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Modelling reef hydrodynamics and sediment mobility under sea level rise in atoll reef island systems

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1 Modelling reef hydrodynamics and sediment mobility under sea level rise in 2 atoll reef island systems

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12

13 **Highlights:**

- 14 • Hydrodynamics and sediment mobility were modelled under reef submergence scenarios.
- 15 • The largest increases in sediment mobility were projected on the inner reef flat.
- 16 • Lagoonal zones were projected to remain as sinks for sediment deposition.
- 17 • Results imply lagoonward island migration is likely to occur under sea level rise.

18

19 **Abstract:** Low-lying coral reef islands will be significantly impacted by future sea level rise (SLR). It is
20 generally expected that SLR will destabilise reef islands because increasing reef submergence allows
21 larger waves, and therefore greater energy transmission, across reef flats. However, the impact of
22 SLR on altering both reef flat sediment transport and sediment delivery to island shorelines is poorly
23 understood. Here, we use the currents of removal approach (coupling two-dimensional wave
24 modelling with settling velocity data from 186 benthic sediment samples) to model shifts in both
25 reef hydrodynamics and benthic sediment transport under scenarios of mean reef submergence
26 (MRS = +0 m, +0.5 m, +1 m) at two atoll rim reef sites in the Maldives. Under contemporary
27 conditions (MRS = +0 m), we found that benthic sediment transport is likely occurring, consistent
28 with active reef-to-island sediment connectivity. Under conditions of increased MRS, shifts in wave
29 velocities, and in turn sediment potential mobility, were both non-linear and non-uniform.
30 Significant between-site differences were found in the magnitude of projected shifts in sediment

31 mobility under scenarios of increased MRS, which implies that morphological responses to increases
32 in MRS are likely to be diverse, even over local scales. Under increased MRS, the largest increases in
33 sediment mobility were projected on the inner reef flat, whereas lagoonal zones remained as sinks
34 for sediment deposition. We thus hypothesize that while reef islands will persist as sedimentary
35 landforms under projected rates of MRS, lagoonward reef island migration is likely to occur. Findings
36 have implications for predicting the future adaptive capacity of atoll nations. The challenge is to
37 incorporate such potential increases in island mobility and intra-regional diversity in reef system
38 geomorphic responses to sea level rise into national-scale vulnerability assessments.

39

40 **Key words:** reef islands, sea level rise, waves, hydrodynamics, sediment transport, Maldives

41

42 **1. Introduction**

43 Low-lying coral reef islands are frequently considered to be among the most vulnerable landforms to
44 climate change and associated sea level rise (SLR; IPCC, 2019). Increases in flooding and wave
45 inundation events have been projected to render atoll nations uninhabitable by the end of the
46 century (Quataert et al., 2015; Storlazzi et al., 2015, 2018). Given their vulnerability, reef islands
47 have received increasing attention from geomorphic (Webb and Kench, 2010; Kench et al., 2015;
48 Duvat et al., 2017; Kench et al., 2018) and hydrodynamic (Quataert et al., 2015; Storlazzi et al., 2015,
49 2018; Beetham et al., 2017) research in recent years. However, existing research efforts have largely
50 focus on individual elements of the reef system without accounting for the important
51 morphodynamic interactions that operate within reef systems. One significant limitation of prior
52 work is that sediment transport processes remain poorly constrained. This knowledge gap is
53 particularly pertinent given that reef islands are formed entirely of sediments produced by
54 organisms in their adjacent marine environments. Sediment transport processes are thus key
55 controls on reef island maintenance and morphological stability, but there is very limited

56 understanding of both contemporary process regimes and how these processes may change under
57 future SLR scenarios.

58 One reason for the paucity of prior research on reefal sediment transport processes is that the
59 classic empirical expressions of clastic sediment entrainment, transport and deposition (Hjulstrom,
60 1935; Shields, 1936; Rouse, 1937) are of limited value in reef environments (Cuttler et al., 2017;
61 Scoffin, 1992). The biogenic nature of reefal sediment, which is derived from a variety of source
62 organisms (e.g. coral, molluscs, foraminifera), results in grains of variable density, size and shape
63 (Sorby, 1879; Chave et al., 1972; Ford and Kench, 2012). Reefal sediments thus violate the
64 assumptions of traditional sediment transport expressions that employ grain size as the primary
65 control on clastic sediment entrainment (Maiklem, 1968; Smithwaite, 1973; Kench and McLean,
66 1996). To address these challenges, the 'currents of removal' approach was developed to provide a
67 more robust means of quantifying reefal sediment transport by analysing sediment hydrodynamic
68 properties (as opposed to grain size) in combination with hydrodynamic data (Kench, 1998; Scoffin,
69 1987). Despite the development of the 'currents of removal' approach, there has been limited
70 application of such approaches to better understand sediment hydrodynamics and transport
71 processes in reef systems. Whilst there is a growing body of literature examining sediment transport
72 processes under modal conditions (e.g. Morgan and Kench, 2016; Pomeroy et al., 2018; Cuttler et al.,
73 2019), there remains a paucity of research into sediment transport dynamics under SLR. A notable
74 exception is work on transport dynamics under SLR scenarios on fringing type reef systems in
75 Hawaii, using numerical modelling in one-dimension (Ogston and Field, 2010) and of profiles in two-
76 dimensions (Storlazzi et al., 2011; Grady et al., 2013). To the best of our knowledge, the only work to
77 investigate sediment transport under SLR in atoll reef island environments has been Shope et al.'s
78 (2017, 2019) analyses of shifts in alongshore sediment transport. We thus present the first analysis
79 of reef island sediment transport under SLR across atoll reef island platforms. Understanding of
80 these processes is especially limited in low-lying atoll reef island systems, yet this knowledge is

81 critical to better constrain future reef island landform trajectories and, in turn, to inform national-
82 scale vulnerability assessments of reef island nations.

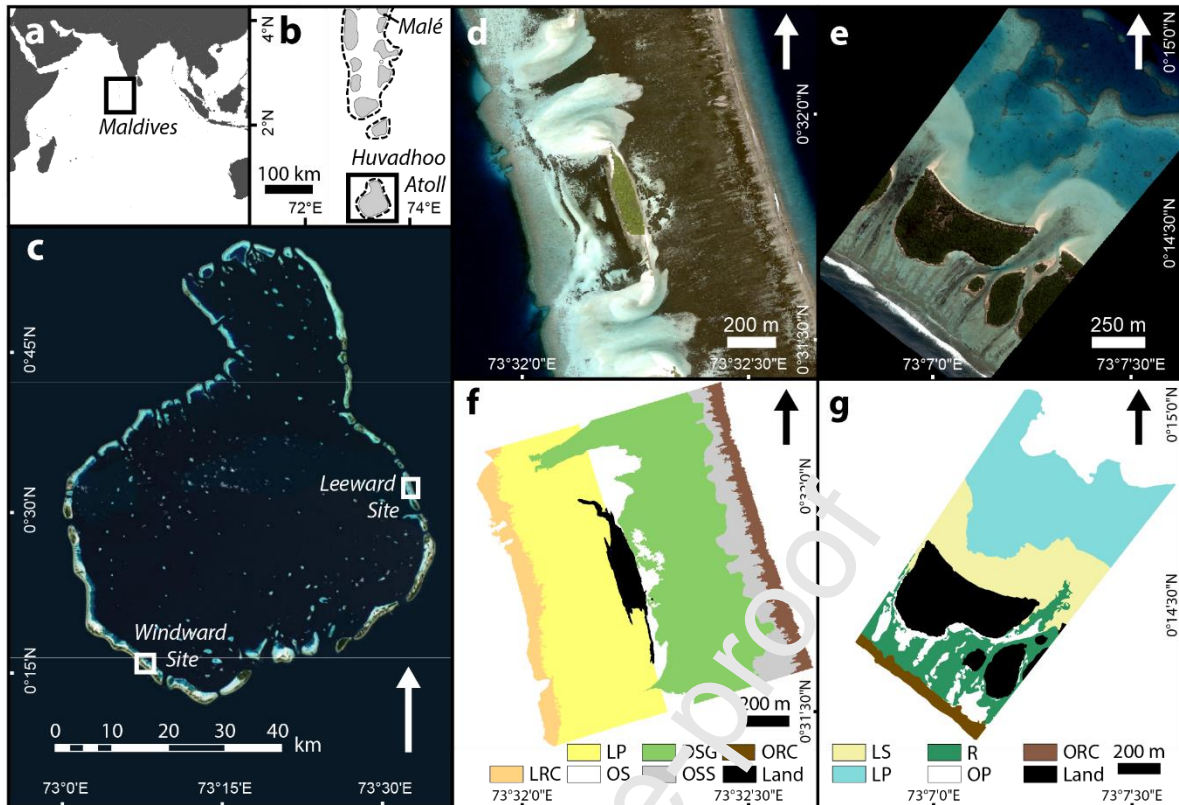
83 Here, we use the ‘currents of removal’ approach to present the first study of both hydrodynamics
84 and benthic sediment transport under different mean reef submergence (MRS) scenarios in an atoll
85 reef island environment. We refer to MRS, as opposed to SLR, as to solely consider SLR invokes the
86 assumption that reef morphology remains static (i.e. no reef growth will occur over the associated
87 timeframe). Rather, we suggest it is more appropriate to employ MRS as it is the difference between
88 vertical reef accretion and SLR that is the key control on across-reef wave energy regimes (Quataert
89 et al., 2015). Data are presented from two contrasting settings (in terms of exposure to open ocean
90 swell) on Huvadhu atoll rim, southern Maldives. We use two-dimensional modelling to simulate
91 wave processes under three scenarios: MRS = +0 m (contemporary conditions), +0.5 m (SLR and reef
92 accretion data from the southern Maldives suggest this would occur by 2100 under RCP8.5; Perry et
93 al., 2018), and +1 m (projected as the upper extreme in the southern Maldives by 2100 under
94 RCP8.5, 95% confidence interval; Perry et al., 2018). Wave model outputs are then coupled with
95 settling velocity data from 186 benthic sediment samples to estimate sediment potential mobility
96 (PM) under each of these MRS scenarios. Results are discussed in the context of the geomorphic
97 implications for reef island futures. We suggest that while reef islands may persist under SLR, there
98 will likely be increased island mobility and local-scale variability in the magnitude of such
99 morphological shifts.

100 **2. Regional Setting**

101 The Maldives is a reef island nation comprised of ~1,200 islands inhabited by a population of
102 ~436,000 (Fig. 1). There is an emerging understanding of reef hydrodynamics (Kench et al., 2006;
103 Mandlier, 2008) and sediment transport (Morgan and Kench, 2014, 2016) under the contemporary
104 process regime on faro type reef platforms (i.e. small annular atoll interior reef platforms) in the
105 Maldives. However, our understanding of reef hydrodynamics and sediment transport on Maldivian

106 linear atoll rim platforms (i.e. elongate reef platforms which form atoll perimeters) is limited. This is
107 a key knowledge gap as sediment transport processes are likely to differ significantly between faro
108 and linear rim platforms as they have distinctly different process regimes. Linear rim platforms are
109 characterised by strong cross-platform wave energy gradients, whereas waves converge at a focal
110 point on faro surfaces as wave energy is incident around 360° of their platform margins (Kench,
111 2013).

112 Straddling the equator, the Maldives archipelago is located in a predominantly storm-free
113 environment (Woodroffe, 1993; Fig. 1). Satellite altimetry data indicate that oceanic swell
114 approaches from south-easterly directions between November and March, and south to south-
115 westerly directions between April and November (Young, 1999). Our study focused on Huvadhoon
116 Atoll, which is approximately 60 km in width, 80 km in length, and has an area of 3,279 km² (Naseer
117 and Hatcher, 2004). Two sections of Huvadhoon Atoll rim were selected as study sites, which
118 represent end-members with respect to their relative exposure to open oceanic swell: a north-
119 eastern leeward site (which contains Galamadhoon island), and a south-western windward site (which
120 contains Mainadhoon, Boduhini and Kudabini islands). The areal extents of the marine environments
121 in the windward and leeward sites are 0.84 km² and 1.06 km², respectively (Table A1). To
122 characterise the oceanic process regime, wave parameters were extracted from WaveWatch III
123 model hindcasts (Tolman, 2009; Durrant et al., 2013) for the period 1979 to 2010 at locations 20 km
124 off the oceanward platform margin at each site. The significant wave height and significant wave
125 period were found to be significantly higher and longer at the windward than the leeward site
126 respectively (paired t-tests; $P = <0.001$; East et al., 2018).



127

128 Figure 1 – Location of the Maldives (a), Huvadho Atoll (b), and leeward and windward study sites
 129 (c). Satellite imagery and classifications of eco-geomorphic zones at the leeward (d, f) and windward
 130 (e, g) sites. At the leeward site, LRC = leeward reef crest, LP = lagoonward patch (reef), OS =
 131 oceanward sand, DSG = dense seagrass, OSS = oceanward sparser seagrass, and ORC = oceanward
 132 reef crest. At the windward site, LP = lagoonward patch (reef), LS = lagoonward sand, OP =
 133 oceanward patch (reef), R = rubble, and ORC = oceanward reef crest. (*width = 2 columns*)

134 3. Materials and methods

135 3.1 Eco-geomorphic zonations

136 As a means of structuring sampling design, eco-geomorphic zones were identified at each site (Table
 137 A1). Zones were selected based on preliminary field surveys and examination of satellite imagery in
 138 order to characterise the range of substrate types, hydrodynamic settings and ecological
 139 communities (Perry et al., 2015). High resolution satellite imagery was used to generate digital
 140 habitat maps of the eco-geomorphic zones at each site (Fig. 1). A WorldView-2 image of the leeward

141 site was acquired on 13th April 2015, and a Quickbird image of the windward site was acquired on
142 27th May 2010 (spatial resolution of visible optical bands = 1.86 m and 2.40 m, respectively). Both
143 images were cloud- and sun glint-free. A Maximum Likelihood Classification was performed on the
144 atmospherically corrected bands. Ground truth data were obtained from each zone (04-06/2013; n =
145 190 and n = 210 for the leeward and windward sites, respectively), which were divided to train (20%)
146 and validate (80%) the classifications. Overall classification accuracies (the number of correctly
147 identified pixels divided by the total number of pixels in the validation; Congalton, 1991) were
148 88.0% and 91.1% at the windward and leeward sites, respectively.

149 **3.2 Hydrodynamic processes**

150 To simulate wave processes, two-dimensional depth-averaged wave modelling was undertaken
151 using a Green-Naghdi (GN) free-surface solver from the open source model Basilisk (Popinet, 2015).
152 This approach has been demonstrated to be effective in simulating wave dispersion, wave breaking,
153 and wet-dry interaction in shallow coastal environments (Bonneton et al., 2011; Tissier et al., 2012;
154 Lannes and Marche, 2015). Basilisk GN is particularly effective in reef environments as it can
155 simulate the behaviour of relatively large amplitude waves across a sudden change in bathymetry
156 (i.e. across a reef crest), which is a challenge for traditional Boussinesq-type models (Roerber and
157 Cheung, 2012). The Basilisk GN solver has been comprehensively evaluated for accurately simulating
158 surf-zone processes in complex reef settings. Benchmark model testing for 1D and 2D scenarios of
159 wave interaction with reefs produced high skill for resolving free surface and velocity across the
160 domain (Beetham et al., 2018). The model has also been proven to successfully replicate field
161 measurements of wave transformation, infragravity wave propagation and wave setup when
162 compared to measurements from an atoll reef in Tuvalu (Beetham et al., 2016). A significant
163 capability of the phase-resolving model is that both currents driven by the orbital motions of
164 individual waves and the mean currents driven by wave setup gradients are represented. The grid
165 size was uniform across the domain with a 5 x 5 m cell size. A consistent implicit quadratic bottom
166 friction coefficient of 0.04 was applied across the model domain. This value was obtained from

167 previous tests of different friction scenarios for implicit quadratic bottom friction across a similar
168 atoll rim reef in Tuvalu, which was comprised of coral, coralline algae, rubble and pavement
169 (Beetham et al., 2016).

170 Bathymetric data were required as inputs to the wave model. Bathymetric digital elevation models
171 of the windward and leeward sites were derived from Quickbird and WorldView-2 imagery
172 respectively. Water depths were obtained in the field using a single beam echosounder to obtain
173 400 individual soundings ($n = 210$ and $n = 190$ at the windward and leeward sites, respectively),
174 which were corrected relative to MSL using the tide tables for Funafuti (00°41S, 173°9E) from the
175 University of Hawaii Sea Level Centre (depth range = 0 to 17 m below MSL). UK Hydrographic Office
176 (1992) charts were used to supplement field data with depths from beyond the oceanward platform
177 margin (these areas were inaccessible due to large oceanic waves; depth range = 15 to 55 m below
178 MSL). Field datasets were then divided to calibrate (50%) and validate (50%) the bathymetric
179 models. Models were generated following the methodology of Stumpf et al. (2003), which applies a
180 band ratio transformation whereby the green and blue bands were extracted from atmospherically
181 corrected images. A ratio layer was produced by dividing the natural log of the green band by the
182 natural log of the blue band. Ratio values were plotted against the calibration data and a second-
183 order polynomial relationship was fitted. The regression equations were applied to the ratio layers
184 to estimate bathymetry across the entirety of each site (spatial resolution = 2.4 m and 1.86 m at the
185 windward and leeward sites, respectively). To validate the models, the field-derived depths of the
186 validation dataset were compared to the model-derived depths (Hamilton et al., 2015). The
187 correlation between field- and model-derived depths was strongly positive in both cases ($R^2 = 0.86$
188 and 0.83 at the windward and leeward sites, respectively; Table A1).

189 Wave height and period data at the lagoonward and oceanward margins of the reef platforms were
190 also required as inputs to the wave model (Table 1). Wave climate data were acquired from three
191 sources. Firstly, oceanward wave data were extracted from WaveWatch III model hindcasts (Tolman,
192 2009; Durrant et al., 2013) for the period 1979 to 2010 at locations 20 km off the oceanward

193 platform margin at each site. Significant wave height and period were extracted and the average
194 taken in order to investigate fair-weather conditions. Secondly, lagoonward wave data for the
195 windward site were obtained from an 8-day field experiment between 8th and 16th November 2007
196 over 16 successive high tidal stages (Mandlier, 2008). Also with the aim of examining a windward rim
197 setting, Mandlier placed instruments at Fares-Maathodaa. Fares-Maathodaa is located ~8 km to the
198 east of the windward site and the platform has a similar aspect relative to incident swell, providing
199 confidence that lagoonward wave conditions are comparable. Mandlier (2008) also collected wave
200 data in the centre of the windward reef platform in a location that approximately corresponds with
201 the lagoonward sand zone in this study. Notably, H_{rms} (average $H_{rms} = \sim 0.05$ m) was found to be
202 comparable to that suggested by the model outputs in the present study (average $H_{rms} = 0.03 \pm 0.05$
203 m; Table A2). Thirdly, lagoonward data for the leeward site were calculated using linear wave theory
204 through application of the JONSWAP approach (Hasselmann et al., 1973) with the revisions
205 suggested by the Shore Protection Manual (1984). Calculations were undertaken using the Swellbeat
206 (2020) Wave Calculator with (1) windspeeds of 10 knots, the average prevailing westerly windspeed
207 calculated using 2014 wind data ($n = 2,643$) from Kaadedhdhoo Airport (0.49°N, 73.00°E;
208 Wunderground, 2015); (2) a duration of 24 hours; and (3) a fetch length of 55 km (westerly distance
209 across the atoll lagoon). In each case, an irregular wave field was imported into both the lagoonward
210 and oceanward fields. The model ran for 2048 s with a spatial resolution of 5.8 m.

211 The model was run three times for each site to represent different scenarios of mean reef
212 submergence (MRS): +0 m (i.e. contemporary conditions), +0.5 m and +1 m. Mean (V_{mean}) and
213 maximum (V_{max}) wave-induced velocities were extracted from the model outputs. The mean velocity
214 (V_{mean}) was calculated for each cell as the average velocity value between $t = 400$ s and 2048 s (i.e.
215 the period during which the wave field was fully developed) and is representative of average
216 currents due to spatial variability in wave setup. V_{max} is the maximum value within each cell between
217 $t = 400$ s and 2048 s and represents wave-driven (short-period) velocities. Hence, both V_{mean} and V_{max}
218 occur under fair-weather conditions with a fully developed wave field. Use of V_{mean} and V_{max} is

219 consistent with the development and prior applications of the currents of removal approach (Kench,
 220 1998). A comparative analysis of V_{max} and $V_{2\%}$ was undertaken and the results were found to be
 221 similar (Fig. A1). Root mean square wave height (H_{rms}) and setup (mean displacement of the free
 222 surface; i.e. the difference between absolute depth and time-averaged water level) were also
 223 calculated for each cell in the model domain to assess differences in wave transformation between
 224 scenarios (Table A2; Fig. A2–A5).

Model inputs		Windward site	Leeward site	Data source
Oceanward margin	H_s (m)	1.55	1.35	Wave Watch III
	T_s (s)	10.1	8.8	Wave Watch III
Lagoonward margin	H_s (m)	0.12 ^a	0.6 ^b	^a Field data
	T_s (s)	8.5 ^a	4 ^b	^b linear wave theory

225 Table 1 – Wave data employed as model inputs from the oceanward and lagoonward margins for
 226 both the windward and leeward study sites. H_s = significant wave height (m), T_s = significant wave
 227 period (s).

228 3.3 Sediment transport

229 A total of 186 benthic surficial sediment samples were collected: 90 from the windward site and 96
 230 from the leeward site (Fig. A6). Equal numbers of samples were collected from each eco-geomorphic
 231 zone ($n = 15$ and $n = 16$ from each zone at the windward and leeward sites respectively). Each
 232 sediment sample was hand scooped using a 500 ml sample pot, rinsed in freshwater twice for 12
 233 hours, soaked in a 5% bleach solution for 24 hours (to neutralise organic matter), and oven dried
 234 (40°C). Sediment was relatively homogeneous in character, comprised of predominantly coral ($72.1 \pm$
 235 0.5%), with lesser proportions of CCA ($11.5 \pm 0.4\%$) and molluscs ($9.1 \pm 0.4\%$; East, 2017). The
 236 hydraulic characteristics of sand-sized (0.063 mm – 2 mm; $-1 - 4 \phi$) sediment were measured by
 237 settling a 15 g sub-sample (obtained using a riffle splitter) through a McArthur Rapid Sediment
 238 Analyser (RSA) with a vertical fall of 1.75 m. A time-series of weight accumulation on the balance
 239 plate was recorded to calculate the settling velocity distribution (χ) and the mean settling velocity
 240 (cm s^{-1} ; Table A3). Sediment grain size distributions were calculated using the equations of Gibbs et
 241 al. (1971) with a grain density of 1.85 g cm^{-3} .

242 The ‘currents of removal’ approach was used to calculate the Potential Mobility (PM) of each
 243 sediment sample following the methodology proposed and validated by Kench (1998). PM is defined
 244 as the proportion (%) of a sample that can be mobilised under normal (i.e. ‘fair-weather’) conditions
 245 and is calculated using wave velocity data in combination with the sediment settling velocity
 246 distributions (χ). Firstly, wave velocities at each sediment sample location were extracted from
 247 wave process model outputs and were used to calculate the mean threshold settling velocity (χ)
 248 for each sediment sample using the experimentally-derived entrainment threshold relationship for
 249 bioclastic sediments reported by Kench and McLean (1996, $R^2 = 0.93$). Secondly, the settling velocity
 250 threshold (χ) at each sample location was calculated on each settling velocity curve of the
 251 concerned sediment sample. PM is the proportion of the sample with equal or slower settling
 252 velocity than the threshold value. This approach was applied six times at each study site: for mean
 253 (V_{mean}) and maximum (V_{max}) velocities associated with MRS = +0 m, +0.5 m and +1 m. In order to
 254 visualise spatial variability, results were interpolated using a block kriging algorithm, whereby kriging
 255 was undertaken within, but not across the boundaries of, each eco-geomorphic zone (spatial
 256 resolution = 6 m).

257 4. Results

258 4.1 Contemporary process regime

259 At both sites, V_{mean} was at a maximum off the oceanward rim, before waves reached the oceanward
 260 reef crest zone ($\sim 1.18 \text{ m s}^{-1}$ and $\sim 0.70 \text{ m s}^{-1}$ at the windward and leeward sites respectively; Fig. 2,
 261 A7-A10; Table 2), and rapidly decreased within the oceanward reef crest zones ($0.39 \pm 0.02 \text{ m s}^{-1}$ and
 262 $0.08 \pm 0.01 \text{ m s}^{-1}$ at the windward and leeward sites, respectively; Table 2). There was an oceanward-
 263 lagoonward decay in V_{mean} with minimum values found off lagoonward island shorelines (0.01 m s^{-1}).
 264 Converse to the oceanward-lagoonward gradient, increases in V_{mean} were found within inter-island
 265 passages, particularly at the windward site (up to 0.75 m s^{-1}). At the leeward site, there was a slight
 266 increase in V_{mean} toward the lagoonward platform margin ($V_{mean} = 0.07 \pm 0.03 \text{ m s}^{-1}$ in the

267 lagoonward reef crest zone). Under V_{max} , trends were comparable though velocities were higher
268 with proximity to the oceanward platform margin whereby $V_{max} = 1.36 \pm 0.28 \text{ m s}^{-1}$ and $0.94 \pm 0.26 \text{ m}$
269 s^{-1} within the oceanward reef crest zones at the windward and leeward sites respectively (Fig. 2, A7-
270 A10; Table 2).

271 As a function of spatial trends in wave velocities, PM data indicated that the predominant direction
272 of sediment transport was along gradients from high PM at the oceanward reef crest to low PM at
273 the lagoonward platform margin (Fig. 3, 4, A11-A16; Table 3). At the windward site, under V_{mean}
274 benthic sediment transport occurred from the oceanward reef crest ($20.4 \pm 13.7\%$) into the
275 remainder of the oceanward environment (PM = $\sim 10\%$), through inter-island passages (up to 100%),
276 and into the lagoonward environment where sediment transport occurred in the lee of the inter-
277 island passages (up to 24%). Under V_{max} , there was greater potential for sediment mobility. Sediment
278 was transported from the oceanward environment (PM = $\sim 100\%$), through inter-island passages (PM
279 = $\sim 100\%$), and into the lagoonward sand zone (PM = $8.3 \pm 24.7\%$). The lagoonward sand zone
280 remained predominantly immobile, except in the lee of the inter-island passages (PM = up to 99%).

281 At the leeward site, PM was lower than that at the windward site. Under V_{mean} , the only potentially
282 mobilised sediment was found within the reef crest zones (average PM = up to 2%). Under V_{max} , PM
283 remained low within the lagoonward zones (average PM = up to 3%), but there was a marked
284 increase in PM of oceanward sediments. Oceanward-lagoonward sediment transport thus likely
285 occurred with progressively decreasing proportions of mobile material from the oceanward reef
286 crest zone (PM = 100%), through the oceanward sparser seagrass (PM = $97.3 \pm 8.2\%$) and dense
287 seagrass (PM = $38.3 \pm 26.3\%$) zones, and towards the oceanward sand zone (PM = $7.7 \pm 7.8\%$).

288 Differences were found in the grain size of potentially mobilised sediment between eco-geomorphic
289 zones (Fig. A15, A16). At the windward site under V_{mean} , mobilisable material was of up to medium-
290 coarse grained sand ($> \sim 1 \phi$) in the oceanward reef crest zone and up to medium-grained sand ($> \sim 1-2$
291 ϕ) across the remainder of the oceanward environment. Within the lagoonward zones, only silt-

292 sized sediment could be mobilised ($>4 \phi$). Under V_{max} , very coarse sand could be mobilised across
 293 the oceanward zones ($>-1 \phi$). In the lagoonward environment, fine to very fine sand ($>\sim 3 \phi$) and fine
 294 grade sand ($>\sim 2.5 \phi$) could be potentially mobilised in the lagoonward sand and patch zones
 295 respectively. At the leeward site under V_{mean} , only fine sand ($>\sim 2.5 \phi$) was potentially mobile. Under
 296 V_{max} , very coarse sand ($>\sim 0.7 \phi$) could be mobilised on the oceanward reef crest. There was an
 297 oceanward-lagoonward decrease in the grain size of potentially mobilised material to medium-fine
 298 sand ($>\sim 2 \phi$) in the oceanward sand zone. Within the lagoonward environment, only fine-grained
 299 material ($>\sim 1.8 \phi$) could be mobilised.

300 4.2 Future process regimes

301 Under scenarios of increased MRS, shifts in wave velocities were both non-linear and non-uniform
 302 (Table 2; Fig. 2, A7-A10). Relatively marginal increases in V_{mean} were projected at both sites (Fig. 2)
 303 with average increases of up to 0.03 m s^{-1} . However, shifts in V_{max} under increased MRS scenarios
 304 were projected to be more pronounced than those associated with V_{mean} , though also non-linear and
 305 non-uniform (Fig. 2). In the oceanward reef crest zone at the windward site, V_{max} decreased by 0.03
 306 m s^{-1} between +0 and +0.5 m MRS, and by a further 0.09 m s^{-1} between +0.5 and +1 m MRS. In the
 307 leeward site oceanward reef crest zone, shifts in V_{max} were only marginal ($\sim 0.02 \text{ m s}^{-1}$). In contrast,
 308 marked increases in V_{max} were found across the remainder of the oceanward environment, for
 309 example, V_{max} was projected to increase by $\sim 0.18 \text{ m s}^{-1}$ in the windward site rubble zone. Similarly, at
 310 the leeward site, V_{max} increased by $\sim 0.14 \text{ m s}^{-1}$ between +0 and +1 m MRS scenarios in the
 311 oceanward sand and dense seagrass zones. In the lagoonward environments, increases in V_{max} were
 312 projected to be smaller in magnitude (average increases of up to $\sim 0.08 \text{ m s}^{-1}$ between +0 and +1 m
 313 MRS).

314 Sediment PM was projected to increase under scenarios of increased MRS (Table 3; Fig. 3, 4, A11,
 315 A12). At the windward site under V_{mean} , PM was projected to increase across the oceanward zones,
 316 though in a non-linear manner. For example, increases in PM were of greater magnitude between +0

317 and +0.5 m MRS (by ~9% and ~5% within the rubble and oceanward patch zones) than between +0.5
318 and +1 m MRS (by ~1% and ~0.5%). Projected increases in PM at the windward site under V_{mean} were
319 significant between both MRS increments (+0 to +0.5 m and +0.5 to +1 m, $P = <0.0005$, Wilcoxon
320 signed ranks tests). Under V_{max} , sediment across the entirety of the windward site oceanward
321 environment attained 100% PM under both scenarios of increased MRS. Converse to PM under
322 V_{mean} , PM in the lagoonward patch zone ($22.4 \pm 26.4\%$ and $30.6 \pm 33.8\%$) was projected to exceed
323 that in the lagoonward sand zone ($15.0 \pm 29.5\%$ and $22.7 \pm 38.6\%$). However, variability remained
324 high due to high PM values within the lee of the inter-island passages (up to 100%). Under V_{max} at
325 the windward site, the projected increase in PM was significant between MRS = +0.5 and +1 m ($P =$
326 0.012), but not between MRS = +0 and +0.5 m ($P = 0.232$; Wilcoxon signed ranks tests).

327 At the leeward site under V_{mean} , shifts in PM were projected to be marginal. Indeed, the magnitude
328 of change in sediment PM under V_{mean} was significantly larger at the windward site than the leeward
329 site ($P = <0.0005$; Mann-Whitney U test). The only projected increase in sediment PM under
330 increased MRS was in the oceanward reef crest zone (to $1.8 \pm 1.7\%$ and $4.3 \pm 4.5\%$ where MRS = +0.5
331 and +1 m respectively). No significant increase in PM was thus found between +0 and +0.5 m MRS at
332 the leeward site under V_{mean} ($P = 0.135$, Wilcoxon signed ranks test). However, increases in PM were
333 significant between +0.5 and +1 m MRS ($P = 0.001$, Wilcoxon signed ranks test). Under V_{max} , PM was
334 modelled as 100% under +0.5 m and +1 m MRS in both the oceanward reef crest and sparser
335 seagrass zones. While projected shifts in PM were marginal towards the oceanward platform
336 margins, the largest increases in sediment PM were found in the remainder of the oceanward zones.
337 For example, increases in PM in the oceanward sand zone were projected to be sufficiently high that
338 they would shift the zone from one of preferential deposition (under V_{max} MRS = +0 m, $PM = 7.7 \pm$
339 7.8%) to preferential sediment transport (under V_{max} MRS = +1 m, $PM = 86.2 \pm 12.2\%$). In contrast,
340 modelled increases in average PM within the lagoonward zones under V_{max} were only marginal (up
341 to 5.3%). Under V_{max} , highly significant increases were projected in PM between both increased MRS
342 increments (+0 to +0.5 m and +0.5 to +1 m; $P = <0.0005$ in both cases, Wilcoxon signed ranks tests).

343 The magnitude of change in sediment PM was significantly greater under V_{max} than V_{mean} ($P = 0.046$;
 344 Wilcoxon signed ranks tests). In contrast to under V_{mean} , the magnitude of change in sediment PM
 345 under V_{max} was significantly larger at the leeward site than the windward site ($P = <0.0005$; Mann-
 346 Whitney U test).

347

Site	Zone	MRS = +0 m		MRS = +0.5 m		MRS = +1 m		
		Mean \pm 1 S.D.	Range	Mean \pm 1 S.D.	Range	Mean \pm 1 S.D.	Range	
Windward	V_{mean} ($m s^{-1}$)	ORC	0.28 \pm 0.05	<i>0.17 - 0.52</i>	0.29 \pm 0.05	<i>0.21 - 0.53</i>	0.31 \pm 0.05	<i>0.22 - 0.56</i>
		R	0.22 \pm 0.08	<i>0 - 0.78</i>	0.25 \pm 0.08	<i>0 - 0.77</i>	0.24 \pm 0.07	<i>0 - 0.71</i>
		OP	0.19 \pm 0.09	<i>0 - 0.61</i>	0.21 \pm 0.1	<i>0 - 0.72</i>	0.22 \pm 0.09	<i>0 - 0.67</i>
		LS	0.1 \pm 0.07	<i>0 - 0.54</i>	0.11 \pm 0.08	<i>0 - 0.45</i>	0.11 \pm 0.08	<i>0 - 0.49</i>
		LP	0.08 \pm 0.03	<i>0.03 - 0.2</i>	0.08 \pm 0.03	<i>0.04 - 0.19</i>	0.08 \pm 0.02	<i>0.04 - 0.18</i>
	V_{max} ($m s^{-1}$)	ORC	1.36 \pm 0.28	<i>0.7 - 2.55</i>	1.33 \pm 0.21	<i>0.85 - 2.29</i>	1.24 \pm 0.22	<i>0.81 - 2.17</i>
		R	0.52 \pm 0.22	<i>0 - 1.37</i>	0.64 \pm 0.23	<i>0 - 1.57</i>	0.7 \pm 0.22	<i>0 - 1.51</i>
		OP	0.51 \pm 0.25	<i>0 - 1.22</i>	0.63 \pm 0.23	<i>0 - 1.26</i>	0.67 \pm 0.27	<i>0 - 1.25</i>
		LS	0.14 \pm 0.11	<i>0 - 0.71</i>	0.18 \pm 0.12	<i>0 - 0.68</i>	0.22 \pm 0.13	<i>0 - 0.77</i>
		LP	0.14 \pm 0.05	<i>0.04 - 0.35</i>	0.15 \pm 0.04	<i>0.08 - 0.32</i>	0.17 \pm 0.04	<i>0.1 - 0.35</i>
Leeward	V_{mean} ($m s^{-1}$)	ORC	0.22 \pm 0.07	<i>0.11 - 0.47</i>	0.23 \pm 0.07	<i>0.12 - 0.46</i>	0.25 \pm 0.07	<i>0.13 - 0.44</i>
		OSS	0.12 \pm 0.01	<i>0.06 - 0.21</i>	0.12 \pm 0.01	<i>0.1 - 0.23</i>	0.13 \pm 0.02	<i>0.11 - 0.26</i>
		DSG	0.1 \pm 0.02	<i>0 - 0.4</i>	0.11 \pm 0.01	<i>0.04 - 0.34</i>	0.11 \pm 0.01	<i>0.05 - 0.19</i>
		OS	0.11 \pm 0.03	<i>0 - 0.31</i>	0.12 \pm 0.03	<i>0 - 0.29</i>	0.12 \pm 0.03	<i>0 - 0.25</i>
		LP	0.06 \pm 0.04	<i>0 - 0.33</i>	0.08 \pm 0.04	<i>0 - 0.43</i>	0.07 \pm 0.03	<i>0 - 0.29</i>
		LRC	0.07 \pm 0.03	<i>0.02 - 0.16</i>	0.07 \pm 0.03	<i>0.04 - 0.16</i>	0.08 \pm 0.03	<i>0.04 - 0.15</i>
	V_{max} ($m s^{-1}$)	ORC	0.94 \pm 0.25	<i>0.45 - 1.66</i>	0.96 \pm 0.21	<i>0.54 - 1.6</i>	0.94 \pm 0.17	<i>0.57 - 1.49</i>
		OSS	0.46 \pm 0.02	<i>0.22 - 0.97</i>	0.55 \pm 0.08	<i>0.38 - 1</i>	0.58 \pm 0.08	<i>0.42 - 0.96</i>
		DSG	0.21 \pm 0.05	<i>0 - 0.54</i>	0.34 \pm 0.07	<i>0.13 - 0.58</i>	0.38 \pm 0.06	<i>0.18 - 0.61</i>
		OS	0.2 \pm 0.04	<i>0 - 0.4</i>	0.29 \pm 0.05	<i>0 - 0.59</i>	0.34 \pm 0.05	<i>0 - 0.62</i>
	LP	0.1 \pm 0.06	<i>0 - 0.4</i>	0.15 \pm 0.07	<i>0 - 0.62</i>	0.18 \pm 0.08	<i>0 - 0.66</i>	
	LRC	0.13 \pm 0.07	<i>0.05 - 0.33</i>	0.15 \pm 0.08	<i>0.06 - 0.39</i>	0.16 \pm 0.09	<i>0.07 - 0.42</i>	

348

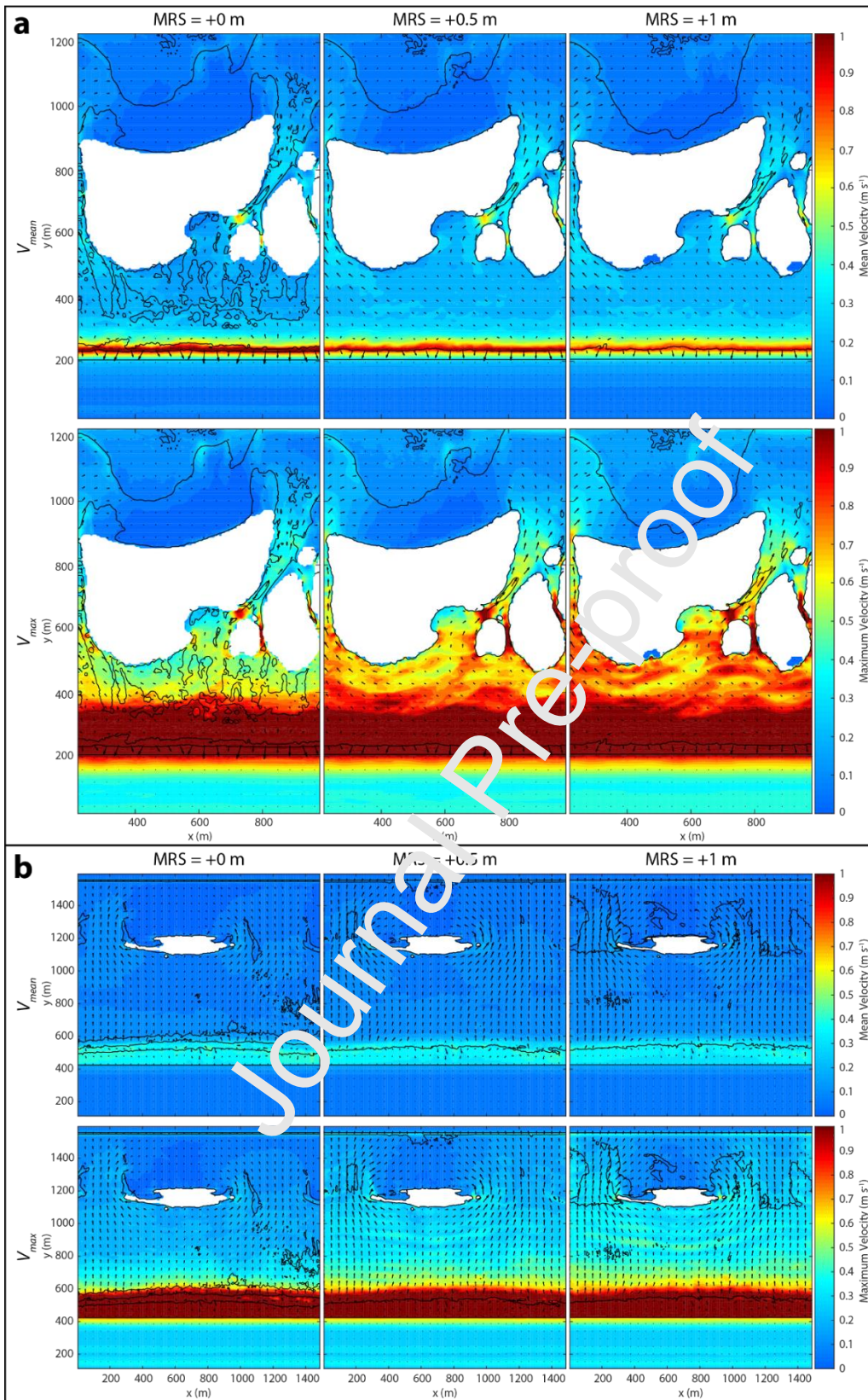
349 Table 2 – Mean (V_{mean}) and maximum (V_{max}) wave velocities ($m s^{-1}$, mean \pm 1 S.D., ranges in italics)
 350 within each eco-geomorphic zone where SLR = 0, 0.5 and 1 m. At the windward site, LP =
 351 lagoonward patch, LS = lagoonward sand, OP = oceanward patch, R = rubble, and ORC = oceanward
 352 reef crest. At the leeward site, LRC = lagoonward reef crest, LP = lagoonward patch, OS = oceanward
 353 sand, DSG = dense seagrass, OSS = oceanward sparser seagrass, and ORC = oceanward reef crest.

Site	Zone	MRS = +0 m		MRS = +0.5 m		MRS = +1 m		
		Mean \pm 1 S.D.	Range	Mean \pm 1 S.D.	Range	Mean \pm 1 S.D.	Range	
Windward	V_{mean} (PM, %)	ORC	20 \pm 13.7	<i>2 - 51</i>	27.4 \pm 14.6	<i>7 - 54</i>	37.9 \pm 20.8	<i>8 - 80</i>
		R	10.3 \pm 20.7	<i>0.5 - 84</i>	19.2 \pm 20.8	<i>3 - 89</i>	20.4 \pm 21.3	<i>5 - 93</i>
		OP	11 \pm 23.7	<i>0 - 100</i>	16.2 \pm 22.9	<i>0 - 100</i>	16.8 \pm 23.2	<i>0 - 100</i>
		LS	1.5 \pm 6	<i>0 - 24</i>	1.2 \pm 4.5	<i>0 - 18</i>	0.8 \pm 2.1	<i>0 - 7</i>
		LP	0.3 \pm 0.7	<i>0 - 2</i>	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>
	V_{max} (PM, %)	ORC	100 \pm 0	<i>100 - 100</i>	100 \pm 0	<i>100 - 100</i>	100 \pm 0	<i>100 - 100</i>
		R	99.9 \pm 0.2	<i>99.5 - 100</i>	100 \pm 0	<i>100 - 100</i>	100 \pm 0	<i>100 - 100</i>
		OP	96.9 \pm 12.6	<i>48 - 100</i>	100 \pm 0	<i>100 - 100</i>	100 \pm 0	<i>100 - 100</i>
		LS	8.3 \pm 24.7	<i>0 - 99</i>	15 \pm 29.5	<i>0 - 99.5</i>	22.7 \pm 38.6	<i>0 - 100</i>
		LP	23.5 \pm 30.2	<i>0 - 83</i>	22.4 \pm 26.4	<i>0 - 60</i>	30.6 \pm 33.8	<i>0 - 85</i>
Leeward	V_{mean} (PM, %)	ORC	1.5 \pm 1.3	<i>0 - 4</i>	1.8 \pm 1.7	<i>0.5 - 5.5</i>	4.3 \pm 4.5	<i>0.5 - 18</i>
		OSS	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>
		DSG	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>
		OS	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>
		LP	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>	0 \pm 0	<i>0 - 0</i>
		LRC	1.7 \pm 4.2	<i>0 - 15</i>	1.7 \pm 4.2	<i>0 - 15</i>	1.7 \pm 4.2	<i>0 - 15</i>
	V_{max} (PM, %)	ORC	100 \pm 0	<i>100 - 100</i>	100 \pm 0	<i>100 - 100</i>	100 \pm 0	<i>100 - 100</i>
		OSS	97.3 \pm 8.2	<i>68 - 100</i>	100 \pm 0	<i>100 - 100</i>	100 \pm 0	<i>100 - 100</i>
		DSG	38.3 \pm 26.3	<i>4 - 95</i>	27 \pm 20.0	<i>40 - 100</i>	95.3 \pm 7.5	<i>76 - 100</i>
		OS	7.7 \pm 7.8	<i>1.5 - 50</i>	14.9 \pm 23.1	<i>0 - 83</i>	86.2 \pm 12.2	<i>54 - 100</i>
		LP	0 \pm 0	<i>0 - 0</i>	0.6 \pm 1.5	<i>0 - 5</i>	5.3 \pm 15.4	<i>0 - 60</i>
LRC	2.8 \pm 5.3	<i>0 - 15</i>	3.1 \pm 6.2	<i>0 - 20</i>	3.8 \pm 8.3	<i>0 - 30</i>		

354

355 Table 3 – Potential Mobility (PM, %, mean \pm 1 S.D., ranges in italics) of sediment within each eco-
356 geomorphic zone where SLR = 0, 0.5 and 1 m. Note that marked spatial variability exists within each
357 zone. At the windward site, LP = lagoonward patch, LS = lagoonward sand, OP = oceanward patch, R
358 = rubble, and ORC = oceanward reef crest. At the leeward site, LRC = lagoonward reef crest, LP =
359 lagoonward patch, OS = oceanward sand, DSG = dense seagrass, OSS = oceanward sparser seagrass,
360 and ORC = oceanward reef crest.

361

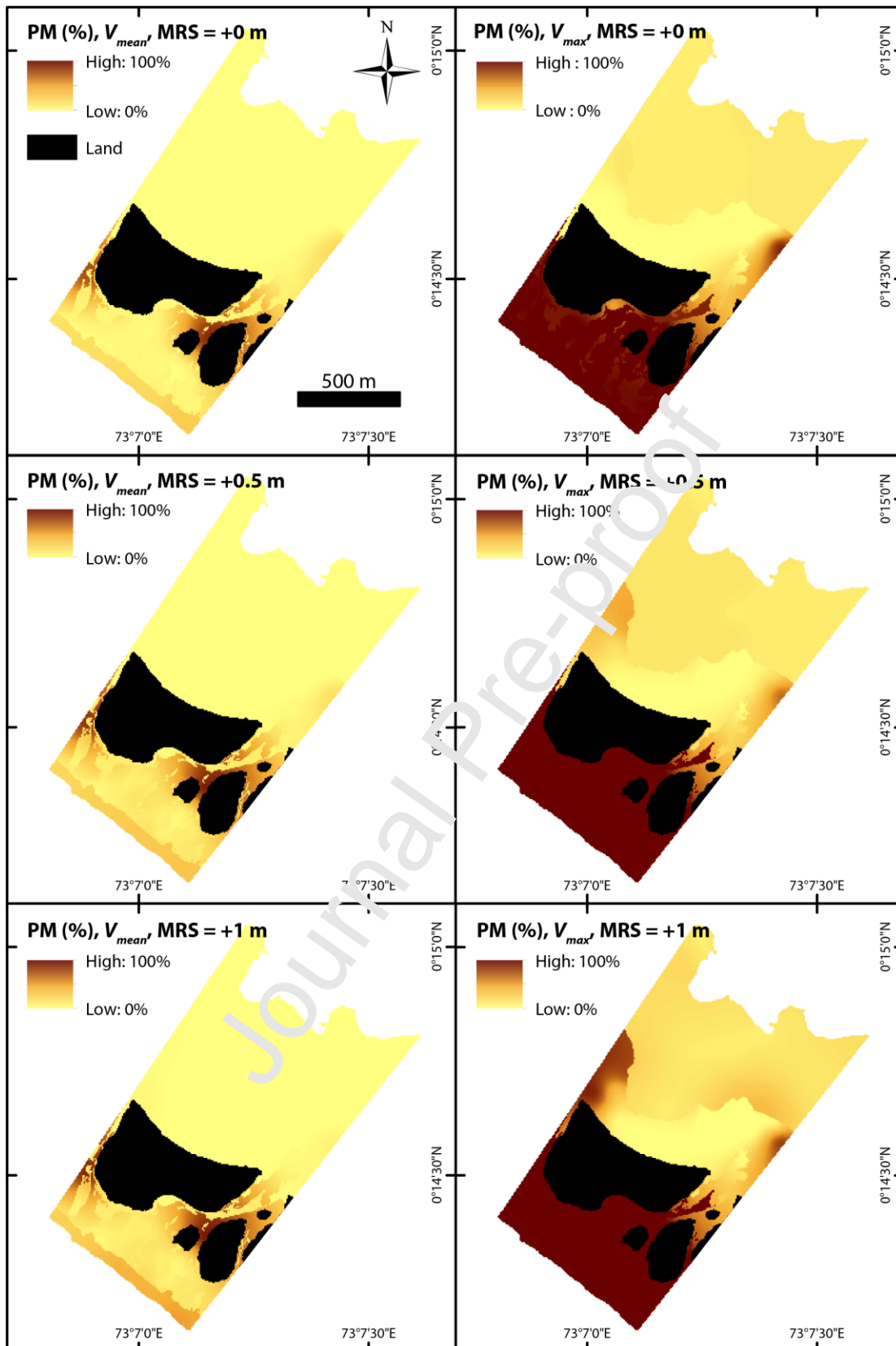


362

363 Figure 2 – Mean (V_{mean}) and maximum (V_{max}) velocities ($m s^{-1}$) across the windward (a) and leeward

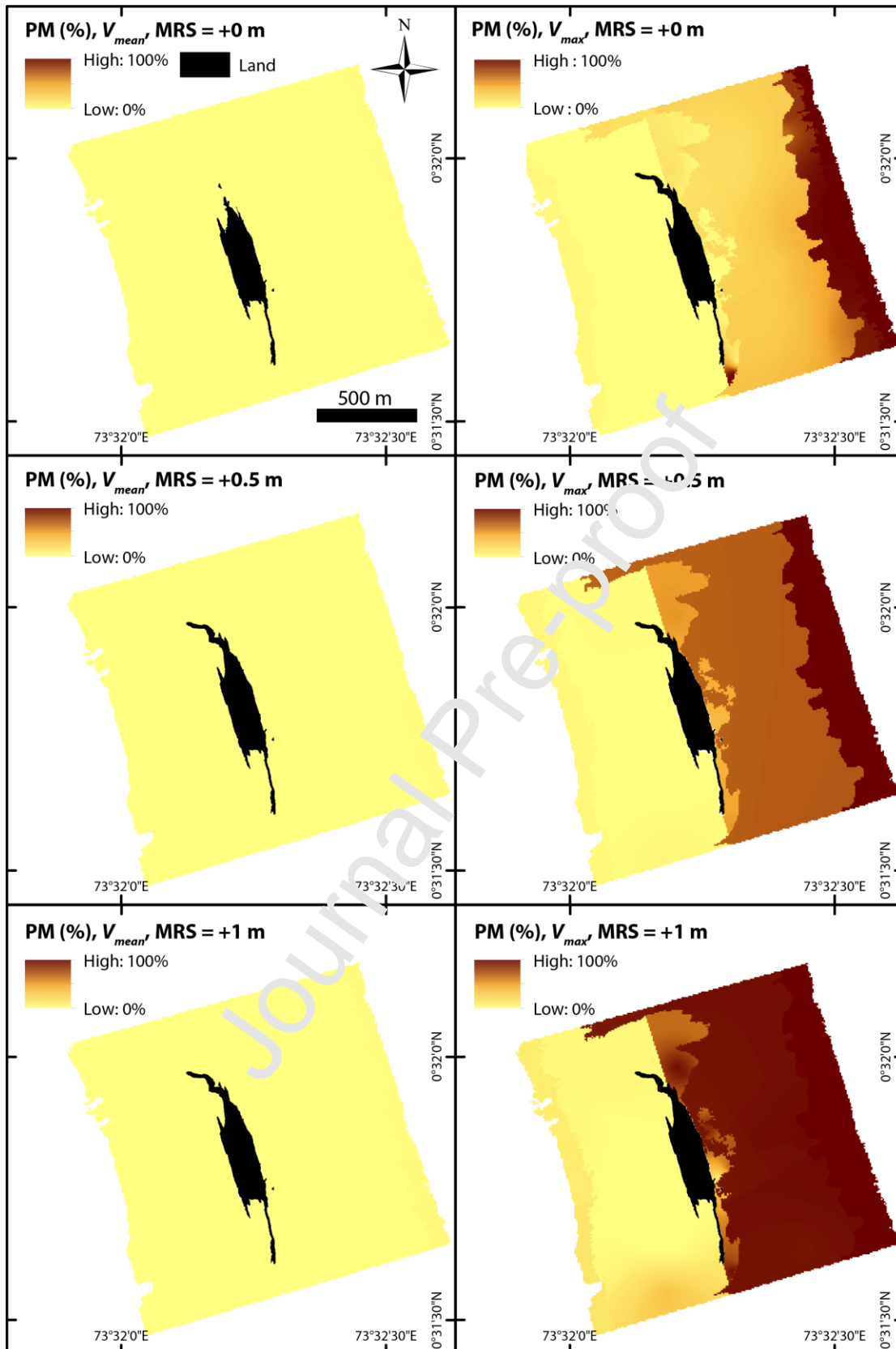
364 (b) sites where MRS = +0 m, +0.5 m, and +1 m. Vectors represent the direction and magnitude of the

365 velocity plotted in each panel. (**Width = 2 columns**)



366

367 Figure 3 – Windward site block kriging results of sediment potential mobility (PM, %) with both
 368 mean (V_{mean}) and maximum (V_{max}) velocities under scenarios of +0 m, +0.5 m, and +1 m MRS. (**Width**
 369 = 2 columns)



370

371 Figure 4 – Leeward site block kriging results of sediment potential mobility (PM, %) with both mean
 372 (V_{mean}) and maximum (V_{max}) velocities under scenarios of +0m, +0.5 m, and +1 m MRS. (**Width = 2**
 373 **columns**)

374 5. Discussion

375 5.1 Wave processes

376 Wave processes under the contemporary process regime were characterised by a general cross-rim
377 oceanward-lagoonward attenuation of wave velocities. Under scenarios of increased reef
378 submergence, changes in wave processes were non-linear and non-uniform, with the magnitude of
379 change varying between zones and between increased MRS projections. These findings contrast
380 widely-held assumptions that wave energy will increase linearly with sea level rise (Ferrario et al.,
381 2014; Quataert et al., 2015). Rather, our results highlight the complex nature of atoll rim process
382 regimes.

383 Results suggest that wave velocities will decrease or remain constant within the oceanward reef
384 crest zones under increasing reef submergence. This is likely driven by a decrease in dissipation
385 during wave breaking, with higher submergence allowing a wider surf zone to develop across the
386 outer reef flat. In contrast, under increased MRS, pronounced increases in velocities were projected
387 across reef flats, driven by an increase in wave height and velocities able to propagate across the
388 outer reef crest. This is primarily attributed to a decrease in dissipation from breaking at the reef
389 crest whereby greater water depths enable a larger proportion of incident wave energy to propagate
390 onto the reef flats. In some instances, this may allow larger waves to cross the reef crest without
391 breaking and greater energies to 'leak' onto the reef platform surface (Brander et al., 2004; Kench et
392 al., 2009a). Indeed, between MRS = +0m and +1m, there was 63% and 253% increase in average
393 wave energy on the reef flat at the windward and leeward sites respectively. In addition, higher
394 submergence decreases hydrodynamic roughness relative to water depth which limits frictional
395 dissipation across the reef flat (Storlazzi et al., 2011). Decreases in live coral cover can also cause
396 reductions in surface rugosity, which may cause further reductions in the frictional dissipation of
397 waves (Harris et al., 2018). Mean velocities, driven by spatial differences in wave setup, are
398 predicted to decrease across the reef flat as wave dissipation at the reef crest is reduced. The net

399 effect of increasing reef submergence is that sediment transport processes will increase across the
400 reef flat because of higher wave orbital velocities, with mean flow a less important control on
401 sediment transport during modal wave conditions.

402 While depth-averaged currents are presented, they are not necessarily representative of the
403 currents that interact with the bed in reef systems (i.e. the reef canopy causes a reduction in
404 velocity; Pomeroy et al., 2017). Cuttler et al. (2018) and Pomeroy et al. (2018) have discussed the
405 contributions of different forcing (wave-driven or mean current) to sediment transport in reef
406 systems and highlight the importance of wave-driven processes for inducing reef sediment
407 transport.

408 **5.2 Sediment Potential Mobility**

409 Under the contemporary process regime ($MRS = +0.1$), there was minimal potential for sediment
410 mobility where mean velocities were considered. However, extracting maximum velocities shows
411 that active oceanward-lagoonward sediment transport occurs at both sites, even under fair-weather
412 conditions. This potentially mobilised material comprised sand-sized sediments (Fig. A15, A16),
413 which are of the same grade as sediments within the upper horizons of the adjacent reef islands
414 (East et al., 2016; 2018). Hence, our findings suggest that active sedimentary linkages exist between
415 reef islands and their adjacent marine environments under fair-weather conditions.

416 While data suggest there is active reef-to-island connectivity, it is pertinent to note that the
417 windward islands are underpinned by conglomerate platforms (~0.4 m above MSL on their
418 oceanward shorelines (East et al., 2018)). While sediment PM was high across the windward site
419 oceanward zones, the transfer of sediments to oceanward island shorelines may be ineffective
420 under present conditions as sediments would need to bypass the conglomerate platform. However,
421 this may change as sea levels rise because (1) the beach will become more connected to the process
422 regime; and (2) shoreline materials may be mobilised more readily.

423 At the windward site sediment PM was 100% across almost the entirety of the oceanward
424 environment under V_{max} . Hence, under present conditions, this site represents a sediment-limited
425 setting (Kench and McLean, 2004) whereby there is a highly efficient and continuous oceanward-
426 lagoonward transfer of all available sediments. As such, the windward site oceanward reef flat zones
427 are generally swept bare of island building (sand-grade; East et al., 2016) sediments. In contrast,
428 under present conditions, the leeward site represents a transport-limited setting where wave
429 energies are insufficient to enable the transfer of sediments from oceanward to lagoonward zones.
430 Hence, the oceanward reef flat zones at the leeward site were characterised by the widespread
431 accumulation of sand-sized sediments.

432 At the windward site, the one exception to the near-unanimously high PM values (~100%) across the
433 oceanward environment was in the embayment area on the central transect where PM = 48%,
434 suggesting that the embayment may represent a depositional sink for medium-to-fine grained sand.
435 This is consistent with shoreline geomorphology, as this was the only portion of the oceanward island
436 shoreline to be composed of sand-sized sediments, while the remainder of the oceanward island
437 margins were comprised of reef rubble and coral boulders. Sediment PM analysis thus provides
438 support for the process of embayment infilling which has been identified as a key mechanism of
439 shoreline accretion in other regions with similar island morphologies (Kench et al., 2015) and has
440 been hypothesized to have occurred within the windward study site (East et al., 2018).

441 The modelled spatial variability in sediment potential mobility contrasts with that found on faro type
442 reef platforms in the Maldives (Vabbinfaru, North Malé Atoll). Morgan and Kench (2016) found the
443 highest PM values were associated with lagoonal deposits, whereas coarser outer reef rim
444 sediments had lower PM values. This contrasts to the trends found in the present study, in which PM
445 was highest toward the oceanward platform rim and lowest within the lagoonward zones. Such
446 differences are a function of the higher wave velocities (as opposed to differences in sediment
447 texture) found on the atoll rim (maximum wave velocities on Vabbinfaru = 0.29 m s^{-1} ; Morgan and

448 Kench, 2016). Indeed, the oceanward margins of atoll rim platforms are exposed to open ocean
449 swell, whereas locally-generated wind-driven waves are incident around faro type platform margins.
450 Hence, we highlight the diversity of atoll reef platform process regimes, even at intra-regional scales.
451 Under scenarios of increased MRS, the non-linearity and non-uniformity of the shifts in wave
452 processes with increased MRS, were mirrored by changes in sediment PM whereby marked inter-
453 and intra-site variability was found in the magnitude of change. Nonetheless, the predominant
454 oceanward-lagoonward sediment transport pathways remained consistent between MRS scenarios.
455 Notably, under V_{max} , the increase in sediment PM at the leeward site was significantly larger than at
456 the windward site. This is due to the highly exposed nature of the windward setting whereby PM
457 was almost uniformly at 100% under contemporary conditions across the oceanward environment
458 and, hence, there is minimal potential for further increases. That is, the windward site is already a
459 sediment-limited setting. In contrast, under increased MRS, the leeward site was characterised by
460 the transition from a transport-limited to a more sediment-limited setting. This between-site
461 variability in shifts in sediment PM under MRS scenarios highlights that reef island responses to
462 future environmental change are likely to be diverse, even over local scales. Notably, while PM
463 remained relatively consistent under increased MRS at the oceanward platform margins, the largest
464 increases in PM were found across the remainder of the oceanward zones. Such inner reef flat zones
465 are those immediately adjacent to oceanward island shorelines, which has important implications
466 for future island stability.

467 **5.3 Geomorphic implications**

468 A crucial consequence of the projected shifts in wave process regime under SLR, is the potential
469 increase in energy delivered to reef island shorelines (Ogston and Field, 2010; Storlazzi et al., 2011;
470 Beetham et al., 2016). Higher wave energies may increase rates of shoreline erosion with reworked
471 sediment transferred back into the marine environment (Storlazzi et al., 2011). In addition, with
472 projected increases in the PM of marine sediments, islands may be recipients of increased volumes

473 of sediment, resulting in shoreline accretion. Indeed, the increases in mobility were of sand-sized
474 sediments (Fig. A15, A16) and thus of an appropriate grade to contribute to island building. Notably,
475 under all scenarios of reef submergence, the lagoonward areas remained as depositional sinks
476 characterised by the limited capacity of hydrodynamics to entrain sediment. This continued capacity
477 for the storage and accumulation of sand-sized sediment highlights the potential for rim reef islands
478 to persist under increased reef submergence.

479 While the mobility of reef island sediments was not investigated directly, our results have clear
480 implications for predicting reef island landform change. Reef islands will continually adjust with
481 shifts in the process regime of the type our model outputs suggest (Beetham and Kench, 2014).
482 Under both scenarios of increased MRS, benthic areas immediately adjacent to the oceanward
483 shorelines of both islands shifted from areas of preferential sediment deposition (i.e. storage) to
484 preferential transport. Hence, erosion will likely occur along these shorelines. Conversely, benthic
485 areas immediately lagoonward of island shorelines remained areas of preferential deposition in both
486 settings. This implies that sediment may thus be removed from oceanward areas and subsequently
487 deposited in the lagoonward environment. This deposited material may either remain below MSL as
488 a benthic deposit or it may attain elevations above MSL, contributing to island accretion. Island
489 accretion may occur via two key mechanisms: (1) 'roll-around' whereby alongshore sediment fluxes
490 facilitate oceanward-lagoonward sediment transport and subsequent alongshore deposition; and/or
491 (2) 'roll-over' as material from the oceanward coast is eroded and deposited towards the lagoon
492 (Woodroffe et al., 1999). Both processes of roll-around and roll-over could thus result in both
493 horizontal and vertical lagoonward island accretion and thus net island migration. Hence, we
494 hypothesize that increases in MSL may result in lagoonward island migration.

495 This hypothesis that increased MRS may drive lagoonward island migration is consistent with several
496 lines of evidence: (1) Analyses of island shoreline evolution over decadal timescales have found
497 island lagoonward migration to occur under SLR. For example, following analyses of all 101 islands of

498 Tuvalu, Kench et al. (2018) suggested there was compelling evidence that SLR was causing the
499 lagoonward migration of atoll rim islands. Similarly, at Funafuti Atoll, which has experienced some of
500 the highest rates of SLR ($\sim 5.1 \pm 0.7 \text{ mm yr}^{-1}$), the predominant direction of island migration was
501 lagoonwards (Kench et al., 2015). Furthermore, Aslam and Kench (2017) analysed shoreline island
502 change on 184 islands in Huvadhu atoll and found lagoonward migration of rim islands to be the
503 second most common mode of island change. Hence, whilst Aslam and Kench have quantified island
504 evolution, here we are able to examine the process mechanism that drives this mode of reef island
505 change. (2) Analytical modelling of reef island futures under SLR and shifts in sediment supply found
506 that island lagoonward migration occurred under all SLR scenarios (Cowell and Kench, 2001; Kench
507 and Cowell, 2001). (3) Palaeo-reconstructions of island evolution within the present study sites
508 (based on 28 core records and 40 AMS radiocarbon dates) reveal notable parallels between the
509 suggestions of future and former island roll-over and roll-around (East et al., 2018). Specifically, roll-
510 over and roll-around were identified as key modes of reef island formation at these sites, likely
511 controlled by higher than present sea levels associated with the mid-Holocene sea-level highstand
512 (Kench et al., 2009b). Hence, results of sediment PM analysis under increased MRS provide support
513 for the suggestion that SLR could lead to a reactivation of the process regime responsible for reef
514 island formation. In turn, future SLR could potentially induce further island building and
515 remobilisation.

516 Processes of island roll-around and roll-over would likely be most prevalent at the leeward site. This
517 is because the increase in sediment PM under increased MRS was significantly larger at the leeward
518 site than at the windward site. Hence, leeward rim islands will likely become more mobile under
519 both scenarios of increased MRS than their windward counterparts. This suggestion is supported by
520 prior work within the present study sites which has shown the leeward site islands have been more
521 mobile than their windward counterparts over both millennial (East et al., 2018) and decadal (Aslam
522 and Kench, 2017) timescales. In addition, numerical modelling of atoll reef island shorelines under
523 SLR in the Pacific has suggested that lagoonward migration of leeward atoll islands may occur under

524 scenarios of increased wave energy (Shope et al., 2017). We thus suggest that reef island future
525 landform trajectories may be diverse and site-specific, even over local scales. The approach we
526 present in this study provides a useful tool for investigating such trajectories of reef island systems.
527 Whilst the findings of this study imply that reef islands may persist into the future, it is pertinent to
528 note several caveats to this prognosis. Firstly, the continued transport of sediment to reef island
529 shorelines is largely contingent upon continued sediment production. Carbonate-producing
530 organisms living in the adjacent reef environments represent the sole sediment source in atoll reef
531 platform settings and thus any shift in reef ecology, and in the ecological morphic zones described in
532 this study, will induce shifts in the rates and types of sediment production. This poses a particular
533 challenge as coral reefs face a range of threats under climate change, including increases in ocean
534 acidity and sea surface temperatures (IPCC, 2019). In the absence of continued sediment production,
535 island persistence would be contingent upon the continued storage and adjustment of a finite
536 volume of sediment. Secondly, whilst increased rates of island migration may enable the physical
537 persistence of reef islands, such shifts in island planform will likely pose a challenge to the
538 infrastructure and communities living in reef island nations. Thirdly, the present study investigates
539 hydrodynamic processes and sediment transport under conditions associated with the upper
540 confidence limits at the end of this century (Perry et al., 2018), however the upper limit of SLR
541 projections by 2,300 are substantially higher (up to 5.4 m under RCP8.5; IPCC, 2019).

542 **6. Conclusion**

543 We present projections of reef hydrodynamics and benthic sediment transport under MRS scenarios
544 in an atoll reef island setting. Under the fair-weather contemporary process regime, this work
545 indicates that benthic sediment transport is occurring on atoll rim platforms with likely active reef-
546 to-island sediment connectivity. Under conditions of increased MRS, shifts in wave processes and
547 sediment potential mobility were non-linear and non-uniform, counter to general assumptions that
548 reef systems will respond linearly to environmental change. Significant between-site differences

549 were found in shifts in sediment PM under increased MRS, which implies that reef system, and in
550 turn reef island, morphological responses to future increases in MRS are likely to be diverse and site-
551 specific, even over local scales. As shifts in sediment PM were significantly larger in magnitude on
552 the leeward rim than on the windward rim, we suggest that geomorphic shifts will be most
553 pronounced on the leeward rim. Under increased MRS, both wave velocities and sediment PM
554 decreased or remained constant at the oceanward platform margins, whereas the largest increases
555 were found on the inner reef flat. The lagoonal zones were projected to remain as sinks for sediment
556 deposition under increased MRS. Due to the coupling of increased sediment PM adjacent to
557 oceanward island shorelines and low sediment PM adjacent to lagoonward island shorelines, we
558 hypothesize that lagoonward reef island migration will occur under increased MRS. These findings
559 have implications for predicting the future adaptive capacity of atoll nations globally. Specifically, the
560 challenge is to incorporate such potential increases in island mobility and intra-regional diversity in
561 reef system geomorphic responses to sea level rise into national-scale vulnerability assessments.

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Journal Pre-proof

772 Conflicts of interest: none

Journal Pre-proof

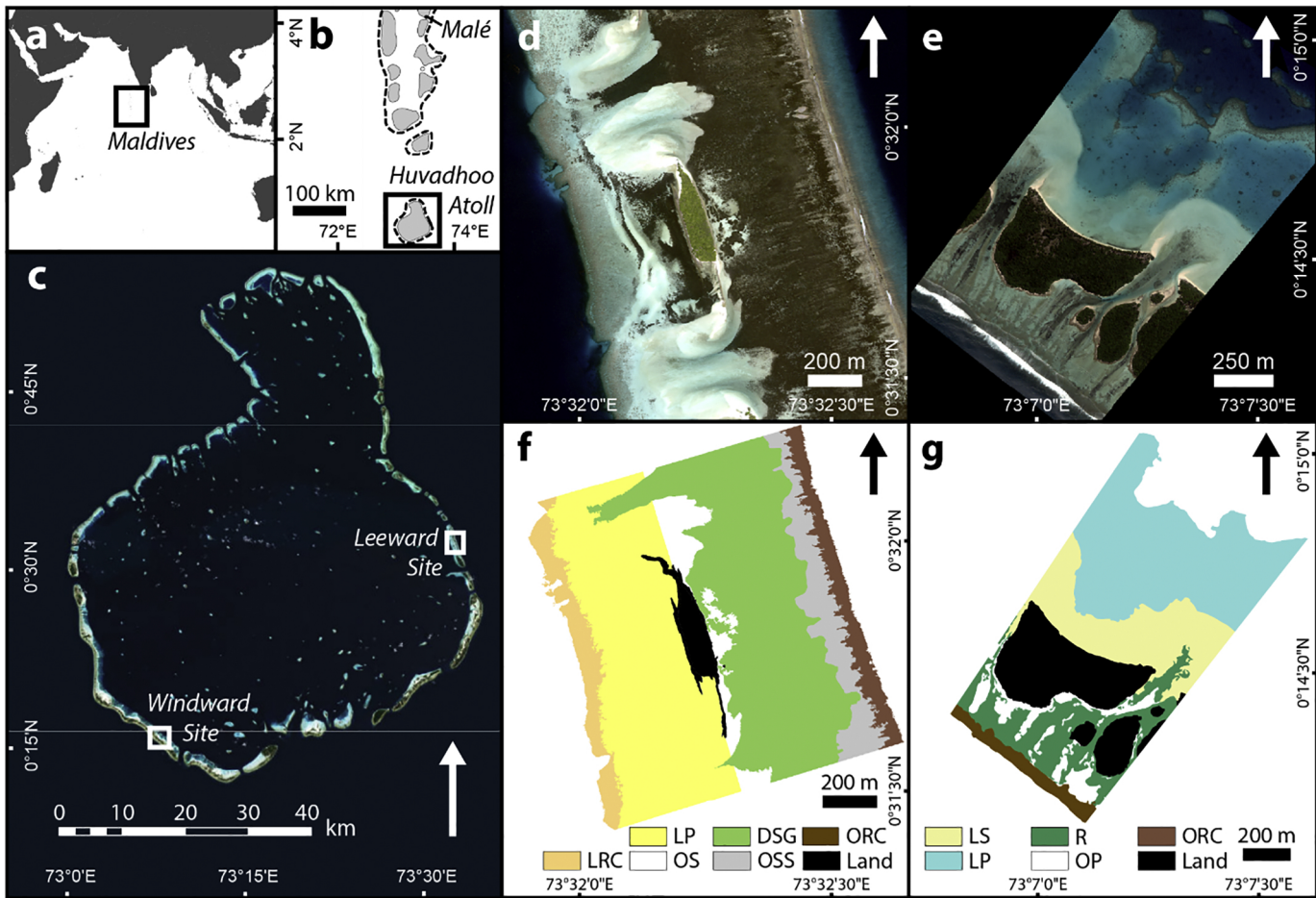


Figure 1

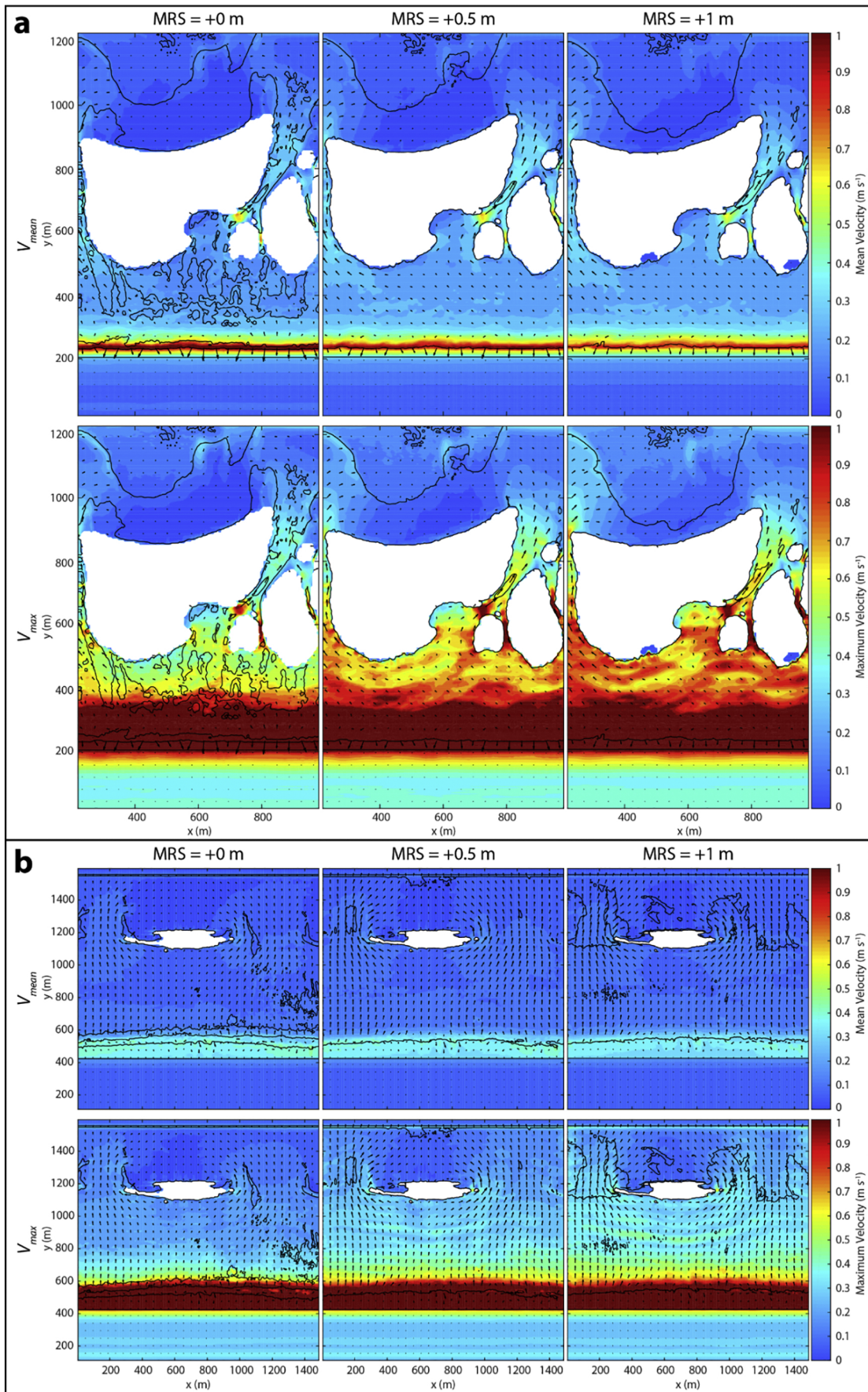


Figure 2

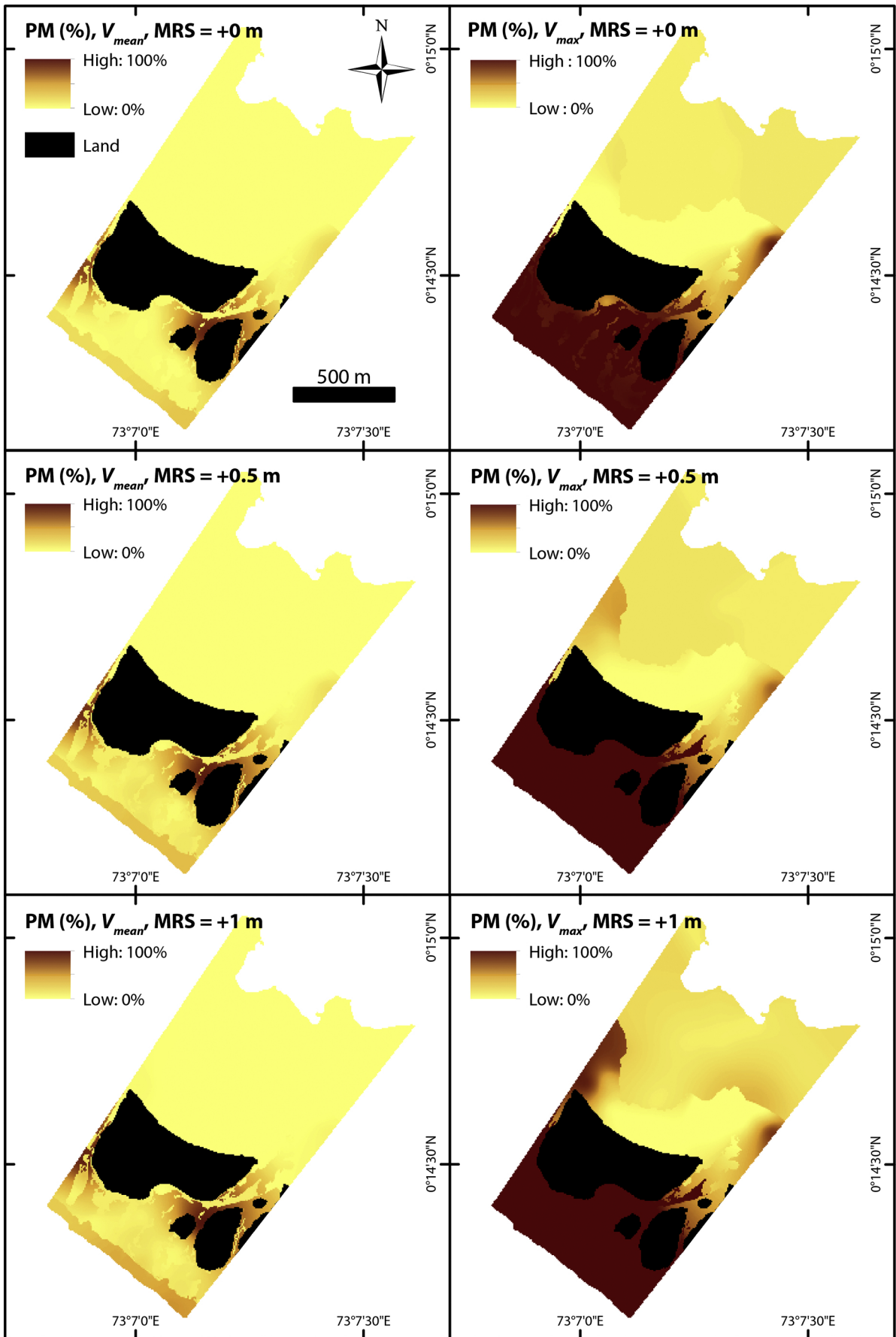


Figure 3

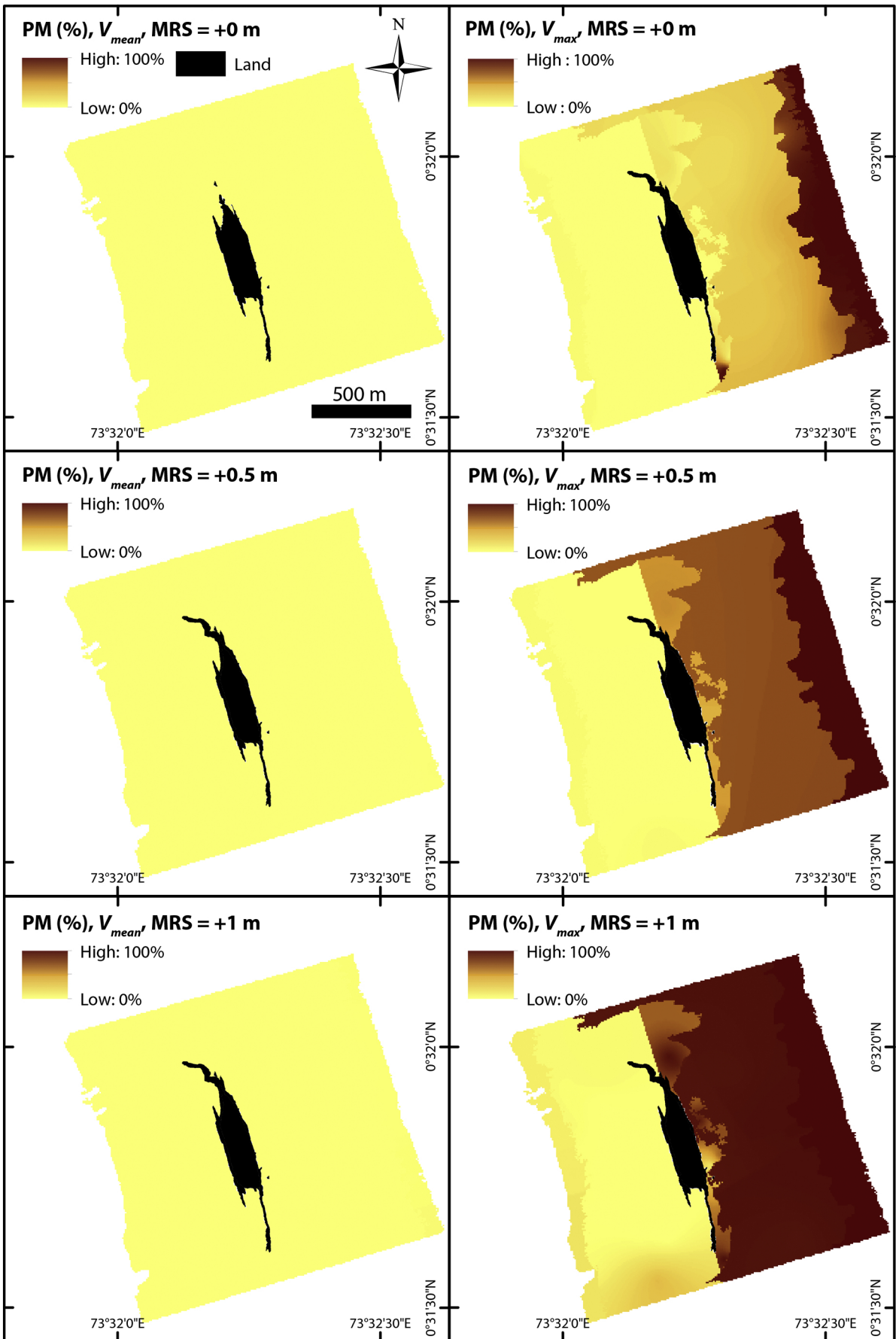


Figure 4