup>. Details of PEO  
281 rejection experiment and determination of pore size distribution are described  
282 in the Supporting Information. As shown in **Figure 4A** and **Table S1**, the top  
283 surface of PK support has the largest mean pore size (54.6 nm) and MWCO  
284 value (369 KDa). After coating the carbon nanotube layer on the PK support,  
285 the mean pore sizes are decreased to 17.8 nm (corresponding to MWCO of  
286 131 KDa) and 13.2 nm (corresponding to MWCO of 121 KDa) for MWCNT layer  
287 and MWCNT/PSBMA layer, respectively. These results agreed well with the  
288 surface morphology change as shown in **Figure 3**. Compared to the MWCNT  
289 layer, the smaller mean pore size of the MWCNT/PSBMA layer may be  
290 ascribed to the swelling chain conformation of PSBMA brushes in the water<sup>24,43</sup>.  
291 In here, the degree of PSBMA swelling (DS) is ~15.5%, which is defined as: DS  
292 =  $W_w/W_d$ , where  $W_w$  and  $W_d$  are the wetted and dried weight of PSBMA modified  
293 MWCNT, respectively. Furthermore, the pristine PK support exhibits the lowest  
294 rejection towards BSA (0%) and alginate (44.4%); on the contrary, the  
295 MWCNT/PSBMA layer has the highest rejection towards BSA (13.2%) and  
296 alginate (71.3%) as shown in **Table S2**. As a general rule, the rejection property  
297 of the asymmetric porous membrane is mainly dominated by the top layer.

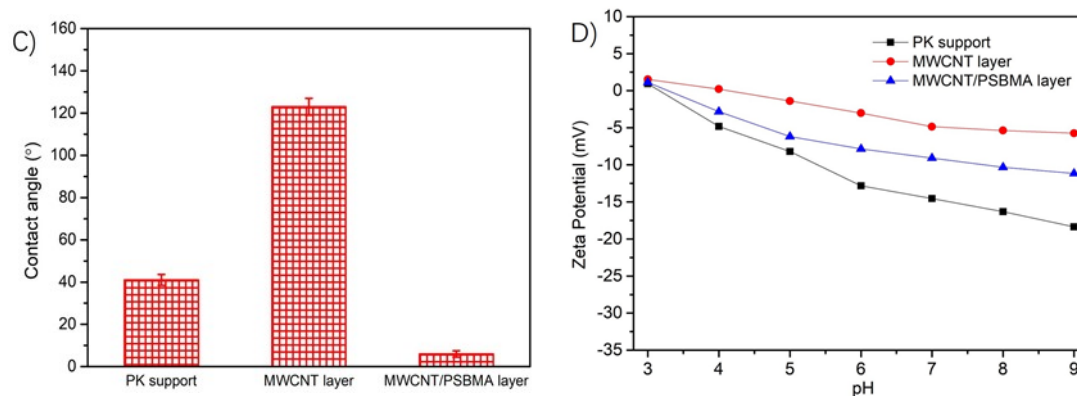
298 Accordingly, our results demonstrate the successful fabrication of zwitterionic  
299 brushes-decorated MWCNT layer on PK support.

300 The membrane surface chemistries of different second skin layers can be  
301 successfully verified by XPS technique. XPS wide scan spectra are shown in  
302 **Figure S4**. As shown in **Figure 4B**, the PK support consists of “C” (~78.5%)  
303 and “O” (~24.5%), which matches well with the elemental composition of PK  
304 molecule. After the MWCNT layer coating on the PK support, “C” (~96.9%)  
305 becomes the primary element and “O” (~3.1%) is detected in a very low  
306 composition concentration. This noticeable change indicates the complete  
307 covering of MWCNT layer on the PK support. In the case of TFC-  
308 MWCNT/PSBMA membrane, more than the primary element of “C” (~84.4%)  
309 and “N” (~12.2%), the presence of “S” (~1.4%) and “N” (~2%) confirms the  
310 successful coating of MWCNT/PSBMA layer on the PK support.

311







312 **Figure 4.** Key membrane characteristics: (A) surface pore size distributions, (B) XPS  
 313 spectroscopy, (C) water contact angles, and (D) zeta potentials as a function of pH of the  
 314 PK support, MWCNT layer and MWCNT/PSBMA layer of the double-skin layer membrane.

315

316 Water contact angle (CA) measurement was employed to assess the  
 317 surface hydrophilicity. As illustrated in **Figure 4C**, the PK support surface  
 318 exhibits a CA of  $\sim 41^\circ$ , which is consistent with previously published data<sup>44</sup>. On  
 319 the other side, the CA of MWCNT layer is significantly increased to  $\sim 123^\circ$ ,  
 320 indicating its hydrophobic nature due to the aromatic rings of carbon nanotube.  
 321 For the zwitterionic PSBMA brushes decorated MWCNT layer, a definite  
 322 reduction of CA to  $\sim 6^\circ$  is observed, which evidences a hydrophilic surface due  
 323 to the grafted PSBMA brushes and may significantly enhance its fouling  
 324 resistance.

325 Membrane surface charges were characterized by zeta potential  
 326 measurements and the results are exhibited in **Figure 4D**. For the experimental  
 327 pH range (e.g., pH 3-9), the PK support zeta potential is slightly positive (e.g.,  
 328 1 mV at pH 3) at the beginning and then increasingly negative with the growing  
 329 pH due to the preferential anion adsorption to the weaker hydrated PK surface.  
 330 This result reflects the characteristic charge curve of non-ionic surface, such as

331 polysulfone membrane<sup>45,46</sup>. After coating the MWCNT layer on the PK support,  
332 the zeta potential becomes least negative due to the presence of the most  
333 hydrophobic MWCNT shielding on the PK support, which reduces the anion  
334 adsorption to a great extent. Compared with the MWCNT layer, the  
335 MWCNT/PSBMA layer exhibits slightly more negative, being consistent with the  
336 previous studies<sup>24,33,47</sup>. Guo et al.<sup>48</sup> explained that the slight negative charge of  
337 PSBMA brushes can be ascribed to its overall acidic characteristic in solution,  
338 since the  $pK_a$  value of sulfonate groups is 2 and  $pK_b$  value of quaternary  
339 ammonium groups is 5.

340

341 **Membrane Intrinsic Transport Properties.** As summarized in **Table 1**,  
342 the  $A$  values of the double-skinned membranes ( $1.87$  and  $1.93 \text{ L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}\cdot\text{bar}^{-1}$   
343 for TFC-MWCNT and TFC-MWCNT/PSBMA membranes, respectively) remain  
344 almost the same as that of TFC-PK membrane ( $2.0 \text{ L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}\cdot\text{bar}^{-1}$ ); while the  $B$   
345 values increases lightly from  $0.38 \text{ L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$  for TFC-PK membrane to  $0.59$  and  
346  $0.51 \text{ L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$  for TFC-MWCNT and TFC-MWCNT/PSBMA membranes,  
347 respectively. It is because  $A$  and  $B$  values are the intrinsic parameters relevant  
348 only to the polyamide layer. The  $S$  values, relevant only to the supporting layer,  
349 increase slightly but not statistically significant after deposition of carbon  
350 nanotube layer on the top of PK support ( $263 \mu\text{m}$  vs  $330 \mu\text{m}$  vs  $306 \mu\text{m}$  for the  
351 TFC-PK, TFC-MWCNT and TFC-MWCNT/PSBMA membranes, respectively).  
352 These results demonstrate that the nanoscale thicknesses of carbon tube

353 layers have no effect on the transport properties of the double-skinned  
354 membranes<sup>49</sup>.

355

356 **Table 1.** Intrinsic properties, structural parameters and salt rejections of the double-  
357 skinned membranes (Detailed testing methods are shown in Supporting Information)

358

Membrane code	$A$ (L·m <sup>-2</sup> ·h <sup>-1</sup> ·bar <sup>-1</sup> )	$B$ (L·m <sup>-2</sup> ·h <sup>-1</sup> )	$S$ (μm)	$R_s$ (%)
TFC-PK	2.00±0.10	0.38±0.10	263±11	97.7±0.2
TFC-MWCNT	1.87±0.21	0.59±0.08	330±7	96.1±0.1
TFC-MWCNT/PSBMA	1.93±0.12	0.51±0.10	306±10	96.8±0.1

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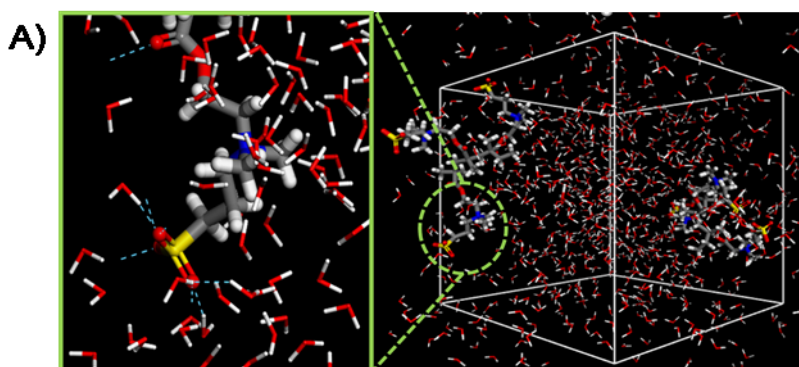
### 360 **Interaction energy between membrane materials and water molecules.**

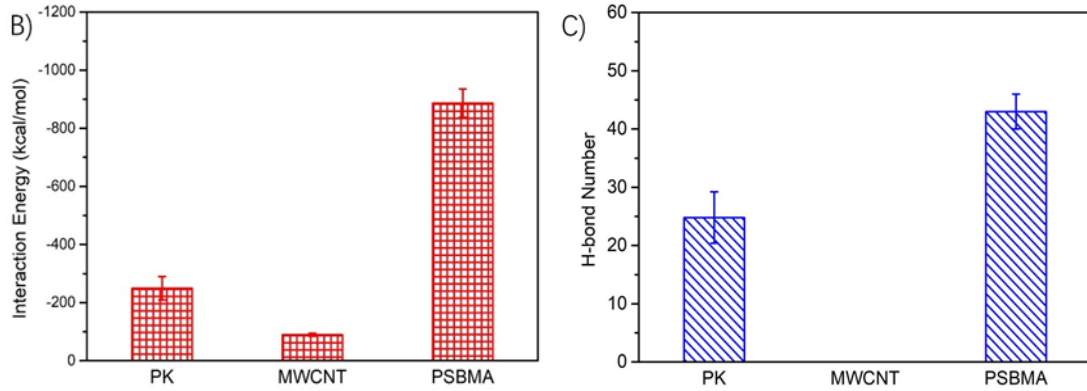
361 The notably enhanced hydrophilicity of the MWCNT/PSBMA surface suggests  
362 that the anti-fouling properties may be improved because of the PSBMA  
363 brushes grafting. In order to understand the hydrophilicity of three different  
364 types of given materials (e.g. PK, MWCNT and PSBMA), molecular dynamics  
365 simulation technique was employed to explore the interactions. During the  
366 simulation process, the interaction between the polymer chain and water  
367 molecules was recorded and analyzed to further compare the hydration  
368 capacities of these three types of membrane materials.

369 **Figure 5** presents the interaction energy and intermolecular H-bonds  
370 between membrane materials and water molecules. As shown in **Figures 5B**  
371 and **5C**, interaction energy between MWCNT and water molecules displays the  
372 largest value of -89.5 kcal/mol, with almost zero H-bonds. This highest energy  
373 can be ascribed to the hydrophobicity of MWCNT, demonstrating that the

374 attachment of organic foulants on its surface could occur easily to minimize the  
375 interfacial energy<sup>50</sup>. For PK polymer, the interaction energy is decreased to -  
376 249.2 kcal/mol, exhibiting H-bonds with a middle number of 24.8. In contrast,  
377 the zwitterionic PSBMA polymer shows the lowest interaction energy value,  
378 -886.8 kcal/mol, representing 71.9% reduction in interaction energy compared  
379 to the PK polymer. Also, the H-bond number is the highest value of 43. These  
380 results are due to its special interactions with water. In addition to the hydrogen  
381 bonding between water molecules and PK polymer, zwitterionic PSBMA  
382 polymers can strongly trap water molecules via the electrostatic force to form a  
383 more tighter hydration layer (**Figure 5A**)<sup>23,24,51</sup>. This hydration layer would  
384 prevent organic foulants from close contact with the modified surface due to no  
385 significant thermodynamic advantage<sup>52</sup>.

386





387 **Figure 5.** Molecular dynamics simulation. (A) H-bonds network between PSBMA and water  
 388 molecules; The atom colors are chosen as follows: C, gray; N, blue; O, red; S, yellow; H,  
 389 white. (B) Interaction energy between PK, MWCNT, PSBMA and water molecules,  
 390 respectively; (C) Intermolecular H-bond number between PK, MWCNT, PSBMA and water  
 391 molecules, respectively.

392

393 **Adsorption Propensity of Proteins and Bacteria.** Anti-fouling properties

394 of the double-skinned membranes were evaluated by its resistance against

395 protein and bacteria adsorption. As the typical protein and bacteria, BSA and

396 *E. coli*, are used as model organic foulants, respectively. Their accumulation on

397 the membrane surface not only compromises the water flux, but also forms a

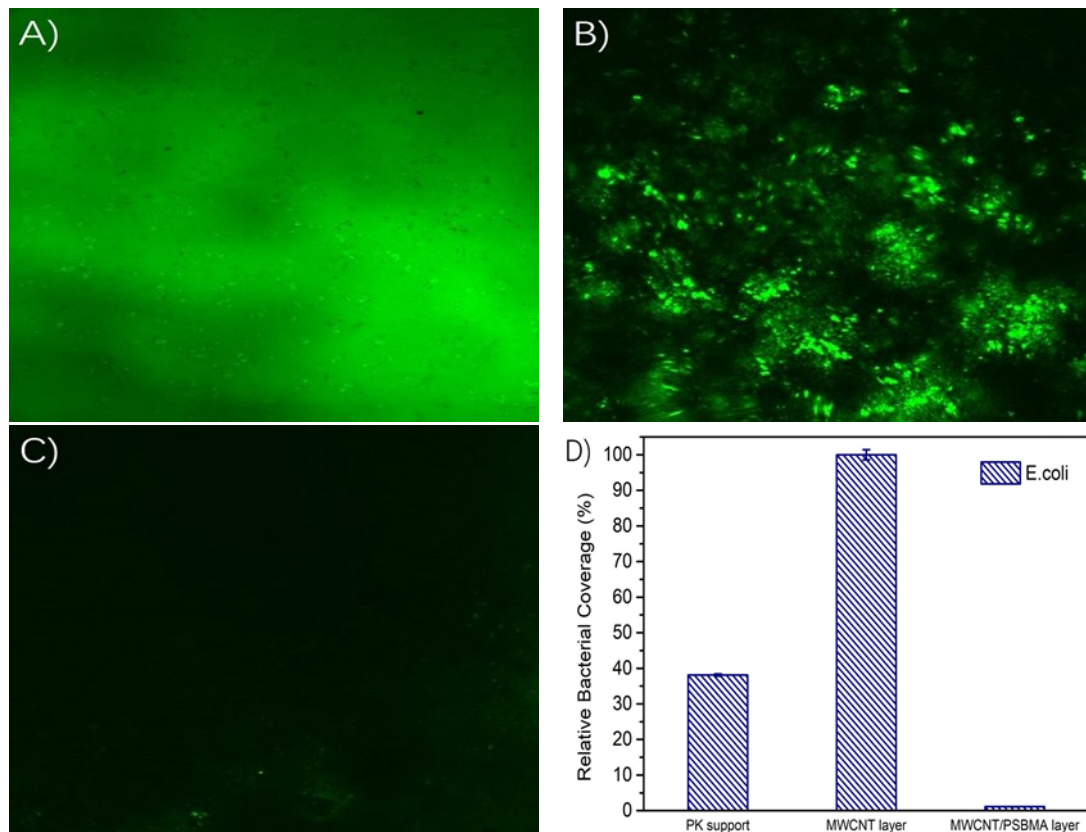
398 conditioning film, which could provide carbon and nitrogen sources for the

399 microbial colonization<sup>53-55</sup>. Therefore, protein fouling resistance is considered

400 as one of the important factors to investigate the anti-fouling properties of

401 double-skinned membranes.

402



403 **Figure 6.** CLSM images of (A) PK support, (B) MWCNT layer, and (C) MWCNT/PSBMA  
 404 layer after protein adsorption tests using FITC-BSA in PBS. TFC-PK, TFC-MWCNT, and  
 405 TFC-MWCNT/PSBMA after 12 h exposure to FITC-BSA in 0.2 M PBS at pH=7. (D) Relative  
 406 adhesion of *E. coli* on the PK support, MWCNT layer and MWCNT/PSBMA layer of FO  
 407 membranes after 24 h contact time, normalized to the result of the MWCNT surface.

408

409 Surface fluorescence intensities were adopted to evaluate the protein  
 410 adsorption after exposure to fluorescein-labeled BSA (FITC-BSA).  
 411 Fluorescence images of the PK support, MWCNT layer and MWCNT/PSBMA  
 412 layer of the double-skinned membranes are showed in **Figure 6**. The  
 413 fluorescence intensities can directly quantify the BSA adsorption degrees on  
 414 membrane surfaces. Despite having a relatively hydrophilic PK surface, the  
 415 TFC-PK membrane still has a brightest fluorescence image (**Figure 6A**). This  
 416 may be because the protein not only on the surface but also underneath the  
 417 surface can be determined by the fluorescence<sup>23</sup>, especially for the porous PK

418 surface. **Figure 6B** illustrates that the MWCNT layer has a slightly weaker  
419 fluorescence intensity due to the decreased surface pore size, while the  
420 MWCNT/PSBMA layer exhibits virtually no fluorescence (**Figure 6C**). It can  
421 conclude that the MWCNT/PSBMA layer possesses the excellent anti-fouling  
422 property toward protein. This difference between the MWCNT layer and  
423 MWCNT/PSBMA layer can be ascribed to the fact that the benzene rings of the  
424 former could attract proteins while the latter has unique interactions with water  
425 and inhibits the protein adsorption.

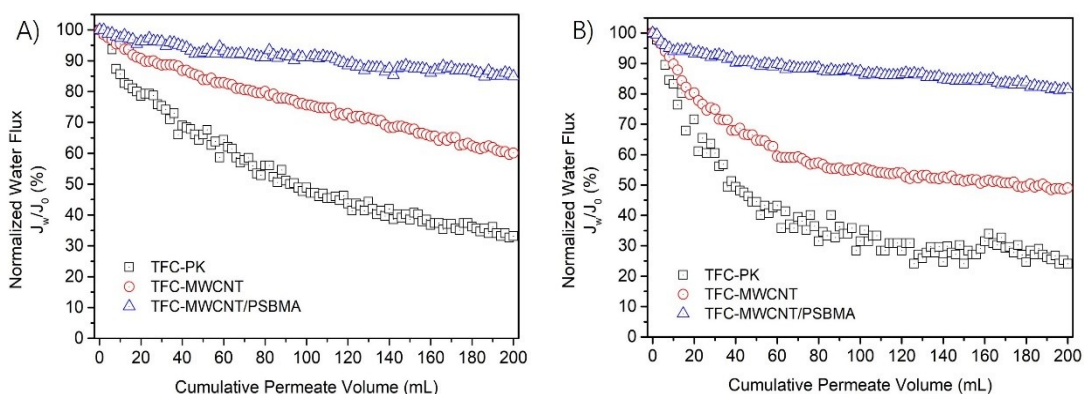
426 Bacteria adsorption tests were also conducted with *E. coli* to inspect the  
427 anti-microbial abilities of the fabricated membranes. As illustrated in **Figure 6D**,  
428 the MWCNT layer has the highest bacteria attachment. After coating with the  
429 zwitterionic brushes-decorated MWCNT layer, the TFC-MWCNT/PSBMA  
430 membrane exhibits a higher anti-adhesive property toward bacteria, with  
431 bacterial coverage reduction of 37% compared to the TFC-PK membrane.

432

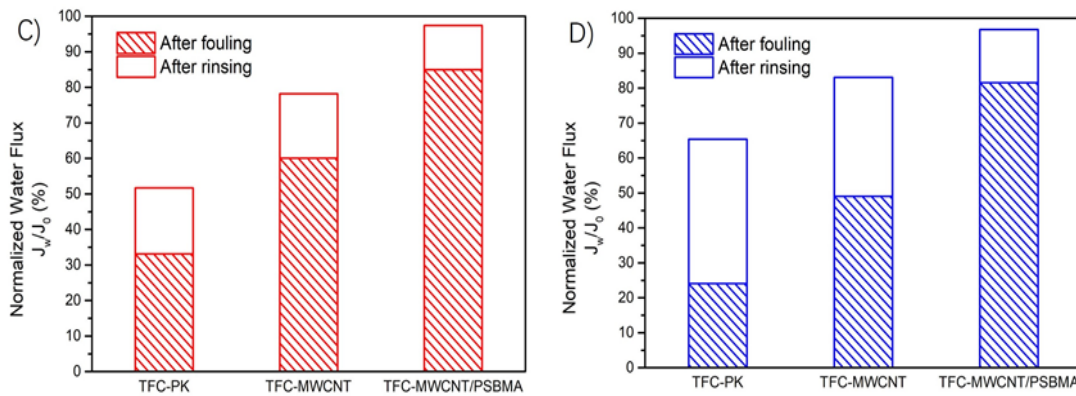
433 **Dynamic Fouling Behavior in PRO mode.** Anti-fouling properties of the  
434 fabricated membranes were assessed by the dynamic BSA and alginate fouling  
435 experiments, when they were tested in PRO mode (membrane polyamide layer  
436 facing to the draw solution). Immediately after fouling, physical flushing with  
437 higher crossflow rate of 21 cm/s was used to clean the fouled membranes for  
438 30 min. **Figure 7** shows the declined flux induced by organic fouling and the  
439 recovered flux after physical cleaning.

440 The TFC-PK membrane, with a porous back side surface, exhibits the most  
441 severe flux decline to 33% of its initial water flux owing to the significant BSA  
442 fouling (**Figures 7A and 7C**). The foulant blockage within the porous support of  
443 the TFC-PK membrane significantly deteriorates the membrane filtration  
444 capacity. By contrast, the TFC-MWCNT/PSBMA membrane whose back  
445 surface sealed with a hydrophilic MWCNT/PSBMA layer, exhibits an improved  
446 flux stability with an 85% retention of the initial water flux. This result  
447 demonstrates the excellent antifouling performance towards BSA foulant of  
448 MWCNT/PSBMA surface, which is consistent to its decreased surface pore  
449 sizes and enhanced hydrophilic properties. Besides, the TFC-MWCNT  
450 membrane has a weaker anti-fouling property with a reduction to 60% of its  
451 initial flux. This is because its most hydrophobic MWCNT surface are easy  
452 subjected to strong BSA foulant adhesion, which matches well with the results  
453 in the static fouling experiments (Section 3.4).

454







455 **Figure 7.** Water flux decline curves for TFC-PK, TFC-MWCNT, and TFC-MWCNT/PSBMA  
 456 membranes obtained from (A) BSA and (B) alginate fouling experiments. Feed solution  
 457 was prepared by adding 30 mg/L foulants and 0.5 mmol/L CaCl<sub>2</sub> to 50 mmol/L NaCl.  
 458 Summarized organic fouling results of (C) BSA and (D) alginate fouling experiments with  
 459 TFC-PK, TFC-MWCNT, and TFC-MWCNT/PSBMA membranes. Blank columns mean the  
 460 percentage of flux recovery after physical cleaning.

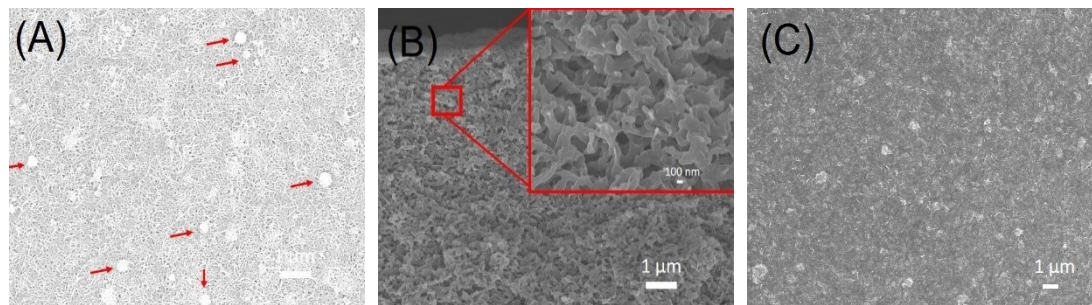
461

462 Compared with BSA fouling, alginate fouling causes more flux decline  
 463 (**Figure 7B**), especially for the TFC-PK and TFC-MWCNT membranes under  
 464 the same tested conditions. As an end of membrane fouling, the water fluxes of  
 465 the TFC-PK and TFC-MWCNT membranes decrease to 24% and 49% of the  
 466 initial water flux, respectively. Ca<sup>2+</sup> ions (0.5 mmol/L) in the feed solution is  
 467 known to aggravate alginate fouling by acting as “bridges” between alginate  
 468 molecules, which leads to form a cross-linked gel-like alginate on the PK and  
 469 MWCNT surfaces and thus causes a significant decrease of water flux<sup>56,57</sup>. By  
 470 comparison, the alginate fouling of the TFC-MWCNT/PSBMA membrane is still  
 471 the least severe with a highest flux retention up to 82% of its initial value, again  
 472 demonstrating the outstanding anti-fouling abilities of the hydrophilic  
 473 MWCNT/PSBMA surface.

474 The above-mentioned filtration performance can be further reinforced by

475 an apparent discrepancy in the water flux recovery efficiencies for these three  
476 membranes as shown in **Figures 7C** and **7D**; the flux recovery of the fouled  
477 membranes follows the order of TFC-PK membrane<TFC-MWCNT  
478 membrane<TFC-MWCNT/PSBMA membrane. For the TFC-PK membrane, the  
479 foulants blocked into the porous PK support, cannot be eliminated by the shear  
480 force of physical cleaning, which leads to severe irreversible fouling. On the  
481 other hand, the MWCNT/PSBMA layer created on the PK support could  
482 defense against the intruding of agglomerated foulants (e.g. alginate gels) into  
483 the pores of PK support, which makes the foulants only possibly deposit on the  
484 surface. The shear force of physical cleaning could easily flush these deposited  
485 foulants away from the membrane surface, and thus the water flux can be  
486 satisfactorily recovered. These anti-fouling mechanisms can be further  
487 demonstrated by the SEM images of fouled TFC-MWCNT/PSBMA membrane.  
488 As shown in **Figure 8A**, the agglomerated organic foulants (e.g. alginate gels)  
489 scatter randomly on the MWCNT/PSBMA surface rather than in the inner PK  
490 support (**Figure 8B**). The cleaned surface is also analyzed and exhibits almost  
491 no fouling surface coverage (**Figure 8C**). Taken together, the overall antifouling  
492 performance of the TFC-MWCNT/PSBMA membrane is better than the other  
493 two membranes when operated in PRO mode, highlighting a versatile approach  
494 to design antifouling FO membranes.

495



496 **Figure 8.** SEM images of MWCNT/PSBMA surface and cross-section (near the  
497 MWCNT/PSBMA layer) of (A, B) fouled and (C) cleaned TFC-MWCNT/PSBMA membrane.  
498 Note: The red arrow in Figure 8A means the alginate gels. The inset in Figure 8B is the  
499 cross-section image of PK support at 100 nm scale.

500

## 501 **Conclusion**

502 In this work, we have successfully designed an anti-fouling double-skinned  
503 FO membrane by constructing zwitterionic brushes-decorated MWCNT layer  
504 on the PK support for improving the organic fouling resistance under PRO mode.  
505 Surface characterization revealed that the introduction of MWCNT/PSBMA  
506 layer could significantly alter the surface morphologies of the PK support, such  
507 as enhanced hydrophilicity, reduced surface roughness and narrowed surface  
508 pored size. Computational methods provided insights into the excellent  
509 hydrophilic nature of zwitterionic PSBMA brushes, and thus the  
510 MWCNT/PSBMA layer surface exhibited the best anti-protein adsorption and  
511 anti-bacterial adhesion properties. In dynamic PRO fouling tests, coating a  
512 MWCNT/PSBMA layer on the PK support achieved the least negative effects  
513 on water flux and the highest recovered water flux in comparison of the pristine  
514 TFC-PK and hydrophobic TFC-MWCNT membranes.

515

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521

## 522 **Appendix A. Supporting information**

523 Supplementary data associated with this article can be found in the online  
524 version at .....

525

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